

# Function- and Data Sheet

Extent shown:  
Blocks chosen: ABK, APP, FB, FDEF, FW

System: SG ME7.3H  
Project: ME 7.3.1H Alfa 2.0l BTS  
Project code: 9/633.3;16  
Release:

Responsible: Martin Enz  
Department: K3/EAF1  
Phone: 20873  
Date of issue: 20.07.2000

program release: 07E0 (Predecessor : 07C0)



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1181	ANALUN	number of combustions for deactivation after detected misfire
1181	ATMABKA	factor reduction of exhaust gas temperature = f(soak time)
1181	ATMABKK	factor reduction for catalyst temperature = f(soak time)
1181	ATMTANS	temperature correction of the exhaust model temperature
1181	AZKELDYN	ignition per cylinder for load dynamics => knock detection
1181	AZKRLDYN	number of ignition per cyl. during knock control load dynamic
1181	AZKRDYDYN	number of ignition for knock control engine speed dynamic
1181	BRABEVI	acceleration at accelerating ramp
1181	BTRKHTMS	Characteristic enabling flag B_trkh
1181	CDCCAS	code word CARB: CAN interface, timeout ASC
1181	CDCCINS	code word CARB: CAN interface, timeout instrument
1181	CDCKKUP	code word CARB: CAN-bus, timeout clutch
1181	CDCEV1	code word CARB: injector 1
1181	CDCEV2	code word CARB: injector 2
1181	CDCEV3	code word CARB: injector 3
1181	CDCEV4	code word CARB: injector 4
1181	CDCEV5	code word CARB: injector 5
1181	CDCEV6	code word CARB: injector 6
1181	CDCEV7	code word CARB: injector 7
1181	CDCEV8	code word CARB: injector 8
1181	CDCFRAO	code word CARB: mixture adaptation factor frao
1181	CDCFRAO2	code word CARB: mixture adaptation factor frao bank 2
1181	CDCFRAU	code word CARB: mixture adaptation factor frau
1181	CDCFRAU2	code word CARB: mixture adaptation factor frau bank 2
1181	CDCFRST	code word CARB: deviation of lambda closed loop control
1181	CDCFRST2	code word CARB : deviation of lambda closed loop control bank 2
1181	CDCHSH	code word CARB: lambda sensor heating downstream cat
1182	CDCHSH2	code word CARB: lambda sensor heating downstream cat
1182	CDCHSV	code word CARB: lambda sensor heating upstream cat
1182	CDCHSV2	code word CARB: lambda sensor heating upstream cat; (bank2)
1182	CDCHSVE	code word CARB: lambda sensor heating power stage upstream cat
1182	CDCHSVE2	code word CARB: lambda sensor heating2 power stage upstream cat
1182	CDCKAT	code word CARB: catalyst conversion
1182	CDCKAT2	code word CARB: catalyst conversion, cyl.row 2
1182	CDCKPE	Code word CARB: fuel pump relay power stage
1182	CDCKRNT	code word CARB: knock control zero test pulse
1182	CDCKROF	code word CARB: knock control offset
1182	CDCKRTP	code word CARB: knock control test pulse
1182	CDCKS1	code word CARB: knock sensor 1
1182	CDCKS2	code word CARB: knock sensor 2
1182	CDCKS3	code word CARB: knock sensor 3
1182	CDCKS4	code word CARB: knock sensor 4
1182	CDCLASH	code word CARB: lambda sensor aging downstream cat
1182	CDCLASH2	code word CARB: lambda sensor aging downstream cat, Cyl.row 2
1182	CDCLATP	code word CARB: lambda sensor aging tp
1182	CDCLATP2	code word CARB: lambda sensor aging tp, cyl. row 2
1182	CDCLATV	code word CARB: lambda sensor aging tv
1182	CDCLATV2	code word CARB: lambda sensor aging tv, cyl.row 2
1182	CDCLSH	code word CARB: lambda sensor downstream catalyst
1182	CDCLSH2	code word CARB: lambda sensor downstream catalyst
1182	CDCLUEA	code word CARB: Power stage engine fan A
1182	CDCLUEB	Code word CARB: Power stage engine fan B
1182	CDCMD	Code word CARB: misfire, multiple
1182	CDCMD00	Code word CARB: misfire cyl. 0
1182	CDCMD01	Code word CARB: misfire cyl. 1
1183	CDCMD02	Code word CARB: misfire cylinder 2
1183	CDCMD03	Code word CARB: misfire cylinder 3
1183	CDCMD04	Code word CARB: misfire cylinder 4
1183	CDCMD05	Code word CARB: misfire cylinder 5
1183	CDCMD06	Code word CARB: misfire cylinder 6
1183	CDCMD07	Code word CARB: misfire cylinder 7
1183	CDCMD08	Code word CARB: misfire cylinder 8
1183	CDCMD09	Code word CARB: misfire cylinder 9
1183	CDCMD10	Code word CARB: misfire cylinder 10
1183	CDCMD11	Code word CARB: misfire cylinder 11
1183	CDCMDB	Code word CARB: Target torque limiter
1183	CDCMILE	Code word CARB: MIL power stage
1183	CDCNWKW	code word CARB: alignment between camshaft and crankshaft
1183	CDCNWKW2	code word CARB: alignment between camshaft 2 and crankshaft
1183	CDCNWS	code word CARB: camshaft control
1183	CDCNWS2	code word CARB: camshaft control bank 2
1183	CDCPH	code word CARB: phase sensor
1183	CDCPH2	code word CARB: phase sensor 2
1183	CDCRKAT	code word CARB: additive adaptive mixture correction rkcat
1183	CDCRKAT2	code word CARB: additive adaptive mixture correction rkcat bank 2
1183	CDCRKAZ	code word CARB: additive adaptive mixture correction rkaz
1183	CDCRKAZ2	code word CARB: additive adaptive mixture correction rkaz bank 2
1183	CDCTA	code word CARB: intake air temperature
1183	CDCTES	code word CARB: canister purge system
1183	CDCTEVE	code word CARB: canister purge valve power stage



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1183	CDCTM	code word CARB: engine coolant temperature TMOT
1183	CDCUB	code word CARB: battery voltage UB (onboard)
1183	CDCUF2SG	Code word CARB: monitoring of the function: data from other ECU
1184	CDCUFMV	Code word CARB: monitoring of the function: torque comparison
1184	CDCUFSKA	Code word CARB: monitoring of the function: safety fuel cut-off
1184	CDCURRAM	Code word CARB: monitoring of the controller: RAM
1184	CDCURROM	Code word CARB: monitoring of the controller: ROM
1184	CDCURRST	Code word CARB: monitoring of the controller: Reset
1184	CDCVKUP	code word CARB: electr. clutch, speed dependent
1184	CDLFRAO	code word lamp : LR-Adaptation multiplicative upper threshold
1184	CDLFRAO2	code word lamp : LR-Adaptation multiplicative upper threshold bank 2
1184	CDLFRAU	code word lamp: LR-Adaptation multiplicative lower threshold
1184	CDLFRAU2	code word lamp: LR-Adaptation multiplicative lower threshold bank 2
1184	CDLFRST	code word lamp: feul supply system short test
1184	CDLFRST2	code word lamp: feul supply system short test bank 2
1184	CDLRKAT	code word lamp : LR-Adaptation additive per time
1184	CDLRKAT2	code word lamp : LR-Adaptation additive per time bank 2
1184	CDLRKAZ	code word lamp : LR-Adaptation additive per ignition
1184	CDLRKAZ2	code word lamp : LR-Adaptation additive per ignition bank 2
1184	DECKSTAI	decrement-step for STADAP-factor
1184	DEVTMAGR	offset for evtmod depending on tsges_w at high tans caused by EGR
1184	DFPSLBIT	Section bits for indication of the activated error paths
1184	DFSEFO2N	max. plausible speed-dependent variance of FSE values
1184	DFSEFON	max. plausible speed-dependent variance of FSE values
1184	DKNOTBEGR	Limitation of set value as f(nmot) if B_dknot = true
1184	DKROFN	limit of integrator rise for zero test
1184	DLAMOB	delta lamda at overboost
1184	DLBTS	Delta nominal Lambda for component protection
1184	DLRKIONLP0	I component as f(abs(dwdkdlr_w)), above NLP
1184	DLRKIUINLP0	I component as f(abs(dwdkdlr_w)), below NLP (weak)
1184	DLRKIUINLP1	I component as f(abs(dwdkdlr_w)), below NLP (medium)
1185	DLRKIUINLP2	I component as f(abs(dwdkdlr_w)), below NLP (strong)
1185	DLURMIN	speed dependensy of engine roughness referenz minimum value 1
1185	DMAUFN	delta torque rise after torque intervention
1185	DMDLWS	Torque for power steering function of the
1185	DMDLWS	Torque for power steering
1185	DMDNSM	Torque offset for after cranking compensation
1185	DMDPUG	delta torque threshold end of dashpot
1185	DMLLNG	LLR: D-gain depending of ngasf for air path
1185	DMLLNGV	LLR: D-gain depending of ngasf for air path
1185	DMLLRLMNN	Lower limit for dmlrl
1185	DMLLRLMXN	Safety concept: upper limit for dmlrl
1185	DMLLRMNN	Lower limit for dmlr_w
1185	DMLLRMXN	Safety concept: upper limit for dmlr
1185	DMLSDUG	Delta torque for finishing positive slope limitation
1185	DMRIFW	Delta relative torque for FGR initialization
1185	DMSTES	characteristic line maximum increase of purge mass flow
1185	DNBURN	Minimum difference in engine-speed for detected combustion
1185	DPUPVDK	pressure difference pu-pvdk
1185	DROLSOLA	Misfire Detection : load-dynamic treshold for deactivation
1185	DLRTML	proportion factor to decrease waiting time up to tmot-threshold for closed loop
1185	DTVKAML	delta-tv for cat oxygen neutralization (air mass dependent)
1185	DTVKAML2	delta-tv for cat oxygen neutralization (air mass dependent) bank2
1185	DVNG	LLR: D-gain depending of ngfil for vehicle at rest
1185	DVNGV	LLR: D-gain depending of ngfil for vehicle rolling
1185	DVSKNBGA	delta velocity for set value correction after acceleration
1185	DVSKNVGA	delta velocity for set value correction after deceleration
1185	DWKRMSN	delta ignition angle knock control distance from mean retarding
1185	DZWAML	Up/down regulation speed between the maps of limitation
1186	DZWDYN	Spark advance for burning-limit angle at tip-in
1186	DZWETA	delta ignition angle from efficiency
1186	DZWMNSTN	nmot dependent offset on latest ign. angle during start
1186	DZWNWSUE	Delta ignition angle dependent on the camshaft overlap
1186	DZWOAGR	AGR-rate-dependent offset of optimum ignition angle
1186	DZWOLA	Lambda dependency of optimum ignition angle referred to Lambda 1
1186	DZWOM	temperature-dependent offset of optimum ignition angle
1186	DZWSPM	delta latest ignition angle relative to engine temperature
1186	DZWSTTA	Delta ignition angle during start
1186	DZWTIN	delta ignition angle at tip-in
1186	EFFDFPM	Declaration of freeze frame extension out of table DFFT
1186	ETADZW	ignition efficiency depending on delta ignition angle
1186	ETALAM	Lambda effectiveness
1186	EVTMODO	offset for evtmod depending on filtered engine temperature
1186	FABMDWA	Factor to decrease the converter torque depending of nturb
1186	FABSTT	Factor parking time for model temperature
1186	FATMRML	divide factor exhaust-/exhaust-pipe temperature
1186	FATMRML2	divide factor exhaust-/exhaust-pipe temperature bank2
1186	FA_CALID	
1186	FBFGRSFW	Correction factor for FGR target acceleration
1186	FBTEB	factor ftefvab-dependending limitation of the canister charge adaptation speed
1186	FBTEVA	factor ftefvva-dependending canister charge adaptation speed
1186	FBZBTEML	Weighting factor integration speed for canister charge adaptation



Page	Parameter	Descriptor
1186	FBZFRAT	weighting factor for integration speed KFFRAT as f(ab0)
1186	FDDN	LLR: weightning factor for D-amplification
1186	FDVAGR	factor temperature for flow through EGR valve
1186	FDVANS	Temperature factor for air at throttle valve
1186	FETATEBN	characteristic line: reduction of engine efficiency as f(nmot)
1187	FFLDZ	Follow-on ignition charging time
1187	FFRITMS	tmst dependent factor to modify I-dynamic of lambda control
1187	FFTCAS	Freeze Frame table: CAN, timeout ASC
1187	FFTCINS	Freeze frame table: CAN-Timeout, instrument panel
1187	FFTCUP	freeze frame table: CAN-timeout KUP-message
1187	FFTEV1	freeze frame table: injector power stage 1
1187	FFTEV2	freeze frame table: injector power stage 2
1187	FFTEV3	freeze frame table: injector power stage 3
1187	FFTEV4	freeze frame table: injector power stage 4
1187	FFTEV5	freeze frame table: injector power stage 5
1187	FFTEV6	freeze frame table: injector power stage 6
1187	FFTEV7	freeze frame table: injector power stage 7
1187	FFTEV8	freeze frame table: injector power stage 8
1187	FFTHSH	Table of ambient condition for heating O2-sensor post cat
1187	FFTHSH2	Table ambient conditions heating lambda sensor downstream catalyst bank2
1187	FFTHSV	Table of ambient condition for heating O2-sensor pre cat
1187	FFTHSV2	Table of ambient condition for heating O2-sensor post cat bank 2
1187	FFTHSVE	Freeze frame table: O2 Sensor Heater power stage
1187	FFTHSVE2	Freeze frame table: O2 Sensor Heater power stage bank 2
1187	FFTKPE	Freeze frame table: fuel pump relay power stage
1187	FFTKRNT	freeze frame table: knock control zero test
1187	FFTKROF	freeze frame table: knock control offset
1187	FFTKRTP	freeze frame table: knock control test pulse
1187	FFTKS1	freeze frame table: knock sensor 1
1187	FFTKS2	freeze frame table: knock sensor 2
1187	FFTKS3	freeze frame table: knock sensor 3
1187	FFTKS4	freeze frame table: knock sensor 4
1187	FFTLASH	Table ambient conditions for Lambda sensor downstream catalyst
1188	FFTLASH2	Table ambient conditions Lambda sensor downstream catalyst bank2
1188	FFTLATP	Table ambient conditions Lambda sensor aging Tp upstream catalyst
1188	FFTLATP2	Table ambient conditions Lambda sensor aging Tp upstream catalyst bank2
1188	FFTLATV	Table ambient conditions Lambda sensor aging Tv upstream catalyst
1188	FFTLATV2	Table ambient conditions Lambda sensor aging Tv upstream catalyst bank2
1188	FFTLSH	Table of ambient conditions Lambda sensor downstream catalyst
1188	FFTLSH2	Table of ambient conditions Lambda sensor downstream catalyst bank 2
1188	FFTMDB	freeze frame table: Target torque limiter
1188	FFTMILE	freeze frame table: MIL power stage
1188	FFTNWKW	freeze frame table: alignment between camshaft and crankshaft
1188	FFTNWKW2	freeze frame table: alignment between camshaft 2 and crankshaft
1188	FFTNWS	freeze frame table: camshaft control
1188	FFTNWS2	freeze frame table: camshaft control bank 2
1188	FFTPH	freeze frame table: phase sensor
1188	FFTPH2	freeze frame table: phase sensor
1188	FFTTA	freeze frame table: air intake temperature TANS
1188	FFTTES	freeze frame table: canister purge valve
1188	FFTTEVE	freeze frame table: canister purge valve (power stage)
1188	FFTTM	freeze frame table: engine temperature TMOT
1188	FFTUB	freeze frame table: battery voltage UB (onboard)
1188	FFTUF2SG	Freeze frame table: monitoring of the function: data from other ECU
1188	FFTUFMV	Freeze frame table: monitoring of the function: torque comparison
1188	FFTUFSKA	Freeze frame table: monitoring of the function: safety fuel cut-off
1188	FFTURRAM	Freeze frame table: monitoring of the controller: RAM
1188	FFTURROM	Freeze frame table: monitoring of the controller: ROM
1188	FFTURRST	Freeze frame table: monitoring of the controller: Reset
1188	FFTVKUP	freeze frame table: "Engine OFF"-request from F1-gearbox (KUP)
1188	FHSTT	factor hot start
1189	FIMHU	Factor pulse abrupt
1189	FIMWU	Factor pulse smooth
1189	FKATEB	Characteristic line fuel portion depending on te / TEMIN
1189	FKAXAVKAT	weighting factor for oxygen capacity depending on avkatf
1189	FKDISA	faktor difference for integrator ambient pressure during fuel cut off
1189	FKHLA	Weighting factor Lambda nominal for catalyzer heating
1189	FKHMD	Weighting factor torque reserve for catalyzer heating
1189	FKKVS	Factor to correct fuel delivery system
1189	FKSTT	factor cold start
1189	FLRAWG	amplification of load controller
1189	FLRFKATE	Rating of factor fkatei from %TEB to optimize the regulation parameter
1189	FLRHG	amplification of load controller
1189	FLRM	Engine temperature dependent factor to modify I-dynamic of lambda control
1189	FLUTN	filter factor running irregularity
1189	FMDGENTA	factor: generator torque due to temperature
1189	FMDKHFH	altitude correction of torque reserve for catalyst heating
1189	FMDKHTM	tmot-correction of torque reserve for catalyst heating
1189	FMDWAT	Factor to calculate the converter torque depending of oil temperature
1189	FNSHO	weighting of afterstart enrichment
1189	FNSSM	after start increase
1189	FNSSTKM	Factor to weight the desired speed at start during catalyst heating





Page	Parameter	Descriptor
1189	FNSSTM	Faktor for target engine speed during start
1189	FNSTABNV	Factor for engine speed stabilisation by torque
1189	FPLMRM	weighting factor for P component of air-mass controller
1189	FPVMXN2	factor for pressure ratio maximum with secondary last sensor
1189	FPWDKAPP	throttle angle dependent on accelerator pedal position, only for calibration
1189	FQTEDL	Factor for exponential decrease of flow rate
1189	FQTEFR	characteristic line: purge rate reduction with big frm-deviation
1190	FQTEPT	characteristic line: for fuel-tank underpressure limitation
1190	FQTEVA	progression of purge rate controller
1190	FRARAWG	amplification factor
1190	FRARHG	amplification factor
1190	FRINH1	Multiplication factor for RIN nominal value downstream of the catalyzer
1190	FRINH2	Multiplication factor for RIN nominal value downstream of the catalyzer
1190	FRINV1	Multiplicativ factor for RIN desired value pre cat
1190	FRINV2	Multiplicativ factor for RIN desired value pre cat
1190	FRLFSDP	injection correction for RLFS
1190	FRLMNH0	correction factor r <sub>lmin</sub> depending on altitude
1190	FSTHO	weighting of factor start
1190	FSWALUV	rough road detection threshold = f (vehicle speed)
1190	FSWALUV1	rough road detection threshold = f (vehicle speed)
1190	FSZTM	Factor dwell angle correction t <sub>mot</sub> depending
1190	FTAGRV	Factor for temperature drop from EGR_pipe to EGR_valve
1190	FTDAG	factor for temperature drop on EGR line
1190	FTEINIX	characteristic line for max. purge rate = F(integral purge flow after TE-Stop)
1190	FTMFFANZ	Follow-on ignition weighting factor
1190	FTMLAKH	t <sub>mot</sub> -correction of lambda-weighting at catalyst heating
1190	FUEPMLD	Factor for gliding transition average pressure (reference pressure turbo)
1190	FUKNSTHO	altitude dependent transient control post cranking factor
1190	FUKNSTM	initial value of transient control post cranking factor
1190	FVERMN	characteristic line: filter factor for purge flow in the manifold with fresh air
1190	FVERZDYN	dynamic factor delay of purge flow in the manifold
1190	FVRMDYN	dynamic factor for purge flow in the manifold with fresh air
1190	FWDMVAD	factor for the weighting of d <sub>mvad_w</sub> in %MDMIN
1190	FWEMXT	maximum factor for fuel cut-in temperature characteristic
1190	FWFTBRTA	Weighting for f <sub>tr</sub> as a function of t <sub>ans</sub>
1191	FWLKFTBR	warm up correction for combustion chamber model
1191	FWMLHFMMN	Weighting factor for min. HFM air-mass threshold as a function of the altitude
1191	FWSTAA1	afterstart correction
1191	FWSTAB1	weighting afterstart decrease range 1
1191	FWSTAB2	weighting afterstart decrease range 2
1191	FWSTAB3	weighting afterstart decrease range 3
1191	FWSTAS1	correction of threshold 1 for afterstart
1191	FWSTAS2	correction of threshold 2 for afterstart
1191	FZANSSA1	factor for ign. sync. decreasing of afterstart enrichment at hot start range 1
1191	FZANSSA2	factor for ign. sync. decreasing of afterstart enrichment at hot start range 2
1191	FZANSSM1	factor for ign. sync. decreasing of afterstart enrichment above SZANSSM
1191	FZANSSM2	factor for ign. sync. decreasing of afterstart enrichment below SZANSSM
1191	FZANSSM3	factor for ign. sync. decreasing of afterstart enrichment in range 3
1191	FZDASHTM	factor for time constant dashpot
1191	FZN1	Cylinder individual factor at neutral camshaft position EV 1
1191	FZNWN1	Cylinder individual factor at active camshaft position EV 1
1191	FZPUSA	correction faktor time constant ambient pressure adaptation during fuel cut-off
1191	FZWSTNM	Ignition angle during start
1191	FZWSTTM	Ignition angle during start
1191	GFDLDN	LLR: weighting factor for D-amplification on the air path
1191	IGESGA	Total transmission ratio
1191	ILMLKAXTK	Threshold of richness area of O <sub>2</sub> purging after fuel cat off, funct. of cat-temp
1191	ILMLKAXTK2	Thresh. of richness area of O <sub>2</sub> purging after fuel cut off, funct. of cat-temp.
1191	ILMRN	integrator gain of air mass controller
1191	IMLKAXTK	integr. air mass threshold f(tkatm) for cancelation of cat oxygen neutralization
1191	IMLKAXTK2	integr. air mass threshold f(tkatm2) for cancelation of cat oxygen neutral.
1191	IMLKHTMS	imlpr-threshold, changing to lambda catalyst heating
1191	INCKSTAI	increment-step for STADAP factor
1192	IVDN	LLR: I-gain for vehicle at rest
1192	IVDNDTE	LLR: I-gain at DTEV
1192	IVDNV	LLR: I-gain for vehicle rolling
1192	KATBFML	filter time constant for signal attenuation in catalyst stress
1192	KATBFML2	filter-time constant for signal attenuation in catalyst stress (assymmetrical)
1192	KATBFXM	max. catalyst load threshold for stop condition
1192	KATMEXML	Temperature of the exotherme in the catalyst tkatm
1192	KATMEXML2	Temperature of the exotherme in the catalyst , bank 2
1192	KATMIEXML	Temperature of the exotherme in the catalyst t <sub>ikatm</sub>
1192	KATMIEXML2	Temperature of the exotherme in the catalyst t <sub>ikatm</sub> , bank 2
1192	KDLASHKI	evaluation factor of I-part of LRHK, f(dlashkm)
1192	KDLASHKI2	evaluation factor of I-part of LRHK, f(dlashkm), bank 2
1192	KDLASHKP	evaluation factor of P-part of LRHK, f(dlashkm)
1192	KDLASHKP2	evaluation factor of P-part of LRHK, f(dlashkm), bank 2
1192	KE1N	knock detection threshold at cylindertimer 1
1192	KE2N	knock detection threshold at cylindertimer 2
1192	KE3N	knock detection threshold at cylindertimer 3
1192	KE4N	knock detection threshold at cylindertimer 4
1192	KE5N	knock detection threshold at cylindertimer 5



Page	Parameter	Descriptor
1192	KE6N	knock detection threshold at cylindertimer 6
1192	KE7N	knock detection threshold at cylindertimer 7
1192	KE8N	knock detection threshold at cylindertimer 8
1192	KEMLN	length of the sampling window for knock control
1192	KFABAK	share factor wall wetting for acceleration enrichment
1192	KFAFTE	map flow-characteristic of PCV (incl. PCV carcoal-canister line)
1192	KFAMAL	map reduction factor of the engine roughness reference value at multiple misfire
1192	KFAMAL1	map reduction factor of the engine roughness reference value at multiple misfire
1192	KFATMLA	map exhaust gas temperature correction = f(lambda)
1193	KFATMLA2	map exhaust gas temperature correction = f(lambda) bank2
1193	KFATMZW	map exhaust gas temperature correktion = f(ignition-variation)
1193	KFATMZW2	map exhaust gas temperature correktion = f(ignition) bank2
1193	KFAVAK	share factor wall wetting for deceleration enleanment
1193	KFBAKL	factor accel. enrichment (short- and long-time part)
1193	KFBRAWA	Target acceleration for resumption
1193	KFBS	bank-selective mixture factor
1193	KFCFO	map for definition of range characteristics (dominant..)
1193	KFCFO2	map for definition of range characteristics (dominant..)
1193	KFDETATE	correction of ignition angle effectiveness for diagnosis of PCV
1193	KFDFBTMN	dynamic factor for combustion chamber temperatur model negativ gradient
1193	KFDFBTMP	dynamic factor for combustion chamber temperatur model positiv gradient
1193	KFDLSD	Damping of PT2 filter in positive torque slope limitation
1193	KFDLUR	map engine roughness difference dluts referenz value
1193	KFDLUR1	map engine roughness difference dluts referenz value
1193	KFDLUR2	map engine roughness difference dluts referenz value
1193	KFDLURZ	map engine roughness difference dluts referenz value at ZAS (cylinder cut-off)
1193	KFDMADAP	upper threshold for torque-intervention during dashpot
1193	KFDMADARO	Upper threshold for torque intervension
1193	KFDMDKOE	Starting value torque filter when air-conditioner compressor is activated
1193	KFDMDPO	Delta torque for starting negative slope limitation
1193	KFDMLSDO	Delta torque for starting positive slope limitation
1193	KFDMLSDS	delta torque for triggering of load-shock damping after shifting procedure
1193	KFDTMRS	char.line for gradient of engine coolant temp. during cutoff for reference model
1193	KFDTMTM	char. map for gradient of engine coolant temperature in substitute temp. model
1193	KFDTMTR	char. map for gradient of engine coolant temperature in reference model
1193	KFDTMTU	char. map for correction gradient of engine coolant temp. at low warming up
1193	KFDYES	Threshold for dynamic presetting values
1194	KFDYESOF	Offset threshold for dynamic presetting values
1194	KFDZWKG	ignition angle correction due to knock limit shift
1194	KFETATE	characteristic map for efficiency at active purging when te is near TEMIN
1194	KFFDLBTS	Factor delta nominal Lambda for component protection
1194	KFFFANZ	Number of sequential sparks
1194	KFFFANZUB	Number of sequential sparks
1194	KFFFRAT	load and speed dependent gradient of FRAT integrator
1194	KFFRMIN	lower limit of control range
1194	KFFTEAN	characteristic map for limitation of the purge rate with no Lambda control
1194	KFFTEAX	Characteristic map for limitation of the purge rate
1194	KFFTV	weighting map for TVLRH
1194	KFFTV2	weighting map for TVLRH bank 2
1194	KFFWL	map warm-up factor
1194	KFFWLRL	map warm-up factor load dependent fraction
1194	KFFWLW	map weighting warm-up factor
1194	KFFWTBR	Weighting factor for combustion chamber temperature model
1194	KFFWTBRA	Weighting factor for combustion chamber temperature model B_agr=true
1194	KFKABMT	Map for correction of calculated amplitude, dependent on ml and cat. temperature
1194	KFKHFM	HFM-correction characteristic map
1194	KFKSWF	map for catalyst protection, weighting factors
1194	KFKWTMP	Characteristic torque reserve for keeping catalyst warm, temporary
1194	KFLASKH	Performance characteristics lambda exhaust nominal at catalyst heating
1194	KFLBTS	Nominal Lambda for component protection
1194	KFLF	lambda characteristic map at part load
1194	KFLMSKH	Performance characteristics lambda engine nominal at catalyst heating
1194	KFLUAR	map for engine roughness distance reference value
1194	KFLUAR1	map for engine roughness distance reference value
1194	KFLUAR2	map for engine roughness distance reference value
1195	KFLUARZ	map for engine roughness distance reference value at ZAS (cylinder cut-off)
1195	KFLURB	map for engine roughness - reference base value
1195	KFLURB1	map for engine roughness - reference base value
1195	KFLURB2	map for engine roughness - reference base value
1195	KFLURBZ	map for engine roughness base value, in case of ZAS
1195	KFLURM	reference base value map for engine roughness for misfire detection
1195	KFLURM1	reference base value map for engine roughness for misfire detection
1195	KFMAKR	map for starting measuring window knock control
1195	KFMDBGRG	map with the value of the torque limitation
1195	KFMDDSLA	Map torque reserve at tester demand of SAI-diagnosis short test
1195	KFMDGEN	Torque intake generator
1195	KFMDKH	Characteristic torque reserve for catalyst heating
1195	KFMDKO	map for torque needed for air condition
1195	KFMDPWM	steady state load of ac-compressor for PWM-signal of its load
1195	KFMDPWME	initial load of ac-compressor for PWM-signal of its load
1195	KFMDRKO	look-up-table: torque loss depended of rl, nmot
1195	KFMDRKOE	look-up-table: torque loss dyn. part dependend of rl, nmot



Page	Parameter	Descriptor
1195	KFMDS	map for engine drag torque
1195	KFMDSZAS	map for engine drag torque during cyclinder cut off
1195	KFMDZOF_JUM	map for offset tolerance depending on permissible torque
1195	KFMIFABG	delta torque for gradient limitation
1195	KFMIFALS	Indicated driver's request torque for charge path at load-shock damping
1195	KFMILSD	Initial value for positive torque slope limitation
1195	KFMIMN	minimum drag torque
1195	KFMIOF	map optimum engine torque
1195	KFMIREF	Map of decreasing control torque for VMAX control
1195	KFMIRL	map for calculation of nominal charge
1195	KFMIZUFIL	Maximum permitted indicated set torque for torque limitation before Filter
1196	KFMIZUNS	Authorized torque for post-start torque increase
1196	KFMIZUOF	Maximum permitted indicated set torque for torque limitation
1196	KFMI_JUM	map of optimum engine torque
1196	KFMLDMN	air mass flow threshold for min. failure
1196	KFMLDMX	air mass flow threshold for max. failure
1196	KFMPED_JUM	map for permissible torque from the pedal position in function monitoring
1196	KFM PNS_JUM	map for permissible torque from pedal position for a cold engine
1196	KFMRES	LLR: torque reserve at idle and near-idle zone
1196	KFMRESK	LLR: torque reserve at idle and near-idle zone clutch disengaged
1196	KFMRESKH	Torque reserve during catalyst heating
1196	KFMRESNL	Torque reserve in non idling state
1196	KFMRESTA	Torque margin dependent on tans
1196	KFMRESTM	Map temp-dependent limiting of torque reserve
1196	KFM SNWDK	Map for scaled mass flow over throttle valve
1196	KFNLLNST	idle speed after start
1196	KFN SA	after start increase
1196	KFN SWRL	weighting of afterstart enrichment
1196	KFNW	characteristic map for variable camshaft spread
1196	KFNWEGM	Fuel cut in map depending on rpm
1196	KFNWWL	
1196	KFPBRK	factor to correct pressure at combustion chamber
1196	KFPBRKNW	factor to correct pressure at combustion chamber by active Camshaft control
1196	KFPED	accelerator pedal characteristic
1196	KFPEDR	Pedal characteristic for reverse gear (only automatic transmission)
1196	KFPLMR	P-component of air mass controller
1196	KFPRG	internal partial exhaust gas pressure dependent on camshaft adjustment sumode=0
1196	KFPRG2SU	internal partial exhaust gas pressure depend on camshaft adjustment sumode=2
1196	KFPRG3SU	internal partial exhaust gas pressure dpent on camshaft adjustment sumode=3
1197	KFPRGSU	internal partial exhaust gas pressure dependent on camshaft adjustment sumode=1
1197	KFPU	pulsation characteristic map
1197	KFPUNW	pulsation map for camshaft control switch over
1197	KFPUSU	pulsation characteristic map at active variable intake system by sumode=1
1197	KFPUSUNW	pulsation characteristic map at active variable intake system and camshaft cont.
1197	KFQTE	Map for purge rate increase / decrease
1197	KFRI	I characteristic map
1197	KFRI2	LR-I-Map for bank 2
1197	KFRINH	MAP for Nernst resistor post cat
1197	KFRINH2	MAP for Nernst resistor post cat bank 2
1197	KFRINV	MAP for Nernst resistor pre cat
1197	KFRINV2	MAP for Nernst resistor post cat , bank 2
1197	KFRLIP_JUM	characteristic map for load signal calculation on throttle angle
1197	KFRLMN	Minimum charge during fuel on
1197	KFRLMNSA	Minimum rl during fuel cut off
1197	KFRLW	rlw-map from throttle valve angle
1197	KFRLWNW	rlw-map from throttle valve angle during variable camshaft
1197	KFRLWSU	rlw-map from throttle valve angle during manifold switch over
1197	KFRLWSUNW	rlw-map from throttle valve angle during manifold switch over and aktive var. ch
1197	KFRP	P characteristic map
1197	KFRP2	LR-P MAP for bank 2
1197	KFRTV	delay time characteristic map
1197	KFRTV2	delay time characteristic map
1197	KFSU	Load/speed performance characteristics for suction tube switchover
1197	KFSU2	map for intake manifold switch over, flap 2
1197	KFSZT	Dwell angle characteristic map
1197	KFTADMS	dynamic evaluation factor for close off of PCV
1197	KFTAGAV	EGR temperature at outlet valve
1198	KFTATM	map exhaust gas temperature f(nmot,rl)
1198	KFTATM2	map exhaus gas temperature f(nmot,rl) bank2
1198	KFTATX	map for max. duty cycle
1198	KFTEKA	characteristic map of desired fuel portion purge control
1198	KFTEVP	Characteristic map for period time of the PCV
1198	KFTPKOR	correction map for the measured cycle duration TP (tpsvkof)
1198	KFTVFRR	Map: Lambda controll after this time reset at reference value
1198	KFTVSA	Retard time for overrrun fuel cut-off
1198	KFURL	conversion factor from ps->rl dependent on camshaft adjustment sumode=0
1198	KFURL2SU	conversion factor from ps->rl dependent on camshaft adjustment sumode=2
1198	KFURL3SU	conversion factor from ps->rl dependent on camshaft adjustment sumode=3
1198	KFURLSU	conversion factor from ps->rl dependent on camshaft adjustment sumode=1
1198	KFUSHK	lambda sensor reference value for lambda control downstream of catalyst
1198	KFUSHK2	lambda sensor reference value for lambda control downstream of catalyst bank2
1198	KFVAKL	factor decel. enleanment (short- and long-time part)



Page	Parameter	Descriptor
1198	KFVERST	weighting map for increasing control of friction torque
1198	KFVOFFS	velocity offset for cruise control
1198	KFWDKMSN	Map for the desired throttle blade angle
1198	KFWDKPP	throttle blade position dependent on air charge signal
1198	KFWDKSMX	max. desired throttle angle
1198	KFWDKSST	desired throttle position at start-up
1198	KFWDKTHO	desired throttle position at start-up - f (high, engine start temperatur)
1198	KFWEE	characteristic map angle end of injection
1198	KFWEEK	map for end of injection angle (cold parameters)
1198	KFWHSTT	map weighting of hot start factor
1198	KFWKSTAB	factor cold re-start for reduction of starting fuel
1198	KFWKSTN	map weighting of factor cold start
1198	KFWKSTT	map weighting of factor cold start
1199	KFWMABG	map for heat-quantity threshold dew-point end upstream bank1
1199	KFWMABG2	map for heat-quantity threshold dew-point end upstream bank2
1199	KFWMKAT	map for heat quantity threshold dew-point end downstream
1199	KFWMKAT2	map for heat quantity threshold dew-point end downstream bank 2
1199	KFWPFGR	Inverse pedal characteristic for cruise mode
1199	KFWTBR	Weighting factor Tans/Tmot for combustion chamber temperature model
1199	KFWTBRA	Weighting factor Tans/Tmot for combustion chamber temperature model B_agr=true
1199	KFWWLML	map weighting warm-up factor
1199	KFWWNS	repeated start time factor
1199	KFZDASH	Time constant for negative torque slope limitation
1199	KFZDASH2	time constant PT1-filter dashpot at low clutch torque
1199	KFZKPUA	time constant for ambient pressure
1199	KFZLSD	Time constant for positive torque slope limitation
1199	KFZNSM	time constant for decay of reference speed
1199	KFZW	Ignition advance-angle charakteristik map
1199	KFZW2	Ignition angle performance characteristics variant 2
1199	KFZWMN	Map for minimal ignition angle
1199	KFZWMNKH	Map for minimal ignition angle catalyst warm-up
1199	KFZWMNST	minimal ignition spark advance for engine start and after start
1199	KFZWMS	Map for ignition value as latest possible value
1199	KFZWOP	optimum ignition angle
1199	KFZWOP2	Optimum ignition angle, variant 2
1199	KFZWVWLNLM	Delta ignition sparc advance during engine warm up phase
1199	KFZWVWLTMT	Delta ignition sparc advance during engine warm up phase
1199	KFZW_UJM	map of optimum ignition angle
1199	KIFZGAWG	amplification of vehicle model integrator at AT
1199	KIFZGHG	amplification of vehicle model integrator at AT
1199	KINMXG	gain of integral component for NMAX control
1200	KINMXRLG	gain of integral component for NMAX control
1200	KIRMSMS	Integration speed matching of mass flow PCV with calculated mass flow
1200	KKFFGRGA	amplification rate during cruising for cruise control
1200	KLAF	characteristic of Saint-Venant
1200	KLAFFE	characteristic of Saint-Venant of purge control valve an line AKF-TEV
1200	KLATMLAE	Temperature of the exotherme decrease during enrichment tikatm
1200	KLATMLAE2	Temperature of the exotherme decrease during enrichment tikatm, bank2
1200	KLATMIZWE	Temperature of the exotherme decrease in cat during ignition retard tikatm
1200	KLATMIZWE2	Temperature of the exotherme decrease in cat during ignition retard tikatm, bank
1200	KLATMLAE	Temperature of the exotherme decrease during enrichment
1200	KLATMLAE2	Temperature of the exotherme decrease during enrichment, bank 2
1200	KLATMZWE	Temperature of the exotherme decrease in cat during ignition retard tkatm
1200	KLATMZWE2	Temperature of the exotherme decrease in cat during ignition retard, bank2
1200	KLDMDLF1	Characteristic curve reserve torque fan
1200	KLDMDLF2	Characteristic curve reserve torque fan 2
1200	KLDMMX	Maximum delta torque for air path
1200	KLDPPK	pressure drop at throttle blade
1200	KLDTPH	Fixed value characteristic for weighting the engine dynamic
1200	KLDTPHST	Fixed value characteristic for the engine start
1200	KLDYNCOR	Value for the dynamic correction after the first ignition
1200	KLETAZUJM	ignition efficiency depending on delta ignition angle
1200	KLFZWMNKH	Spark retard gradient of burning limit during after-start at cat.heating
1200	KLFZWMNST	Spark retard gradient of burning limit during after-start
1200	KLNLPHN	Correction of the phase frequency characteristic of the sensor
1200	KLNPED_UJM	Speed lim. as func. of nominal pedal value, in DK drive standby func.,func.mon.
1200	KLNRWLTMT	Weighting of relative nominal filling over engine temp. for addressing KFNWS
1200	KLRSYNIN	
1200	KLRSYNPN	
1201	KLTDS	Conversion line for tank pressure sensor DS-T2
1201	KLTNRDE	characteristic for tooth times at reverse rotation
1201	KLWDKABST	Weighting desired throttle position at start-up
1201	KLWDKPED	Offset desired throttle position at start-up
1201	KLWDKTAN	weight of throttle position at start up with intake air temperatur
1201	KLWNWI	Fixed value characteristic for weighting the angular displacement
1201	KRAFGRGA	amplification rate at ramp for cruise control
1201	KRAL1N	load range for adaption maps 1
1201	KRAL2N	load range dor adaption maps 2
1201	KRAL3N	load range for adaption maps 3
1201	KRDWSN	knock control delta angle safety
1201	KRFKN	retard step knock occurrence
1201	KRMXN	maximum retard adjustment



Page	Parameter	Descriptor
1201	KRN LZAR	cylinder individual rpm limit for lead by leading cylinder
1201	KRVFN	number of firings/cyl. or time for ignition advancing
1201	KRVFSN	number of firings/cyl. or delay-time during fast ignition advancing of the KC
1201	KSTAI	workingrange for STADAP factor
1201	LALIUSH	lambda linearization, sensor behind catalyst
1201	LALIUSH2	lambda linearization, sensor behind catalyst, bank 2
1201	LALIUSRH	lambda linearization, sensor behind catalyst
1201	LALIUSRH2	lambda linearization, sensor behind catalyst
1201	LAMFA	Lambda driver demand
1201	LAMKAML	lambda setpoint for catalyst deoxidation (dependent on air mass)
1201	LAMKAML2	lambdasetpoint for catalyst deoxidation (air mass dependent), bank 2
1201	LAMLGMTM	lambda limit "lean"
1201	LASDSLA	Lambda exhaust nominal at secondary air adaption/short test
1201	LASTMOT	tmot-correction of lambda exhaust nominal
1201	LIMXDNS	upper integrator limit for standing car
1202	LIMXVDNS	upper integrator limit for rolling car
1202	LISTM	value of idle speed control integrator during start
1202	LKRN	load-signal threshold knock control
1202	LMSTMOT	tmot-correction of lambda engine nominal
1202	LNXQTM	natural logarithm from temperature quotient
1202	LSAKTD	Impact of slow front sensor on cat. monitoring
1202	LURBRL8	reference value for engine roughness, vehicle speed zero
1202	LURKH	dmrkh-depen. engine roughness reference correction value, during cat heating
1202	LURKTM	Tmot-dependent engine roughness reference correcting value
1202	LURMIN1	speed dependency of engine roughness referenz minimum value 1
1202	LURMIN2	speed dependency of engine roughness referenz minimum value 2
1202	LURMIN3	speed dependency of engine roughness referenz minimum value 3
1202	LZFUER	guide cylinder assignment
1202	MASK_40MS	40ms mask for function monitoring
1202	MASK_FUAE	Mask for task splitting in monitoring functions (part 1: inputs)
1202	MDKOAB	Torque threshold to shut down the compressor during acceleration
1202	MDKOAN	Torque threshold to switch the AC-compressor off
1202	MDKOEN	Torque threshold to switch the AC-compressor on
1202	MDSH	Part of the resistant torque depending on altitude
1202	MDSM	temperatuer share of engine friction torque
1202	MDSMZAS	temperatuer share of engine friction torque during cylinder cut off
1202	MIFAMXNOT	maximum indicated engine torque at limp home
1202	MKFADPN	clutch torque for switch-over dashpot-filter time
1202	MKFADPN1	clutch torque for switch-over dashpot-fil. time when AC comp. has been enabled
1202	MKLLS	torque needed for air condition fan
1202	MLHFM	air-mass meter characteristic line
1202	MLSUS	reference of air mass flow integral
1202	MRFARUGDN	Reset threshold for linear pedal travel in the non-reduced DK range
1203	MRFAVLN	Full load detection threshold of the relative driver request
1203	MRFAVV	threshold to switch end of injection angle at max. driver request
1203	MRFGRIXM	Maximum FGR initialization value
1203	MSNTAG	EGR mass flow standardised
1203	MSNTATE	Characteristic standardized mass flow through TEV
1203	M_SRST_UM	Mask B_srst_um - information SW-reset from cyclic RAM-check
1203	NARLLGA	speed threshold for AR at idle
1203	NASNOTKL	characteristic line rotational speed against engine stall
1203	NDFILOG	Threshold for filter output ndfil
1203	NDIFFOG	Threshold engine speed difference for initialization of AR during braking
1203	NFS2M	Target idle speed 2, B.fs = 1
1203	NFSKHM	LL nominal speed with driving graduations and catalyzer heating
1203	NFSM	desired engine speed DRIVE-position switch on
1203	NGALUN	Misfire Detection : treshold for gradient of engine speed
1203	NGKRWN	threshold revolution gradient for dynamics detection
1203	NLL2M	Target engine speed 2
1203	NLLCVTMXV	Limitation of the target speed (CVT transmission)
1203	NLLKHM	Nominal idling speed during catalyzer heating
1203	NLLM	desired engine speed
1203	NMAXDVG	rpm limit in case of fault detection velocity signal
1203	NMXDAEF	maximum permitted engine speed for throttle actuator substitute function
1203	NMXPG	P component for NMAX control
1203	NMXPRLG	P component for NMAX control
1203	NNSTA	engine-speed transition normal -> start
1203	NSLPP	Target speed depending on the pump pressure of power steering
1203	NSLPPFS	Target speed depending on the pump pressure of power steering with B.fs=1
1203	NSTAMXHA	engine speed limit until STADAP is active depend. on altitude
1203	NSTNM	transition start -> normal
1204	NWDKSST	threshold for deactivation desired throttle position without torque structur
1204	NWECVTM	Fuel restart-speed at CVT
1204	NWENG	Fuel cut-in engine speed
1204	NWENGFS	Delta Fuel cut-in engine speed with Drive
1204	NZHDTL	Speed threshold for decrementing time counter for hot idling
1204	NZHITL	Speed threshold for incrementing time counter for hot idling
1204	PAGAVML	exhaust gas pressure at outlet valve
1204	PLRHAV	Weighting factor of P-part LRHK depending on catalyst age
1204	PLRHAV2	Weighting factor of P-part LRHK depending on catalyst age range 2
1204	PLRHML	p-part of LRHK, f(dushk)
1204	PLRHML2	Partie p. dans LRHK, agit avec la difference de tension de sonde aval cata banc2



Page	Parameter	Descriptor
1204	PRG2SUNM	internal exhaust-gas part. press. dependent on the speed at active SU (2nd flap)
1204	PRG3SUNM	inter. exhaust-gas part. press. dependent on speed at active SU (1st + 2nd flap)
1204	PRGNM	internal exhaust-gas partial pressure dependent on the speed
1204	PRGSUNM	inter. exhaust-gas partial press. dep. on speed in case of active SU (1st flap)
1204	PUKANS	correction of pulsation depending on intake air temperature
1204	PVDN	LLR: P-gain for vehicle at rest
1204	PVDNKH	proportional ISC when secondary air activ
1204	PVDNST	proportional ISC in start
1204	PVDNV	LLR: P-gain for vehicle rolling
1204	PVLDN	LLR: P-gain for vehicle at rest (air path)
1204	PVLDNV	LLR: P-gain for vehicle at rest (air path)
1204	REDABM	fuel cut-off table for torque reduction
1204	REDABMB	fuel cut-off table for torque reduction slave1 or ecu B (SGB)
1204	REDABMC	fuel cut-off table for torque reduction slave 2 or ecu C
1204	REDABMZ	fuel cut-off table for torque reduction during ZAS
1204	REDZEM	threshold between ignition intervention and injector disabling
1204	RKBAUM	rk-threshold for acceleration enrichment display
1205	RKRMX1N	Maximum of reference level for knock detection threshold cylinder group 1
1205	RKRMX2N	maximum of reference level for knock detection threshold cylinder group 2
1205	RKVAUM	rk-threshold for deceleration enrichment display
1205	RLDKTSO	upper load characteristic line for DKAT-active
1205	RLDKTSU	lower load characteristic line for DKAT-active
1205	RLLRHON	char. line on nmot, upper rl control threshold for downstream lambda control
1205	RLLRHUN	char. line on nmot, lower control threshold rl for downstream lambda control
1205	RLLRUN	char.line above nmot,lower rL control limit for controller in front of catalyst
1205	RLNOT	limp-home relative air charge rl in case of E_DK and E_LM
1205	RLSALUN	threshold load fuel cut-off detection for deactivating misfire detection
1205	RLVMXN	maximum volumetric flow with open throttle valve
1205	RLVSMXN	maximum volumetric flow with open throttle valve and SU
1205	SDK10TEUB	wdkba dependet basic point (number 10)
1205	SDN06LLSB	10 Sst.
1205	SENZZYL	knock sensor for sw-cylinder counter 0-7
1205	SFR05TEUB	frmit dependet basic point (number 5)
1205	SGA08MDUB	base point distribution of actual gear 8 b.pt.
1205	SGSC_ANZ	number of module calls of %UFGSGSC (refer to %URPAK) in the monitoring function
1205	SGSC_K	Constant for module %UFGSGSC (see %URPAK)
1205	SIM06ESUW	Distribution for integrated air massflow since end of start
1205	SKO06KOUB	Distribution PWM-signal: load of ac-compressor
1205	SKS06ESUB	Distribution for the start adaption factor kstaa
1205	SLFOOZLN	speed dep. upper threshold for learning filter value at fuel-on/-off adaptation
1205	SLFOON	speed dep. upper threshold for learning filter value at fuel-on/-off adaptation
1205	SMI04LLUB	distribution: ind. torque for torque-reserve
1205	SMK08MDSUB	Antisurge torque dependent basic point (number =8)
1205	SML05DKUB	base point distribution air mass
1205	SML06TEUB	ml dependet basic point (number 6)
1206	SNG06LLSB	Datapoint distribution, speed gradient, 6 datapoints
1206	SNM05DKUB	base point distribution nmot
1206	SNM06ESUB	Distribution for engine speed
1206	SNM06KOUB	distribution for ac-compressor torque function
1206	SNM06LLUB	distribution of engine speed
1206	SNM08DMUB	Datapoint distribution in DMD, 8 speed datapoints
1206	SNM08KOUB	Datapoint distribution for air-conditioner compressor control 8 nmot
1206	SNM08_LUB	Base point distribution engine speed, 8 base points
1206	SNM10TEUB	nmot dependet basic point (number 10)
1206	SNM12FEUB	set points of WDKSMX, WDKUGDN
1206	SNM16KRUB	datapoint distribution engine speed, 16 datapoints
1206	SNM16OPUW	16 speed set points for ?
1206	SNM16ZUUB	break point distribution engine speed, 16 base pts.
1206	SNS06LLSB	Datapoint distribution, set-speed deviation, 06 datapoints., idle-speed control.
1206	SQM05TEUB	air mass quotient dependet basic point (number =5)
1206	SRL04DYUB	basepoint distribution of rl, 4 basepoints
1206	SRL04KRUB	datapoint distribution relative charge, 4 datapoints
1206	SRL06KOUB	6 air charge set points for A/C-compressor torque loss
1206	SRL08DMUB	Datapoint distribution in DMD, 8 load datapoints
1206	SRL08NXUB	
1206	SRL11OPUW	set point distribution relative charge
1206	SRL12ZUUB	break point distribution of relative air charge, 12 base points
1206	SRP06ESUB	Distribution for relative air charge
1206	SRST1_LJR	value for RAM data redundancy of bit B_SRST_LJM = 1
1206	STA04LLUB	distribution: tans for torque reserve
1206	STA06ESUB	Distribution for the air temperature in the intake manifold
1206	STA06LLUB	temperature: ambient air, PWM -signal of AC/compressor
1206	STM04SAUB	Datapoint distribution, engine temperature, 4 datapoints
1207	STM06LLUB	Datapoint distribution, engine temperature, 6 datapoints
1207	STM06_LUB	Datapoint distribution, engine temperature, 6 datapoints
1207	STM12ESUB	Distribution for the engine coolant temperature tmot
1207	STN06LLUB	distribution: time after start; for determination of idle speed after start
1207	STS08ESUB	Distribution for engine coolant temperature at start
1207	STS12ESUB	Distribution for engine coolant temperature at start
1207	SY_2SG	system constant 2 motronic systems
1207	SY_650ICLK	system constant: external clock frequency of CC650
1207	SY_AGR	System constant AGR present



Page	Parameter	Descriptor
1207	SY_ASG	automatic standard transmission
1207	SY_ASR	system constant ASR present
1207	SY_AWUE	injection valve cutoff possible by function AWUE
1207	SY_BDE	system constant GDI
1207	SY_BGVZS	
1207	SY_BKV	system constant: brake booster
1207	SY_BLOOP	sys. con. resetting of irreversible EGAS fault possible during clearing of FCM
1207	SY_CANAC	systemconstant: AC-compressor signal from CAN
1207	SY_CDCCSIZE	System constant: Number of values CDC to each fault path
1207	SY_CDKSIZE	System constant: Number of values CDK to each fault path
1207	SY_CDTSIZE	System constant: Number of values CDT to each fault path
1207	SY_CLASIZE	System constant: Number of values CLA to each fault path
1207	SY_CONFSL	System constant: secondary air present vorhanden
1207	SY_COPOTI	System constant CO-Poti present
1207	SY_CVT	system constant: CVT transmission exists
1207	SY_DEGFE	system constant diagnosis input values load monitoring
1207	SY_DFPMENV	system constant: environmental conditions in fault code memory
1207	SY_DGANZ	system constant number rotational-speed sensor
1207	SY_DLDP	SY_DLDP = 1 there ist a DLDP in system
1208	SY_DLS	system constant digital idle speed control
1208	SY_DLSHV	Sys. constant condition %DLSHV (sensor exchange behind KAT) existent
1208	SY_DOPZW	System constant doubled ignition output included
1208	SY_DTES	system constant diagnosis evap system
1208	SY_DVEADA	system constant BGVE: disabling injection and ignition during DV-E-adaptation
1208	SY_EGAS	System constant E-GAS present
1208	SY_EGFE	system constant input variable for charge detection
1208	SY_FANT	system constant increase of the fuel cut-off speed at tester intervention
1208	SY_FFESIZE	system constant: Size of Freeze Frame-extension
1208	SY_FFTSIZE	System constant: Number of values FFT to each fault path
1208	SY_FFZ	system constant interval ignition
1208	SY_FREQ_CP	system constant cpu frequency
1208	SY_FWFGR	
1208	SY_GAP	system constant: number of missing teeth in the gap
1208	SY_GGTS	system constant: sensor variable exact temperature signal
1208	SY_GRDWRT	System constant basic value, space between SW reference mark to OT in ° KW
1208	SY_GRDWRBT	system constant basic value 2.ECU, space between SW reference mark to OT in °KW
1208	SY_GRNDWRT	system constant basis angle ref. tr-mark
1208	SY_JNLOBD	system constant to select the communication protocols for scan tool operation
1208	SY_KL50	System constant: information available in the ECU if starter is cranking
1208	SY_KLDF	system constant for generator DF-signale
1208	SY_KOBIDIR	AC- with bidirect. connection
1208	SY_KOEVAB	coordination injection valve cutoff by function KOEVAB
1208	SY_KOPWM	PWM-compressor-signal enabled
1208	SY_KR_INT	system constant: CC650 present
1208	SY_KS1	system constant: input of the CC195 onto which knock sensor 1 is connected
1208	SY_KS2	system constant: input of the CC195 onto which knock sensor 2 is connected
1208	SY_KS3	system constant: input of the CC195 onto which knock sensor 3 is connected
1209	SY_KS4	system constant: input of the CC195 onto which knock sensor 4 is connected
1209	SY_KSDIFF	system constant: connection type of knock sensor(s)
1209	SY_LFS	System constant Fan Control configuration
1209	SY_LWS	system constant steering angle via CAN
1209	SY_ME7	system constant ECU
1209	SY_NACH	System constant ignition output after KL15 off included
1209	SY_NWS	system constant camshaft control: none, 2 point, continous
1209	SY_NWSA	system constant camshaft control outlet
1209	SY_NWVAR	system constant for camshaft configuration
1209	SY_NZUEB	system constant engine speed threshold for switching between ignition modes 1+2
1209	SY_PBRPW	system constant plausibility check brake/PWG
1209	SY_PGRAD	system constant: kind of the phase signal
1209	SY_PGRAD2	system constant: kind of the 2. phase signal
1209	SY_PGRAD3	system constant: kind of the 3. phase signal
1209	SY_PH2OFST	system const. offset in syncros between the 2 active phase signals,2 PGs only
1209	SY_PHTWIN	system constant 1/2 phase sensing system (sensor, wheel)
1209	SY_RDE	detection of reverse rotation of the engine in project included
1209	SY_REDMX	system constant: max. cylinder cutoff step
1209	SY_RLAPP	rlsol control during application possible
1209	SY_SGANZ	system constant number engine control unit
1209	SY_SLS	system constant for engines with secondary air pump
1209	SY_STADAP	system constant start adaptation
1209	SY_STERHK	system parameter condition stereo downstream catalyst
1209	SY_STERSY	System constant Condition stereo Lambda control symmetrical
1209	SY_STERVK	system constant condition: stereo exhaust system upstream of cat
1209	SY_SU	system constant: version of intake runner length adjuster
1209	SY_SWE_B	system constant for rough road detection using PWM signal from ABS
1209	SY_SWE_C	system constant for rough road detection using CAN
1210	SY_SWE_S	system constant for rough road detection using engine roughness statistics
1210	SY_TEETH	system constant: number of teeth at the crankshaft wheel (gapteeth included)
1210	SY_TFA	configuration for installation position for intake-air sensor
1210	SY_TFBA	system constant service device intervention accel. enrichment
1210	SY_TFNS	system constant service device intervention afterstart factor
1210	SY_TFST	system constant service device intervention start factor
1210	SY_TFVA	system constant service device intervention decel. enleanment



Page	Parameter	Descriptor
1210	SY_TFWL	system constant service device intervention warm-up factor
1210	SY_TSFSIZE	System constant: Number of values TSF to each fault path
1210	SY_TURBO	system constant for exhaust-gas turbocharger
1210	SY_TWDKS	system constant: input of desired angle DVE via tester is possible
1210	SY_TZW	System constant tester manipulation of zwist included
1210	SY_JBR	system constant: Voltage behind main relay ubr exists
1210	SY_VS	system constant valve stroke control: no, 2 position
1210	SY_WMAX	System constant earliest ignition timing that can be outputed
1210	SY_WMIN	System constant latest ignition timing that can be outputed
1210	SY_ZAS	system constant cylinder deactivation ZAS included
1210	SY_ZNDAUS	System constant ignition timing output (single or double fir.), 1: single,2: d.
1210	SY_ZYLZA	system constant number of cylinders
1210	SY_ZZBANK	system constant assignment of cyl. to bank1/bank2, 0 bank1, 1 b.2, binary value
1210	SY_ZZBANKB	system const. ass. of cyl. to exhaust bank1/2 for slave1/SGB; 0 b1, 1 b2 bynary
1210	SY_ZZBANKC	system const. ass. of cyl. to exhaust bank1/2 for slave2/SGC; 0 b1, 1 b2 bynary
1210	SZANSSM1	switching level 1 of afterstart enrichment
1210	SZANSSM2	switching level 2 of afterstart enrichment
1210	TADTEAMX	characteristic line for max. duty cycle = F(integral purge flow after TE-Stop)
1210	TANDT	threshold difference intake air temperature for hot start
1210	TANDT1	delta threshold intake air temperature for hot start
1210	TANSELI	intake air temperature calculation, inverse function
1211	TAPVLTM	threshold soak time for EKP-lead time
1211	TATEMSN	characteristic line of the PCV duty-cycle depending on the desired mass-flow
1211	TDLAMBTSTA	delay time to enable nominal Lambda component protection
1211	TDMFWEMI	filter-time constant at hard fuel cut-in
1211	TFWDKPN	time constant for filtering DK angle before comp. with subs. value from charging
1211	THSHKTK	Line for switch off time of lambda sensor heating post cat dep. on temp
1211	THSHKTK2	ine for switch off time of lambda sensor heating 2 post cat dep. on temp
1211	THSVKTA	Line of switching off time for lambda sensor heating depending on exh.gas temp
1211	THSVKTA2	Line of switching off time for lambda sensor heating depending on exh.gas temp 2
1211	TKOAMNN	minimum shutdown time for air-conditioning compressor
1211	TKOAMXN	maximum shutdown time for air-conditioning compressor
1211	TKOBEMNN	Minimum switch-on time for compres. after triggering by B_kobped or B_kobwped
1211	TKODPAMNN	Minimum cut-out time of the air-conditioner compressors during acceleration (dwp)
1211	TKODPAMXN	Maximum cut-out time for compressor cut-out by dwped
1211	TKOEMNN	minimal time of air-condition compressor beeing swiched on
1211	TKOWPAMNN	Minimum cut-out time at full load (by wped)
1211	TKOWPAMXN	Maximum cut-out time at full load (by wped)
1211	TLRBAM	blocking time for activation LC after BA
1211	TLRRTMS	lock time for CL lambda control after start, depending on engine start temperatu
1211	TLRVAM	blocking time for activation LC after VA
1211	TLRZWTMS	Time until hard LC switch on after start (CARB)
1211	TMDMMAT	Default temperature dependent on parking time during TDTMMA
1211	TMLFAROF	Engine coolant temperature below which After run is terminated
1211	TMLRTMS	engine temp. threshold for lambda control depending on cranking temp. tmst
1211	TMOTELI	engine temperature calculation, inverse function
1211	TN2FGRGA	double denominator time constant for cruise control
1211	TNLSGM	Delay time for ECU shut-off
1211	TSBBVTMS	time delay control readiness after sensor readiness
1212	TSPERN	lock time for p-offset after lambda sensor voltage jump
1212	TSPERN2	lock time for p-offset after lambda sensor voltage jump, bank 2
1212	TSWKNBGA	time to set value correction after acceleration finished
1212	TSWKNVGA	time to set value correction after deceleration finished
1212	TTEVUB	Battery-voltage depending delay time of canister purge valve
1212	TVFSAM	Delay time after DRIVE-position switch off
1212	TVFSEM	delay time after DRIVE-position switch on
1212	TVKTDTK	temperature dependant delay time for catalyst monitoring
1212	TVKUPHS	delay time for clutch switch during shifting in higher gear
1212	TVKUPRS	delay time for clutch switch during shifting in lower gear
1212	TVLADV	Integrator time constant at vlast-calculation
1212	TVLLRI	delay time to enable I-component after start-up
1212	TVLLRPD	Maximal delay time to enable PD components after start-up
1212	TVNWSTTM	delay time : enable of camshaft control after start, depending on engine temp
1212	TVSATEM	delay time for closing of the PCV after readiness for fuel cut off
1212	TVSATM	delay time after cranking for fuel cut off
1212	TVSLR	Duration of LRS downtime commanded via valve stroke control
1212	TVSUM	delay time for intake manifold switch over in dependence of engine temperatur
1212	TVUB	voltage correction
1212	TWDKSNST	time constant for filtering of reference throttle blade position
1212	TWDKSV	time constant for filtering of reference throttle blade position
1212	TWLRRTMS	waiting time up to check engine temp. signal exceeding threshold for closed loop
1212	TWSTT	threshold soak time for re-start
1212	TZ2FGRGA	double numerator time constant for cruise control
1212	UDKSNO	upper reference voltage threshold for diagnosis knock sensors
1212	UDKSNU	lower reference voltage threshold for diagnosis knock sensors
1212	UEVERG	Gear ratio depending of the gear
1212	URL2SUNM	conversion factor from ps->rl dependent on nmot.w for active SU (2nd flap)
1213	URL3SUNM	conversion factor from ps->rl dependent on nmot.w for active SU (1st + 2nd flap)
1213	URLNM	conversion factor from ps->rl dependent on nmot.w
1213	URLSUNM	conversion factor from ps->rl dependent on nmot.w for active SU (1st flap)
1213	VLMXVZ	Max. value for vlast_w
1213	WDKARN	threshold throttle angle for activation of the mixture adaptation





Page	Parameter	Descriptor
1213	WDKHKDN	High threshold throttle plate for altitude adaptation
1213	WDKHKN	Low threshold throttle plate for altitude adaptation
1213	WDKPMXN	maximum throttle angle for plausibility check with charge signal
1213	WDKSNLN	desired throttle angle at kl15 off
1213	WDKUGDN	throttle angle necessary for 95 % of the maximum possible air charge
1213	WEAN	angle injection break off
1213	WEEM	correction of prestorage angle
1213	WEEMRFAN	end of injection angle at max relative driver request
1213	WEESTATI	Offset for injection end angle towards early
1213	WEESTM	correction of pretiming of injection during start
1213	WEESTN	end of injection angle during start
1213	WFRL	fuel wall hang.up
1213	WKRLZOF	Bloc of fixed values: ignition reatard offset for guided cylinder
1213	WPEDKO	Accelerator position treshold for the A/C cut off
1213	WPFGRBMR	Back-calculated pedal value during acceleration with FGR
1213	WPHN	phase correction
1213	WPUAVLN	Throttle valve anglv as of which VL ambient pressure adaptation is active
1213	WPUAVLSN	Throttle valve angle as of which VL ambient pressure adaptation is blocked
1213	ZATMAML	time constant for exhaust gas temperature model
1213	ZATMAML2	time constant for exhaust gas temperature model bank2
1213	ZATMIKML	time constant for modelled temperature in catayst tikatm
1213	ZATMIKML2	time constant for modelled temperature in catayst bank 2
1213	ZATMKML	time constant for catalyst temperature model tkatm
1214	ZATMKML2	time constant for catalyst temperature model bank2
1214	ZATMRML	time constant for exhaust model temperature - pipe temperature
1214	ZATMRML2	time constant for exhaust model temperature - pipe temperature bank2
1214	ZBALM	reduction factor L-memory (tmot) for accel. enrichment
1214	ZBTEML	integration speed for canister charge adaptation
1214	ZDBTMN	time constant combustion chamber temperatur model for negativ gradient
1214	ZDBTMP	time constant combustion chamber temperatur model for positiv gradient
1214	ZKFRAOA	time constant for frao-integrator, f(number of starts with fuel in oil)
1214	ZKFRAUA	time constant for frau-integrator, f(number of starts with
1214	ZKMSDKT	integrator speed for fast constant mass-flow adaption
1214	ZKPVDKT	integrator speed for slow constant mass-flow adaption
1214	ZKRKATA	integration speed integrator rkat, f(abo)
1214	ZKRKAZA	integration speed integrator rkaz, f(abo)
1214	ZKTABTU	time constant for engine cooling
1214	ZLASOHML	time constant for PT1-filter of the pseude lambda behind catalyst
1214	ZLASOHML2	Time constant for PT1-filter of pseudo lambda post cat, bank 2
1214	ZLRHML	time constant of lambda control integrator downstream catalyst
1214	ZLRHML2	time constant of lambda control integrator downstream catalyst bank 2
1214	ZMDNSM	time constant for decay of torque offset after cranking
1214	ZPVDKR	time constant for filtering of pvdkr
1214	ZVALM	reduction factor L-memory (tmot) for decel. enleanment
1214	ZZWEETM	Switchover threshold pattern angle

## ASCETBLK 1.10 Description of ASCET block library

### FDEF ASCETBLK 1.10 Function definition

#### Representation of engine management functions:

To represent engine management functions physical information (data flow) is distinguished from digital control information (control flow).  
Data flow: load signal, speed, control factor  
Control flow: condition idle, switch driving position, error catalyst  
Solid lines mark the data flow, dotted lines mark the control flow.



#### Baseblocks (general description):

- Blocks with marker "NOV" store the value of the output (integrator value, flag, RAM-cell) in a non volatile RAM (otherwise in a volatile RAM). The behaviour of these blocks is identical to their pendants without "NOV" marker.
  - The main inputs and outputs ("in" and "out") have no symbol in the block icon; if there are no other characteristics their default values are 0.0 (float) bzw. FALSE (bool).
  - Unconnected inputs are configured with 0.0 (float) bzw. FALSE (bool), if there are no other agreements.
  - Some blocks have a special input at their left upper corner (default TRUE), usually connected with a calculation raster trigger to determine the frequency of calculation explicitly. Raster time describes the time gap between two cycles.
  - Any deviation from following default configuration of input and output values will be described in the documentation of each block.
- |         |               |               |                            |
|---------|---------------|---------------|----------------------------|
|         | brevé in icon | default value | designation                |
| INPUTS: | E             | TRUE          | enable calculation         |
|         | I             | FALSE         | initialization             |
|         | IV            | 0.0           | initial value              |
|         | K             | 0.0           | here: integration factor K |
|         | MX            | 1E35          | upper limitation of output |
|         | MN            | -1E35         | lower limitation of output |

#### ascetblk-teil0gb



#### Integrator K

new value of integrator := old value of integrator + K \* rasterTime \* in  
INPUTS: K integration factor



#### Integrator T

new value of integrator := old value of integrator + (rasterTime / T) \* in  
The minimum value of T is limited to rasterTime.  
INPUTS: T time constant of integration



#### Recursion

new value := old value + m \* (in - old value)  
INPUTS: m weighting factor



#### Lowpass

new value of lowpass := old value of lowpass + (rasterTime / T) \* (in - old value of lowpass)  
The minimum value of T will be limited to rasterTime.  
INPUTS: T time constant



#### Input-Switchover

The icon shows the default position of the switch, default value of non-wired inputs is 0.0 .



#### Exclusive-OR

Output-signal is TRUE when exactly one input-signal is TRUE.



#### Edge (bidirectional)

A positive or negative edge at input triggers a TRUE at output during this simulation step.



#### Maximum (2 inputs)

The value of output is equal to maximum of all input values.  
Output i indicates the index of first input generating maximum.

#### ascetblk-teil1gb



**Limiter**

The value of output-signal is equal to input-signal limited to the range [MN, MX].  
TRUE at output "B" indicates an active limitation, otherwise this output is FALSE.



**Absolute value**

The value of output-signal is equal to absolute value of input-signal.



**Hysteresis**

Wiring of hysteresis determines right and left breakover point of hysteresis:  
wired left breakover point right breakover point

LSP und delta	LSP	LSP + delta
LSP und RSP	LSP	RSP
delta und RSP	RSP - delta	RSP

All other wirings of the inputs LSP, RSP and delta produce FALSE as output-value (incorrect wiring).



**Signum**

Input value < 0.0, causes -1.0 at output, otherwise output value is equal to 1.0 .



**Accumulator**

The accumulator-value is changed by input-value and limited to the range [MN, MX].



**FLAG**

Imitation of one volatile 1 bit-RAM-cell.



**RAM**

Imitation of an volatile RAM-cell.

**ascetblk-teil2gb**



**RS-FlipFlop**

The RS-FlipFlop has a set-input S and a reset-input R, reset dominates set.  
The value of output !Q is always inverted to output Q.



**Delay raster**

Signal delay by one cycle of calculation grid, out(i) := in(i-1).  
A non-wired raster-input causes signal delay of one simulation step.



**Turn-off delay**

If input-signal switches from TRUE to FALSE the output-signal follows this alteration with a delay. Delay time is determined by input DELAY. Switching input to TRUE during delay time causes TRUE at output immediately.



**Turn-on delay**

If input-signal switches from FALSE to TRUE the output-signal follows this alteration with a delay. Delay time is determined by input DELAY. Switching input to FALSE during delay time causes FALSE at output immediately.



**Timer**

A positive edge at input starts the timer running down:  
- the start value of timer is determined by value at input SV (in seconds ).  
- the output switches to TRUE and stays TRUE until timer expires.  
Further positive edges at input have no effect until the timer time has expired.  
FALSE at input E stops the timer until TRUE at this input causes continuation of running down.

INPUTS: in start timers  
SV start value of timer  
OUTPUTS: B timer is running



**Timer-Retrigger**

Basic function like "Timer", difference: A further positive edge at input causes always restart of timer.

**ascetblk-teil3gb**



### Time-Counter

TRUE at input resets time-counter to 0.0. R = FALSE, starts time-counter.  
FALSE at input E stops the time-counter. The time-counter output shows the elapsed time in seconds.  
INPUTS: R reset of time-counter



### Counter

The counter will be incremented or decremented in every simulation step. True at input I causes determination of count-direction depending on actual startvalue and endvalue.  
If value of input SV is greater than value of input EV then counter counts up, otherwise it counts down until endvalue is reached. Reaching endvalue will be indicated by TRUE at output B.  
The counter may be stopped with help of input E.  
INPUTS: SV startvalue of counter  
EV endvalue of counter  
I initialize and start counter  
OUTPUTS: B endvalue reached



### Statemachine

The control flow is represented by logical gate arrays and statemachines. The sequence control in a statemachine may be modeled with help of states and transitions.

State: In a statemachine is always exactly one state active, that means all corresponding (ellipsis) actions will be done. The name of every state is represented inside the ellipsis.

Transition: The Transition from one state to an other one in case of fulfilling the state transition condition. All corresponding transition actions will be done.

The condition, that will be checked for transition, is shown beside the transition arrow.

The string beside the transition is only a logical name representing the condition. The afterfollowing text contains the full description. The condition with the lowest number has the highest priority.

Every statemachine has exactly one welldefined start state (S) and a reset state (R).

If RESET-condition is fulfilled in any state, the reset state becomes actual state for next simulation step.

ascetblk-teil4gb

## ABK ASCETBLK 1.10 Abbreviations

## FW ASCETBLK 1.10 Fixed Values

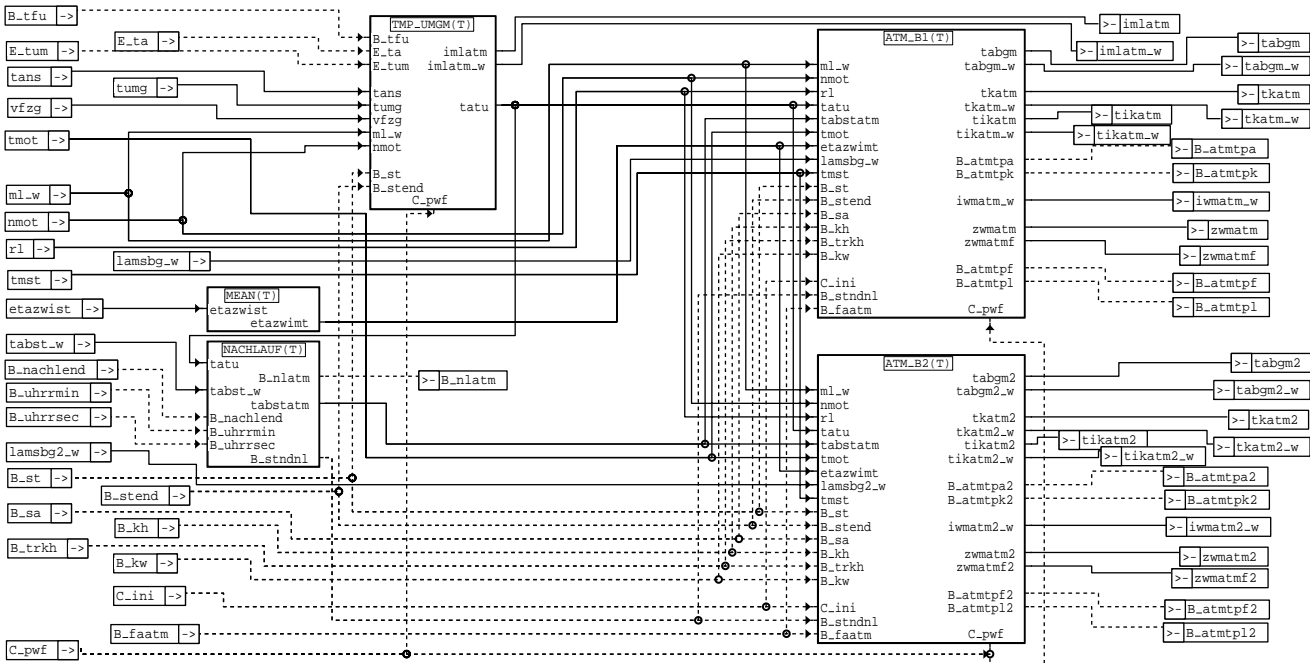
Parameter	Value	Description
-----------	-------	-------------

## FB ASCETBLK 1.10 Detailed description of function

## APP ASCETBLK 1.10 Application hint

## ATM 33.10 Exhaust temperature model

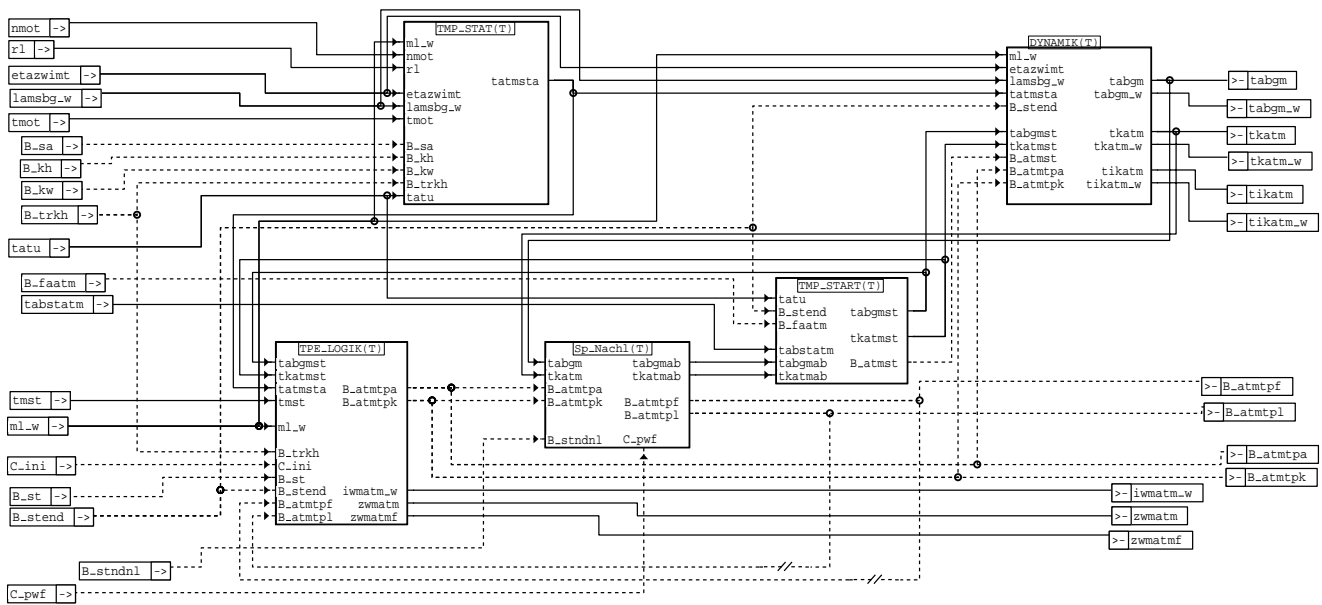
### FDEF ATM 33.10 Function definition



atm-atm

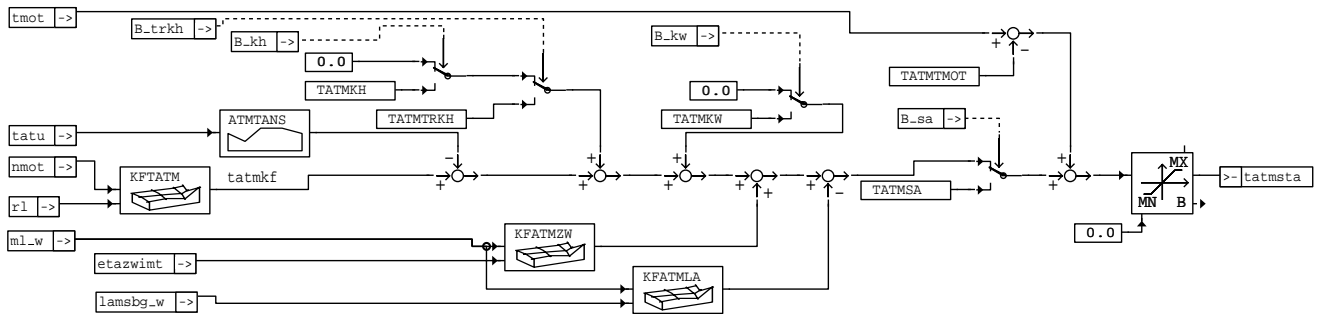


### ATM\_B1 Model overview



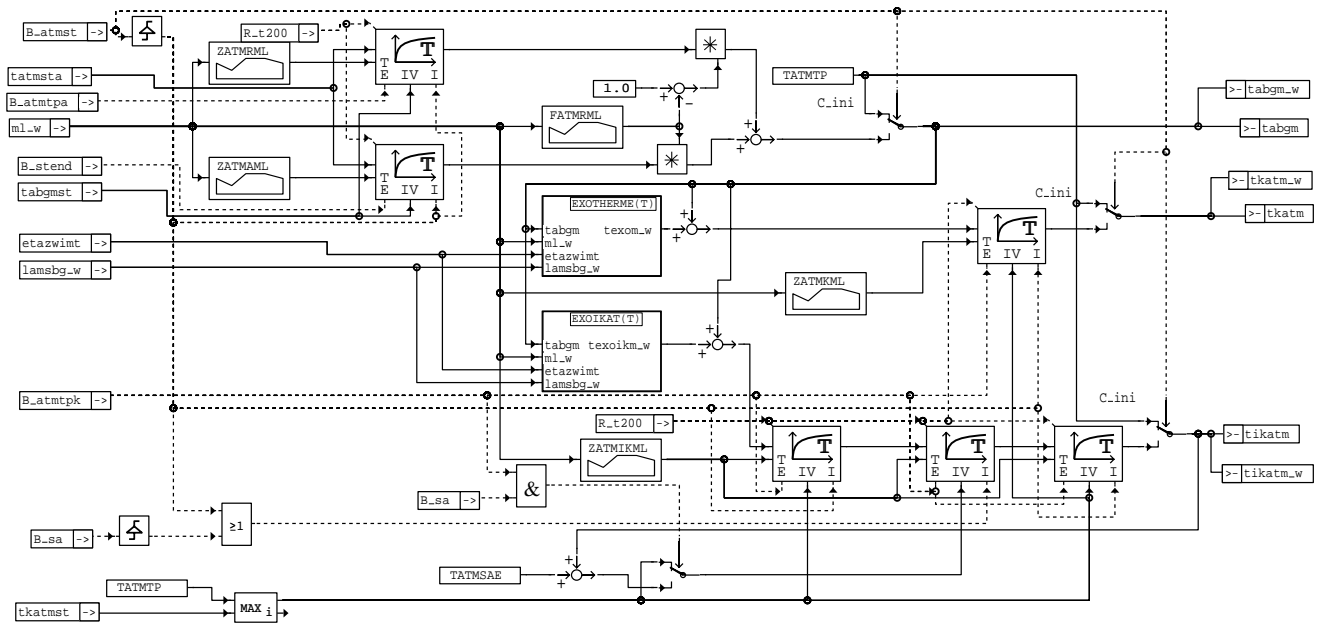
### atm-atm-b1

TMP\_STAT Temperature correction at fuel cutoff, intake air, catalyst heating warming, ignition angle, lambda and cold engine



### atm-tmp-stat

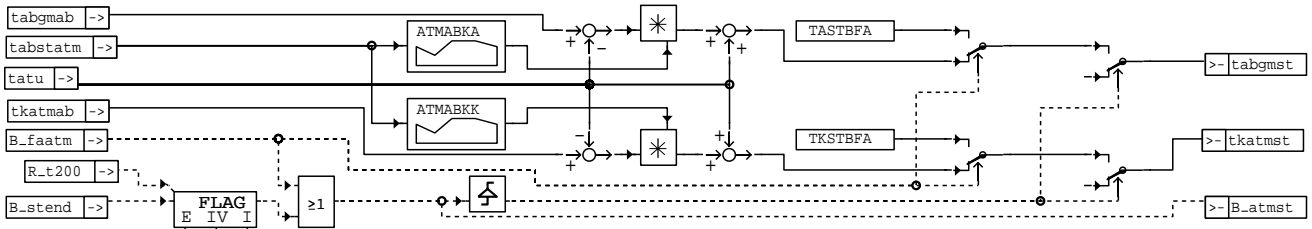
DYNAMIK Temperature-dynamics of exhaust gas, pipe-wall and catalyst



### atm-dynamik

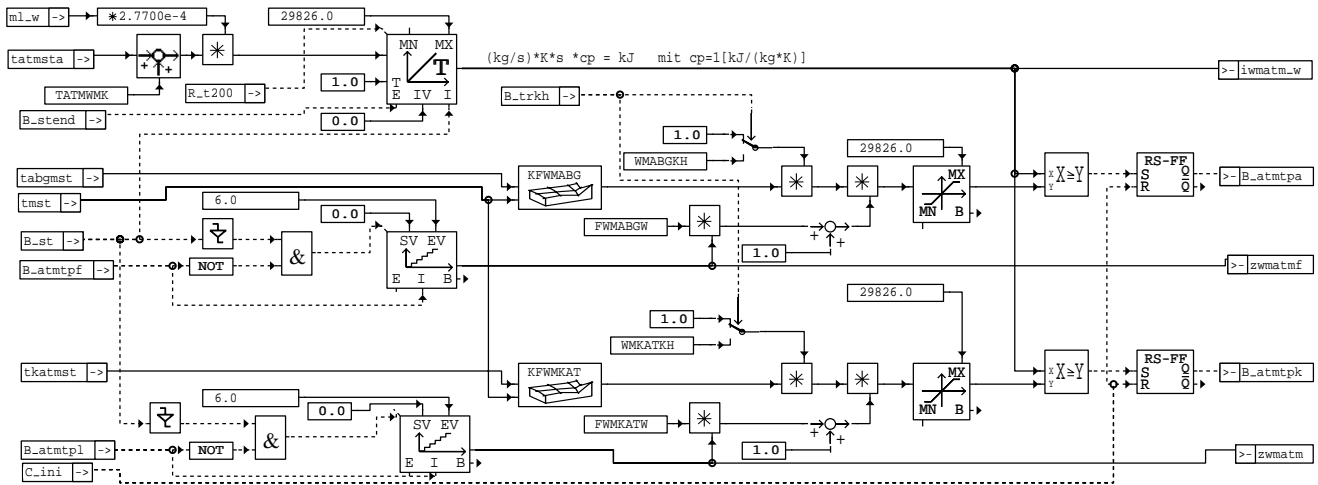


**TMP\_START** Calculation of exhaust gas - and pipe-wall temperature at engine start



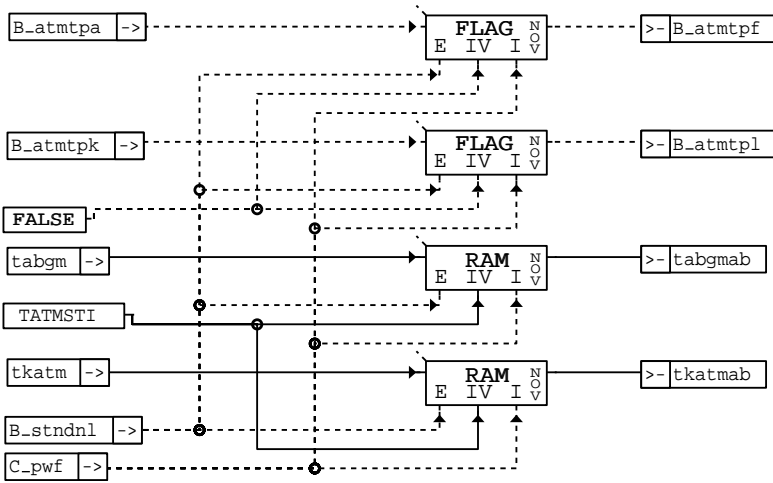
### atm-tmp-start

**TPE\_LOGIK** Calculation of exceed dew-point for lambdasensor upstream and downstream



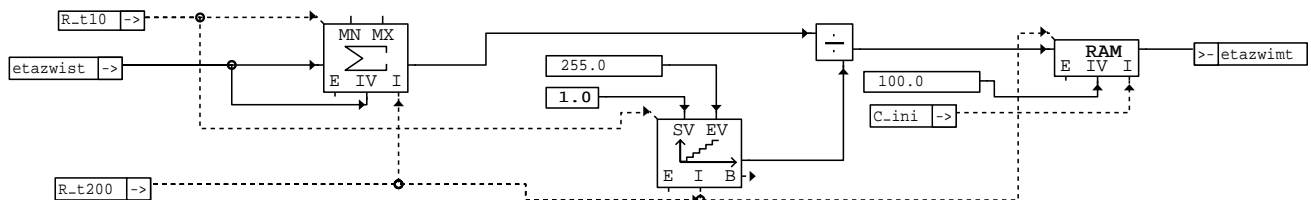
### atm-tpe-logik

**SP\_NACHL** Store exceed dew-point flag and temperature tabgm, tkatm at switch off delay



### atm-sp-nachl

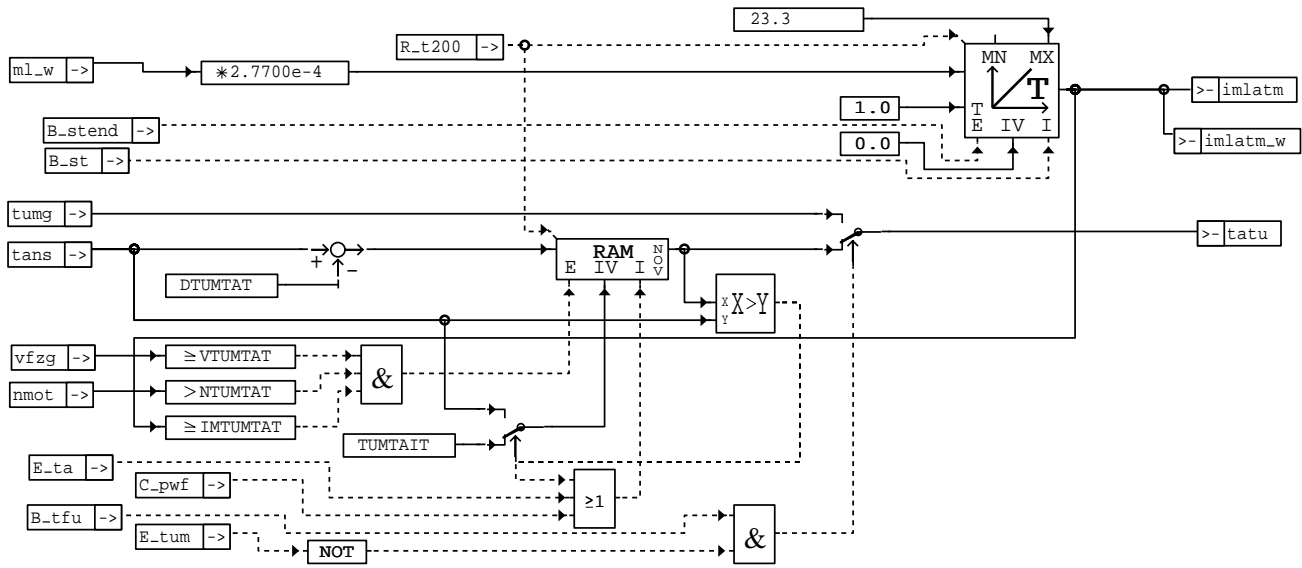
**MEAN** etazwist-mean-value



### atm-mean

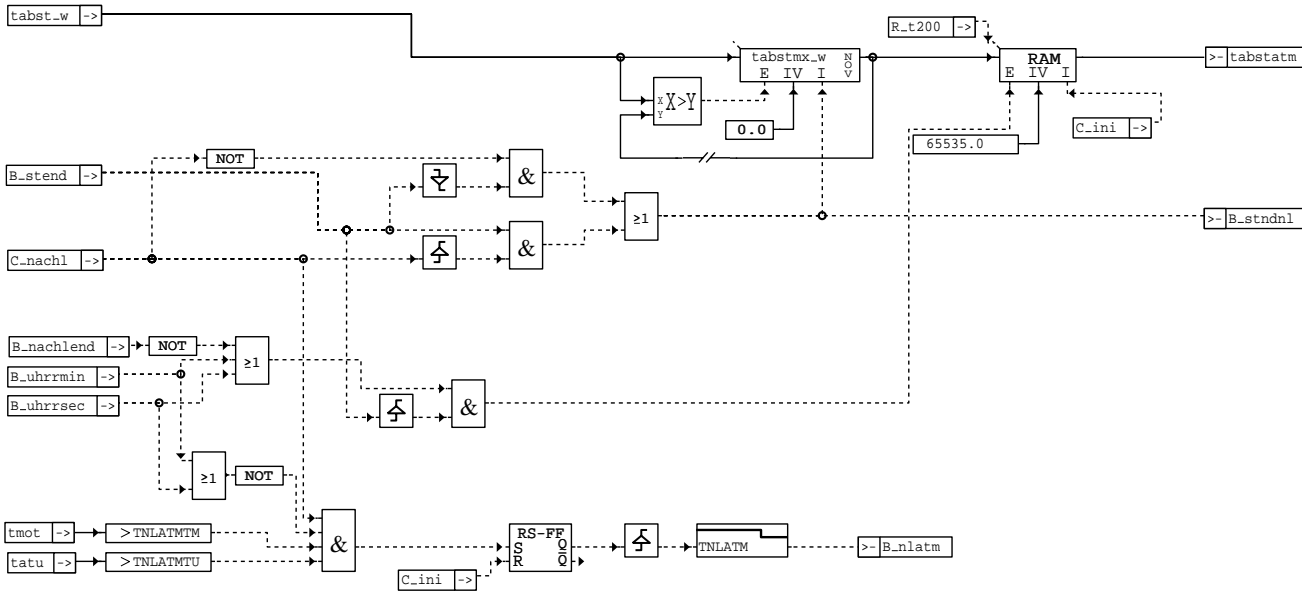


TMP\_UMGM If there is no ambient-air-sensor, calculation of the ambient temperature from tans (intake air temperature)



### atm-tmp-umgm

NACHLAUF If tabst\_w not ok tabstatm = max-value, B\_nlatm = f(tmot,tatu)



### atm-nachlauf

#### ABK ATM 33.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ATMABKA	TABSTATM		KL	factor reduction of exhaust gas temperature = f(soak time)
ATMABKK	TABSTATM		KL	factor reduction for catalyst temperature = f(soak time)
ATMTANS	TATU		KL	temperature correction of the exhaust model temperature
DTUMTAT			FW	offset intake-air temperatur -> ambient temperature
FATMRML	ML_W		KL	divide factor exhaust-/exhaust-pipe temperature
FATMRML2	ML_W		KL	divide factor exhaust-/exhaust-pipe temperature bank2
FWMABGW			FW	factor heat quantity upstream when dew-point end not reached last trip
FWMABGW2			FW	factor heat quantity upstream when dew-point end not reached last trip bank2
FWMKATW			FW	factor heat quantity downstream when dew-point end not reached last trip
FWMKATW2			FW	factor heat quantity downstream when dew-point end not reached last trip bank2
IMTUMTAT			FW	threshold integrated air mass for determination ambient temp. (from TANS)
KATMEXML	ML_W		KL	Temperature of the exotherme in the catalyst tkatm
KATMEXML2	ML_W		KL	Temperature of the exotherme in the catalyst , bank 2
KATMIEXML	ML_W		KL	Temperature of the exotherme in the catalyst tikatm
KATMIEXML2	ML_W		KL	Temperature of the exotherme in the catalyst tikatm, bank 2
KFATMLA	ML_W	LAMSBG_W	KF	map exhaust gas temperature correction = f(lambda)
KFATMLA2	ML_W	LAMSBG2_W	KF	map exhaust gas temperature correction = f(lambda) bank2
KFATMZW	ML_W	ETAZWIMT	KF	map exhaust gas temperature correction = f(ignition-variation)



Parameter	Source-X	Source-Y	Type	Description
KFATMZW2	ML_W	ETAZWIMT	KF	map exhaust gas temperature correktion = f(ignition) bank2
KFTATM	NMOT	RL	KF	map exhaust gas temperature f(nmot,rl)
KFTATM2	NMOT	RL	KF	map exhaus gas temperature f(nmot,rl) bank2
KFWMABG	TABGMST	TMST	KF	map for heat-quantity threshold dew-point end upstream bank1
KFWMABG2	TABGMST2	TMST	KF	map for heat-quantity threshold dew-point end upstream bank2
KFWMKAT	TKATMST	TMST	KF	map for heat quantity threshold dew-point end downstream
KFWMKAT2	TKATMST2	TMST	KF	map for heat quantity threshold dew-point end downstream bank 2
KLATMILAE	LAMSBG_W		KL	Temperature of the exotherme decrease during enrichment tikatm
KLATMILAE2	LAMSBG2_W		KL	Temperature of the exotherme decrease during enrichment tikatm, bank2
KLATMIZWE	ETAZWIMT		KL	Temperature of the exotherme decrease in cat during ignition retard tikatm
KLATMIZWE2	ETAZWIMT		KL	Temperature of the exotherme decrease in cat during ignition retard tikatm, bank
KLATMLAE	LAMSBG_W		KL	Temperature of the exotherme decrease during enrichment
KLATMLAE2	LAMSBG2_W		KL	Temperature of the exotherme decrease during enrichment, bank 2
KLATMZWE	ETAZWIMT		KL	Temperature of the exotherme decrease in cat during ignition retard tkatm
KLATMZWE2	ETAZWIMT		KL	Temperature of the exotherme decrease in cat during ignition retard, bank2
NTUMTAT			FW	threshold engine speed for determination ambient temperature (from TANS)
TABGMEX			FW	Exhaust-gas temperature below the catalyzer light-off temperature
TASTBFA			FW	modelled-temperature exhaust gas start value at B_faاتم-condition function
TATMKH			FW	exhaust gas temperature correction at catalyzer heating
TATMKH2			FW	exhaust gas temperature correction at catalyzer heating bank2
TATMKW			FW	exhaust gas temperature correction at catalyzer warming
TATMSA			FW	exhaust gas temperature at fuel cut off
TATMSAE			FW	exothermal temperature offset at fuel cut off
TATMSAE2			FW	exothermal temperature offset at fuel cut off, bank2
TATMSTI			FW	initial value tabgm, tkatm at power fail
TATMTMOT			FW	engine temperature warmed up engine, for temperature correction cold engine
TATMTP			FW	exhaust temperature at dew point
TATMTRKH			FW	correction of exhaustgas temperature at catalyzer fast heating
TATMTRKH2			FW	correction of exhaustgas temperature at catalyzer fast heating, bank2
TATMWMK			FW	Temperature offset for heat-quantity calculation
TIKATMOE			FW	Temperature correction in catalyzer without exotherm reaction tikatm
TKATMOE			FW	Temperature correction catalyzer without exotherm reaction tkatm
TKSTBFA			FW	modelled-temp. catalyzer start value at B_faاتم-cond.(short dew-point end time)
TNLATM			FW	minimal ECM-afterrun for ATM - afterrun-time
TNLATMTM			FW	at tmot > limit ECM_afterrun for ATM B_nlatm = 1
TNLATMTU			FW	at tumg (tatu-ATM) > limit SG-afterrun-time B_nlatm = 1
TUMTAIT			FW	initial value of ambient temperature (from TANS)
VTUMTAT			FW	threshold velocity for determination ambient temperature from TANS
WMABGKH			FW	factor for heat-quantity-correction at catalyzer heating for dew-point end
WMABGKH2			FW	factor for heat-quantity-correction at catalyzer heating for dewpoint-end bank2
WMKATKH			FW	factor for heat-quantity-correction at cat. heating for B_atmtpk downstream cat.
WMKATKH2			FW	factor for heat-quantity-correction at cat. heating for B_atmtpk downstream cat.
ZATMAML	ML_W		KL	time constant for exhaust gas temperature model
ZATMAML2	ML_W		KL	time constant for exhaust gas temperature model bank2
ZATMIKML	ML_W		KL	time constant for modelled temperature in catalyzer tikatm
ZATMIKML2	ML_W		KL	time constant for modelled temperature in catalyzer bank 2
ZATMKML	ML_W		KL	time constant for catalyzer temperature model tkatm
ZATMKML2	ML_W		KL	time constant for catalyzer temperature model bank2
ZATMRML	ML_W		KL	time constant for exhaust model temperature - pipe temperature
ZATMRML2	ML_W		KL	time constant for exhaust model temperature - pipe temperature bank2
Variable	Source		Type	Description
B_ATMST	ATM		LOK	Flag start-value tabgmst, tkatmst calculated
B_ATMST2	ATM		LOK	Flag start-value tabgmst, tkatmst calculated bank 2
B_ATMTPA	ATM		AUS	condition temperature upstream catalyzer exceeds dew-point
B_ATMTPA2	ATM		AUS	condition temperature upstream catalyzer exceeds dew-point2
B_ATMTPF	ATM		AUS	condition dew-point exceeds upstream (last trip)
B_ATMTPF2	ATM		AUS	condition dew-point exceeds upstream (last trip) bank2
B_ATMTPK	ATM		AUS	condition temperature downstream catalyzer exceeds dew-point
B_ATMTPK2	ATM		AUS	condition temperature downstream catalyzer exceeds dew-point2
B_ATMTPPL	ATM		AUS	condition temperature downstream catalyzer exceeds dew-point (last trip)
B_ATMTPPL2	ATM		AUS	condition temperature downstream catalyzer exceeds dew-point (last trip) bank2
B_FAATM			EIN	condition function request short dew-point end time
B_KH	BBKHZ		EIN	condition catalyzer heating activated
B_KW	BBKHZ		EIN	Condition catalyzer warming
B_NACHLEND	MOTAUS		EIN	condition ECU switch off delay regularly finished
B_NLATM	ATM		AUS	request for ECM exhaust-temp.modell ATM
B_SA	MDRED		EIN	Condition fuel cut-off
B_ST	SWADAP		EIN	condition for start
B_STEND	BBSTT		EIN	condition end of start
B_STNDNL	ATM		LOK	condition start of ECU-after run or end of start (1->0)
B_TFU	PROKON		EIN	condition ambient temperature sensor exists
B_TRKH	BBKHZ		EIN	Flag for catalyzer fast heating
B_JHRRMIN	PROKON		EIN	Condition clock with a relative counter of minutes
B_UHRRSEC	PROKON		EIN	Condition clock with a relative counter of seconds
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_NACHL			EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
ETAZWIMT	ATM		LOK	mean efficiency at actual ignition angle (200 ms)
ETAZWIST	MDIST		EIN	actual ignition angle effectiveness
E_TA	GGTFA		EIN	error flag: TANS





Variable	Source	Type	Description
E_TUM		EIN	Error Flag: ambient (air) temperature tumg
IMLATM	ATM	AUS	integrated air mass flow from engine start to maximum value
IMLATM_W	ATM	AUS	integrated air mass flow from engine start to max. value (word)
IWMATM2_W	ATM	AUS	heat quantity to dew-point end
IWMATM_W	ATM	AUS	heat quantity to dew-point end
LAMSBG2_W	LAMSOLL	EIN	required lambda limitation Bank2
LAMSBG_W	LAMSOLL	EIN	Desired Lambda limitation (word)
ML_W	EGFE	EIN	air mass flow filtered (Word)
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
R_T10		EIN	Time schedule 10 ms
R_T200		EIN	Time schedule 200 ms
TABGM	ATM	AUS	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	AUS	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TABGM2_W	ATM	AUS	Exhaust gas temperature in front of the catalyzer from model (Word) bank2
TABGMAB	ATM	LOK	exhaust gas temperature (modelled) at switch off
TABGMAB2	ATM	LOK	exhaust gas temperature (modelled) at switch off
TABGMST	ATM	LOK	Exhaust gas temperature at engine start
TABGMST2	ATM	LOK	Exhaust gas temperature at engine start bank2
TABGM_W	ATM	AUS	Exhaust gas temperature in front of the catalyzer from model (Word)
TABSTATM	ATM	LOK	soak time at ECM for ATM
TABSTMX_W	ATM	LOK	soaking time maximum query for exhaust gas temp. model
TABST_W	BGTABST	EIN	soak time
TANS	SWADAP	EIN	Intake air temperature
TATMKF	ATM	LOK	exhaust gas temperature-modelled from map KFTATM
TATMKF2	ATM	LOK	exhaust gas temperature-modelled from map KFTAMT bank2
TATMSTA	ATM	LOK	exhaust gas temperature-modelled steady-stade
TATMSTA2	ATM	LOK	exhaust gas temperature-modelles steady-stade
TATU	ATM	LOK	intake air or ambient temperature
TEXOIKM2_W	ATM	LOK	Bank2
TEXOIKM_W	ATM	LOK	exothermic temperature increase in the catalyst for tikatm
TEXOM2_W	ATM	LOK	exothermic temperature increase in the catalyst for tkatm2, bank2
TEXOM_W	ATM	LOK	exothermic temperature increase in the catalyst for tkatm
TIKATM	ATM	AUS	exhaust gas temperature in catalyst (modelled)
TIKATM2	ATM	AUS	exhaust gas temperature in catalyst (modelled) bank2
TIKATM2_W	ATM	AUS	exhaust gas temperature in catalyst (modelled) bank2
TIKATM_W	ATM	AUS	exhaust gas temperature in catalyst (modelled)
TKATM	ATM	AUS	catalyst temperature (model)
TKATM2	ATM	AUS	catalyst temperature (model), bank2
TKATM2_W	ATM	AUS	catalyst temperature modelled (word) bank2
TKATMAB	ATM	LOK	exhaust gas temperature downstream cat.(modelled) at switch off
TKATMAB2	ATM	LOK	exhaust gas temperature downstream cat.(modelled) at switch off bank 2
TKATMST	ATM	LOK	catalyst temperature modelled start value = f(last value, soak time)
TKATMST2	ATM	LOK	catalyst temperature modelled start value = f(last value, soak time) bank 2
TKATM_W	ATM	AUS	catalyst temperature modelled (word)
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
TUMG		EIN	Ambient air temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)
ZWMATM	ATM	AUS	counter for dew-point end not reached for heat quantity threshold
ZWMATM2	ATM	AUS	counter for dew-point end not reached for heat quantity threshold
ZWMATMF	ATM	AUS	counter for dew-point end not reached for heat quantity threshold upstream
ZWMATMF2	ATM	AUS	counter for dew-point end not reached for heat quantity threshold upstream

### FB ATM 33.10 Detailed description of function

The simulated exhaust and catalyst temperature is used:

- For catalyst monitoring: If the catalyst temperature falls short of its light-off temperature, then this catalyst could erroneously be detected as defective.
- For the downstream Lambda control: The downstream Lambda controller is activated after cranking, but only, if the catalyst has exceeded its light-off temperature.
- For sensor heater control after engine start: If the simulated dew point temperature has been exceeded, then the sensor heater can be completely turned on.
- For sensor heater control monitoring: If the exhaust temperature exceeds a given threshold (e.g. 800 deg C), then the sensor heater is turned off (in order to avoid overheating of the sensor).
- For engine fan control: Activation of engine fan during power latch when tabgm > TABGLF and other conditions (see %MLS).
- For switch-on protection of components by mixture enrichment

By introducing this function, only approximations of the exhaust and catalyst temperature are obtained. For application especially the monitoring areas

- dew point characteristic of the exhaust
  - catalyst monitoring
  - activation and deactivation of the sensor heater
  - switch-on protection of components
- must be critically observed.



## 1. Base function temperature $t_{atmsta}$

The steady state exhaust gas temperature upstream catalyst is determined by the  $n_{mot}/r_l$  dependent characteristic map KFTATM. This temperature is corrected by

- ambient temperature (ATMTANS)
- fuel cutoff (TATMSA)
- catalyst heating or - warming (TATMKH, TATMKW)
- ignition angle (KFATMZW temperature =  $f(ML, ETAZWIST)$ )
- lambda nominal value (KFATMLA temperature =  $f(ML, LAMSBG\_W)$ )
- cold engine temperature (TMOT - TATMTMOT ; TATMTMOT = 90 °C)

The temporal influence of the exhaust gas temperature upstream and downstream of the catalyst:

This function is simulated with filter for exhaust gas, pipe-wall and catalyst. The "heat transport" is approx. proportional to the air massflow. Therefore, the filter time constants are depending on airflow and determined by a characteristic line. The appropriate filter values reflect the exhaust gas temperature upstream of catalyst (ZATMAML), pipe-wall (ZATMRML) and downstream of catalyst (ZATMKML).

Correction of exhaust gas temperature with time characteristic of the pipe wall temperature.

If the exhaust gas temperature in the manifold increases 'in jumps', initially with a small time constant (5-15s) the exhaust gas temperature upstream of the cat. increases by a specific (smaller) amount. Then the exhaust gas temperature increases further as a result of the heating up of the exhaust pipe, with a larger time constant (50-200s). This pipe wall temperature effect is especially necessary in more precise exhaust gas temperature simulation. The pipe wall temperature effect is shown by a filter (with high time constant) which is calculated parallel to the filter for the exhaust gas temperature. Splitting of the two effects is dependent on air-mass. At low air-mass flow the pipe wall temperature effect is significantly greater than at higher air-mass flow. The filter value for the exhaust gas temperature is multiplied directly by the splitting factor (FATMRML), while the filter value for the pipe wall temperature is multiplied by a factor (1-FATMRML).

The two corrected filter values are added together and produce the exhaust gas temperature.

During extended fuel cutoff conditions with low exhaust gas temperatures, the catalyst may fall short of the light-off temperature. For these operating conditions, the exhaust temperature at the filter input is switched to the constant value TATMSA.

During catalyst heating ( $B_{-kh} = 1$ ) temperature TATMKH is added to TATMML characteristic line.

As long as condensation in the exhaust system is detected by the "Dewpoint end" detecting logic, then the almost constant temperatures  $t_{abgmst}$  or  $t_{katmst}$  are simulated by switching ( $B_{-atmtpa}$ ,  $B_{-atmtpk}$ ) the filters to this values. The "Dewpoint end" set time must always be longer than the condensed water in the wall near the lambda sensor.

At low  $t_{atu}$   $t_{kabgm}$  and  $t_{katm}$  are corrected with the curve ATMTANS.

## 2. "Dewpoint end"-detection

Temperature  $t_{abgmst}$  and  $t_{katmst}$  at engine start.

At switch off delay ( $C_{-nachl} = 1$ ) the modelled temperatures  $t_{abgm}$  and  $t_{katm}$  are stored.

At engine start the start-temperature  $t_{abgmst}$  is calculated as a function of stored temperature  $t_{abgm}$  and stop-time ( $t_{abst\_w}$ ) as a characteristic curve ATMAKA (cooling down factor) corrected with ambient temperature.

The calculation for  $t_{katmst}$  is similar to the calculation of  $t_{abgmst}$ .

Integrated heat quantity  $i_{wmatm\_w}$

The exceed dew-point time is nearly proportional to the integrated heat quantity after engine start.

Heat quantity is the integral of temperature ( $t_{atmsta}$ ) \*  $m_l$  \*  $c_p$  (nearly 1 kJ / (kg\*k))

Exceed dew-point time for the lambda sensor upstream flag  $B_{-atmtpa}$  and lambda sensor downstream flag  $B_{-atmtpk}$

The calculated start-temperature  $t_{abgmst}$  should be the pipe-wall-temperature at engine start.

If the temperature  $t_{abgmst}$  is lower than 60 °C then condensation water could be in the pipe. At the map KFWMABG the threshold values for the heat quantity can be set.

The higher the air massflow and the temperature  $t_{atmsta}$  get after cranking, the shorter are the "dewpoint end" times.

Extension of the "dewpoint end" times

In case the condensation has not completely evaporated after the last start (due to short engine operation), and in the meantime the exhaust system has cooled off, then even more condensation must evaporate during the following engine run.

If the "dewpoint end" time for the catalyst temperature has not been reached ( $B_{-atmtpk}$ ) after the last engine start,

then a counter is incremented. The higher the number of those starts the higher is the factor to increase the threshold value of the map KFWMABG-values.

If the integrator ( $i_{wmatm\_w}$ ) reaches the thresholds, then the appropriate conditions  $B_{-atmtpa}$  resp.  $B_{-atmtpk} = 1$  are set.

## 3. Temperature changes on ignition retard and fuel enrichment.

As the engine efficiency falls due to ignition retard the exhaust gas temperature increases. The temperature changes can be set at the map KFATMZW. ( $etazwimt$  is the mean value over 200ms of the  $etazwist$ -value)

With fuel enrichment the exhaust gas temperature falls. The temperature correction is set in the map KFATMLA.

## APP ATM 33.10 Application hint

### 1. Installation locations of temperature measuring sensors for application purposes (listed in direction of exhaust flow)

- For sensor installation upstream of catalyst
  1. Exhaust gas temperature (center of pipe) for high temperatures at high load for sensor heating shut-off
  2. Pipe wall temperature for determining the "dewpoint end" times (protection from condensation)
- upstream of catalyst
  3. Exhaust gas temperature (center of pipe) for determining the light-off temperature of the catalyst
- in catalyst
  4. Ceramic temperature in catalyst (in the last third of catalyst or touching the end of monolith) for determining the airflow dependent time constants
- downstream of catalyst
  5. Pipe wall temperature at the Lambda sensor location for determining the "dewpoint end" time

The temperature measuring point 3 may not be necessary if the distance from sensor to catalyst is less than 30 cm. In this case, the temperature difference from sensor location to catalyst may be neglected.



## 2. Characteristic map KFTATM

The steady state exhaust gas temperature upstream catalyst depends on nmot and rl. The values of the characteristic map could be set at driving on a roller test bench. Better values have to be set at driving on road conditions.

## 3. Characteristic line ZATMAML, ZATMKML, ZATMRML, FATMRML

The air massflow dependent time constants ZATMAML (temperature measuring points 1 and 3), as well as ZATMKML ( temperature measuring point 4) can be determined by means of "load jumps", or more accurately of "airflow jumps". In this case, full load and especially fuel cutoff conditions are to be avoided at "airflow jumps".

Example: For an airflow jump from 30 kg/h to 80 kg/h, the measured time constant is referred to 80 kg/h.

## 4. The "dewpoint end" times for exhaust gas temperatures (exhaust pipe center) and pipe wall are very different. For "dewpoint end" times, the pipe wall temperatures upstream of catalyst (measuring point 2) resp. downstream of catalyst (temperature measuring point 5) should be used. In case, these times are too long (concerning delayed readiness for operation of the Lambda control), then the temperature characteristics at the sensor location must be evaluated in more detail. In order to avoid sensor damaging due to condensation, the maximum sensor heating may only be applied, when the dewpoint temperature has been exceeded or the "dewpoint end" time has been detected, and therefore, condensation can no longer occur.



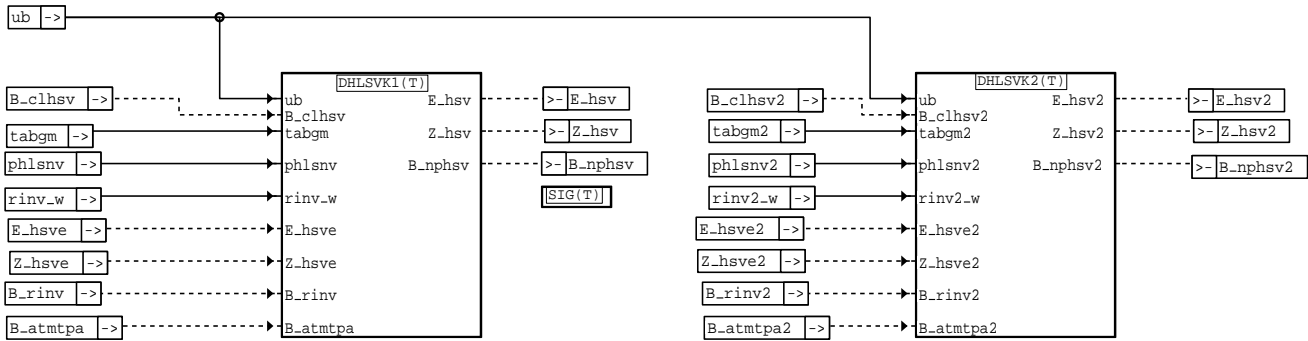
Typical values:

KFTATM	[grd C]	nmot [l/min]	800	1200	1800	2400	3000	4000	5000	6000
		rl[-]	15	380	400	420	450	480	520	580
	22	400	420	450	480	520	550	580	610	
	30	420	450	480	520	550	580	610	650	
	50	450	480	520	550	580	610	650	700	
	70	470	520	550	580	610	660	700	750	
	100	490	550	580	610	650	700	750	790	
	120	510	560	610	650	700	750	790	840	
	140	530	580	650	700	750	790	840	900	
KFATMZW	[grd C]	ML [kg/h]	20	40	80	150	250	400		
		ETAZWIST[-]	1.0	0	0	0	0	0		
		0.95	15	40	50	60	70	75		
		0.90	15	60	80	100	125	140		
		0.80	20	80	120	150	180	200		
		0.70	25	100	150	190	210	220		
		0.60	30	115	175	210	230	245		
KFATMLA	[grd C]	ML [kg/h]	20	40	80	150	250	400		
		LAMSBG_W[-]	1.15	5	10	30	50	60	70	
		1.0	0	0	0	0	0	0		
		0.95	5	10	20	30	40	45		
		0.90	15	25	40	50	60	75		
		0.80	30	40	60	70	85	100		
		0.70	40	60	80	90	100	120		
KFWMABG	[kJ]	tabgmst [Grad C]	-40	0	15	25	50			
		tmst [Grad C]	-40	200	160	150	140	100		
		0	180	150	120	110	80			
		15	160	140	60	55	30			
		25	140	120	30	30	15			
		60	120	30	15	10	5			
KFWMKAG	the values correspond to KFWMABG * 5									
ZATMAML	ml [kg/h], Zeitkonst. [sek]	10, 30 ; 20, 20 ; 40, 13 ; 80, 5 ; 180, 4 ; 400, 3 ;								
ZATMKML	ml [kg/h], Zeitkonst. [sek]	10, 150 ; 20, 60 ; 40, 35 ; 80, 20 ; 180, 10 ; 400, 7 ;								
ZATMRML	ml [kg/h], Zeitkonst. [sek]	10, 300 ; 20, 80 ; 40, 55 ; 80, 30 ; 180, 20 ; 400, 10 ;								
FATMRML	ml [kg/h], Zeitkonst. [sek]	10, 0.5 ; 20, 0.6 ; 40, 0.7 ; 80, 0.8 ; 180, 0.95 ; 400, 0.95 ;								
TATMTTP	Temp [Grad C]	50								
ATMABKA	tabst [s] , Faktor	10, 0.95 ; 50, 0.7 ; 180, 0.5 ; 360, 0.3 ; 600, 0.15 ; 1000, 0 ;								
ATMABKK	tabst [s] , Faktor	10, 0.90 ; 50, 0.6 ; 180, 0.4 ; 360, 0.25 ; 600, 0.15 ; 1000, 0 ;								
ATMTANS	TANS [°C], Temp [Grad C]	-40, 60 ; -10, 20 ; 20, 0 ;								
TATMSA	Temp [Grad C]	100								
TATMKH	Temp [Grad C]	200								
TATMKW	Temp [Grad C]	100								
TATMTMOT	Temp [Grad C]	90								
TUMTAIT	Temp [Grad C]	20								
TASTBFA	Temp [Grad C]	40								
TKSTBFA	Temp [Grad C]	40								
TATMWMK	Temp [Grad C]	- 80								
WMABGKH	Faktor	0.3								
FWMABGW	Faktor	0.25								
FWMKATW	Faktor	0.25								
DTUMTAT	temperature [°C]	20								
VTUMTAT	velocity [km/h]	40								
NTUMTAT	engine speed [l/min]	1800								
IMTUMTAT	air mass [kg]	1								
TNLATMTM	temp [deg. C]	80								
TNLATMTU	temp [deg C]	5								
TNLATM	time [s]	660								

## DHLSVK 3.20 Diagnosis sensor heating upstream catalyst

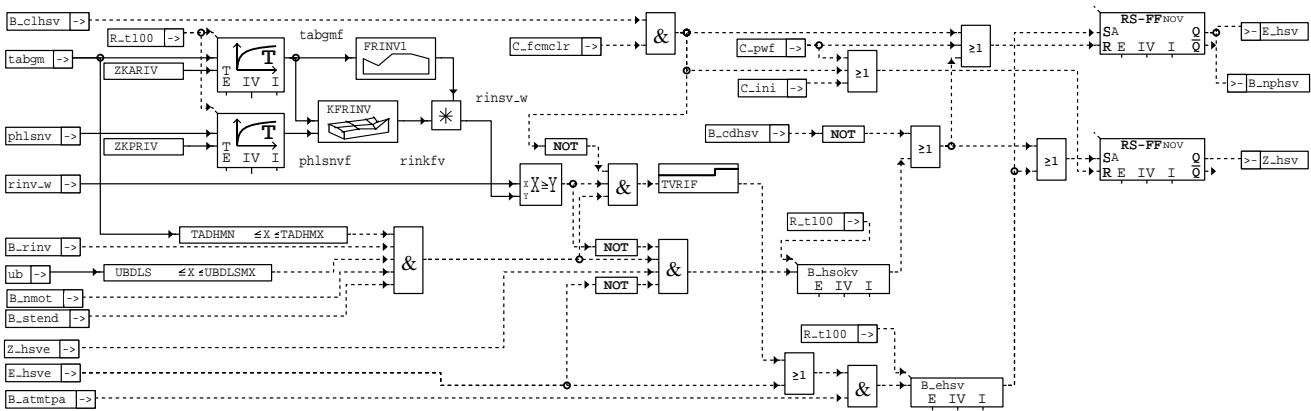
### FDEF DHLSVK 3.20 Function definition

Overview heater diagnosis



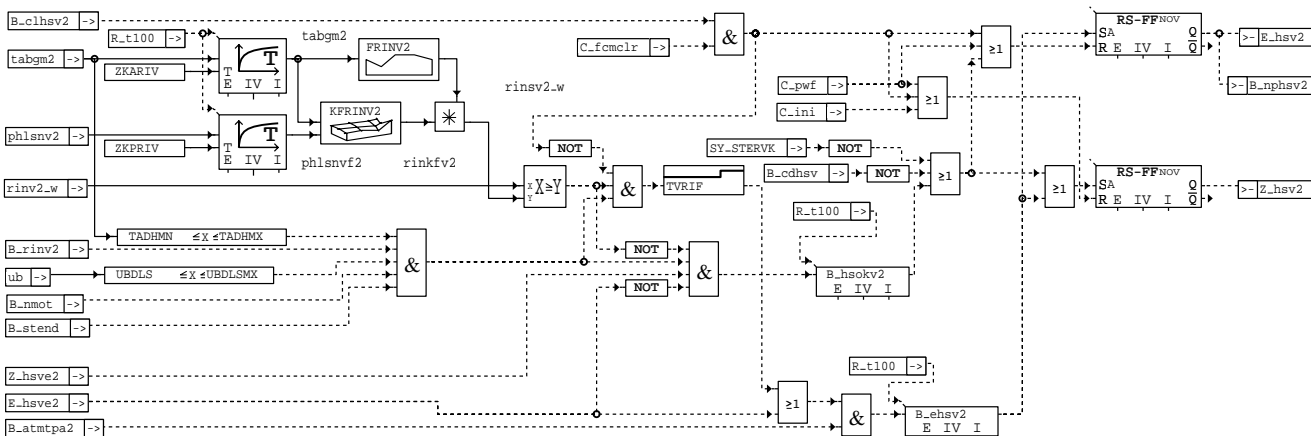
### dhlsvk-dhlsvk

Heater diagnosis bank1 upstream catalyst



### dhlsvk-dhlsvk1

Heater diagnosis bank2 upstream catalyst



### dhlsvk-dhlsvk2

Status fault path: sfphsv  
 Error flag: E\_hsv  
 Cycle flag: Z\_hsv  
 Fault type: TYP\_hsv:  
 (B\_mxhsv, B\_mnhsv, B\_sihsv, B\_nphsv)  
 Clear fault path: B\_clhsv

Default value active: B\_bkhsv (optional)  
 Fault path code: CDTHSV  
 Fault class: CLAHSV  
 Fault intensity: TSFHSV  
 CARB CODE: CDCHSV  
 Table of ambient cond.: FFTHSV



## ABK DHLSVK 3.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCHSV	BLOKNR		KL	code word CARB: lambda sensor heating upstream cat
CDCHSV2	BLOKNR		KL	code word CARB: lambda sensor heating upstream cat; (bank2)
CDTHSV			FW	code word tester: oxygen sensor heater upstream catalyst
CDTHSV2			FW	code word tester: oxygen sensor heater upstream catalyst, cyl. row 2
CLAHSV			FW	fault class: heating of O2 sensor upstream cat
CLAHSV2			FW	fault class: heating of O2 sensor upstream cat bank 2
FFTHSV	BLOKNR		KL	Table of ambient condition for heating O2-sensor pre cat
FFTHSV2	BLOKNR		KL	Table of ambient condition for heating O2-sensor post cat bank 2
FRINV1	TABGMF		KL	Multiplicativ factor for RIN desired value pre cat
FRINV2	TABGMF2		KL	Multiplicativ factor for RIN desired value pre cat
KFRINV	TABGMF	PHLSNVF	KF	MAP for Nernst resistor pre cat
KFRINV2	TABGMF2	PHLSNVF2	KF	MAP for Nernst resistor post cat , bank 2
TADHMN			FW	lower Temperature threshold for die heater diagnostic routine
TADHMX			FW	upper Temperature threshold for die heater diagnostic routine
TSFHSV			FW	fault active time: lambda sensor heating catalyst upstream
TSFHSV2			FW	fault active time: lambda sensor heating catalyst upstream, bank 2
TVRIF			FW	Delay time for Ri fault
UBDLS			FW	battery voltage threshold for release the sensor diagnosis
UBDLSMX			FW	upper battery voltage threshold for the sensor diagnosis
ZKARIV			FW	Filter time constant for modeling of dynamic of ceramic temp. from ATM pre cat
ZKPRIV			FW	Filter for modeling of dynamic of ceramic temp. from electric circuit pre cat

Variable	Source	Type	Description
A	DHLSVK	LOK	vector ECU-states
BLOKNR		EIN	DAMOS source for block number
B_ATMTPA	ATM	EIN	condition temperature upstream catalyst exceeds dew-point
B_ATMTPA2	ATM	EIN	condition temperature upstream catalyst exceeds dew-point2
B_CDHSV	PROKON	EIN	function active per codeword CDHSV
B_CLHSV		EIN	condition clear failure path DHLSVK
B_CLHSV2		EIN	condition clear failure path DHLSVK2
B_EHSV	DHLSVK	LOK	Condition error HSV
B_EHSV2	DHLSVK	LOK	Condition error HSV2
B_HSOKV	DHLSVK	LOK	Condition Lambda sensor heating OK pre cat
B_HSOKV2	DHLSVK	LOK	Condition Lambda sensor heating 2 OK pre cat
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_NPHSV	DHLSVK	AUS	Nernst resistance sensor upstream of the catalyzer too large
B_NPHSV2	DHLSVK	AUS	Nernst resistance sensor 2 upstream of the catalyzer too large
B_RINV	GGLSV	EIN	Condition: Internal resistance Ri of O2 sensor activ,pre cat
B_RINV2	GGLSV	EIN	Condition: Internal resistance Ri of O2 sensor activ,pre cat bank 2
B_STEND	BBSTT	EIN	condition end of start
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail intialisation
E_HSV	DHLSVK	AUS	error flag: lambda sensor heating upstream cat
E_HSV2	DHLSVK	AUS	error flag: lambda sensor heating upstream cat on the right
E_HSVE	DHLSVKE	EIN	error flag: lambda sensor heating upstream cat (Endstufe)
E_HSVE2	DHLSVKE	EIN	error flag: lambda sensor heating upstream cat on the right (Endstufe)
PHLSNHF	DHLSVK	DOK	Standardized heating power of Lambda sensor downstream of catalyzer, filtered
PHLSNV	HLS	EIN	normalized heating power of lambda sensor upstream of catalyzer
PHLSNV2	HLS	EIN	normalized heating power of lambda sensor 2 upstream of catalyzer
PHLSNVF2	DHLSVK	DOK	Norm heating power of lambda sensor 2 pre cat, filtered
RINKFV	DHLSVK	DOK	Internal resistance of lambda sensor from map pre cat
RINKFV2	DHLSVK	DOK	Internal resistance of lambda sensor 2 from map pre cat
RINSV2_W	DHLSVK	DOK	Limit value of internal resistor of Nernst cell of lambda sen post cat bank 2
RINSV_W	DHLSVK	DOK	Limit value of internal resistor of Nernst cell of lambda sen. post cat
RINV2_W	GGLSV	EIN	Actuel value of internal resistance of lambda sensor 2, pre ca
RINV_W	GGLSV	EIN	Actuel value of internal resistance of lambda sensor,pre cat (word)
R_T100		EIN	Time schedule 100 ms
SFPHSV	DHLSVK	AUS	Fault-path status: Lambda-sensor heating upstream of catalytic converter
SFPHSV2	DHLSVK	AUS	Fault-path status: Lambda-sensor 2 heating upstream of catalytic converter
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TABGMF	DHLSVK	DOK	Exhaust gas temperature upsteam cat from exhaust temperature -filtered-
UB	SWADAP	EIN	battery voltage
Z_HSV	DHLSVK	AUS	cycle flag of lambda sensor heating upstream cat
Z_HSV2	DHLSVK	AUS	cycle flag of lambda sensor heating upstream cat, cylinder row 2
Z_HSVE	DHLSVKE	EIN	cycle flag of lambda sensor heating upstream cat (Endstufe)
Z_HSVE2	DHLSVKE	EIN	cycle flag of lambda sensor heating upstream cat, cylinder row 2 (Endstufe)

Parameter	Value	Description
CDTHSV		code word tester: oxygen sensor heater upstream catalyst
CDTHSV2		code word tester: oxygen sensor heater upstream catalyst, cyl. row 2
CLAHSV		fault class: heating of O2 sensor upstream cat
CLAHSV2		fault class: heating of O2 sensor upstream cat bank 2
TADHMN		lower Temperature threshold for die heater diagnostic routine
TADHMX		upper Temperature threshold for die heater diagnostic routine
TSFHSV		fault active time: lambda sensor heating catalyst upstream
TSFHSV2		fault active time: lambda sensor heating catalyst upstream, bank 2
TVRIF		Delay time for Ri fault



Parameter	Value	Description
UBDLS		battery voltage threshold for release the sensor diagnosis
UBDLSMX		upper battery voltage threshold for the sensor diagnosis
ZKARIV		Filter time constant for modeling of dynamic of ceramic temp. from ATM pre cat
ZKPRIV		Filter for modeling of dynamic of ceramic temp. from electric circuit pre cat

### FB DHLSVK 3.20 Detailed description of function

With this DHLSVK an indirect check is performed on whether the heating of the Lambda sensor is operational, i.e. the measurement of the heater current by means of a shunt performed so far is abandoned.

As criterion for the diagnosis the internal resistance of the Nernst cell of the Lambda sensor is used. With defective sensor heating the internal resistance (rin<sub>v\_w</sub>) is essentially larger. For the determination of rin<sub>v\_w</sub> the sensor voltage must be periodically connected to load with 0,5mA for 10ms (%GGLSV).

In addition the switching behaviour of the heater power stage is monitored in the CJ920.

Diagnosis internal resistance of the Nernst cell

Since the internal resistance rin<sub>v\_w</sub> is also dependent on the exhaust gas temperature and on the el. heating performance (phl<sub>snv</sub>), the typical value of rin<sub>v\_w</sub> is stored in a map from tab<sub>gm</sub> and phl<sub>snv</sub>.  
tab<sub>gm</sub> and phl<sub>snv</sub> are filtered, since a change only affects rin<sub>v\_w</sub> after a delay.

Preconditions:

1. rin<sub>v\_w</sub> is updated (B<sub>\_rin<sub>v\_w</sub></sub> = 1)
2. The exhaust gas temperature is greater than the threshold TADH<sub>MN</sub> and lower than TADH<sub>MX</sub>
3. UB is within the diagnosis range

Diagnosis:

If rin<sub>v\_w</sub> is less than rin<sub>sv\_w</sub>, then B<sub>\_hsokv</sub> is set (Ri OK!) if additionally the switching behaviour of the power stage is OK.  
If rin<sub>v\_w</sub> is greater, then B<sub>\_nphsv</sub> is set (Ri is of too high-resistance).

Diagnosis switching behaviour of the heater power stage

For diagnosis purposes the power stage is switched off every 10s for 100ms (in %HLS resp. %HLSHK).

The diagnosis of the power stage %DECJ detects via a serial interface to the CJ920 an abnormal behaviour of the power stage and gives the faults B<sub>\_mxhsve</sub>, B<sub>\_mnhsv</sub> and B<sub>\_sihsve</sub>.

The fault E<sub>\_hsve</sub> also sets the fault E<sub>\_hsv</sub>.

Fault management

The debouncing of the heater faults is performed during two drives. If a heater fault is detected the fault lamp is only triggered if a fault is again detected during the second drive.

### APP DHLSVK 3.20 Application hint

Fault memory relevant values of the %DHLSVK are assigned to the %DFPM<sub>hsv</sub> in the function-orientated selection.

To be adjusted:

TADH <sub>MN</sub> = 200°C	UHSN = 13.0V (%HLSHK)	Filter values	LSH25P	LSH25PL	LSF4.7
UBDLS = 10.7V	TADH <sub>MX</sub> = 600°C	ZKARIH =	20s	46s	21s
UBDLSMX = 15.5V		ZKPRIH =	35s	35s	10s

TVRIF = 6s

The debouncing time for B<sub>\_nphsv</sub> is set to the triple value of TRIIMPH (in %GGLSV), i.e. the fault is only registered after three Ri measurements.

KFRIN<sub>V\_W</sub>

The map values are determined by a measuring sensor with typical Nernst and heater internal resistance (from K3-LS/ESV).

The measuring sensor must be of the same type as the intended control sensor.

Adjust exhaust gas temperature to a base point value by an according selection of load and engine speed. It is possible to adjust phl<sub>snv</sub> (performance) to a base point value by changing THSVKTA (in %HLS resp. %HLSHK). Enter the value of rin<sub>v\_w</sub> into the map after approx. 60s.







## FB DSWEC 6.20 Detailed description of function

### 1. General function description

#### 1.1 Task of the function

The task of the %DSWEC is to detect that a rough road is being driven across by means of the transmitted wheel acceleration bsc. As soon as a rough road is detected the bit b\_swe\_c is set upon which, e.g. the rough road detection is temporarily deactivated (also see %DMDSTP). The deactivation is necessary since drive shaft vibrations due to a rough road can lead to a misdetection of misfire.

#### 1.2 Reference source of the wheel acceleration signal bsc(n)

The wheel acceleration signal bsc(n) needed for the evaluation is made available by a customer-specific function %BGRBS. In principle 3 different versions of the %BGRBS can be distinguished:

- (a) In the standard version the %BGRBS receives that wheel acceleration (maximum selection), which is send by the ABS ECU via the CAN-bus.
- (b) In case the ABS ECU transmits the no. of wheel rotations instead of the wheel acceleration via the CAN-bus, a conversion of the no. of wheel rotations into wheel acceleration is performed in the %BGRBS.
- (c) Special solution for vehicles without CAN-bus on which, however, an ABS-sensor is mounted, but no segment times are formed in the motronic. In this case the %BGRBS calculates the wheel acceleration from the wheel speed.  
Hint : On vehicles without CAN-bus (resp. also without ABS ECU) but with mounted ABS-sensor the segment times should preferably be formed from the ABS sensor signal and for the rough road detection the %DSWER should be used.

#### 1.3 Signal requirement for bsc(n)

The wheel acceleration signal bsc(n) must have been derived from the ABS wheel sensor signal. The accuracy should be at least  $1 [m/s^2]$  and it should preferably be present in the 10ms time grid.

### 2. Concrete description of the signal path

#### 2.1 Filtering of the the acceleration signal

From the acceleration signal bsc(n) the memory value bssp(n) is formed by non-linear filtering as follows:

$$\begin{aligned} bssp(n) &= bssp(n-1) + FIBSALU * [ bsc(n) - bssp(n-1)] && \text{for } bsc(n) > bssp(n-1) && (1) \\ bssp(n) &= bssp(n-1) - FABSALU * (\text{time interval}) && \text{for } bsc(n) < bssp(n-1) && (2) \end{aligned}$$

(time interval = 100 ms)

The filter calculation for the upward control (1) is performed in the same time grid in which the signal bsc(n) is available [usually in the 10ms or in the 20ms grid]. The filter calculation for the downward control (2) is on contrast performed only in the 100ms time grid.

[For the selection of the filter coefficients also see application hints.]

#### 2.3 Rough road decision

The filter output value bssp(n) is compared to the threshold FSWALUV,1. FSWALUV,1 is a speed-dependent characteristic line with 4 base points. (with interpolation, result is fswares).

For B\_wk=0 FSWALU is accessed, for B\_wk=1 FSWAKLUV1 is accessed.

As long as the value bssp(n) lies above FSWALUV,1 the bit B\_swev is set.

As long as no error is detected (E\_swe = 0; is formed in %BGRBS), the output signal b\_swe\_c corresponds to the bit B\_swev.

However, as soon as the result of the rough road calculation is no longer meaningful, due to an error (E\_swe = 1; e.g. defect ABS wheel sensor) the rough road bit b\_swe\_c is set to zero. Thus it is avoided that, e.g. in case of a sensor fault, the misfire detection is permanently deactivated via b\_swe\_c. [ The decision on whether in this case the misfire detection should be deactivated or not must take place in the %DMDSTP].

#### 2.4 Deactivation of the function via the Euro-switch B\_cdswe

The function %DSWEC is deactivated if the Euro-switch has the value B\_cdswe = 0. In this case always b\_swe\_c = 0.

## APP DSWEC 6.20 Application hint

### Reference source bsc(n)

For the use of the %DSWEC a customer-specific function %BGRBS is necessary, which supplies the necessary input signal bsc(n). [For this also see point 1.2 of the function description !]

### Selecting the filter coefficients

The filter coefficient FIBSALU for the upward control of the value bssp(t) must be chosen so great that a sufficiently quick rough road detection is possible. In case the acceleration signal is directly available from the ABS ECU via CAN-bus, a filtering may possibly not be necessary for upward control. In this case FIBSALU can be set to one.

### Calculation of the acceleration

Measured values e.g. DIM:

Mode of acquisition: time-synchronous

ECU-grid: 10ms

Scanning time: 10ms

Analog window1 (length: 30sec or longer): bsc, bssp

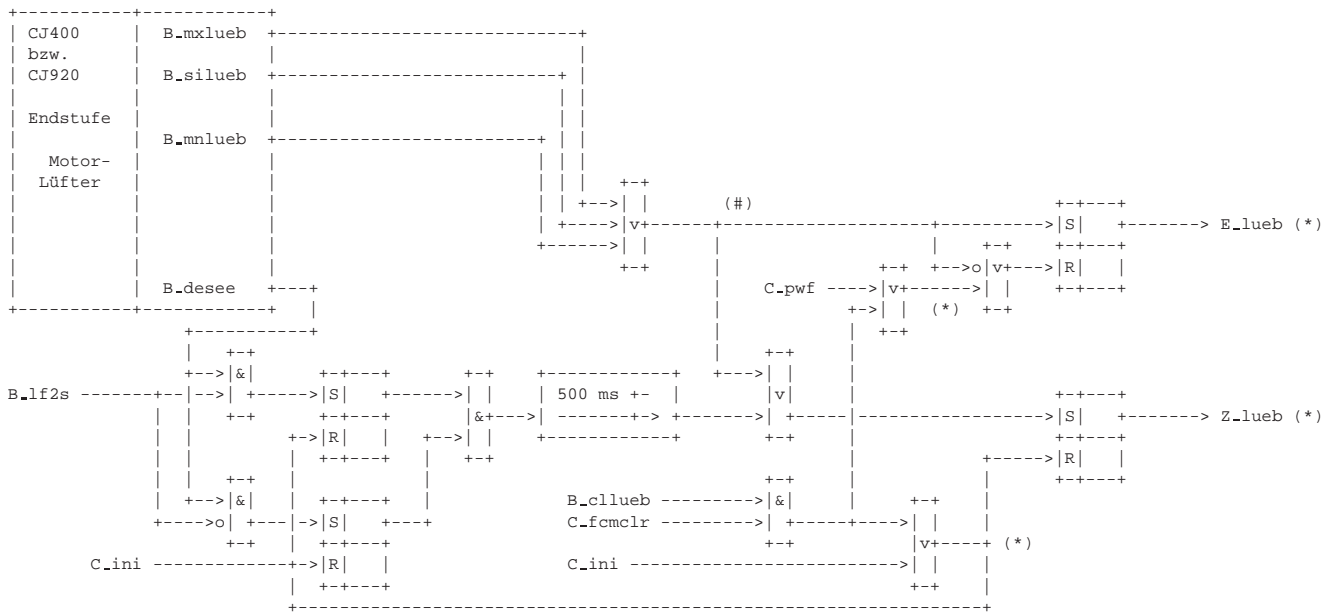
Digital window (length: as analog window1): b\_swe\_c

Digits: vfzg





Diagnosis CJ400, resp. CJ 920 see %DECJ



(\*) deviant from the description this path is served in the module %DFPM resp. the flags are managed in %DFPM;  
 (#) deviant from the description this path is served in the module %DECJ;

Substitution measures: non

error memory management:  
-----

Status error path luea, lueb: SFPLUEA, SFPLUEB  
 Error flag : E\_luea, E\_lueb  
 Cycle flag : Z\_luea, Z\_lueb  
 Error type : B\_mnluea, B\_mnluea  
 B\_mxluea, B\_mxluea  
 B\_siluea, B\_siluea  
 Delete error path:  
 Error path : CDTLUEA, CDTLUEB  
 Error class : CLALUEA, CLALUEB  
 Error intensity : TSFLUEA, TSFLUEB  
 Carb code : CDCLUEA, CDCLUEB  
 Environmental conditions : FFTLUEA, FFTLUEB

### ABK DMLSE 9.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCLUEA	BLOKNR		KL	code word CARB: Power stage engine fan A
CDCLUEB	BLOKNR		KL	Code word CARB: Power stage engine fan B
CDTLUEA			FW	code word tester: Power stage engine fan A [253]
CDTLUEB			FW	code word tester: Power stage engine fan B [252]
FLCLUEA			FW	fault set debouncing: Power stage engine fan A
FLCLUEB			FW	Fault set debouncing: Power stage engine fan B
HLCLUEA			FW	fault reset debouncing: Power stage engine fan A
HLCLUEB			FW	fault reset debouncing: Power stage engine fan B
TSFLUEA			FW	fault active time: power stage engine fan A
TSFLUEB			FW	fault active time: power stage engine fan B

Variable	Source	Type	Description
B_CLMLE		EIN	condition: clear fault path cooling fan power stage
B_DESEE	DMLSE	LOK	Diagnosis power stage: entry conditions fulfilled
B_LF1S	LFS	EIN	fan 1 on condition
B_LF2S	LFS	EIN	fan 2 on condition
C_INI	SWADAP	EIN	ECU-condition for intialisation
E_LUEA	DMLSE	AUS	error flag: electric fan output stage A
E_LUEB	DMLSE	AUS	error flag: electric fan output stage B



Variable	Source	Type	Description
Z_LUEA	DMLSE	AUS	cycle flag: electric fan output stage A
Z_LUEB	DMLSE	AUS	cycle flag: electric fan output stage B

### FW DMLSE 9.30 Fixed Values

Parameter	Value	Description
CDTLUEA		code word tester: Power stage engine fan A [253]
CDTLUEB		code word tester: Power stage engine fan B [252]
FLCLUEA		fault set debouncing: Power stage engine fan A
FLCLUEB		Fault set debouncing: Power stage engine fan B
HLCLUEA		fault reset debouncing: Power stage engine fan A
HLCLUEB		fault reset debouncing: Power stage engine fan B
TSFLUEA		fault active time: power stage engine fan A
TSFLUEB		fault active time: power stage engine fan B

### FB DMLSE 9.30 Detailed description of function

Together with the CJ400/CJ920 diagnosis %DECJ the secondary air valve power stage diagnosis forms a function unit. The diagnosis describes the forming of the error bit E\_luea/b and of the cycle bit Z\_luea/b.

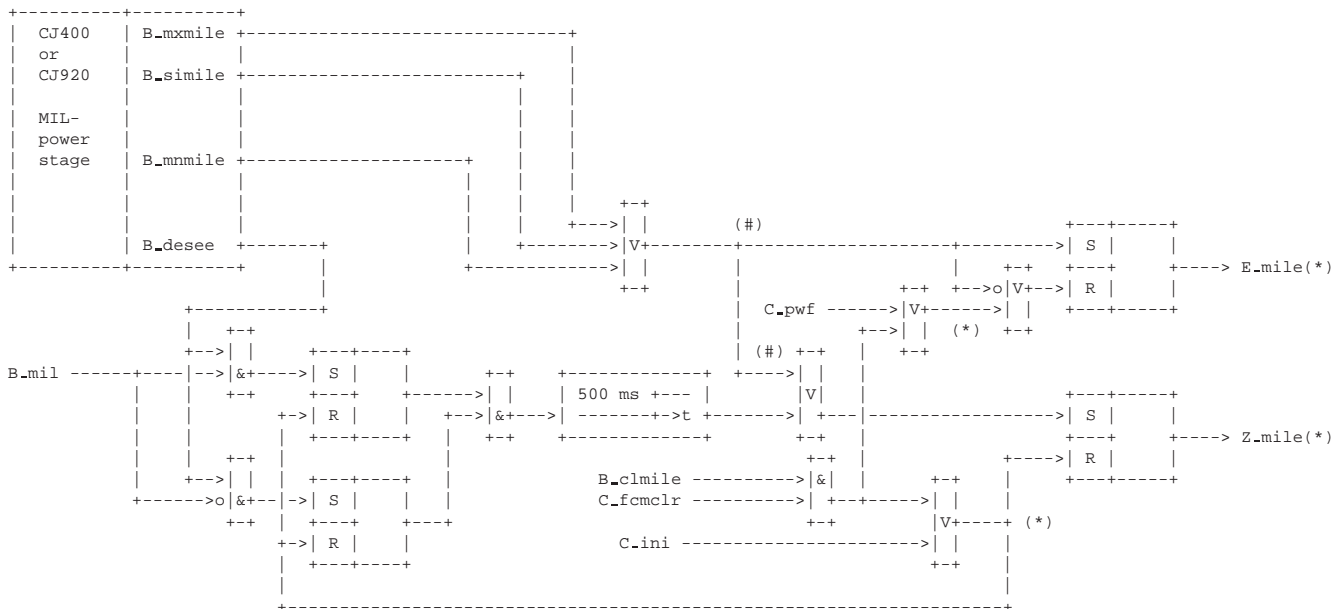
The setting of the cycle flag is performed for one via an error entry and for the other via a definitely checked not to be due error. This definite check is given if both switch states of the power stage, i.e. an on-state and an off-state were reached once. If an error is detected an error verification is activated in %DECJ which is performed independent of the external power stage request and which is definitely terminated after approx. 500 ms. Thereafter the the cycle flag is set in case no error occurred.

### APP DMLSE 9.30 Application hint

## DMILE 8.20 OBDII; MIL-power stage

### FDEF DMILE 8.20 Function definition

Diagnose CJ 400, or CJ 920 see %DECJ



(\*) in difference to this description this part is handled within module %DFPM.  
 (#) in difference to this description this part is handled within module %DECJ.

Fault path managment:  
-----

Status of fault path mile: sfpmile  
 Errorflag MILE: E\_mile  
 Cycleflag MILE: Z\_mile  
 Fault types MILE: B\_mxmile; B\_mmmile; B\_simile

Delete fault path: C\_fmclr & B\_clmile  
 Tester code fault path MILE: CDTMILE  
 Class of fault path MILE: CLAMILE  
 Fault active time MILE: TSFMILE  
 CARB-code MILE: CDCMILE  
 Ambient conditions MILE: FFTMILE



### ABK DMILE 8.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCMILE	BLOKNR		KL	Code word CARB: MIL power stage
CDTMILE			FW	code word tester: MIL power stage
CLAMILE			FW	error class: MIL power stage
FFTMILE	BLOKNR		KL	freeze frame table: MIL power stage
TFSMILE			FW	fault active time: MIL power stage

Variable	Source	Type	Description
B_CLMILE	DMILE	LOK	condition clear fault path MIL power stage
B_DESEE	DKOSE	EIN	Diagnosis power stage: entry conditions fulfilled
B_MIL		EIN	MIL turn-on
B_MNMLE	DMILE	AUS	Error type: short circuit to ground at MIL power stage
B_MXMLE	DMILE	AUS	Error type: short circuit to B+ at MIL power stage
B_SIMILE	DMILE	AUS	Error type: interruption at MIL power stage
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail intialisation
E_MILE	DMILE	AUS	Error flag: MIL power stage
SFPMILE	DMILE	AUS	status fault path: MIL power stage
Z_MILE	DMILE	AUS	Cycle flag: MIL power stage

### FW DMILE 8.20 Fixed Values

Parameter	Value	Description
CDTMILE		code word tester: MIL power stage
CLAMILE		error class: MIL power stage
TFSMILE		fault active time: MIL power stage

### FB DMILE 8.20 Detailed description of function

Precondition for this diagnostic of the MIL powerstage is the use of powerstage type CJ401.  
Recognition of non plausible function of the powerstage and its fault type is described in %DECJ.

#### Activation of the cycle flag:

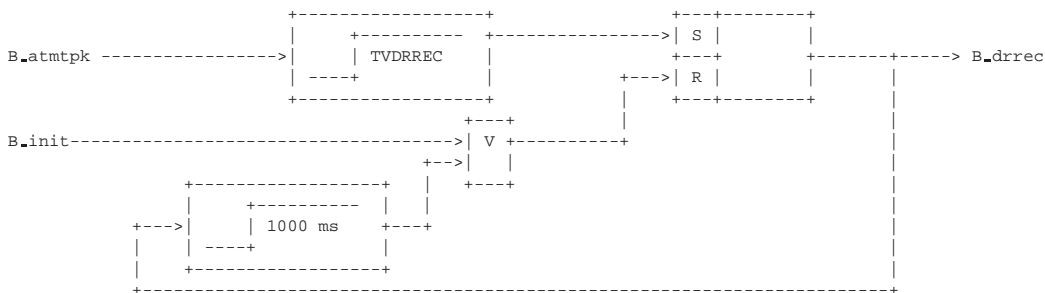
Whenever both states on/off of the powerstage are reached without fault, the cycle flag is set.  
If with one of the states on/off a fault occurs, %DECJ starts a verification in addition to the regular use of the powerstage.  
Duration of this verification is less than 500ms. If the fault is detected with this verification, the cycle flag is set.

### APP DMILE 8.20 Application hint

Default value for CDTMILE = 165 dez.

## DMS 6.10 Diagnosis; permanent data aquisition (serial)

### FDEF DMS 6.10 Function definition



### ABK DMS 6.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TVDRREC			FW	Delay time for trigger driverecorder

### FW DMS 6.10 Fixed Values

Parameter	Value	Description
TVDRREC		Delay time for trigger driverecorder



## FB DMS 6.10 Detailed description of function

Zur Auslösung der Aufzeichnung des Drive-Recorder-Dauermessmodus wird das Bit B\_drrec erzeugt.  
Gemäß der Spezifikation des Drive-Recorders soll das Triggerbit < 10 s anstehen.

Um bei den Dauerlaufmessungen zu kurze Fahrzyklen auszuschließen (z.B. um auch die Werte der Widerstandsmessung der Hinterkat-Sonde korrekt zu erfassen) wird das Triggerbit B\_drrec ans die Taupunkterkennung nach Kat mit zusätzlicher Verzögerungszeit gekoppelt.

Ferner werden für das Dauerlaufmesssystem verschiedene Bits auf Byte bzw. Wortgrößen zusammengefasst, um die Datenübertragung zu vereinfachen.

Byte-Größen: (zur einfacheren grafischen Darstellung bei Auswertung der Messungen)  
Zur einfacheren Auswertung der Bytes sind nicht verwendete Bits mit 1 auf gefüllt. (Alles ok = FF)

Projekte Fire, B-Motor - Eco:

B0.0 = Z_kat1	B1.0 = Z_tfm
B0.1 = Z_hsh	B1.1 = Z_fral
B0.2 = Z_lashl	B1.2 = Z_swe
B0.3 = Z_lshl	B1.3 = Z_md04
B0.4 = Z_hsv	B1.4 = Z_md03
B0.5 = Z_latvl	B1.5 = Z_md02
B0.6 = Z_latpl	B1.6 = Z_md01
B0.7 = Z_lsvl	B1.7 = z_md
W150.0 = 0	W151.0 = B_tesl15h
W150.1 = 0	W151.1 = B_mldyn
W150.2 = B_tehb	W151.2 = B_dlatp
W150.3 = B_te	W151.3 = B_gaefra
W150.4 = B_lrhk	W151.4 = B_gae
W150.5 = B_lr	W151.5 = B_fra
W150.6 = B_sa	W151.6 = B_tra
W150.7 = B_ll	W151.7 = B_lra
W150.8 = 0	W151.8 = 0
W150.9 = 0	W151.9 = 0
W150.10 = 0	W151.10 = 0
W150.11 = 0	W151.11 = 0
W150.12 = B_dkatlp	W151.12 = 0
W150.13 = B_dkatsp	W151.13 = 0
W150.14 = B_dkatst	W151.14 = 0
W150.15 = B_dkatst	W151.15 = 0

Projekte C-Motor

B0.0 = Z_kat1	B1.0 = Z_ev1	B2.0 = 1
B0.1 = Z_hsh	B1.1 = Z_swe	B2.1 = 1
B0.2 = Z_lashl	B1.2 = Z_md05	B2.2 = 1
B0.3 = Z_lshl	B1.3 = Z_md04	B2.3 = 1
B0.4 = Z_hsv	B1.4 = Z_md03	B2.4 = Z_sue
B0.5 = Z_latvl	B1.5 = Z_md02	B2.5 = Z_nwse
B0.6 = Z_latpl	B1.6 = Z_md01	B2.6 = Z_tfm
B0.7 = Z_lsvl	B1.7 = z_md	B2.7 = Z_fral
W150.0 = 0	W151.0 = B_tesl15h	
W150.1 = 0	W151.1 = B_mldyn	
W150.2 = B_tehb	W151.2 = B_dlatp	
W150.3 = B_te	W151.3 = B_gaefra	
W150.4 = B_lrhk	W151.4 = B_gae	
W150.5 = B_lr	W151.5 = B_fra	
W150.6 = B_sa	W151.6 = B_tra	
W150.7 = B_ll	W151.7 = B_lra	
W150.8 = 0	W151.8 = 0	
W150.9 = 0	W151.9 = 0	
W150.10 = 0	W151.10 = 0	
W150.11 = 0	W151.11 = 0	
W150.12 = B_dkatlp	W151.12 = 0	
W150.13 = B_dkatsp	W151.13 = 0	
W150.14 = B_dkatst	W151.14 = 0	
W150.15 = B_dkatst	W151.15 = 0	



Projekte B-Motor y

B0.0 = Z_hsv2	B1.0 = 1	B2.0 = 1
B0.1 = Z_latv2	B1.1 = Z_tfm	B2.1 = Z_ev1
B0.2 = Z_latp2	B1.2 = Z_fra2	B2.2 = Z_swe
B0.3 = Z_lsv2	B1.3 = Z_fra1	B2.3 = Z_md04
B0.4 = Z_hsv	B1.4 = Z_kat1	B2.4 = Z_md03
B0.5 = Z_latv1	B1.5 = Z_hsh	B2.5 = Z_md02
B0.6 = Z_latp1	B1.6 = Z_lash1	B2.6 = Z_md01
B0.7 = Z_lsv1	B1.7 = z_lsh1	B2.7 = Z_md

W150.0 = 0	W151.0 = B_mldyn
W150.1 = B_gae2	W151.1 = B_teslash
W150.2 = B_gae1	W151.2 = B_dlatp2
W150.3 = B_lra2	W151.3 = B_dlatp1
W150.4 = B_lra1	W151.4 = B_tehb
W150.5 = B_lrhk	W151.5 = B_te
W150.6 = B_lrb2	W151.6 = B_sa
W150.7 = B_lrb1	W151.7 = B_l1
W150.8 = 0	W151.8 = 0
W150.9 = 0	W151.9 = 0
W150.10 = b_gefra2	W151.10 = 0
W150.11 = b_gefra1	W151.11 = B_lrsync
W150.12 = B_frao2	W151.12 = B_dktlp
W150.13 = B_frao1	W151.13 = B_dkatasp
W150.14 = B_rkat2	W151.14 = B_dkatsb
W150.15 = B_rkat1	W151.15 = B_dkatst

Projekte V6

B0.0 = Z_hsv2	B1.0 = Z_kat21	B2.0 = Z_swe	B3.0 = 1
B0.1 = Z_latv2	B1.1 = Z_hsh2	B2.1 = Z_md06	B3.1 = 1
B0.2 = Z_latp2	B1.2 = Z_lash2	B2.2 = Z_md05	B3.2 = Z_ev1
B0.3 = Z_lsv2	B1.3 = Z_lsh2	B2.3 = Z_md04	B3.3 = 1
B0.4 = Z_hsv	B1.4 = Z_kat1	B2.4 = Z_md03	B3.4 = 1
B0.5 = Z_latv1	B1.5 = Z_hsh	B2.5 = Z_md02	B3.5 = Z_tfm
B0.6 = Z_latp1	B1.6 = Z_lash1	B2.6 = Z_md01	B3.6 = Z_fra2
B0.7 = Z_lsv1	B1.7 = z_lsh1	B2.7 = Z_md	B3.7 = Z_fra1

W150.0 = B_tehb	W151.0 = 0
W150.1 = B_te	W151.1 = B_mldyn
W150.2 = B_sa	W151.2 = B_gaefra2
W150.3 = B_l1	W151.3 = B_gaefra1
W150.4 = B_lrhkb2	W151.4 = B_teslash2
W150.5 = B_lrhkb1	W151.5 = B_teslash1
W150.6 = B_lrb2	W151.6 = B_dlatp2
W150.7 = B_lrb1	W151.7 = B_dlatp1
W150.8 = B_frao2	W151.8 = 0
W150.9 = B_frao1	W151.9 = B_dktlp
W150.10 = B_rkat2	W151.10 = B_dkatasp2
W150.11 = B_rkat1	W151.11 = B_dkatasp1
W150.12 = B_gae2	W151.12 = B_dkatsb2
W150.13 = B_gae1	W151.13 = B_dkatsb1
W150.14 = B_lra2	W151.14 = B_dkatst2
W150.15 = B_lra1	W151.15 = B_dkatst1

**APP DMS 6.10 Application hint**

Wertebereich von TVDDREC: 0 ... 255 s

## ASCETSDB 1.13 ASCET-SD description of block library

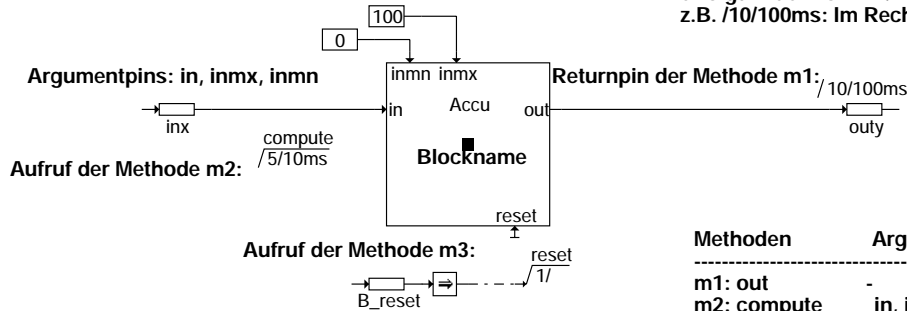
### FDEF ASCETSDB 1.13 Function definition Graphische Darstellung der Grundelemente

Die Grundelemente werden im Diagramm durch rechteckige Bloecke dargestellt. Die Kommunikation der Grundelemente wird durch Verbindungslinien dargestellt.

Die Schnittstellen der Grundelemente sind die Pins am Rand der Bloecke. Jeder Block besitzt einen Returnpin, der das Ergebnis des Blocks ausgibt. Weiterhin gibt es Argumentpins, die Eingaben in den Block bereitstellen, und Methodenpins, die bei Methoden ohne Eingabeargumente und Rueckgabewert verwendet werden.

Die Methoden rufen Funktionen im Block auf.

Die Angabe des Prozesses und der Reihenfolge erfolgt in der Form: "/Reihenfolge/Prozess"  
z.B. /10/100ms: Im Rechenraster 100ms der zehnte Aufruf.



Methoden	Argumente	Rueckgabewert
m1: out	-	Float
m2: compute	in, inmx, inmn	-
m3: reset	-	-

Obiges Beispiel zeigt einen Block mit 3 Methoden:

- Die Methode m1 "out" hat einen Rueckgabewert.

- Die Methode "out" wird durch die Anforderung des Rueckgabewerts vom nachfolgenden Block outy, der im Rechenraster 100 ms in der Reihenfolge an zehnter Position steht, aufgerufen.

- Die Methode m2 "compute" hat drei Argumente (in, inmn, inmx), jedoch keinen Rueckgabewert.

- Die Methode "compute" wird im Rechenraster 10 ms in der Reihenfolge an fnfter Position aufgerufen.

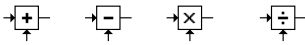
- Die Methode m3 "reset" hat weder Argumente noch Rueckgabewert. Deshalb ist diese durch den "Methodenpin" dargestellt. Die Methode "reset" wird aufgerufen, wenn B\_reset true ist.

ascetsdb-beschreibung

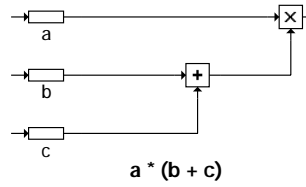
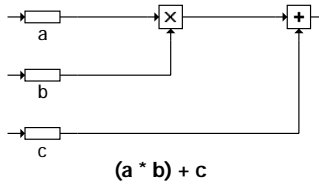
ascetsdb-beschreibung



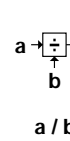
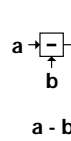
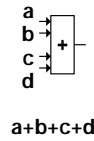
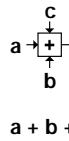
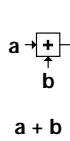
## Arithmetische Operationen



Mit Hilfe der arithmetischen Operationen (Addition, Subtraktion, Multiplikation und Division) koennen Gleichungen beschrieben werden. Gleichungen werden graphisch so dargestellt, da der Rueckgabewert der einen Operation das Argument der nachfolgenden Operation ist.



Nachfolgend werden die Argumente der Primitivoperationen und deren Reihenfolge dargestellt:



$a \rightarrow \text{*-} \rightarrow b$     Negation:  $b = -a$

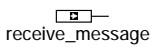
$a \rightarrow \text{|x|} \rightarrow b$     Betrag:  $b = |a|$

$a \rightarrow \text{MAX} \rightarrow c$     Maximum der Eingangswerte:  $c = \text{MAX}(a,b)$

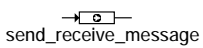
$a \rightarrow \text{MIN} \rightarrow c$     Minimum der Eingangswerte:  $c = \text{MIN}(a,b)$

ascetsdb-a1arithmet

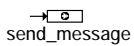
## Variablen



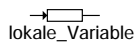
Receive Messages sind Eingangsvariablen der Funktion, die von einer anderen Funktion bereitgestellt werden.



Send/Receive Messages sind Ausgangsvariablen der Funktion, die sowohl innerhalb als auch ausserhalb der Funktion verwendet werden.



Send Messages sind Ausgangsvariablen der Funktion und stehen den uebrigen Funktionen zur Verfuegung.

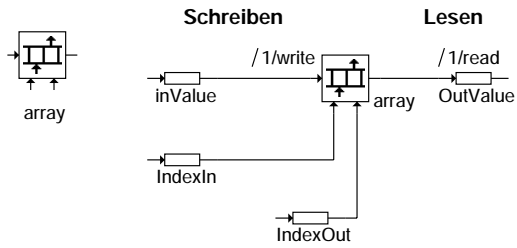


Lokale Variablen werden nur innerhalb der Funktion bereitgestellt und verwendet.

ascetsdb-a2variable

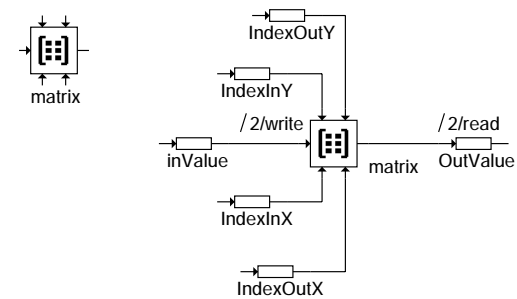
## Arrays und Matrizen

Arrays und Matrizen haben zwei Methoden, um auf die Elemente schreibend und lesend zuzugreifen. Das Schreiben und Lesen kann unabhängig von einander erfolgen



### Array:

- Der zu schreibende Wert wird an den linken Pin, der zugehörige Index an den linken unteren Pin angeschlossen.
- Der zu lesende Wert wird an den rechten Pin, der zugehörige Index an den rechten unteren Pin angeschlossen.



### Matrix:

- Matrizen verhalten sich wie Arrays, jedoch haben hier die Methoden zwei Indexargumente (x,y):
- Um schreibend zuzugreifen, wird der Index x unten links, der Index y oben links angeschlossen.
  - Um lesend zuzugreifen, wird der Index x unten rechts, der Index y oben rechts angeschlossen.

ascetsdb-a3arraysun



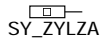
**Konstanten**



**Boolsche Konstanten**

ascetsdb-a4konstant

### Systemkonstanten



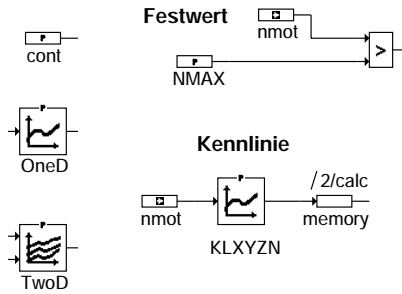
ascetsdb-a5systemko

Systemkonstanten sind Konstanten, die fest im Programm verankert sind. Diese sind nicht applizierbar. Die Systemkonstanten koennen Funktionsteile bedingt ein oder ausschalten.

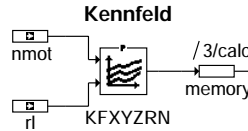
**Beispiel**

SY\_ZYLZA: Zylinderzahl  
SY\_TURBO: Motor mit bzw. ohne Turbolader

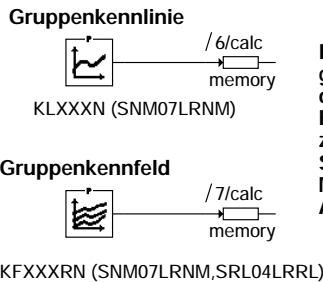
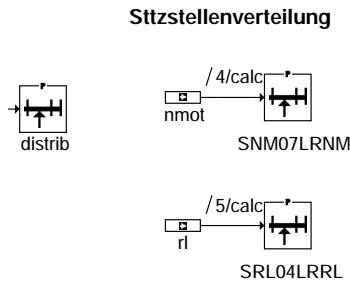
## Festwerte, Kennlinien, Kennfelder, Gruppenkennlinien, Gruppenkennfelder und Stützstellenverteilung



Festwerte sind applizierbare Parameter.



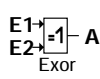
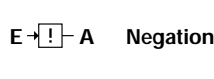
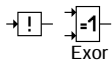
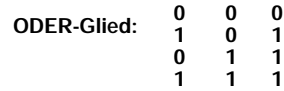
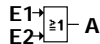
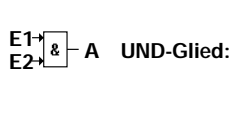
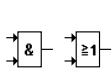
Kennlinien haben ein Argument, Kennfelder haben zwei Argumente als Eingang. Beide haben einen Rueckgabewert.



Bei Gruppenkennlinien und Gruppenkennfelder greifen mehrere Kennlinien bzw. Kennfelder auf die gleiche Stützstellenverteilungen zu. Hierzu wird zuerst aus der abhaengigen Groee, z.B. nmot, die aktuelle Stuetzstelle aus der Stuetzstellenverteilung, z.B. SNM07LRNM, berechnet. Mit dieser aktuellen Stuetzstelle erfolgt die Berechnung de Ausgabewerts der Gruppenkennlinie bzw. -kennfelds.

ascetsdb-a6klkfgklu

### Bitoperationen



ascetsdb-a7bitopera

### Vergleicher

Die Vergleicher liefern am Ausgang TRUE, wenn der Vergleich zutrifft. Ist der Vergleich nicht erfuehlt, liefert der Ausgang FALSE.



Groesser, Groesser gleich

Der Vergleich wird immer von oben nach unten gelesen:

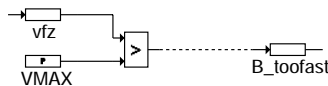


Kleiner, Kleiner gleich

Wenn vfz groesser als VMAX, ist die Bedingung B\_toofast TRUE



Gleich, Ungleich

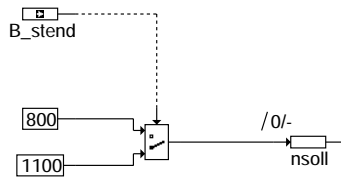


ascetsdb-a8vergleic

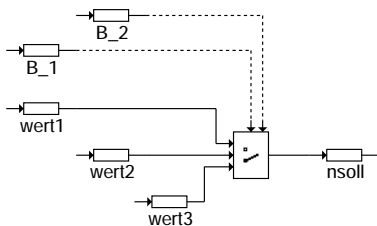


## Multiplex Operator "Muxer", "Schalter"

Ein Muxer schaltet abhaengig von Eingangsbedingungen einen Wert zum Ausgang durch. Das Icon des Muxers ist in Ruhestellung dargestellt, d.h. wenn die Eingangsbedingungen false sind.



**Beispiel "Einfach-Muxer":**  
- wenn B\_stend = false: nsoll = 1100  
- wenn B\_stend = true: nsoll = 800

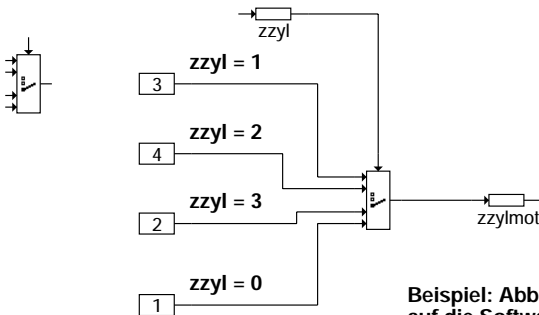


Bei kaskadierten Muxern ist jedem Wert eine Eingangsbedingung zugeordnet. Der oberste Wert, dessen Eingangsbedingung true ist, wird durchgeschaltet. Ist keine Eingangsbedingung true wird der unterste Wert durchgeschaltet.

**Beispiel "Mehrfach-Muxer":**  
- wenn B\_1 = true: nsoll = wert1  
- wenn B\_1 = false & B\_2 = true: nsoll = wert2  
- wenn B\_1 = false & B\_2 = false: nsoll = wert3

ascetsdb-a9multiple

## CASE Operator



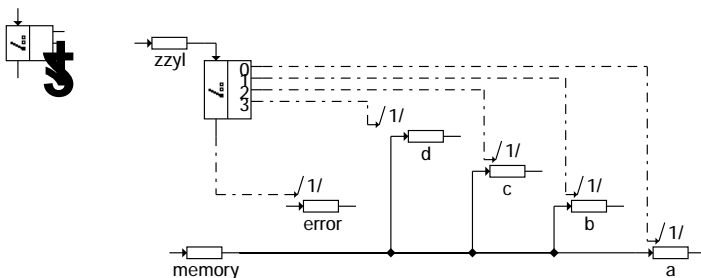
Der CASE Operator schaltet abhaengig von einem oben anliegenden diskreten Steuerwert (1,2,3,..) einen der brigen linken Eingaenge auf den Ausgang durch. Ist der Steuerwert 1 wird der erste, ist er 2 wird der zweite Wert und sofort durchgeschaltet. Ist der Wert auerhalb des Bereiches, wird der unterste Eingang (default) durchgeschaltet.

**Beispiel: Abbildung der physikalischen Zylindernummer auf die Software-Zylindernummer**

ascetsdb-a10caseope

## Switch

Der SWITCH Operator aktiviert abhaengig von einem oben anliegenden diskreten Steuerwert (1,2,3,..) die passenden Kontrollfluesse ueber die rechten Ausgaenge. Existiert kein passender Ausgang, wird der Kontrollflu am untere Ausgang aktiviert.



**Beispiel:**

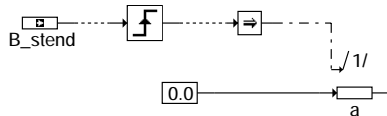
Abhaengig von zzyl wird eine der folgenden Operationen ausgefuehrt:  
- wenn zzyl = 0: a = memory  
- wenn zzyl = 1: b = memory  
- wenn zzyl = 2: c = memory  
- wenn zzyl = 3: d = memory  
- sonst: error = memory

ascetsdb-a11kontrol

### If ..... then



Die If .. Then Operation wertet eine logische Bedingung aus und aktiviert bei TRUE alle Rechenfolgen, die an den Kontrollflu angeschlossn sind. Die Recheneihenfolge ist durch die Numerierung festgelegt.



Beispiel: Wenn B\_stend nach true wechselt, wird tnst = 0 gesetzt.

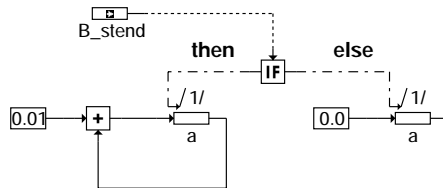
### If .. Then .. Else

If



else

Die If .. Then .. Else Operation wertet eine logische Bedingung aus und aktiviert bei TRUE alle Rechenfolgen des then-Kontrollzweigs und bei FALSE alle Rechenfolgen des else-Kontrollzweigs. Die Recheneihenfolge am jeweiligen Kontrollzweig ist durch die Numerierung festgelegt.



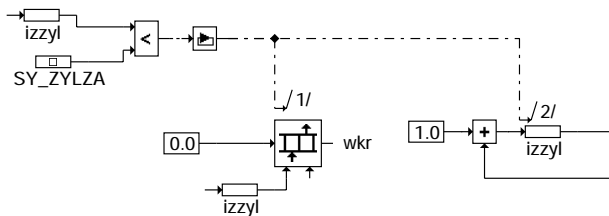
Beispiel: Wenn B\_stend = true, wird tnst im 10 ms Raster um 0.01 sec erhoeht. Sonst (B\_stend = false) wird tnst = 0 gesetzt.

ascetsdb-a12kontrol

### While-Schleife



Die Rechenfolge innerhalb des Kontrollfusses der Schleife wird solange ausgefuehrt, wie die Eingangsbedingung erflit ist, also TRUE ist. Die Schleife wird abgebrochen, wenn die Eingangsbedingung FALSE ist. Der Wert fr das Beenden der While-Schleife wird normalerweise innerhalb der Schleife gebildet. Meistens handelt es sich hierbei um einen Zaehler, der bis zu einem bestimmten Wert zaehlen soll.



Beispiel: Das Array wkr[i] wird solange mit 0 beschrieben, wie izzyl < SY\_ZYLZA ist. Mit der Zaehlvariablen izzyl am Indexeingang des Arrays wird jedes Element des Arrays mit 0 initialisiert wird.

ascetsdb-a13while

### Break

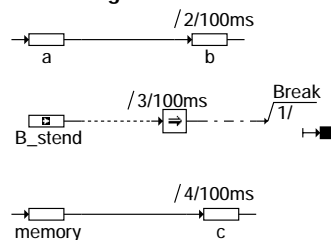
Break

/0/-



Die Break Operation bricht einen Prozess, z.B. den Funktionsanteil in einem Rechenraster, vorzeitig ab. Alle nachfolgenden Berechnungen der Funktion im Prozess mit hoeherer Nummer bei der Reihenfolge werden nicht ausgefuehrt.

Beispiel:

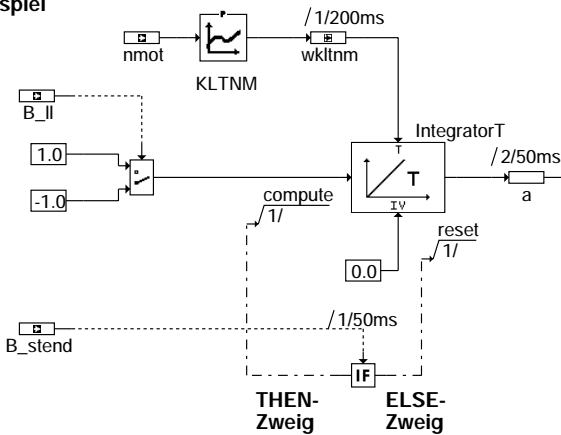


Entsprechend der Reihenfolge wird nach der Operation b = a genau dann ein Break ausgeloeht, wenn B\_stend = TRUE ist. Tritt ein Break ein, wird der Prozess 100ms angebrochen. Die nachfolgende Operation c = memory wird nicht mehr ausgefuehrt.

ascetsdb-a14kontrol



### Beispiel



Solange die Bedingung  $B\_stend = FALSE$  ist, wird im Rechenraster 50ms die Methode "reset" des Integrators ausgeführt. Diese Methode bewirkt, da die interne Speicherzelle des Integrators mit dem IV-Wert, also 0.0, initialisiert wird. Wird jetzt die Bedingung  $B\_stend = TRUE$ , wird der linke Kontrollflu aktiviert und die Methode "compute" des Integrators zur Ausführung gebracht. Die Methode "compute" hat als Argumente die Zeit T und den Eingangswert. Dieser ist von B\_II abhängig. Mit  $B\_II = TRUE$  ist der Eingangswert = 1.0, mit  $B\_II = FALSE$  ist der Eingangswert = -1.0. Die Zahlen vor dem Rechenraster geben die Reihenfolge an: Im Rechenraster 200ms wird die Zeitkonstante T berechnet und in der Send/Receive Message wkltnm gespeichert. Im Rechenraster 20ms wird zuerst die IF .. THEN .. ELSE Abfrage durchgeführt. Im zweiten Schritt wird der Integrationswert in die Variable a geschrieben.

ascetsdb-bbeispiele

### ABK ASCETSDB 1.13 Abbreviations

### FW ASCETSDB 1.13 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB ASCETSDB 1.13 Detailed description of function

### APP ASCETSDB 1.13 Application hint

### SYABK 8.3 Symbols and abbreviations

### FDEF SYABK 8.3 Function definition

SYMBOLS:

<pre> -----+-----&gt;               +-----&gt;       branching of signal lines           </pre>	<pre> -----+ ----- -----&gt;               +-----&gt;       crossing of signal lines           </pre>	<pre> +-----+   +---+10 ms  --&gt;  ---+ +---+ +---+ +-----+ mono-flop 10 ms           </pre>
<pre> F1 -&gt;o--- addition point F1 + F2 + ^ F2   +++ ----&gt; V ----&gt; OR member ----&gt;    +++ "/" is also used)           </pre>	<pre> F1 -&gt;o subtraction point F1 - F2 - ^ F2   +++ --&gt;o   ----&gt; tendency at input +++ (in descriptions "! " is also used)           </pre>	<pre> +++ ----&gt; &amp; ----&gt; AND member ----&gt;    +++ +++ ----&gt; o----&gt; tendency at output +++           </pre>
<pre> B_lr switches; are designated in / in dormant position --o o-- Text describes switchover condition           </pre>	<pre> dummy connectors (replaces output of  "  0 -* * * ---- in factor frames acc. +++ to given section)           </pre>	<pre> +++ a ---&gt; : ----&gt; a / b division of two b ---&gt;    Variables (b can also +++ come from below)           </pre>
<pre> +-----+ dead time member xe   Tt+----  xa ----&gt;     ----&gt; xa delayed by Tt  ---+   +-----+           </pre>	<pre> +-----+ B_s ---&gt; S  flip  ----&gt; R/S flip +++ flop B_lr ---&gt; R  flop   +++           </pre>	<pre> +-----+ two-point member xe   +--- 1   xa ----&gt; ----- ----&gt; xe continuously   -1-+   xa either -1 or 1 +-----+           </pre>
<pre> +-----+ switch-on B_lr  TBLRH +---   B_lrhk restrainer --&gt; -----+t  ----&gt; +-----+ if B_lr for t= TBLRH uninterrupted after which B_lrhk=1 " / B_lr=0 =&gt; B_lrhk=0           </pre>	<pre> +-----+ complex function see   %ZWB   page %ZWB +-----+           </pre>	<pre> e +-----+ a quantity formation --&gt;   x   ----&gt; +-----+ a =  e            </pre>

ascetsdb-bbeispiele



<pre> +-----+  WMAX +---  upper limiting to WMAX   /   and lower limiting to  ---+ WMIN  WMIN +-----+ </pre>	<pre> +-----+   +-----  upper limiting to --&gt;  / TLMX  ---&gt; TLMX +-----+ </pre>	<pre> +-----+   TLMIN //   lower limiting to --&gt;  ----- ---&gt; TLMIN +-----+ </pre>
<pre> +-----+   MIN   smallest value selection +-----+ </pre>	<pre> +-----+   MAX   largest value selection +-----+ </pre>	<pre> +---&lt;---+ LR on -&gt; DTMR  &lt;- hysteresis, LR V ^ switch on if off     Tmot &gt; TMRE -----&gt;+ shut-down if TMRE   Tmot &lt; TMRE - DTMR </pre>
<pre> +-----+ B_lr comparator Tmot -&gt; &gt;TMLR -----&gt; if Tmot &gt; TMLR +-----+ then B_lr = 1 </pre>	<pre> +-----+ integrator e   ^ /   a --&gt;    / ZLRHK  ---&gt; with time +-----+&gt;t  constants ZLRHK </pre>	<pre> +-----+ low pass e   ^ . *  em -&gt;    * ZKFRM  ---&gt; with time constants   *-----&gt;t  ZKFRM +-----+ </pre>

Symbolic abbreviations used in plausibility checks:

```

-----
SB1, SB2... Specification conditions 1 and 2
F1, F2.... Error 1 and 2
SB1 & SB2 Condition 1 and condition 2 fulfilled
-----
SB1 \ SB2 Condition 1 or condition 2 fulfilled
-----
!SB1 Condition 1 not fulfilled
-----
F1: SB1 Error 1 set if condition 1 is fulfilled
F2: SB1 & !SB2 Error 2 set if condition 1 is fulfilled and condition 2 is not fulfilled

```

## SWADAP 1.2 Software adapter ME2.3 -> ME7

### FDEF SWADAP 1.2 Function definition

Umsetzung Flags:

=====

```

ME2.3 ME7.x

EMS_KLIMA B_ko
B_AC & !EMS_KLIMA B_acres
B_AC B_ac
B_br B_bremse
B_kup B_kuppl
B_dknot_fr B_dknolu
B_ska B_dkpu
B_start B_st
B_ursta B_pwf
E_hfm oder E_lm E_lm
B_fs B_fs
B_dllr = 0
B_pn = 0
B_mdmin = 0
B_mdmax = 0

```

Umsetzung RAM-Daten:

=====

Korrekturfaktor Druck vor Drosselklappe

```

ME2.3: fdkha 1 Byte, [0...<2], 1Inc = 2/256
ME7.x: fpvdk_w 2 Byte, [0...<4], 1Inc = 4/65536

```

gefilterter Drehzahlgradient

```

ME2.3: ngrad2cpl 1 Byte, [-10240... 10160 Upm/s], 1Inc = 80 Upm/s
ME7.x: ngfil 1 Byte, [-12800... 12700 Upm/s], 1Inc = 100 Upm/s
ME7.x: ngfil_w 2 Byte, [-12800...<12800 Upm/s], 1Inc = 100/256 Upm/s

```

Motordrehzahl

```

ME2.3: nist_lu 2 Byte, [0...65535 Upm], 1Inc = 1 Upm
ME7.x: nmot 1 Byte, [0...10200 Upm], 1Inc = 40 Upm
ME7.x: nmot_w 2 Byte, [0...16383.75 Upm], 1Inc = 0.25 Upm

```

relative Last

```

ME2.3: FAKTOR * tl_ 2 Byte, 14.18%/ms * [0...174.76ms], 1Inc = 2.666us
ME7.x: rl 1 Byte, [0...191.25%], 1Inc = 0.75%
ME7.x: rl_w 2 Byte, [0...1535.98 %], 1Inc = 0.75%/32

```

Luftmassenstrom, 8Bit

```

ME2.3: mlsm 1 Byte, [0...1020 kg/h], 1Inc = 4 kg/h
ME7.x: ml 1 Byte, [0...1020 kg/h], 1Inc = 4 kg/h

```



Luftmassenstrom, 16Bit

ME2.3: mlsmw 2 Byte, [0...6553.5 kg/h], 1Inc = 0.1 kg/h  
ME7.x: ml\_w 2 Byte, [0...6553.5 kg/h], 1Inc = 0.1 kg/h

Motortemperatur

ME2.3: tmotlin 1 Byte, [-40...216°C], 1Inc = 1K  
ME7.x: tmot 1 Byte, [-48...143.25 °C], 1Inc = 0.75K

Ansauglufttemperatur

ME2.3: tanslin 1 Byte, [-40...216°C], 1Inc = 1K  
ME7.x: tans 1 Byte, [-48...143.25 °C], 1Inc = 0.75K

Winkel Fahrpedal

ME2.3: sw\_ped 2 Byte, [0...<100%], 1Inc = 100%/32768  
ME7.x: wped\_w 2 Byte, [0...<102.4%], 1Inc = 0.4%/256

Batteriespannung

ME2.3: ubatt 1 Byte [0...17V], 1Inc = 0.067V  
ME7.x: ub 1 Byte [0...17V], 1Inc = 0.067V

Lambdasondenspannung vor Kat

ME2.3: Usvk1\_w [0...5V], 1Inc = 5V/1024  
Usvk2\_w [0...5V], 1Inc = 5V/1024  
ME7.x: usvk\_w [0...5V], 1Inc = 5V/1024  
usvk2\_w [0...5V], 1Inc = 5V/1024

Lambdasondenspannung hinter Kat

ME2.3: Ushk1\_w [0...5V], 1Inc = 5V/1024  
Ushk2\_w [0...5V], 1Inc = 5V/1024  
ME7.x: ushk\_w [0...5V], 1Inc = 5V/1024  
ushk2\_w [0...5V], 1Inc = 5V/1024

Mit der ME7.x neu eingeführte RAM-Größen:

=====

AGR-Rate

agrr = 0 1 Byte, [0..99.6%], 1Inc = 0.39%

Delta-Drehmoment von Antiruckel-Funktion

dmar\_w = 0% 2 Byte, [-100...<100%], 1Inc = 2/65536

Momentenreserve für Katheizen

dmrkh\_w = 0% 2 Byte, [0...<100%], 1Inc = 1/65536

Lastsignaländerung

drl\_w = rl\_w[z] - rl\_w[z-1] 2 Byte, [-768...768%/seg], 1Inc = 0.75% / 32

Korrekturfaktor Temperatur vor Drosselklappe

ftvdk = 1 1 Byte, [0... <2], 1Inc = 2/256

Gangstufe

gangi = 2 1 Byte, [0...255], 1Inc = 255

Basis-Lambda für Momentenschnittstelle, 8Bit

lambas = 1 1 Byte, [0... <2], 1Inc = 2/256

Basis-Lambda für Momentenschnittstelle, 16Bit

lambas\_w = 1 2 Byte, [0...<16], 1Inc = 16/65536

Ladebilanz der Batterie

lbz = 0 1 Byte, [0..99.6%], 1Inc = 0.39%

Wandler-Verlustdrehmoment

mdwan\_w = 0% 2 Byte, [0...<100%], 1Inc = 1/65536

Drehmoment, Tankentlüftung, begrenzt

mitebg\_w = 0% 2 Byte, [0...<100%], 1Inc = 1/65536

Drehmoment für Geschwindigkeitsbegrenzung

mivmx\_w = 99.992% 2 Byte, [0...<100%], 1Inc = 1/65536

langsamer Anteil des ASR-Eingriffs

miasrl\_w = 100% 2 Byte, [0...<100%], 1Inc = 100% / 65536

ASR-Drehmomentanforderung

miasrs\_w = 100% 2 Byte, [0...<100%], 1Inc = 100% / 65536

indiziertes Soll-Motormoment für Getriebeschutz

miges\_w = 100% 2 Byte, [0...<100%], 1Inc = 100% / 65536

indiziertes Soll-Motormoment Getriebeschutz für schnellen Eingriff

migs\_w = 100% 2 Byte, [0...<100%], 1Inc = 100% / 65536

MSR-Drehmomentanforderung







Variable	Source	Type	Description
USHK2_W	SWADAP	AUS	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst 2
USHK_W	SWADAP	AUS	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst
USVK2_W	SWADAP	AUS	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVK_W	SWADAP	AUS	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst
VFZG	SWADAP	AUS	vehicle speed (km/h)
WPED_W	SWADAP	AUS	normed angle acceleration pedal

### FW SWADAP 1.2 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB SWADAP 1.2 Detailed description of function

Diese Funktion setzt für die ersten Programmstände der ME7, die in der ME2.3 - Umgebung laufen, die erforderlichen ME2.3 - Größen in die neuen Hauptsignale für die ME7 um.

### APP SWADAP 1.2 Application hint

## STECK 420.11 Plug pin arrangement

### DFE STECK 420.11 Function definition

Steckerbelegung ME3.1 auf Basis Anschlussplan Y 261 C21 878 / 1 (09/610.X)

Motor-Stecker

=====

PCB-Pin-No	Hybrid Pin-No	Signal 09/610	Function
F01/1	M01	A.T.DCM	C-Motor Throttle Valve Minus
A03	M02	A.S.LSHVK2	Oxygen Sensor Heating 2 in Front Of Catalyst
E13	M03	A.P.EV3	Fuel Injector Driver 3, Cyl. 4
E12	M04	A.S.SU1	Driver Output Variable Intake Manifold 1
C21	M05	A.T.TEV	Driver Output Canister Purge Valve
E43	M06	M.R.KS2	Reference Ground Knock Sensor B
D10	M07	M.R.LS2VK	Reference Ground Oxygen Sensor 2 In Front Of Catalyst
E21	M08	---	---
E46	M09	---	---
E38	M10	E.F.DGA	Engine Speed Sensor, Connector A
C35	M11	---	---
C23	M12	---	---
E08	M13	---	---
F17	M14	A.P.ZUE3I	Ignition Coil Driver 4, Cyl 1, 4 Lateral Spark
F06	M15	---	---
F20	M16	A.P.ZUE1I	Ignition Coil Driver 1, Cyl 1, 4 Central Spark
F02/1	M17	A.T.DCP	DC-Motor Throttle Valve Plus
B01	M18	---	---
E25	M19	A.P.EV1	Fuel Injector Driver 1, Cyl. 1
E01	M20	---	---
E05	M21	---	---
E42	M22	E.A.KS1	Knock Sensor 1
D08	M23	E.A.LS1VK	Oxygen Sensor 1 In Front Of Catalyst
E31	M24	E.A.IP1S	Throttle Valve Position Potentiometer 1
E29	M25	E.A.TMOT	Engine Temperature
E28	M26	M.R.SEN *	Reference Ground HFM,TANS,TMOT, IP, SP
D13	M27	---	---
C32	M28	E.A.LS1HK	Oxygen Sensor 1 in Behind Catalyst
C37	M29	---	---
F05	M30	A.P.ZUE4I	Ignition Coil Driver 3 / Cyl 2, 3 Lateral Sark
F19	M31	A.P.ZUE2I	Ignition Coil Driver 2 / Cyl 2, 3 Central Spark
F13	M32	---	---
F01/2	M33	A.T.DCM	DC-Motor Throttle Valve "Minus"
A01	M34	A.S.LSHVK1	Oygen Sensor Heating 1 In Front Of Catalyst
E26	M35	A.P.EV2	Fuel Injector Driver 2 / Cyl 3
E02	M36	A.S.NWS	Variable Camshaft Phasing On/Off
E05	M37	---	---
E44	M38	---	---
D09	M39	E.A.LS2VK	Oxygen Sensor 2 In Front Of Catalyst



E34	M40	E.A.IP2S	Throttle Valve Position Potentiometer 2
E18	M41	---	---
E40	M42	E.S./F.ZYHA	CAM Sensor (Hall)
C34	M43	---	---
C33	M44	---	---
E04	M45	---	---
	M46	---	---
	M47	---	---
	M48	---	---
F02/2	M49	A.T.DCP	DC-Motor Throttle Valve "Plus"
A05	M50	A.S.LSHHK1	Oxygen Sensor Heating 1 Behind Catalyst
E33	M51	U.U.5V1 *	Stabilized Sensor Supply Voltage 1
E14	M52	A.P.EV4	Fuel Injector Driver 4 / Cyl 2
E03	M53	---	---
E41	M54	M.R.KS1	Reference Ground Knock Sensor 1
D07	M55	M.R.LS1VK	Reference Ground Oxygen Sensor 1 In Front Of Catalyst
E47	M56	---	---
E45	M57	---	---
C22	M58	A.U.5V23*	Stabilized Sensor Supply Voltage 2 (Accelerator Pedal / Throttle Sensor)
E37	M59	E.F.DGB	Engine Speed Sensor, Connector B
C31	M60	M.R.LS1HK	Reference Ground Oxygen Sensor 1 Behind Catalyst
C36	M61	---	---
	M62	---	---
	M63	---	---
	M64	---	---

Fahrzeugstecker  
=====

E06	F01	---	---
D02	F02	---	---
A06	F03	B.D.IMMO	Immobilizer Interface
E27	F04	---	---
E22	F05	---	---
E18	F06	E.S.KO	AC Compressor Request
D20	F07	U.U.5V22	Stabilized Sensor Supply Voltage (Accelerator Pedal)
C24	F08	E.A.SP1S	Accelerator Pedal Position Input 1
C40	F09	E.S.ML1	Quadrinary (Input Switch FAN 1) Low Level
D24	F10	E.S.AUS	Cruise Control on/off
D23	F11	---	---
D12/1	F12	B.D.CANL	CAN-Interface "Low"
D03	F13	A.S.KOS	Driver Output AC Control
	F14	---	---
B04	F15	U.U.UBD	Continuous Supply Voltage
B03/3	F16	U.U.UBR	Switched Battery Voltage, Main Relay
	F17	---	---
E11	F18	---	---
C30	F19	A.S.TMOT	Motor Temperature Warning Lamp
E23	F20	U.U.UPROG	FLASH Programming Enable
E32	F21	---	---
D06	F22	E.A./S.FST	Fuel Level Information
	F23	---	---
C26	F24	M.R.SP1	Reference Ground 1 Accelerator Pedal
A04	F25	M.R.SP2/SEN1 *	Ref. Ground 2 Accelerator Pedal , Reference Ground HFM,TANS,TMOT,IP
D21	F26	E.S.BR	Brake Light Switch
D14	F27	E.S.BL	Brake Light
D15	F28	E.S.FP	Program Switch / Program Switch Control Light
D11/1	F29	B.D.CANH	CAN-Interface "High"
C29	F30	A.S./T.EKP	Fuel Pump Relay / Switchmode Fuel Pump Driver
B02	F31	A.S.HR	Driver Output Main Relay
B03/2	F32	U.U.UBR	Switched Battery Voltage, Main Relay
E15	F33	---	---
C28	F34	---	---
C38	F35	A.P.DMTN	Engine Speed Signal (TN Signal)
	F36	---	---
D05	F37	---	---
E17	F38	---	---
	F39	---	---
C25	F40	E.A.SP2S	Accelerator Pedal Position Input 2
C27	F41	E.S.ML2	Quadrinary (Input Switch FAN 2) Hight Level
D22	F42	E.S.WA	Cruise Control Resume
D20	F43	E.S.SB	Cruise Control Set Acceleration
D13	F44	E.F.VFZ	Vehicle Speed Sensor
D11/2	F45	B.D.CANH	CAN-Interface "High"
D01	F46	A.S.FELA	Malfunction Indicator Light



A02	F47	E.S.KL15	Ignition Switch
B03/1	F48	U.U.UBR	Switched Battery Voltage, Main Relay
	F49	---	---
E07	F50	A.S.FAN1	Driver Output FAN Contr. 1
	F51	---	---
D04	F52	A.S.FGR	Control Light Cruise Control
C39	F53	B.D.DIAK	Diagnostic K-Line
E45	F54	E.A.TANS	Intake Air Temperature
	F55	---	---
E20	F56	A.U.5V21	Stabilized Sensor Supply 1 (PWG + DVE)
E47	F57	E.A.HFM	Hot Film Air Mass Meter
D17	F58	E.S.SV	Cruise Control Set Deceleration
D16	F59	E.S.KUP	Input Switch Clutch Control
D19	F60	E.S.PMOEL	Oil Pressure Switch
D12/2	F61	B.D.CANL	CAN-Interface "LOW"
E10	F62	A.S./T.FAN2	Driver Output Fan Control 2
E33	F63	A.U.5V1	Stabilized Sensor Supply Voltage 1
	F64	---	---

Legende:

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1.Pinart

- A Ausgang
- E Eingang
- EA Ein- und Ausgang
- U Spannungsversorgung
- M Masse
- M/A Alternativbelegung, hier Masse- bzw. Ausgang

2.Signalart

- A. Analoge Spannung
- F. Frequenzsignal
- M. Masse
- P. Pulsdauersignal
- R. Referenzmasse
- S. Schaltsignal
- C. Schirmung
- D. Serielle Datenleitung
- U. Spannungsversorgung für/von SG
- T. Tastverhältnis, Pulsweitenmodulation

ECU MOTRONIC ME3.1 u-HYBRID

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			49
	17	33	50
1	18	34	51
2	19	35	52
3	20	36	53
4	21	37	54
5	22	38	55
6	23	39	56
7	24	40	57
8	25	41	58
9	26	42	59
10	27	43	60
11	28	44	61
12	29	45	62
13	30	46	63
14	31	47	64
15	32	48	
16			

Engine Connector

			16
64	48	32	15
	47	31	
63	46	30	14
	45	29	
62	44	28	13
	43	27	
61	42	26	12
	41	25	
60	40	24	11
	39	23	
59	38	22	10
	37	21	
58	36	20	9
	35	19	
57	34	18	8
	33	17	
56			7
55			6
54			5
53			4
52			3
51			2
50			1

Vehicle Connector

ECU MOTRONIC ME3.1 PC BOARD

	21	14	7	
	20	13	6	
	19	12	5	
	18	11	4	
	17	10	3	
	16	9	2	++
	15	8	1	F
	48	36	24	12
	47	35	23	11
	46	34	22	10
	45	33	21	9
	44	32	20	8
	43	31	19	7
	42	30	18	6
	41	29	17	5
	40	28	16	4
	39	27	15	3
	38	26	14	2
	37	25	13	1
				E
	24	18	12	6
	23	17	11	5
	22	16	10	4
	21	15	9	3
	20	14	8	2
	19	13	7	1
				D
	40	30	20	10
	39	29	19	9
	38	28	18	8
	37	27	17	7
	36	26	16	6
	35	25	15	5
	34	24	14	4
	33	23	13	3
	32	22	12	2
	31	21	11	1
				C
	4	8	4	
	3	7	3	
	2	6	2	++
	1	5	1	A



## ABK STECK 420.11 Abbreviations

## FW STECK 420.11 Fixed Values

Parameter	Value	Description
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## FB STECK 420.11 Detailed description of function

## APP STECK 420.11 Application hint

## PROKON 53.11 Project configurations

### DDEF PROKON 53.11 Function definition

1. Software-Konfiguration über nicht applizierbare Systemkonstanten

1a. Kundenspezifische Systemkonstanten (FERRARI)

Label	Wert	Beschreibung
SY_AIRBAG	1	1 = Airbagsignal bzw. Crash-Schalter vorhanden
SY_ELKUP	1	1 = mit elektronischer Kupplung (= SY_ME73)
SY_HYBRID	1	1 = Hybrid-SG (0 = Leiterplatten-SG)
SY_SERIE	0	0 = Applikationseprom (1 = Serieneprom)
SY_SGALAD	0	0 = keine Lastabfalldiagnose
SY_ZYKL...	0	= SY_ZYKL_ROM_CHECK_INAKTIV; 0 = aktiv (Serie)
SY_2HFM	1	1 = Berücksichtigung des 2.HFM aufgrund der Saugrohrgeometrie

1b. Motorspezifikation

Label	Wert	Beschreibung
SY_EGFE	1	Eingangsgröße Füllungserfassung (siehe App.hinweise)
SY_GAP	2	Anzahl fehlender Zähne in Lücke
SY_GRDWRT	114	Grundwert, Abstand Software-Bezugsmarke (2. neg. Flanke nach Lücke) zu OT 120 [° KW] - 6° KW
SY_GRUNDWERT	114	(= SY_GRDWRT)
SY_G_INKR	75	Inkrement pro Zahn (= (SY_G_ZAHN*100)/SY_N_INKR)
SY_G_ZAHN	6	°KW pro Zahn (=720/SY_NWZAEHNE)
SY_INGASOS	6	(= SY_OVERSIZE+SY_ZYLZA)
SY_NWZAEHNE	120	Anzahl Zähne pro NWU (ohne Lücke) (= 2*SY_TEETH)
SY_N_INKR	8	Anzahl Inkremente pro Zahn
SY_OVERSIZE	2	siehe %BGNG
SY_PH2OFST	0	Offset für 2. Phasengeber
SY_TEETH	60	Anzahl Zähne pro KWU (ohne Lücke)
SY_TNZAEHNE	30	Anzahl Zähne je TN (= SY_NWZAEHNE/SY_ZYLZA)
SY_TNZAEH...	28	Anzahl Zähne je TN-Lücke (= SY_TNZAEHNE-SY_GAP)
SY_ZWOFFSET	152	Inkremente zwischen TR und OT (= SY_Z_OT*SY_N_INKR)
SY_ZYLZA	4	Zylinderanzahl (pro SG)
SY_Z_OT	19	Zähne zwischen TR und OT (= SY_GRUNDWERT/SY_G_ZAHN)



1c. Motorfunktionen (HW-Komponenten)

Label	Wert	Beschreibung
SY_AGR	0	0 = AGR nicht vorhanden
SY_CAN	0	0 = kein full CAN
SY_CONFSL	1	1 = Sekundärluftpumpe vorhanden
SY_DOPZW	1	1 = doppelte Zündausgabe bei Phasengebernotlauf
SY_EGAS	1	1 = EGAS vorhanden
SY_FGR	1	1 = mit FGR (nur in der Software wegen Überwachung!)
SY_GGTS	0	0 = ohne Auswertung Gebergröße genaues Temperatursignal
SY_KOPWM	0	0 = kein PWM-Signal vom Klimakompressor
SY_LECK	0	0 = kein DVE mit hoher Leckluft
SY_LENKH...	0	= SY_LENKHILFE_PORT; 0 = kein Schalter Lenkhilfe verbaut
SY_MAX-EV	4	Anzahl Ausgangspins für EVs
SY_NLDG	0	0 = kein DG-Notlauf
SY_NWS	1	Nockenwellensteuerung: 1 = 2-Pkt.verstellung (siehe App.hinweise)
SY_NZUEB	800	Umschaltung des Zündbereiches (Schließzeit/Winkelausgabe) [U/min]
SY_PBRPW	0	0 = keine Plausibilitätsprüfung Bremse/PWG
SY_PGRAD	1	Typ des Nockenwellengeberrades: 1 = ein Impuls pro 720°KW (siehe App.hinweise)
SY_PGRAD2	0	Typ des 2. Nockenwellengeberrades: 0 = kein Geberrad vorhanden (siehe App.hinweise)
SY_PHTWIN	0	0 = kein zweiter Phasensensor vorhanden (= SY_PGRAD2)
SY_SU	2	Saugrohrumschaltung: 2 = zwei Schaltausgänge (siehe App.hinweise)
SY_TFA	0	0 = TANS-Sensor (siehe App.hinweise)
SY_TFMA	1	1 = TANS-Sensor vorhanden (Initial. GGTFM-Ersatzwert)
SY_TFMAP	0	0 = TANS-Sensor-Beschaltung ohne Parallel-Widerstand
SY_TFMO	0	0 = TOEL-Sensor nicht vorhanden (Initial. GGTFM-Ersatzwert)
SY_TFUMG	0	0 = kein Umgebungstemperaturfühler vorhanden
SY_TURBO	0	0 = ohne Turbolader (LDR)
SY_UBR	0	0 = keine Spannung ubr hinter Hauptrelais
SY_WNBM	6	Winkel Zahnabstand Kurbelwellensignal (= 360/SY_TEETH)

1d. Systemkonstanten für Diagnose

Label	Wert	Beschreibung
SY_AAV	1	1 = mit AAV (in %TEBEB)
SY_CDCCSIZE	8	Anzahl CARB-Fehler-Code pro Fehler (= 4*SY_SGANZ)
SY_CDKSIZE	2	Anzahl Kunden-Fehler-Code pro Fehler (= SY_SGANZ)
SY_CDTSIZE	2	Anzahl CDT-Code pro Fehler (= SY_SGANZ)
SY_CLASIZE	2	Anzahl Fehlerklassen pro Fehler (= SY_SGANZ)
SY_DELFCS	0	0 = Lösche alle FCM
SY_DFPMEV	2	Anzahl Umweltbedingungen, die im freeze frame gespeichert sind
SY_DFPMVAR	3	DFPM Version
SY_DFPMTIM	2	Größe der Zeit (Betrieb oder Real) in Bytes
SY_DLDP	0	0 = ohne DFP-LDPE
SY_DLS	0	0 = kein DLS-Eingriff in AZUE
SY_DLSUV	0	0 = ...
SY_DTANKL	0	0 = keine Diagnose leerer Tank vorhanden
SY_DVEADA	1	1 = BGDVE: Sperren von Einspritzung durch DV-E-Adaption erlaubt
SY_ENVBLOK	2	DFPM: Anzahl Blöcke mit Umweltbedingungen
SY_FCMSIZE	20	Anzahl der FCM Zeilen
SY_FFCSIZE	11	Größe des CARB freeze frame
SY_FFESIZE	0	Größe des erweiterten freeze frame
SY_FFTSIZE	2	Anzahl Umweltbedingungen pro Fehler, die im freeze frame gespeichert sind (= SY_DFPMEV)
SY_INI_OBD	0	0 = System unterstützt ISO 14230-4 mit schneller Ini und ISO 9141 mit 5 Baud Initialisierung
SY_ISOPROT	0	0 = ISO 9141
SY_TSFSIZE	1	Anzahl Fehlerschwere pro Fehler

1e. Zylinderabhängige Systemkonstanten

Label	Wert	Beschreibung
SY_KOEVA	0	0 = keine Koordination der EV-Abschaltung über KOEVAB
SY_REDMX	4	maximale Reduzierstufe (= SY_ZYLZA)
SY_TN	1	Drehzahlmesser-Signal: 0=kein tn-Sign., 1=Syncroausgabe, 2=toggeln
SY_ZAS	0	0 = Zylinderabschaltung (ZAS) nicht vorhanden
SY_ZKANZAHL	4	Zündkreisanzahl (= SY_ZYLZA/SY_ZNDAUS)
SY_ZNDAUS	1	Zündausgabe (1 = Einzelfunken oder 2 = Doppelfunken) (siehe App.hinweise)
SY_ZZBANK	0	Zylinderzuordnung Bank1 und Bank2 (siehe App.hinweise)
SY_ZZBANKB	0	Zylinderzuordnung Bank1 und Bank2 (siehe App.hinweise)



1f. Systemkonstanten der Klopfregelung

Label	Wert	Beschreibung
SY_INJTIM...	64	=SY_INJTIM_PRE; Vorteiler des Timers, an dem die KR hängt (= SY_TIMER8_PRESCALER)
SY_KRMFTI...	64	=SY_KRMFTIM_PRE; Vorteiler des Timers, an dem die KR hängt (= SY_TIMER8_PRESCALER)
SY_KR_EXT	1	1 = KR extern (wenn 0, dann muß SY_KR_INT = 1 sein)
SY_KR_INT	0	0 = KR intern (wenn 0, dann muß SY_KR_EXT = 1 sein)
SY_KS1	0	Eingang des CC195 an den Klopfsensor 1 angeschlossen ist
SY_KS2	1	Eingang des CC195 an den Klopfsensor 2 angeschlossen ist
SY_KS3	2	Eingang des CC195 an den Klopfsensor 3 angeschlossen ist
SY_KS4	3	Eingang des CC195 an den Klopfsensor 4 angeschlossen ist
SY_SHK_OT	1	1 = ...

1g. Systemkonstanten der Lambdaregelung

Label	Wert	Beschreibung
SY_AAU	0	0 = keine Vorgabe Sollambda für Abgasuntersuchung
SY_LAMBTS	0	0 = kein Bauteileschutz
SY_STEREO	0	0 = Mono - Lambdaregelung
SY_STERVK	0	0 = Mono - Lambdaregelung vor Kat.
SY_STERHK	0	0 = Mono - Lambdaregelung hinter Kat.
SY_STETLR	1	1 = Stetige Lambda-Regelung vorhanden
SY_UBDEDIS	5.9247	Ubatt-Schwelle (physikalisch) für Sperren der DV-E-Endstufe
SY_UBDEEN	6.9462	Ubatt-Schwelle (physikalisch) für Freigeben der DV-E-Endstufe
SY_UBOKDIS	5.9247	UB-Wert (physikalisch) für ES-Abschaltung von DC-Motor
SY_UBOKEN	6.9462	UB-Wert (physikalisch) für ES-Freigabe von DC-Motor
SY_UB13V	13.0071	UB-Wert für HLSU [V] (= 191 dez)
SY_USOFF	0.0	Spannungsoffset zwischen El.masse und Lambdasondenmasse [0...5V] (= 205 dez)
SY_ZP_LA...	0	=SY_ZP_LAMREG_EUUI; 0 = Standard, VK-Sonde an VK-AD-Kanal angeschlossen

1h. Systemkonstanten zur Konfiguration von Software und Funktionen

Label	Wert	Beschreibung
EPK_MAX_LEN	50	Länge der Epromkennung
ERCOS_T...	5	= ERCOS_TIMER_INPUT_SEL (= SY_ERCOS_TIMER_INPUT_SEL)
FREQ_CPU	20000	(= SY_FREQ_CPU)
PRESCALER	5	(= SY_PRESCALER)
SY_ASICR...	1	= SY_ASICRUNTIME; 1 = ASIC-Laufzeit aufgerundet auf ganze ms
SY_ATR	0	0 = keine Abgastemperaturregelung
SY_EEPROM...	1	=SY_EEPROM_ADDRESS_MODE; 1 = Wordadressierung (Hybridversion) (=SY_HYBRID)
SY_EEPROM...	1024	=SY_EEPROM_SIZE; Eepromgröße in Bytes
SY_ERCOS...	5	= SY_ERCOS_TIMER_INPUT_SEL
SY_FREQ_CPU	20000	CPU-Frequenz
SY_KWP71	0	0 = Keyword-Protokoll KWP71 nicht vorhanden
SY_ME71	0	0 = kein ME7.1-SG
SY_ME73	1	1 = ME7.3-SG
SY_ME75	0	0 = kein ME7.5-SG
SY_ME751	0	0 = kein ME7.5.1-SG
SY_PRESCALER	5	...
SY_REVTIM...	16	=SY_REVTIM_PRE; Vorteiler des Timers, an dem die Drehzahlerkennung hängt (= SY_TIMER1_PRESCALER)
SY_RLTEST	50	Testkonstante für rlvsol_w
SY_TIMER1...	16	=SY_TIMER1_PRESCALER; Prescaler von Timer1
SY_TIMER3...	64	=SY_TIMER3_PRESCALER; Prescaler von Timer3
SY_TIMER8...	64	=SY_TIMER8_PRESCALER; Prescaler von Timer8
SY_WFS	1	1 = WFS-Funktion aktiv
SY_WMAX	72	frühester ausgebarbarer Zündwinkel (entspricht 58,5°KW)
SY_WMIN	-36	spätester ausgebarbarer Zündwinkel (entspricht -24°KW)



ii. Systemkonstanten zur Konfiguration der SCATT-Testerschnittstelle

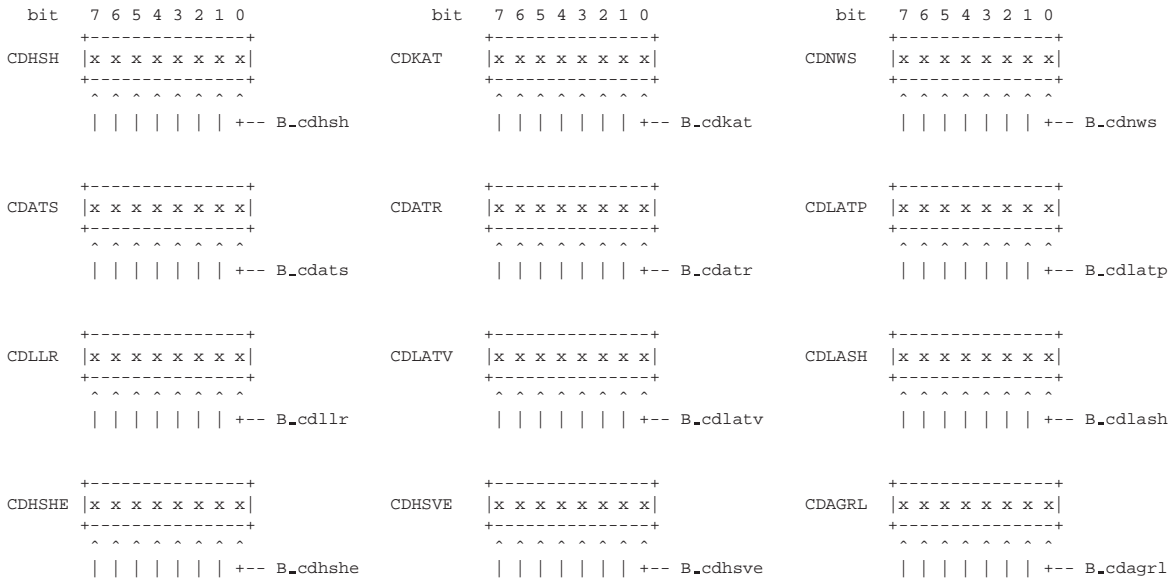
Label	Wert	Beschreibung
SY_M1I00A	190	Codierung von DATA A in Mode 1 PID \$00 nach SAE J1979
SY_M1I00B	31	Codierung von DATA B in Mode 1 PID \$00 nach SAE J1979
SY_M1I00C	224	Codierung von DATA C in Mode 1 PID \$00 nach SAE J1979
SY_M1I00D	16	Codierung von DATA D in Mode 1 PID \$00 nach SAE J1979
SY_M2I00A	127	Codierung von DATA A in Mode 2 PID \$00 nach SAE J1979
SY_M2I00B	184	Codierung von DATA B in Mode 2 PID \$00 nach SAE J1979
SY_M2I00C	0	Codierung von DATA C in Mode 2 PID \$00 nach SAE J1979
SY_M2I00D	0	Codierung von DATA D in Mode 2 PID \$00 nach SAE J1979
SY_M5IH00A	194	Codierung von DATA A in Mode 5 PID \$00 nach SAE J1979 f. S.h. Kat
SY_M5IH00B	0	Codierung von DATA B in Mode 5 PID \$00 nach SAE J1979 f. S.h. Kat
SY_M5IH00C	0	Codierung von DATA C in Mode 5 PID \$00 nach SAE J1979 f. S.h. Kat
SY_M5IH00D	0	Codierung von DATA D in Mode 5 PID \$00 nach SAE J1979 f. S.h. Kat
SY_M5IV00A	0	Codierung von DATA A in Mode 5 PID \$00 nach SAE J1979 f. S.v. Kat
SY_M5IV00B	0	Codierung von DATA B in Mode 5 PID \$00 nach SAE J1979 f. S.v. Kat
SY_M5IV00C	0	Codierung von DATA C in Mode 5 PID \$00 nach SAE J1979 f. S.v. Kat
SY_M5IV00D	1	Codierung von DATA D in Mode 5 PID \$00 nach SAE J1979 f. S.v. Kat
SY_M5IH20A	0	Codierung von DATA A in Mode 5 PID \$20 nach SAE J1979 f. S.h. Kat
SY_M5IH20B	0	Codierung von DATA B in Mode 5 PID \$20 nach SAE J1979 f. S.h. Kat
SY_M5IH20C	0	Codierung von DATA C in Mode 5 PID \$20 nach SAE J1979 f. S.h. Kat
SY_M5IH20D	0	Codierung von DATA D in Mode 5 PID \$20 nach SAE J1979 f. S.h. Kat

Label	Wert	Beschreibung
SY_M5IV20A	0	Codierung von DATA A in Mode 5 PID \$20 nach SAE J1979 f. S.v. Kat
SY_M5IV20B	0	Codierung von DATA B in Mode 5 PID \$20 nach SAE J1979 f. S.v. Kat
SY_M5IV20C	0	Codierung von DATA C in Mode 5 PID \$20 nach SAE J1979 f. S.v. Kat
SY_M5IV20D	0	Codierung von DATA D in Mode 5 PID \$20 nach SAE J1979 f. S.v. Kat
SY_M5IH40A	0	Codierung von DATA A in Mode 5 PID \$40 nach SAE J1979 f. S.h. Kat
SY_M5IH40B	0	Codierung von DATA B in Mode 5 PID \$40 nach SAE J1979 f. S.h. Kat
SY_M5IH40C	0	Codierung von DATA C in Mode 5 PID \$40 nach SAE J1979 f. S.h. Kat
SY_M5IH40D	0	Codierung von DATA D in Mode 5 PID \$40 nach SAE J1979 f. S.h. Kat
SY_M5IV40A	0	Codierung von DATA A in Mode 5 PID \$40 nach SAE J1979 f. S.v. Kat
SY_M5IV40B	0	Codierung von DATA B in Mode 5 PID \$40 nach SAE J1979 f. S.v. Kat
SY_M5IV40C	0	Codierung von DATA C in Mode 5 PID \$40 nach SAE J1979 f. S.v. Kat
SY_M5IV40D	0	Codierung von DATA D in Mode 5 PID \$40 nach SAE J1979 f. S.v. Kat
SY_M5IH60A	0	Codierung von DATA A in Mode 5 PID \$60 nach SAE J1979 f. S.h. Kat
SY_M5IH60B	0	Codierung von DATA B in Mode 5 PID \$60 nach SAE J1979 f. S.h. Kat
SY_M5IH60C	0	Codierung von DATA C in Mode 5 PID \$60 nach SAE J1979 f. S.h. Kat
SY_M5IH60D	0	Codierung von DATA D in Mode 5 PID \$60 nach SAE J1979 f. S.h. Kat
SY_M5IV60A	0	Codierung von DATA A in Mode 5 PID \$60 nach SAE J1979 f. S.v. Kat
SY_M5IV60B	0	Codierung von DATA B in Mode 5 PID \$60 nach SAE J1979 f. S.v. Kat
SY_M5IV60C	0	Codierung von DATA C in Mode 5 PID \$60 nach SAE J1979 f. S.v. Kat
SY_M5IV60D	0	Codierung von DATA D in Mode 5 PID \$60 nach SAE J1979 f. S.v. Kat
SY_M5IH80A	0	Codierung von DATA A in Mode 5 PID \$80 nach SAE J1979 f. S.h. Kat
SY_M5IH80B	0	Codierung von DATA B in Mode 5 PID \$80 nach SAE J1979 f. S.h. Kat
SY_M5IH80C	0	Codierung von DATA C in Mode 5 PID \$80 nach SAE J1979 f. S.h. Kat
SY_M5IH80D	0	Codierung von DATA D in Mode 5 PID \$80 nach SAE J1979 f. S.h. Kat
SY_M5IV80A	0	Codierung von DATA A in Mode 5 PID \$80 nach SAE J1979 f. S.v. Kat
SY_M5IV80B	0	Codierung von DATA B in Mode 5 PID \$80 nach SAE J1979 f. S.v. Kat
SY_M5IV80C	0	Codierung von DATA C in Mode 5 PID \$80 nach SAE J1979 f. S.v. Kat
SY_M5IV80D	0	Codierung von DATA D in Mode 5 PID \$80 nach SAE J1979 f. S.v. Kat
SY_M6I00A	160	Codierung von DATA A in Mode 6 PID \$00 nach SAE J1979
SY_M6I00B	0	Codierung von DATA B in Mode 6 PID \$00 nach SAE J1979
SY_M6I00C	0	Codierung von DATA C in Mode 6 PID \$00 nach SAE J1979
SY_M6I00D	0	Codierung von DATA D in Mode 6 PID \$00 nach SAE J1979
SY_M8I00A	128	Codierung von DATA A in Mode 8 PID \$00 nach SAE J1979
SY_M8I00B	0	Codierung von DATA B in Mode 8 PID \$00 nach SAE J1979
SY_M8I00C	0	Codierung von DATA C in Mode 8 PID \$00 nach SAE J1979
SY_M8I00D	0	Codierung von DATA D in Mode 8 PID \$00 nach SAE J1979
SY_M8I00E	0	Codierung von DATA E in Mode 8 PID \$00 nach SAE J1979









## ABK PROKON 53.11 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDAGR			FW	code word DAGR inactiv (EURO-coding)
CDAGRL			FW	code word to disable position sensor diagnosis (EURO coding)
CDATR			FW	configuration byte diagnosis exhaust temperature control
CDATS			FW	configuration byte diagnosis exhaust temperature sensor
CDDST			FW	code word CARB: EURO byte for deactivation of tank press. sensor diagn.
CDHSH			FW	code word heating diagnose after Kat (CDHSH = 0 => no diagnosis)
CDHSHE			FW	Eurobit for output stage diag. of lambda sensor heating downstream of the cat.
CDHSV			FW	code word heating diagnose upstr. Kat (CDHSV = 0 => no diagnosis)
CDHSVE			FW	Code word DHLSE power stage of heater for diagnosis pre cat
CDKAT			FW	code word: catalyst diagnosis in OBDII-mode (inverse: European mode)
CDKVS			FW	code word: DKVS active/inactive, CD.=0 -> no diagnosis
CDLASH			FW	code word O2-sensor aging diagnosis (SHK) in OBDII mode (invers => Europe mode)
CDLATP			FW	code word oxgen sensor aging diagnosis (TP) in OBDII mode (inv.: in Europe mode)
CDLATV			FW	code word lambda sensor monitoring (Tv) in OBDII mode (invers: Europe mode)
CDLDP			FW	code word LDP diag. in OBDII mode (inverse: Europe mode), CD.=0 -> no diapos.
CDLLR			FW	code word DLLR inactiv (EURO-coding), CD.=0 -> no diagnosis
CDLSA			FW	code word oxgen sensor aging diagnosis, configuration byte, for application
CDLSH			FW	code word lambda sensor diagnosis behind KAT in OBDII-Mode (invers: Europe mode)
CDLSV			FW	code word oxygen sensor diagnosis upstr. KAT in OBDII mode
CDMD			FW	code word DMD inactive(EURO-coding), CD.=0 -> no diagnosis
CDNWS			FW	code word DNWS disable (EURO-coding), CD.=0 -> no diagnosis
CDSLS			FW	code word secondary air system in OBDII mode (inv: Europe mode)
CDSLSE			FW	eurobyte for output stage diagnosis of secondary-valve/pump
CDSWE			FW	code word DSWE inactive (EURO-Coding), CD.=0 -> no diagnosis
CDTANKL			FW	code word DTANKL inactiv (EURO-coding), CD.=0 -> no diagnosis
CDTES			FW	code word disable canister-purge monitoring (Euro coding), CD.=0 -> no dia.
CSCATT			FW	eurobyte for scan-tool
CWERFIL			FW	Codeword for selection of misfire fault codes for output to scan tool
CWKKLIMA			FW	code word air condition
CWKONABG			FW	code word for configuration exhaust emission treatment
CWKONFZ1			FW	code word for configuration vehicle
CWKONLS			FW	code word for configuration lambda sensor
CWMDAPP			FW	code word for calibration without torque structure
CWOBD			FW	code word for configuration OBD certification
CWTF			FW	code word for configuration temperature sensors
CWUHR			FW	code word for the clock
NSWO1			FW	engine-speed threshold 1 for switching calculation
NSWO2			FW	engine-speed threshold 2 for switching calculation

Variable	Source	Type	Description
B_4WD	PROKON	AUS	Condition 4 wheel drive
B_ABSTNL	PROKON	AUS	condition soak time calculation via ECM-afterrun
B_ASRFZ	PROKON	AUS	Condition for ASR in the automobile
B_AUTGET	PROKON	AUS	condition automatic gearbox
B_CDAGR	PROKON	AUS	function active per codeword CDAGR
B_CDAGRL	PROKON	AUS	function active per codeword CDAGRL
B_CDATR	PROKON	AUS	condition: diagnose exhaust temperature control enabled
B_CDATS	PROKON	AUS	condition diagnosis exhaust temperature sensor enabled
B_CDDST	PROKON	AUS	function active per codeword CDDST
B_CDHSH	PROKON	AUS	function active per codeword CDHSH
B_CDHSHE	PROKON	AUS	function active per codeword CDHSHE



Variable	Source	Type	Description
B_CDHSV	PROKON	AUS	function active per codeword CDHSV
B_CDHSVE	PROKON	AUS	function active per codeword CDHSVE
B_CDKAT	PROKON	AUS	function active per codeword CDKAT
B_CDKVS	PROKON	AUS	function active per codeword CDKVS
B_CDLASH	PROKON	AUS	function active per codeword CDLASH
B_CDLATP	PROKON	AUS	function active per codeword CDLATP
B_CDLATV	PROKON	AUS	function active per codeword CDLATV
B_CDLDP	PROKON	AUS	function active per codeword CDLDP
B_CDLLR	PROKON	AUS	function active per codeword CDLLR
B_CDLSA	PROKON	AUS	function active per codeword CDLSA
B_CDLSH	PROKON	AUS	function active per codeword CDLSH
B_CDLSV	PROKON	AUS	function active per codeword CDLSV
B_CDMD	PROKON	AUS	function active per codeword CDMD
B_CDNWS	PROKON	AUS	function active per codeword CDNWS
B_CDSLS	PROKON	AUS	function active per codeword CDSLS
B_CDSLSE	PROKON	AUS	function active per codeword CDSLSE
B_CDSWE	PROKON	AUS	function active per codeword CDSWE
B_CDTANKL	PROKON	AUS	function active per codeword CDTANKL
B_CDTES	PROKON	AUS	function active per codeword CDTES
B_CSCATT	PROKON	AUS	Function shut down by code word CSCATT
B_CVT	PROKON	AUS	Condition continuously variable transmission
B_F1GETR	PROKON	AUS	Condition F1-gearbox (electronic clutch control)
B_FPWDKAP	PROKON	AUS	throttle-valve control by accelerator pedal
B_KATFZ	PROKON	AUS	condition: cat fitted in vehicle
B_KATH	PROKON	AUS	Condition cat-heater installed in vehicle
B_KLIMA	PROKON	AUS	Condition air condition
B_LDSAFW	PROKON	AUS	Boost control in open loop application mode with fixed value LDRAPP
B_LDSAPP	PROKON	AUS	Boost control in open loop application mode with KFLDRAPP
B_LS3	PROKON	AUS	Condition 3. Lambda sensor installed downstream of outlet (Bank1)
B_LS32	PROKON	AUS	Condition 3. Lambda sensor installed downstream of outlet (Bank2)
B_LS4	PROKON	AUS	Condition 4. Lambda sensor installed downstream of outlet (Bank1)
B_LS42	PROKON	AUS	Condition 4. Lambda sensor installed downstream of outlet (Bank2)
B_LSH	PROKON	AUS	Cond. lambda sensor inst. downstr. of cat., 2. sensor downst. of outlet (Bank1)
B_LSH2	PROKON	AUS	Cond. lambda sensor inst. downstr. of cat., 2. sensor downst. of outlet (Bank2)
B_LSV	PROKON	AUS	Cond. lambda sensor inst. upstr. of the cat., 1. sensor downst. of outlet(Bank1)
B_LSV2	PROKON	AUS	Cond. lambda sensor inst. upstr. of the cat., 1. sensor downst. of outlet(Bank2)
B_MT	PROKON	AUS	Condition manuell gear box
B_NSWO1	PROKON	AUS	condition engine speed > NSWO1
B_NSWO2	PROKON	AUS	condition engine speed > NSWO2
B_SLSFZ	PROKON	AUS	condition: SLS fitted in vehicle
B_TFU	PROKON	AUS	condition ambient temperature sensor exists
B_UHRRMIN	PROKON	AUS	Condition clock with a relative counter of minutes
B_UHRRSEC	PROKON	AUS	Condition clock with a relative counter of seconds
B_WDKSAP	PROKON	AUS	throttle-blade contol by fixed value, bit 1 has priority
B_ZWAPPL	PROKON	AUS	Condition ignition-timing applications without torque intervention
CW_ERFIL	PROKON	AUS	Status codeword for selection of misfire fault codes for output to scan tool
CW_OBD	PROKON	AUS	Status Code word CWOBD
NMOT	SWADAP	EIN	engine speed
SY_2SG	PROKON	AUS	system constant 2 motronic systems
SY_AAU	PROKON	AUS	system constant: lambda value possible for exhaust-emission check by tester
SY_AAV	PROKON	AUS	system constant condition : shut-off-valve available
SY_AGR	PROKON	AUS	system constant EGR present
SY_AIRBAG	PROKON	AUS	system constant airbag-signal present
SY_ATR	PROKON	AUS	system constant exhaust-gas temperatur controller built in
SY_CAN	PROKON	AUS	system constant CAN configuration
SY_CDCSIZE	PROKON	AUS	system constant: freeze frame count
SY_CDKSIZE	PROKON	AUS	system constant CDK-size
SY_CDTSIZE	PROKON	AUS	system constant: freeze frame count
SY_CLASIZE	PROKON	AUS	system constant: freeze frame count
SY_CONFSL	PROKON	AUS	system constant: secondary air present
SY_DELFCSM	PROKON	AUS	system constant: selection of the reset routine for scan tool mode \$04
SY_DFPMTIM	PROKON	AUS	system constant: Time info in fault code memory
SY_DFPMVAR	PROKON	AUS	system constant: Version of DFPM
SY_DGANZ	PROKON	AUS	system constant, number of speed sensors
SY_DLS	PROKON	AUS	system constant
SY_DOPZW	PROKON	AUS	system constant, ignition type (0=single, 1=double)
SY_DTANKL	PROKON	AUS	system constant "fuel tank empty" diagnosis active
SY_DVEADA	PROKON	AUS	system constant BGVE: disabling injection and ignition during DV-E-adaptation
SY_EGAS	PROKON	AUS	system constant E-GAS present
SY_EGFE	PROKON	AUS	system characteristic input-value
SY_FCMSIZE	PROKON	AUS	system constant: Maximum number of fault entries
SY_FFCSIZE	PROKON	AUS	system constant: Size of CARB-Freeze Frame
SY_FFESIZE	PROKON	AUS	system constant: Size of Freeze Frame-extension
SY_FFTSIZE	PROKON	AUS	System constant: freeze frame count/field
SY_FLUQ	PROKON	AUS	System constant misfire detection quantization irregular running
SY_FREQCPU	PROKON	AUS	System constant CPU frequency
SY_GAP	PROKON	AUS	system constant: number of missing teeth in the gap
SY_GGGTS	PROKON	AUS	system constant: sensor variable exact temperature signal
SY_GRDWRT	PROKON	AUS	System constant basic value, space between SW reference mark to OT in teeth
SY_HYBRID	PROKON	AUS	System constant hybrid ECU (false = conventional, true = hybrid)
SY_JSOPROT	PROKON	AUS	System constant: tester protocol selection of the ISO-standards for scan tool
SY_KMTR	PROKON	AUS	system constant: cooling-agent temperature control exists



Variable	Source	Type	Description
SY_KS1	PROKON	AUS	system constant: input of the CC195 onto which knock sensor 1 is connected
SY_KS2	PROKON	AUS	system constant: input of the CC195 onto which knock sensor 2 is connected
SY_KS3	PROKON	AUS	system constant: input of the CC195 onto which knock sensor 3 is connected
SY_KS4	PROKON	AUS	system constant: input of the CC195 onto which knock sensor 4 is connected
SY_KWP71	PROKON	AUS	System constant key-word protocol KWP71 present
SY_LAMBTS	PROKON	AUS	system constant component protection present
SY_LLR	PROKON	AUS	System constant LLR configuration
SY_M1I00A	PROKON	AUS	System constant coding from DATA A in Mode 1 PID \$00 acc. to SAE J1979
SY_M1I00B	PROKON	AUS	System constant coding from DATA B in Mode 1 PID \$00 acc. to SAE J1979
SY_M1I00C	PROKON	AUS	System constant coding from DATA C in Mode 1 PID \$00 acc. to SAE J1979
SY_M1I00D	PROKON	AUS	System constant coding from DATA D in Mode 1 PID \$00 acc. to SAE J1979
SY_M2I00A	PROKON	AUS	System constant coding from DATA A in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00B	PROKON	AUS	System constant coding from DATA B in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00C	PROKON	AUS	System constant coding from DATA C in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00D	PROKON	AUS	System constant coding from DATA D in Mode 2 PID \$00 acc. to SAE J1979
SY_M5IH00A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH20A	PROKON	AUS	Sys. con. cod. DATA A in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20B	PROKON	AUS	Sys. con. cod. DATA B in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20C	PROKON	AUS	Sys. con. cod. DATA C in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20D	PROKON	AUS	Sys. con. cod. DATA D in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH40A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$40 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH40B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$40 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH40C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$40 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH40D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$40 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH60A	PROKON	AUS	Sys. con. cod. DATA A in mode 5 PID \$60 acc. to SAE J1979 sen. downstream cat.
SY_M5IH60B	PROKON	AUS	Sys. con. cod. DATA B in mode 5 PID \$60 acc. to SAE J1979 sen. downstream cat.
SY_M5IH60C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$60 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH60D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$60 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH80A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$80 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH80B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$80 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH80C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$80 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH80D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$80 acc. to SAE J1979 for sen. downst. cat.
SY_M5IV00A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80A	PROKON	AUS	Sys. const. cod. DATA A Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80B	PROKON	AUS	Sys. const. cod. DATA B Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80C	PROKON	AUS	Sys. const. cod. DATA C Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80D	PROKON	AUS	Sys. const. cod. DATA D Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M6I00A	PROKON	AUS	System constant coding from DATA A in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00B	PROKON	AUS	System constant coding from DATA B in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00C	PROKON	AUS	System constant coding from DATA C in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00D	PROKON	AUS	System constant coding from DATA D in Mode \$06 PID \$00 acc. to SAE J1979
SY_M8I00A	PROKON	AUS	System constant coding from DATA A in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00B	PROKON	AUS	System constant coding from DATA B in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00C	PROKON	AUS	System constant coding from DATA C in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00D	PROKON	AUS	System constant coding from DATA D in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00E	PROKON	AUS	System constant coding from DATA E in mode 8 PID \$00 according to SAE J1979
SY_MAX_EV	PROKON	AUS	Maximal amount of outputs reserved for injectors
SY_NLDG	PROKON	AUS	System constant: TRUE crankshaft limp home function available
SY_NWS	PROKON	AUS	system constant camshaft control: none, 2 point or continuous
SY_NZUEB	PROKON	AUS	nnot Schwelle für Übergang von Z1 nach Z2
SY_PBRPW	PROKON	AUS	system constant plausibility check brake/pedal-travel sensor
SY_PGRAD	PROKON	AUS	system constant: kind of the phase signal
SY_PGRAD2	PROKON	AUS	system constant: kind of the 2. phase signal
SY_PH2OFST	PROKON	AUS	system const. offset in syncros between the 2 active phase signals, 2 PGs only
SY_PHTWIN	PROKON	AUS	system constant 1/2 phase sensing system (sensor, wheel)
SY_REDMX	PROKON	AUS	system constant: max. cylinder cutoff step
SY_SGANZ	PROKON	AUS	system constant, number of engine ECU's
SY_STEREO	PROKON	AUS	system constant condition: stereo lambda control
SY_STERHK	PROKON	AUS	system parameter condition stereo downstream catalyst
SY_STERSY	PROKON	AUS	system constant condition stereo lambda control symmetrical
SY_STERVK	PROKON	AUS	system constant condition: stereo exhaust system upstream of cat
SY_STETLR	PROKON	AUS	System constant condition continuous Lambda control present



Variable	Source	Type	Description
SY_SU	PROKON	AUS	system constant: version of intake runner length adjuster
SY_SWE_S	PROKON	AUS	System constant: SWE by statistics
SY_TAGR	PROKON	AUS	system constant service device intervention EGR rate
SY_TCNS	PROKON	AUS	system constant service device
SY_TDZW	PROKON	AUS	System constant
SY_TEBF	PROKON	AUS	system constant initial filling fuel system (service device)
SY_TEETH	PROKON	AUS	system constant: number of teeth with gap teeth on the crankshaft wheel
SY_TFA	PROKON	AUS	configuration of the fitting position of air temperature sensor
SY_TFBA	PROKON	AUS	system constant service device intervention accel. enrichment
SY_TFMA	PROKON	AUS	system constant: intake air temperature signal available (initial. GGTFM)
SY_TFMAP	PROKON	AUS	system constant: intake air temp.sensor with shunt resistor in input circuitry
SY_TFMO	PROKON	AUS	system constant: engine oil temperature signal available (initial. GGTFM)
SY_TFNS	PROKON	AUS	system constant service device intervention afterstart factor
SY_TFRK	PROKON	AUS	system constant service device correction of relative fuel mass rk
SY_TFST	PROKON	AUS	system constant service device intervention start factor
SY_TFUMG	PROKON	AUS	system constant: ambient temperature sensor present
SY_TFVA	PROKON	AUS	system constant service device intervention decel. enleanment
SY_TFWL	PROKON	AUS	system constant service device intervention warm-up factor
SY_TLR	PROKON	AUS	system constant service device intervention LR, modif. of integrator stop time
SY_TMDR	PROKON	AUS	system constant service device
SY_TN	PROKON	AUS	system constant tn-signal, SY_ZYLZA/SY_TN = amount tn-impulses over 720 ° crank.
SY_TNLS	PROKON	AUS	system constant service device
SY_TRLX	PROKON	AUS	System constant for correction by service tester to rImax exists
SY_TSFSIZE	PROKON	AUS	System constant: freeze frame count
SY_TURBO	PROKON	AUS	system constant for turbocharged engine
SY_TVVR	PROKON	AUS	system constant tester connection to vmax-control
SY_UB13V	PROKON	AUS	System constant UB value for 13 Volt
SY_UBDEDIS	PROKON	AUS	Ubatt threshold for disabling the DV-E output stage
SY_UBDEEN	PROKON	AUS	Ubatt threshold for enabling the DV-E output stage
SY_UBOKDIS	PROKON	AUS	System constant UB value for ES shutoff of DC motor
SY_UBOKEN	PROKON	AUS	System constant UB value for ES enabling of DC motor
SY_UBR	PROKON	AUS	system constant onboard battery voltage scanned from main relay input
SY_UJMLS	PROKON	AUS	System constant voltage difference between sensor ground and electronic ground
SY_USOFF	PROKON	AUS	System constant voltage difference between sensor ground and electronic ground
SY_WMAX	PROKON	AUS	System constant earliest ignition timing that can be outputed
SY_WMIN	PROKON	AUS	System constant latest ignition timing that can be outputed
SY_WNB	PROKON	AUS	System constant for angle of tooth distance from crankshaft signal
SY_ZAS	PROKON	AUS	system constant cylinder deactivation ZAS included
SY_ZNDAUS	PROKON	AUS	System constant ignition timing output (single or double fir.)
SY_ZYLZA	PROKON	AUS	system constant number of cylinders
SY_ZZBANK	PROKON	AUS	system constant cylinder assignment bank1/bank2, 0 bank1, 1 b.2, binary value

### FW PROKON 53.11 Fixed Values

Parameter	Value	Description
CDAGR		code word DAGR inactiv (EURO-coding)
CDAGRL		code word to disable position sensor diagnosis (EURO coding)
CDATR		configuration byte diagnosis exhaust temperature control
CDATS		configuration byte diagnosis exhaust temperature sensor
CDDST		code word CARB: EURO byte for deactivation of tank press. sensor diagn.
CDHSH		code word heating diagnose after Kat (CDHSH = 0 => no diagnosis)
CDHSHE		Eurobit for output stage diag. of lambda sensor heating downstream of the cat.
CDHSV		code word heating diagnose upstr. Kat (CDHSV = 0 => no diagnosis)
CDHSVE		Code word DHLSE power stage of heater for diagnosis pre cat
CDKAT		code word: catalyst diagnosis in OBDII-mode (inverse: European mode)
CDKVS		code word: DKVS active/inactive, CD.=0 -> no diagnosis
CDLASH		code word O2-sensor aging diagnosis (SHK) in OBDII mode (invers => Europe mode)
CDLATP		code word oxgen sensor aging diagnosis (TP) in OBDII mode (inv.: in Europe mode)
CDLATV		code word lambda sensor monitoring (Tv) in OBDII mode (invers: Europe mode)
CDLDP		code word LDP diag. in OBDII mode (inverse: Europe mode), CD.=0 -> no diapos.
CDLLR		code word DLLR inactiv (EURO-coding), CD.=0 -> no diagnosis
CDLSA		code word oxgen sensor aging diagnosis, configuration byte, for application
CDLSH		code word lambda sensor diagnosis behind KAT in OBDII-Mode (invers: Europe mode)
CDLSV		code word oxygen sensor diagnosis upstr. KAT in OBDII mode
CDMD		code word DMD inactive(EURO-coding), CD.=0 -> no diagnosis
CDNWS		code word DNWS disable (EURO-coding), CD.=0 -> no diagnosis
CDSL		code word secondary air system in OBDII mode (inv: Europe mode)
CDSLSE		eurobyte for output stage diagnosis of secondary-valve/pump
CDSWE		code word DSWE inactive (EURO-Coding), CD.=0 -> no diagnosis
CDTANKL		code word DTANKL inactiv (EURO-coding), CD.=0 -> no diagnosis
CDTES		code word disable canister-purge monitoring (Euro coding), CD.=0 -> no dia.
CSCATT		eurobyte for scan-tool
CWERFIL		Codeword for selection of misfire fault codes for output to scan tool
CWKLIMA		code word air condition
CWKONABG		code word for configuration exhaust emission treatment
CWKONFZ1		code word for configuration vehicle
CWKONLS		code word for configuration lambda sensor
CWMDAPP		code word for calibration without torque structure
CWOBD		code word for configuration OBD certification
CWTF		code word for configuration temperature sensors
CWUHR		code word for the clock



Parameter	Value	Description
NSWO1		engine-speed threshold 1 for switching calculation
NSWO2		engine-speed threshold 2 for switching calculation

## FB PROKON 53.11 Detailed description of function

### 1. Introduction:

The function describes the project configuration. That is to say that all system constants, all global code words (affecting several functions) and all Euro switches are listed here.

### 2.1. Software configuration by means of system constants SY....:

System constants cause a differing (certain) compilation and thereby lead to different Hex files. System constants cannot be applied and cannot be read by VS100.

In %PROKON, system-constant send connectors are defined as receive connectors in the functional FDEFs. The differentiation is made:

```
"- System computing variables: "
  purely computing variables, e.g.: SY_REDMX
"- System description constants: "
  can switch over functional sections/characteristics, e.g.: SY_ZYLZA,
```

### 2.2. Project configuration by code words CW..:

Code words can be applied as fixed values. The same program is always used for implementing changes in code words. E.g.: CWKONFZ1

The interface between %PROKON and the functions that use global words is established by means of status bits and

bytes. These bits are evaluated in %PROKON from the code words (send connector) and read into the corresponding functions (receive connector).

Project configuration at a late date is thereby possible by using a tester at the end of the line.

### 2.2.1. Deactivation of diagnostic functions by means of the Euro switch CD..:

Code words which cause a shut-down of diagnostic functions (Euro switches) are designated with CD... . E.g.: CDSLS

## APP PROKON 53.11 Application hint

### SY\_ZZBANK: Zylinderzuordnung

Ferrari F131 --> 2 Steuergeräte, die getrennt betrachtet werden (jedes für sich ist Bank1):

Zündreihenfolge Gesamtsystem: 1 8 3 6 4 5 2 7

```
Bank rechts  Zylinder Nr.  - - - - 2 4 3 1 <--- Zündreihenfolge in Pfeilrichtung
Bank links  Zylinder Nr.  - - - - 7 5 6 8 <--- Zündreihenfolge in Pfeilrichtung
              EvNr       8 7 6 5 4 3 2 1 <--- Einspritzreihenfolge in Pfeilrichtung-Zählweise 1 ... SY_ZYLZA
              | | | | | | |
SY_ZZBANK = zzbank = 0 dez  0 0 0 0 0 0 0 0   Zylinderzuordnung zur Bank:  Bit = false (0)= Ev gehört zu Bank1,
SY_ZZBANKB = zzbankb = 0 dez 0 0 0 0 0 0 0 0   Bit = true (1)= Ev gehört zu Bank 2
```

### SY\_NWS: Nockenwellenverstellung

```
= 0: keine NWS
= 1: 2-Punkt-NWS
= 2: stetige NWS
> 2: nicht definiert
```

### SY\_PGRAD: Typ des Nockenwellengeberrades

```
= 0: kein Geberrad vorhanden
= 1: 1 Impuls pro 720°KW
= 2: nicht definiert
= 3: nicht definiert
= 4: 4 Impulse pro 720°KW (BOSCH Standard Schnellstartgeberrad)
```

### SY\_PGRAD2: Typ des 2. Nockenwellengeberrades --> siehe SY\_PGRAD

### SY\_SU: Saugrohrrumschaltung

```
= 0: keine SU
= 1: ein Schaltausgang
= 2: zwei Schaltausgänge
> 2: nicht definiert
```

### SY\_EGFE: Eingangsgröße Füllungserfassung

```
Bit 0: HFM vorhanden (B_hfmv)
Bit 1: Drucksensor hinter der Drosselklappe vorhanden (B_dssv)
Bit 2: Drucksensor vor der Drosselklappe vorhanden (B_dslvh)
Bit 3: Umgebungsdrucksensor (Pu-Sensor) (B_dsuv)
```

### SY\_TFA: Einbauort TANS-Sensor

```
Bit0: TANS-Sensor im HFM
Bit1: TANS-Sensor nicht im HFM
```

### SY\_ZNDAUS: 1= Einzelfunken, 2= Doppelfunken



## DEKON 40.10 Configuration of power stage diagnosis

### FDEF DEKON 40.10 Function definition

Assignment of output stages to components

#### 1. Configuration of output stages

The configuration is made with the Label ESKONF by 7 bytes.  
Every byte is standing for 4 output stages. Therefore every output stage has got 2 consecutive configuration Bits.

For Hybrid-ECUs and PCB-ECUs the Label have to be filled with different data, because of the different assignment of output stages to the components.

#### Enable of the output stages diagnosis

With the configurations-Bytes in ESKONF the functions have to be set active / inactive depending on the available components in the car. At the same time with the 2 Bits the function of the diagnosis is set.  
Assignment of the Bit pattern:

Pair of Bits:

1. Bit	2. Bit	
0	0	Diagnosis active with OBDII-malfunction storage with test of healing
0	1	Diagnosis active without OBDII-malfunction storage with test of healing
1	0	Diagnosis active without OBDII-Fehlerspeicherung without test of healing (-> EKP)
1	1	Diagnosis not active

The output stage diagnosis is set to "inactive" when the component ist not built-in, or also when no output stage diagnosis for is available for that component.

The following tables show a surviev of the assignment of the output stages in the hybrid ECU for the projects Alfa Romeo B-Motor.

Projekt: ME 7.3.1H B-Motor 2.0I, 1.8I mit SU- und NM-Verstellung

ESKONF		Bit	76	54	32	10
Byte	Wert /dez	"				
0	0		EV4 00 E_ev4/PIN M52	EV3 00 E_ev3/PIN M03	EV2 00 E_ev2/PIN M35	EV1 00 E_ev1/PIN M19
1	48		LSHVK1 00 E_hsv1/PIN M34	xxxx 11 E_xxxx/PIN M21	TEV 00 E_teve/PIN M05	MIL 00 E_mile/PIN F46
2	131		EKP 10 E_kpe/PIN F30	LUE1 00 E_luea/PIN F50	LSHVK2 00 E_hsv2/PIN M02	xxxx 11 E_xxxx/PIN F02
3	240		---	---	KOS 00 E_kose/PIN F13	LUE2 00 E_lueb/PIN F62
4	195		xxxx 11 E_xxxx /PIN M53	SU1 00 E_sue/PIN M04	NWS 00 E_nwse/PIN M36	xxxx 11 E_xxxx/PIN M20
5	255		xxxx 11 E_xxxx/PIN F18	xxxx 11 E_xxxx/PIN F33	xxxx 11 E_xxxx/PIN F34	xxxx 11 E_xxxx/PIN F01
6	255		xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M45	xxxx 11 E_xxxx/PIN M45





Projekt:ME 7.3.1H B-Motor 1.6l Y mit NW-Verstellung

Byte Wert Bit 76 54 32 10  
" /dez "

0	0	EV4 00 E_ev4/PIN M52	EV3 00 E_ev3/PIN M03	EV2 00 E_ev2/PIN M35	EV1 00 E_ev1/PIN M19
1	48	LSHVK1 00 E_hsve/PIN M34	xxxx 11 E_xxxx/PIN M21	TEV 00 E_teve/PIN M05	MIL 00 E_mile/PIN F46
2	131	EKP 10 E_kpe/PIN F30	LUE1 00 E_luea/PIN F50	LSHVK2 00 E_hsve2/PIN M02	xxxx 11 E_xxxx/PIN F02
3	240	---	---	KOS 00 E_kose/PIN F13	LUE2 00 E_lueb/PIN F62
4	243	xxxx 11 E_xxx /PIN M53	xxxx 11 E_xxx/PIN M04	NWS 00 E_nwse/PIN M36	xxxx 11 E_xxxx/PIN M20
5	255	xxxx 11 E_xxxx/PIN F18	xxxx 11 E_xxxx/PIN F33	xxxx 11 E_xxxx/PIN F34	xxxx 11 E_xxxx/PIN F01
6	255	xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M45	xxxx 11 E_xxxx/PIN M45



Projekt:ME 7.3.1H B-Motor 1.6l ECO

Byte Wert Bit 76 54 32 10  
" /dez "

0	0	EV4 00 E_ev4/PIN M52	EV3 00 E_ev3/PIN M03	EV2 00 E_ev2/PIN M35	EV1 00 E_ev1/PIN M19
1	48	LSHVK1 00 E_hsve/PIN M34	xxxx 11 E_xxxx/PIN M21	TEV 00 E_teve/PIN M05	MIL 00 E_mile/PIN F46
2	131	EKP 10 E_kpe/PIN F30	LUE1 00 E_luea/PIN F50	LSHVK2 00 E_hsve2/PIN M02	xxxx 11 E_xxxx/PIN F02
3	240	---	---	KOS 00 E_kose/PIN F13	LUE2 00 E_lueb/PIN F62
4	255	xxxx 11 E_xxx /PIN M53	xxxx 11 E_xxx/PIN M04	xxxx 11 E_xxxx/PIN M36	xxxx 11 E_xxxx/PIN M20
5	255	xxxx 11 E_xxxx/PIN F18	xxxx 11 E_xxxx/PIN F33	xxxx 11 E_xxxx/PIN F34	xxxx 11 E_xxxx/PIN F01
6	255	xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M13	xxxx 11 E_xxxx/PIN M45	xxxx 11 E_xxxx/PIN M45

Definition der Fehlerspeicherschnittstellen

### ABK DEKON 40.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ESKONF			FW	configuration of power stage (actuators)

### FW DEKON 40.10 Fixed Values

Parameter	Value	Description
ESKONF		configuration of power stage (actuators)



## FB DEKON 40.10 Detailed description of function

### APP DEKON 40.10 Application hint

## VS\_VERST 2.40 Adjusting parameters for McMess

### FDEF VS\_VERST 2.40 Function definition

Position	Label	Adjusting variable	Initial.value	Variable	Limit	Quant/INC.	Frame	%Section
1	vszw	Ignition timing	0° KW	Byte	-96..95.25°KW	0.75 °KW		ZUE
2	vsfrk	Mixture factor	1,0	Byte	0.75..1.25	0.001953		ESGRU
3	vsvw	Advancement angle	0° KW	Byte	-768°...762°	6° KW		ESVW
4	vsns	Nominal speed	0 RPM	Byte	0..2550/min	10 RPM		LLRNS
5	vszskr[0]	Ignition timing firing 1	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
6	vszskr[1]	Ignition timing firing 2	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
7	vszskr[2]	Ignition timing firing 3	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
8	vszskr[3]	Ignition timing firing 4	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
9	vszskr[4]	Ignition timing firing 5	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
10	vszskr[5]	Ignition timing firing 6	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
11	vszskr[6]	Ignition timing firing 7	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
12	vszskr[7]	Ignition timing firing 8	0°	Byte	-96..95.25°KW	0.75 °KW		KRRA
13	vske	Knock detection threshold	0	Byte	-8..8	0,0627		KRKE
14	vsdmr	Torque reserve	0 %	Byte	0..99.6%	0.3906%		MDKOL
15	vsfpes	Manifold air pressure	1	Byte	0..2	0,0078		AES

In case turbo installed: SY\_TURBO = true

16	vsrlmx	max.rl for LDR	0%	Byte	Conv.: rel_sb_q0p75			LDRLMX
17	vsldtv	TV LDR for appl. control	0%	Byte	Conv.: tv_ub_q0p64			LDTVMA

In case camshaft adjustment present: SY\_NWS = 2

18	vswnws	Angle NW for VANOS	0°	Byte	wkw_ub_q0p25	0,25 °KW		WNWEIN
----	--------	--------------------	----	------	--------------	----------	--	--------

%VS\_VERST describes the parameters to be adjusted by means of McMess. The effects of the adjustment are described in the pertinent sections on the individual functions (refer to above table in %Section).

The RAM cells are set once to the initialization values given above for the following conditions:

1. C.ini
2. For B\_mcacti = 0 (McMESS is not active). B\_mcacti is updated in the 1-sec time frame.
3. For entry and exit in McMESS communication (item 3 not applicable as required, corresponds to item 2).

If CWVSV = 0 VS\_VERST isn't active. Only for CWVSV > 0 adjustment with McMess is possible.

### ABK VS\_VERST 2.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWVSV			FW	code word f. deactivation VS_VERST (CWVSV = 0: VS_VERST inactive)
Variable	Source		Type	Description
B_MCACTI	VS_VERST		LOK	Condition McMESS active
SY_NWS	PROKON		EIN	system constant camshaft control: none, 2 point or continuous
SY_TURBO	PROKON		EIN	system constant for turbocharged engine
VSDMR	VS_VERST		AUS	adjustable torque reserve via VSxy
VSFPSES	VS_VERST		AUS	factor for modifying intake manifold pressure during Application injection
VSFRK	VS_VERST		AUS	Correction of the relative fuel mass by adjusting systems
VSKE	VS_VERST		AUS	adjustable offset for knock detection threshold via VS20
VSLDTV	VS_VERST		AUS	Correction value boost control from VS-system for application
VSNS	VS_VERST		AUS	Change of target engine speed with calibrating tool VSxy



Variable	Source	Type	Description
VSRLMX	VS_VERST	AUS	Additive load correction for rlmx from application system
VSVW	VS_VERST	AUS	change in the phase injection angle by the application system
VSWNWS	VS_VERST	AUS	Change of the variable camshaft angle by adjusting system VSxy
VSZW	VS_VERST	AUS	Ignition-timing correction by adjusting system
VSZWKR	VS_VERST	AUS	cylinder individual adjustment of ignition angle by VS2x

### FW VS\_VERST 2.40 Fixed Values

Parameter	Value	Description
CWVSV		code word f. deactivation VS_VERST (CWVSV = 0: VS_VERST inactive)

### FB VS\_VERST 2.40 Detailed description of function

#### APP VS\_VERST 2.40 Application hint

## EG 4.0 Input variables including diagnostics for these

### FDEF EG 4.0 Function definition

The functional group EG contains the detection of input signals of the engine control system (ECS) and its diagnosis. Over and above that, further engine parameters are calculated using the measured input values.

The group is structured in following subgroups:

```
EGNWE: input values rotational speed- and angle detection
EGFE: input signals load detection
EGTE: input parameter of temperature acquisition
EGAK: input signal of exhaust value of catalyst
EGEG: input variable E-Gas
EGKE: input signals knock detection
EGAG: general input values
```

### ABK EG 4.0 Abbreviations

#### FW EG 4.0 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB EG 4.0 Detailed description of function

The function group "input signals" separates parts of the system that depend direct on the sensor acquisition, from these parts of the engine control functions which are independent from the hardware.

Inputs of the group EG are signals from sensors (e.g. output signal of the inductive rotational speed sensor). These signals are calculated in the corresponding function to physical - sensor independent - state variables of the engine or vehicle (e.g. engine speed nmot in 1/min). There is a diagnosis of the detected signals. If a fault is detected an adequate limp home function is activated.

Finally further engine parameters are calculated using the direct measured values, because of their physical relationship (e.g. speed gradient using the rotational speed, relative air charge using the intake-air mass). For this calculation simple relationships like differential quotients for computing the gradient are used as well as complex physical models in calculating the engine load.

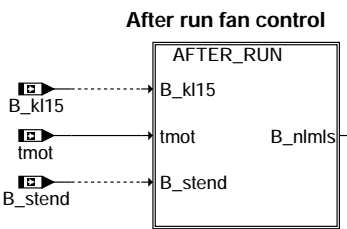
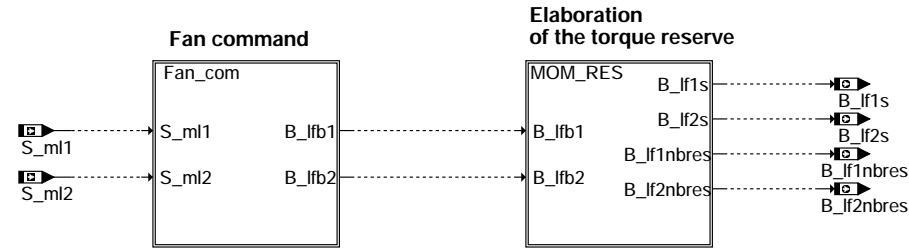
The relevant functions are designated after following conventions in general:

contraction	description
- EG...	functional group of input value detection.
- GG...	function for sensor signals which describes the evaluation of the sensor signals and often the diagnosis of the sensor. These functions are sensor specific and depend on the ECU hardware.
- D...	diagnosis function which describes the check of the sensor signal if it is not included in GG functions.
- BG...	calculated value: describes the determination of engine parameters which can not be measured directly.

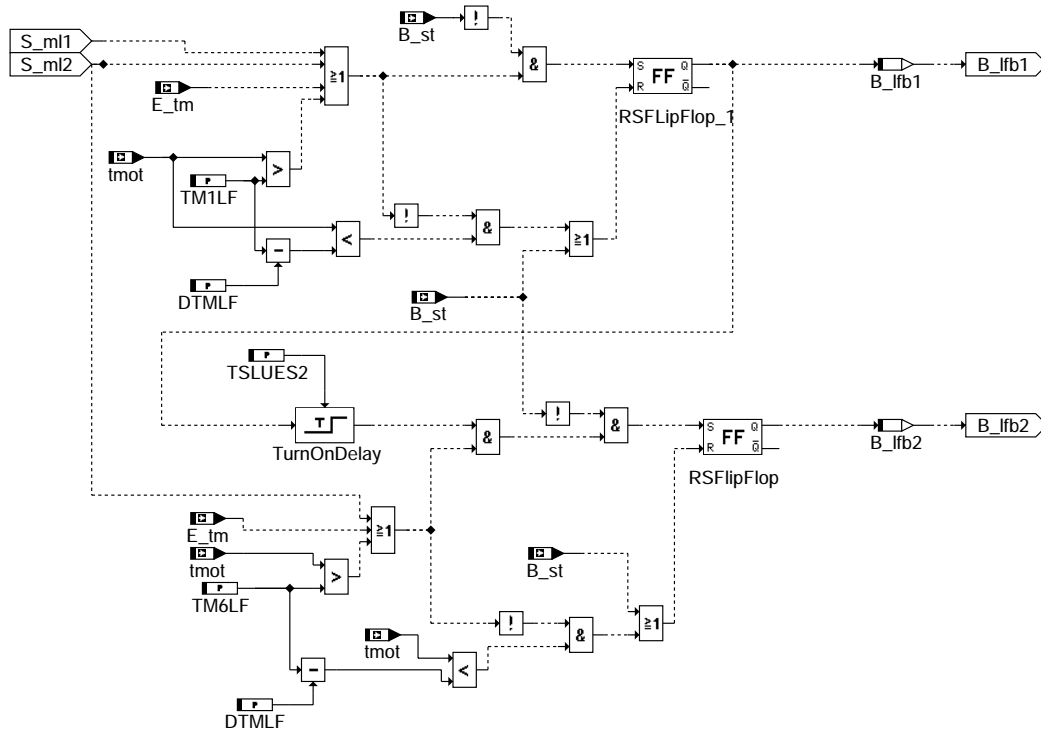
APP EG 4.0 Application hint

## LFS 18.30 Engine cooling fan control

### FDEF LFS 18.30 Function definition



ifs-main

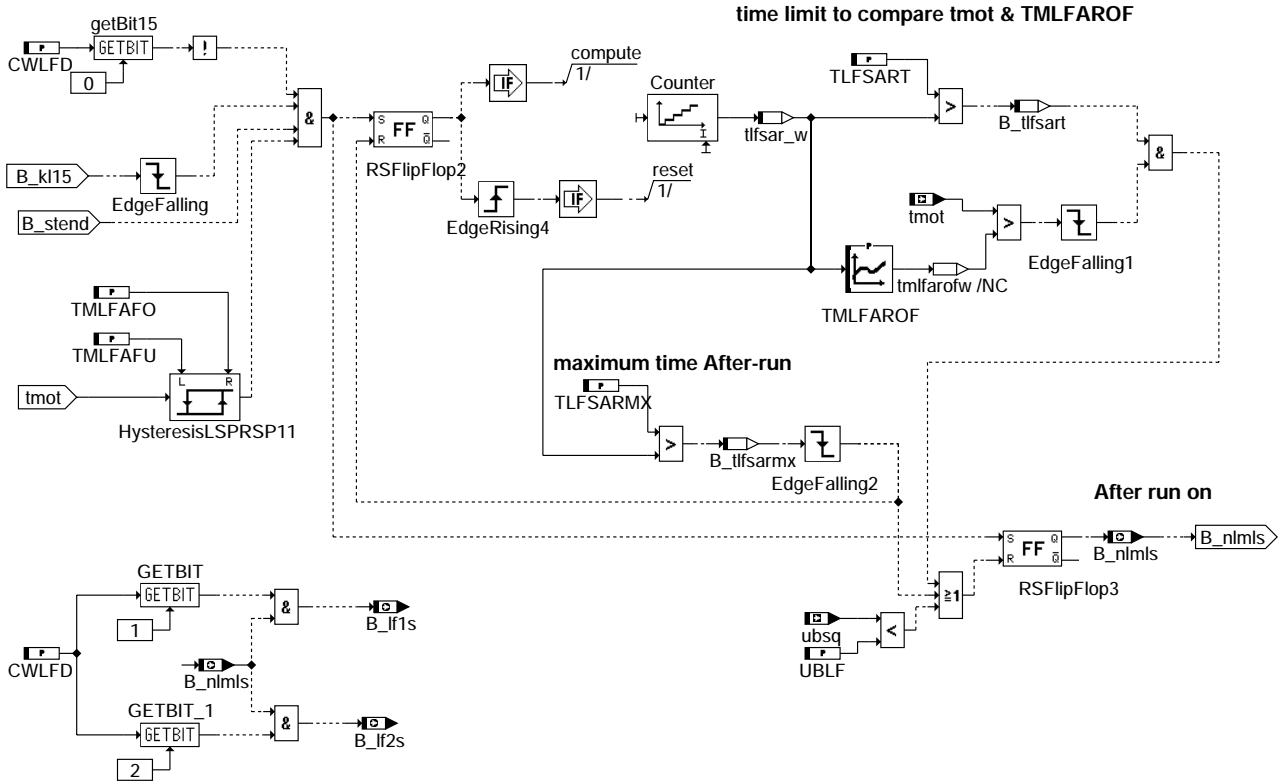


ifs-fan-com

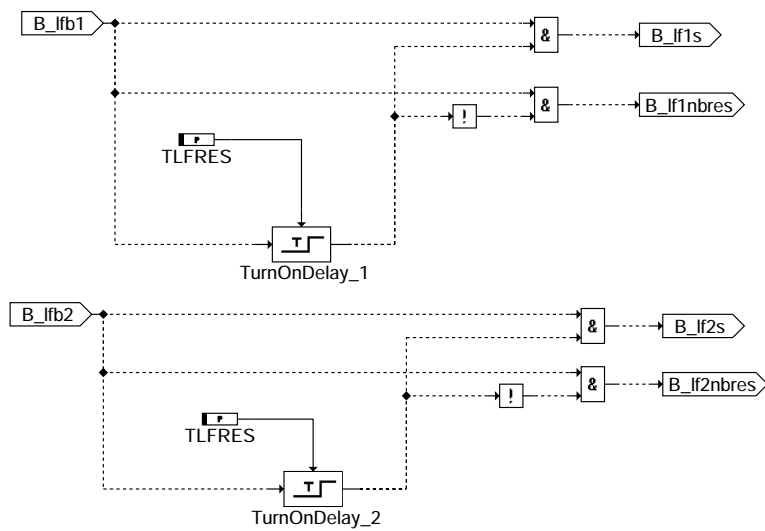
ifs-main

ifs-fan-com

## After run Cooling fan Control



### ifs-after-run



### ifs-mom-res

No text for FDEF available!

### ABK LFS 18.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWLFD			FW	Codewort : configuration of the fan control
DTMLF			FW	hysteresis engine temperature fan control
TLFRES			FW	time of delay prior to changing the fan speed (torque reseve)
TLFSARMX			FW	maximum time for the after-run operation
TLFSART			FW	time limit in after-run to compare engine coolant temperature
TM1LF			FW	Engine temperature threshold 1 for cooling fan control step 1
TM6LF			FW	Engine temperature threshold 6 for cooling fan control step 2
TMLFAFO			FW	engine cooling temperature above which After-run operation is started
TMLFAFU			FW	engine cooling temperature above which After run operation is started



Parameter	Source-X	Source-Y	Type	Description
TMLFAROF	TLFSAR_W		KL	Engine coolant temperature below which After run is terminated
TSLUES2			FW	Delay time of fan stage 1 to 2 in [sec]
UBLF			FW	minimal battery voltage for fan afterrun

Variable	Source	Type	Description
B_KL15		EIN	condition ignition switch on
B_LF1NBRES	LFS	AUS	Condition for torque reserve for engine cooling fan step 1 normal operation on fan 1 on condition
B_LF1S	LFS	AUS	Condition for torque-reserve build at engine-fan stage 2, normal operation on fan 2 on condition
B_LF2NBRES	LFS	AUS	Condition for torque-reserve build at engine-fan stage 2, normal operation on fan 2 on condition
B_LF2S	LFS	AUS	Condition for torque-reserve build at engine-fan stage 2, normal operation on fan 2 on condition
B_LFB1	LFS	LOK	fan 1 stand by condition
B_LFB2	LFS	LOK	fan 2 stand by condition
B_NLMLS	LFS	AUS	request for ECM afterrun from the engine-fan-control
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_TLFSARMX	LFS	LOK	Condition: time limit during After run to compare tmot
B_TLFSART	LFS	LOK	Condition: time limit during After run to compare tmot
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
S_ML1		EIN	
S_ML2		EIN	
TLFSAR_W	LFS	LOK	time during After run to compare Engine coolant temperature
TMOT	SWADAP	EIN	Engine temperature
UBSQ	GGUB	EIN	battery voltage (on board), converted to standard quantization

### FW LFS 18.30 Fixed Values

Parameter	Value	Description
CWLF		Codewort : configuration of the fan control
DTMLF		hysteresis engine temperature fan control
TLFRES		time of delay prior to changing the fan speed (torque reseve)
TLFSARMX		maximum time for the after-run operation
TLFSART		time limit in after-run to compare engine coolant temperature
TM1LF		Engine temperature threshold 1 for cooling fan control step 1
TM6LF		Engine temperature threshold 6 for cooling fan control step 2
TMLFAFO		engine cooling temperature above which After-run operation is started
TMLFAFU		engine cooling temperature above which After run operation is started
TSLUES2		Delay time of fan stage 1 to 2 in [sec]
UBLF		minimal battery voltage for fan afterrun

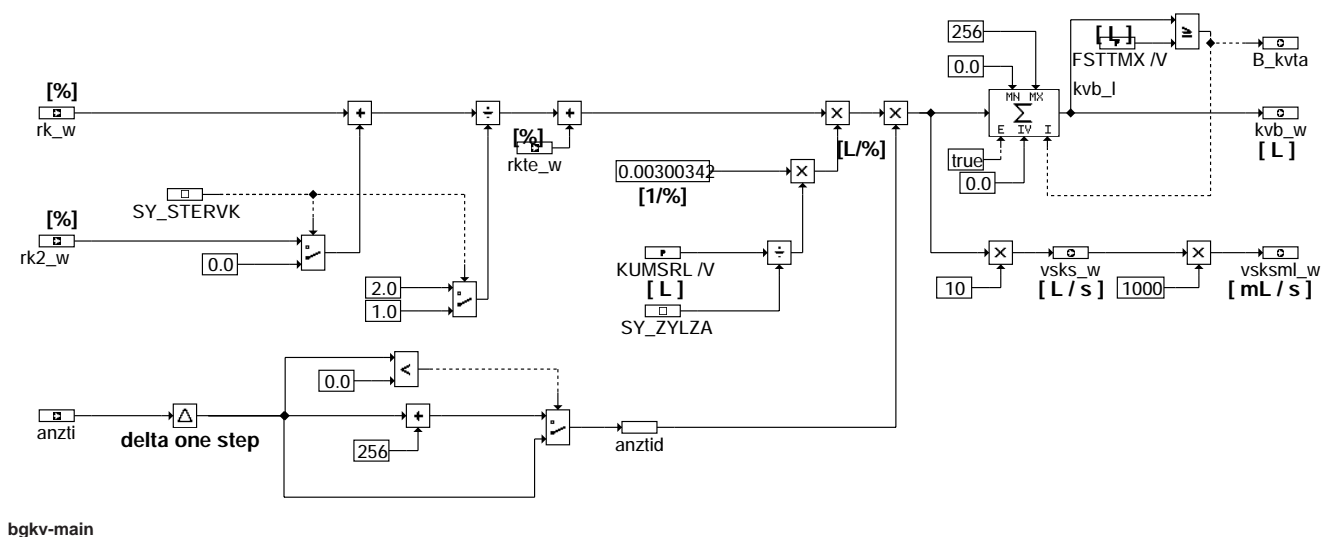
### FB LFS 18.30 Detailed description of function

### APP LFS 18.30 Application hint

### BGKV 1.30 Calculation variable consumed fuel

### FDEF BGKV 1.30 Function definition

Overview of the function: BGKV





## ABK BGKV 1.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FSTTMX			FW	maximum fuel tank capacity
KUMSRL			FW	conversion constant from mass flow to relative air charge
SY_STERVK			SYS	system constant condition: stereo exhaust system upstream of cat
SY_ZYLZA			SYS	system constant number of cylinders

Variable	Source	Type	Description
ANZTI	ACIFI	EIN	injection counter
ANZTID	BGKV	LOK	difference between injection counters in the calculation matrix
B_KVTA	BGKV	AUS	condition consumed fuel larger then tank capacity
KVB_W	BGKV	AUS	consumed fuel
RK2_W	MSF	EIN	relative fuel mass Bank2
RKTE_W	TEB	EIN	relative fuel part of the purge control
RK_W	MSF	EIN	relative fuel mass
VSKSML_W	BGKV	AUS	volumetric flow of fuel in ml/s
VSKS_W	BGKV	AUS	Volumetric flow of fuel in L/s

## FW BGKV 1.30 Fixed Values

Parameter	Value	Description
FSTTMX		maximum fuel tank capacity
KUMSRL		conversion constant from mass flow to relative air charge

## FB BGKV 1.30 Detailed description of function

Motivation:  
=====

The quantity of fuel used up is needed for diagnosis of the fluid-level sensor in the tank with respect to the consumption. The value for the amount of fuel consumed can also be used as consumption information for the driver.

Task:  
=====

Calculation of the fuel consumed, whereby the integration can only then be reset when the quantity of fuel consumed is the same as the tank contents.

Principle:  
=====

The relative quantity of fuel injected  $rk_w$  is totaled together with the quantity of fuel from the tank ventilation  $rkte_w$  following a conversion of this into a volume. The total of the fuel masses  $rk_w$  and  $rk2_w$  calculated in synchronization is carried out in the 100-ms time frame. To do this, the difference is formed from the injection counter  $anzti$  from the last 100-ms mark and multiplied by the current value from  $rk_w$ . For a two-bank system, the fuel consumed is calculated from the mean value from both of the relative fuel masses  $rk_w$  and  $rk2_w$ .

The conversion of the relative fuel mass  $rk_w$  to the magnitude of the fuel consumed  $kvb_w$  is realized by multiplication of a constant conversion factor (0.00300342) and  $KUMSRL/cylinder$  number.

Physical relationship of the conversion factor:  
=====

Initially it applies that:

$$KUMSRL = VH [dm^3] / 2578 = \text{engine displacement volume} / 2578$$

The conversion factor is then given from the definition for  $rk_w$ :

$$kvb_w / rk_w = \text{Fuel consumed} / \text{rel. fuel mass} = \frac{\text{Air density} * \text{Cylinder displacement volume}}{\text{Fuel density} * \text{A/F ratio} * 1.0 * 100\%}$$

$$\frac{\rho_{0air} [g/dm^3] * KUMSRL[dm^3]/cylinder \text{ no.} * 2578}{\rho_{0KS} [g/dm^3] * LST * 100 [\%]}$$

$$\rho_{0KS} [g/dm^3] * LST * 100 [\%]$$

using the values:

$$\rho_{0air} = 1.293 [g/dm^3]$$

$$\rho_{0KS} = 755.0 [g/dm^3]$$

$$LST = 14.7$$

$$\text{it is given that: } rk_w[\%] * 0.00300342[1/\%] * KUMSRL [L] / ZYLZA = kvb_w [L]$$

A value in liters should be given as the output variable of the function for the fuel consumed during the current driving cycle. The totalizer shall not overrun and is only then reset when an applicable mark  $KVBMX$  is reached.  $FSTTMX$  is thereby the maximum possible volume of fuel consumed during a driving cycle. This maximum volume should be the maximum tank quantity.

Remarks on ASCET-SD diagram  
=====

a) The function with the remark "delta one step" realizes the following function in accordance with the name assigned for this:  
 $anztid(t) = anzti(t) - anzti(t-1)$

if  $t$  is discrete time variable.

b) The switching design according to "delta one step" shall support the overrun function of the  $anzti$  counter.





## APP BGKV 1.30 Application hint

For the application,  
- the maximum tank quantity must be entered in FSTTMX

## BGBSZ 4.10 Calculated Variable Operating Track Counter

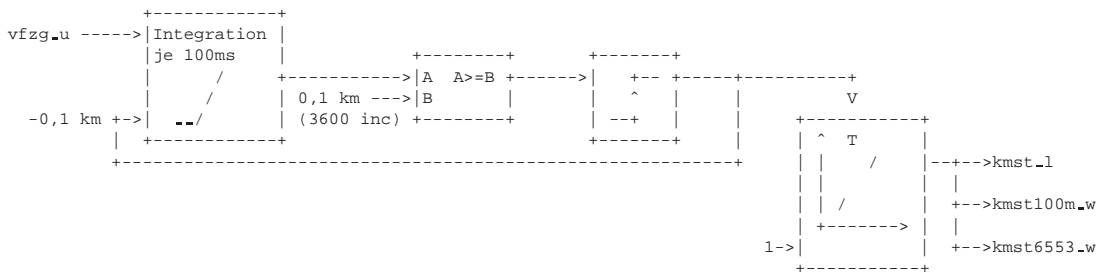
### FDEF BGBSZ 4.10 Function definition

Die im Folgenden berechneten Daten werden über KWP 2000 an den Diagnose-Tester ausgegeben.

Betriebsstrecke kmst\_l1:  
-----

Ebenfalls wird durch Aufaddieren der Geschwindigkeit vfzg\_u in einem festen Zeitraster (100ms) die in diesem Fahrzyklus zurückgelegte Strecke kmst100m berechnet. Die Strecke wird im Nachlauf auf die gesamte mit dem Fahrzeug zurückgelegte Strecke aufaddiert und im EEPROM abgelegt als kmst\_l1. Der 'Kilometerstand' wird als 32bit Größe mit 100m/Inc abgespeichert.

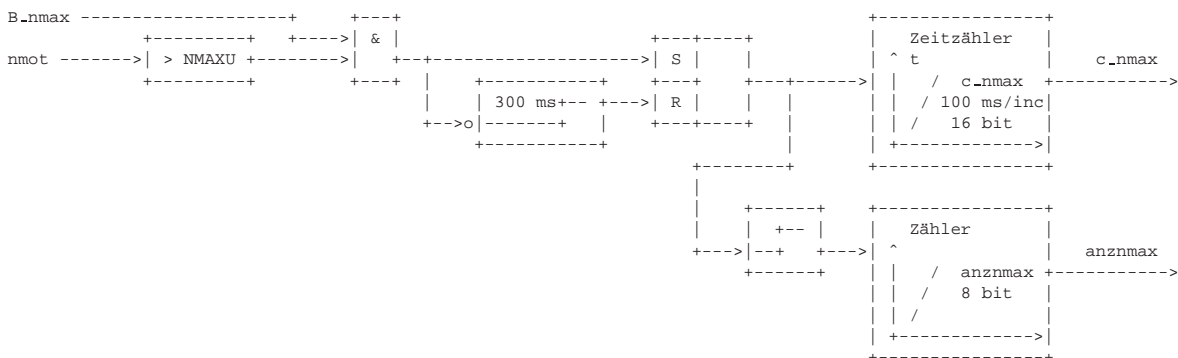
Achtung: In Verbindung mit einem Geschwindigkeitsgeber-Fehler kann der 'Kilometerstand' verfälscht werden.



Maximaldrehzahl nmaxa:  
-----

In dem Programm wird die jemals gefahrene Höchstdrehzahl erfasst und abgespeichert (nmaxa). Dieser Wert wird ebenfalls im EEPROM abgespeichert.

Anzahl und Dauer der Fahrten in der Drehzahlbegrenzung:  
-----



NMAXU: Da B\_nmax auch bei Drehzahlbegrenzung bei EGAS-Notlauf oder Getriebeschutz gesetzt wird. Vorschlagswert NMAXU: Nähe NMAXD ca. 6000 1/min. Entprellzeit 300 ms: notwendig, da B\_nmax bei aktiver Drehzahlbegrenzung ca. im "100 ms-Takt" jitters.



## ABK BGBSZ 4.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
NMAXU			FW	lower n max threshold
Variable	Source		Type	Description
ANZNMAX	BGBSZ		AUS	Number of times NMAX exceeded
B_NMAX	NMAXMD		EIN	1 = maximum engine speed exceeded
C_NMAX	BGBSZ		AUS	
KMST100M_W	BGBSZ		AUS	Kilometers covered by vehicle (Odometer) 100m/Inc as 16 bit low-word
KMST6553_W	BGBSZ		AUS	Kilometers covered by vehicle (Odometer) 6553,6km /Inc as 16 bit high-word
KMST_L	BGBSZ		AUS	Kilometers covered by vehicle (Odometer) 100m/Inc as 32bit-longword
NMOT	SWADAP		EIN	engine speed
VFZG_U	DFFTCNV		EIN	Vehicle speed

## FW BGBSZ 4.10 Fixed Values

Parameter	Value	Description
NMAXU		lower n max threshold

## FB BGBSZ 4.10 Detailed description of function

### APP BGBSZ 4.10 Application hint

## EGNWE 1.0 Input values rotational speed- and angle detection

### FDEF EGNWE 1.0 Function definition

### ABK EGNWE 1.0 Abbreviations

### FW EGNWE 1.0 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB EGNWE 1.0 Detailed description of function

description missing !!!!

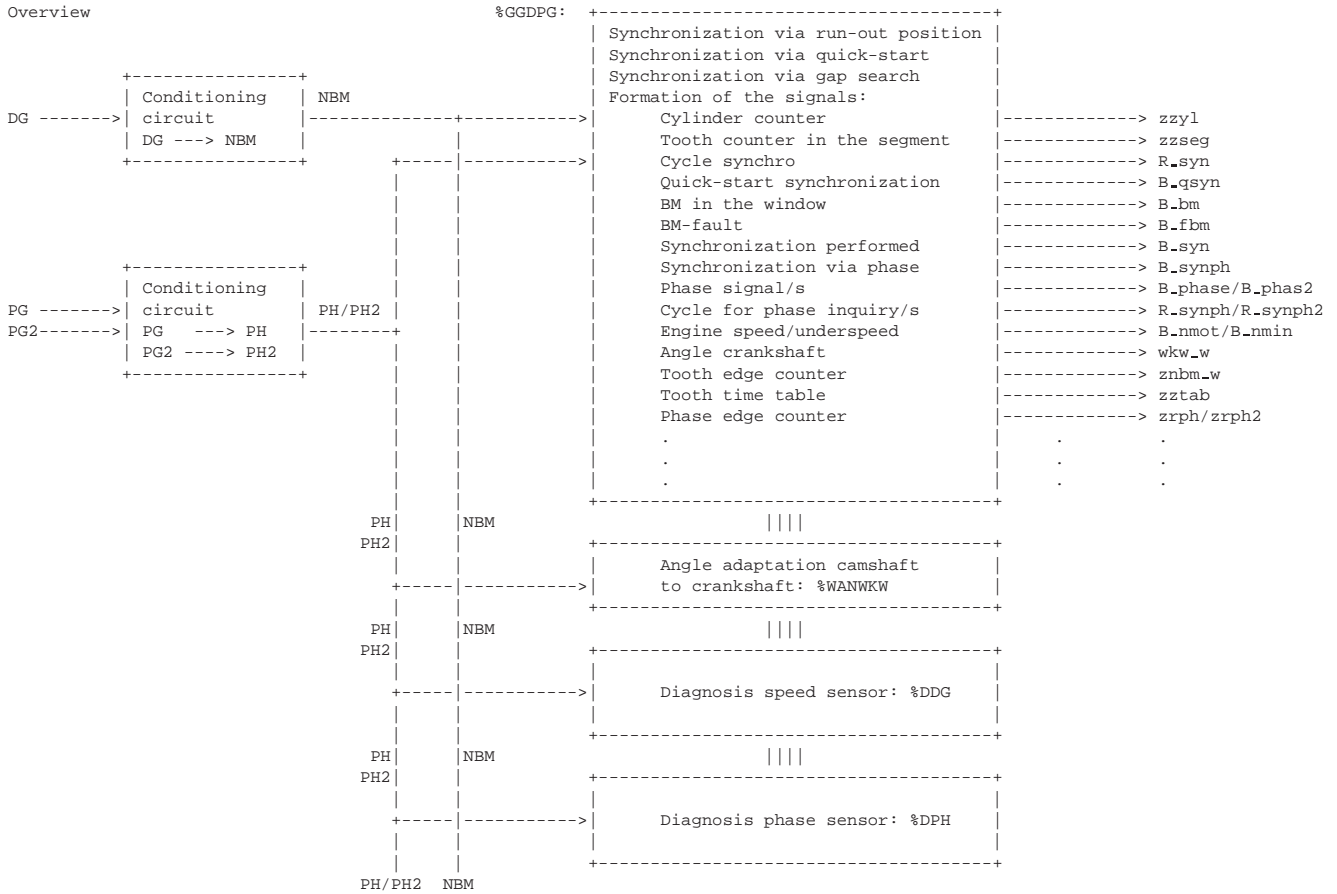
### APP EGNWE 1.0 Application hint

## GGDPG 14.30 Input Signals: engine speed and phase sensor

### FDEF GGDPG 14.30 Function definition

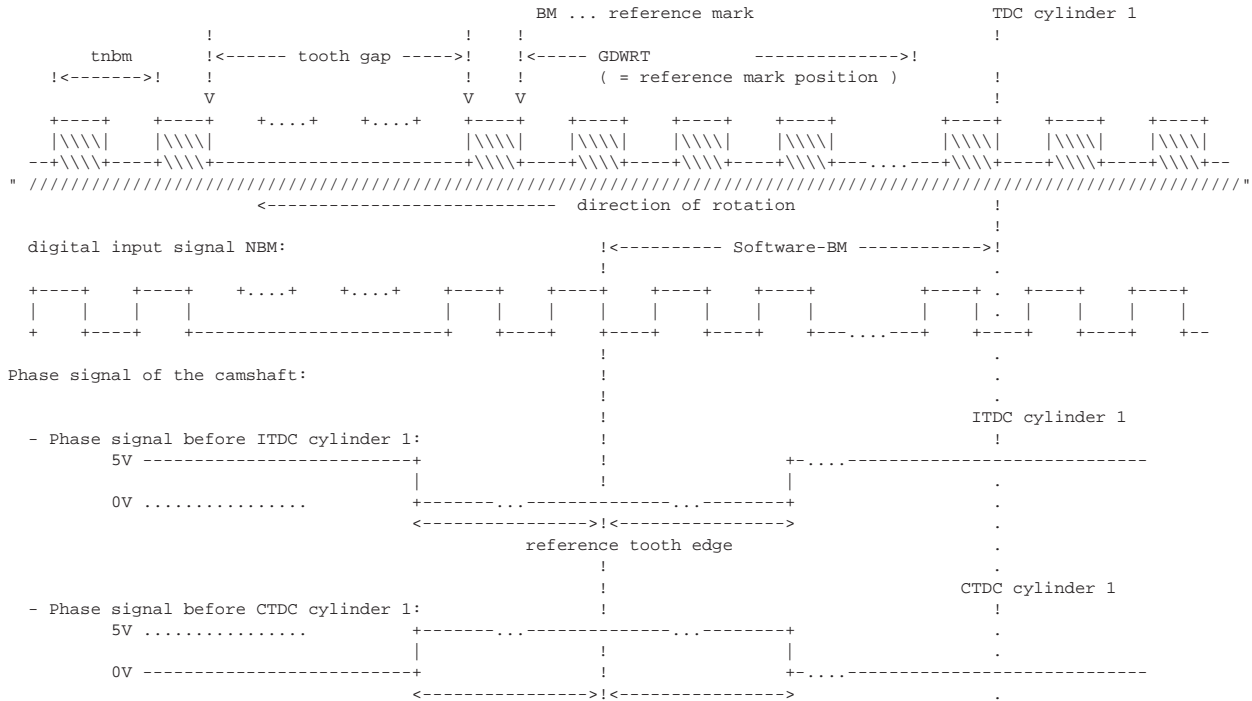


Overview





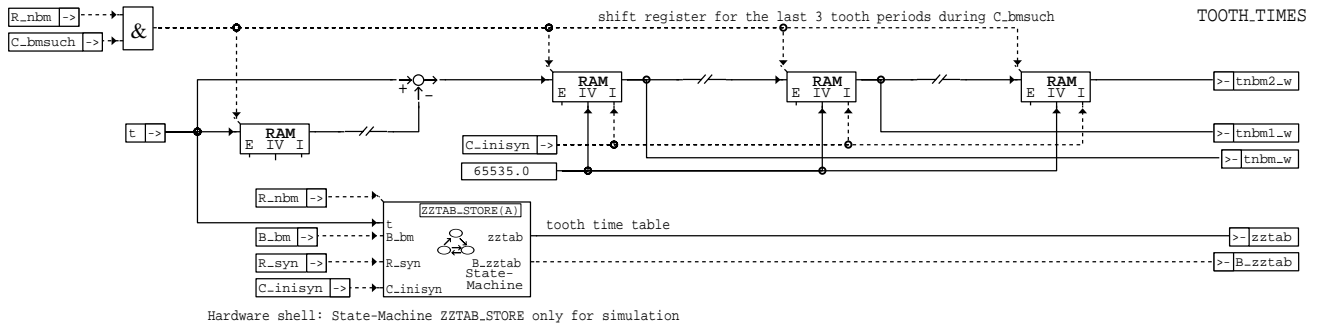
mechanical 60-2 crankshaft ring gear:



The section %GGDPG contains the following functions:

- CRANK\_ANGLE
  - \* Tooth debouncing, B\_zprel
  - \* Continuous tooth counter znbm\_w resp. angle counter wkw\_w
  - \* Angle at the beginning of the working cycle wkw\_bzm0\_w
  - \* Angle at the beginning of the segment wkwsyn\_w
- PHASE\_SIGNAL
  - \* Scanning of the phase signal B\_phase, B\_phas2
  - \* Phase edge counter zrph, zrph2
- TOOTH\_TIMES
  - \* Formation of the tooth times tnbm\_w, tnbm1\_w and tnbm2\_w during the gap search
  - \* Formation of the tooth time table zztab after found gap
- MIN\_SPEED
  - \* Monitoring of the crankshaft (CS) signal for engine speed (B\_nmot) resp. underspeed (B\_nmin)
- SYNCHRONIZATION
  - \* Synchronization search
    - Gap search, setting of B\_bm
    - Phase synchronization at the gap
    - Quick-start synchronization via the quick-start sensor wheel
  - \* Monitoring of the synchronization search, B\_nobm
  - \* Gap check, B\_bm, B\_fbm
    - Gap correct ==> B\_bm=1, B\_fbm=0
    - Gap 1 tooth incorrect ==> B\_bm=1, B\_fbm=1, trigger correction by 1 tooth
    - Gap not found ==> B\_bm=1, B\_fbm=1, trigger new synchronization
- SYNCHRO
  - \* Formation of the cylinder counter
  - \* Generation of the synchro interrupt (R\_syn)
  - \* Generation of the cycles for the phase inquiry (R\_synph, R\_synph2)
  - \* Crankshaft revolution counter (uzkw\_w)
  - \* Calculation of the initialization values for the cylinder and the tooth counter from the stop position wkwstop calculated in the run-out detection.





ggdpg-tooth-times

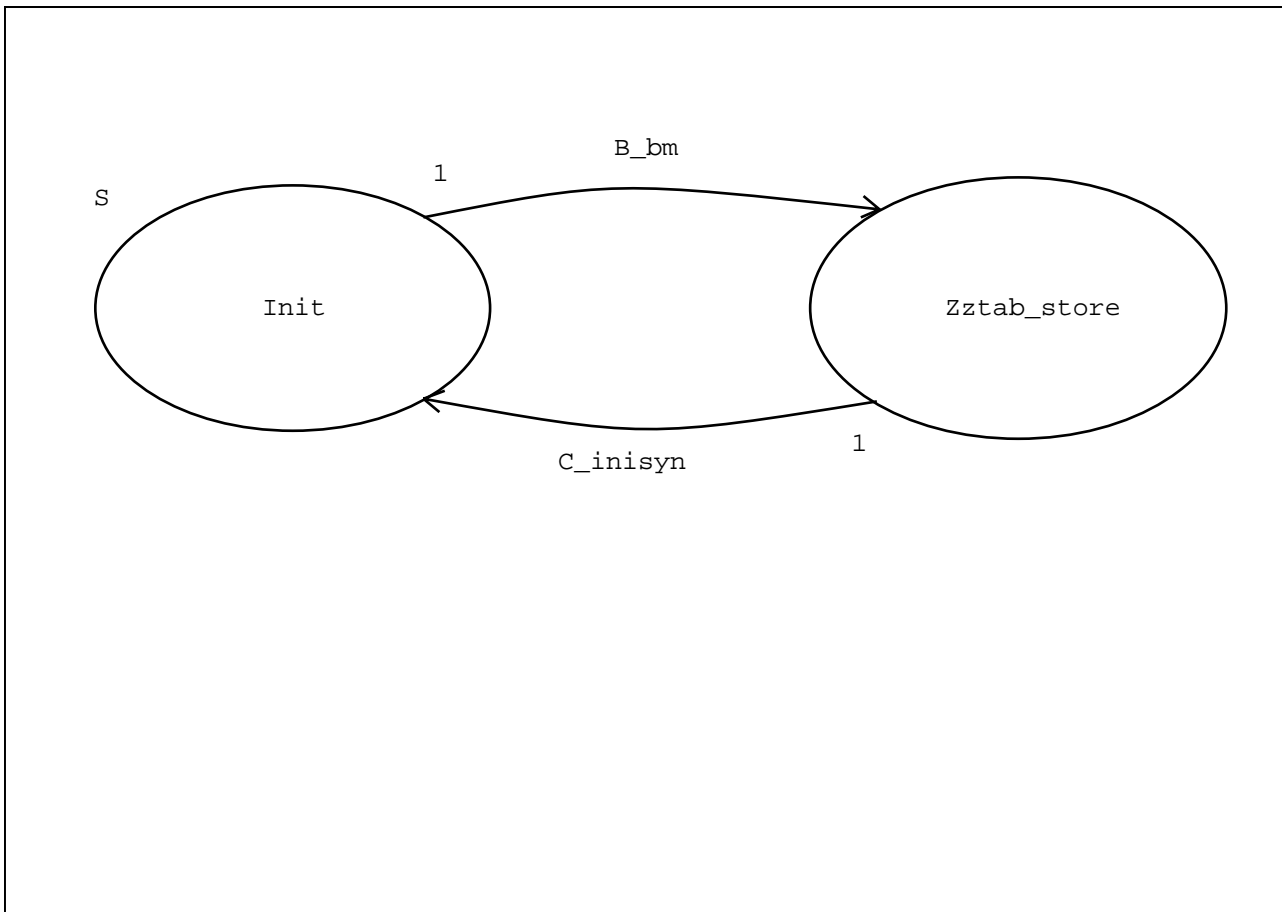
**ggdpg-tooth-times**

Calculation of the tooth times resp. formation of the tooth time table.

During the reference mark search phase (C\_bmsuch) the period tnbm\_w is formed with each tooth and shifted to a shift register with 3 elements (tnbm\_w, tnbm1\_w and tnbm2\_w).

As soon as the reference mark was found (B\_bm = 1) the system time t of the respective tooth is written into the tooth time table in ZTAB\_STORE. The condition B\_zztab is set as soon as the tooth time table is completely filled (2. synchro).

The partial function ZTAB\_STORE is calculated in the hardware casing and is illustrated here as state machine for the simulation.



ggdpg-zztab-store

**ggdpg-zztab-store**



State machine to store the system time t into the tooth time table when a tooth interrupt occurs.

At each tooth interrupt the table pointer zztaptr is increased and the current segment time t is written into the tooth time table. In the synchro interrupt the two latest tooth times are copied to the beginning of the table and the pointer is set to the second table entry.

```

State Machine ZZTAB_STORE
-----
|      Transition name +- Transition condition
|      |              +- Action code
|      |              |
|      |              |
V      V              V
-----

Init
    Entry:                -- ZZTAB_STORE
                          -- generates the tooth time table

    B_zztab := false;
    zztaptr := 2;

    B_bm:    B_bm = true
-----

Zztab_store
    -- Model of the tooth time table
    -- Description of the parameters:
    -- Inputs:
    --     R_nbm:    tooth interrupt schedule
    --     R_syn:    synchro schedule
    --     t:        time, based on processor cycle time
    --     C_inisyn: initializing state
    --     B_bm:    condition reference gap found, to
    --              enable the writing of the table
    -- Outputs:
    --     zztab(0:SY_ZSGMT+2): tooth time table,
    --                          length: segment length + 3
    --     B_zztab:    tooth time table valid
    -- Variables:
    --     zztaptr:    Pointer to last entry in the table

    Entry:    zztab(zztaptr) := t;

    Action:   if ( R_nbm ) then
                zztaptr := zztaptr + 1;
                zztab(zztaptr) := t;
            endif;

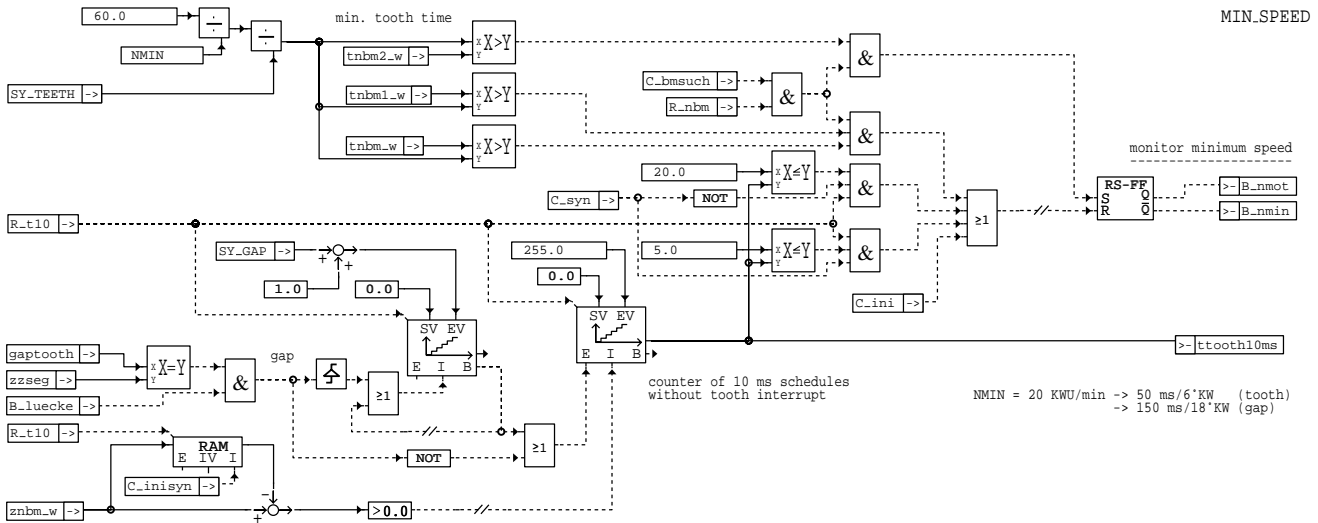
            if ( R_syn ) then
                zztab(1) := zztab(zztaptr);
                zztab(0) := zztab(zztaptr - 1);
                if ( B_zztab = false ) then
                    B_zztab := true;
                endif;
                zztaptr := 1;
            endif;

    C_inisyn: C_inisyn
-----

Local variables:

    Int zztaptr := 2;

```



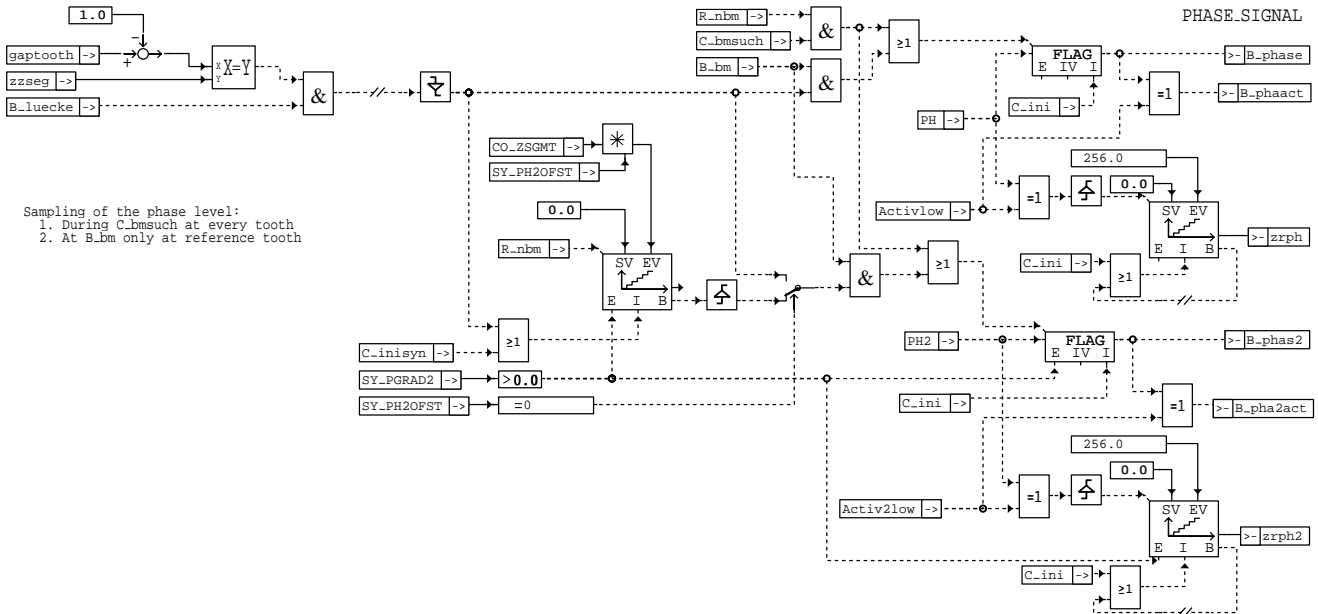
ggdpg-min-speed

### ggdpg-min-speed

Formation of the condition underspeed (B\_nmin) resp. engine speed (B\_nmot).

During the speed search (C\_nsuch) the tooth time  $tnbm2\_w$  is compared in the tooth interrupt to the minimum tooth time NMIN and if necessary B\_nmot is set. Resetting of B\_nmot is performed, if during the speed search phase  $tnbm\_w$  and  $tnbm1\_w$  again become greater than the minimum tooth time or if the counter  $ttooth10ms$  reaches the value 20 (200 ms) resp. during synchronized operation 5 (corresponds to a tooth time of 50 ms). B\_nmin results as a complement of B\_nmot.

The counter  $ttooth10ms$  is incremented in the 10 ms cycle, if no new tooth has occurred, otherwise the counter is reset to 0. During the gap the counter is incremented only every 3rd cycle, so as to make sure that an early underspeed exiting at the gap does not occur.



ggdpg-phase-signal

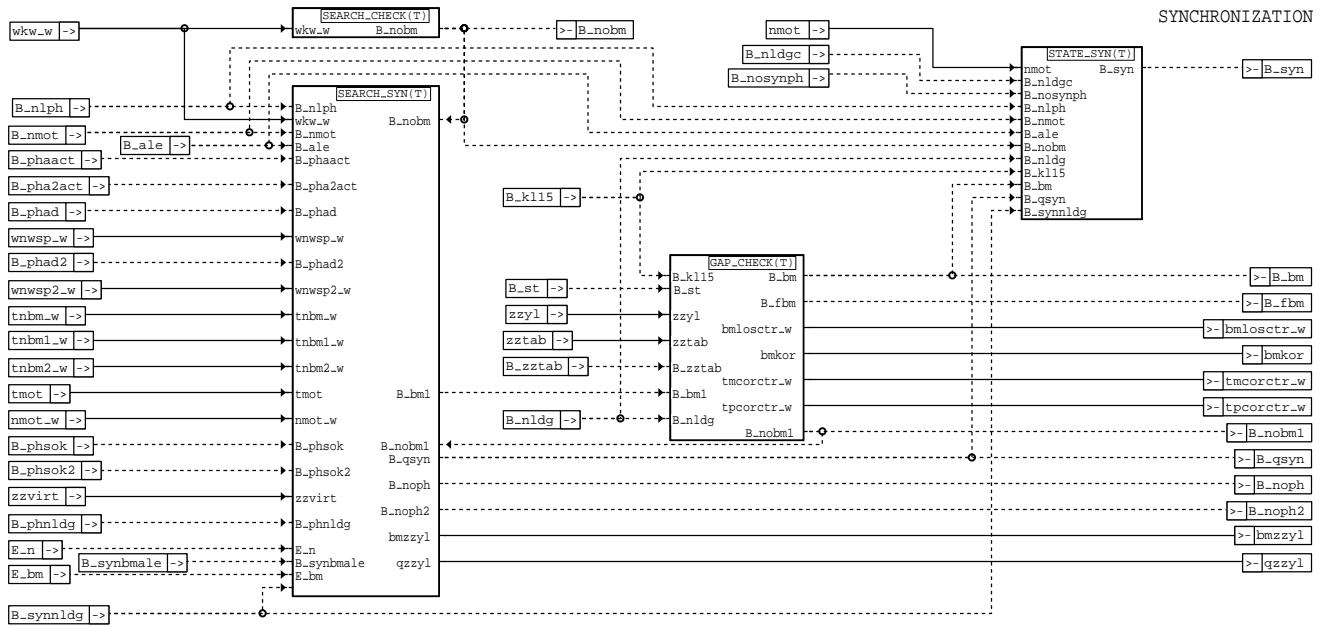
### ggdpg-phase-signal

Scanning of the phase level PH resp. PH2.

The phase levels PH resp. PH2 are scanned in the tooth interrupt during the reference mark search phase (C\_bmsuch). During the subsequent operation synchronized via B\_bm, PH is scanned at the second tooth after the gap ( $zzseg = (gap\ tooth - 1)$  and  $B\_luecke = true$ ). When  $SY\_PH2OFST = 0$ , PH2 is scanned together with PH, otherwise delayed by  $SY\_PH2OFST$  segments to PH. The thus scanned variables B\_phase and B\_phas2 (standardization: B\_phaact, B\_pha2act) can be represented at the VS100.

For the hardware casing the level at the first reference mark of the respective phase sensor is defined by means of the macros Activlow resp. Activ2low. By means of the logic operation  $(PH * EXOR\ Activlow)$  the 'active' phase edge is determined and the number of 'active' phase edges is summed up in  $zrph*$ .

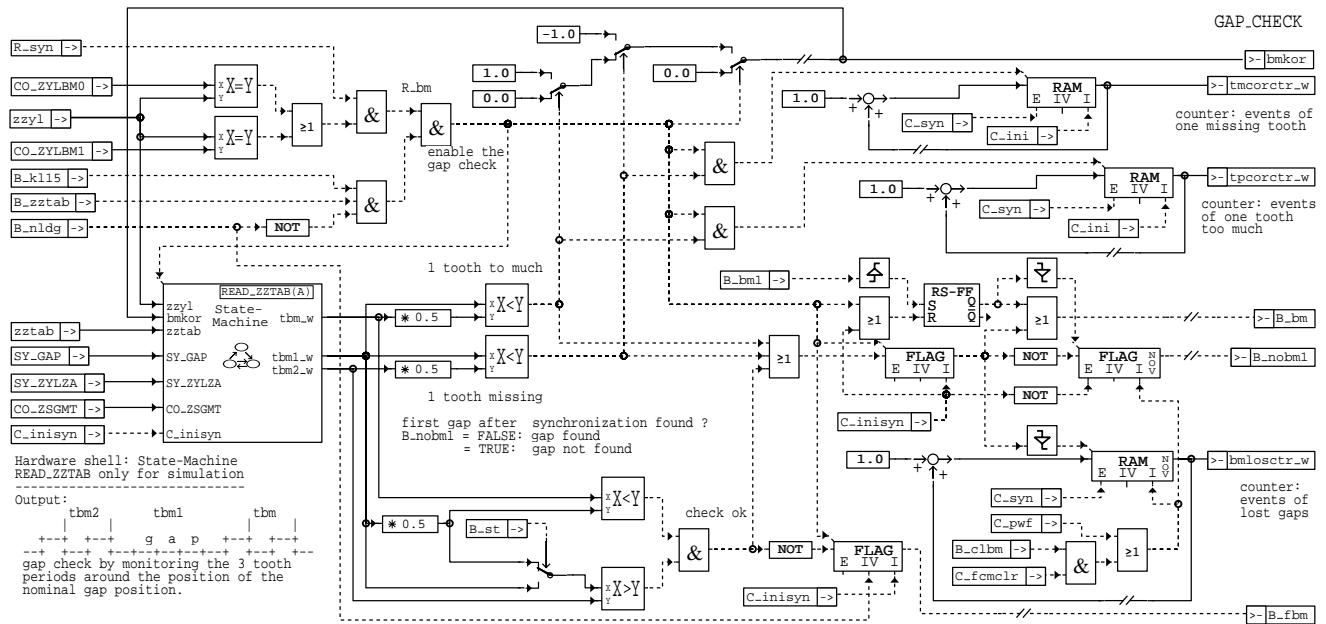




### ggdpg-synchronization

Functional overview synchronization:

SEARCH_SYN	Synchronization search
SEARCH_CHECK	Checking of the synchronization search
GAP_CHECK	Checking of the gap
STATE_SYN	Formation of the condition synchronization



### ggdpg-gap-check

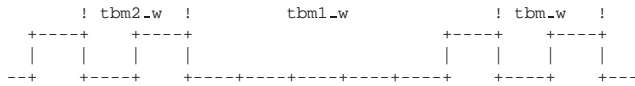
Checking of the gap by means of the tooth time table: Gap check

As soon as the gap was found (B\_bml 0->1) B\_bm is set. Thereafter it is checked during the gap check, whether the gap has been found correctly. The gap check is performed during the synchro after the gap segment (zzyl=CO\_ZYLBMO or zzyl=CO\_ZYL\_BM1) if: Terminal 15 ON, tooth time table valid and not speed sensor limp-home. The state machine READ\_ZZTAB calculates the 3 tooth periods of the teeth in front (tbm2\_w) and after (tbm1\_w) and after (tbm\_w) the expected gap. The partial function READ\_ZZTAB is calculated in the hardware casing and is illustrated here as state machine for the simulation.

By means of these 3 tooth times the following 3 conditions are checked:



1. Gap correct:

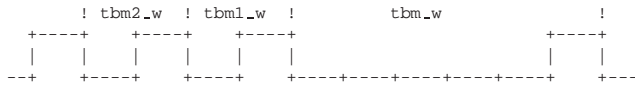


B\_st = TRUE -> Condition: (tbm1\_w > tbm2\_w) and (tbm1\_w \* 0.5 > tbm\_w)  
B\_ST = FALSE -> Condition: (tbm1\_w \* 0.5 > tbm2\_w) and (tbm1\_w \* 0.5 > tbm\_w)

A differentiation for engine start is necessary, because of the very high relative dynamic at this operating point.

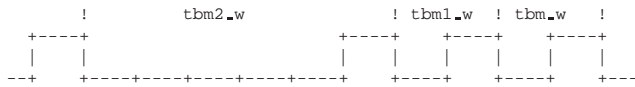
If the gap is at the correct position, B\_bm remains set and the gap check is terminated.

2a. Gap by 1 tooth too late ==> 1 tooth too many:



Condition: tbm1\_w < 0.5 \* tbm\_w

2b. Gap by 1 tooth too early ==> 1 tooth too little:

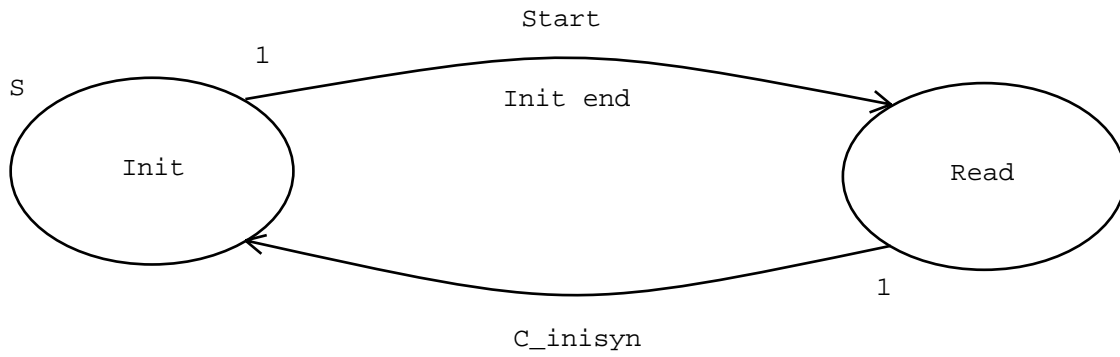


Condition: tbm1\_w < 0.5 \* tbm2\_w

If the gap is incorrect by one tooth, then B\_bm also remains set. Parallel to that B\_fb is set and the tooth counter zzseg for the subsequent segment is corrected by means of bmkor and the corresponding counter tmcrcr\_w resp. tpcrcr\_w is incremented.

If neither of these conditions is fulfilled, then the gap was not found. B\_bm was reset and the counter bmlosctr\_w was incremented. This causes an immediate new synchronization, since B\_syn is also reset via B\_bm.

If the gap is not found during the 1st gap check, then B\_nobml (permanent RAM) is set simultaneously in order to suppress the quick-start during the following start.



ggdpg-read-zztab

ggdpg-read-zztab



State machine to calculate the 3 tooth times around the gap from the tooth time table.

During the gap check the pointer zztaptr is set to the 2nd tooth after the expected gap and the periods are outputted as differences of the last tooth times. On engines with an odd number of cylinders the 2nd gap (zzyl > 0) lies at mid segment, otherwise the gap lies at the end of the segment.

Zustand

Übergangsname		+- Übergangsbedingung	
Aktionen		+- Aktions-Code	
V	V	V	V

Init

```

-- -- READ_ZZTAB
--
-- read out of tooth time table and calculation
-- of the 3 tooth periods around the gap:
--           zztaptr----+
--                   |
--           tbm2         tbm1         tbm
--           |           |           |
-- +---+ +---+   g a p   +---+ +---+
-- --+ +---+ +-----+-----+ +---+ +---+
-- zztaptr is the pointer to the reference
-- tooth in the tooth time table.

Entry:      tbm_w := 65535;
            tbm1_w := 65535;
            tbm2_w := 65535;

Action:     call noOp(0);

Init end:   tbm_w = 65535
    
```

Read

```

Action:     if ( R ) then
            if ( (SY_ZYLZA = 3 or SY_ZYLZA = 5 ) and zzyl > 0 ) then
                zztaptr := CO_ZSGMT / 2 + 1 - SY_GAP;
            else
                zztaptr := CO_ZSGMT + 1 - SY_GAP;
            endif;

            if (SY_ZYLZA = 3 and zzyl = 0) then
                zztaptr := zztaptr + bmkor;
            endif;

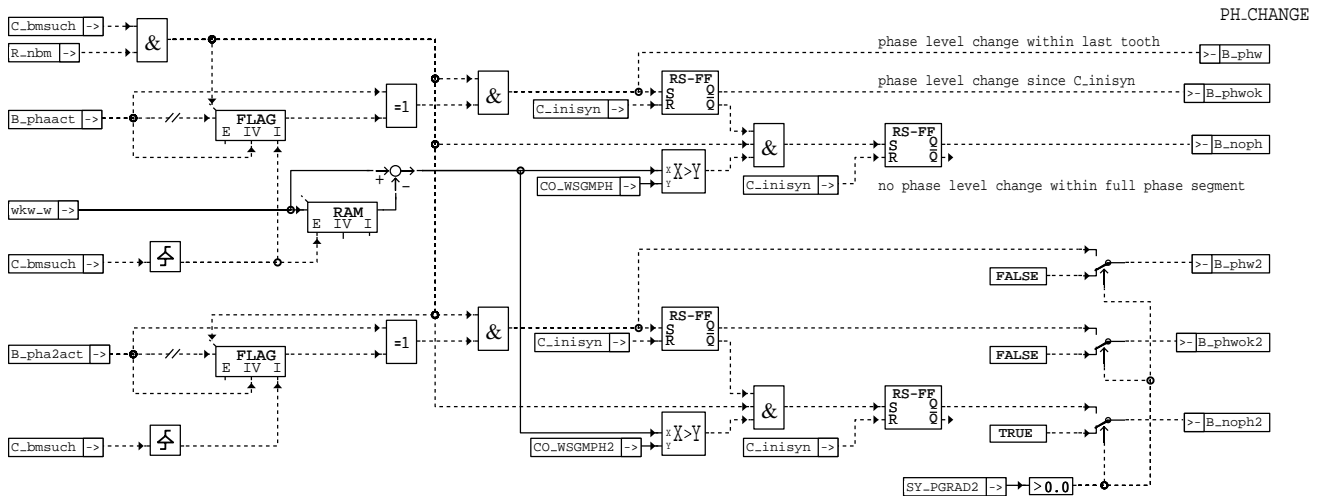
            tbm_w := zztab(zztaptr) - zztab(zztaptr - 1);
            tbm1_w := zztab(zztaptr - 1) - zztab(zztaptr - 2);
            tbm2_w := zztab(zztaptr - 2) - zztab(zztaptr - 3);
        endif;

C_inisyn:   C_inisyn
    
```

Local Variables:

```
Float zztaptr := 0.0;
```

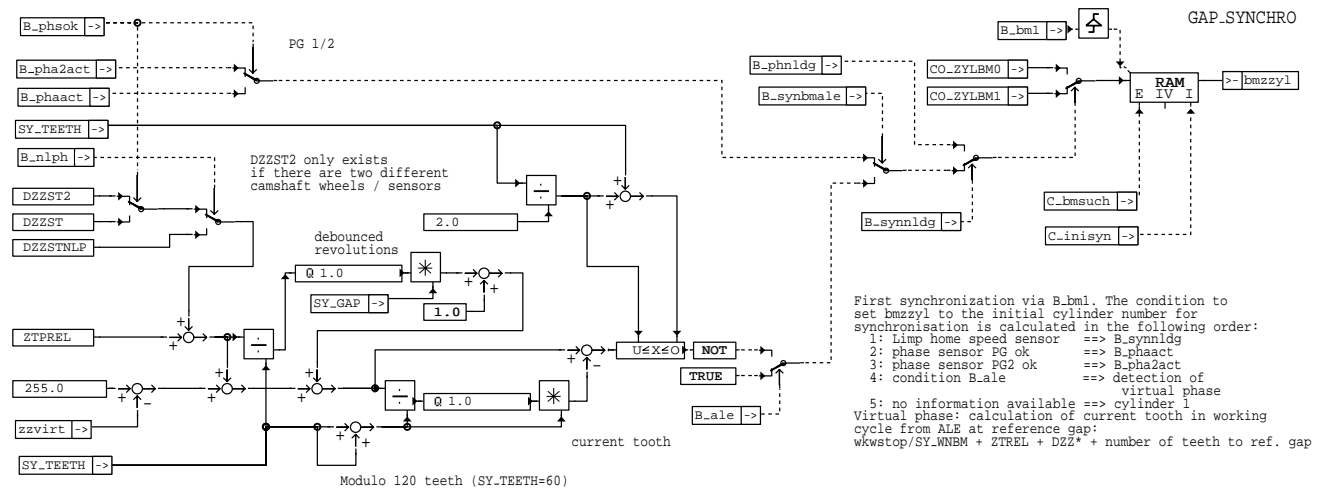




### ggdpg-ph-change

Monitoring of the phase level (B\_phaact resp. B\_pha2act) in the tooth cycle during C\_bmsuch.

Via the temporarily stored phase level it is checked by an exclusive OR whether the respective phase level B\_pha\*act has changed since the last tooth interrupt and if necessary the bit for an occurred phase change (B\_phw\*) is set. During the first phase change the bit B\_phwok\* is additionally set. Thereby it is possible to inquire later whether a phase change has occurred since C\_inisyn. If no edge occurs within the crank angle CO\_WSGMPH\*, then the bit B\_noph\* is set.



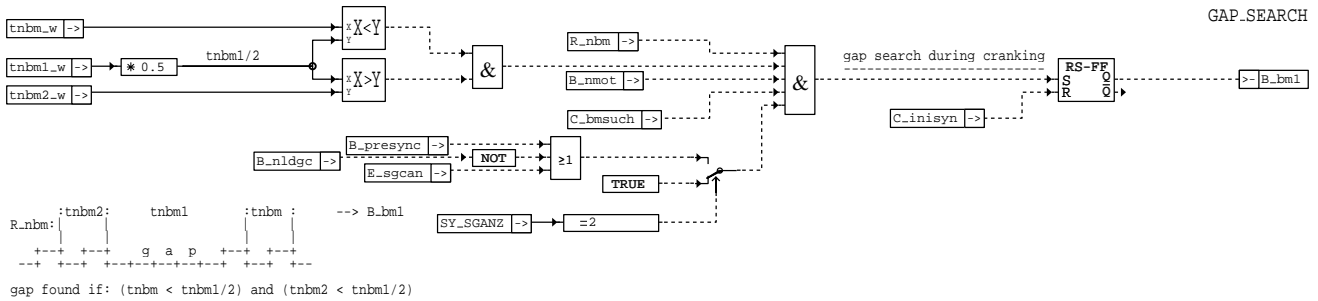
### ggdpg-gap-synchro

Determination of the cylinder number at synchronization via the reference mark.

If the gap is found (B\_bml 0 -> 1), then the initialization value bmzzyl for the cylinder counter is loaded in dependency on the phase information with CO\_ZYLB0 or CO\_ZYLB1. The phase information is calculated with the following priority:

- |  |           |
|--|-----------|
| 1. Synchronization at speed sensor limp-home, phase position is calculated in %NLDG: | B_synnldg |
| 2. Phase sensor PG has been diagnosed as being o.k. (B_phsok), phase from PG:        | B_phaact  |
| 3. Phase sensor PG2 has been diagnosed as being o.k. (B_phsok2), phase from PG2:     | B_pha2act |
| 4. Phase from run-on detection (B_ale) via virtual engine position:                  | zzvirt    |
| 5. No information, synchronization to cylinder 1:                                    | CO_ZYLB0  |

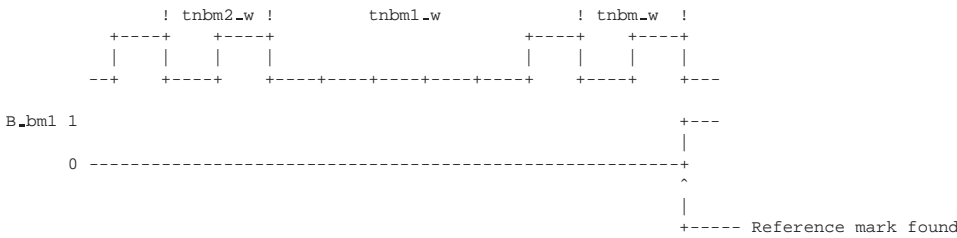
At priority 2 and 3 the normalized phase signal (high-level at B0) is scanned at the detected reference gap. Priority 3 is only calculated if a 2nd phase sensor exists in the system (SY\_PGRAD2 > 0) and if this sensor provides a signal at the reference mark that can be used for the synchronization (SY\_PH2OFST = 0). At priority 4 the angle in the working cycle is calculated at the reference gap via the information of the run-out detection. This only takes effect if there is no camshaft sensor for synchronization available and B\_ale=TRUE.



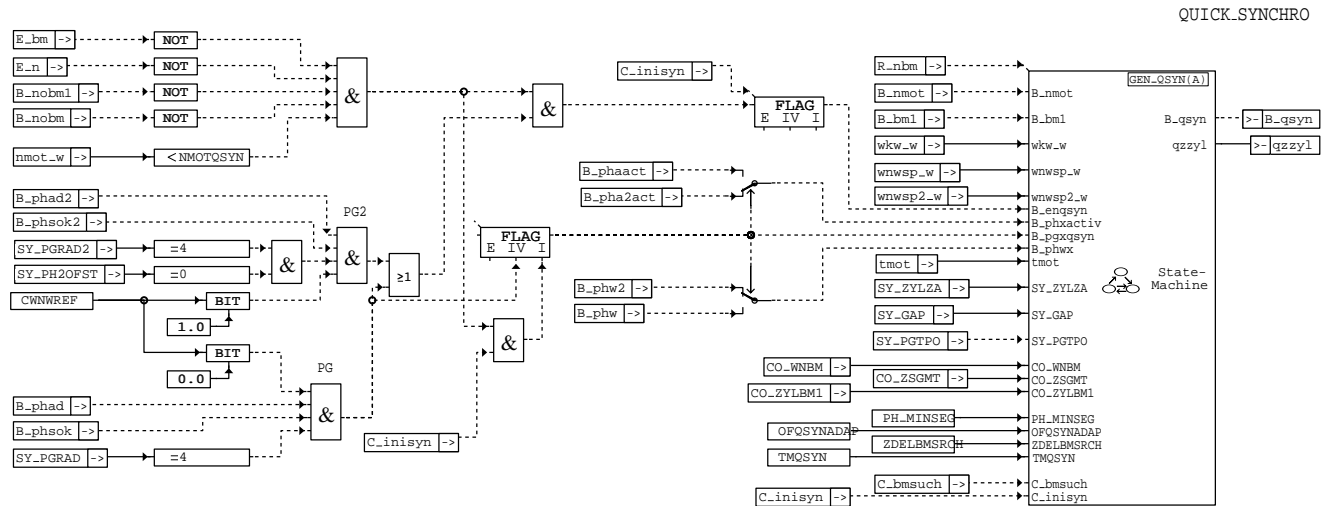
### ggdpg-gap-search

Gap search by an evaluation of the last 3 tooth times.

During the gap search phase (C\_bmsuch) the tooth time tnbm1\_w is halved and compared to the tooth times tnbm\_w, tnbm2\_w at set B\_nmot. If (tnbm\_w < tnbm1\_w / 2) and (tnbm2 < tnbm1 / 2) results, then the gap is detected and B\_bml is set.



At a 2 ECU concept the synchronization via B\_bml is locked if the second ECU is in the crankshaft sensor limp home mode and the synchronization via the limp home function is not yet found. If there is an error E\_sgcan the synchronization is released in general, because it is not to be assumed of a double error.

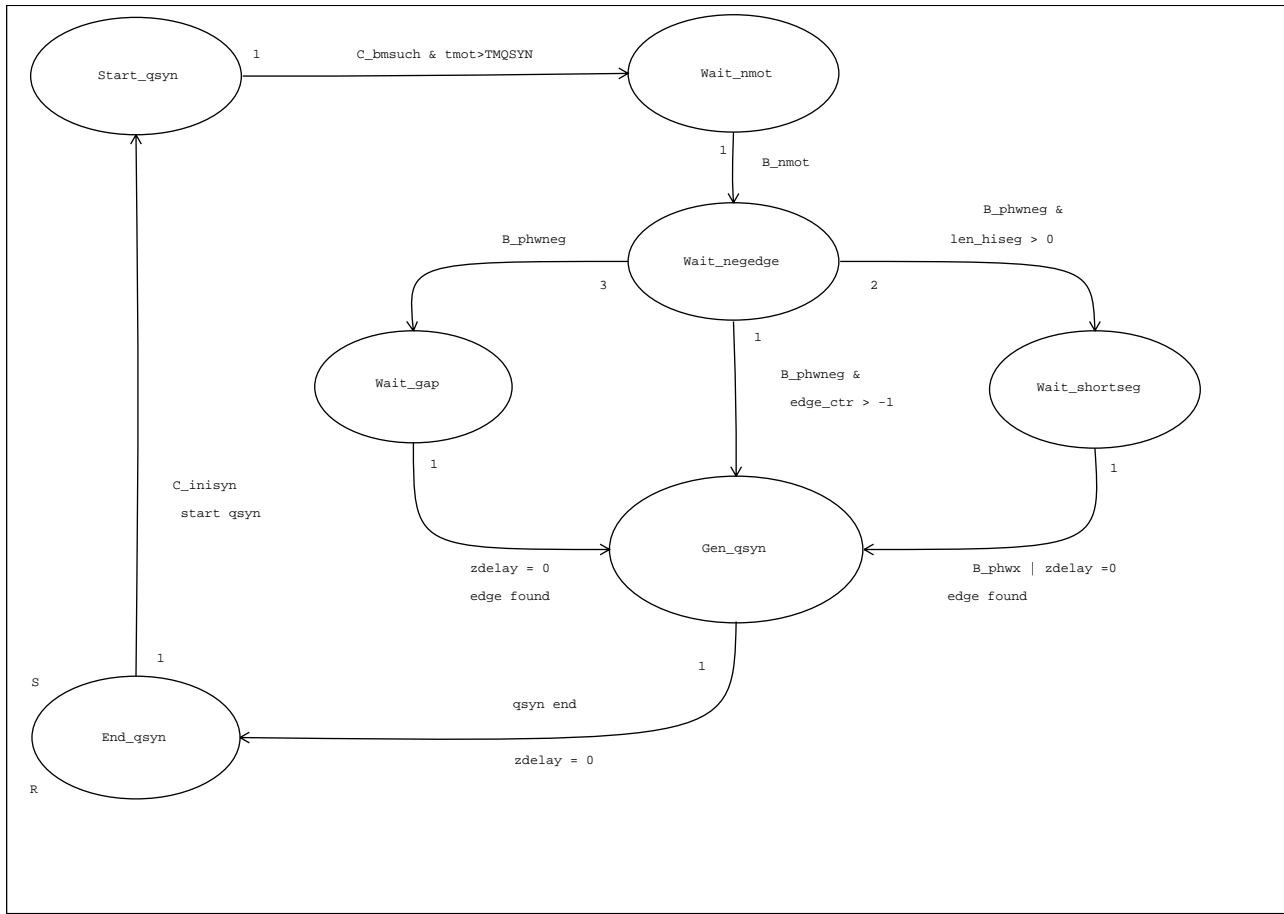


### ggdpg-quick-synchro

Enabling (B\_ensyn) and selection of the phase sensor (B\_pgxsyn) for the quick-start via the phase sensor signal.

Preconditions for the quick-start are: The quick-start sensor wheel (SY\_PGRAD\* = 4), the adaptation of the phase edges must have been performed (B\_phad\* = true), the phase sensor may not be defective (B\_phsok\* = 1, E\_n = 0, B\_bm = 0), the engine temperature must be above the threshold TMQSYN, the speed limit NMOTQSYN must have been undershot and no reference-mark fault may have occurred (B\_nobm = 0, B\_nobm1 = 0). To be able to use the phase sensor PG2 for the quick-start, its phase signal must lie in-phase to the phase sensor PG (SY\_PG2OFST = 0). B\_ensyn is set, if during C\_inisyn these conditions are fulfilled for at least one phase sensor. When enabling the quick-start the phase sensor for the quick-start is selected by means of B\_pgxsyn (B\_pgxsyn = 0 ==> PG2, B\_pgxsyn = 1 ==> PG).

The CodeWord CWNWREF indicates whether the camshaft is in reference position during start.



### ggdpg-gen-qsyn

The state machine GEN\_QSYN tries to calculate the engine position from the phase signal and to trigger a synchronization via B\_qsyn. Exactly at the beginning of a synchro B\_qsyn must be set, in which qzyl contains the cylinder number of this segment.

Due to the initialization C\_inisyn the state changes to Start\_qsyn, provided B\_engsyn is enabled and remains there until the reference mark search phase (C\_bmsuch) and the engine temperature is above a threshold (tmot > TMQSYN). During a re-synchronization (C\_inisyn) the Bit B\_qsyn is reset to FALSE.

In Wait\_nmot information on possible phase edges are collected, but not yet evaluated since B\_nmot is not yet given. With B\_nmot the state changes to Wait\_negedge. Exit condition from this state is a found negative phase edge in the phase signal. As long as the exit condition is not fulfilled, the phase signal is evaluated analogous as in Wait\_nmot. In dependency on the available information a jump to Wait\_gap, to Wait\_shortseg or directly to Gen\_qsyn is performed.

In Wait\_gap a certain number of teeth is waited for until a gap should occur, provided that the engine is after the 2nd or 4th phase edge. If the reference mark does not occur then a distinction can be made between the 1st and 3rd phase edge and thereby the engine position can be determined.

In Wait\_shortseg the length of the phase segment before the falling edge is known. Now it is waited whether a rising edge will occur after the falling edge within the crank angle PH\_MINSEG. With this additional information it is known, which edge it is.

When jumping into Gen\_qsyn, the last negative edge and the angle difference since this edge is known. Now the number of teeth until the next segment and the cylinder number are calculated. Once this amount of teeth has passed B\_qsyn is set and the quick-start is terminated.

An early termination and jump to the state End\_qsyn is achieved as soon as the gap was found (reset-condition B\_bml).

Zustand	Übergangsname	+ - Übergangsbedingung	Aktionen	+ - Aktions-Code
End_qsyn	Reset-Bedingung:	B_bml or (B_engsyn = false)		

-- Dies ist der Reset-Zustand, er wird aus allen Zuständen angesprungen, wenn die Reset-Bedingung erfüllt ist.  
-- Start and Resetstate.  
In synchronized condition or if the quick start function is disabled (B\_engsyn = false) the State-Machine remains in this state without any action. The function is not calculated.





```

Entry:                                -- End.qsyn: Entry
stateqsyn := 6;

Action: call noOp(0);                 -- No operation, the quick start function is
                                        -- not enabled or already finished

C_inisyn: C_inisyn                     -- Exit to Start.qsyn.
    
```

```

-----
Start.qsyn                             -- The state is called during C_inisyn). The system
                                        -- remains in this state untill C_bmsuch to start the
                                        -- quick synchronization via the phase signal.

Entry:                                -- Start.qsyn: Entry
stateqsyn := 0;

Action: call noOp(0);                 -- No operation, waiting for C_bmsuch

C_bmsuch & tmot>TMQSYN:
    C_bmsuch and (tmot > TMQSYN)      -- Tooth debouncing finished and tmot greater threshold
                                        -- ==> exit to Wait_nmot
    
```

```

-----
Wait_nmot                               -- The system is in C_bmsuch condition, but B_nmot is
                                        -- not yet set. In this state the phase edges are
                                        -- monitored, a flag for the phase change is set and
                                        -- the corresponding wkw_w is stored.
    
```

```

Entry:                                -- Wait_nmot: Entry
                                        -- Initialization

stateqsyn := 1;
B_phwneg := false;                   -- reset flag for falling edge
B_phwpos := false;                   -- reset flag for rising edge
edge_ctr := -1;                       -- reset edge index
len_hiseg := 0;                       -- reset indicator for length of high segment
len_loseg := 0;                       -- reset indicator for length of low segment
if ( B_pgxqsyn ) then                  -- select adaptation value from correct PG
    tmp := wnwspx_w(0);                -- PG
else
    tmp := wnwspx2_w(0);               -- PG2
endif;
tmp := (tmp - OFQSYNADAP) / CO_WNBM;  -- calculation from first phase edge to the
wnwspx_w(0) := truncate(tmp);          -- tooth before wnwspx_w(0) - OFQSYNADAP
if ( wnwspx_w(0) < tmp ) then          -- correct wnwspx_w(0) to tooth after wnwspx_w(0)
    wnwspx_w(0) := wnwspx_w(0) + 1;   -- tooth after wnwspx_w(0)
endif;
wnwspx_w(0) := wnwspx_w(0) * CO_WNBM; -- Calculate from tooth to crank angle:
                                        -- Adapted phase edge, rounded to the next tooth

if ( B_pgxqsyn ) then                  -- select adaptation value from correct PG
    tmp := wnwspx_w(1);                -- PG
else
    tmp := wnwspx2_w(1);               -- PG2
endif;
tmp := (tmp - OFQSYNADAP) / CO_WNBM;  -- calculation from second phase edge to the
wnwspx_w(1) := truncate(tmp);          -- tooth before wnwspx_w(1) - OFQSYNADAP
if ( wnwspx_w(1) < tmp ) then          -- correct wnwspx_w(1) to tooth after wnwspx_w(1)
    wnwspx_w(1) := wnwspx_w(1) + 1;   -- tooth after wnwspx_w(1)
endif;
wnwspx_w(1) := wnwspx_w(1) * CO_WNBM; -- Calculate from tooth to crank angle:
                                        -- Adapted phase edge, rounded to the next tooth

if ( B_pgxqsyn ) then                  -- select adaptation value from correct PG
    tmp := wnwspx_w(2);                -- PG
else
    tmp := wnwspx2_w(2);               -- PG2
endif;
tmp := (tmp - OFQSYNADAP) / CO_WNBM;  -- calculation from third phase edge to the
wnwspx_w(2) := truncate(tmp);          -- tooth before wnwspx_w(2) - OFQSYNADAP
if ( wnwspx_w(2) < tmp ) then          -- correct wnwspx_w(2) to tooth after wnwspx_w(2)
    wnwspx_w(2) := wnwspx_w(2) + 1;   -- tooth after wnwspx_w(2)
endif;
wnwspx_w(2) := wnwspx_w(2) * CO_WNBM; -- Calculate from tooth to crank angle:
                                        -- Adapted phase edge, rounded to the next tooth

if ( B_pgxqsyn ) then                  -- select adaptation value from correct PG
    tmp := wnwspx_w(3);                -- PG
else
    tmp := wnwspx2_w(3);               -- PG2
endif;
tmp := (tmp - OFQSYNADAP) / CO_WNBM;  -- calculation from 4. phase edge to the
wnwspx_w(3) := truncate(tmp);          -- tooth before wnwspx_w(3) - OFQSYNADAP
if ( wnwspx_w(3) < tmp ) then          -- correct wnwspx_w(3) to tooth after wnwspx_w(3)
    wnwspx_w(3) := wnwspx_w(3) + 1;   -- tooth after wnwspx_w(3)
endif;
    
```



```

endif;
wnwspw_w(3) := wnwspw_w(3) * CO_WNBW;

Action:
if ( R_nbm and B_phwx ) then
  if ( B_phxactiv ) then
    wkwneg_w := wkw_w;
    B_phwneg := true;

    if ( B_phwpos ) then
      if ( wkwneg_w - wkwpos_w > 90 ) then
        len_hiseg := 2;
      else
        len_hiseg := 1;
      endif;
    else
      if ((wkwneg_w > PH_MINSEG) and SY_PGTP0) then
        len_hiseg := 2;
      endif;
    endif;
  else
    wkwpos_w := wkw_w;
    B_phwpos := true;

    if ( B_phwneg ) then
      if ( wkwpos_w - wkwneg_w > 90 ) then
        len_loseg := 2;
      else
        len_loseg := 1;
      endif;
    else
      if ((wkwpos_w > PH_MINSEG) and SY_PGTP0) then
        len_loseg := 2;
      endif;
    endif;
  endif;
endif;

B_nmot:      B_nmot
-- B_nmot is now set, exit to Wait_negedge.

```

```

-----
Wait_negedge

Entry:
stategsyn := 2;
wkwstart_w := wkw_w;

if ( B_phwneg and B_phwpos and (wkwpos_w > wkwneg_w) ) then
  if ( len_hiseg > 0 ) then
    if ( len_loseg = 2 ) then
      if ( len_hiseg = 2 ) then
        edge_ctr := 2;
      else
        edge_ctr := 3;
      endif;
    else
      if ( len_hiseg = 2 ) then
        edge_ctr := 1;
      else
        edge_ctr := 0;
      endif;
    endif;
  else
    B_phwneg := false;
  endif;
endif;

Action:
if ( R_nbm and B_phwx ) then
  if ( B_phxactiv ) then
    wkwneg_w := wkw_w;
    B_phwneg := true;

```



```

if ( B_phwpos ) then
  if ( wkwneg_w - wkwpos_w > 90 ) then
    len_hiseg := 2;
  else
    len_hiseg := 1;
  endif;
else
  if ((wkwneg_w > PH_MINSEG) and SY_PGTP0 ) then
    len_hiseg := 2;
  endif;
endif;

if ( len_hiseg = 2 ) then
  if ( wnwspx_w(2) - (wkwneg_w - wkwstart_w) < 360 - (3 + SY_GAP) * CO_WNBM ) then
    edge_ctr := 1;
  endif;
elseif ( len_hiseg = 1 ) then
  if ( wnwspx_w(0) - (wkwneg_w - wkwstart_w) < - (3 + SY_GAP) * CO_WNBM ) then
    edge_ctr := 3;
  endif;
endif;

else
  wkwpos_w := wkw_w;
  B_phwpos := true;

  if (( wkwpos_w > PH_MINSEG) and SY_PGTP0 ) then
    len_loseg := 2;
  endif;
endif;
endif;

edge_ctr > -1: B_phwneg and edge_ctr > -1
len_hiseg > 0: B_phwneg and len_hiseg > 0
B_phwneg: B_phwneg

```

-----  
Wait\_shortseg

Entry:

```

stategsyn := 4;

if ( len_hiseg = 2 ) then
  edge_ctr := 2;
else
  edge_ctr := 3;
endif;

znbm_act := (wnwspx_w(edge_ctr) + PH_MINSEG) / CO_WNBM;

zdelay := PH_MINSEG / CO_WNBM;
if ( modulo(znbm_act, CO_ZSGMT) > 0 ) then
  zdelay := zdelay + CO_ZSGMT - modulo(znbm_act, CO_ZSGMT);
endif;

if ( zdelay > 90 / CO_WNBM ) then
  zdelay := 90 / CO_WNBM;
endif;

if ( zdelay > (wkw_w - wkwneg_w) / CO_WNBM ) then
  zdelay := zdelay - (wkw_w - wkwneg_w) / CO_WNBM;
else
  zdelay := 0;
endif;

```



```

Action:
    if ( R.nbm ) then
        zdelay := zdelay - 1;
    endif;

Exit:
    if ( B.phxactiv = false ) then
        if ( len_hiseq = 2 ) then
            edge_ctr := 1;
        else
            edge_ctr := 0;
        endif;
    endif;

B.phwx | zdelay = 0:
    (B.phwx and (wkw_w <> wkwneg_w)) or (zdelay = 0)

```

-- Wait\_shortseg: Action  
-- waiting for the rising edge  
-- decrement zdelay

-- Wait\_shortseg: Exit  
-- Check current phase level:  
-- If phase is high ==> phase change  
-- edge\_ctr from entry code was wrong: reset  
-- if long segment before falling edge  
-- ==> long high, short low ==> edge 1  
-- otherwise  
-- ==> short high, short low ==> edge 0  
-- end of if loop segment length

-- The crank position is known (edge\_ctr is set to the index of the last falling edge). Exit to Gen\_ksyn.  
The exit condition is checked before the action code.  
B.phwx is only set for one tooth interrupt.

---

```

Wait_gap

Entry:
    stateqsyn := 3;

Action:
    if ( R.nbm ) then
        zdelay := zdelay - 1;
    endif;

Exit:
    if ( B.phxactiv ) then
        edge_ctr := 2;
    else
        edge_ctr := 0;
    endif;

zdelay = 0:

```

-- The last edge was a falling one, more information is not available.  
In the entry code the system calculates zdelay as the maximum between the number of teeth from the adapted phase edge 1 to the reference tooth after the first gap and the number of teeth from the adapted phase edge 3 to the reference tooth after the second reference gap.  
In the action code, the system waits for 'zdelay' number of teeth. If the reference gap appears after during this 'delay', the quick start function is finished aborted by the reset condition B.bml.  
Otherwise the current position is known by checking the phase level. The number of delayed teeth is in all cases longer than a short segment (between edge(1) and the 1. reference gap is a phase change).  
In case of B.phactiv the phase level did not change, which means the last segment wasn't a short one, so the system was at the third edge (edge\_ctr = 2), otherwise the system was at the first edge (edge\_ctr = 0).

-- Wait\_gap: Entry  
-- calculate max = maximum number of teeth between:  
-- wnwspx\_w(1) and the 1. reference tooth  
-- and wnwspx\_w(3) and the 2. reference tooth  
zdelay := (max(360 - wnwspx\_w(1), 720 - wnwspx\_w(3)) - (wkw\_w - wkwneg\_w)) / CO\_WNBm - SY\_GAP + ZDELMSRCH;

-- Wait\_gap: Action  
-- Waiting for 'zdelay' teeth  
-- decrement zdelay

-- Wait\_gap: Exit  
-- check current phase level:  
-- phase is low ==> no phase change  
-- ==> edge 2  
-- otherwise phase change  
-- ==> edge 0  
-- end checking phase level  
In this transition the gap did not appear. So the crank position is known (edge\_ctr is set to the index of the last falling edge). Exit to Gen\_ksyn.

---

```

Gen_ksyn

```

-- The system had a falling edge at wkwneg\_w. The index of the edge is stored in edge\_ctr. So the current engine position is calculated from the tooth after (wnwspx[edge\_ctr] + (wkw - wkwneg\_w))/SY\_WNBm.  
In the entry-code the current engine position (znbm\_act), the cylinder number (qzzy1) und the number of teeth (zdelay) to the next synchro schedule are calculated.  
If qzzy1 is less than SY\_ZYLZA, zdelay is checked against 0. In this case the engine is exactly at the synchro position and B\_ksyn is set immediately, otherwise 'zdelay' number of teeth are waited in the action-code, until B\_ksyn is set. If qzzy1 is equal to SY\_ZYLZA, the engine is already in the last synchro before the reference gap 0. In this case it does not make sense to wait for B\_ksyn.



```

Entry:
stateqsyn := 5;
znbm_act := (wnwsp_x_w(edge_ctr) + wkw_w - wkwneg_w) / CO_WNBm;
if ( znbm_act >= 720 / CO_WNBm ) then
  znbm_act := znbm_act - 720 / CO_WNBm;
endif;
qzzyl := truncate(znbm_act / CO_ZSGMT);
zdelay := CO_ZSGMT - modulo(znbm_act, CO_ZSGMT);
if ( zdelay = CO_ZSGMT ) then
  zdelay := 0;
else
  qzzyl := qzzyl + 1;
endif;
if ( qzzyl < SY_ZYLZA ) then
  if ( zdelay = 0 ) then
    B_qsyn := true;
  endif;
else
  zdelay := 0;
endif;

Action:
if ( R_nbm ) then
  zdelay := zdelay - 1;
  if ( zdelay = 0 ) then
    B_qsyn := true;
  endif;
endif;

zdelay = 0:
zdelay = 0;

-- Wait_qsyn: Entry
-- current engine position / CO_WNBm;
-- overflow correction
-- current cylinder number
-- teeth to next synchro
-- current tooth is a synchro start tooth
-- ==> no delay, qzzyl is correct
-- otherwise
-- increase cylinder counter qzzyl
-- check next synchro
-- if synchro ok.
-- if zdelay already zero:
-- ==> start immediately
-- end if zdelay zero
-- else no valid synchro found,
-- quick start finished immediatly
-- end checking next synchro

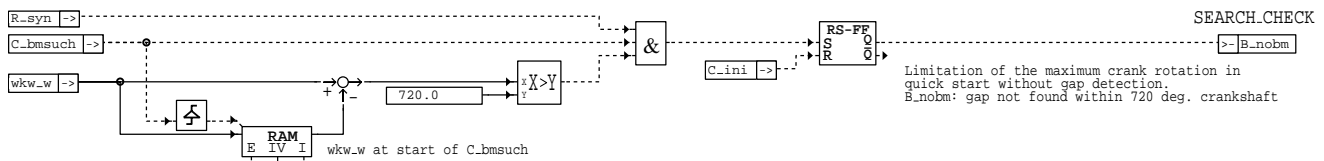
-- Wait_qsyn: Action
-- wait zdelay teeth
-- decrement zdelay
-- if delay end:
-- ==> start synchro

-- Qsyn is finished. Exit to End_qsyn.
  
```

Lokale Variablen:

```

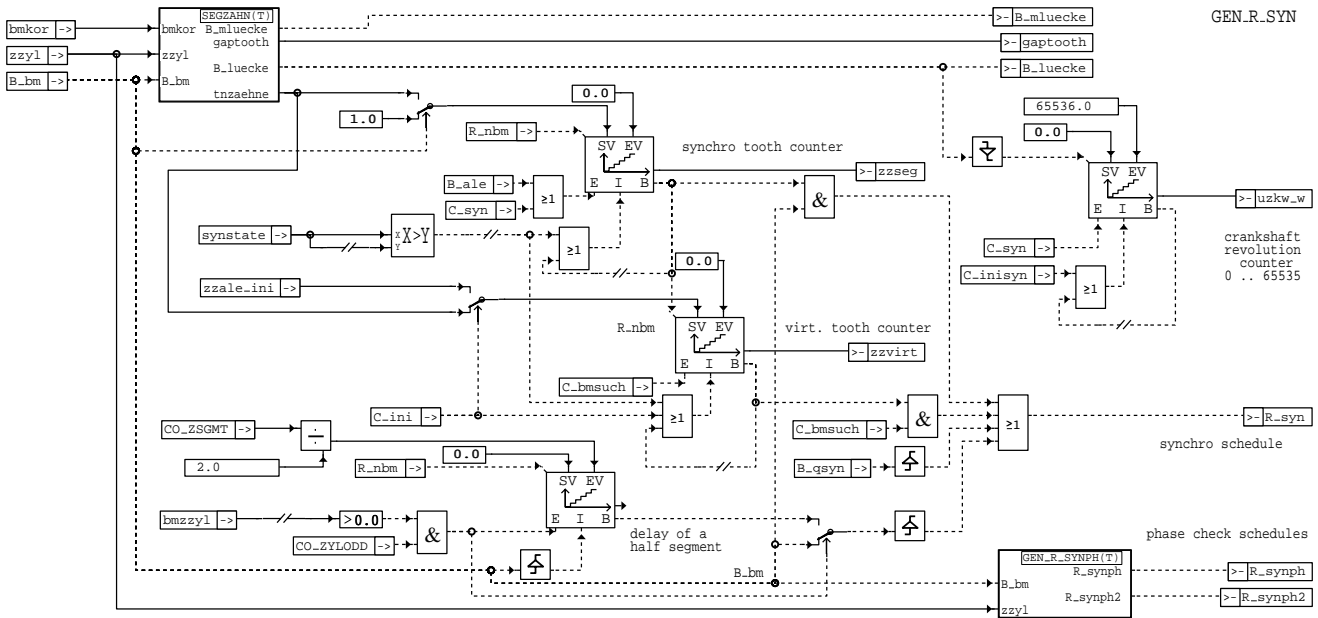
Bool B_phwneg      := false;
Bool B_phwpos      := false;
Float edge_ctr     := -1.0;
Float wkwneg_w     := 0.0;
Float wkwpos_w     := 0.0;
Float wkwstart_w  := 0.0;
Float zdelay       := 0.0;
Float znbm_act     := 0.0;
Float len_loseg    := 0.0;
Float len_hiseg    := 0.0;
Float wnwsp_x_w(4) := 0.0;
Float stateqsyn    := 0.0;
Float tmp          := 0.0;
  
```



ggdpg-search-check

If the system is already in the synchronized state during the reference mark search (due to run-out detection or quick-start sensor wheel) then it is checked whether the reference mark is found within 720 degrees crankshaft (CS) and if necessary B\_nobm is set and thereby the synchronization is aborted.

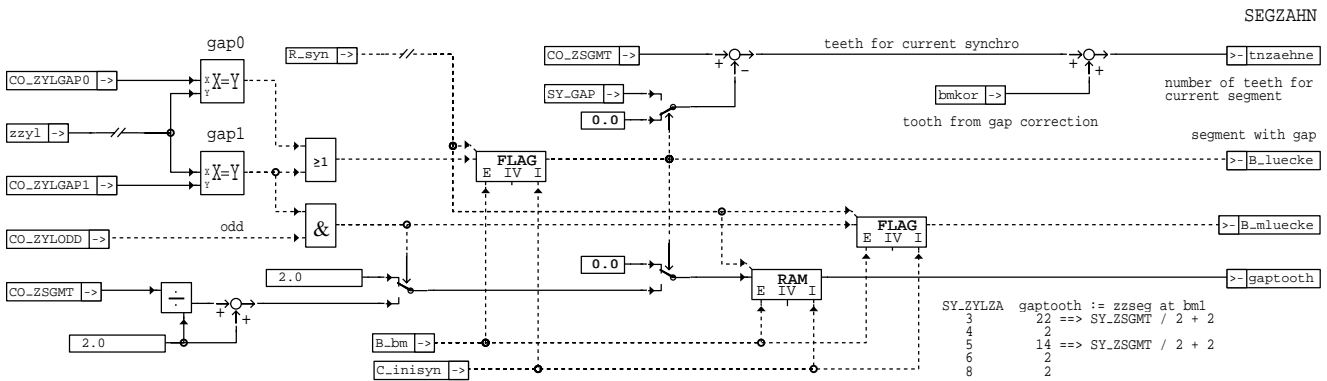




### ggdpg-gen-r-syn

Partial function to generate the synchro interrupt R\_syn.

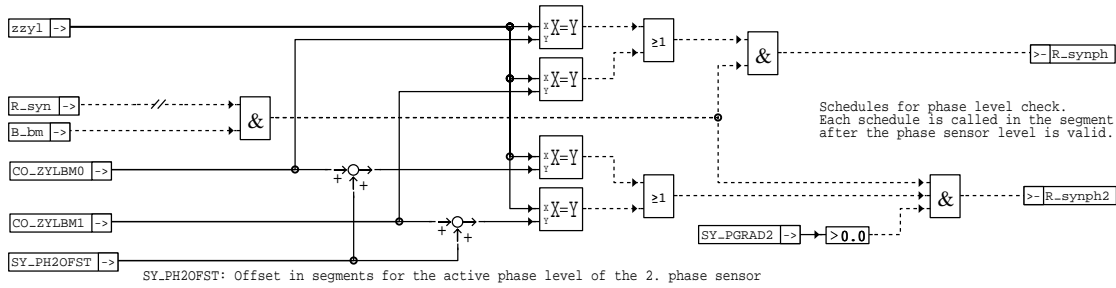
The counter zzvirt is set to zzale\_ini in C\_ini with valid run-out detection (B\_ale). This counter is enabled in C\_bmsuch and decremented in the tooth interrupt. If zzseg = 0, then a synchro interrupt R\_syn is triggered and zzseg is set to the number of teeth per segment (tnzaehne). If a re-synchronization (B\_qlsyn or B\_bm) occurs, then the counter is increased by changing the synchronizing state (synstate). R\_syn is also triggered when B\_qlsyn and B\_bm are set for the first time. On engines with an odd amount of cylinders R\_syn is triggered, at B\_bm and 2nd reference mark (bmzzyl > 0) delayed by half a segment to the reference mark. When the reference mark occurs the state C\_bmsuch is terminated. Now the counter zzseg becomes active, which counts down tnzaehne respectively and which triggers an R\_syn at 0. The counter uzkw\_w is incremented in each synchro after the gap (every crankshaft revolution).



### ggdpg-segzahn

SEGZAHN provides the following information for the respective current segment:

- tnzaehne: Number of teeth of the segment to initialize the counters zzvirt resp. zzseg. The tooth to be corrected from the gap check is taken into account in this variable.
- B\_luecke: The reference mark lies within the current segment
- B\_mluecke: The middle reference mark lies within the current segment (only with odd cylinder numbers)
- gaptooth: Tooth count of the tooth after the gap



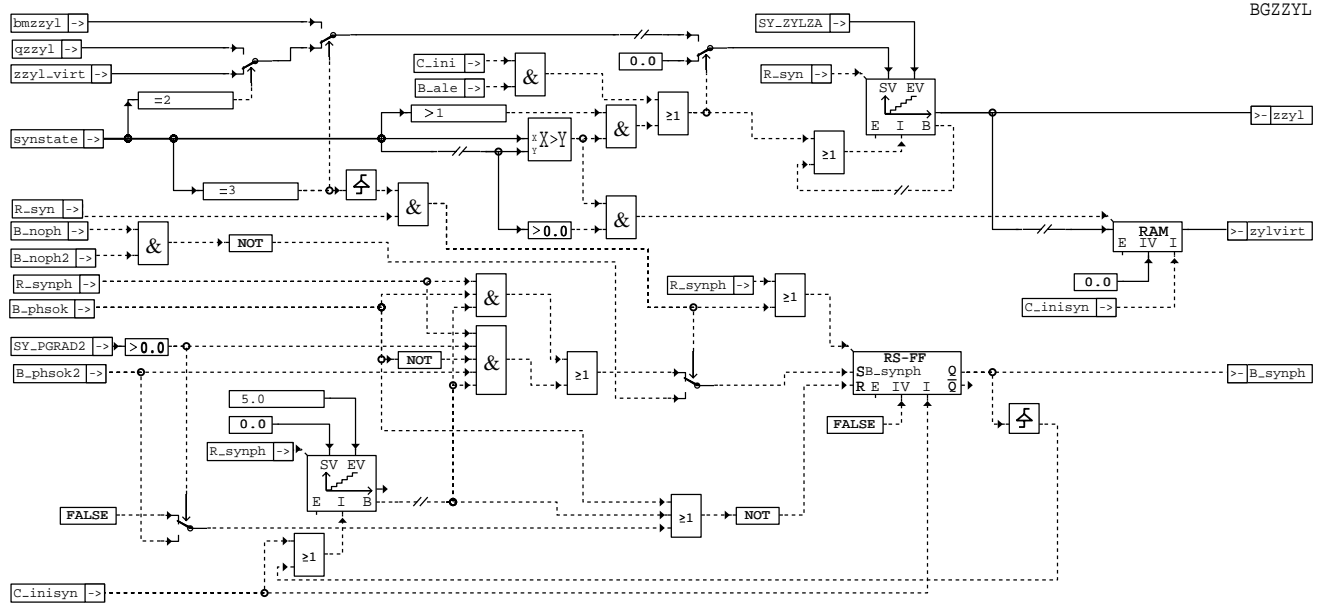
GEN\_R\_SYNPH

ggdpg-gen-r-synph

### ggdpg-gen-r-synph

Generation of the cycle for the phase inquiry.

In the cycle R\_syn the cylinder counter is checked on whether the phase inquiry of the respective phase sensors can be performed in this synchro and if necessary a R\_synph\* is triggered.



BGZZYL

ggdpg-bgzzy1

### ggdpg-bgzzy1

Management of the cylinder counter zzy1.

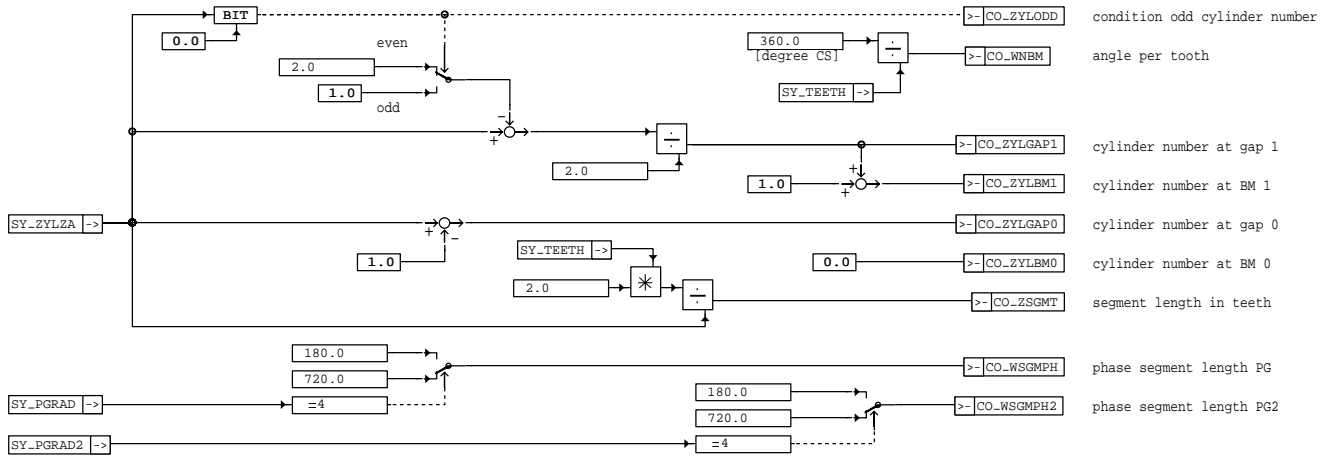
At new synchronization resp. re-synchronization after quick-start (ALE → QSYN, ALE → BM or QSYN → BM) the cylinder counter is initialized from zzy1.virt, qzzy1 or bmzzy1. At each synchro cycle R\_syn, zzy1 is incremented until zzy1 = SY\_ZYLZA - 1. When zzy1 = SY\_ZYLZA, zzy1 is immediately reset to 0. When a re-synchronization occurs the value of zzy1 is re-stored into zylvirt prior to the initialization.

The correct synchronization is indicated in B\_synph. At the first synchro B\_synph is set provided no fault has been diagnosed. During the next 5 cycles for the phase inquiry R\_synph the synchronization is checked. If still no fault occurs till then, B\_synph2 remains set and the checking is terminated.





CONSTANTS



SY\_PGRAD/2: 0 sensor not available  
1 standard phase sensor wheel  
4 quick start sensor wheel

SY\_ZYLZA Segments with gap:  
1. gap, 2. gap ==>  
3 1, 2 ==> (SY\_ZYLZA - 1) / 2, SY\_ZYLZA - 1, SY\_ZYLGA1 + 1, 0  
4 1, 3 ==> (SY\_ZYLZA - 2) / 2, SY\_ZYLZA - 1, SY\_ZYLGA1 + 1, 0  
5 2, 4 ==> (SY\_ZYLZA - 1) / 2, SY\_ZYLZA - 1, SY\_ZYLGA1 + 1, 0  
6 2, 5 ==> (SY\_ZYLZA - 2) / 2, SY\_ZYLZA - 1, SY\_ZYLGA1 + 1, 0  
8 3, 7 ==> (SY\_ZYLZA - 2) / 2, SY\_ZYLZA - 1, SY\_ZYLGA1 + 1, 0

ggdpg-constants

**ggdpg-constants**

Generation of the constants important for %GGDPG, which are derived from system constants.

**ABK GGDPG 14.30 Abbreviations**

Abbreviation Meaning

- DG crankshaft position sensor
- PG camshaft position sensor
- TPO TRUE POWER ON (camshaft position sensor)
- \* Wildcard to distinguish between phase sensor 1 and 2, e. g. PG\* = PG1 or PG2
- KW Crankshaft
- NW Camshaft

Label	Source	Type	Quantization	Description
Activlow	System	Macro		Level definition: Phase level PG low at first reference mark BM0
Activ2low	System	Macro		Level definition: Phase level PG2 low at first reference mark BM0
CO_WNBGM	Constants	const	1° CA	Angle per tooth (6° CA at a 60-2 pulse-generator wheel)
CO_ZSGMT	Constants	const	1	Number of teeth per segment (without gap)
CO_WSGMPH	Constants	const	6° CA	Distance in degrees CA between the falling edges in the phase sensor signal
CO_WSGMPH2	Constants	const	6° CA	Distance in degrees CA between the falling edges in the 2. phase sensor signal
CO_ZYLODD	Constants	Flag	0/1	Flag engine with odd number of cylinders
CO_ZYLGA0	Constants	const	1	Cylinder number at gap 0
CO_ZYLB0	Constants	const	1	Cylinder number at reference mark 0
CO_ZYLGA1	Constants	const	1	Cylinder number at gap 1
CO_ZYLB1	Constants	const	1	Cylinder number at reference mark 1

CWNWREF -> characteristic of the camshaft at start  
 Bit 0: =1 camshaft of PG1 secure in reference position at engine start  
 Bit 2: =1 camshaft of PG2 secure in reference position at engine start  
 Bit 2 - 7 not in use

Parameter	Source-X	Source-Y	Type	Description
CWNWREF			FW	characteristics of the camshaft at engine start
DZZST			FW	number of teeth when tooth suppression during start
DZZST2			FW	Number of teeth for tooth debouncing with second phase sensor
DZZSTNLP			FW	Number of teeth for tooth debouncing at camshaft limp home mode
NMIN			FW	minimum engine speed
NMOTQSYN			FW	engine speed threshold to enable quick start via phase sensor signal
NSYN2SG			FW	Engine speed threshold for new synchronization at 2 ECU-concept with NLDG
OFQSYNADAP			FW	offset between adapted phase edge and phase edge in start
PH_MINSEG			FW	length of short segment at the quick start phase sensor signal
TMQSYN			FW	engine temperature threshold to enable quick start via phase sensor signal
TPREL			FW	tooth debouncing time during initialisation
ZDELBMSRCH			FW	additional tooth offset to wait for the next gap in quick start
ZTPREL			FW	number of teeth during start recognition

Variable	Source	Type	Description
BMLOSCTR_W	GGDPG	AUS	counter (word) re-synchronizations due to a loss of the reference gap
BMZZYL	GGDPG	LOK	initial value for cylinder counter after first reference gap



Variable	Source	Type	Description
B_ALE	ALE	EIN	condition engine stop position detected
B_BM	GGDPG	AUS	condition reference mark detected
B_CLBM		EIN	condition clear fault path reference mark sensor
B_ENQSYN	GGDPG	LOK	condition enable phase signal quick start
B_FBM	GGDPG	AUS	condition reference mark error => at least 1 tooth too few/many
B_KL15		EIN	condition ignition switch on
B_LUECKE	GGDPG	AUS	current segment covers the reference gap
B_MLUECKE	GGDPG	AUS	condition segment at mid reference gap at engines with odd number of cylinders
B_NLDG		EIN	condition limp-home function speed sensor
B_NLDGC		EIN	Second ECU is in the speed sensor limp home mode (via CAN)
B_NLPH	NLPH	EIN	condition no signal from the phase sensors
B_NMIN	GGDPG	AUS	condition lower speed: n < NMIN
B_NMOT	GGDPG	AUS	condition engine speed: n > NMIN
B_NOBM	GGDPG	AUS	condition BM-gap after > 60 teeth not found
B_NOBM1	GGDPG	AUS	condition 1. BM-gap after synchronization not found
B_NOPH	GGDPG	AUS	Phase signal not found
B_NOPH2	GGDPG	AUS	2. phase signal not found
B_NOSYNPH	NLPH	EIN	Flag for wrong cylindernumber at synchronisation-gap
B_PGQSYN	GGDPG	LOK	condition for using phase sensor PG/PG2 für quick start
B_PHA2ACT	GGDPG	AUS	condition signal of phase sensor 2 is high activ
B_PHA2ACT	GGDPG	AUS	condition signal of phase sensor 1 is high activ
B_PHAD	WANWKW	EIN	adaptation crankshaft/camshaft performed
B_PHAD2	WANWKW	EIN	adaptation crankshaft/camshaft 2 performed
B_PHAS2	GGDPG	AUS	Condition phase 2 low/high
B_PHASE	GGDPG	AUS	Condition phase low/high
B_PHNLDG	NLDG	EIN	phase identification in speed sensor limp home function
B_PHSOK	DPH	EIN	Condition phase signal ok
B_PHSOK2	DPH	EIN	Condition phase signal 2 ok
B_PHW	GGDPG	LOK	condition phase change during last tooth in gap search
B_PHW2	GGDPG	LOK	condition phase change on 2. PG during last tooth in gap search
B_PHWNEG	GGDPG	LOK	condition falling edge in phase signal used for quick start
B_PHWOK	GGDPG	LOK	condition phase change recognized
B_PHWOK2	GGDPG	LOK	condition phase change PG2 recognized
B_PHWPOS	GGDPG	LOK	condition rising edge in phase signal used for quick start
B_PRESYN		EIN	Synchronization is found by the second ECU at limp home (via CAN)
B_QSYN	GGDPG	AUS	Condition quick synchronization
B_ST	SWADAP	EIN	condition for start
B_STARTINI	GGDPG	AUS	start bit to distinguish first synchronization with KL15 from new synchr.
B_SYN	GGDPG	AUS	condition synchronization succeeded
B_SYNBMALE	GGDPG	LOK	Condition: No camshaft sensor for synchronization available
B_SYNNLDG	NLDG	EIN	condition: limp home crank position detected from PG-signal
B_SYNPH	GGDPG	AUS	condition synchronization phase
B_ZPREL	GGDPG	AUS	condition tooth debouncing ready
B_ZZTAB	GGDPG	AUS	condition: tooth time table valid
C_BMSUCH		EIN	ECU-condition: searching for reference mark
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_INISYN		EIN	ECU-condition for intialisation of angle synchronization
C_NSUCH		EIN	ECU-condition: searching for engine speed signal
C_PWF	SWADAP	EIN	ECU-condition powerfail intialisation
C_SYN		EIN	ECU-condition angle synchronization available
EDGE_CTR	GGDPG	LOK	index of the phase edge at recognized quick start position
E_BM	DDG	EIN	error flag: reference mark sensor
E_N	DDG	EIN	error flag: engine speed sensor
E_SGCAN		EIN	Error local CAN (2 ME)
GAPTOOTH	GGDPG	AUS	content of the tooth counter to check the gap
LEN_HISEG	GGDPG	LOK	length of the last 'high' phase segment during quick start
LEN_LOSEG	GGDPG	LOK	length of the last 'low' phase segment during quick start
NBM		EIN	input speed signal
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
PH		EIN	Input signal phase
PH2		EIN	Input signal phase 2
QZZYL	GGDPG	LOK	initial value cylinder counter at B_qsyn
R	GGDPG	DOK	vector computing base flags (only CU model)
R_BM	GGDPG	DOK	Schedule of reference mark (BM-gap)
R_NBM	GGDPG	AUS	Schedule of tooth signal
R_NBMNLDG	NLDG	EIN	software generated tooth interrupt from limp home speed sensor
R_SYN	GGDPG	AUS	Synchro schedule
R_SYNPH	GGDPG	AUS	synchro schedule for phase scan
R_SYNPH2	GGDPG	AUS	synchro schedule for phase scan 2
R_T10		EIN	Time schedule 10 ms
STATEQSYN	GGDPG	LOK	state of the quick-start State-Machine GEN_QSYN
SYNSTATE		EIN	current mode of synchronization
SY_GAP	PROKON	EIN	system constant: number of missing teeth in the gap
SY_NLDG	PROKON	EIN	System constant: TRUE crankshaft limp home function available
SY_PGRAD	PROKON	EIN	system constant: kind of the phase signal
SY_PGRAD2	PROKON	EIN	system constant: kind of the 2. phase signal
SY_PGTP0		EIN	system constant: performance of the camshaft sensor at power on
SY_PH2OFST	PROKON	EIN	system const. offset in syncros between the 2 active phase signals,2 PGs only
SY_SGANZ	PROKON	EIN	system constant, number of engine ECU's
SY_TEETH	PROKON	EIN	system constant: number of teeth with gap teeth on the crankshaft wheel



Variable	Source	Type	Description
SY_ZYLZA	PROKON	EIN	system constant number of cylinders
T		EIN	time
TMCORCTR_W	GGDPG	AUS	counter reference gap correction at a missing tooth
TMOT	SWADAP	EIN	Engine temperature
TNBM1_W	GGDPG	AUS	tooth periode of the second last NBM signal
TNBM2_W	GGDPG	AUS	tooth periode of the third last NBM signal
TNBM_W	GGDPG	AUS	tooth periode of the last NBM signal
TPCORCTR_W	GGDPG	AUS	counter reference gap correction at an additional tooth
TTOOTH10MS	GGDPG	AUS	counter 10 ms schedules without tooth interrupt
UZKW_W	GGDPG	AUS	revolution counter crankshaft
WKWBZM0_W	GGDPG	AUS	crank angle at the zero point of the working cycle: R_syn & zzyl = 0 (word)
WKWNEG_W	GGDPG	LOK	crank angle at the falling phase edge in quick start
WKWPOS_W	GGDPG	LOK	crank angle at the rising phase edge in quick start
WKWSTART_W	GGDPG	LOK	crank angle at NMIN detection in quick start
WKWSTOP	ALE	EIN	engine stopping position in working cycle
WKWSYN_W	GGDPG	AUS	crank angle at start of the synchro (word)
WKW_W	GGDPG	AUS	crank angle (word)
WNWSP2_W	WANWKW	EIN	Adaptation angle of the camshaft 2 in retarded end position
WNWSP_W	WANWKW	EIN	Adaptation angle of the camshaft in retarded end position
ZDELAY	GGDPG	LOK	tooth delay counter in quick start
ZNBM_W	GGDPG	AUS	counter tooth interrupt (word)
ZRPH	GGDPG	AUS	counter schedule of phase signal
ZRPH2	GGDPG	AUS	counter schedule of phase signal 2
ZYLVIRT	GGDPG	AUS	content of the cylinder counter before new synchronisation from quick start
ZZALE_INI	GGDPG	LOK	initial value for tooth counter zzseg at active engine stop position (B_ale)
ZZSEG	GGDPG	AUS	tooth counter in segment
ZZTAB	GGDPG	AUS	tooth time table
ZZVIRT	GGDPG	AUS	virtual teeth counter in start until synchronisation
ZZYL	GGDPG	AUS	SW-cylinder counter
ZZYL_VIRT	GGDPG	LOK	initial value cylinder counter at active engine stop position (B_ale)

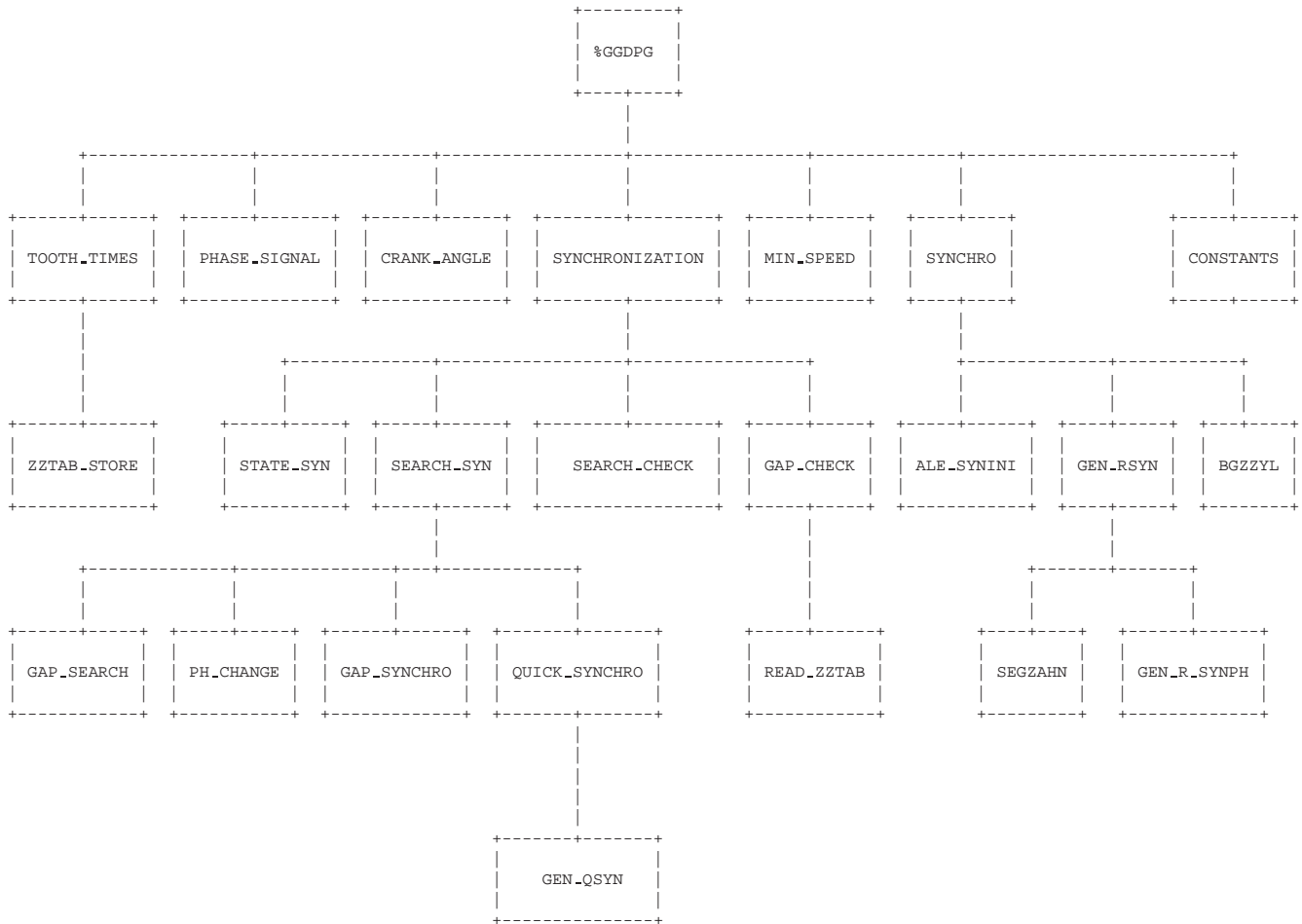
### FW GGDPG 14.30 Fixed Values

Parameter	Value	Description
CWNWREF		characteristics of the camshaft at engine start
DZZST		number of teeth when tooth suppression during start
DZZST2		Number of teeth for tooth debouncing with second phase sensor
DZZSTNLP		Number of teeth for tooth debouncing at camshaft limp home mode
NMIN		minimum engine speed
NMOTQSYN		engine speed threshold to enable quick start via phase sensor signal
NSYN2SG		Engine speed threshold for new synchronization at 2 ECU-concept with NLDG
OFQSYNADAP		offset between adapted phase edge and phase edge in start
PH_MINSEG		length of short segment at the quick start phase sensor signal
TMQSYN		engine temperature threshold to enable quick start via phase sensor signal
TPREL		tooth debouncing time during initialisation
ZDELBSRCH		additional tooth offset to wait for the next gap in quick start
ZTPREL		number of teeth during start recognition



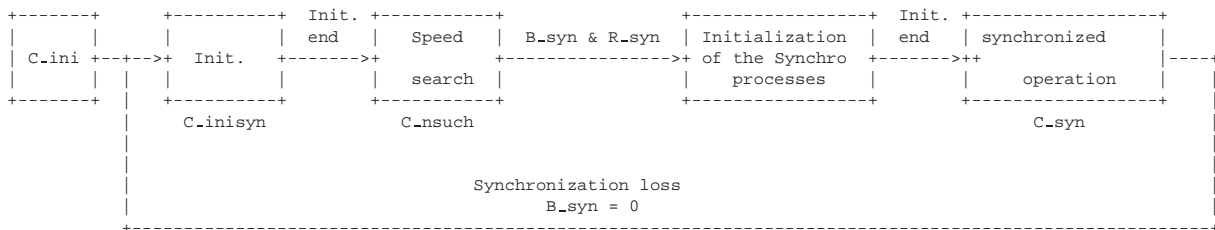
## FB GGDPG 14.30 Detailed description of function

Overview of the partial functions

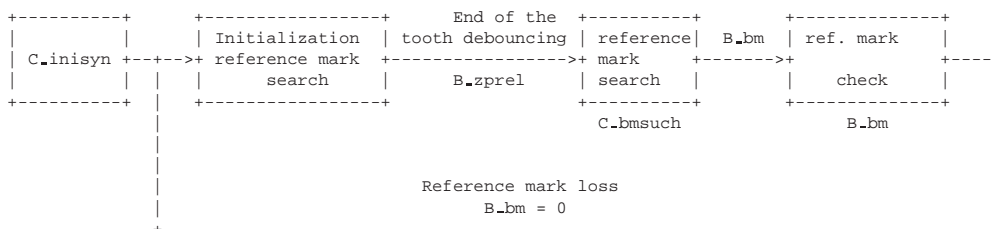


The sequential control for the synchronization and reference mark search is realized in %SYSYNC as follows:

Synchronization:



Reference mark search:





By this control the following sequence results after terminal 15 ON:

1. In the control unit initialization C\_ini the cylinder counter zzyl and the virtual tooth counter zzvrt are initialized from the stop position wkwstop and the bit B\_syn is set with valid stop position (B\_ale = true).
2. After the control unit initialization C\_ini immediately the synchro initialization follows C\_inisyn.
3. Subsequent to C\_inisyn immediately the speed search C\_nsuch is performed.
4. The speed search C\_nsuch starts the debouncing of the speed signal, for this at first the time TPREL, hence the number of teeth DZZST are debounced in the partial function CRANK\_ANGLE. After the debouncing B\_zprel is set.
5. With B\_zprel the reference mark search phase C\_bmsuch starts. The tooth time tnbm\_w is formed during C\_bmsuch, which is shifted to a shift register in the tooth interrupt (tnbm1\_w, tnbm2\_w). As soon as tnbm2\_w < tooth time(NMIN), B\_nmot is set.
6. With B\_nmot the actual gap search is started in GAP\_SEARCH. Parallel to the gap search the virtual angular basis runs provided a valid stop position is given (B\_ale) and the synchronization search via the quick-start sensor wheel. In the process the virtual position can be re-synchronized when the quick-start position is found (B\_qsyn). B\_qsyn leads to an immediate triggering of a virtual synchro interrupt.
7. With the first synchro interrupt (also virtual) the system changes to the synchronized state C\_syn. The current synchronization state is outputted in the variable synstate (0=not, 1=run-out detection, 2=quick-start wheel, 3=reference mark). In the state synstate = 1 (synchronized via run-out detection) only the injection is enabled, in the states synstate > 1 (quick-start sensor wheel resp. reference mark) the injection as well as the ignition are enabled.
8. When finding the gap, B\_bm is set and the system changes from C\_bmsuch to the reference mark check. This state is described by B\_bm. If in each synchro cycle after the gap the reference mark is not found, then B\_bm and B\_syn are reset and a new synchronization (C\_inisyn) is triggered.

#### Tooth debouncing

After the initialization C\_inisyn the state directly enters the speed search phase C\_nsuch. At the first tooth edge the debouncing time TPREL is started. During this time no tooth interrupts are evaluated. Subsequent to TPREL also DZZST tooth edges are debounced. If the first camshaft sensor is defective and a second sensor is available there are DZZST2 tooth edges debounced (different sensor or camshaft wheel). B\_zprel is set after this tooth debouncing and the counter znbm\_w resp. wkw\_w is reset. If the condition B\_nlpf is set (camshaft limp home function) then tooth edges for several engine cycles are debounced to clear out possible residual charge.

#### Reference mark search phase

With B\_zprel the reference mark search (C\_bmsuch) is started. In this state the following functions are calculated in the tooth interrupt:

- The virtual engine position from the stop position (zzvirt, zzyl)
- Crank-angle determination and synchronization via the quick-start sensor wheel (B\_syn, qzzyl)
- Reference mark search (B\_bm)

Once the gap is detected the system changes from the state C\_bmsuch to the reference mark check (B\_bm).

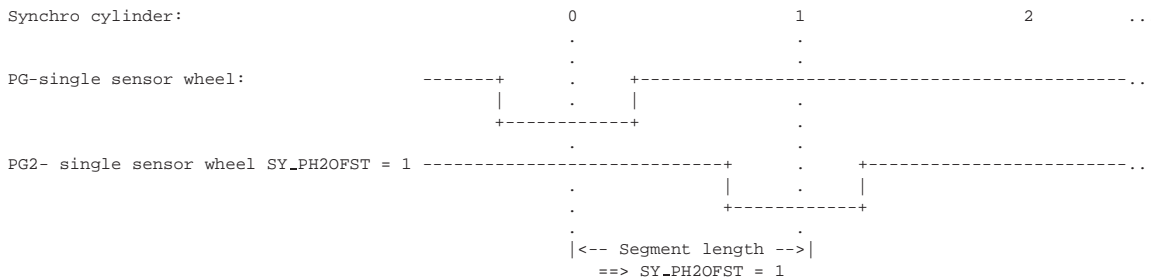
#### Synchronization via run-out detection

In C\_ini the virtual cylinder counter zzvrt and the cylinder counter zzyl are initialized from the stop position wkwstop at valid run-out detection. The tooth counter zzvrt is incremented in the tooth interrupt after the tooth debouncing (C\_bmsuch). When zzvrt = 0, a synchro interrupt R\_syn is triggered and zzvrt is set to the number of teeth per segment.

#### Scanning of the phase signal

The phase level is scanned in the tooth interrupt during C\_bmsuch. With found reference mark (B\_bm) the phase level PH is scanned at each second tooth edge after the gap. For the second phase sensor a distinction is made on whether its active phase level also lies within the gap (SY\_PH2OFST = 0) or is shifted by a manifold of a segment (SY\_PH2OFST > 0). SY\_PH2OFST corresponds to the distance between the phase levels in segments.

Example:



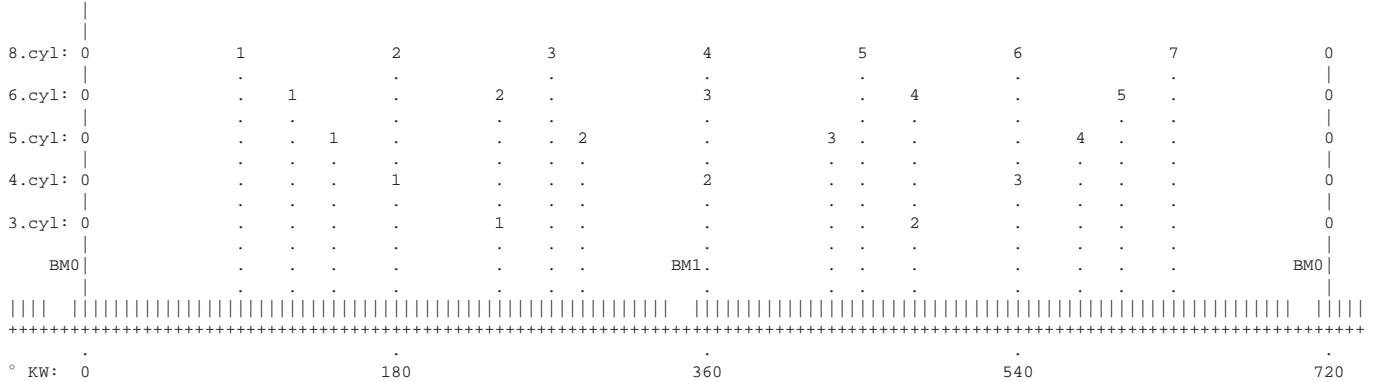
When SY\_PH2OFST = 0, the phase level PH2 lies simultaneous to PH and can therefore also be scanned at the reference mark.  
When SY\_PH2OFST > 0, the phase level is scanned staggered by SY\_PH2OFST segments (SY\_PH2OFST \* CO\_ZSGMT) to the reference mark.



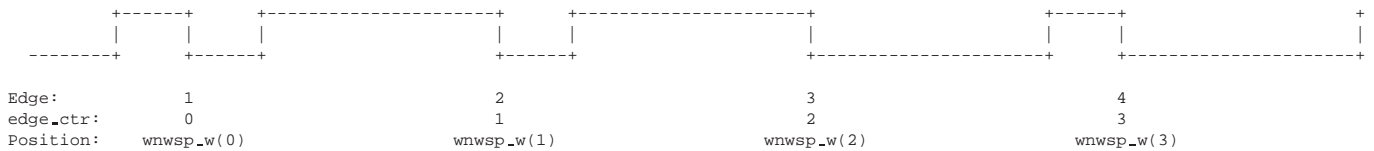


Assignment phase signal, synchro cycle to crank angle, quick-start sensor wheel

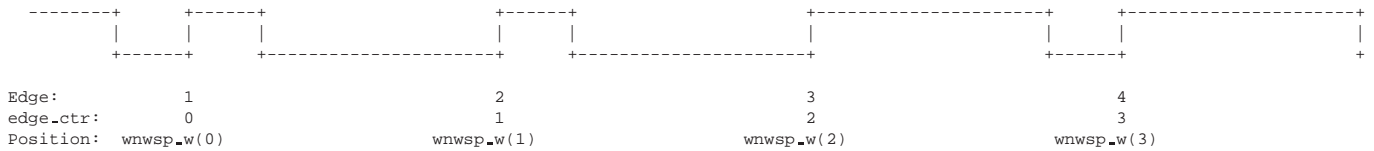
SW-reference mark



Quick-start phase sensor wheel SY\_PGRAD = 4, low-active:



Quick-start phase sensor wheel SY\_PGRAD = 4, high-active:



Synchronization via quick-start sensor wheel

If a system possesses a quick-start sensor wheel (SY\_PGRAD\* = 4) and if the phase edges have been adapted (B\_phad = true), then the phase sensor signal is used for the quick-start synchronization below the speed threshold NMOTQSYN. The function is only released via a CodeWord if the camshaft is in the reference position at engine start. The phase level scanned in the tooth interrupt is checked for edge changes and if necessary the flag B\_phw is set. During quick-start always B\_nmot is waited for. After B\_nmot the negative phase edge is evaluated and the quick-start is initiated. By evaluating the positive edges resp. by waiting for further teeth at first the index of the edge (edge\_ctr) is determined and then the number of teeth till the next segment beginning. Once these teeth have been waited for B\_qlsyn is set and thereby a synchronization via the quick-start sensor is triggered. If the system is already in the synchronized state (run-out detection), then a re-synchronization is performed. The detailed sequence of the quick-start is as follows:

stategsyn	State	Remark
0	Start_qlsyn	Entry state into the quick-start at C_inisyn. Nothing is calculated in this state, waiting for tooth debouncing. Transition to Wait_nmot in the reference mark search phase C_bmsuch if tmot > TMQSYN.
1	Wait_nmot	B_nmot is not yet set, the tooth debouncing has taken place. The phase changes are recorded (wkwneg_w and B_phwneg at negative, wkwpos_w and B_phwpos at positive phase edge). Transition to Wait_negedge with B_nmot.
2	Wait_negedge	Waiting for a negative phase edge (B_phwneg). During entry a check is performed on whether a negative phase edge has already been detected and if necessary the exit condition is checked. If B_phwneg is not yet given then the negative edge is waited for and hence the exit condition is checked. The following exit conditions are possible:  Prio 1: Phase edge has already been detected (edge_ctr > -1) ==> Gen_qlsyn Prio 2: Length of the high segment is known (len_hiseq > 0) ==> Wait_shortseg Prio 3: Only the negative phase edge has been detected ==> Wait_gap
3	Wait_gap	In this state only the negative phase edge was detected. The number of teeth from the 2nd phase edge to the 1st reference mark as well as from the 4th phase edge to the 2nd reference mark is calculated and the tooth counter zdelay is set to maximum value. Once these teeth have passed either a reference mark occurs (this terminates the quick-start immediately, exit via the reset condition after End_qlsyn) or the negative edge can be determined by the current phase level, at high level the engine was at the 1st otherwise at the 3rd edge. The exit therefore takes place when zdelay = 0 after Gen_qlsyn, where here the phase edge (edge_ctr) during the exit is determined by level inquiry.



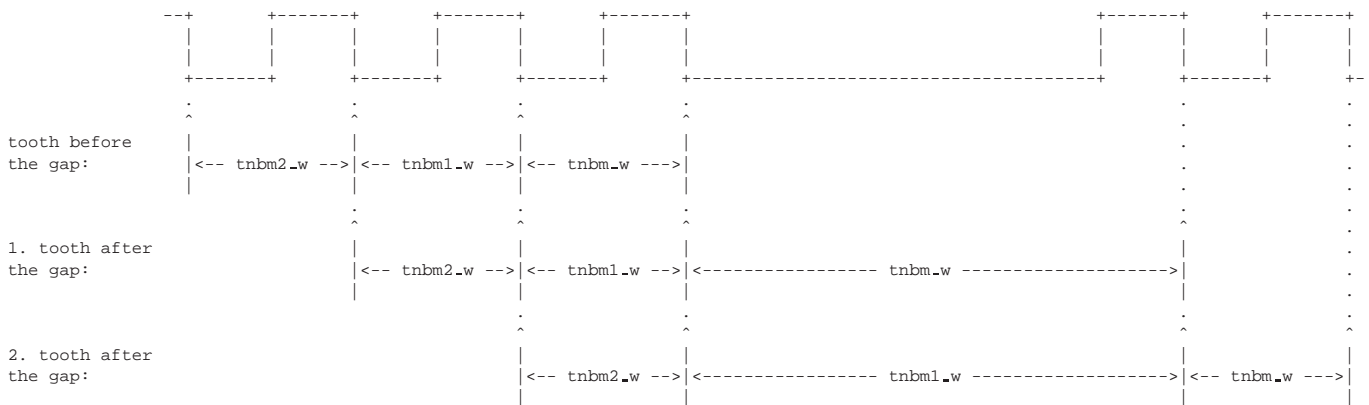
- 4        Wait\_shortseg    The length of the last high segment is known in this state. With a high segment the engine is at the 2nd or 3rd, otherwise at the 1st or 4th phase edge. By waiting for a short low segment it is possible to identify the phase edge. The exit to Gen\_qlsyn is therefore performed at a positive edge or after zdelay teeth have passed. Zdelay is calculated from the distance of the phase edge with following long low segment plus PHMINSEG until the next synchro beginning. During the exit a check is then performed on whether a edge change has occurred and thereby the phase edge (edge\_ctr) is defined.
- 5        Gen\_qlsyn        The negative phase edge (edge\_ctr) and the difference between the current position and the phase edge (wkw\_w - wkwneg\_w) is known when entering this state. Thereby the current position is determined, the number of teeth until the next synchro (zdelay) as well as its cylinder number (qzzyl) is calculated. Thereafter zdelay teeth are waited for and then B\_qlsyn is set. Thereby the quick-start is terminated and the state machine changes to End\_qlsyn.
- 6        End\_qlsyn        End of the quick-start. This state is start as well as reset state at the same time. The reset condition is B\_bml (reference mark found) or B\_engsyn (quick-start not enabled).

Synchronization via reference mark, gap search  
-----

At virtual synchronized operation (run-out detection resp. quick-start sensor wheel) the system is in the state C\_bmsuch. The gap is still searched for in the tooth interrupt in this state. For this, each last tooth time tnbm\_w is shifted to the shift register tnbm1\_w and tnbm2\_w and the current tooth time is calculated again. The gap is detected in GAP\_SEARCH and B\_bm is set, if the following condition is fulfilled:

$$(tnbm_w < tnbm1_w / 2) \text{ and } (tnbm2_w < tnbm1_w / 2)$$

Ex.:



==> Reference mark at the 2nd tooth after the gap found, B\_bm = 1

The cylinder counter is initialized new by means of the phase information and a re-synchronization is triggered after B\_bm was set. Simultaneously the state C\_bmsuch is terminated, the system runs in the state "synchronized via reference mark" (B\_bm = true).

Monitoring of the gap search  
-----

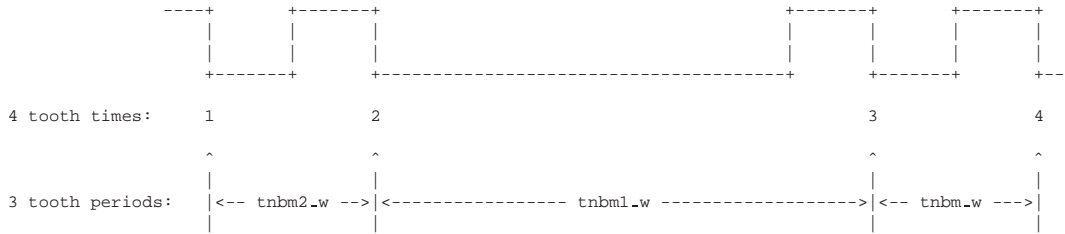
If the gap is not found within 720° KW in the speed search phase, then the bit B\_nobm is set and thereby a virtual synchronization is reset via B\_syn. The synchronized operation is aborted after this resetting and the system can only still be synchronized by the reference mark (B\_bm 0->1). The bit B\_nobm is reset in C\_ini.

Synchronized via reference mark, gap check  
-----

The synchro cycle (R\_syn) is generated via the counter zzseg during operation B\_bm. At the beginning of the synchro, zzseg is each time loaded with the number of teeth of the subsequent segment. This counter is decremented in the tooth interrupt and when zzseg = 0 the next synchro cycle is generated. When loading the counter zzseg after a gap segment a possible correction by 1 tooth from the last segment is taken into consideration.

Each gap check is performed in the segment after the gap. Since the position of the gap in the last segment is known, this can be checked by means of the tooth time table. At first the 4 tooth times at the gap are read and the 3 tooth periods are calculated as follows:



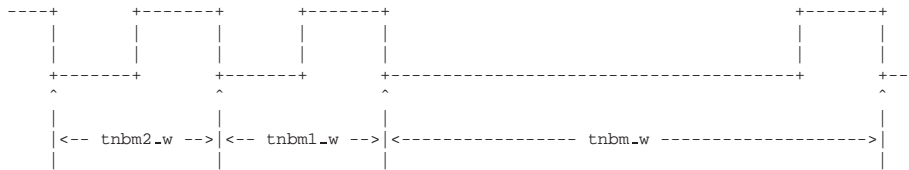


With the condition:

B\_st = TRUE: (tnbm\_w < tnbm1\_w / 2) and (tnbm2\_w < tnbm1\_w)  
B\_st = FALSE: (tnbm\_w < tnbm1\_w / 2) and (tnbm2\_w < tnbm1\_w / 2)

the gap is detected as being correct analogous to the gap search. In this case B\_fbm = 1 and B\_bm = 0 do not change. If a fault by one tooth occurred since the last reference mark, then this can be detected by the following conditions and it can be corrected by setting bmkor. In case of a fault by 1 tooth B\_bm = 1 remains set and B\_fbm is additionally set.

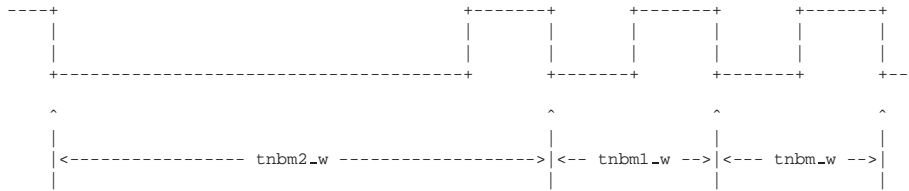
1 tooth too many:



Detection by:  $tnbm_w / 2 > tnbm1_w$

In this case the tooth counter zzseg is decremented by 1 via bmkor = -1 and the fault is corrected in the segment to follow. At each correction by -1 tooth the counter tpcorctr\_w is increased by 1.

1 tooth too little:



Detection by:  $tnbm2_w / 2 > tnbm1_w$

In this case the tooth counter zzseg is incremented by 1 via bmkor = 1 and the fault is corrected in the segment to follow. At each correction by 1 tooth the counter tpcorctr\_w is increased by 1.

If none of these conditions occur, then the gap was not found, the reference mark loss counter bmlosctr\_w was incremented, B\_bm and thereby B\_syn were reset and thus a new synchronization was forced.

Tooth periods, tooth time table

During the reference mark search phase the tooth period tnbm\_w is calculated as of the second tooth interrupt and shifted to the shift register tnbm\_w, tnbm1\_w, tnbm2\_w. These tooth periods are used to set resp. reset the conditions B\_nmot resp. B\_nmin, to calculate the engine speed (%BGNMOT) and to search the gap.

As of B\_bm only the counter zzseg is still decremented in the tooth interrupt and the accompanying segment time t is written into the tooth time table zztb. The tooth time table is an array of tooth times with (SY\_ZSGMT + 3) elements. The table is written into as of the 2nd element when the first synchro triggered by B\_bml occurs. At each following synchro cycle (R\_syn) the two last tooth times are copied to the table positions 0 and 1 and the table is again written into as of position 2. Once the table has been written into for the first time, B\_zztb is set. The length of the table (CO\_ZSGMT + 3) thus results from the 2 entries of the teeth from the previous segment and the segment length plus one tooth, which can be corrected without a synchronization loss.

Monitoring of minimum speed

The 3 last tooth periods are used during the reference mark search (C\_bmsuch) for the monitoring of the minimum speed. The tooth period for the setting of B\_nmot is obtained from the speed threshold NMIN as follows:

$$\text{min. tooth time} = (60 / \text{NMIN}) / \text{SY\_TEETH.}$$

B\_nmot is set when:  $tnbm2_w < \text{min. tooth time}$

By using tnbm\_2 to set B\_nmot it is ensured that the tnbm shift register is completely filled and that the gap can immediately be searched for with B\_nmot. When B\_nmot is set, B\_nmin is reset.

Resetting of B\_nmot is performed when:  $(tnbm_w > tnbm_{\text{min}_w}) \text{ and } (tnbm1_w > tnbm_{\text{min}_w})$



By monitoring the two tooth times `tnbm_w` and `tnbm1_w` it is ensured that `B_nmot` cannot be reset by the "gap tooth".

At operation synchronized via reference mark (`B_bm`) the minimum speed is monitored by the counter `ttooth10ms`. If no tooth interrupt occurred since the last 10 ms cycle, then this counter is incremented (if the crankshaft is at the "gap tooth" -> triple tooth time, then only every third cycle is incremented), otherwise the counter is reset to 0. If no tooth interrupt occurs within 50 ms (50 ms tooth period corresponds to a minimum speed of 20 rpm at `SY_TEETH = 60`), then `B_nmot` is reset.

When resetting `B_nmot`, `B_nmin` is automatically set again. With `B_nmot` also `B_syn` is reset and thereby a new synchronization (`C_inisyn`) is triggered.

Formation of the cylinder counter  
-----

The cylinder counter `zzyl` indicates the SW cylinder number of the current synchro. In the process `zzyl` is incremented at the beginning of the synchro cycle, when `zzyl = SY_ZYLZA` it is reset to 0 again.

In case of a new resp. re-synchronization the cylinder counter is initialized as follows:

synstate	Initialization from:	Meaning
1	<code>zzyl_virt</code>	With valid run-out position the start position is determined in <code>C_ini</code> from <code>wkwstop</code> by adding the debounced teeth and from this the start values for the tooth counter <code>zzale_ini</code> and the cylinder counter <code>zzyl_virt</code> are initialized. Taking this position as a basis the virtual angular basis is followed up after the tooth debouncing until a re-synchronization is performed via the quick-start or the gap.
2	<code>qzzyl</code>	At quick-start the cylinder number of the following segment is determined when the engine position was found and at its synchro beginning a synchro cycle is triggered via <code>B_qsyn</code> . By the change from <code>synstate</code> to <code>synstate = 2</code> , the cylinder counter <code>zzyl</code> is initialized to <code>qzzyl</code> .
3	<code>bmzzyl</code>	When the gap was found, the cylinder number for the segment following the gap is determined ( <code>bmzzyl</code> ) by means of phase determination (see below). During the change from <code>synstate</code> to <code>synstate = 3</code> , <code>zzyl</code> is initialized with <code>bmzzyl</code> .

Calculation of `bmzzyl`:

The segment to follow the gap must be initialized by `bmzzyl = CO_ZYLB0` or `bmzzyl = CO_ZYLB1`, dependent on the current phase position. The phase position is determined according to the following sequence:

1. At limp-home speed sensor the phase position is calculated in `%NLDG` and made available by `B_phnldg` ==> `B_phnldg`
2. Phase sensor PG detected as not defective (`B_phsok`) ==> `B_phaact`
3. Optional second phase sensor PG2 detected as not defective (`B_phsok2`) ==> `B_pha2act`
4. Run-out detection valid (`B_ale`), the virtual position calculated from the stop position is valid ==> `zzvirt`
5. Neither phase position nor virtual engine position known, synchronization to cylinder after BM 0 ==> `CO_ZYLB0`

Priority 3 is only available if a second phase sensor exists (`SY_PGRAD2 > 0`) and if it provides a signal at the reference mark that can be used for the synchronization (`SY_PH2OFST = 0`).

If there is no camshaft sensor information available at the reference gap for synchronization and `B_ale` is TRUE so the engine position is calculated via the run-out position. The actual engine position results in the following way:

$$\text{wkwstop} / \text{CO\_WNBM} + \text{ZTPREL} + \text{DZZSTNLP} + \text{tooth edges from the end of tooth debouncing till the reference gap} + \text{gap correction}$$

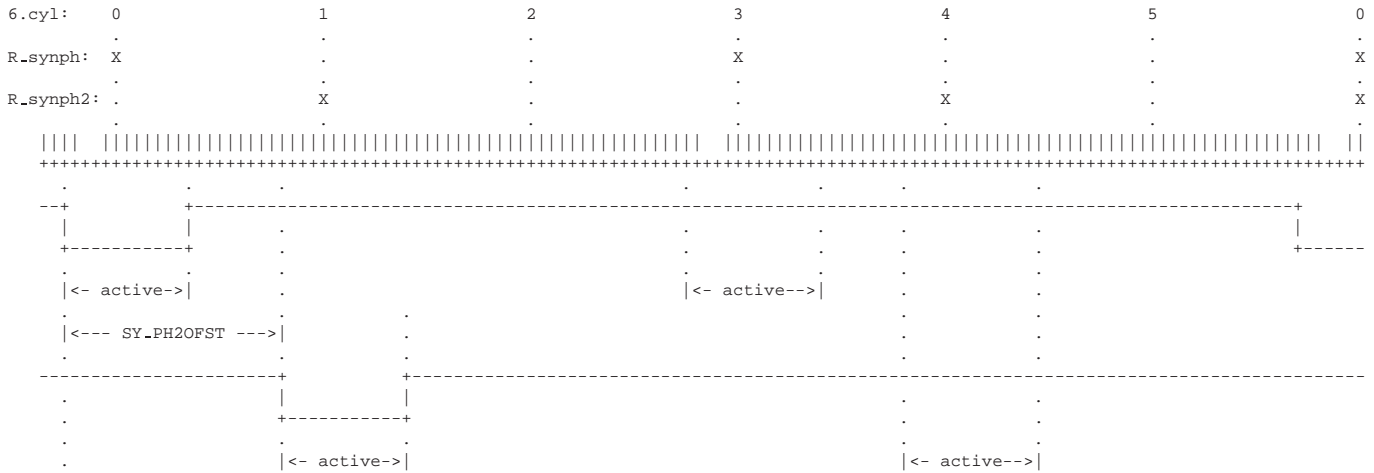
there `zzvirt` is initialized with `zzale_ini = 255 - wkwstop / CO_WNBM` in `C_ini` (`zzvirt` is decremented at each tooth)

Tooth number at reference gap: `ZTPREL + DZZSTNLP + 255 - zzvirt + gap correction`

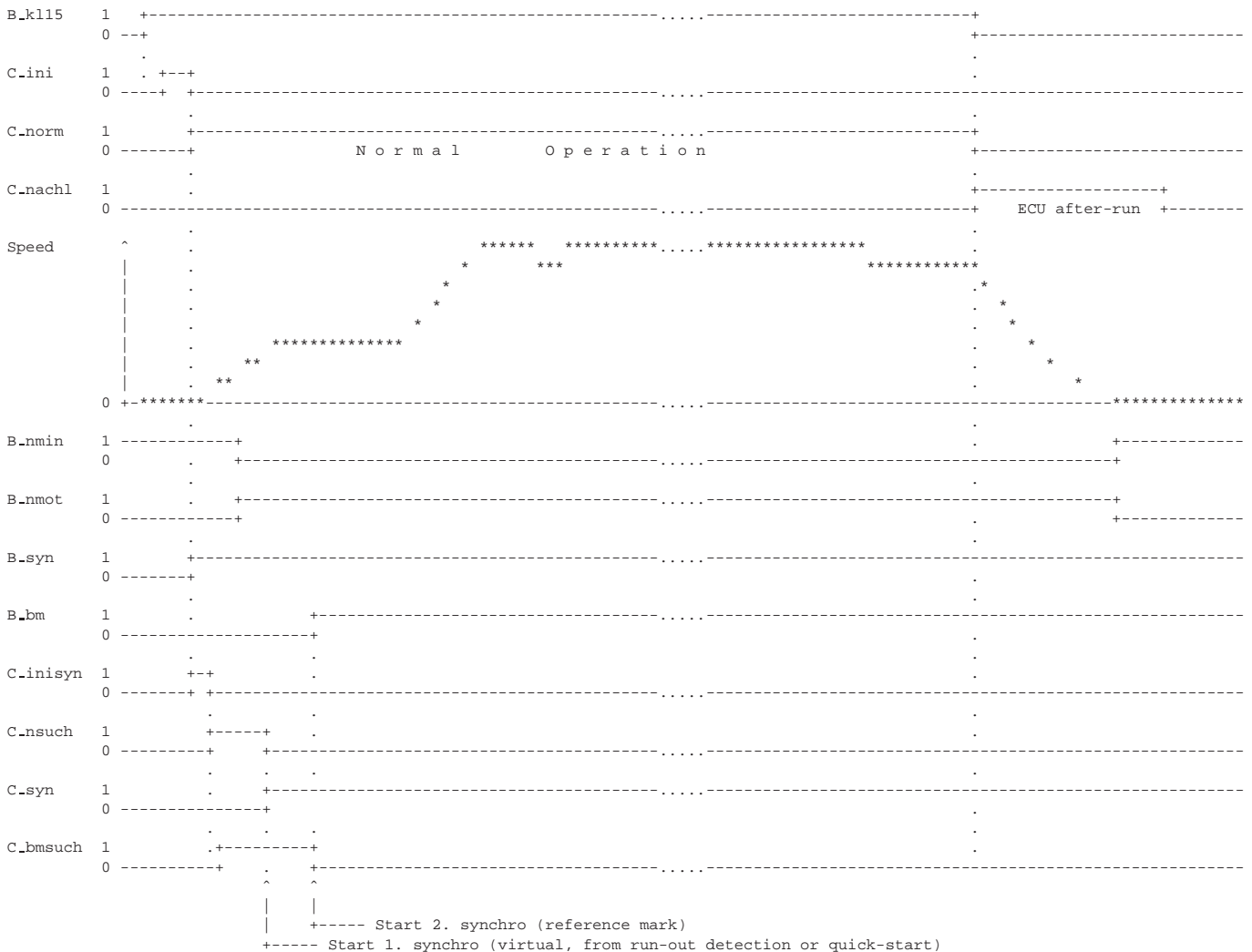
Cycle for phase inquiry, `R_synph` and `R_synph2`  
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The cylinder number `zzyl` is inquired upon in the synchro interrupt to generate a cycle for the phase inquiry. If the beginning of the current segment lies in resp. directly after the active phase position, then the cycle for phase inquiry/phase monitoring is triggered. That angle range is referred to as active phase position, at which the phase position can definitely be determined. For the first phase sensor PG these are always those segments, which follow the gap. For the second phase sensor PG2 the active phase position lies staggered by `SY_PH2OFST`.

Example (6 cylinder, `SY_PH2OFST = 1`):

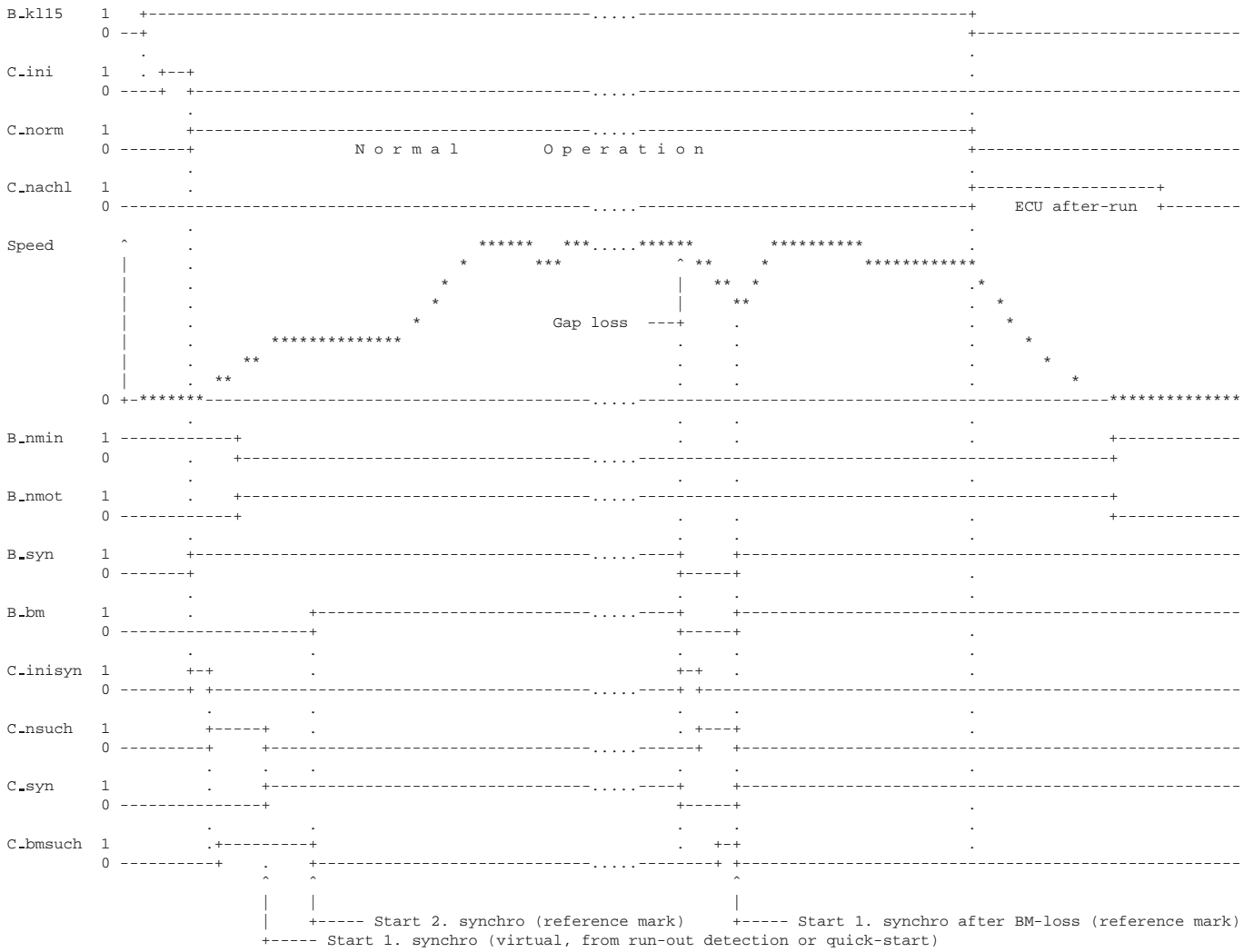


1. Timing: Sequence of a typical operating cycle:



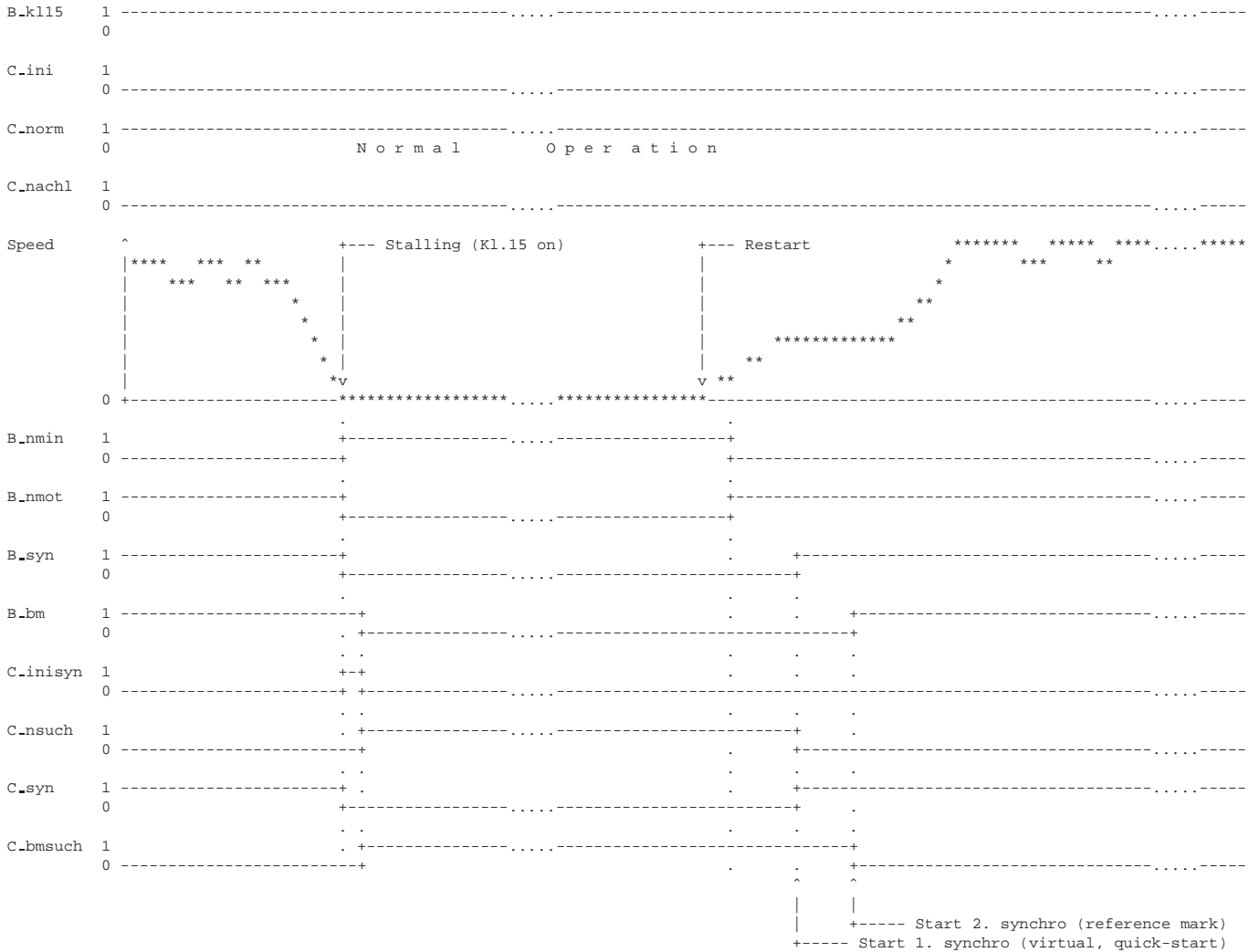


## 2. Timing: Synchronization loss (e.g. two teeth too many detected):





3. Timing: Stalling and Kl.15 remains on, hence restart without Kl.15 off



Monitor for New-Synchronization

At a new synchronization all relevant values are initialized to neutral values. Because of the immediately initialization after the new synchronization it is not possible to see the corresponding Bit which has requested the new synchronization. To make the fault location easier a new synchronization monitor is formed. This monitor makes it possible to register the reason of the last new synchronization with VS100.

In the Byte NSYNGGDPG a Bit is set at a corresponding position, which tells the condition which has requested the new synchronization. The Byte NSYNGGDPG is always initialized at C\_ini with 00000000.

- NSYNGGDPG Bit 0 new synchronization requested via B\_nobm
- Bit 1 new synchronization requested via rising edge of B\_nmin and C\_syn
- Bit 2 new synchronization requested via falling edge of B\_bm

Are there are occurring several new synchronizations during one driving cycle with different reasons, so there are several Bits of NSYNGGDPG set to 1.

**APP GGDPG 14.30 Application hint**

For the application of the %GGDPG the following variables possibly need to be adjusted:

Speed-signal debouncing

TPREL	30 ms	Time debouncing at engine start. During the speed search phase (C_nsuch) the time debouncing TPREL is started at the first tooth interrupt. No tooth interrupts are evaluated during this time.
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**DZZST**      2      Tooth debouncing at engine start. After the time debouncing (TPREL) additionally DZZST teeth are debounced. The condition  $B_{zprel}$  is set after this debouncing and thereby the gap search ( $C_{bmsuch}$ ) is started. Dependent of the used camshaft sensor (TPO / not TPO -> default phase level) and the position of the phase signal to the reference mark, the value DZZST must be set appropriate. It must be guaranteed that the phase level at the first found reference mark has the correct level.

**DZZST2**      2      This value only exists if there are two different camshaft signals. As long as there are no different camshaft sensors or wheels are used it is  $DZZST2 = DZZST$ . If on the other hand for example PG1 is a TPO sensor and PG2 is a none TPO sensor, then there must be a appropriate bigger value applied.

**DZZSTNLP**    232      Makes sure that at camshaft sensor limp home the engine is turned several times to clear out possible residual charge.

**ZTPREL**      8      To calculate the virtual engine start position the debounced teeth (DZZST and ZTPREL) are added to the stop position  $wkwstop$  determined in the section §ALE. In the process, ZTPREL represents the teeth passed before resp. during the time debouncing (TPREL).

To determine ZTPREL the virtual engine position at the first reference mark needs to be observed (without PG quick-start). The counter  $zsvirt$  (virtual segment tooth counter) is frozen when the gap is found and the cylinder counter  $zyl$  is re-stored in  $zylvirt$ . At optimum virtual engine position  $zsvirt$  must stop at  $SY\_GAP$  and the cylinder counter must be incremented by 1 (due to the gap the virtual engine position runs at  $SY\_GAP$  teeth too late and would trigger a virtual segment after these teeth). If the virtual engine position lies by a certain variable incorrect during several starts, then this can be corrected with ZTPREL.

Condition engine speed  $B_{nmot}$   
-----

**NMIN**      20 rpm      Speed threshold for the setting of  $B_{nmot}$  in the speed search phase ( $C_{nsuch}$ ). In case of systems with a high rotational dynamik at start / cold start the value has to be increased (for e.g. 35 rpm), else there could be a wrong detection of the gap. Danger of a wrong synchronization !

PG quick-start  
-----

**NMOTQSYN**    500 rpm      Upper speed threshold for PG quick-start. For run-time reasons the PG quick-start function  $GEN\_QSYN$  calculated in the tooth interrupt is switched off. The functionality is anyhow not needed at higher engine speeds.

**OFQSYNADAP**   0 °KW      Offset between adapted phase edge and the phase edge at start (phase response correction). The phase edge stored in  $wnwsp\_w\_x$  has been adapted at idle speed. Due to a phase response of the phase sensor signal the PG edge may be shifted at start (typ. 100 rpm).

The actual phase angle at quick-start is therefore calculated according to:

$$\text{Angle\_actual}(\text{edge } x) = \text{wnwsp\_w\_x} - \text{OFQSYNADAP}$$

**PH\_MINSEG**    54 °KW      Segment length of a short segment. This variable is used at quick-start to inquire upon a small resp. large segment. For safety reason this value should be chosen at least by one tooth (6°KW) larger than the longest 'Short-Segment' occurring in the PG signal. In the process high as well as low segments must be taken into consideration. If this value is chosen too large, the worst-case is that a short segment is detected too late and a synchro can no longer be triggered. Rule of the thumb for the definition:

$$\text{PH\_MINSEG} = \text{longest 'Short-Segment' rounded to next full tooth} + 6 \text{ °KW}$$

$$\text{EX.: longest 'Short-Segment' = } 44 \text{ °KW, rounded to } 48 \text{ °KW} \\ \Rightarrow \text{PH\_MINSEG} = 54 \text{ °KW}$$

**TMQSYN**      143.25 °C      Lower engine temperature threshold to enable the phase sensor PG for the quick-start.

**ZDELBMSRCH**   1      At quick-start, in the state 'Wait\_gap' it is calculated after how many teeth the reference mark occurs, in case the engine is at the 2nd resp. 4th phase edge. To this number of teeth additionally ZDELBMSRCH teeth are added. If no gap occurs within this crank angle, then the last edge can be identified by means of the phase level. This value may not be chosen too large since the inquiry for phase level will no longer work and a synchro beginning can no longer be found due to waiting for too long (especially on 4- and 8-cylinder engines).

Recommendation:  $ZDELBMSRCH < 6$  for all engines, dependent on the length of the short segment and on the mounting position of the sensor signal related to the crankshaft

$$ZDELBMSRCH = 1 \text{ for 4- and 8-cylinder engines} \\ ZDELBMSRCH = 3 \text{ for all other engines}$$

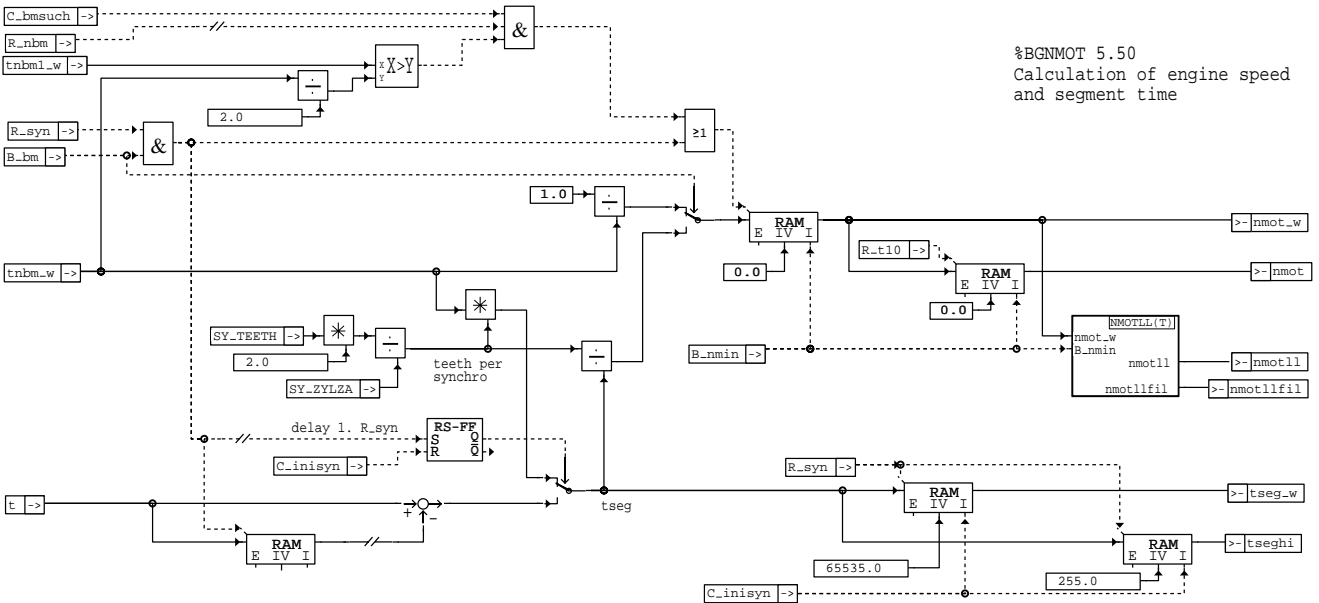
**CWNWREF**      Indicates whether the camshaft is in reference position during engine start. It is the case if the system has no camshaft adjustment or the camshaft has a mechanical locking element.

2 ECU-concept  
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**NSYN2SG**      800 1/min      engine speed threshold up to which a new synchronisation is triggered if there was no run-up of the engine at the moment of detection of the crankshaft sensor limp home at the second ECU.

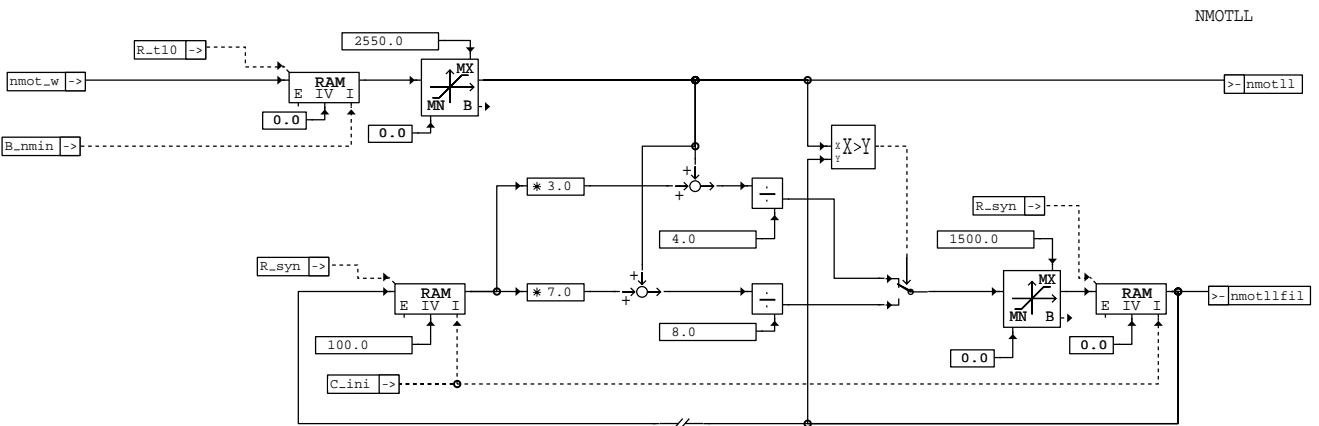
**BGNMOT 5.50 Calculated variable: engine speed**

**FDEF BGNMOT 5.50 Function definition**



**bgnmot-bgnmot**

Calculation of the engine speed *nmot* resp. *nmot\_w* as well as of the segment time *tseg\_w* (*tseg\_hi* represents a high-level byte of *tseg\_w* since an overflow can occur in *tseg\_w* at low engine speeds). The engine speed *nmot\_w* is calculated from the tooth-period time *tnbm\_w* during the gap search (*C\_bmsuch*). At synchronized operation (*B\_bm* = true) the calculation is performed from the segment time.



**bgnmot-nmotll**

Engine speed for lower speed range

The actual engine speed is stored from *nmot\_w* to *nmotll* with the corresponding quantization at the 10 ms cycle. If the engine speed is greater than 2550 rpm *nmotll* stops at the value of 2550 rpm. In the ECU switch off *nmotll* is no longer calculated.

The engine speed *nmotll* is filtered by a first-order time-delay element (*nmotllfil*). The time constant of the filter is different, dependent whether there is an acceleration or a deceleration. The filtered engine speed is only calculated up to 1500 rpm to keep the running time as short as possible.

$$nmotllfil(k) = \frac{7 * nmotllfil(k-1) + nmotll(k)}{8} \quad \text{at acceleration}$$

$$nmotllfil(k) = \frac{3 * nmotllfil(k-1) + nmotll(k)}{4} \quad \text{at deceleration}$$



## ABK BGNMOT 5.50 Abbreviations

Variable	Source	Type	Description
B_BM	GGDPG	EIN	condition reference mark detected
B_NMIN	GGDPG	EIN	condition lower speed: $n < NMIN$
C_BMSUCH		EIN	ECU-condition: searching for reference mark
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_JNISYN		EIN	ECU-condition for intialisation of angle synchronization
NMOT	BGNMOT	AUS	engine speed
NMOTLL	BGNMOT	AUS	engine speed
NMOTLLFIL	BGNMOT	AUS	filtered engine speed nmotll
NMOT_W	BGNMOT	AUS	engine speed
R_NBM	GGDPG	EIN	Schedule of tooth signal
R_SYN	GGDPG	EIN	Synchro schedule
R_T10		EIN	Time schedule 10 ms
SY_TEETH	PROKON	EIN	system constant: number of teeth with gap teeth on the crankshaft wheel
SY_ZYLZA	PROKON	EIN	system constant number of cylinders
T		EIN	time
TNBM1_W	GGDPG	EIN	tooth periode of the second last NBM signal
TNBM_W		EIN	tooth periode of the last NBM signal
TSEghi	BGNMOT	AUS	segment cycle time, high, low byte of the high word
TSEG_W	BGNMOT	AUS	segment cycle time

## FW BGNMOT 5.50 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

## FB BGNMOT 5.50 Detailed description of function

The calculation of the segment time `tseg_w` is performed in the synchro-interrupt. The temporarily stored time of the previous synchro is subtracted from the current system time `t`. Since no temporarily stored time yet exists at the first synchro the segment time is calculated from the latest tooth time, `tnbm_w` multiplied by the number of teeth per segment. At low engine speeds overflows occur in `tseg_w`, which are stored in `tseghi`.

The engine speed `nmot_w` is calculated in the tooth interrupt from the latest tooth time `tnbm_w` during the reference mark search (`C_bmsuch`). If triple the tooth time occurs after the reference mark gap then the speed value of the latest tooth is maintained. At synchronized operation (`B_bm = true`) `nmot_w` is calculated in the cycle `R_syn` from the segment time `tseg`. In the 10 ms-cycle `nmot` and `nmotll` from `nmot_w` are re-quantized and updated.

## APP BGNMOT 5.50 Application hint

## RDE 1.40 Detection of reverse rotation

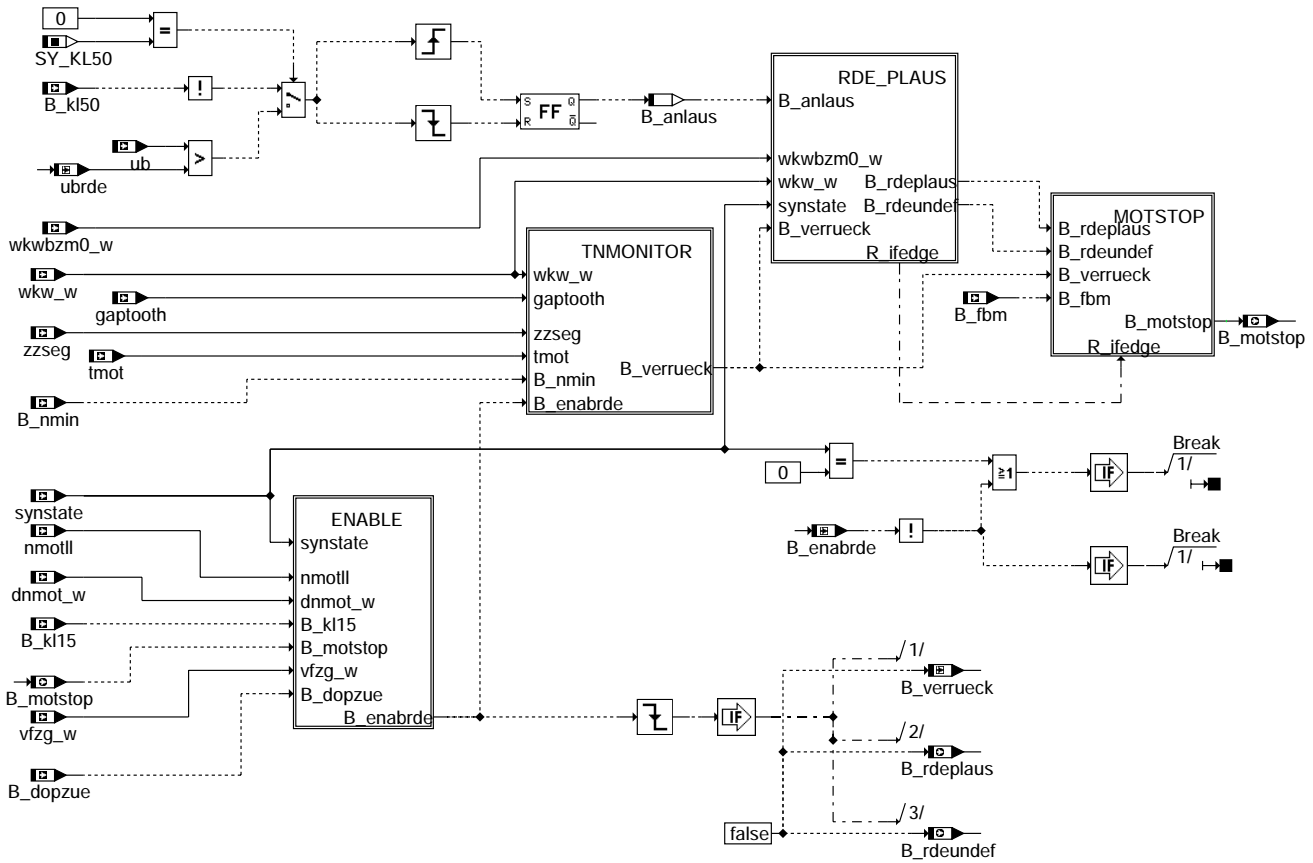
### FDEF RDE 1.40 Function definition

The decision whether to include the function in the program status can be made using the system constant `SY_RDE`.

```
SY_RDE = 1 (TRUE)  Function included in the program status (must be applied with care whatever the case)
SY_RDE = 0 (FALSE) Function not included in the program status
```



## RDE 1.40: Detection of reverse rotation

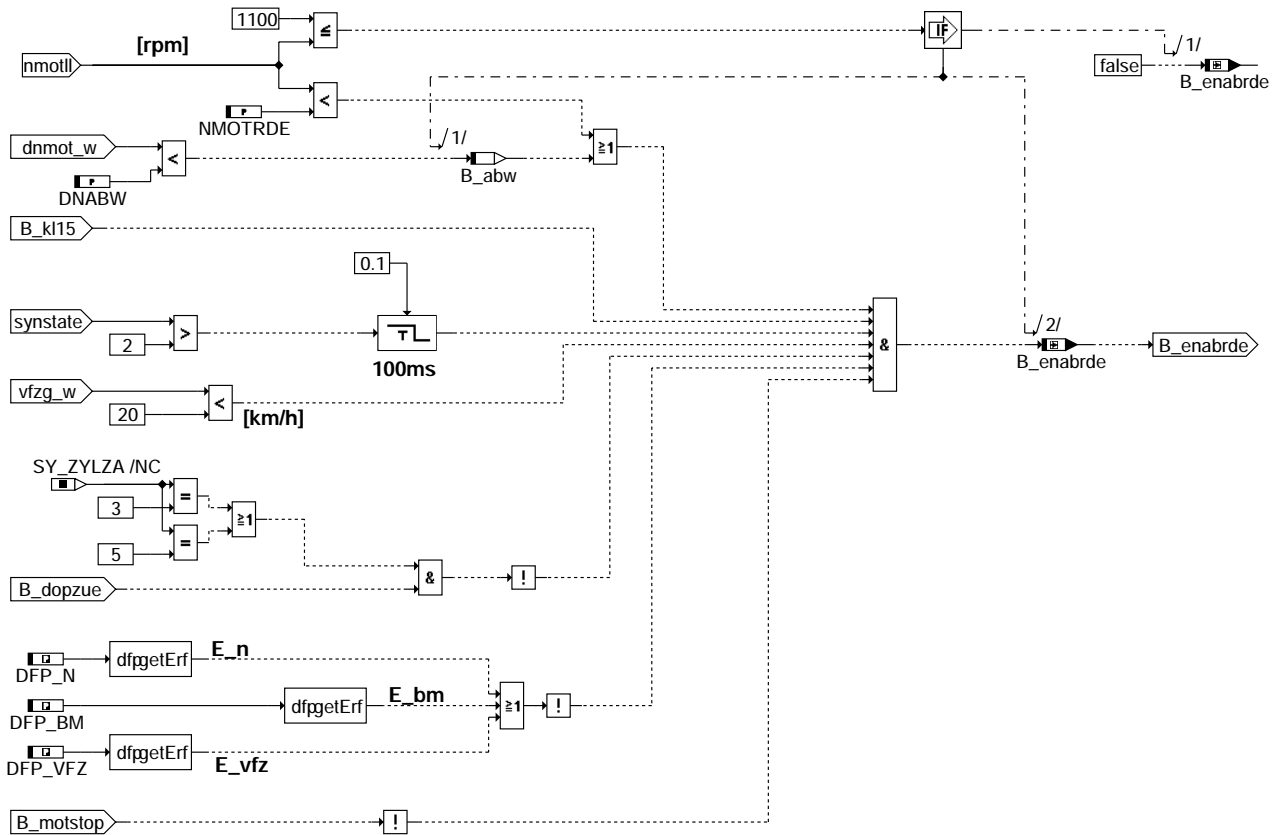


### rde-main

Function overview of turn-back detection

- Enable turn-back detection on the basis of various parameters and thresholds
- Check whether the starter is disengaged
- Monitoring the tooth periods
- Plausibility check of the turn-back points found
- Suppression of injections and ignitions

## Hierarchy: ENABLE



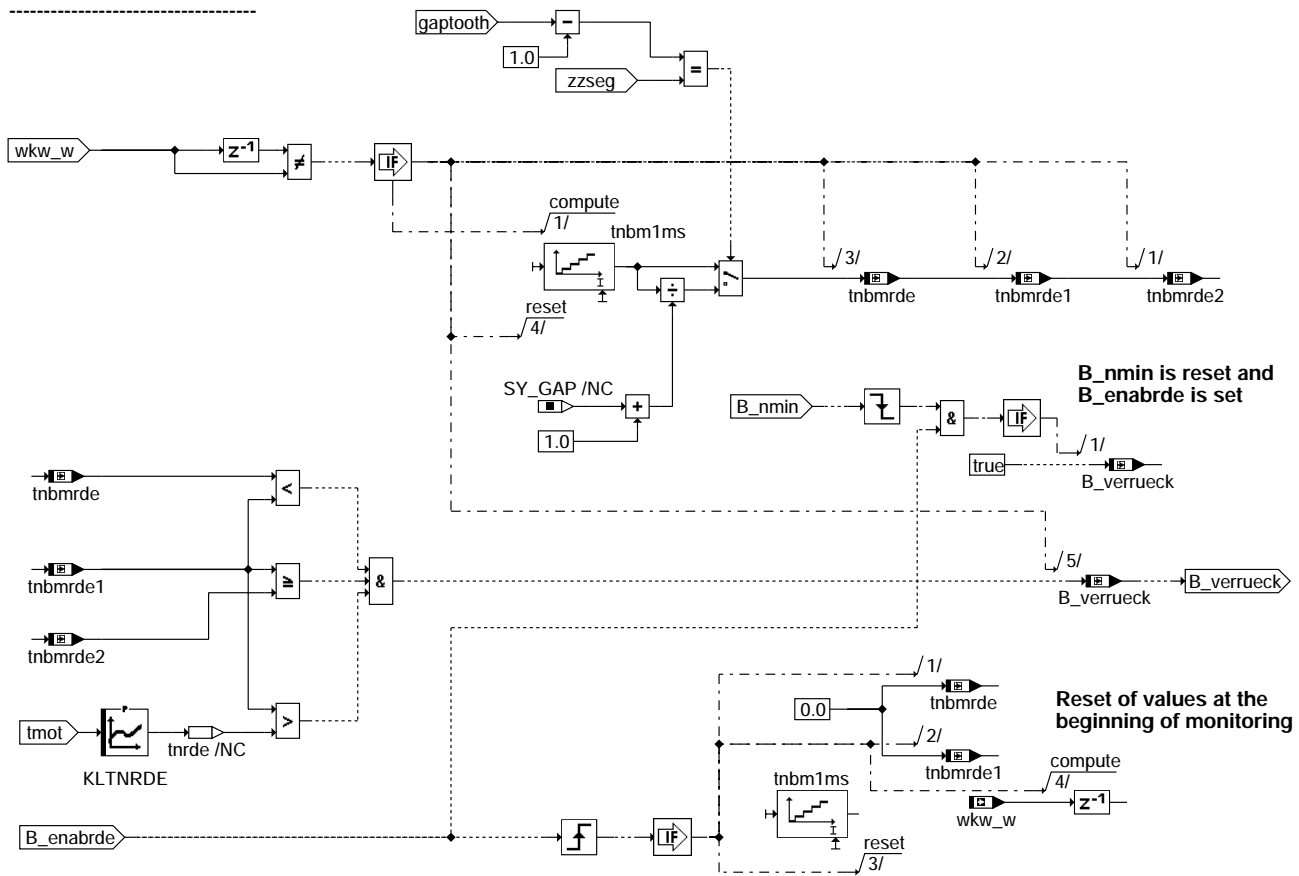
### rde-enable

ENABLE: Enable turn-back detection

The function is only calculated if the speed is less than 1100 RPM. The bit **B\_enabrde** is otherwise set to FALSE. A further speed condition must be fulfilled so that **B\_enabrde** will be set. The function is enabled when the speed is below the threshold **NMOTRDE** (less than the idle speed) or there are large negative speed dynamics (quick stalling of the engine). In this case, the condition **B\_abw** is set if **dnmot\_w** is less than the threshold **DNABW**.

The function only runs at key ON (terminal 15) and when the engine is in synchronization. The function will continue running for 100 ms after synchronization has been lost (detection of turn back and underspeed exit).

## Hierarchy: TNMONITOR



### rde-tnmonitor

TNMONITOR: Monitoring the tooth periods

A counter is incremented in the 1-ms schedule as long as there is no tooth interrupt. The three most recent values are temporarily stored in a shift register. If the value `tnbmrde1` exceeds an absolute value and if the condition:

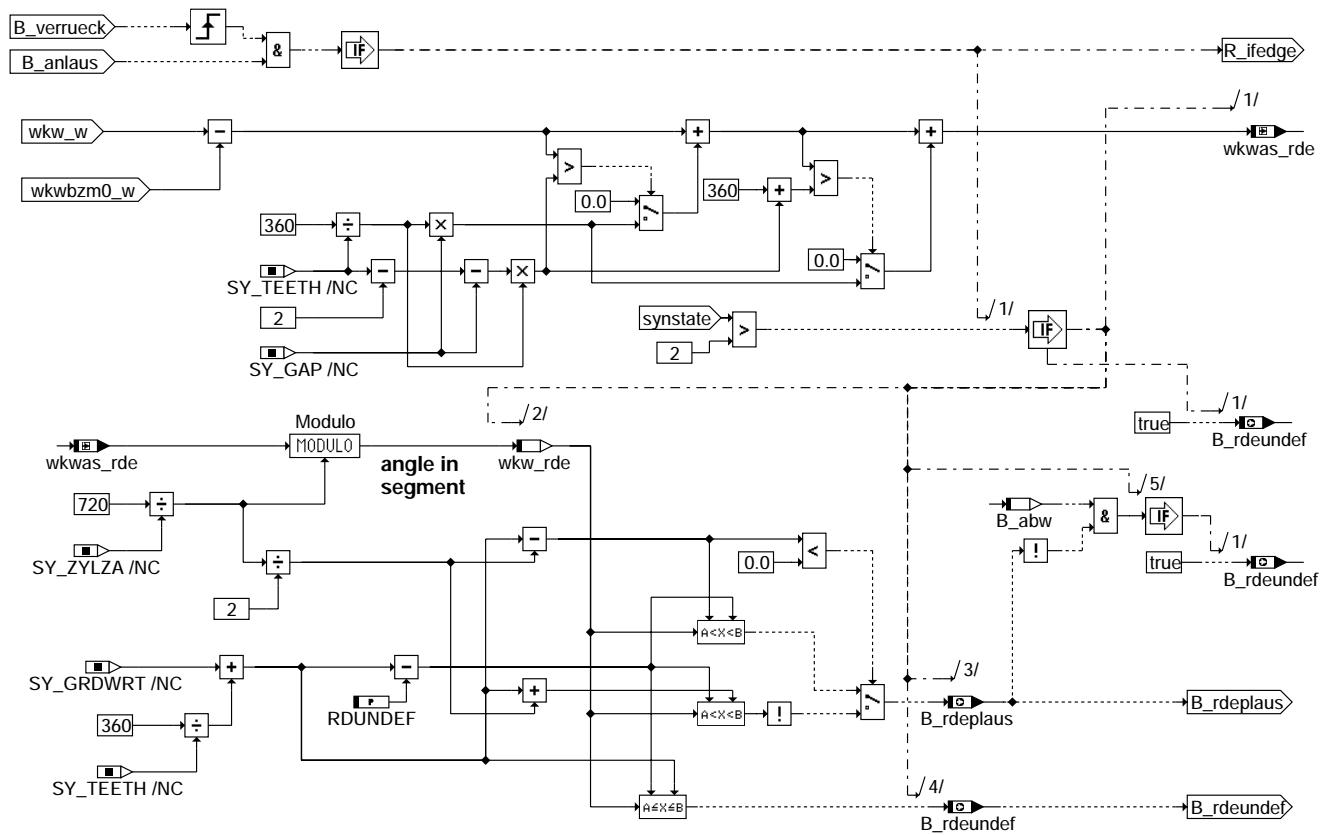
$$\text{tnbmrde} < \text{tnbmrde1} \geq \text{tnbmrde2} \quad \text{also applies, then the condition of suspected turn-back is set.}$$

The two most recent values from the shift register are initialized when tooth-time monitoring has been enabled by `B_enabrde`. The calculation of the tooth periods is only executed in synchronized operation (`synstate = 3`).

The turn-back tooth period is saved over a `tmot`-dependent characteristic curve. The tooth periods in the compression phase are longer at low temperatures because of the higher friction.

If `B_nmin` is reset when `B_enabrde` is still set, then the condition `B_verrueck` is also set.

## Hierarchy: RDE\_PLAUS



### rde-rde-plaus

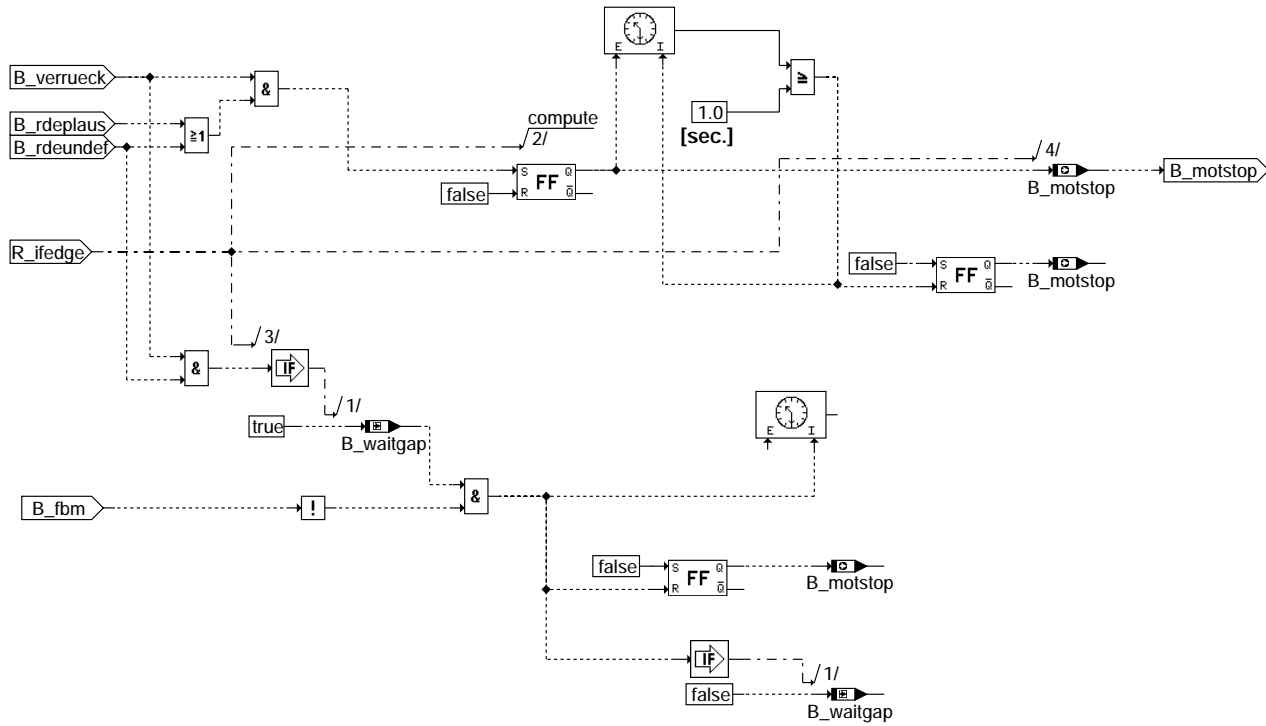
RDE\_PLAUS: Plausibility check of the turn-back point

When a potential turn-back point has been found ( $B\_verrueck$ ), then the angle in the working cycle ( $wkwas\_rde$ ) is first of all calculated using the gap correction. It is determined on the basis of  $wkwas\_rde$  whether the engine is in a compression phase at this angle or is just before the ITDC. Two conditions are deduced from this:

- $B\_rdeplaus$ : Possible turn-back in a plausible turn-back range
- $B\_rdeundef$ : No statement is possible whether the tooth periods come from a turn-back

The condition  $B\_rdeundef$  is set if the possible turn-back point does not lie in a plausible range yet the condition  $B\_abw$  is set. A plausibility check of the position of the turn-back point is only executed for synchronized operation. The condition  $B\_rdeundef$  is set without a plausibility check if there is no synchronization.

## Hierarchy: MOTSTOP



### rde-motstop

MOTSTOP: Suppression of injections and ignitions

The condition B\_motstop is set and a timer s started when turn-back has been detected (B\_verrueck and (B\_rdeplaus or B\_rdeundef)). There is no further output of injections or ignitions when the condition B\_motstop is set. The condition is canceled when the timer reaches a value of 1000 ms.

Provided the following gap check was successful, the condition is canceled before the 1000 ms elapse if B\_motstop has been set by B\_rdeundef.

### ABK RDE 1.40 Abbreviations

RDE: Turn-back detection

Parameter	Source-X	Source-Y	Type	Description
DNABW			FW	engine speed difference at engine stall
KLNRDE	TMOT		KL	characteristic for tooth times at reverse rotation
NMOTRDE			FW	engine speed threshold to release function RDE
RDUNDEF			FW	angle range within there is no validity of the reverse detection
SY_GAP			SYS (REF)	system constant: number of missing teeth in the gap
SY_GRDWRT			SYS (REF)	System constant basic value, space between SW reference mark to OT in ° KW
SY_KL50			SYS (REF)	System constant: information available in the ECU if starter is cranking
SY_TEETH			SYS (REF)	system constant: number of teeth at the crankshaft wheel (gapteeth included)
SY_ZYLZA			SYS (REF)	system constant number of cylinders
UBDTRDE			FW	battery voltage drop for recognizing 'starter cranking'

Variable	Source	Type	Description
B_ABW	RDE	LOK	condition engine stalled
B_ANLAUS	RDE	LOK	Condition for starter disengaged
B_DOPZUE	NLPH	EIN	Condition double ignition
B_ENABRDE	RDE	LOK	Condition for release the function for engine reverse detection
B_FBM	GGDPG	LOK	condition reference mark error => at least 1 tooth too few/many
B_KL15		EIN	condition ignition switch on
B_KL50		EIN	Condition clamp 50
B_MOTSTOP	RDE	AUS	Condition to abort injection and ignition for a definite time
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_RDEPLAUS	RDE	AUS	Condition: reverse rotation is plausible
B_RDEUNDEF	RDE	AUS	Condition: there is no validity for of a reverse rotation
B_VERRUECK	RDE	LOK	Condition: suspect of engine reverse rotation
B_WAITGAP	RDE	LOK	condition: waiting for the next gap check at RDE
DFP_BM	RDE	DOK	ECU int. fault path no.: reference mark
DFP_N	RDE	DOK	ECU int. fault path no.: engine speed sensor



Variable	Source	Type	Description
DFP_VFZ	RDE	DOK	ECU int. fault path no.: vehicle speed signal
DNMOT_W	BGNG	EIN	engine speed difference between two following segments
E_BM	DDG	EIN	error flag: reference mark sensor
E_N	DDG	EIN	error flag: engine speed sensor
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
GAPTOOTH	GGDPG	EIN	content of the tooth counter to check the gap
NMOTLL	BGNMOT	EIN	engine speed
SYNSTATE		EIN	current mode of synchronization
TMOT	SWADAP	EIN	Engine temperature
TNBMRDE	RDE	LOK	Tooth periode of the last nbm signal (at 1ms schedule)
TNBMRDE1	RDE	LOK	Tooth periode of the second to last nbm signal (at 1ms schedule)
TNBMRDE2	RDE	LOK	Tooth period of the third to last nbm signal (at 1ms schedule)
UB	SWADAP	EIN	battery voltage
UBRDE	RDE	LOK	Threshold for battery voltage to detect starter disengaged
VFZG_W	GGVFZG	EIN	Vehicle speed
WKWAS_RDE	RDE	LOK	Corrected angle at working cycle for RDE
WKWBZM0_W	GGDPG	EIN	crank angle at the zero point of the working cycle: R_syn & zzyl = 0 (word)
WKW_W	GGDPG	EIN	crank angle (word)
WUB		EIN	battery voltage; scanned value of ADC
ZZSEG	GGDPG	EIN	tooth counter in segment

### FW RDE 1.40 Fixed Values

Parameter	Value	Description
DNABW		engine speed difference at engine stall
NMOTRDE		engine speed threshold to release function RDE
RDUNDEF		angle range within there is no validity of the reverse detection
UBDTRDE		battery voltage drop for recognizing 'starter cranking'

### FB RDE 1.40 Detailed description of function

#### 1. Enable turn-back detection

=====

Any turn-back by the engine can only take place at a low speed or when at a standstill. It is no longer necessary to calculate the function above 1100 1/min. Furthermore, synchronization must have occurred based on the reference mark because it is only as of here that the gap information is available. Monitoring is not necessary if there is no synchronization because neither injections nor ignitions are outputted. So as to be able to detect a turn-back point with subsequent underspeed exit however, the function still has to be calculated 100 ms after loss of synchronization.

In the normal case, it is sufficient to calculate the function at speeds below the idle speed. If the engine stalls very quickly however, then the speed cannot be updated sufficiently quickly (speed determined over one segment). The function is therefore also enabled if a large negative speed gradient is given at speeds lower than 1100 RPM.

The vehicle speed must be less than 20 km/h so as not to falsely detect turn-back in there is interference in the speed-sensor signal.

Neither is there any turn-back detection for 3 and 5-cylinder engines if the phase position is not known (engine is running with double ignition output). If the phase position is not determined in engines with an odd number of cylinders, then it is not possible to check the plausibility of the turn-back angle.

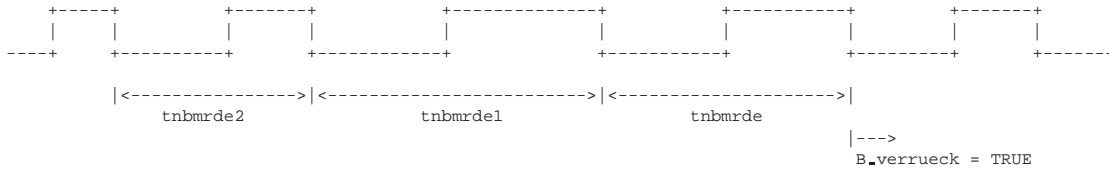
Also, there is no turn-back detection executed if there is an error in the speed-sensor signal. The function is disabled as well if an error is determined in the vehicle speed.

#### 2. Monitoring the tooth period

=====

There is no longer any tooth interrupt in the ECU during synchronized operation. The hardware counter, *wkw\_w*, is therefore monitored in the 1-ms schedule for monitoring the tooth period. The number of 1-ms frames is incremented by a counter as long as the value for *wkw\_w* does not change. This time has to be converted to a standard tooth period at the gap. The most recent tooth periods are stored temporarily in a shift register.

Usual course for the signal (nbm) at the turn-back point:



The condition for a suspected turn-back is set when the following requirements are met:

$$tnbmrde2 \leq tnbmrde1 > tnbmrde \quad \text{and} \quad tnbmrde1 > KLTNRDE(tmot)$$

If the tooth period at the turn-back point is greater than 50 ms, then underspeed exit follows (synchronization is canceled). Also, the condition B\_verrueck is set if the condition B\_nmin is set again within 100 ms after abort of the synchronization.

### 3. Plausibility check of the turn-back point =====

There is no plausibility check executed for the turn-back range if it is detected that the starter motor has engaged. It is assumed in this case that the engine cannot turn back if the starter has disengaged.

If the B\_kl50 is available in the system for the starter, then this condition will be inquired. If the condition is not available in the system, then the battery voltage is evaluated accordingly in order to detect whether the starter has engaged. A battery-voltage threshold is defined in the initialization, C\_ini, for this:  $ubrde = wub - UBDTRDE$ . A maximum selection is executed (plausibility check) and  $ubrde = 10 \text{ V}$  is set if the threshold is less than 10 V.

Correction of the angle  $wkw\_w - wkwzbm0\_w$  by the teeth missing in the gap. If the angle is after the first gap, then the correction angle is added to the missing teeth. If the position for this is after the second gap, then this angle is added a second time.

The current crankshaft angle  $wkwas\_rde$  is checked for a plausible turn-back range by the condition B\_verrueck. The engine is in a plausible range when, to within half a segment in front of the ITDC, the piston is in the cylinder undergoing compression. The condition is therefore given for the plausible turn-back range:

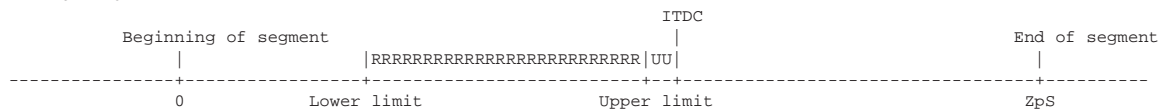
B\_rdeplaus            lower limit < angle in the segment < upper limit

where:    lower limit =  $SY\_GRDWRT + 1 \text{ tooth increment} - \text{segment}/2$     ==>  $tnbmrde1$  for segment/2 in front of ITDC  
           upper limit =  $SY\_GRDWRT + 1 \text{ tooth increment} - RDUNDEF$         ==>  $tnbmrde1$  at ITDC - fixed value

If the corresponding tooth periods occur directly in front of or at the ITDC, then no information can be obtained whether the engine is turning back or is still running over the TDC, and hence continues to turn in the forwards direction. The condition B\_rdeundef is set in this case.

The following 2 cases are given for the lower limit since the tooth in the segment is always  $\geq 0$ :

#### 1. Lower limit $\geq 0$ :



#### 2. Lower limit < 0:



RRRR = Plausible turn-back range  
UU = Undefined range

If the engine stalls quickly (B\_abw = TRUE), then turn-back can take place at any engine position because of the high kinetic energy in the powertrain. The condition B\_rdeundef is therefore always set in this case.

The condition B\_rdeundef is also set during non-synchronized operation since no plausibility check is possible in this case.







## ABK KVA 36.10 Abbreviations

## FW KVA 36.10 Fixed Values

Parameter	Value	Description
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## FB KVA 36.10 Detailed description of function

## APP KVA 36.10 Application hint

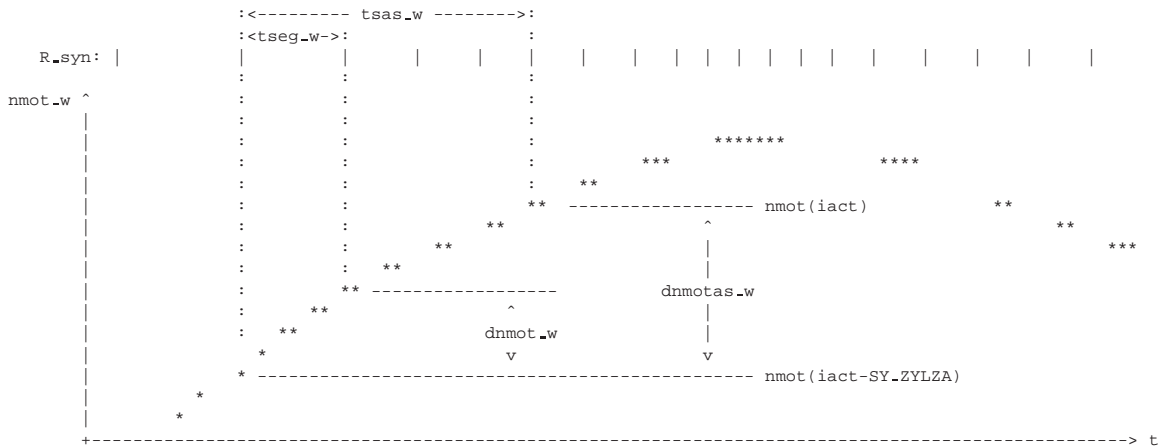
## BGNG 5.20 Calculated variable: engine-speed gradient

### FDEF BGNG 5.20 Function definition

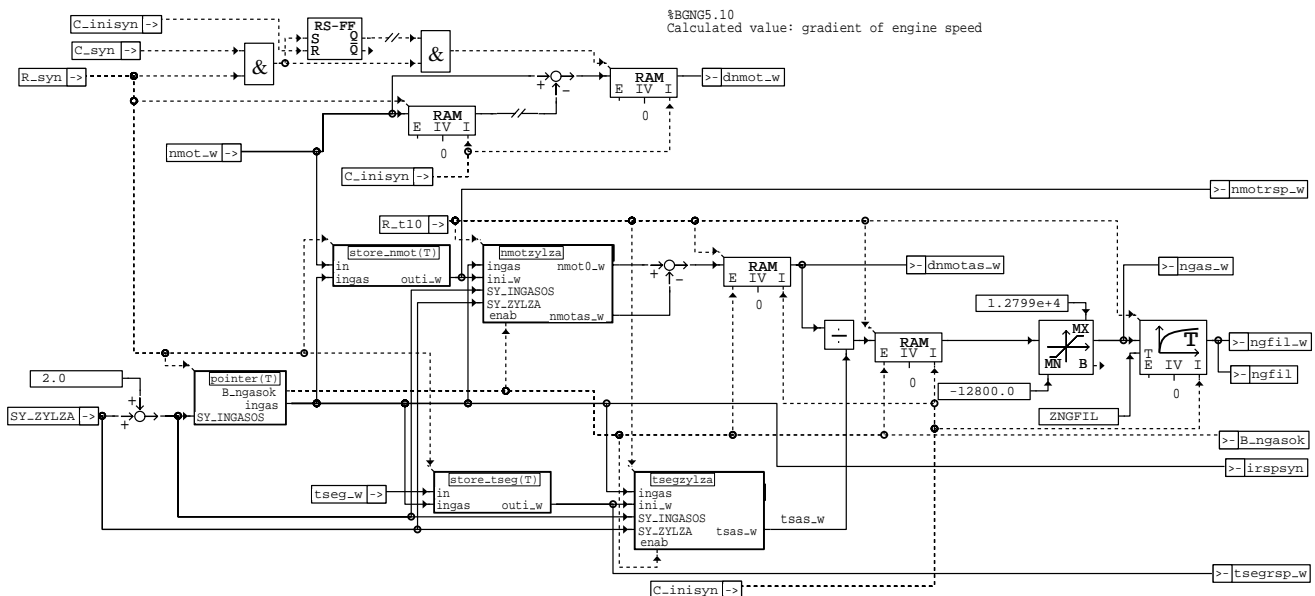
The function %BGNG calculates the following values:

- **dnmot\_w**: The engine speed gradient over one segment, calculated in the synchro schedule  
 $dnmot\_w = nmot(iact) - nmot(iact-1)$
- **dnmotas\_w**: Differenz in engine speed over one engine cycle, calculated in the 10 ms schedule  
 $dnmotas\_w = nmot\_w(iact) - nmot\_w(iact-SY\_ZYLZA)$ .  
The required engine speed values  $nmot\_w(i)$  are stored in a memory array in the synchro schedule.
- **tsas\_w**: Time for one engine cycle:  
 $tsas\_w = \text{Summe}(tseg\_w(i), i=1, SY\_ZYLZA)$ .  
The required segment time values  $tseg\_w(i)$  are stored in a memory array in the synchro schedule.
- **ngas\_w**: Engine speed gradient over one engine cycle, calculated in the 10 ms schedule  
 $ngas\_w = dnmotas\_w / tsas\_w$ .
- **ngfil\_w**: Engine speed gradient  $ngas\_w$ , filtered with the time constant ZNGFIL.

Engine speed gradient at a 4 cylinder engine: SY\_ZYLZA = 4



Overview of engine speed gradient calculation:

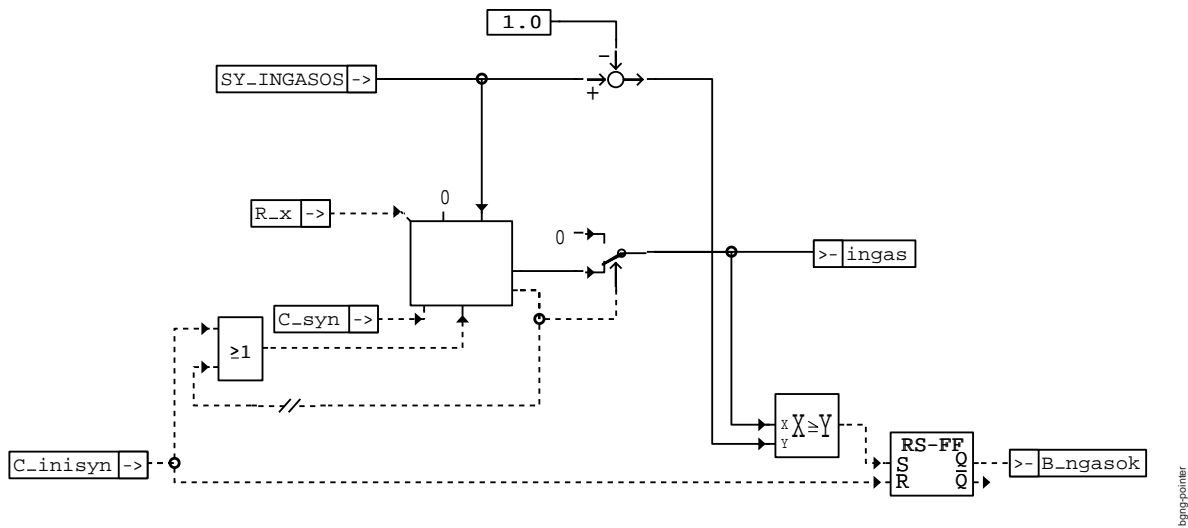


bgng-bgng

bgng-bgng

Pointer for the engine speed and segment time memory array:

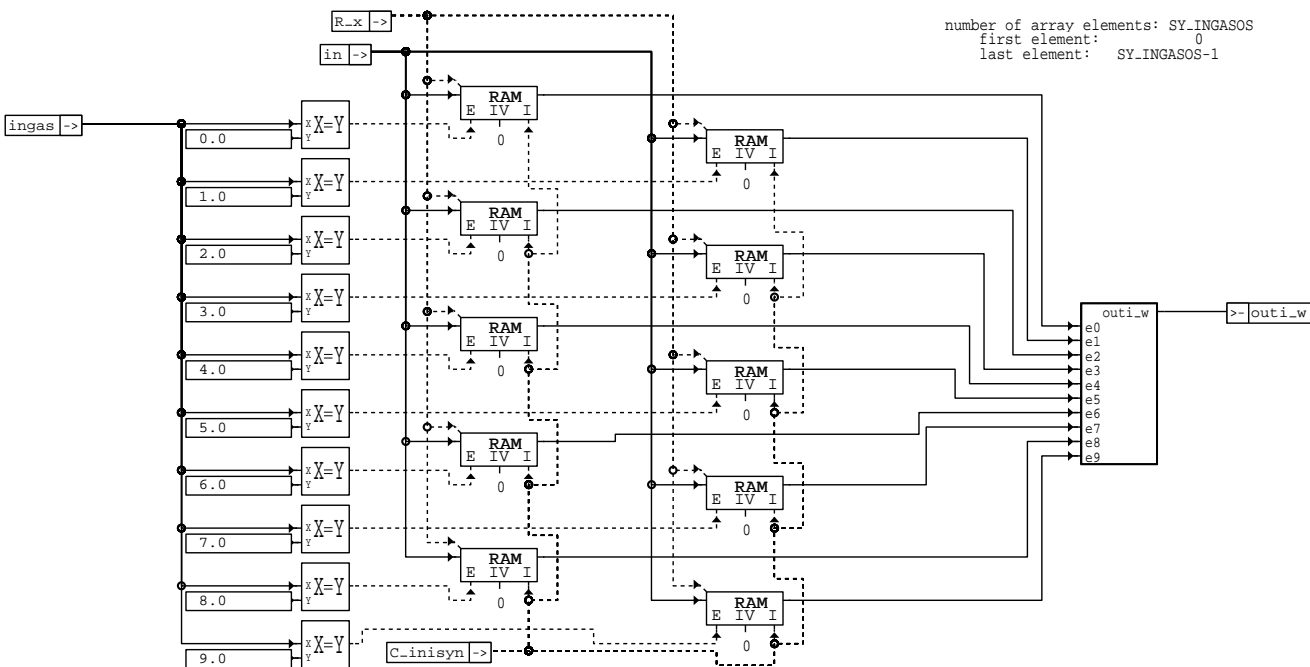
The array contains  $SY\_INGASOS = SY\_ZYLZA + 2$  values to prevent overwriting during the calculation in the 10 ms schedule by a synchro interrupt. B\_ngasok enables the calculation of the values over the engine cycle.



### bgng-pointer

Storing the segment times in the synchro schedule:

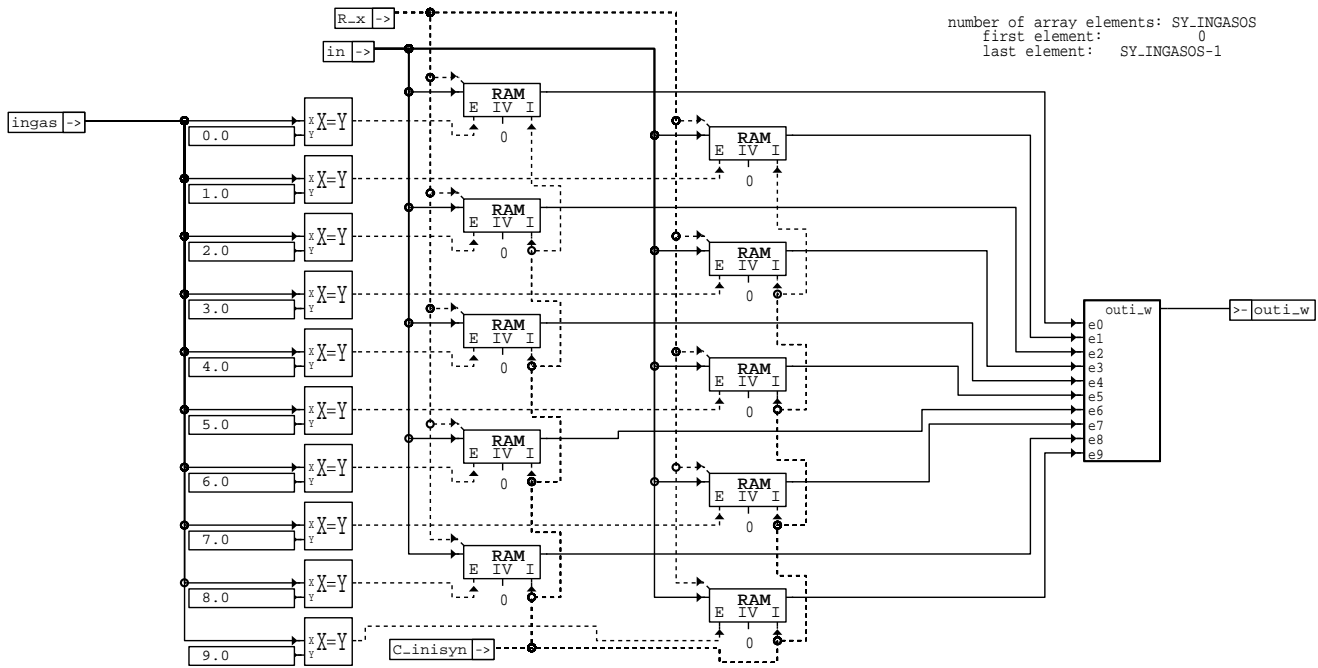
The array is filled dependand on SY\_ZYLZA with maximum SY\_INGASOS values.



### bgng-store-tseg

Storing the engine speed values in the synchro schedule:

The array is filled dependand on SY\_ZYLZA with maximum SY\_INGASOS values.



**bgng-store-nmot**

**ABK BGNG 5.20 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
ZNGFIL			FW	time constant for engine gradient filter
<b>Variable</b>	<b>Source</b>		<b>Type</b>	<b>Description</b>
B_NGASOK	BGNG		AUS	condition memory array for ngas calculation valid
C_INISYN			EIN	ECU-condition for intialisation of angle synchronization
C_SYN			EIN	ECU-condition angle synchronization available
DNMOTAS_W	BGNG		AUS	engine speed difference during one working cycle
DNMOT_W	BGNG		AUS	engine speed difference between two following segments
INGAS	BGNG		LOK	Memory array pointer for engine speed gradient calculation over the engine cycle
IRSPSYN	BGNG		AUS	index to address memory of tsegrsp_w, nmotrsp_w, rsp_w
NGAS_W	BGNG		AUS	engine speed gradient during one working cycle
NGFIL	BGNG		AUS	filtered engine-speed gradient
NGFIL_W	BGNG		AUS	filtered engine-speed gradient
NMOTRSP_W	BGNG		AUS	Start Ring buffer for rpm value
NMOT_W	SWADAP		EIN	engine speed
R_SYN	GGDPG		EIN	Synchro schedule
R_T10			EIN	Time schedule 10 ms
SY_INGASOS	BGNG		LOK	system constant size of the memory array for engine speed gradient calculation
SY_ZYLZA	PROKON		EIN	system constant number of cylinders
TSAS_W	BGNG		LOK	time during one working cycle for ngas_w
TSEGRSP_W	BGNG		AUS	Begin of ring buffer for segment time
TSEG_W	BGNMOT		EIN	segment cycle time

**FW BGNG 5.20 Fixed Values**

Parameter	Value	Description
ZNGFIL		time constant for engine gradient filter

**FB BGNG 5.20 Detailed description of function**

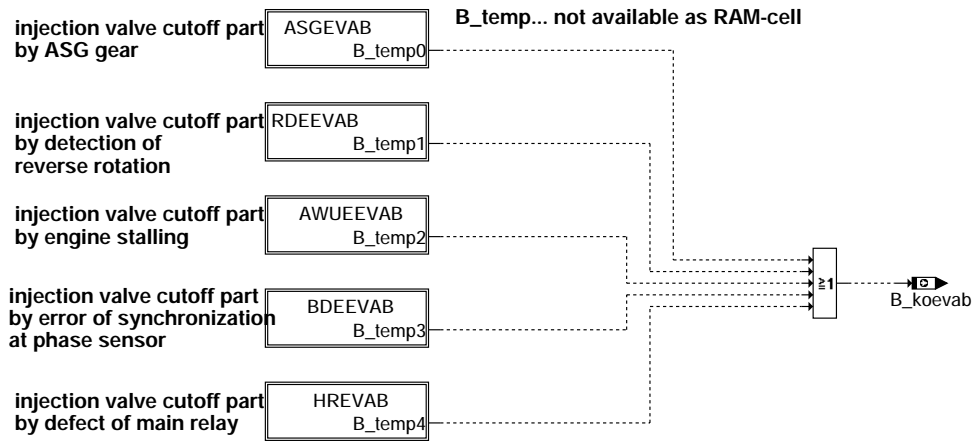
**APP BGNG 5.20 Application hint**

Recommendation for first application:

ZNGFIL = 50 ms

## KOEVAB 1.20 coordination of injection valve cutoff

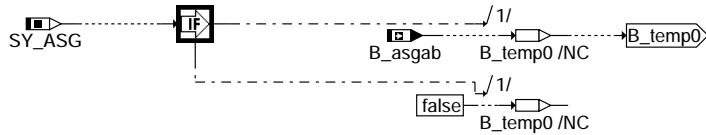
### FDEF KOEVAB 1.20 Function definition KOEVAB 1.20



#### koevab-main

Injection valve cutoff by Automatic Gear Box (AGB/ASG)

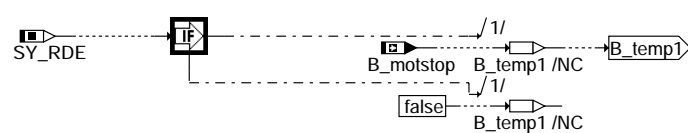
#### injection valve cutoff part by ASG gear



#### koevab-asgevab

Injection valve cutoff after recognized backward rotation during engine coasting

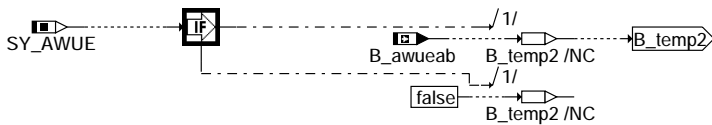
#### injection valve cutoff part by detection of reverse rotation



#### koevab-rdeevab

Injection valve cutoff after recognized engine stalling

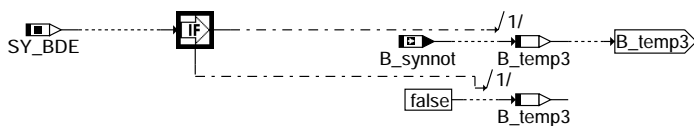
#### injection valve cutoff part by engine stalling



#### koevab-awueevab

Ev Disconnection because of lost synchronization on BDE systems

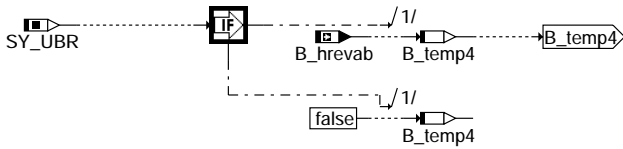
#### injection valve cutoff part by error of synchronization at phase sensor



#### koevab-bdeevab

Injection valve cutoff after recognized main relay error

### injection valve cutoff part by defect of main relay



koevab-hrevab

### ABK KOEVAB 1.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SY_ASG			SYS (REF)	automatic standard transmission
SY_AWUE			SYS (REF)	injection valve cutoff possible by function AWUE
SY_BDE			SYS (REF)	system constant GDI
SY_RDE			SYS (REF)	detection of reverse rotation of the engine in project included
SY_UBR			SYS (REF)	system constant: Voltage behind main relay ubr exists

Variable	Source	Type	Description
B_ASGAB	DVKUP	EIN	Engine shut off by ASG
B_AWUEAB		EIN	injection valve cutoff active by function AWUE
B_HREVAB		EIN	demand injection valve cutoff at error of main relay
B_KOEVAB	KOEVAB	AUS	injection valve cutoff active by function KOEVAB
B_MOTSTOP	RDE	EIN	Condition to abort injection and ignition for a definite time
B_SYNNOT		EIN	Prohibits injection if phase synchronization could not be detected

### FW KOEVAB 1.20 Fixed Values

Parameter	Value	Description

### FB KOEVAB 1.20 Detailed description of function

The function Co-ordination of injection valve cutoff (KOEVAB) links the individual interventions which result in a complete injection valve cutoff.  
The system constant value activates the respective intervention. To ensure this, the system constant values must be specified in the section PROKON.  
The individual interventions are linked together by a logical OR operation; this means: if one of the interventions is active (B...), the value B.koevab is set true. This causes the function AEVABZK to cutoff all injection valves commanded by the respective Motronic control device.

### APP KOEVAB 1.20 Application hint

## WANWKW 13.30 Angle adaptation of alignment between camshaft and crankshaft

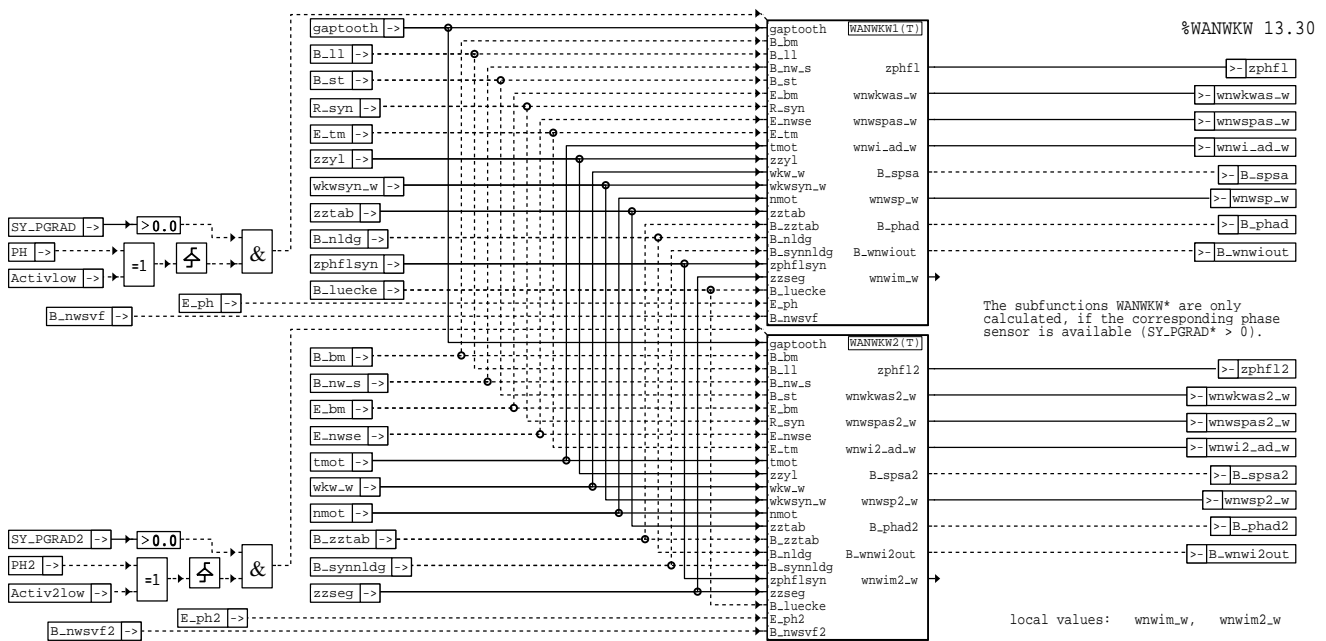
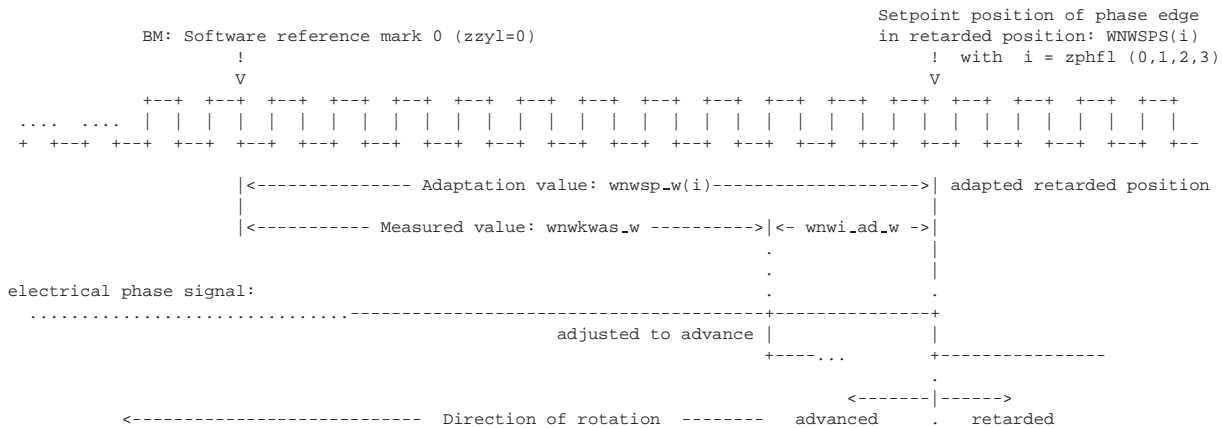
### FDEF WANWKW 13.30 Function definition

Task of the function angle adaptation of alignment between camshaft und crankshaft:

- Determination of the position of the camshaft signal relative to the crankshaft signal in the working cycle: wnwkw\*\_\*w
- Phase edge counter in the working cycle: zphfl\*
- Adaptation of a defined normal position of the camshaft (retarded position) relative to the crankshaft during idling, edge-specific: wnwsp\*\_\*w(i) with i=zphfl\*
- Formation of the deviation between current actual position of the camshaft relative to the adapted position:wnwi\*\_\*ad\_\*w
- Formation of the condition "angle adaptation permissible": B\_\*spsa\*
- Formation of the condition "angle adaptation successful": B\_\*phad\*



Signal assignment, crankshaft - camshaft:



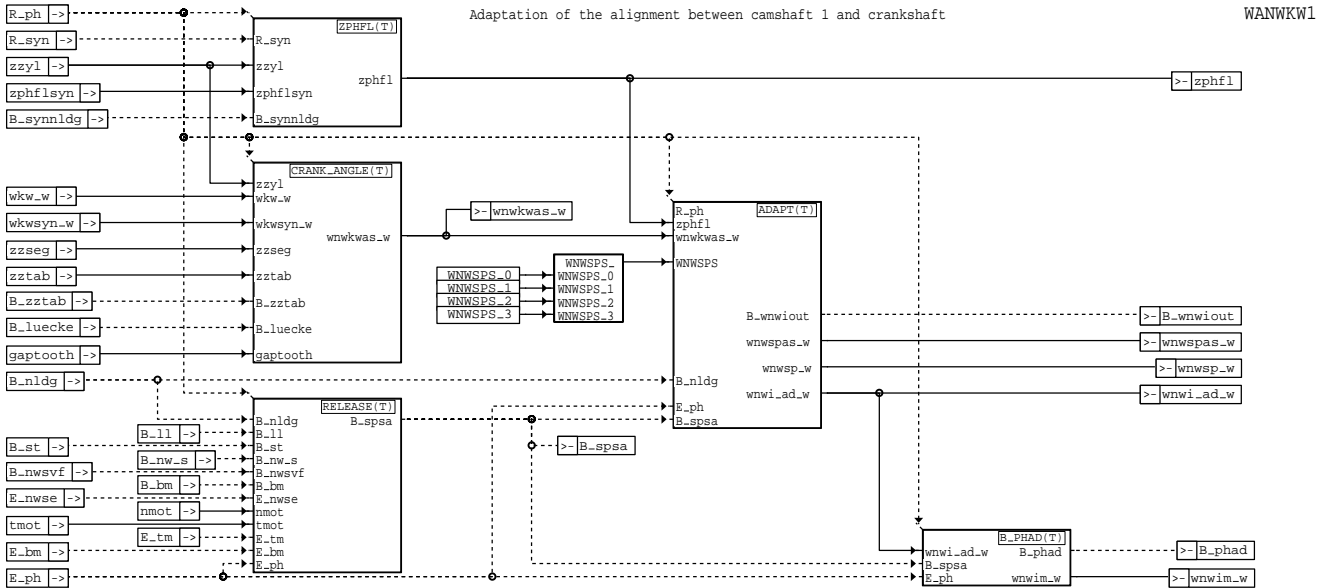
The subfunctions WANWKW\* are only calculated, if the corresponding phase sensor is available (SY\_PGRAD\* > 0).

### wanwk-wanwk

Overview over the angle adaptation:

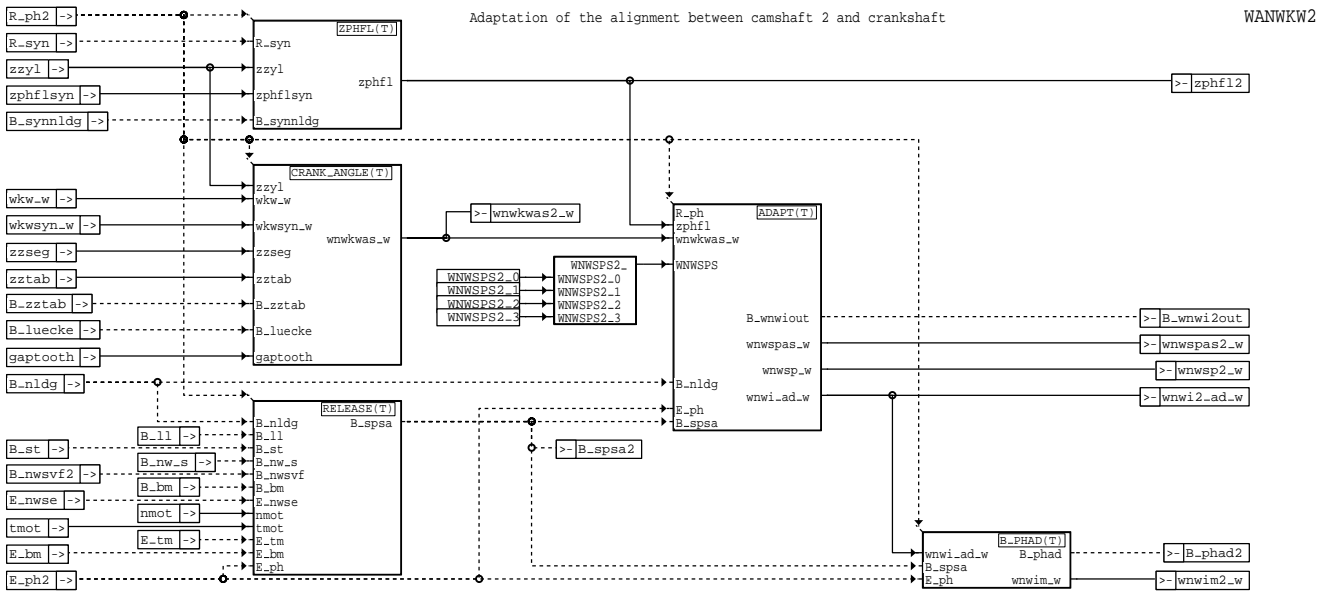
- Representation of the angle adaptation for 2-bank-system (V-engines): WANWKW1, WANWKW2. The adaptation for systems with two banks is calculated separately for both banks. Apart from the output values the subfunctions are identical.
- Deactivation of the one bank WANWKW\* via the system constant SY\_PGRAD\* = 0 (see configuration in %PROKON).
- Activ\*low is used for the hardware shell and defines the phase level at the first reference gap (zzy1 = 0).

WANWKW1: Subfunction for bank 1:



**wanwk-wanwk1**

WANWKW2: Subfunction for bank 2:



**wanwk-wanwk2**

Overview of the subfunctions of the angle adaptation WANWKW\*:

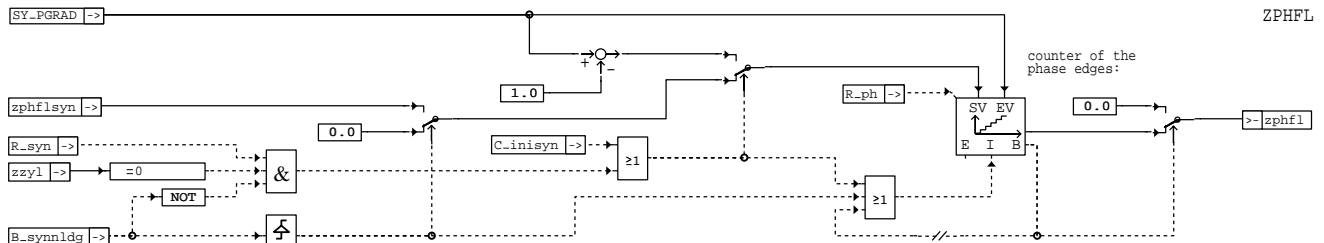
(subfunctions are calculated separately for both banks, \*: wildcard for bank 1 or bank 2)

- ZPHFL: Calculation of the current edge number, values go from zero up to SY\_PGRAD\* - 1: zphfl\*
- CRANK\_ANGLE: Hardware casing for the calculation of the crankshaft angle in the working cycle at the current phase edge (0..720°KW); tooth improvement of the angle by forming the ratio of the current tooth time with regard to the last tooth period tbnm\_w: wnwkwas\*\_w
- ADAPT: Adaptation of the reference position (retard position) of the edges, if the adaptation release is given via B\_spsa\*: wnwsps\*\_w resp. wnwsps\*\_w(zphfl\*); Calculation of the adjustment angle of the camshaft or rather the deviation of the actual angle from the adapted reference angle: wnwi\*\_ad\_w
- RELEASE: Release of the adaptation: B\_spsa\*
- B\_PHAD: Determination "angle adaptation successful": B\_phad\*

ZPHFL: Determination of the counter phase edges:

**zphfl\*:** The phase edge counter zphfl resp. zphfl2 is incremented at the phase interrupts R\_ph\* and synchronized during each working cycle at the reference mark gap 0 (R\_syn & zzyl = 0). In limp-home DG zphfl is initialized after detection of the engine position (B\_synnldg). The synchronization on account of the speed sensor signal at the t-mark (R\_syn & zzyl = 0) should not occur at the speed sensor limp-home. The order of the limp-home extrapolated angular base can be shifted at high dynamic. Therefore the counter could be mis-synchronized.

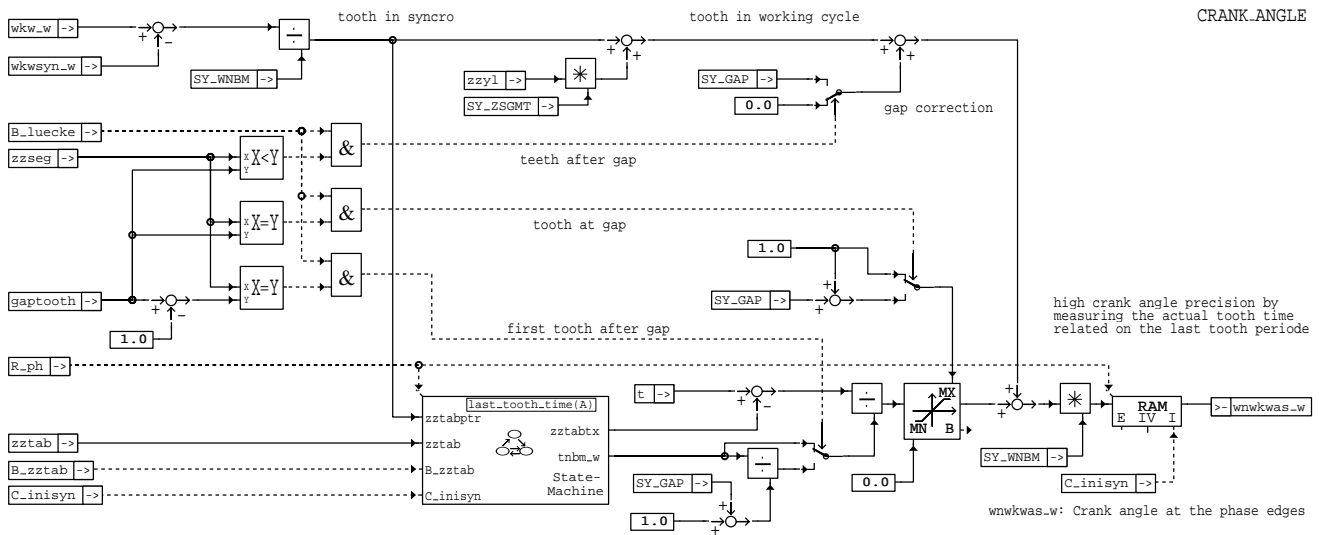
Mode of counting: 0,1,2,3 (max. SY\_PGRAD\* - 1)



wanwkw-zphfl

CRANK\_ANGLE: Determination of the engine position at the phase edges related to the crankshaft reference mark 0 (zzyl=0):

**wanwkwas\*\_w:** The current position of the engine in the working cycle is determined in the phase interrupt R\_ph\*. First, the actual tooth in the working cycle is calculated. Afterwards a tooth improvement is achieved by an evaluation of the tooth period tnm\_w and the time difference between the phase interrupt and the last tooth (t - zztabtx). At the tooth after the gap, the last tooth period is reduced by (1 + SY\_GAP), because this period contains 1 plus the 'missing' teeth. Zero point of the crankshaft angle: Software reference mark at cylinder 1 (R\_syn & zzyl=0). Value range: 0..720 °CKS

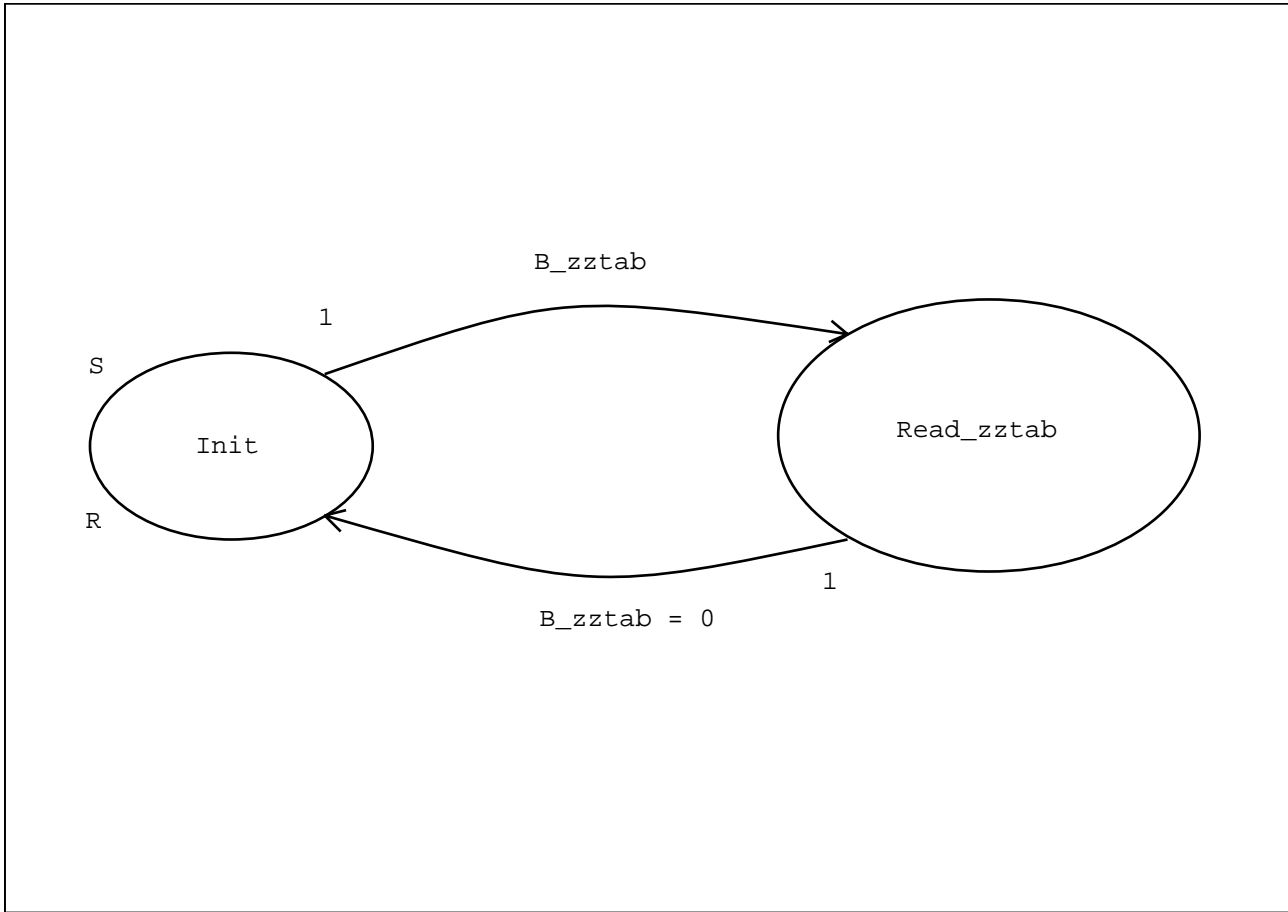


wanwkw-crank-angl

**last\_tooth\_time:** read out of the system time of the tooth before the phase edge and the corresponding phase edge

The State-machine last\_tooth\_time reads the system time of the tooth before the phase edge (zztabtx) and calculates the corresponding tooth period out of the tooth time table. Both values are read out if the condition B\_zztab is TRUE.

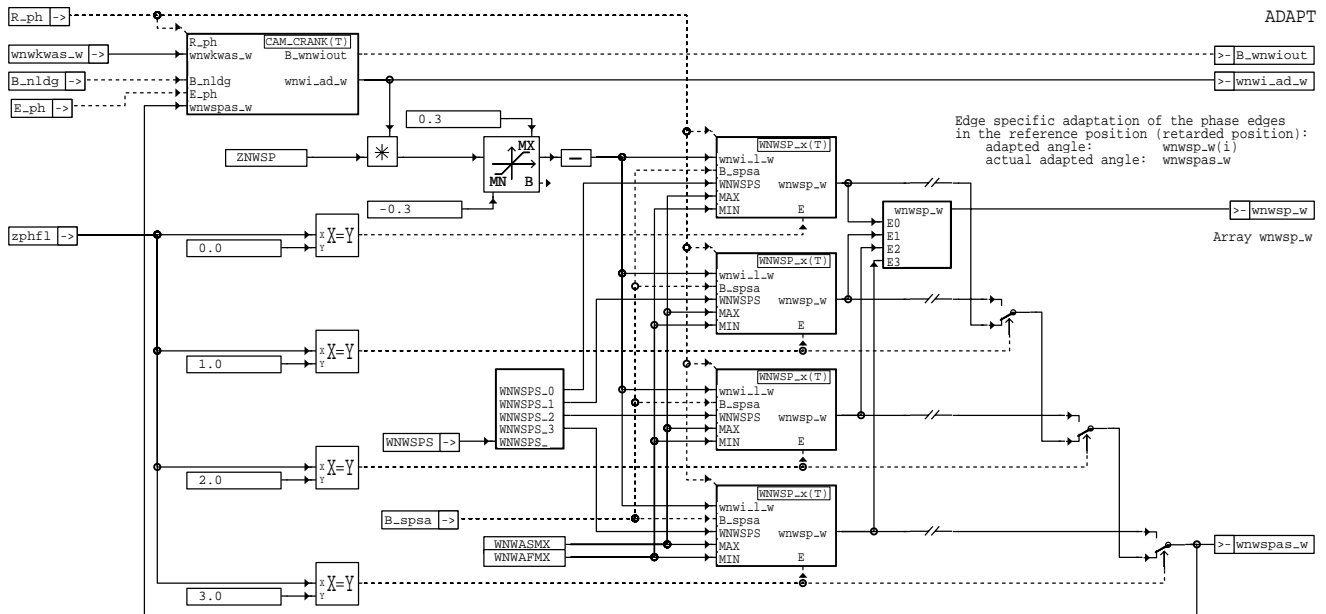




**wanwkw-last-tooth**

ADAPT: Adaptation of the edge-specific reference position (retard position) in the working cycle:

wnwsp\*\_w(i): Adaptation of phase edge i. Value range: 0 .. 720°CKS, zero point as wnwkw\*\_w  
WNWSP\*\_i Initialization of wnwsp\*\_w(i) in case of powerfail (C\_pwf) resp. "delete fault memory" (C\_fmclr)



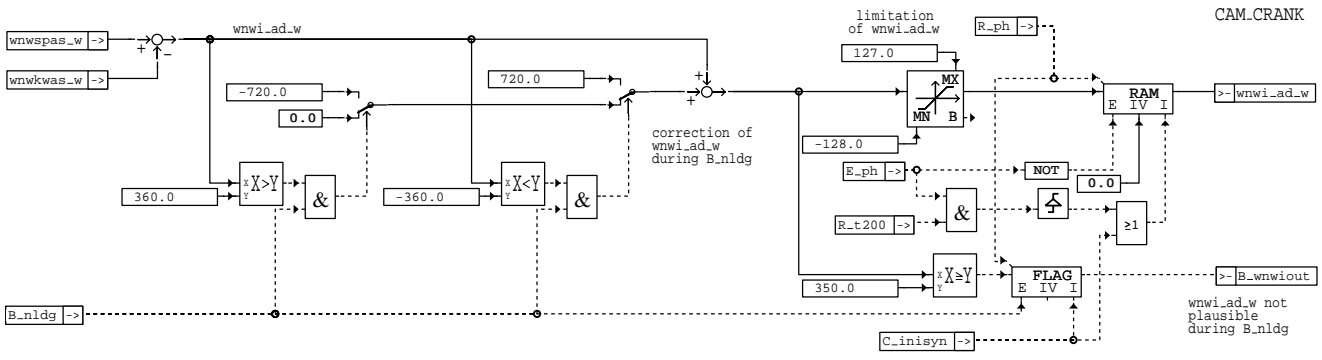
**wanwkw-adapt**

The angle deviations  $wnwi\_ad\_w$ , weighted with  $ZNWS$ , are integrated during the adaptation ( $B\_spsa^* = 1$ ) at the corresponding phase edge  $zphfl^*$  in the accumulators  $wnwsp^*_w(i)$  with  $i = zphfl^*$ . With decreasing angle deviation the edge-specific adaptation values  $wnwsp^*_w(i)$  stabilize. The last adaptation value is made available to the subfunction  $CAM\_CRANK$  via the value  $wnwspas^*_w$  for the calculation of the current  $wnwi\_ad\_w$ .

All subfunctions  $WNWS$  are identical and therefore only once described

**CAM\_CRANK:** Determination of the angle deviation of the current angle position of the CMS edges to the adapted reference value:

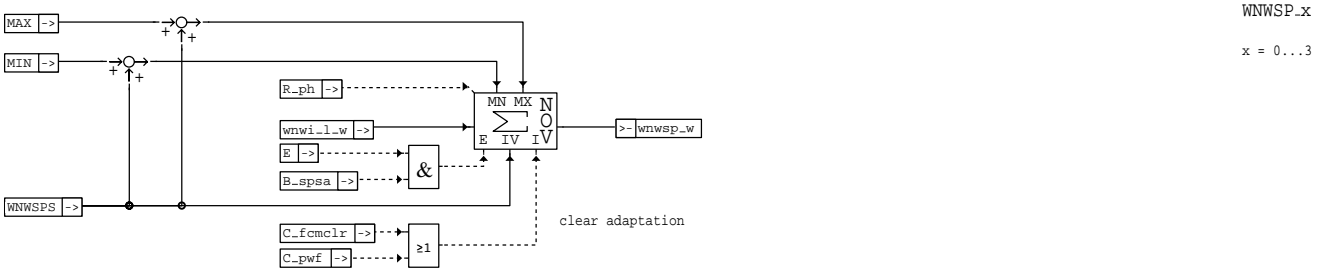
**wnwi\_ad\_w:** Difference between adapted value of the current phase edge  $wnwspas^*_w$  and the actual position  $wnwkwas^*_w$ . In  $limphome$  DG,  $wnwi\_ad\_w$  may have an overflow of one working cycle ( $720^\circ$ CKS), which is corrected. If the difference after this correction is still too high, the condition  $B\_wnwiout$  is set. Value range:  $-128 \dots 128^\circ$ CKS



**wanwk-cam-crank**

**WNWSP\_x:** Accumulator to integrate the angle deviation  $wnwi\_ad\_w$

All subfunctions  $WNWS$  are identical and are illustrated only once in the following definition.



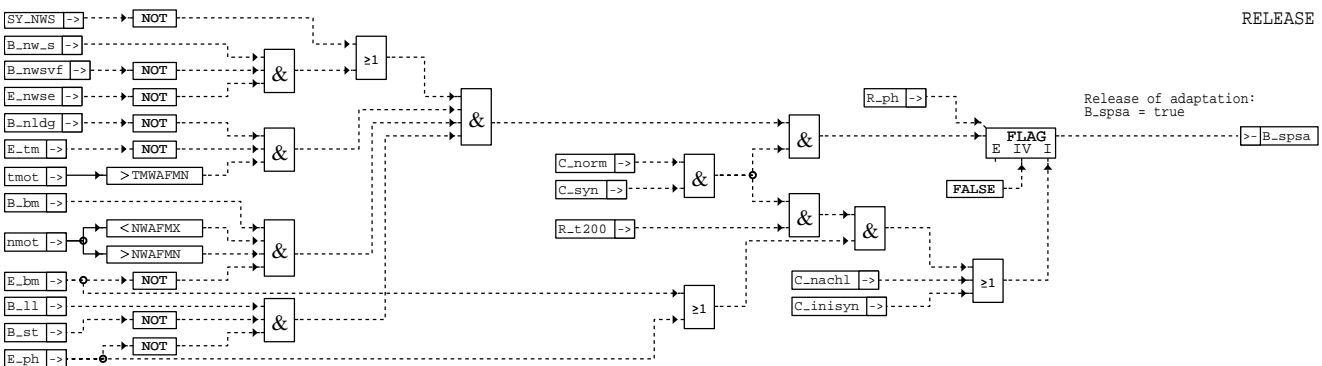
**wankw-wnwsp-x**

Via the enable-input  $E$ , the adaptation is released at the actual phase edge ( $zphfl^* = i$ ). The angle deviation  $wnwi\_ad\_w$  is added up to the limitation of the accumulator  $WNWS$  +  $MIN$ ,  $WNWS$  +  $MAX$ . So  $WNWS\_x$  is an integrator for the angle deviation at the phase edge  $i$ .

The adapted value is initialized to the nominal phase edge  $WNWS$  at powerfail ( $C\_pwf$ ) and at clearing the error flags ( $C\_fcmclr$ ).

**RELEASE:** Release of the adaptation

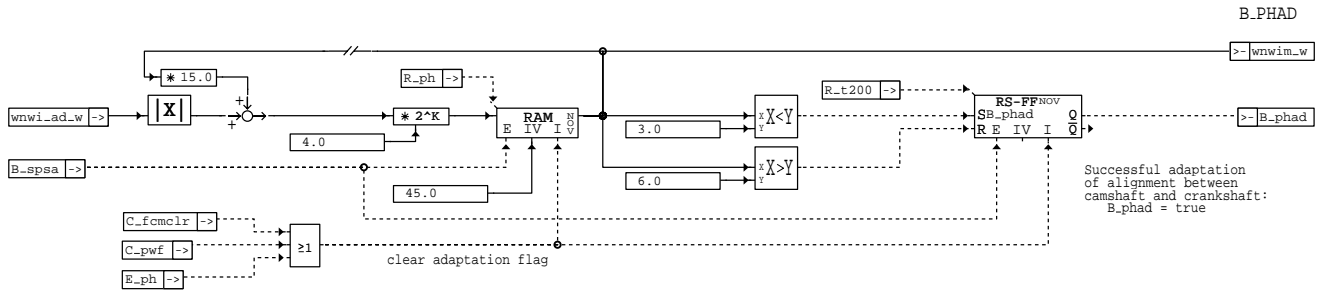
Dependent on the following illustrated conditions the adaptation is released via the condition  $B\_spsa^*$ .



**wankw-release**

**B.PHAD: Condition "adaptation successful"**

The adaptation is considered to be successful (B\_phad\*=true) if the amount of the floating average value of wnw\_i\*\_ad\_w in wnwim\*\_w remains under a lower threshold value (3°). If an upper threshold value (6°) is exceeded the condition B\_phad\* is reset again. An error on the phase signal (E\_ph\*) or deleting the adaptation values (C\_pwf or C\_fcmclr) also lead to the condition B\_phad\* being reset.



**wanwk-w-b-phad**

**ABK WANWKW 13.30 Abbreviations**

- BM reference gap
- BM0 reference gap at cylinder 1 (zzyl = 0)
- \* wildcard for bank1 (\* = ''), Bank2 (\* = '2')
- DG engine speed sensor
- PG\* phase sensor
- Activ\*low definition of the phase level PG\* at BM0 for the hardware shell
- CKS crankshaft
- °CKS degree crank angle
- CMS camshaft
- °CMS degree cam angle

Parameter	Source-X	Source-Y	Type	Description
NWAFMN			FW	lower limit of engine speed for release of camshaft adaptation
NWAFMX			FW	upper limit of engine speed for release of camshaft adaptation
TMWAFMN			FW	minimum engine temperature for angle adaptation camshaft
WNWAFMX			FW	adaptation limit of the retarded end position in the advanced direction
WNWASMX			FW	upper camshaft adaptation limit of the retarded end position(retarded direction)
WNWSPS2_0			FW	setangle of the edge 0 of the camshaft 2 in the reference position
WNWSPS2_1			FW	setangle of the edge 1 of the camshaft 2 in the reference position
WNWSPS2_2			FW	setangle of the edge 2 of the camshaft 2 in the reference position
WNWSPS2_3			FW	setangle of the edge 3 of the camshaft 2 in the reference position
WNWSPS_0			FW	setangle of the edge 0 of the camshaft in the reference position
WNWSPS_1			FW	setangle of the edge 1 of the camshaft in the reference position
WNWSPS_2			FW	setangle of the edge 2 of the camshaft in the reference position
WNWSPS_3			FW	setangle of the edge 3 of the camshaft in the reference position
ZNWSP			FW	time constant for camshaft adaptation of the retarded end position

Variable	Source	Type	Description
B_BM	GGDPG	EIN	condition reference mark detected
B_LL	MSF	EIN	Condition idle
B_LUECKE	GGDPG	EIN	current segment covers the reference gap
B_NLDG		EIN	condition limp-home function speed sensor
B_NWSVF	DNWS	EIN	condition camshaft control in advanced end position
B_NWSVF2	DNWS	EIN	condition camshaft control of bank 2 in advanced end position
B_NW_S	NWS	EIN	state information: camshaft control in retarded position
B_PHAD	WANWKW	AUS	adaptation crankshaft/camshaft performed
B_PHAD2	WANWKW	AUS	adaptation crankshaft/camshaft 2 performed
B_SPSA	WANWKW	AUS	condition adaptation of alignment between crankshaft and camshaft released
B_SPSA2	WANWKW	AUS	condition adaptation of alignment between crankshaft and camshaft 2 released
B_ST	SWADAP	EIN	condition for start
B_SYNNLDG	NLDG	EIN	condition: limp home crank position detected from PG-signal
B_WNW2OUT	WANWKW	AUS	condition: difference in crank angle wnw_i*_ad_w not plausible
B_WNW1OUT	WANWKW	AUS	condition: difference in crank angle wnw_i*_ad_w not plausible
B_ZZTAB	GGDPG	EIN	condition: tooth time table valid
C_FCMCLR		EIN	system state: reset fault memory
C_INISYN		EIN	ECU-condition for intialisation of angle synchronization
C_NACHL		EIN	ECU condition for ECU switch off delay
C_NORM		EIN	ECU-condition normal engine management operation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
C_SYN		EIN	ECU-condition angle synchronization available
E_BM	DDG	EIN	error flag: reference mark sensor
E_NWSE	DNWSE	EIN	error flag: power stage of camshaft control valve
E_PH	DPH	EIN	error flag: phase sensor
E_PH2	DPH	EIN	error flag: phase sensor 2
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
GAPTOOTH	GGDPG	EIN	content of the tooth counter to check the gap
NMOT	SWADAP	EIN	engine speed



Variable	Source	Type	Description
PH		EIN	Input signal phase
PH2		EIN	Input signal phase 2
R_PH	WANWKW	LOK	Schedule of phase signal
R_PH2	WANWKW	LOK	Schedule of phase signal 2
R_SYN	GGDPG	EIN	Synchro schedule
R_T200		EIN	Time schedule 200 ms
SY_GAP	PROKON	EIN	system constant: number of missing teeth in the gap
SY_NWS	PROKON	EIN	system constant camshaft control: none, 2 point or continuous
SY_PGRAD	PROKON	EIN	system constant: kind of the phase signal
SY_PGRAD2	PROKON	EIN	system constant: kind of the 2. phase signal
SY_WNBM	PROKON	EIN	System constant for angle of tooth distance from crankshaft signal
SY_ZSGMT		EIN	system constant segment length in camshaft teeth
T		EIN	time
TMOT	SWADAP	EIN	Engine temperature
TNBM.W	WANWKW	DOK	tooth periode of the last NBM signal
WKWSYN.W	GGDPG	EIN	crank angle at start of the synchro (word)
WKW.W	GGDPG	EIN	crank angle (word)
WNWI2_AD.W	WANWKW	AUS	difference in crank angle between adapted and current 2. phase edge (word)
WNWIM2.W	WANWKW	LOK	average deviation of the adaptation camshaft 2 /crankshaft
WNWIM.W	WANWKW	LOK	average deviation of the adaptation camshaft / crankshaft
WNWI_AD.W	WANWKW	AUS	difference in crank angle between adapted and current phase edge (word)
WNWKWAS2.W	WANWKW	AUS	angle between camshaft and crankshaft regarding a working cycle
WNWKWAS.W	WANWKW	AUS	angle between camshaft and crankshaft regarding a working cycle
WNWSP2.W	WANWKW	AUS	Adaptation angle of the camshaft 2 in retarded end position
WNWSPAS2.W	WANWKW	AUS	adaptation angle of the camshaft position regarding a working cycle
WNWSPAS.W	WANWKW	AUS	adaptation angle of the camshaft position regarding a working cycle
WNWSP.W	WANWKW	AUS	Adaptation angle of the camshaft in retarded end position
ZPHFL	WANWKW	AUS	counter of the equidistant phase edges
ZPHFL2	WANWKW	AUS	counter of the equidistant phase edges 2
ZPHFLSYN	NLDG	EIN	phase edge counter at detecting the crank position in limp home DG
ZZSEG	GGDPG	EIN	tooth counter in segment
ZZTAB	GGDPG	EIN	tooth time table
ZZYL	GGDPG	EIN	SW-cylinder counter

### FW WANWKW 13.30 Fixed Values

Parameter	Value	Description
NWAFMN		lower limit of engine speed for release of camshaft adaptation
NWAFMX		upper limit of engine speed for release of camshaft adaptation
TMWAFMN		minimum engine temperature for angle adaptation camshaft
WNWAFMX		adaptation limit of the retarded end position in the advanced direction
WNWASMX		upper camshaft adaptation limit of the retarded end position(retarded direction)
WNWSPS2_0		setangle of the edge 0 of the camshaft 2 in the reference position
WNWSPS2_1		setangle of the edge 1 of the camshaft 2 in the reference position
WNWSPS2_2		setangle of the edge 2 of the camshaft 2 in the reference position
WNWSPS2_3		setangle of the edge 3 of the camshaft 2 in the reference position
WNWSPS_0		setangle of the edge 0 of the camshaft in the reference position
WNWSPS_1		setangle of the edge 1 of the camshaft in the reference position
WNWSPS_2		setangle of the edge 2 of the camshaft in the reference position
WNWSPS_3		setangle of the edge 3 of the camshaft in the reference position
ZNWSP		time constant for camshaft adaptation of the retarded end position

### FB WANWKW 13.30 Detailed description of function

Angle detection of alignment between crankshaft and camshaft

In the case CMS interrupt, the angle  $wnwkwas*_w$  is measured relative to the zero point in the working cycle ( $R_{syn} & zzy1=0$ ):  
 $wnwkwas*_w = (\text{tooth in working cycle} + \text{tooth improvement}) * SY_{WNBM}$

Release of the adaptation:

The adaptation is only released if the first gap check was successful ( $B_{bm}=1$ ), if a engine speed window is not exceeded, if the engine is idling and no longer in the start range and if the engine speed and phase signals are error-free.

On systems with camshaft adjustment the adaptation is only released if it is sure that adjustment is in the retarded position ( $B_{nw_s}$ ) and that the diagnosis for camshaft adjustment has not detected the advanced position ( $B_{nwsvf}$ ).

Each adaptation of the CMS position to the software reference mark  $wnwsp*_w(i)$  is performed in the CMS interrupt ( $R_{ph}$ ) providing that the condition  $B_{spsa}$  is fulfilled: The difference to the current adaptation value is given by the deviation  $wnwi*_ad_w$ . With, e.g., a positive  $wnwi*_ad_w$ , the current value  $wnwkwas*_w$  is greater than the adaptation value  $wnwsp*_w(i)$ . The adaptation then tracks  $wnwsp*_w(i)$ .



The adaptation angle  $wnwsp\_w(i)$  is tracked via a low pass with the time constant ZNWSP and is limited by the limit values WNWASMX and WNWAFMX with reference to the setpoint value WNWSPS\*(i). The adaptation value  $wnwsp\_w(i)$  is stored in the permanent RAM. In the event of powerfail, the RAM-cells  $wnwsp\_w(i)$  are loaded with the fixed values WNWSPS\*(i).

The floating average value  $wnwim\_w$  of the angle  $wnwi\_ad\_w$  is used to determine whether the adaptation condition can be applied. The adaptation status is stored in the condition B\_phad\*:

B\_phad\* = 1: Adaptation of the phase edge is being performed and is valid  
B\_phad\* = 0: Adaptation of the phase edge is not valid

The adaptation for the second camshaft is performed in the same way as for the first camshaft. The adaptation is performed separately for both sides, i.e. two adaptation angles  $wnwsp\_w(i)$ ,  $wnwsp2\_w(i)$  exist as well as, two deviations  $wnwi\_ad\_w$ ,  $wnwi2\_ad\_w$  from these adaptation angles, two floating average values of the adaptation value  $wnwim\_w$ ,  $wnwim2\_w$ , and two resulting conditions B\_phad, B\_phad2. The values  $wnwkwas\_w$ ,  $wnwkwas2\_w$  und  $wnwspas\_w$ ,  $wnwspas2\_w$  are also both available in this case. There are the labels of the first bank: WNWSPS\_0, WNWSPS\_1, WNWSPS\_2, WNWSPS\_3, and the labels of the second bank: WNWSPS2\_0, WNWSPS2\_1, WNWSPS2\_2, WNWSPS2\_3.

Example:



## APP WANWKW 13.30 Application hint

Guidance values for initial application:

WNWSPS(i) Setpoint value for the crankshaft between software reference mark before cylinder 1 and phase edge [°CKS]

	edge:	1	2	3	4
e.g. 1-finger rotor [°CKS]:	==> SY_PGRAD=1	690		any	
quick start wheel with 4-finger-rotor [°CKS]:	==> SY_PGRAD=1	104	284	464	644

TMWAFMN	60°C
NWAFMX	1500 rpm
NWAFMN	600 rpm
ZNWSP	< 10%
WNWAFMX	- 25°CKS
WNWASMX	+ 25°CKS

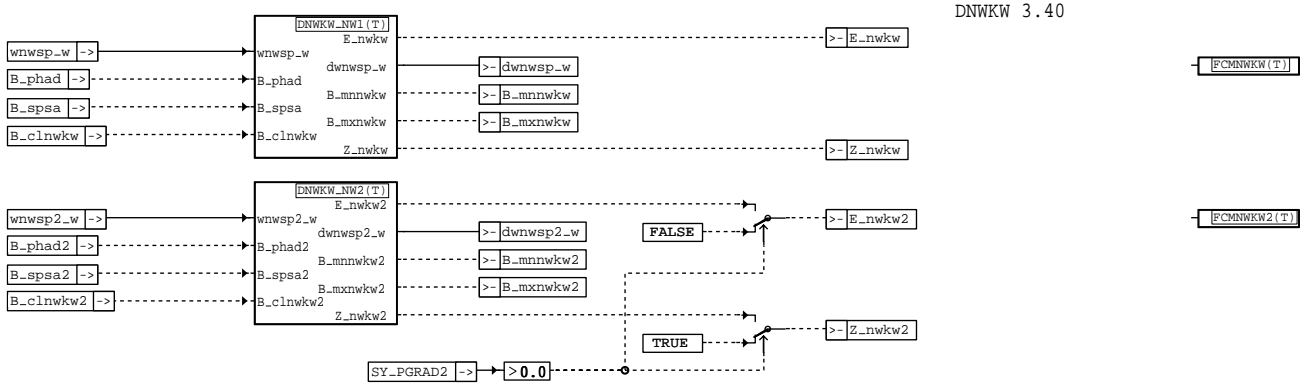
Function check procedure:

1. Locate the position of the phase signal in the working cycle (INKA-VADI or oszilloscope)
2. check parameter against unplaussible values, adjust WNWSPS to the position of the phase signals
3. check the following labels against unplaussible values in idle condition (VS100-VSO):  
zphfl (way of counting: 0, ... SY\_PGRAD-1),  
wnwkwas\_w (position of actual phase edge)  
B\_spsa (Release of Adaptation, changes true/false by changing engine speed or idle/part load),  
wnwspas\_w (wnwspas\_w = wnwsp\_w(zphfl), note: values should not run into limitation: WNWSPS+WNWASMX or WNWSPS+WNWAFMX),  
wnwi\_ad\_w (differenz wnwspas\_w - wnwkw\_w, --> zero, if adaptation successful),  
B\_phad (compare against wnwim\_w, = true, if wnwim < 3°)
4. Check of the adaptation in idle condition (VS100-VSO):  
set WNWASMX/WNWAFMX to high values, p.e. +/- 100°; set WNWSPS to a value, so that wnwsp runs into limitation;  
reset WNWSPS to correct value and monitor the adaptation values; stabilisation of the values after about 10 sec.
5. Check of the adaptation in no idle condition and camshaft control  
B\_spsa = false, camshaft in retarded position: wnw\_i\_ad\_w = 0, in advanced position wnw\_i = CMS shift angle  
(Check analog signals of speed and phase sensors with INKA-VADI or oszilloscope)

## DNWKW 3.40 Diagnosis alignment between camshaft and crankshaft

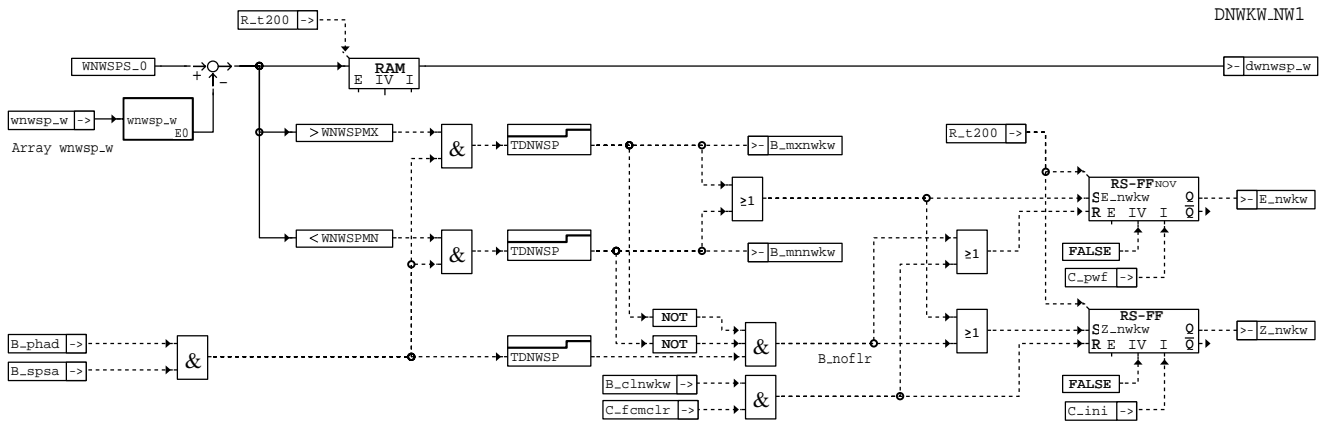
### FDEF DNWKW 3.40 Function definition

The section %DNWKW describes the diagnosis of the alignment between the camshaft/s and the crankshaft. Therefore the adapted position of the first phase edge (see %WANWKW) is compared with its nominal position.



### dnwk-dnwk

In case of a system with two phase sensors ( $SY\_PGRAD2 > 0$ ), both sensors are monitored separately. The diagnosis of the 2. phase sensor PG2 is done in the same way as for the 1. phase sensor PG, due to this the DNWKW\_NW2 is not illustrated in the following. If the system includes only one phase sensor, DNWKW\_NW2 is not calculated and the flags E\_nwk2 and Z\_nwk2 are initialized with neutral values.



### dnwk-dnwk-nw1

Determination of the deviation of the camshaft position from the setpoint position:

$$dwnwsp\_w = WNWSPS\_0 - wnwsp\_w(0);$$

adjusted to advanced:  $dwnwsp\_w > 0$   
retarded:  $dwnwsp\_w < 0$

Formation of the fault condition E\_nwk\* and of the fault type:

Fault:

$dwnwsp\_w > WNWSPMX$ :	B_mxnkw*	Camshaft position adjusted to advanced
$dwnwsp\_w < WNWSPMN$ :	B_mnnkw*	Camshaft position adjusted to retarded
else:	E_nwk*=0	Camshaft position is within the permissible range of tolerance

Fault memory management:

Status fault path NWKW:	SFPNWKW	Status fault path NWKW2:	SFPNWKW2
Error flag NWKW:	E_nwk	Error flag NWKW2:	E_nwk2
Cycle flag NWKW:	Z_nwk	Cycle flag NWKW2:	Z_nwk2
Fault type NWKW:	B_mxnkw B_mnnkw	Fault type NWKW2:	B_mxnkw2 B_mnnkw2
Delete fault path:	C_fcmclr & B_clnkw	Delete fault path:	C_fcmclr & B_clnkw2
Fault path NWKW :	CDTNWKW	Fault path NWKW2 :	CDTNWKW2
Fault class NWKW:	CLANWKW	Fault class NWKW2:	CLANWKW2
Fault intensity NWKW:	TSFNWKW	Fault intensity NWKW2:	TSFNWKW2
Carb code NWKW:	CDCNWKW	Carb code NWKW2:	CDCNWKW2
Environmental cond. NWKW:	FFTNWKW	Environmental cond. NWKW2:	FFTNWKW2



## ABK DNWKW 3.40 Abbreviations

*	wildcard for PG or PG2
PG	first phase sensor
PG2	second phase sensor
CKS	crankshaft

Parameter	Source-X	Source-Y	Type	Description
CDCNWKW	BLOKNR		KL	code word CARB: alignment between camshaft and crankshaft
CDCNWKW2	BLOKNR		KL	code word CARB: alignment between camshaft 2 and crankshaft
CDTNWKW			FW	code word tester: alignment between camshaft and crankshaft
CDTNWKW2			FW	code word tester: alignment between camshaft 2 and crankshaft
CLANWKW			FW	fault class: alignment between camshaft and crankshaft
CLANWKW2			FW	fault class: alignment between camshaft 2 and crankshaft
FFTNWKW	BLOKNR		KL	freeze frame table: alignment between camshaft and crankshaft
FFTNWKW2	BLOKNR		KL	freeze frame table: alignment between camshaft 2 and crankshaft
TDNWSP			FW	Time delay for the checking of the camshaft shift
TSFNWKW			FW	fault active time: alignment between camshaft and crankshaft
TSFNWKW2			FW	fault active time: alignment between camshaft 2 and crankshaft
WNWSPMN			FW	Border angle of the retarded shift for the assignment of camshaft to crankshaft
WNWSPMX			FW	Border angle of the advanced shift for the assignment of camshaft to crankshaft
WNWSPS2_0			FW	setangle of the edge 0 of the camshaft 2 in the reference position
WNWSPS_0			FW	setangle of the edge 0 of the camshaft in the reference position

Variable	Source	Type	Description
B_CLNWKW		EIN	condition clear fault path alignment between camshaft and crankshaft
B_CLNWKW2		EIN	condition clear fault path alignment between camshaft 2 and crankshaft
B_MNNWKW	DNWKW	AUS	fault type: camshaft retarded
B_MNNWKW2	DNWKW	AUS	fault type: camshaft 2 retarded
B_MXNWKW	DNWKW	AUS	fault type: camshaft advanced
B_MXNWKW2	DNWKW	AUS	fault type: camshaft 2 advanced
B_PHAD	WANWKW	EIN	adaptation crankshaft/camshaft performed
B_PHAD2	WANWKW	EIN	adaptation crankshaft/camshaft 2 performed
B_SPSA	WANWKW	EIN	condition adaptation of alignment between crankshaft and camshaft released
B_SPSA2	WANWKW	EIN	condition adaptation of alignment between crankshaft and camshaft 2 released
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DWNWSP2_W	DNWKW	AUS	Deviation of the adap. angle 2 from engine-spec. setpoint angle of the camshaft
DWNWSP_W	DNWKW	AUS	Deviation of the adap. angle from engine-spec. setpoint angle of the camshaft
E_NWKW	DNWKW	AUS	error flag: alignment between camshaft and crankshaft
E_NWKW2	DNWKW	AUS	error flag: alignment between camshaft 2 and crankshaft
R_T200		EIN	Time schedule 200 ms
SFPNWKW	DNWKW	AUS	status fault path: alignment between camshaft and crankshaft
SFPNWKW2	DNWKW	AUS	status fault path: alignment between camshaft 2 and crankshaft
SY_PGRAD2	PROKON	EIN	system constant: kind of the 2. phase signal
WNWSP2_W	WANWKW	EIN	Adaptation angle of the camshaft 2 in retarded end position
WNWSP_W	WANWKW	EIN	Adaptation angle of the camshaft in retarded end position
Z_NWKW	DNWKW	AUS	cycle flag: alignment between camshaft and crankshaft
Z_NWKW2	DNWKW	AUS	cycle flag: alignment between camshaft 2 and crankshaft

## FW DNWKW 3.40 Fixed Values

Parameter	Value	Description
CDTNWKW		code word tester: alignment between camshaft and crankshaft
CDTNWKW2		code word tester: alignment between camshaft 2 and crankshaft
CLANWKW		fault class: alignment between camshaft and crankshaft
CLANWKW2		fault class: alignment between camshaft 2 and crankshaft
TDNWSP		Time delay for the checking of the camshaft shift
TSFNWKW		fault active time: alignment between camshaft and crankshaft
TSFNWKW2		fault active time: alignment between camshaft 2 and crankshaft
WNWSPMN		Border angle of the retarded shift for the assignment of camshaft to crankshaft
WNWSPMX		Border angle of the advanced shift for the assignment of camshaft to crankshaft
WNWSPS2_0		setangle of the edge 0 of the camshaft 2 in the reference position
WNWSPS_0		setangle of the edge 0 of the camshaft in the reference position

## FB DNWKW 3.40 Detailed description of function

Determination of the deviation of the camshaft position from the setpoint position:

The deviation of the camshaft position from the engine-specific setpoint position is given by:

$$dwnwsp*_w = WNWSPS*_0 - wnwsp*_w(0). \quad (* = Wildcard for PG oder PG2)$$

By comparing the limitation values the conditions "adjusted to advanced" B\_mxnkw\*, "adjusted to retarded" B\_mnnkw\*, resp. "adjustment in the permissible range" E\_nkw\* are set = false.

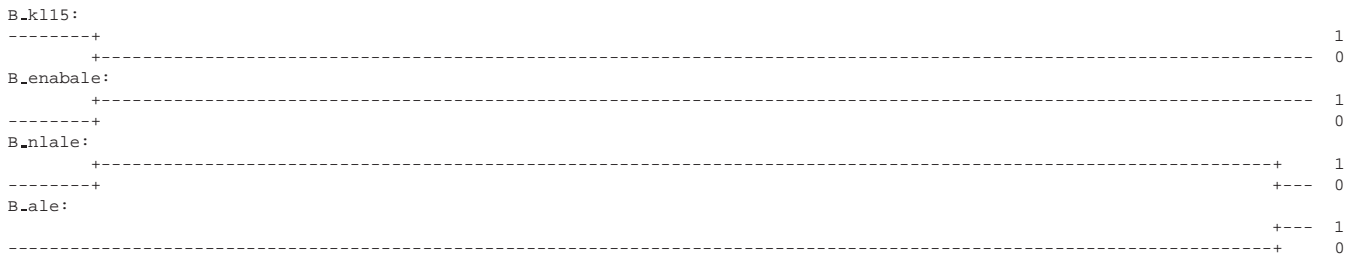
The setting of the conditions is only performed if the angle adaptation (B\_spsa\*) is active and if it was successful (B\_phad\*). In order to set the fault condition the limit must have been exceeded for the period of time TDNWSP. If after this period of time the limit is still exceeded the fault condition is set.







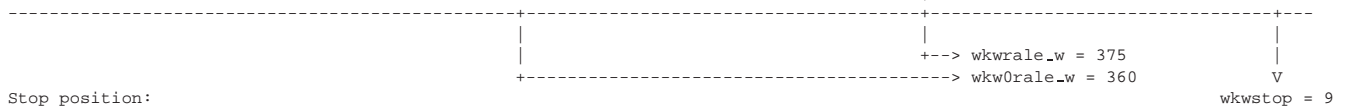
Run-out Detection with Back-Swing Detection:



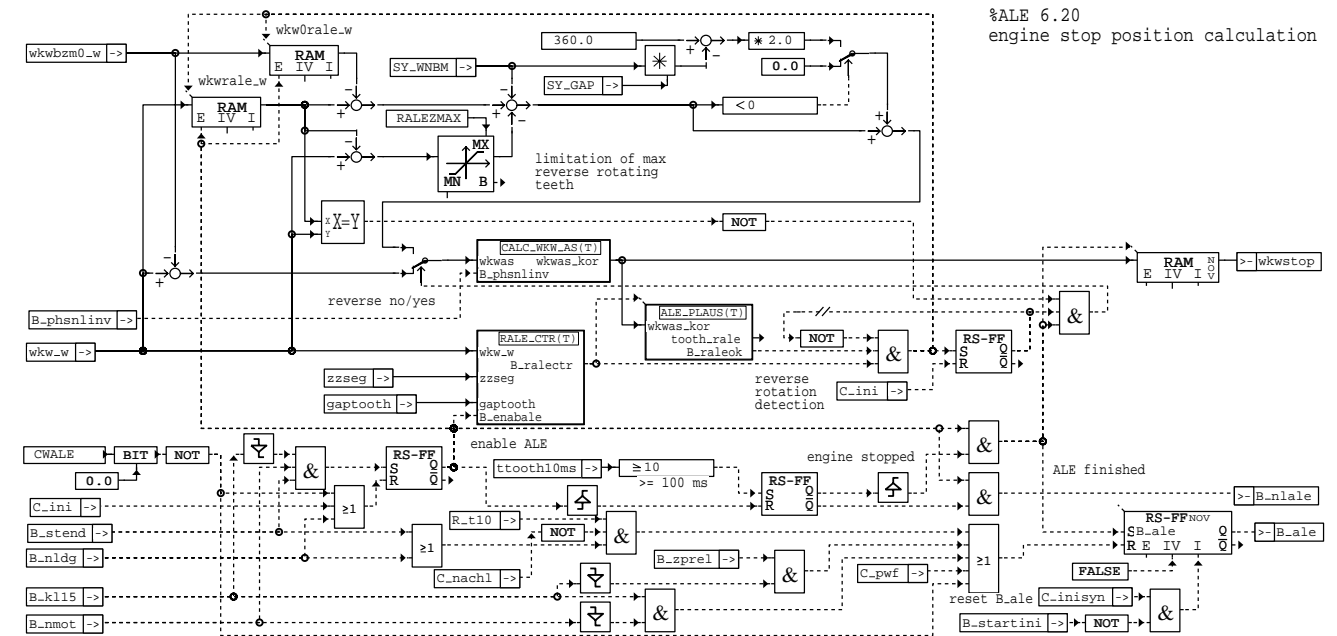
NBM with back swing:



Back-swing detection:



Stop position:

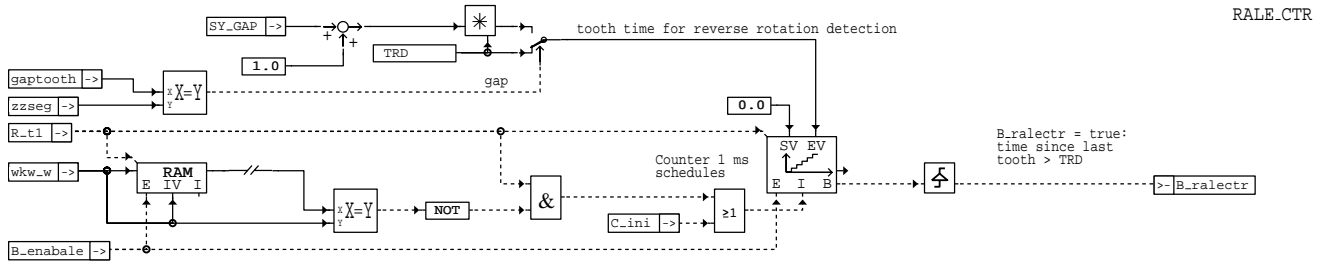


ale-ale

Functional Overview of Run-out Detection

- Calculation of wkwstop from wkw\_w, wkwbzm0\_w, wkw0rale\_w and wkwrale\_w
- Reverse rotation detection with the setting of a RS-FF's at first detection
- Logic for the setting and resetting of B\_enabale, B\_nlale and B\_ale

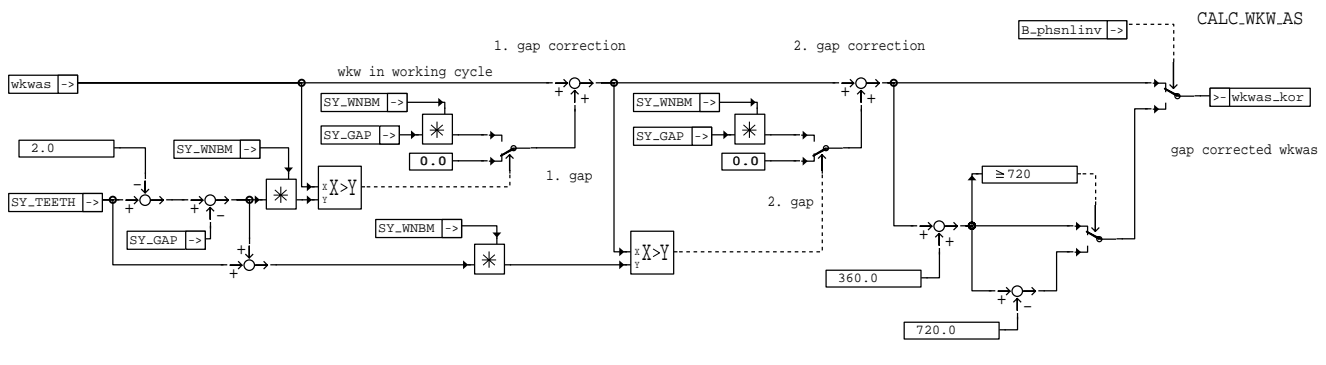
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**ale-rale-ctr**

RALE\_CTR: Condition last tooth time > TRD

B\_ralectr is formed from a counter, which counts in the 1 ms cycle for as long as no tooth interrupt occurs. The counter is reset after each tooth interrupt. As soon as the counter reaches the value TRD (resp. in the gap  $(1 + SY\_GAP) * TRD$ ), B\_ralectr is set.

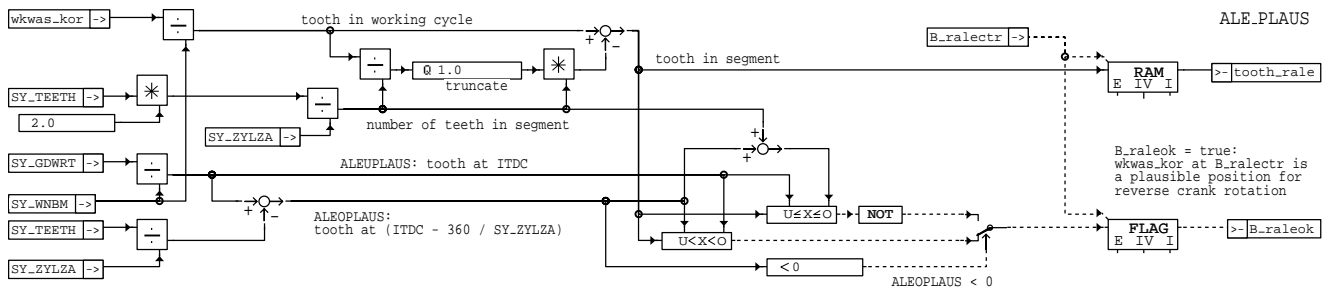


**ale-calc-wkw-a**

CALC\_WKW\_AS: Correction of the angle wkw

Correction of the angle wkw by the missing teeth of the gaps. If wkw lies after the first gap then the correction angle of the missing teeth is summed up. If this position lies after the second gap then this angle is summed up again.

When the phase sensor limp-home has detected in the current driving cycle that the angle position is incorrect by one crankshaft revolution (B\_phsnlinv = 1), the stop position is corrected accordingly.



**ale-ale-plaus**

ALE\_PLAUS: Checking of the crank angle wkw\_kor for plausible reverse rotation range

With the condition B\_ralectr the current crank angle wkw\_kor is checked for plausible reverse rotation range. The engine is within a plausible range, if the piston in the cylinder is just in compression within half a segment before ignition TDC. The condition for the plausible reverse rotation range therefore results:

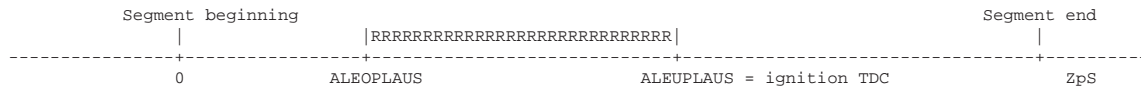
$$ALEOPLAUS < \text{tooth in the segment} < ALEUPLAUS$$

with:  $ALEUPLAUS = SY\_GDWRT / SY\_WNBM$  ==> ZOT  
 $ALEOPLAUS = (ALEUPLAUS - SY\_TEETH / SY\_ZYLZA)$  ==> segment/2 before ignition TDC

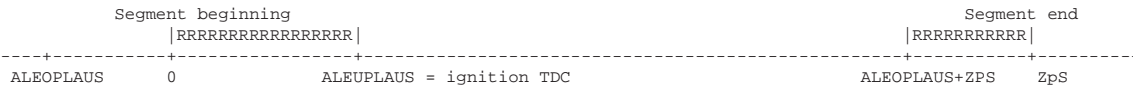
Since the tooth in the segment is always  $\geq 0$ , the following 2 cases result from ALEOPLAUS:



1. ALEOPLAUS >= 0:



2. ALEOPLAUS < 0:



RRRR = plausible reverse rotation range

## ABK ALE 6.20 Abbreviations

ZOT = ignition TDC

ZpS = teeth per segment = 2 \* SY-TEETH / SY-ZYLZA

Parameter	Source-X	Source-Y	Type	Description
CWALE			FW	run-out position is calculated
RALEZMAX			FW	Limitation of the number of reverse rotating teeth during engine stopping
TRD			FW	tooth period time for reverse rotation during stop
Variable	Source		Type	Description
B_ALE	ALE		AUS	condition engine stop position detected
B_ENABALE	ALE		LOK	condition: release for calculation of the engine stop position
B_KL15			EIN	condition ignition switch on
B_NLALE	ALE		AUS	request for ECM afterrun from the function ALE
B_NLDG			EIN	condition limp-home function speed sensor
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_PHSNLINV	NLPH		EIN	condition invert phase relation
B_RALECTR	ALE		LOK	condition last tooth time > TRD
B_RALEOK	ALE		LOK	condition last tooth was in the plausible reverse rotation range
B_STARTINI	GGDPG		EIN	start bit to distinguish first synchronization with KL15 from new synchr.
B_STEND	BBSTT		EIN	condition end of start
B_ZPREL	GGDPG		EIN	condition tooth debouncing ready
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_JNISYN			EIN	ECU-condition for intialisation of angle synchronization
C_NACHL			EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
GAPTOOTH	GGDPG		EIN	content of the tooth counter to check the gap
R_T1			EIN	Time schedule 1 ms
R_T10			EIN	Time schedule 10 ms
SY_GAP	PROKON		EIN	system constant: number of missing teeth in the gap
SY_GDWRT			EIN	system constant: crank angle between reference gap to ITDC cylinder 1
SY_TEETH	PROKON		EIN	system constant: number of teeth with gap teeth on the crankshaft wheel
SY_WNBMM	PROKON		EIN	System constant for angle of tooth distance from crankshaft signal
SY_ZYLZA	PROKON		EIN	system constant number of cylinders
TOOTH_RALE	ALE		LOK	first reverse rotating tooth in segment
TTOOTH10MS	GGDPG		EIN	counter 10 ms schedules without tooth interrupt
WKWAS	ALE		LOK	crank position in working cycle without gap correction
WKWAS_KOR	ALE		LOK	crank position in working cycle with gap correction
WKWBZM0_W	GGDPG		EIN	crank angle at the zero point of the working cycle: R_syn & zyl = 0 (word)
WKWSTOP	ALE		AUS	engine stopping position in working cycle
WKW_W	GGDPG		EIN	crank angle (word)
ZZSEG	GGDPG		EIN	tooth counter in segment

## FW ALE 6.20 Fixed Values

Parameter	Value	Description
CWALE		run-out position is calculated
RALEZMAX		Limitation of the number of reverse rotating teeth during engine stopping
TRD		tooth period time for reverse rotation during stop

## FB ALE 6.20 Detailed description of function

The calculation of the stop position is enabled when terminal 15 is off (B\_kl15 1->0), provided end of start was reached (B\_stend), engine speed is still detected (B\_nmot) and no limp-home speed sensor is given ==> B\_enabale = true. In this case the after-run bit (B\_nlale) is also set.

If a tooth period with a period time greater than TRD occurs while the engine is running on (B\_ralectr) and if the current engine position lies within a plausible reverse rotation range (B\_raleok), then reverse rotation is detected and the crank angle position wkw\_w resp. wkw\_bzm0\_w is re-stored to wkw\_rale\_w resp. wkw0rale\_w.

After the back-swing detection the counter wkw\_w continues. 100 ms after the last tooth interrupt (Counter: ttooth10ms >= 10) the run-out detection is aborted and the stop position wkwstop is calculated. In the process two cases need to be distinguished:

1. Reverse rotation detected and engine has rotated back by at least 1 tooth (wkw\_rale\_w

wkw\_w).

The backward rotated crank angle results from the current crank angle and the crank angle, which was stored at the moment of the reverse rotation. To minimize the fault in case of a further 'reverse rotation' of the engine (engine rotates forward again), this angle is limited to RALEZMAX. This angular difference plus one tooth must be subtracted from the reverse rotation point and then results in the stop position:

$$\text{wkwstop} = (\text{wkwrale}_w - \text{wkw0rale}_w) - (\text{Min}((\text{wkw}_w - \text{wkwrale}_w), \text{RALEZMAX}) + \text{SY_WNB M})$$

Thereafter a possibly occurring overflow in the working cycle still needs to be corrected.

2. Engine has not rotated backward.

The current stop position results from:

$$\text{wkwstop} = \text{wkw}_w - \text{wkw bzm0}_w$$

In both cases a gap correction is still performed by means of CALC\_WKW\_AS. After wkwstop has been calculated the condition run-out detection valid (B\_ale = 1) is set and the after-run bit (B\_nlae) is reset.

B\_ale is reset at power fail (C\_pwf), when stalling the engine (B\_kl15 and B\_nmot 1->0), at terminal 15 off and once the tooth debouncing has elapsed (B\_kl15 1->0 and B\_zprel) as well as during transition to the post-start range (B\_stend 0->1), new synchronization at drive (B\_startini = FALSE) or at limp-home speed sensor (B\_nldg 0->1).

If the engine position is changed once the vehicle has been parked (e.g. pushing while gear is engaged) then the actual engine position is changed. Since then the start position does not correspond to the run-out position, at restart a timing fault of the first injection pulses occurs until a new synchronization is performed. Thereby prolonged starting times may occur.

The calculation of the run-out position can be switched off via the code word CWALE. The bit B\_ale is set in this case to FALSE in the ECU run-on.

## APP ALE 6.20 Application hint

TRD:

This value determines, at which tooth period duration a back swing of the engine is detected. If the value is chosen too high, back swinging is not always detected. If on the other hand the value is chosen too low, back swinging is detected too early or incorrectly. In order to choose the correct value several run-on attempts are to be performed and in the process the digital tooth signals after the conditioning circuit (CJ53, CJ400) should be recorded. From this the back-swing position can be detected and typical values for the tooth period during back swing can be measured. The smallest tooth period, at which back swinging occurs is to be chosen as application value. Typical values for the tooth period during back swinging are: 25 to 50 ms.

RALEZMAX:

This value indicates the maximum permitted number of backward rotated teeth. If the reverse rotation point lies shortly before TDC then the engine rotates back far and into the previous compression. This can lead to another reversing of the direction of rotation so that the engine rotates forward again. Since this reversing of the direction of rotation can no longer be detected, the number of backward rotating teeth is limited.

CWALE:

CWALE = 1: the run-out position is calculated the normal engine turn off  
CWALE = 0: the run-out position is not calculated. The bit B\_ale is set to FALSE

The code word must set to 1 in normal case. It is because of the calculation of the camshaft limp home position. So the run-out position is not only used for a fast synchronization in the start. The code word is to switch off the run-out detection with the object to test. If there is no injection permitted via the run-out position this must be applied by the temperature threshold TMESP.

In order to ensure a reliable run-out detection the maximum after-run time should be at least 3 sec.

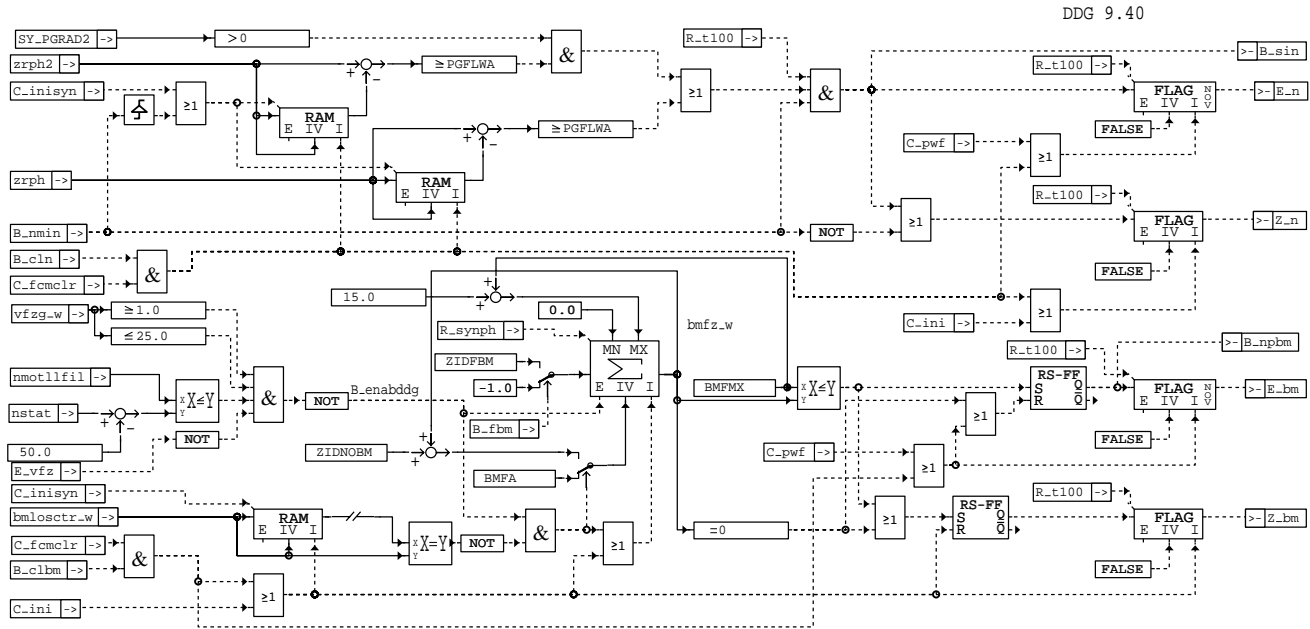
Check of the virtual engine position:

At start virtual R\_syn cycles are triggered already prior to the synchronization. During the transition into the next synchronization state (quick-start wheel or reference mark) the deviation to the actual engine position can be evaluated.



## DDG 9.50 Diagnosis: engine speed sensor

### FDEF DDG 9.50 Function definition



### ddg-ddg

The section DDG describes the diagnosis of the engine speed sensor (DG) at the camshaft. The diagnosis is using the following signals/events:

- DG diagnosis by monitoring the phase sensors (PG and PG2) level changes below minimum speed
- DG diagnosis by monitoring the reference gap

#### Fault memory management:

Status fault path:	SFPN	Status fault path BM:	SFPBM
Error flag N:	E_n	Error flag BM:	E_bm
Cycle flag N:	Z_n	Cycle flag BM:	Z_bm
Fault type N:	B_sin	Fault type BM:	B_npbm

Delete fault path:	C_fmclr & B_cln	Delete fault path:	C_fmclr & B_clbm
Fault path N:	CDTN	Fault path BM:	CDTBM
Fault class N:	CLAN	Fault class BM:	CLABM
Fault intensity N:	TSFN	Fault intensity BM:	TSFBM
Carb code N:	CDCN	Carb code BM:	CDCBM
Environmental cond. N:	FFTN	Environmental cond. BM:	FFTBM

Fault	Fault type	Description
E_n	B_sin	during engine speed search no DG-signal (PGFLWA PG-phase level changes during B_nmin = 1 ==> no DG-signal)
E_bm	B_npbm	multiple loss of the reference gap or tooth corrections in synchronized condition (counter value = BFMX)

### ABK DDG 9.50 Abbreviations

DG engine speed sensor at the crankshaft  
PG phase sensor  
PG2 optional 2. phase sensor  
PH phase sensor signal from the camshaft  
BM reference gap

Parameter	Source-X	Source-Y	Type	Description
BMFA			FW	Numbers of BM-errors (initial value of counter)
BMFMX			FW	Counter maximale value for BM-errors
PGFLWA			FW	Number of edges of phase signal for error B_signal of the engine speed sensor
ZIDFBM			FW	counter increments on tooth correction at BM-check
ZIDNOBM			FW	counter increments after a loss of the reference gap



Variable	Source	Type	Description
BMFZ_W	DDG	LOK	counter errors in reference gap detection for speed sensor diagnosis
BMLOSTR_W	GGDPG	EIN	counter (word) re-synchronizations due to a loss of the reference gap
B_CLBM		EIN	condition clear fault path reference mark sensor
B_CLN		EIN	condition clear fault path engine speed sensor
B_ENABDDG	DDG	LOK	suppression of the engine speed diagnose for E_bm
B_FBM	GGDPG	EIN	condition reference mark error => at least 1 tooth too few/many
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_NPBM	DDG	AUS	Fault type: reference gap is often lost
B_SIN	DDG	AUS	Fault type: no signal from the crankshaft position sensor
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_JNISYN		EIN	ECU-condition for intialisation of angle synchronization
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BM	DDG	AUS	error flag: reference mark sensor
E_N	DDG	AUS	error flag: engine speed sensor
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
NMOTLLFIL	BGNMOT	EIN	filtered engine speed nmotll
NSTAT	LLRNS	EIN	Stationary reference speed
R_SYNPH	GGDPG	EIN	synchro schedule for phase scan
R_T100		EIN	Time schedule 100 ms
SY_PGRAD2	PROKON	EIN	system constant: kind of the 2. phase signal
VFZG_W	GGVFZG	EIN	Vehicle speed
ZRPH	GGDPG	EIN	counter schedule of phase signal
ZRPH2	GGDPG	EIN	counter schedule of phase signal 2
Z_BM	DDG	AUS	cycle flag: reference mark sensor
Z_N	DDG	AUS	cycle flag: engine speed sensor

### FW DDG 9.50 Fixed Values

Parameter	Value	Description
BMFA		Numbers of BM-errors (initial value of counter)
BMFMX		Counter maximale value for BM-errors
PGFLWA		Number of edges of phase signal for error B_signal of the engine speed sensor
ZIDFBM		counter increments on tooth correction at BM-check
ZIDNOBM		counter increments after a loss of the reference gap

### FB DDG 9.50 Detailed description of function

The input signals of the DDG are built in the sections %GGDPG, %SYSICON and %SYSYN.

Fault E\_n: The diagnosis of the DG is made as follows:

Monitoring the phase level changes below minimum engine speed:  
The PG-signal is used as a referenz. When getting some phase interrupts R\_ph without detecting an engine speed signal, then the speed sensor is faulty. To detect this, the number of phase interrupts are checked via the phase interrupt counter zrph below minimum engine speed (B\_nmin). The error flag E\_n and the fault type B\_sin is set, as soon as PGFLWA number of phase level changes during B\_nmin are monitored.  
The error is reset as soon as engine speed is detected.





Fault E<sub>bm</sub>: The diagnosis of the DG is made as follows:

In synchronized condition the reference gap is checked in %GGDPG in each synchro after the gap. A loss of the gap causes a re-synchronization (E<sub>bm</sub> 1 -> 0) which increases a counter (bmlosctr\_w). In case the gap is wrong by one tooth, a gap correction will be made and the flag B<sub>fbm</sub> will be set. The diagnosis uses this information. At a gap loss a counter is increased by ZIDNOBM. At a gap correction the counter is increased by ZIDFBM. If the gap is correct, the counter will be decreased by 1. As soon as the counter reaches BMFMX the error B<sub>npbm</sub> is set. The error is reset as soon as the counter has counted down to 0.

Fade out of the Diagnose (E<sub>bm</sub>):

If there is a operating error of the driver (slowly engine stalling, wrong gear shifting at start) there could be a vibration of the crankshaft. This may affect a frequently loss of the reference gap during this operation point, which cause an error entry although there is no damage at the system.

To prevent the error entry in this case, the diagnose for intermittent contact (E<sub>bm</sub>) will fade out, if the engine speed is below idling speed and the car is in motion. The calculation of the fade out condition takes part in the 10ms cycle. Because of large fluctuation of the engine speed during this operation point the filtered engine speed nmotllfil is used as input value. If the error bit E<sub>vfz</sub> is set, there is no fade out of the diagnose on principle.

### APP DDG 9.50 Application hint

Recommendation for first application:

```

PGFLWA:      depending on the number of phase signal per cam rotation, minimum 8 rotations should be used until the
              error is set (standard wheel: 8   quick start wheel: 24)
ZIDFBM:      150
ZIDNOBM:     1200
BMFA:       1000
BMFMX:      4000
CDTN:       110          CDTBM:      111
CLAN:       3           CLABM:      6
TSFN:      255          TSFBM:      255
CDCN:      824,823,821,822d  CDCBM:    824,823,821,822d
FPTN:      ub, tmot     FFTBM:      ub, tmot
  
```

Function test:

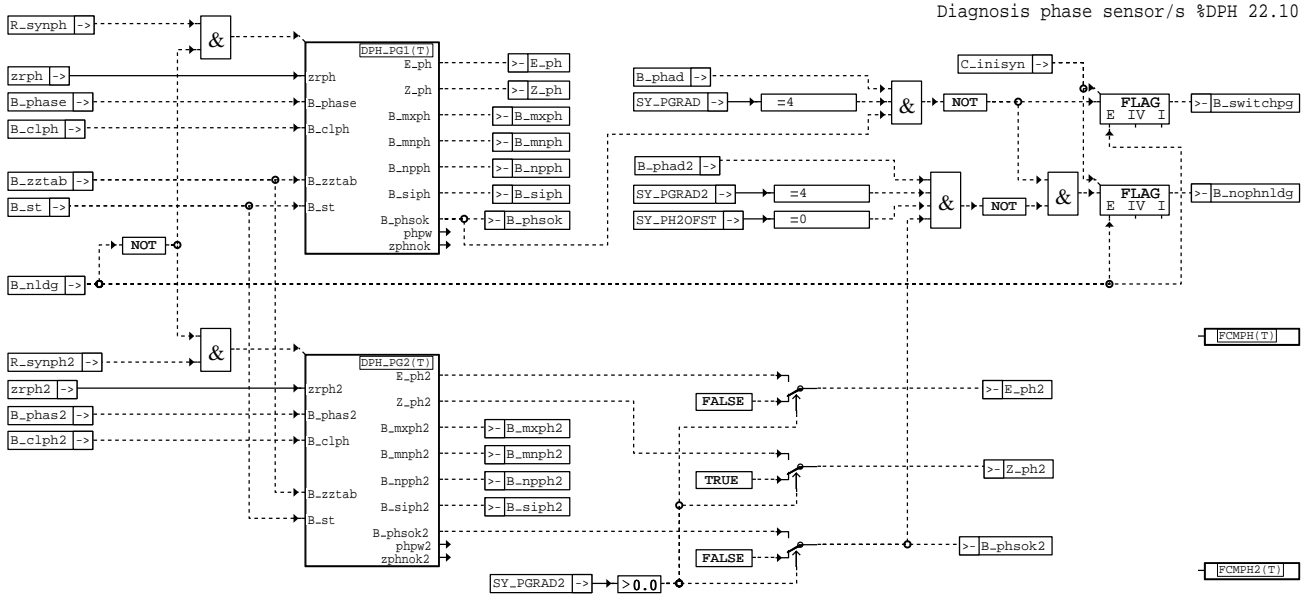
1. Measure the following signals with VS100-VSO:
  - RAM cells: nmot, B<sub>nmin</sub>, zrph, E<sub>n</sub>, E<sub>bm</sub>, Z<sub>n</sub>, Z<sub>bm</sub>, B<sub>sin</sub>, B<sub>fbm</sub>, bmlosctr\_w, B<sub>npbm</sub>
  - Label: PGFLWA, ZIDFBM, ZIDNOBM, BMFA, BMFMX
2. Check, if DG-signal is existing:
  - ignition on: B<sub>nmin</sub> = true, zrph = 0, E<sub>n</sub> = false, Z<sub>n</sub> = false, E<sub>bm</sub> = false, Z<sub>bm</sub> = true
  - start engine: B<sub>nmin</sub> = false, Z<sub>n</sub> = true, zrph is incremented, nmot plausible, E<sub>n</sub> = false
3. Check not connected DG (disconnect DG sensor or disconnect both DG signal wires at the ECU adaptor)
  - ignition on: B<sub>nmin</sub> = true, zrph = 0, E<sub>n</sub> = false, Z<sub>n</sub> = false
  - apply starter, engine does not start: B<sub>nmin</sub> = true, Z<sub>n</sub> = false, zrph is incremented;
  - as soon as zrph > PGFLWA: E<sub>n</sub> = true and Z<sub>n</sub> = true, B<sub>sin</sub> = true;
4. Reset error flag: Reconnect the DG sensor / wires
  - ignition on: B<sub>nmin</sub> = true, zrph = 0, E<sub>n</sub> = true, Z<sub>n</sub> = false
  - start engine: B<sub>nmin</sub> = false -> E<sub>n</sub> = false, Z<sub>n</sub> = true
5. At systems with 2. phase sensor, disconnect PG and repeat steps 1 to 4 by monitoring zrph2 instead of zrph
6. Test intermittend contact:
  - Connect DG, start engine and wait until Z<sub>bm</sub> = true. During monitoring the counter bmfz\_w disconnect and connect the DG wires several times. Reconnect the DG wires correctly as soon as the error is detected (E<sub>bm</sub> = 1) and wait until the error disappears (E<sub>bm</sub> = 0).

In the function %GGVFZG the change-over threshold for vfz\_gw to 0 (Label VRFGRMN) should not be set higher than 3 km/h because of the perfect funktion of the diagnose fade out.



## DPH 22.10 Diagnosis; plausibility test phase sensor

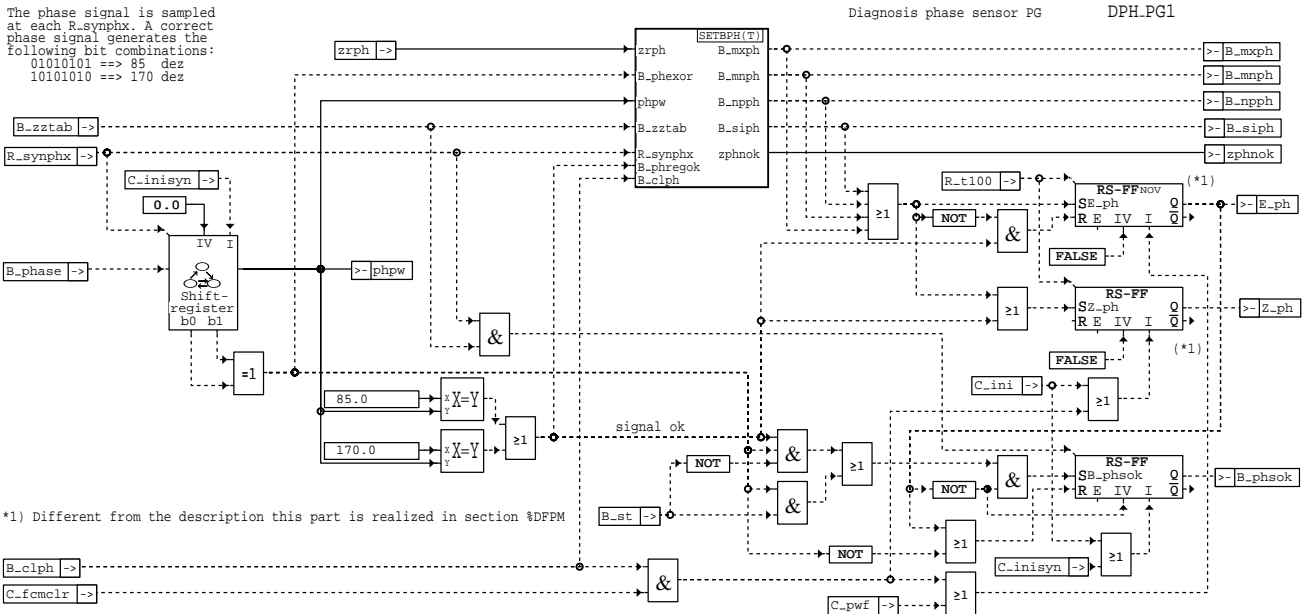
### FDEF DPH 22.10 Function definition



### dph-dph

The section DPH describes the diagnosis of the phase sensor / of the phase sensors (PG/PG2) at the camshaft (CMS).

The phase signal is sampled at each R\_synphx. A correct phase signal generates the following bit combinations:  
01010101 ==> 85 dez  
10101010 ==> 170 dez



(\*1) Different from the description this part is realized in section %DFPM

### dph-dph-pg1

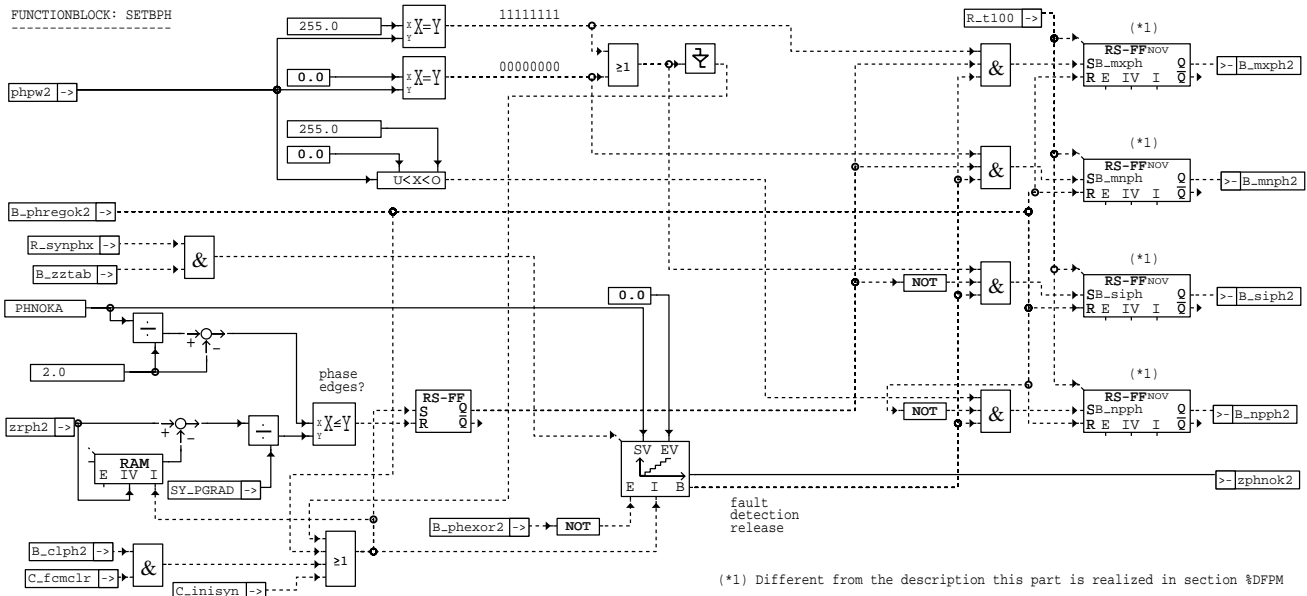
DPH\_PG1: Diagnosis of the phase sensor PG

For the diagnosis the level of the PG signal is inquired upon in each synchro grid for phase inquiry (R\_synph\*). During correct operation the PG level changes alternately (010101...). If it does not change then a PG fault is assumed.





FUNCTIONBLOCK: SETBPH



dph-setbph

### dph-setbph

Setting of error types

If there appears another type of the error E\_ph, the previous error type will reset and the new type will set.

DPH\_PG2: Diagnosis of the phase sensor PG2

In case of a system with two phase sensors (SY\_PGRAD > 0), both of them are monitored separately. The diagnosis of the 2nd phase sensor PG2 is analogous to the 1st phase sensor PG, therefore the subfunction DPH\_PG2 is not illustrated in the following definition. In case of only one phase sensor, DPH\_PG2 is not calculated and the flags E\_ph2, Z\_ph2 and B\_phok2 are initialized with neutral values.

Fault memory management:

Status fault path PH:	sfpph	Status fault path PH2:	sfpph2
Error flag PH:	E_ph	Error flag PH2:	E_ph2
Cycle flag PH:	Z_ph	Cycle flag PH2:	Z_ph2
Fault type PH:	B_mxph B_mnph B_npph	Fault type PH2:	B_mxph2 B_mnph2 B_npph2

Delete fault path:	C_fcmclr & B_clph	Delete fault path:	C_fcmclr & B_clph2
Fault path PH:	CDTPH	Fault path PH2:	CDTPH2
Fault class PH:	CLAPH	Fault class PH2:	CLAPH2
Fault intensity PH:	TSPFH	Fault intensity PH2:	TSPFH2
Carb code PH:	CDCPH	Carb code PH2:	CDCPH2
Environmental cond. PH:	FFTPH	Environmental cond. PH2:	FFTPH2

### ABK DPH 22.10 Abbreviations

PG first phase sensor  
PG2 second phase sensor  
\* wildcard for PG or PG2

Parameter	Source-X	Source-Y	Type	Description
CDCPH	BLOKNR		KL	code word CARB: phase sensor
CDCPH2	BLOKNR		KL	code word CARB: phase sensor 2
CDTPH			FW	code word tester: phase sensor
CDTPH2			FW	code word tester: phase sensor 2
CLAPH			FW	fault class: phase sensor
CLAPH2			FW	fault class: phase sensor 2
FFTPH	BLOKNR		KL	freeze frame table: phase sensor
FFTPH2	BLOKNR		KL	freeze frame table: phase sensor 2
PHNOKA			FW	start value for counter phase signal not ok
TSPFH			FW	fault active time: phase sensor
TSPFH2			FW	fault active time: phase sensor 2

Variable	Source	Type	Description
B_CLPH		EIN	condition clear fault path PH
B_CLPH2		EIN	condition clear fault path Phase sensor 2
B_MNPH	DPH	AUS	error type: short circuit ground of phase sensor



Variable	Source	Type	Description
B_MNPH2	DPH	AUS	error type: short circuit ground of phase sensor 2
B_MXPH	DPH	AUS	error type: short circuit Ubat phase sensor
B_MXPH2	DPH	AUS	error type: short circuit Ubat phase sensor 2
B_NLDG		EIN	condition limp-home function speed sensor
B_NOPHNLDG	DPH	AUS	condition no phase sensor signal for limphome engine speed sensor available
B_NPPH	DPH	AUS	condition signal of camshaft sensor not plausible (ph)
B_NPPH2	DPH	AUS	condition signal of camshaft sensor not plausible (ph2)
B_PHAD	WANWKW	EIN	adaptation crankshaft/camshaft performed
B_PHAD2	WANWKW	EIN	adaptation crankshaft/camshaft 2 performed
B_PHAS2	GGDPG	EIN	Condition phase 2 low/high
B_PHASE	GGDPG	EIN	Condition phase low/high
B_PHEXOR	DPH	LOK	The two lowest significant bits of phpw are unequal
B_PHEXOR2	DPH	LOK	The two lowest significant bits of phpw2 are unequal
B_PHREGOK	DPH	LOK	No error of bit pattern in phase register 1
B_PHREGOK2	DPH	LOK	No error of bit pattern in phase register 2
B_PHSOK	DPH	AUS	Condition phase signal ok
B_PHSOK2	DPH	AUS	Condition phase signal 2 ok
B_SIPH	DPH	AUS	condition no alternating phase levels PG in the reference marks
B_SIPH2	DPH	AUS	condition no alternating phase levels PG2 in the reference mark s
B_ST	SWADAP	EIN	condition for start
B_SWITCHPG	DPH	AUS	condition to switch to phase sensor PG2 for the engine speed sensor limphome
B_ZZTAB	GGDPG	EIN	condition: tooth time table valid
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_JNYSYN		EIN	ECU-condition for intialisation of angle synchronization
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_PH	DPH	AUS	error flag: phase sensor
E_PH2	DPH	AUS	error flag: phase sensor 2
PHPW	DPH	LOK	Slopes of phase signal (8 bit shifting)
PHPW2	DPH	LOK	Slopes of phase signal 2 (8 bit shifting)
R_SYNPH	GGDPG	EIN	synchro schedule for phase scan
R_SYNPH2	GGDPG	EIN	synchro schedule for phase scan 2
R_T100		EIN	Time schedule 100 ms
SFPPH	DPH	AUS	status fault path: phase sensor
SFPPH2	DPH	AUS	status fault path: phase sensor
SY_PG2AD	PROKON	EIN	system constant: kind of the phase signal
SY_PG2AD2	PROKON	EIN	system constant: kind of the 2. phase signal
SY_PH2OFST	PROKON	EIN	system const. offset in syncros between the 2 active phase signals,2 PGs only
ZPHNOK	DPH	LOK	Counter fault of phase signal
ZPHNOK2	DPH	LOK	Counter fault of phase signal 2
ZRPH	GGDPG	EIN	counter schedule of phase signal
ZRPH2	GGDPG	EIN	counter schedule of phase signal 2
Z_PH	DPH	AUS	cycle flag: phase sensor
Z_PH2	DPH	AUS	cycle flag: phase sensor 2

### FW DPH 22.10 Fixed Values

Parameter	Value	Description
CDTPH		code word tester: phase sensor
CDTPH2		code word tester: phase sensor 2
CLAPH		fault class: phase sensor
CLAPH2		fault class: phase sensor 2
PHNOKA		start value for counter phase signal not ok
TSFPH		fault active time: phase sensor
TSFPH2		fault active time: phase sensor 2

### FB DPH 22.10 Detailed description of function

The current level of the PG is entered into a shift register (phpw\*) in the synchro grid for phase inquiry (R\_synph\*). During the next R\_synph\* schedule the content of the register is shifted and the new PG level is recorded.

Thus, under normal conditions, the 8-bit register is allocated with 01010101 or 10101010.

If this register allocation is not given a PG fault exists:

Register contents	Fault
1111 1111 and no phase edges	-> B_mx*** Max fault (e. g. short circuit to UB)
0000 0000 and no phase edges	-> B_mn*** Min fault (e. g. short circuit to ground)
1111 1111 or 0000 0000 and phase edges	-> B_si*** Signal fault (e. g. wrong mounted PG*)
not equal 0101 0101 or not equal 1010 1010	-> B_np*** Plausibility fault (e. g. intermittend contact)
0101 0101 = 85 dez or 1010 1010 = 170 dez	-> no fault or fault healing

At the same time the number of fault occurrences are counted (zphnok\*), during which no change of level is detectable in the synchro grid for phase inquiry (R\_synph\*). If the downward counter zphnok\* reaches the value 0 then in connection with the above-described fault type a fault is set (E\_\*\* = 1, Z\_\*\* = 1, B\_\*\*\*\* = 1).



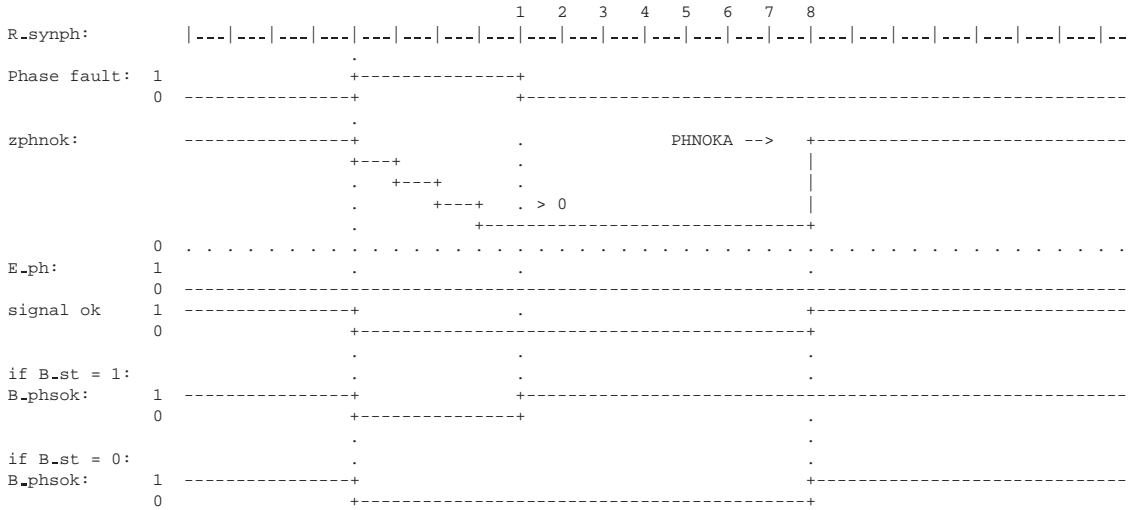
In the initialization (C\_inisyn), when deleting the error B\_clph\* or at a correct PG\*-signal the fault counter (zphnok\*) gets the starting value PHNOKA. This value is also set, as soon as one of the fault types B\_mxp\* or B\_mnp\* changes from 1 to 0 (disabling the fault type B\_siph\* during fault healing).

During the start of the engine it is important to obtain information about the functioning of the PG as quickly as possible (before the entire shift register has been filled). B\_phsok\* (phase sensor PG\* OK) is initialized during C\_ini and C\_inisyn from E\_ph\*. This condition is reset as soon as the first missing phase change is detected.

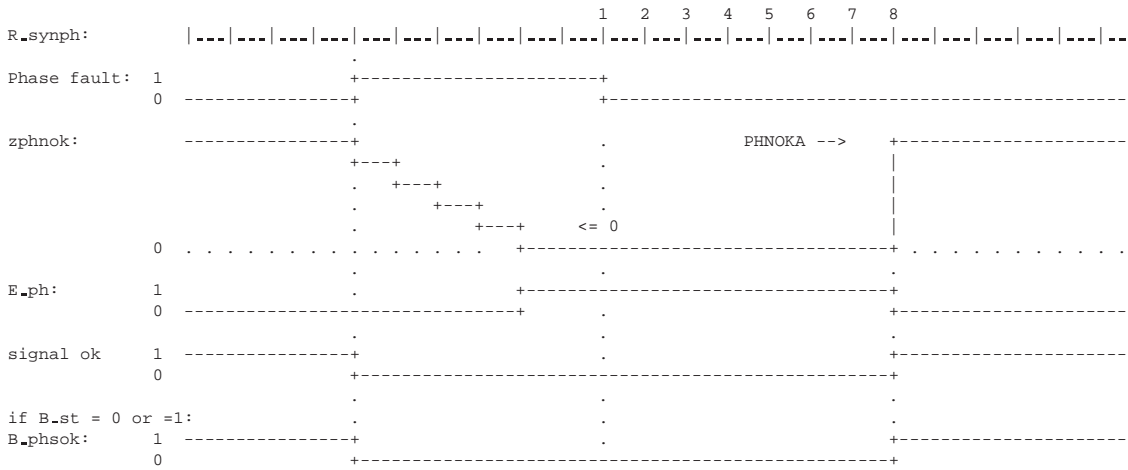
For the setting and resetting of B\_phsok\* the last two entries of the shift register are used. In order to guarantee the correct setting of B\_phsok\*, the condition is first calculated after C\_inisyn (e.g. while the engine starts) at the second R\_synph\*. At the first R\_synph\* there is no sufficient information.

Case example for B\_phsok:

Case 1: No fault entry is yet made in E\_ph:



Case 2: A fault entry is done in E\_ph:



signal ok => 1 means: Contents of the shift register is 01010101 or 10101010  
=> 0 otherwise

### APP DPH 22.10 Application hint

PHNOKA: 12 (> 7, so that the correct fault type is entered in B\_mx\*\*, B\_mn\*\*, B\_np\*\* or B\_si\*\*)

Function test:

1. Measurement values:

digital values: B\_phase, B\_phsok, B\_st, E\_ph, Z\_ph, B\_npph, B\_mnp, B\_mxp, B\_siph  
phpw.0 (bit 0), phpw.1 (bit 1), ..

analog values: zphnok (0..20), zzy1 (0..20), phpw (0..260), nmot (0..2000),  
if required: PH and NBM via analog card (VADI)

Measurement grid: 10 ms



## 2. Measurement sequence:

### 2.1 Test of signal position:

procedure: start engine, during engine operation connect the phase signal as follows:

- Disconnection of the phase signal at the ECU-adapter: --> B\_phase=0, E\_ph=1, B\_mnp=1, phpw=0
- Phase short circuit to ground: --> B\_phase=1, E\_ph=1, B\_mxph=1, phpw=255
- Phase short circuit to UB/cable drop-off: --> B\_phase=\*, E\_ph=1, B\_npph=1, 0 < phpw < 255
- Phase loose contact: --> B\_phase=alternating, E\_ph=0, phpw=85 V phpw=170
- Phase ok: --> phpw.0=B\_phase
- Phase signal fault: --> B\_phase=const(0 or 1), E\_ph=1, B\_siph=1, phpw=0 or 255

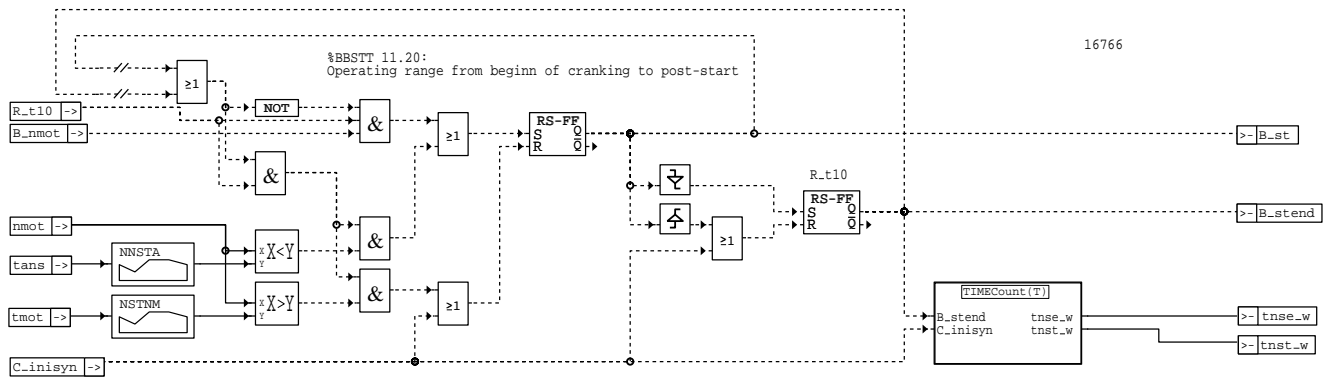
The fault type B\_siph = 1 can only occur at a wrong mounted phase sensor. To test this, the signal needs to be shifted so that no alternating phase level appears.

### 2.2 Fault entry, fault healing:

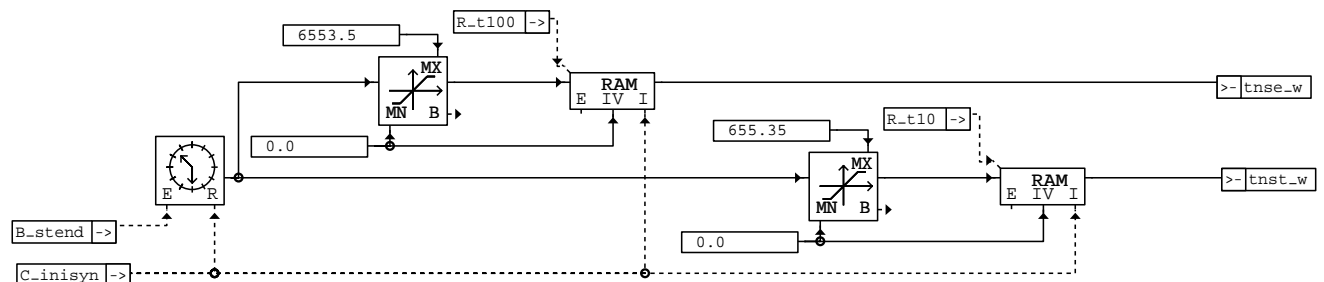
- Engine operation with phase ok: --> B\_phsok=1, E\_ph=0
- Engine stop/start (phase ok): --> B\_phsok=1, E\_ph=0
- Transition from phase ok to "not ok": --> B\_phsok=0, if zphnok=0: E\_ph=1
- Engine stop/start (phase not ok): --> B\_phsok=0, E\_ph=1
- Transition from phase "not ok" to ok: --> after 8 alternating entries in phpw: E\_ph=0, B\_phsok=1
- Engine stop/start (phase ok): --> B\_phsok=1, E\_ph=0
- Transition from phase ok to "not ok": --> B\_phsok=0, if zphnok=0: E\_ph=1
- Engine stop, after KL15 off: phase ok
- Engine start (phase ok): --> B\_phsok=0, E\_ph=1
- after 8 alternating entries in phpw: E\_ph=0, B\_phsok=1

## BBSTT 11.20 Condition Engine start

### DFE BBSTT 11.20 Function definition



#### bbst-bbst



#### bbst-timecount

Start condition B\_st: - B\_st is set if after KL15 On the start detection is completed and the engine is cranking (!B\_nmin).  
- B\_st is reset when the start end speed NSTNM is exceeded. The start condition applies again if the engine speed drops below NNSTA.

Time after start tnst\_w: At the end of start, the post-start time tnst\_w is initiated. As soon as the maximum value of tnst\_w is reached, tnst\_w is limited to this value (dito tnse\_w).



### ABK BBSTT 11.20 Abbreviations

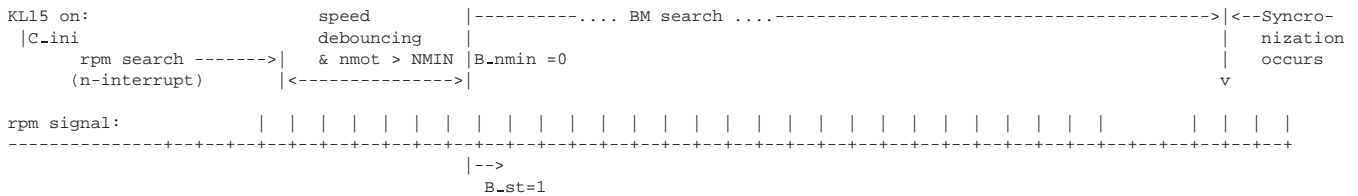
Parameter	Source-X	Source-Y	Type	Description
NNSTA	TANS		KL	engine-speed transition normal -> start
NSTNM	TMOT		KL	transition start -> normal
Variable	Source		Type	Description
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_ST	BBSTT		AUS	condition for start
B_STEND	BBSTT		AUS	condition end of start
C_JNISYN			EIN	ECU-condition for intialisation of angle synchronization
NMOT	SWADAP		EIN	engine speed
R_T10			EIN	Time schedule 10 ms
R_T100			EIN	Time schedule 100 ms
TANS	SWADAP		EIN	Intake air temperature
TMOT	SWADAP		EIN	Engine temperature
TNSE_W	BBSTT		AUS	time counter at end of start (16 bit)
TNST_W	BBSTT		AUS	time after end of start

### FW BBSTT 11.20 Fixed Values

Parameter	Value	Description
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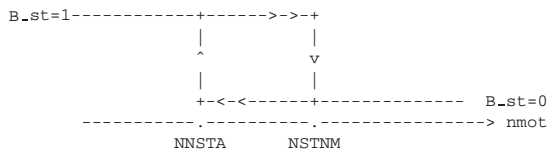
### FB BBSTT 11.20 Detailed description of function

1. Transition from initialization to start: start process (overview):

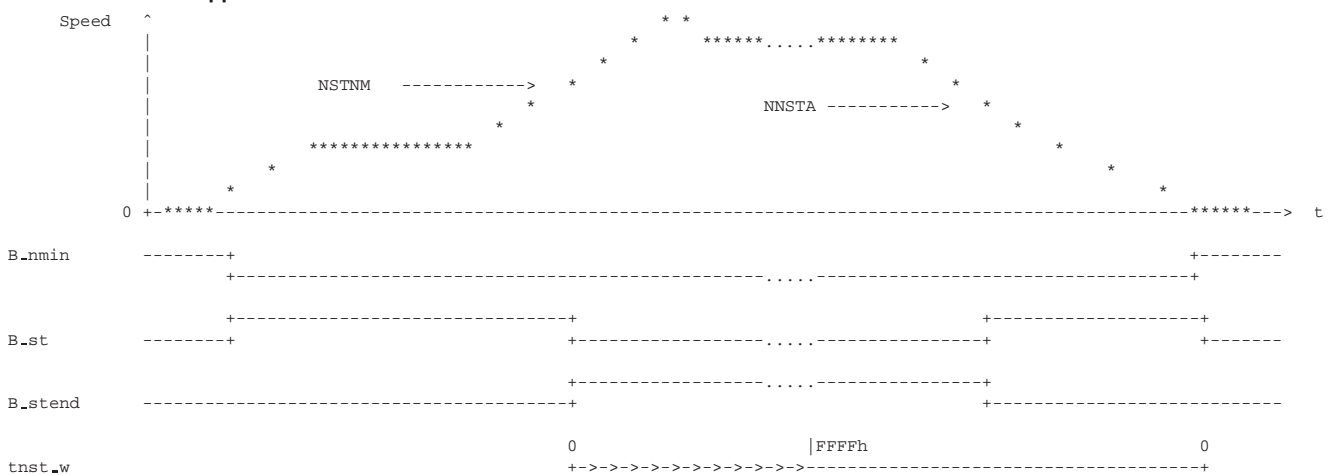


After initialization the tooth interrupt is enabled and the system is waiting for the first rpm signal. With the first rpm signal the speed debouncing is initiated. After the rpm signal is debounced and the minimum engine speed is exceeded, the start condition is set.

2. Transition from start to post-start:



### APP BBSTT 11.20 Application hint



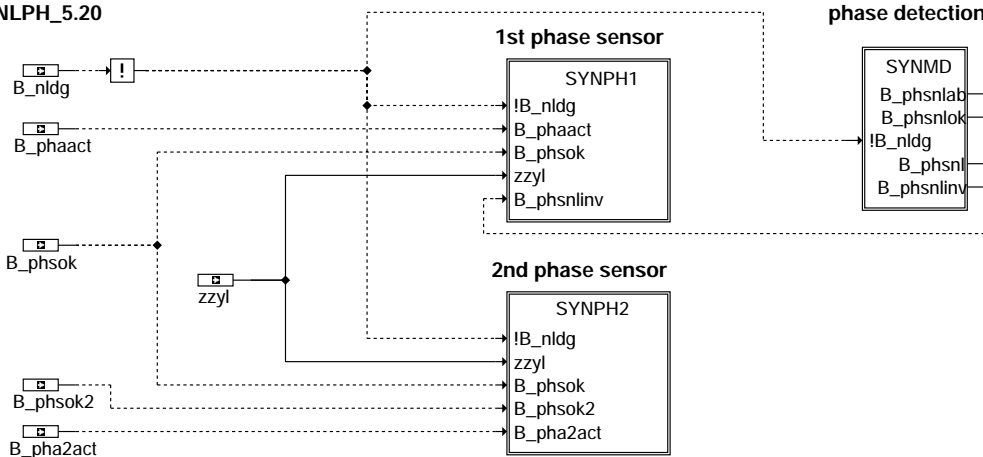
## NLPH 5.20 limp-home for phase synchronization

### FDEF NLPH 5.20 Function definition

The section NLPH describes the checking of the synchronization by means of the correctly operating phase sensors given in the system. The cylinder counter zzyl is initialized from the phase information during the synchronization in %GGDPG. With defective phase sensor (PG) and not defective phase sensor 2 (PG2) (SY\_PGRAD2 > 0 and B\_phsok2) the latter is used for the synchronization (SYNPH2). If the PG2 signal also lies above the reference mark (SY\_PH2OFST = 0), then it is possible to synchronize directly to PG2 with defective PG. Otherwise always PG is synchronized to and in the cycle R\_synph2 PG2 is used to check for correct synchronization and to trigger a new synchronization (SYNPH1) if necessary. If no PG2 is given or if it is also defective the cylinder counter is initialized from the virtual engine position, provided the run-on position is valid (B\_ale = 1).

At not clear phase position it is optionally possible to cause a double ignition output and by means of injection cut-out misfiring can be stimulated, by the evaluation of which the correct phase position can be determined and possibly a new synchronization is started (SYNMD).

### NLPH\_5.20

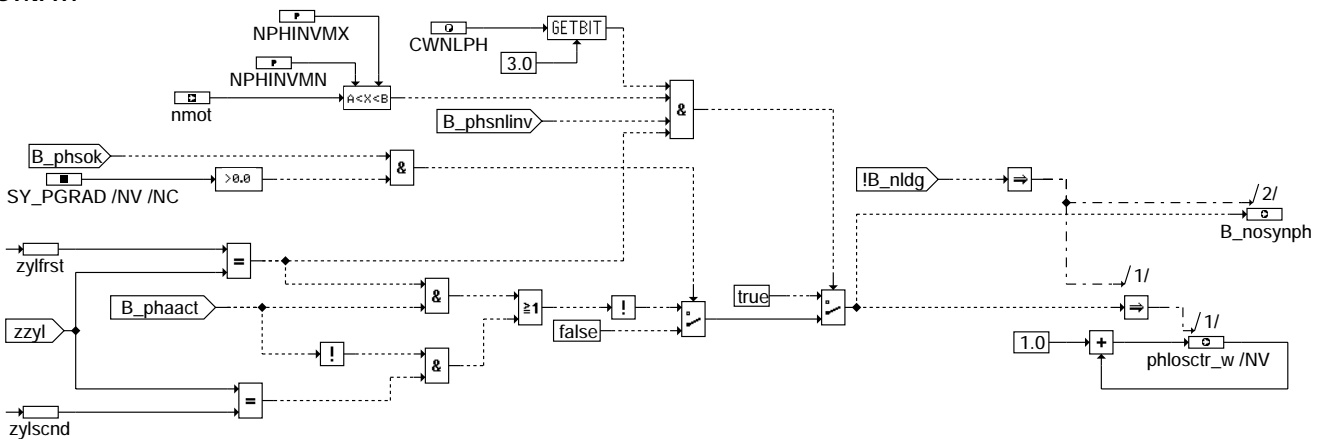


nlph-main

### Subfunction Block SYNPH1

The function SYNPH1 is calculated in the synchro cycle for the phase inquiry of the phase sensor PG1. With correctly operating PG1 the cylinder number zzyl is compared to the cylinder number of the phase position of the PG1. If the phase position does not agree an immediate new synchronization is triggered via B\_nosynph. If it was detected in PHNLERK that the phase position is not correct then the new synchronization is triggered also here.

### SYNPH1



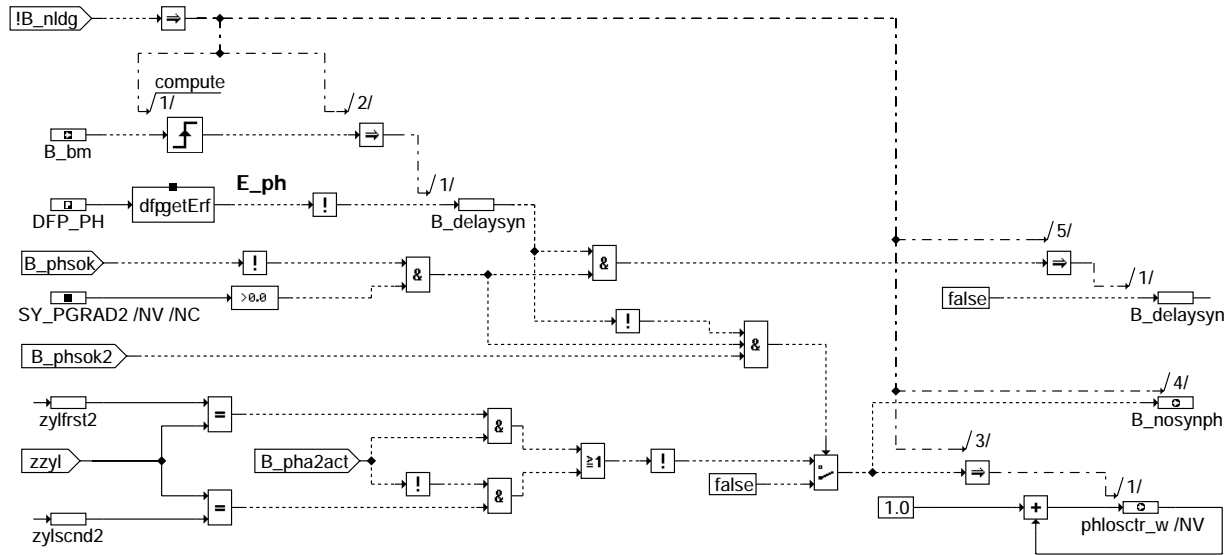
nlph-synph1



Subfunction Block SYNPH2

At given PG2 and defective PG the function is calculated in the synchro cycle for the phase inquiry of the PG2. With correctly operating PG2 and inactive B\_delaysyn the cylinder number zzyl is compared to the cylinder number of the phase position for PG2. If the phase position does not agree a new synchronization is triggered via B\_nosynph. At active B\_delaysyn the check is not performed but B\_delaysyn is reset. This causes the synchronization check being delayed by one reference mark. Thereby a possible new synchronization is also delayed by one reference mark cycle and thus it is performed 3 reference marks later.

**SYNPH2**



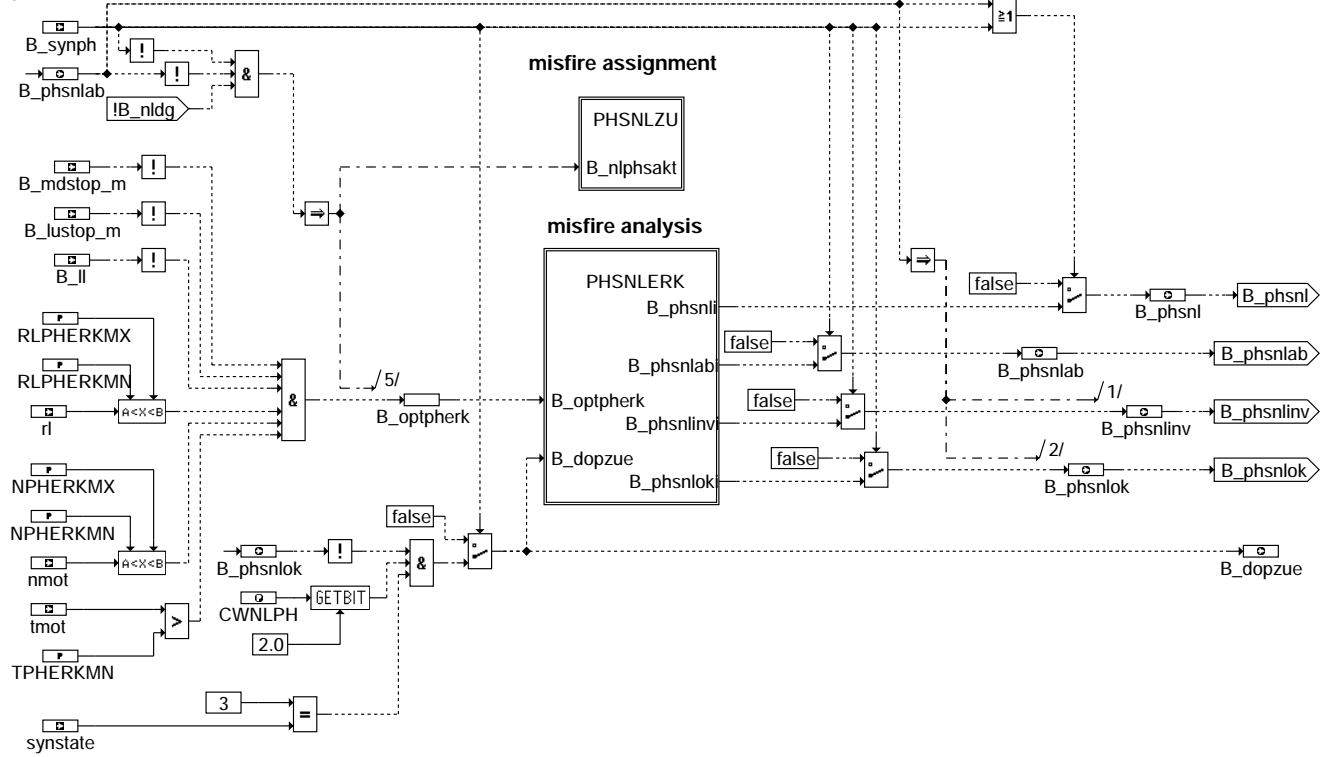
**nlph-synph2**

Subfunction Block SYNMD

SYNMD decides by means of the operating parameters of the engine and the readiness bits of the misfire detection on a possible phase detection and on the output of the double ignition.

The bit B\_dopzue is set in the first synchro after found reference mark (BM), if B\_synph = FALSE. Due to the sequence of the processes, however, the double ignition is only outputted in the next synchro (second synchro).

## SYNMD



## nlph-synmd

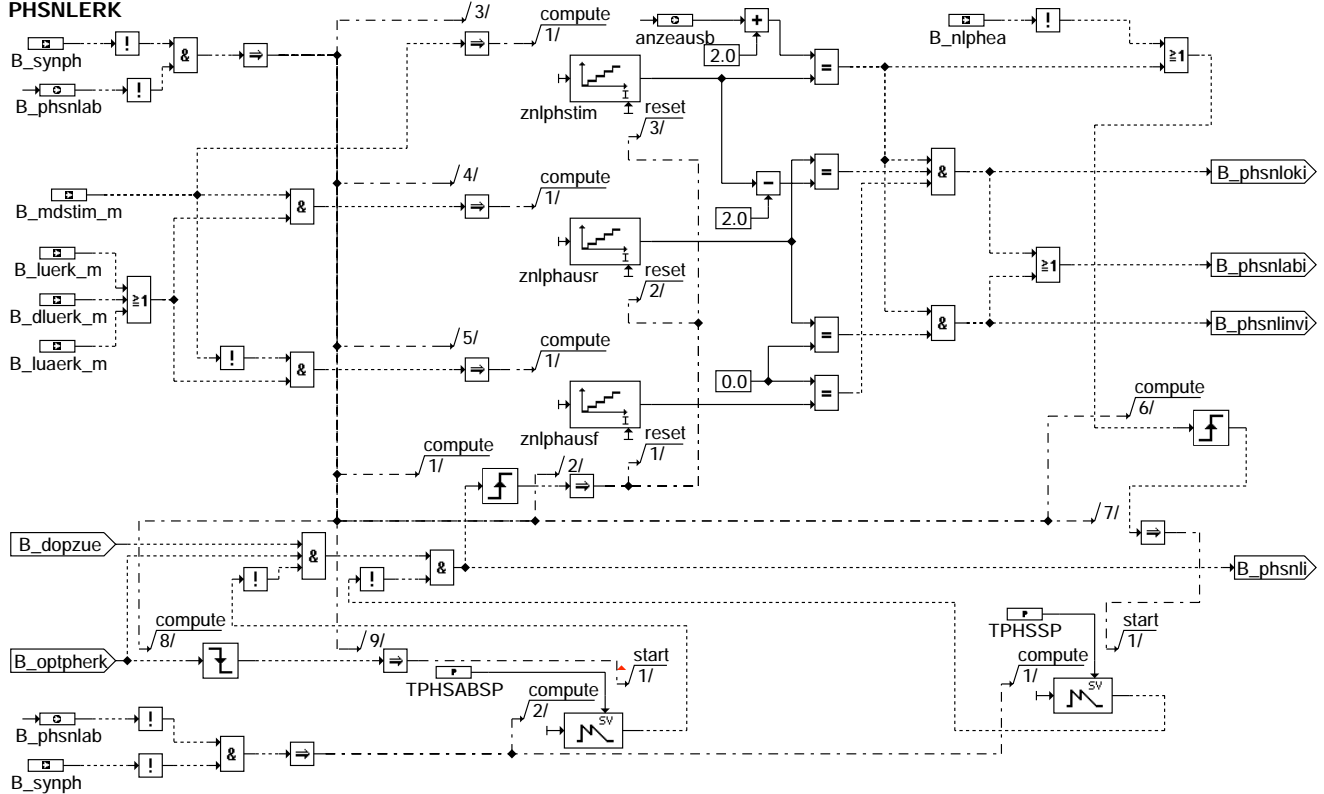
### Subfunction Block PHSNLERK

By comparison of the stimulated misfiring with the detected misfiring it is checked whether the present phase position is correct, incorrect or whether it cannot be precisely decided upon. If the bit patterns of stimulation and detection agree, the phase position is correct. The phase position is incorrect if there is no agreement. By means of the two timers it is possible to delay another detection.

nlph-synmd



### PHSNLERK

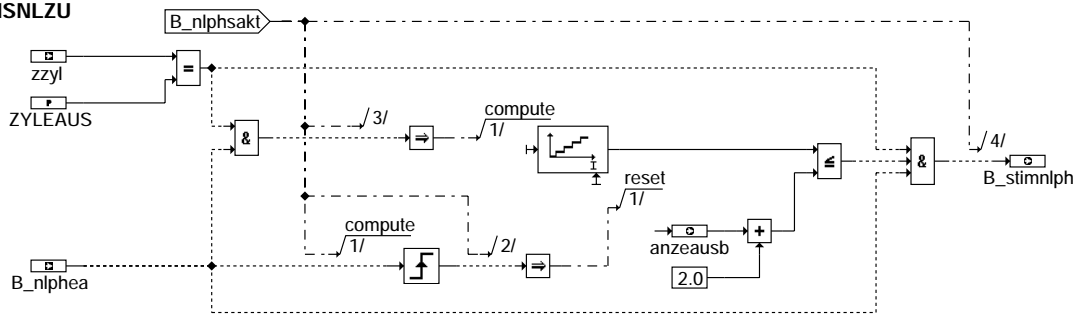


### nlph-phnslerk

#### Subfunction Block PHSNLZU

By the pieces of information injection cut-out started, cylinder counter and cylinders to be cut-out a bit pattern is generated for the misfire detection so that it can supply the bit B\_mdstim.m needed in PHSNLERK. B\_stimnlph is generated twice as many times as misfires occur, since the first injection cut-out will not lead to misfiring in the present and possibly also not in the next working cycle but only in the one after that (pre-injection etc.)

### PHSNLZU



### nlph-phnslzu

#### ABK NLPH 5.20 Abbreviations

Abbreviation Description

Variable	TYPE	Description
ZYL_FRST	const	Cylinder counter for segment with active PG signal ( zzy1 = 0 )
ZYL_SCND	const	Cylinder counter for segment with inactive PG signal ( zzy1 = int((SY_ZYLZA + 1) / 2) )
ZYL_FRST2	const	Cylinder counter for segment with active PG2 signal ( zzy1 = ZYL_FRST + SY_PH2OFST )
ZYL_SCND2	const	Cylinder counter for segment with inactive PG2 signal ( zzy1 = ZYL_SCND + SY_PH2OFST )

Parameter	Source-X	Source-Y	Type	Description
ANZEAUS			FW	number of the injections to fade out
CWNLPH			FW	release of the specific phase sensor limp home function



Parameter	Source-X	Source-Y	Type	Description
NPHERKMN			FW	minimal engine speed for phase detection
NPHERKMX			FW	maximum engine speed for phase detection
NPHINVMN			FW	minimal engine speed for initialisation
NPHINVMX			FW	maximum engine speed for initialisation
RLPHERKMN			FW	minimal load for phase detection
RLPHERKMX			FW	maximum load for phase detection
SY_PGRAD			SYS (REF)	system constant: kind of the phase signal
SY_PGRAD2			SYS (REF)	system constant: kind of the 2. phase signal
SY_PH2OFST			SYS (REF)	system const. offset in syncros between the 2 active phase signals,2 PGs only
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TPHERKMN			FW	minimal engine temperature for phase detection
TPHSABSP			FW	lockout time for phase detection, after leaving the suitable operating range
TPHSSP			FW	lockout time for phase detection after unsuccessful detection
ZYLEAUS			FW	cylinder to fade out

Variable	Source	Type	Description
ANZEAUSB	NLPH	AUS	number of injections to fade out; limited between 4 and 7
B_BM	GGDPG	EIN	condition reference mark detected
B_CLPH		EIN	condition clear fault path PH
B_DELAYSYN	NLPH	LOK	Flag for delaying a re-synchronisation by 1 synchronisation gap
B_DLUERK_M		EIN	monitor, misfire detected in DMDDL
B_DOPZUE	NLPH	AUS	Condition double ignition
B_LL	MSF	EIN	Condition idle
B_LUAERK_M		EIN	monitor, misfire detected in DMDLUA
B_LUERK_M		EIN	monitor, condition for misfire detected in DMDLU
B_LUSTOP_M		EIN	misfire detection stop, monitor value
B_MDSTIM_M		EIN	monitor, cond. for stimulated ignition misfiring, stimuli-signal from ZAG
B_MDSTOP_M		EIN	monitor, misfire detection stopped
B_NLDG		EIN	condition limp-home function speed sensor
B_NLPH	NLPH	AUS	condition no signal from the phase sensors
B_NLPHEA	AEVAB	EIN	Injector deactivation for limp-home phase synchronization active
B_NOSYNPH	NLPH	AUS	Flag for wrong cylindernumber at synchronisation-gap
B_OPTPHERK	NLPH	LOK	condition suitable engine operating state for phase detection
B_PHA2ACT	GGDPG	EIN	condition signal of phase sensor 2 is high activ
B_PHAACT	GGDPG	EIN	condition signal of phase sensor 1 is high activ
B_PHSNL	NLPH	AUS	Condition phase search during phase sensor limp-home
B_PHSNLAB	NLPH	AUS	condition phase detection during phase sensor emergency operation finished
B_PHSNLINV	NLPH	AUS	condition invert phase relation
B_PHSNLOK	NLPH	AUS	condition phase detection during phase sensor emergency operation successful
B_PHSOK	DPH	EIN	Condition phase signal ok
B_PHSOK2	DPH	EIN	Condition phase signal 2 ok
B_PWF		EIN	Condition for powerfail
B_STIMNLPH	NLPH	AUS	condition misfire stimulated by NLPH
B_SYNPH	GGDPG	EIN	condition synchronization phase
DFP_PH	NLPH	DOK	ECU int. fault path no.: phase sensor
E_PH	DPH	EIN	error flag: phase sensor
NMOT	SWADAP	EIN	engine speed
NSYNNLPH	NLPH	LOK	Monitor for reasons of new synchronization at NLPH
PHLOSCTR_W	NLPH	AUS	counter re-synchronisation due to wrong synchronisation at reference gap (word)
RL	SWADAP	EIN	relative air charge
SYNSTATE		EIN	current mode of synchronization
TMOT	SWADAP	EIN	Engine temperature
ZNLPHAUSF	NLPH	LOK	Counter of detected misfire at wrong position
ZNLPHAUSR	NLPH	LOK	Counter of detected misfire at right position
ZNLPHSTIM	NLPH	LOK	Counter of stimulated Bits from misfire detection monitor
ZYLEAUSB	NLPH	AUS	cylinder to fade out; binary description
ZZYL	GGDPG	EIN	SW-cylinder counter

### FW NLPH 5.20 Fixed Values

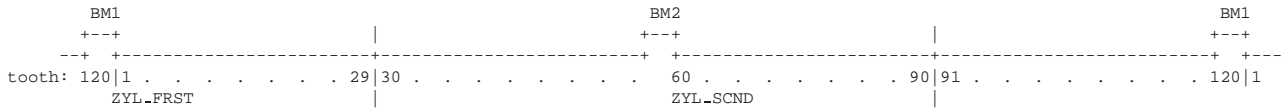
Parameter	Value	Description
ANZEAUS		number of the injections to fade out
CWNLPH		release of the specific phase sensor limp home function
NPHERKMN		minimal engine speed for phase detection
NPHERKMX		maximum engine speed for phase detection
NPHINVMN		minimal engine speed for initialisation
NPHINVMX		maximum engine speed for initialisation
RLPHERKMN		minimal load for phase detection
RLPHERKMX		maximum load for phase detection
TPHERKMN		minimal engine temperature for phase detection
TPHSABSP		lockout time for phase detection, after leaving the suitable operating range
TPHSSP		lockout time for phase detection after unsuccessful detection
ZYLEAUS		cylinder to fade out



## FB NLPH 5.20 Detailed description of function

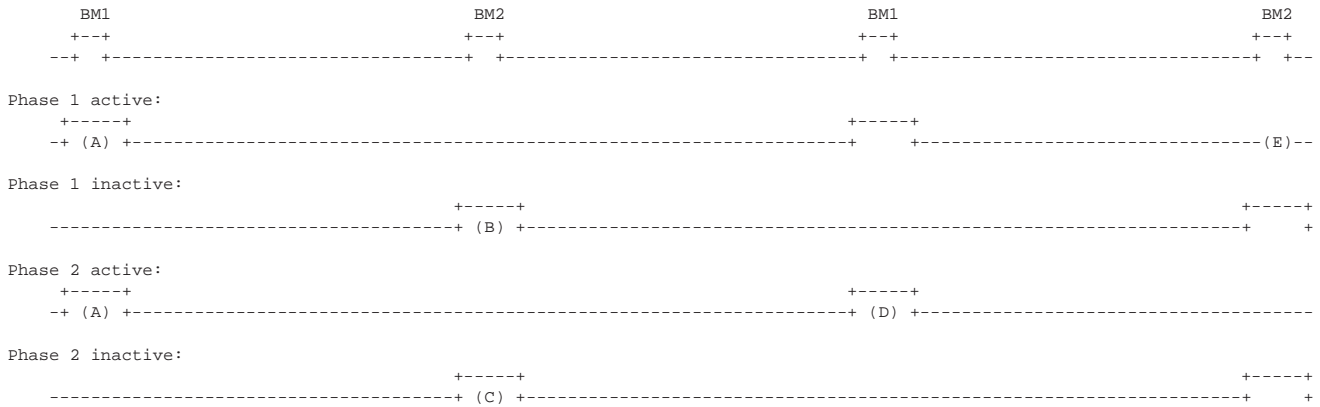
The function NLPH describes the synchronization monitoring by means of phase sensor PG1 resp. PG2. In case of incorrect synchronization a new synchronization is triggered. The initialization of the cylinder counter is performed in %GGDPG. In the process a distinction is made between 3 modes of operation:

1. Systems without second phase sensor (SY\_PGRAD2 = 0) resp. second phase sensor defective. With valid run-on detection the current tooth number is calculated via the virtual engine position. If this tooth lies between 30 and 90 then the engine lies within the synchronization range of ZYL\_SCND, otherwise ZYL\_FRST:



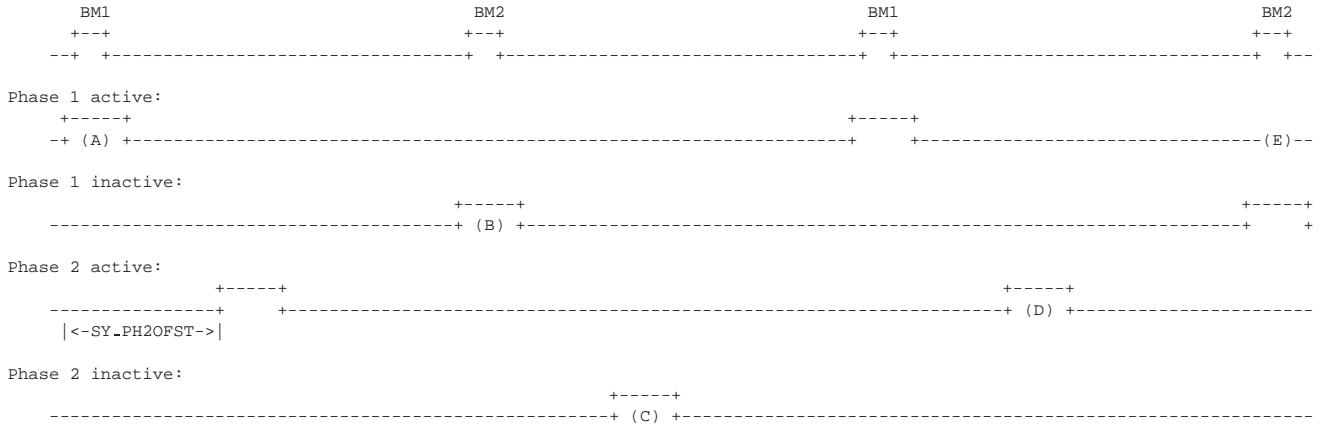
With invalid run-on detection zzyl is synchronized to ZYL\_FRST.

2. Systems with second phase sensor (SY\_PGRAD2 > 0) and phase position of PG2 above the reference mark (SY\_PH2OFST = 0).



With defective PG synchronization is performed directly to PG2 in the reference mark. If no fault entry of the phase sensor PG is given at engine start then synchronization to the latter is performed at the first reference mark (A) and the flag B.delaysyn is set. A defective PG is detected at the second reference mark (B) by B\_phase = false and a switch-over to PG2 is performed. B.delaysyn has the effect that the phase position is checked by means of PG2 only at the next reference mark (D). With incorrect synchronization a new synchronization is triggered by setting B\_nosynph. Since no PG fault entry is given up to this new synchronization, synchronizing is again performed to PG at the next reference mark (E). Since this reference mark has an inverse phase position with regard to (A) a correct synchronization is now performed.

3. Systems with second phase sensor (SY\_PGRAD2 > 0) with phase position of PG2 not above the reference mark. The system constant SY\_PH2OFST indicates the offset in segments between the active phase positions:



In this case synchronization cannot be performed via PG2. If no fault message is given at engine start then the bit B\_delaysyn is set and the engine is synchronized with PG (A). The defect of the phase sensor is only detected at the next reference mark by B\_phase = false (B). With defective PG the phase position for the phase inquiry of PG2 is checked only two segments later due to B\_delaysyn (D). If now an incorrect phase position is given then a new synchronization to PG is triggered by setting B\_nosynph. This new synchronization is performed at the next reference mark (E), where here the inverse phase position to the first synchronization (A) is now given and thereby a correct synchronization will be performed by the defective PG.

If no phase sensor is available and if the operations have been enabled via CWNLPH, the engine will start with double ignition output. In case the engine is at an appropriate operating point, a number of injections to be adjusted for a cylinder also to be defined will be cut-out in the function %AEVAB. Since the misfire detection operates in the background the bit B\_stimnlph is put at its disposal for the ignition-synchronous assignment in PHSNLZU. Then the bit patterns of stimulation and detected misfiring generated by it are to be compared (PHSNLERK). With correct phase position both are congruent. For this anzeausb cut-outs must have led to misfiring in the respective cylinder and no other misfiring may have occurred. On these conditions the double ignition output can be terminated. If no misfire is detected for the cut-out cylinder, the phase position is not correct. Dependent on the application of CWNLPH either a new synchronization to suitable phase position is triggered in SYNPH1, which hence leads to another check, or the double ignition output is maintained. Should it not be possible to precisely determine the phase position on above-mentioned conditions or should %AEVAB abort the injection cut-out early, the detection is aborted and at the earliest after TPHSSP another attempt is made. If the guidelines, which are required for a successful phase search, change during the detection this will lead to an abort. A new attempt is only possible at the earliest after TPHSABSP.

Monitor for New Synchronization  
=====

During a new synchronization relevant variables are initialized to neutral values. Since a new synchronization is performed immediately once the respective requirement is set, it can no longer be seen with VS100, which condition has requested the new synchronization. In order to make the search for faults easier a new-synchronization-monitor is therefore formed that makes it possible to capture the reason for the last new synchronization with VS100.

In the byte NSYNNLPH a bit is set to one at the corresponding position that indicates which condition has requested the new synchronization. The byte NSYNNLPH is always initialized in C.ini with 00000000.

- |          |       |  |
|----------|-------|--|
| NSYNNLPH | Bit 0 | New synchronization requested by B_nosynph (first phase sensor)                    |
|          | Bit 1 | New synchronization requested by B_nosynph (second phase sensor)                   |
|          | Bit 2 | not occupied   |
|          | Bit 3 | not occupied   |
|          | Bit 4 | New synchronization requested by B_nosynph (phase detection via misfire detection) |

If several new synchronizations occur during a driving cycle with various causes then it is also possible that several bits of NSYNNLPH are set to one.

## APP NLPH 5.20 Application hint

With double ignition output it may be necessary to decrease the maximum engine speed (NMAXDZ) in order to protect components.

Allocation of CWNLPH (condition: respective bit = 1):

- 0. Bit: not occupied
  - 1. Bit: run-on detection permissible
  - 2. Bit: limp-home via double ignition (NLPH 5.10)
  - 3. Bit: new synchronization after detection by means of cylinder cut-out permissible
- The remaining bits are still free.

The cylinder cut-out can be disabled by a limitation of the operating map.

Typical Values:

-----

ANZEAUS:	5	Number of injections to be cut-out
NPHERKMN:	2000 rpm	Minimum engine speed for phase search
NPHERKMX:	4000 rpm	Maximum engine speed for phase search
NPHINVNM:	2520 rpm	Minimum engine speed for new synchronization
NPHINVMX:	3520 rpm	Maximum engine speed for new synchronization
RLPHERKMN:	40 %	Minimum load for phase search
RLPHERKMX:	60 %	Maximum load for phase search
TPHERKMN:	80 °C	Minimum engine temperature for phase search
TPHSABSP:	10 s	Blocking time for the phase search, if the appropriate operating range was exited (should not be chosen too high!)
TPHSSP:	60 s	Blocking time for phase search after unsuccessful search
ZYLEAUS:	0	Cylinder to be cut-out

The number of injections to be cut-out is to be limited between 4 to 7.

For ZYLEAUS a 0 is to be entered for the 1st cylinder and so on until n-1 for the nth cylinder.

Adjustable variables in other functions for NLPH:

%NMAXMD	NMAXDZ	Half the maximum engine speed, e.g. 3400 rpm for systems with single-spark coils Maximum engine speed, e.g. 6800 rpm for systems with twin-spark coils
	DNMADZ	10 corresponds to a ramp of 1000 rpm
%GGDFG	DZZSTNLP	116 corresponds to 2 engine revolutions

## NLDG 2.10 limp-home for defective engine speed sensor

### FDEF NLDG 2.10 Function definition

Dummy Modul

-----

This modul doesn't include any functionality of a limp home function for the crankshaft position sensor. There is only a definition of some variables which are used in other functions. These variables are set to default values:

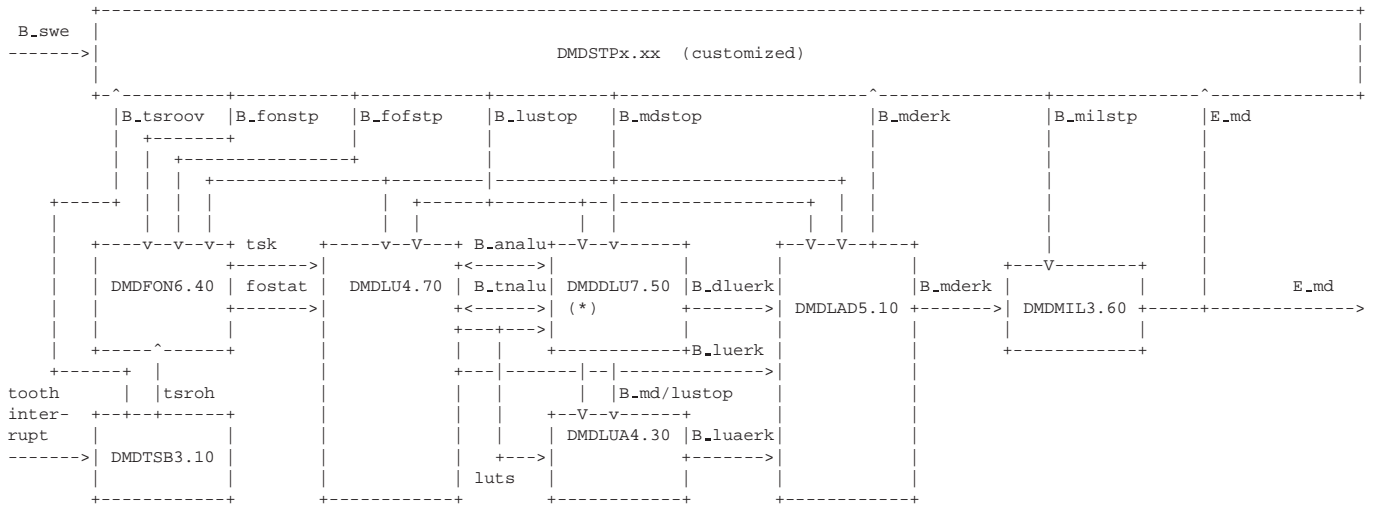
```
B_synnlldg = false
B_nldg = false
B_phnldg = false
zphflsyn = 0
```



## DMDUE 9.120 Diagnostic routine misfire detection Overview

### FDEF DMDUE 9.120 Function definition

modular concept misfire detection



\* function only for engines with even number of cylinders

With the Codeword CDMD the whole misfire detection can be stopped.  
If B\_cdmd=0, misfire detection is stopped and E\_ase=0, E\_ask=0, Z\_ase=1, Z\_ask=1, B\_mderk=0.  
For B\_cdmd=1 misfire detection is active.

In case of 2 ecu's (SY\_2SG = 1) all function except of %DMDSTP are deactivated in the Master-ECU (B\_master = 1) and are calculated in the Slave-ECU (B\_master = 0).  
The Stop-Conditions have to be transmitted via CAN from the Master-ECU to the Slave-ECU. The Slave-ECU has to evaluate the stop-conditions from the Master-ECU.

To ensure correct function of the misfire-detection algorithms the system for measuring the segment durations (speed sensor, sensor wheel) has to met the following specifications:

- Chapter: Komponenten Gruppe Sensoren  
Designation: KGS\_DG  
Title: Eingeber-Inkrementsystem
- Geberradspezifikation zur Aussetzererkennung über Drehzahlerfassung

### ABK DMDUE 9.120 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDMD			FW	code word DMD inactive(EURO-coding), CD.=0 -> no diagnosis
Variable	Source		Type	Description
B_CDMD	PROKON		EIN	function active per codeword CDMD
B_MASTER			EIN	Condition MASTER-ECU
B_MDSTIM_M	DMDUE		LOK	monitor, cond. for stimulated ignition misfiring, stimuli-signal from ZAG
B_MDZYL1_M	DMDUE		LOK	monitor, cylinder 1 identification
B_PHSNL	NLPH		EIN	Condition phase search during phase sensor limp-home
B_ZASA_M	DMDUE		LOK	monitor, ZAS load switchover is active
FDMD_M	DMDUE		LOK	status diagnosis misfire detection, drum, delayed output
FLG_M	DMDUE		LOK	monitor status calculation of the engine roughness
SY_2SG	PROKON		EIN	system constant 2 motronic systems

### FW DMDUE 9.120 Fixed Values

Parameter	Value	Description
CDMD		code word DMD inactive(EURO-coding), CD.=0 -> no diagnosis

### FB DMDUE 9.120 Detailed description of function

The description can be found in the single function-descriptions

This function only describes the interface between the different functions.





## FW DMDTSB 3.10 Fixed Values

Parameter	Value	Description
KAMFZ		start of sampling segment time monitoring misfire detection

## FB DMDTSB 3.10 Detailed description of function

The beginning of the measuring window (= segment start) can be shifted via KAMFZ in 6 deg. crankshaft angle (CA) steps (corresponds to one tooth).

KAMFZ gives the beginning of the measuring window in deg. CA before DTC. KAMFZ is limited by the software to the following values:

$$\begin{aligned} \text{KAMFZ,max} &= \text{SY\_GRDWRT} + (\text{segment length in no. of teeth} - 1) * 6 \text{ deg. CA} \\ \text{KAMFZ,min} &= \text{SY\_GRDWRT} - (\text{segment length in no. of teeth} - 1) * 6 \text{ deg. CA} \end{aligned}$$

(KAMFZ is a signed value!; SY\_GRDWRT is the distance R\_syn (tr-mark) to DTC)

The length of the measuring window in deg. CA is dependent on the amount of cylinders. It corresponds to the distance between two DTCs:

$$\text{Length of measuring window} = 360 / (\text{SY\_ZYLZA} / 2) \text{ deg. CA.}$$

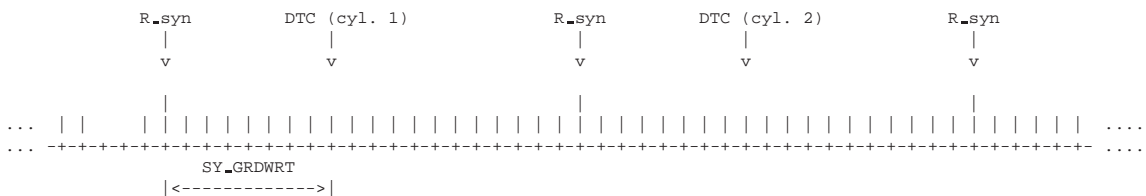
For the quantization of tsroh\_w (tsroh2\_w) two system frequencies are distinguished (20 MHz, 24 MHz, see table).

Quantization for tsroh\_w (tsroh2\_w):

cylinder number	system frequency	
	20 MHz (SY_FREQCPU = 20 000) tsquant = 0,8 us	24 MHz (SY_FREQCPU = 24 000) tsquant = 0,666 us
3	3/2 * tsquant	3/2 * tsquant
4	3/2 * tsquant	4/3 * tsquant
5	1 * tsquant	4/3 * tsquant
6	1 * tsquant	1 * tsquant
8	1 * tsquant	1 * tsquant
12	1 * tsquant	1 * tsquant

In case of segment time overflow, i.e. tsroh\_w or tsroh2\_w can no longer be represented as 16 bit value, the condition B\_tsroov (ts-overflow) is set and tsroh\_w resp. tsroh2\_w is limited to maximum value.

CA signal (ex. 6-cyl.):



Ex. 1:  $\text{KAMFZ} = 30 \text{ deg. CA} (= 5 \text{ teeth} * 6 \text{ deg. CA})$

segment pos. for tsroh\_w of cyl. 1      segment pos. for tsroh\_w of cyl. 2

Ex. 2:  $\text{KAMFZ} = -12 \text{ deg. CA} (= 2 \text{ teeth} * 6 \text{ deg. CA} * \text{neg. direction})$

segment pos. for tsroh\_w of cyl. 1      segment pos. for tsroh\_w of cyl. 2







## ABK DMDFON 6.40 Abbreviations

Indices and reference points used:

- (n) = Crankshaft segments
- (i) = Camshaft revolutions; NW - rev.
- (j) = Crankshaft revolutions; KW - rev.
- (t) = Time

ts(n)	Segment duration of Crankshaft segment n
ts(n+1)	Segment duration of Crankshaft segment n+1
zylza	Number of cylinders
Zdg.	Ignition, is counted through in ignition order
xx	Operating ranges (speed, load)
nn	Engine speed range

Parameter	Source-X	Source-Y	Type	Description
ALFO			FW	start value for learning filter at fuel-on/fuel-off adaptation
ANWFOHE			FW	number of camshaft rotations for healing
ANWFOST			FW	number of camshaft rotations for reactivation the adaptation after disabling
CDFO			FW	code to deactivate and reset the adaptation
DFSEFO2N	NMOT		KL	max. plausible speed-dependent variance of FSE values
DFSEFON	NMOT		KL	max. plausible speed-dependent variance of FSE values
DFSERES			FW	difference of adaptation values to reset fuel-on/-off adaptation
FLFO			FW	filter factor for learningfilter of fuel-on/-off adaptation
FS1FO			FW	filter factor segment duration filter 1 of fuel-on/-off adaptation
FS2FO			FW	filter factor segment duration filter 2 of fuel-on/-off adaptation
KFCFO	NMOT	RL	KF	map for definition of range characteristics (dominant..)
KFCFO2	NMOT	RL	KF	map for definition of range characteristics (dominant..)
LURFOST			FW	engine roughness referenz value for stop of the fuel-on/-off adaptation
MDERFOKH			FW	number of misfires to stop adaptation (healing) when B_kh = 1
MDERKFON			FW	number of misfires to stop adaptation (healing)
SLFOO2N	NMOT		KL	speed dep. upper threshold for learning filter value at fuel-on/-off adaptation
SLFOON	NMOT		KL	speed dep. upper threshold for learning filter value at fuel-on/-off adaptation
SLFOU			FW	lower threshold for learning filter value at fuel-on/-off adaptation
TNSTFON			FW	time after engine start to enable adaptation stop (healing)

Variable	Source	Type	Description
ANWFOH	DMDFON	LOK	counts number of camshaft rotations for healing of fuel-on/-off adaptation
ANWFOS	DMDFON	LOK	counts number of camshaft rot.(conditions for adapt. OK to beginning of learning)
B_AUTGET	PROKON	EIN	condition automatic gearbox
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_FODO	DMDFON	LOK	condition fuel-on/-off adaptation in a dominant operating range active
B_FODON	DMDFON	LOK	condition fuel-on adaptation in a speed dominant operating range active
B_FOF	DMDFON	DOK	condition fuel-off adaptation active
B_FOFSTP	DMDSTP	EIN	condition fuel-off adaptation stopped
B_FOFJM	DMDFON	LOK	monitor, condition fuel-off adaptation active
B_FOHE	DMDFON	LOK	actual range is a healing range
B_FOHOLD	DMDFON	LOK	fuel-on adaptation deactivated
B_FOLUNW	DMDFON	LOK	condition to large for fuel-on/-off adaptation
B_FON	DMDFON	DOK	condition fuel-on adaptation active
B_FONSTP	DMDSTP	EIN	condition fuel-on adaptation stopped
B_FONTM	DMDFON	LOK	engine temperature high enough for fuel-on-adaption
B_FONJM	DMDFON	LOK	monitor, condition fuel-on adaptation active
B_FOR	DMDFON	DOK	condition fuel-on/-off adaptation actual ready
B_FOR11	DMDFON	LOK	map range 11 ready
B_FOR12	DMDFON	LOK	map range 12 ready
B_FOR13	DMDFON	LOK	map range 13 ready
B_FOR21	DMDFON	LOK	map range 21 ready
B_FOR22	DMDFON	LOK	map range 22 ready
B_FOR23	DMDFON	LOK	map range 23 ready
B_FOR31	DMDFON	LOK	KF range 31 already learned
B_FOR32	DMDFON	LOK	KF range 32 already learned
B_FOR33	DMDFON	LOK	KF range 33 already learned
B_FOR41	DMDFON	LOK	KF range 41 already learned
B_FOR42	DMDFON	LOK	KF range 42 already learned
B_FOR43	DMDFON	LOK	KF range 43 already learned
B_FOR51	DMDFON	LOK	KF range 51 already learned
B_FOR52	DMDFON	LOK	KF range 52 already learned
B_FOR53	DMDFON	LOK	KF range 53 already learned
B_FOR61	DMDFON	LOK	KF range 61 already learned
B_FOR62	DMDFON	LOK	KF range 62 already learned
B_FOR63	DMDFON	LOK	KF range 63 already learned
B_FOR71	DMDFON	LOK	KF range 71 already learned
B_FOR72	DMDFON	LOK	KF range 72 already learned
B_FOR73	DMDFON	LOK	KF range 73 already learned
B_FOR81	DMDFON	LOK	KF range 81 already learned
B_FOR82	DMDFON	LOK	KF range 82 already learned
B_FOR83	DMDFON	LOK	KF range 83 already learned
B_FORDO	DMDFON	DOK	condition fuel-on/-off adaptation in at least one dominant range ready
B_FORDOMJ	DMDFON	LOK	monitor, cond. adaptation in at least one dominant range ready
B_FORN	DMDFON	DOK	condition fuel-on/-off adaptation actual speed range ready
B_FORN01	DMDFON	LOK	at least one range in speed range 01 is ready



Variable	Source	Type	Description
B_FORN02	DMDFON	LOK	at least one range in speed range 02 is ready
B_FORN03	DMDFON	LOK	at least one range in speed range 03 is ready
B_FORN04	DMDFON	LOK	at least one range in speed range 04 is ready
B_FORN05	DMDFON	LOK	at least one range in speed range 05 is ready
B_FORN06	DMDFON	LOK	at least one range in speed range 06 is ready
B_FORN07	DMDFON	LOK	at least one range in speed range 07 is ready
B_FORN08	DMDFON	LOK	at least one range in speed range 08 is ready
B_FORN_M	DMDFON	LOK	monitor, cond. adaptation in actual speed range ready
B_FORSET	DMDFON	LOK	reset of fuel-on/-off adaptation
B_FORUN	DMDFON	LOK	state fuel-on/-off adaptation active
B_FOR_M	DMDFON	LOK	monitor, cond. adaptation in actual range ready
B_FOS	DMDFON	LOK	condition fuel-on/-off actual range is a fuel cut-off range
B_FOXFG	DMDFON	LOK	condition fuel-on/-off allowed
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_MASTER		EIN	Condition MASTER-ECU
B_MDERK	DMDLAD	EIN	misfiring detected from multiple functions
B_MDSTOP	DMDSTP	EIN	misfire detection stop
B_MDSTOP_M		EIN	monitor, misfire detection stopped
B_MDZYL1	DMDFON	DOK	con. for cylinder ident. (f.t>TALUST),LU-calculation disabled (f.t<TALUST)
B_MDZYL1_M		EIN	monitor, cylinder 1 identification
B_PLOK	DMDFON	LOK	FSE values in all speed ranges plausible
B_PLOK01	DMDFON	LOK	FSE values in speed range 01 plausible
B_PLOK02	DMDFON	LOK	FSE values in speed range 02 plausible
B_PLOK03	DMDFON	LOK	FSE values in speed range 03 plausible
B_PLOK04	DMDFON	LOK	FSE values in speed range 04 plausible
B_PLOK05	DMDFON	LOK	FSE values in speed range 05 plausible
B_PLOK06	DMDFON	LOK	FSE values in speed range 06 plausible
B_PLOK07	DMDFON	LOK	FSE values in speed range 07 plausible
B_PLOK08	DMDFON	LOK	FSE values in speed range 08 plausible
B_PLOKN	DMDFON	DOK	FSE values in actual speed range plausible
B_PLOKN_M	DMDFON	LOK	monitor, FSE values in actual speed range plausible
B_TSROOV	DMDTSB	EIN	condition segment duration word overflow
B_TSROOV_M	DMDFON	LOK	monitor, condition segment duration word overflow
CFOXX	DMDFON	LOK	shows characteristics of actual map area (fuel-on/-off adaptation)
DFSE01	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 01 positiv
DFSE02	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 02 positiv
DFSE03	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 3 positiv
DFSE04	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 4 positiv
DFSE05	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 5 positiv
DFSE06	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 6 positiv
DFSE07	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 7 positiv
DFSE08	DMDFON	LOK	state plausibility check of fuel-on/-off adaptation in map range 8 positiv
DFSEN	DMDFON	LOK	difference of FSE values in normal operation at actual speed range
DFSERESZ	DMDFON	LOK	reset counter plausibility check FSE
FDMD_M	DMDFON	LOK	status diagnosis misfire detection, drum, delayed output
FFONN1	DMDFON	LOK	status byte fuel-on/-off adaptation (map ranges ready)
FFONN2	DMDFON	LOK	status byte fuel-on/off adaptation (map ranges ready)
FFONN3	DMDFON	LOK	status byte fuel-on/-off adaptation (map ranges ready)
FFORN1	DMDFON	LOK	status byte fuel-on/-off adaptation (speed ranges ready)
FFPL1	DMDFON	LOK	status byte of fuel-on/-off adaption (FSE values in speed ranges plausible I)
FLG_M	DMDFON	LOK	monitor status calculation of the engine roughness
FLMX	DMDFON	LOK	actual maximum learning filter value
FLMXRESZ	DMDFON	LOK	reset counter learning filter not plausible
FLN11_02	DMDFON	LOK	learning filter value, negative, operating range 11, cylinder 2
FLN11_03	DMDFON	LOK	learning filter value, negative
FLN11_04	DMDFON	LOK	learning filter value, negative
FLN11_05	DMDFON	LOK	learning filter value, negative
FLN11_06	DMDFON	LOK	learning filter value, negative
FLN11_07	DMDFON	LOK	learning filter value, negative
FLN11_08	DMDFON	LOK	learning filter value, negative
FLN11_09	DMDFON	LOK	learning filter value, negative
FLN11_10	DMDFON	LOK	learning filter value, negative
FLN11_11	DMDFON	LOK	learning filter value, negative
FLN11_12	DMDFON	LOK	learning filter value, negative
FLN12_02	DMDFON	LOK	learning filter value, negative
FLN12_03	DMDFON	LOK	learning filter value, negative
FLN12_04	DMDFON	LOK	learning filter value, negative
FLN12_05	DMDFON	LOK	learning filter value, negative
FLN12_06	DMDFON	LOK	learning filter value, negative
FLN12_07	DMDFON	LOK	learning filter value, negative
FLN12_08	DMDFON	LOK	learning filter value, negative
FLN12_09	DMDFON	LOK	learning filter value, negative
FLN12_10	DMDFON	LOK	learning filter value, negative
FLN12_11	DMDFON	LOK	learning filter value, negative
FLN12_12	DMDFON	LOK	learning filter value, negative
FLN13_02	DMDFON	LOK	learning filter value, negative
FLN13_03	DMDFON	LOK	learning filter value, negative
FLN13_04	DMDFON	LOK	learning filter value, negative
FLN13_05	DMDFON	LOK	learning filter value, negative
FLN13_06	DMDFON	LOK	learning filter value, negative
FLN13_07	DMDFON	LOK	learning filter value, negative
FLN13_08	DMDFON	LOK	learning filter value, negative



Variable	Source	Type	Description
FLN13_09	DMDFON	LOK	learning filter value, negative
FLN13_10	DMDFON	LOK	learning filter value, negative
FLN13_11	DMDFON	LOK	learning filter value, negative
FLN13_12	DMDFON	LOK	learning filter value, negative
FLN21_02	DMDFON	LOK	learning filter value, negative
FLN21_03	DMDFON	LOK	learning filter value, negative
FLN21_04	DMDFON	LOK	learning filter value, negative
FLN21_05	DMDFON	LOK	learning filter value, negative
FLN21_06	DMDFON	LOK	learning filter value, negative
FLN21_07	DMDFON	LOK	learning filter value, negative
FLN21_08	DMDFON	LOK	learning filter value, negative
FLN21_09	DMDFON	LOK	learning filter value, negative
FLN21_10	DMDFON	LOK	learning filter value, negative
FLN21_11	DMDFON	LOK	learning filter value, negative
FLN21_12	DMDFON	LOK	learning filter value, negative
FLN22_02	DMDFON	LOK	learning filter value, negative
FLN22_03	DMDFON	LOK	learning filter value, negative
FLN22_04	DMDFON	LOK	learning filter value, negative
FLN22_05	DMDFON	LOK	learning filter value, negative
FLN22_06	DMDFON	LOK	learning filter value, negative
FLN22_07	DMDFON	LOK	learning filter value, negative
FLN22_08	DMDFON	LOK	learning filter value, negative
FLN22_09	DMDFON	LOK	learning filter value, negative
FLN22_10	DMDFON	LOK	learning filter value, negative
FLN22_11	DMDFON	LOK	learning filter value, negative
FLN22_12	DMDFON	LOK	learning filter value, negative
FLN23_02	DMDFON	LOK	learning filter value, negative
FLN23_03	DMDFON	LOK	learning filter value, negative
FLN23_04	DMDFON	LOK	learning filter value, negative
FLN23_05	DMDFON	LOK	learning filter value, negative
FLN23_06	DMDFON	LOK	learning filter value, negative
FLN23_07	DMDFON	LOK	learning filter value, negative
FLN23_08	DMDFON	LOK	learning filter value, negative
FLN23_09	DMDFON	LOK	learning filter value, negative
FLN23_10	DMDFON	LOK	learning filter value, negative
FLN23_11	DMDFON	LOK	learning filter value, negative
FLN23_12	DMDFON	LOK	learning filter value, negative
FLN31_02	DMDFON	LOK	learning filter value, negative
FLN31_03	DMDFON	LOK	learning filter value, negative
FLN31_04	DMDFON	LOK	learning filter value, negative
FLN31_05	DMDFON	LOK	learning filter value, negative
FLN31_06	DMDFON	LOK	learning filter value, negative
FLN31_07	DMDFON	LOK	learning filter value, negative
FLN31_08	DMDFON	LOK	learning filter value, negative
FLN31_09	DMDFON	LOK	learning filter value, negative
FLN31_10	DMDFON	LOK	learning filter value, negative
FLN31_11	DMDFON	LOK	learning filter value, negative
FLN31_12	DMDFON	LOK	learning filter value, negative
FLN32_02	DMDFON	LOK	learning filter value, negative
FLN32_03	DMDFON	LOK	learning filter value, negative
FLN32_04	DMDFON	LOK	learning filter value, negative
FLN32_05	DMDFON	LOK	learning filter value, negative
FLN32_06	DMDFON	LOK	learning filter value, negative
FLN32_07	DMDFON	LOK	learning filter value, negative
FLN32_08	DMDFON	LOK	learning filter value, negative
FLN32_09	DMDFON	LOK	learning filter value, negative
FLN32_10	DMDFON	LOK	learning filter value, negative
FLN32_11	DMDFON	LOK	learning filter value, negative
FLN32_12	DMDFON	LOK	learning filter value, negative
FLN33_02	DMDFON	LOK	learning filter value, negative
FLN33_03	DMDFON	LOK	learning filter value, negative
FLN33_04	DMDFON	LOK	learning filter value, negative
FLN33_05	DMDFON	LOK	learning filter value, negative
FLN33_06	DMDFON	LOK	learning filter value, negative
FLN33_07	DMDFON	LOK	learning filter value, negative
FLN33_08	DMDFON	LOK	learning filter value, negative
FLN33_09	DMDFON	LOK	learning filter value, negative
FLN33_10	DMDFON	LOK	learning filter value, negative
FLN33_11	DMDFON	LOK	learning filter value, negative
FLN33_12	DMDFON	LOK	learning filter value, negative
FLN41_02	DMDFON	LOK	learning filter value, negative
FLN41_03	DMDFON	LOK	learning filter value, negative
FLN41_04	DMDFON	LOK	learning filter value, negative
FLN41_05	DMDFON	LOK	learning filter value, negative
FLN41_06	DMDFON	LOK	learning filter value, negative
FLN41_07	DMDFON	LOK	learning filter value, negative
FLN41_08	DMDFON	LOK	learning filter value, negative
FLN41_09	DMDFON	LOK	learning filter value, negative
FLN41_10	DMDFON	LOK	learning filter value, negative
FLN41_11	DMDFON	LOK	learning filter value, negative
FLN41_12	DMDFON	LOK	learning filter value, negative
FLN42_02	DMDFON	LOK	learning filter value, negative



Variable	Source	Type	Description
FLN42_03	DMDFON	LOK	learning filter value, negative
FLN42_04	DMDFON	LOK	learning filter value, negative
FLN42_05	DMDFON	LOK	learning filter value, negative
FLN42_06	DMDFON	LOK	learning filter value, negative
FLN42_07	DMDFON	LOK	learning filter value, negative
FLN42_08	DMDFON	LOK	learning filter value, negative
FLN42_09	DMDFON	LOK	learning filter value, negative
FLN42_10	DMDFON	LOK	learning filter value, negative
FLN42_11	DMDFON	LOK	learning filter value, negative
FLN42_12	DMDFON	LOK	learning filter value, negative
FLN43_02	DMDFON	LOK	learning filter value, negative
FLN43_03	DMDFON	LOK	learning filter value, negative
FLN43_04	DMDFON	LOK	learning filter value, negative
FLN43_05	DMDFON	LOK	learning filter value, negative
FLN43_06	DMDFON	LOK	learning filter value, negative
FLN43_07	DMDFON	LOK	learning filter value, negative
FLN43_08	DMDFON	LOK	learning filter value, negative
FLN43_09	DMDFON	LOK	learning filter value, negative
FLN43_10	DMDFON	LOK	learning filter value, negative
FLN43_11	DMDFON	LOK	learning filter value, negative
FLN43_12	DMDFON	LOK	learning filter value, negative
FLN51_02	DMDFON	LOK	learning filter value, negative
FLN51_03	DMDFON	LOK	learning filter value, negative
FLN51_04	DMDFON	LOK	learning filter value, negative
FLN51_05	DMDFON	LOK	learning filter value, negative
FLN51_06	DMDFON	LOK	learning filter value, negative
FLN51_07	DMDFON	LOK	learning filter value, negative
FLN51_08	DMDFON	LOK	learning filter value, negative
FLN51_09	DMDFON	LOK	learning filter value, negative
FLN51_10	DMDFON	LOK	learning filter value, negative
FLN51_11	DMDFON	LOK	learning filter value, negative
FLN51_12	DMDFON	LOK	learning filter value, negative
FLN52_02	DMDFON	LOK	learning filter value, negative
FLN52_03	DMDFON	LOK	learning filter value, negative
FLN52_04	DMDFON	LOK	learning filter value, negative
FLN52_05	DMDFON	LOK	learning filter value, negative
FLN52_06	DMDFON	LOK	learning filter value, negative
FLN52_07	DMDFON	LOK	learning filter value, negative
FLN52_08	DMDFON	LOK	learning filter value, negative
FLN52_09	DMDFON	LOK	learning filter value, negative
FLN52_10	DMDFON	LOK	learning filter value, negative
FLN52_11	DMDFON	LOK	learning filter value, negative
FLN52_12	DMDFON	LOK	learning filter value, negative
FLN53_02	DMDFON	LOK	Learning filter value, negative
FLN53_03	DMDFON	LOK	learning filter value, negative
FLN53_04	DMDFON	LOK	learning filter value, negative
FLN53_05	DMDFON	LOK	learning filter value, negative
FLN53_06	DMDFON	LOK	learning filter value, negative
FLN53_07	DMDFON	LOK	learning filter value, negative
FLN53_08	DMDFON	LOK	learning filter value, negative
FLN53_09	DMDFON	LOK	learning filter value, negative
FLN53_10	DMDFON	LOK	learning filter value, negative
FLN53_11	DMDFON	LOK	learning filter value, negative
FLN53_12	DMDFON	LOK	learning filter value, negative
FLN61_02	DMDFON	LOK	learning filter value, negative
FLN61_03	DMDFON	LOK	learning filter value, negative
FLN61_04	DMDFON	LOK	learning filter value, negative
FLN61_05	DMDFON	LOK	learning filter value, negative
FLN61_06	DMDFON	LOK	learning filter value, negative
FLN61_07	DMDFON	LOK	learning filter value, negative
FLN61_08	DMDFON	LOK	learning filter value, negative
FLN61_09	DMDFON	LOK	learning filter value, negative
FLN61_10	DMDFON	LOK	learning filter value, negative
FLN61_11	DMDFON	LOK	learning filter value, negative
FLN61_12	DMDFON	LOK	learning filter value, negative
FLN62_02	DMDFON	LOK	learning filter value, negative
FLN62_03	DMDFON	LOK	learning filter value, negative
FLN62_04	DMDFON	LOK	learning filter value, negative
FLN62_05	DMDFON	LOK	learning filter value, negative
FLN62_06	DMDFON	LOK	learning filter value, negative
FLN62_07	DMDFON	LOK	learning filter value, negative
FLN62_08	DMDFON	LOK	learning filter value, negative
FLN62_09	DMDFON	LOK	learning filter value, negative
FLN62_10	DMDFON	LOK	learning filter value, negative
FLN62_11	DMDFON	LOK	learning filter value, negative
FLN62_12	DMDFON	LOK	learning filter value, negative
FLN63_02	DMDFON	LOK	learning filter value, negative
FLN63_03	DMDFON	LOK	learning filter value, negative
FLN63_04	DMDFON	LOK	learning filter value, negative
FLN63_05	DMDFON	LOK	learning filter value, negative
FLN63_06	DMDFON	LOK	learning filter value, negative
FLN63_07	DMDFON	LOK	learning filter value, negative



Variable	Source	Type	Description
FLN63_08	DMDFON	LOK	learning filter value, negative
FLN63_09	DMDFON	LOK	learning filter value, negative
FLN63_10	DMDFON	LOK	learning filter value, negative
FLN63_11	DMDFON	LOK	learning filter value, negative
FLN63_12	DMDFON	LOK	learning filter value, negative
FLN71_02	DMDFON	LOK	learning filter value, negative
FLN71_03	DMDFON	LOK	learning filter value, negative
FLN71_04	DMDFON	LOK	learning filter value, negative
FLN71_05	DMDFON	LOK	learning filter value, negative
FLN71_06	DMDFON	LOK	learning filter value, negative
FLN71_07	DMDFON	LOK	learning filter value, negative
FLN71_08	DMDFON	LOK	learning filter value, negative
FLN71_09	DMDFON	LOK	learning filter value, negative
FLN71_10	DMDFON	LOK	learning filter value, negative
FLN71_11	DMDFON	LOK	learning filter value, negative
FLN71_12	DMDFON	LOK	learning filter value, negative
FLN72_02	DMDFON	LOK	learning filter value, negative
FLN72_03	DMDFON	LOK	learning filter value, negative
FLN72_04	DMDFON	LOK	learning filter value, negative
FLN72_05	DMDFON	LOK	learning filter value, negative
FLN72_06	DMDFON	LOK	learning filter value, negative
FLN72_07	DMDFON	LOK	learning filter value, negative
FLN72_08	DMDFON	LOK	learning filter value, negative
FLN72_09	DMDFON	LOK	learning filter value, negative
FLN72_10	DMDFON	LOK	learning filter value, negative
FLN72_11	DMDFON	LOK	learning filter value, negative
FLN72_12	DMDFON	LOK	learning filter value, negative
FLN73_02	DMDFON	LOK	learning filter value, negative
FLN73_03	DMDFON	LOK	learning filter value, negative
FLN73_04	DMDFON	LOK	learning filter value, negative
FLN73_05	DMDFON	LOK	learning filter value, negative
FLN73_06	DMDFON	LOK	learning filter value, negative
FLN73_07	DMDFON	LOK	learning filter value, negative
FLN73_08	DMDFON	LOK	learning filter value, negative
FLN73_09	DMDFON	LOK	learning filter value, negative
FLN73_10	DMDFON	LOK	learning filter value, negative
FLN73_11	DMDFON	LOK	learning filter value, negative
FLN73_12	DMDFON	LOK	learning filter value, negative
FLN81_02	DMDFON	LOK	learning filter value, negative
FLN81_03	DMDFON	LOK	learning filter value, negative
FLN81_04	DMDFON	LOK	learning filter value, negative
FLN81_05	DMDFON	LOK	learning filter value, negative
FLN81_06	DMDFON	LOK	learning filter value, negative
FLN81_07	DMDFON	LOK	learning filter value, negative
FLN81_08	DMDFON	LOK	learning filter value, negative
FLN81_09	DMDFON	LOK	learning filter value, negative
FLN81_10	DMDFON	LOK	learning filter value, negative
FLN81_11	DMDFON	LOK	learning filter value, negative
FLN81_12	DMDFON	LOK	learning filter value, negative
FLN82_02	DMDFON	LOK	learning filter value, negative
FLN82_03	DMDFON	LOK	learning filter value, negative
FLN82_04	DMDFON	LOK	learning filter value, negative
FLN82_05	DMDFON	LOK	learning filter value, negative
FLN82_06	DMDFON	LOK	learning filter value, negative
FLN82_07	DMDFON	LOK	learning filter value, negative
FLN82_08	DMDFON	LOK	learning filter value, negative
FLN82_09	DMDFON	LOK	learning filter value, negative
FLN82_10	DMDFON	LOK	learning filter value, negative
FLN82_11	DMDFON	LOK	learning filter value, negative
FLN82_12	DMDFON	LOK	learning filter value, negative
FLN83_02	DMDFON	LOK	learning filter value, negative
FLN83_03	DMDFON	LOK	learning filter value, negative
FLN83_04	DMDFON	LOK	learning filter value, negative
FLN83_05	DMDFON	LOK	learning filter value, negative
FLN83_06	DMDFON	LOK	learning filter value, negative
FLN83_07	DMDFON	LOK	learning filter value, negative
FLN83_08	DMDFON	LOK	learning filter value, negative
FLN83_09	DMDFON	LOK	learning filter value, negative
FLN83_10	DMDFON	LOK	learning filter value, negative
FLN83_11	DMDFON	LOK	learning filter value, negative
FLN83_12	DMDFON	LOK	learning filter value, negative
FLP11_02	DMDFON	LOK	learning filter value, positive
FLP11_03	DMDFON	LOK	learning filter value, positiv
FLP11_04	DMDFON	LOK	learning filter value, positiv
FLP11_05	DMDFON	LOK	learning filter value, positiv
FLP11_06	DMDFON	LOK	learning filter value, positiv
FLP11_07	DMDFON	LOK	learning filter value, positiv
FLP11_08	DMDFON	LOK	learning filter value, positiv
FLP11_09	DMDFON	LOK	learning filter value, positiv
FLP11_10	DMDFON	LOK	learning filter value, positiv
FLP11_11	DMDFON	LOK	learning filter value, positiv
FLP11_12	DMDFON	LOK	learning filter value, positiv



Variable	Source	Type	Description
FLP12_02	DMDFON	LOK	learning filter value, positiv
FLP12_03	DMDFON	LOK	learning filter value, positiv
FLP12_04	DMDFON	LOK	learning filter value, positiv
FLP12_05	DMDFON	LOK	learning filter value, positiv
FLP12_06	DMDFON	LOK	learning filter value, positiv
FLP12_07	DMDFON	LOK	learning filter value, positiv
FLP12_08	DMDFON	LOK	learning filter value, positiv
FLP12_09	DMDFON	LOK	learning filter value, positiv
FLP12_10	DMDFON	LOK	learning filter value, positiv
FLP12_11	DMDFON	LOK	learning filter value, positiv
FLP12_12	DMDFON	LOK	learning filter value, positiv
FLP13_02	DMDFON	LOK	learning filter value, positiv
FLP13_03	DMDFON	LOK	learning filter value, positiv
FLP13_04	DMDFON	LOK	learning filter value, positiv
FLP13_05	DMDFON	LOK	learning filter value, positiv
FLP13_06	DMDFON	LOK	learning filter value, positiv
FLP13_07	DMDFON	LOK	learning filter value, positiv
FLP13_08	DMDFON	LOK	learning filter value, positiv
FLP13_09	DMDFON	LOK	learning filter value, positiv
FLP13_10	DMDFON	LOK	learning filter value, positiv
FLP13_11	DMDFON	LOK	learning filter value, positiv
FLP13_12	DMDFON	LOK	learning filter value, positiv
FLP21_02	DMDFON	LOK	learning filter value, positiv
FLP21_03	DMDFON	LOK	learning filter value, positiv
FLP21_04	DMDFON	LOK	learning filter value, positiv
FLP21_05	DMDFON	LOK	learning filter value, positiv
FLP21_06	DMDFON	LOK	learning filter value, positiv
FLP21_07	DMDFON	LOK	learning filter value, positiv
FLP21_08	DMDFON	LOK	learning filter value, positiv
FLP21_09	DMDFON	LOK	learning filter value, positiv
FLP21_10	DMDFON	LOK	learning filter value, positiv
FLP21_11	DMDFON	LOK	learning filter value, positiv
FLP21_12	DMDFON	LOK	learning filter value, positiv
FLP22_02	DMDFON	LOK	learning filter value, positiv
FLP22_03	DMDFON	LOK	learning filter value, positiv
FLP22_04	DMDFON	LOK	learning filter value, positiv
FLP22_05	DMDFON	LOK	learning filter value, positiv
FLP22_06	DMDFON	LOK	learning filter value, positiv
FLP22_07	DMDFON	LOK	learning filter value, positiv
FLP22_08	DMDFON	LOK	learning filter value, positiv
FLP22_09	DMDFON	LOK	learning filter value, positiv
FLP22_10	DMDFON	LOK	learning filter value, positiv
FLP22_11	DMDFON	LOK	learning filter value, positiv
FLP22_12	DMDFON	LOK	learning filter value, positiv
FLP23_02	DMDFON	LOK	learning filter value, positiv
FLP23_03	DMDFON	LOK	learning filter value, positiv
FLP23_04	DMDFON	LOK	learning filter value, positiv
FLP23_05	DMDFON	LOK	learning filter value, positiv
FLP23_06	DMDFON	LOK	learning filter value, positiv
FLP23_07	DMDFON	LOK	learning filter value, positiv
FLP23_08	DMDFON	LOK	learning filter value, positiv
FLP23_09	DMDFON	LOK	learning filter value, positiv
FLP23_10	DMDFON	LOK	learning filter value, positiv
FLP23_11	DMDFON	LOK	learning filter value, positiv
FLP23_12	DMDFON	LOK	learning filter value, positiv
FLP31_02	DMDFON	LOK	learning filter value, positiv
FLP31_03	DMDFON	LOK	learning filter value, positiv
FLP31_04	DMDFON	LOK	learning filter value, positiv
FLP31_05	DMDFON	LOK	learning filter value, positiv
FLP31_06	DMDFON	LOK	learning filter value, positiv
FLP31_07	DMDFON	LOK	learning filter value, positiv
FLP31_08	DMDFON	LOK	learning filter value, positiv
FLP31_09	DMDFON	LOK	learning filter value, positiv
FLP31_10	DMDFON	LOK	learning filter value, positiv
FLP31_11	DMDFON	LOK	learning filter value, positiv
FLP31_12	DMDFON	LOK	learning filter value, positiv
FLP32_02	DMDFON	LOK	learning filter value, positiv
FLP32_03	DMDFON	LOK	learning filter value, positiv
FLP32_04	DMDFON	LOK	learning filter value, positiv
FLP32_05	DMDFON	LOK	learning filter value, positiv
FLP32_06	DMDFON	LOK	learning filter value, positiv
FLP32_07	DMDFON	LOK	learning filter value, positiv
FLP32_08	DMDFON	LOK	learning filter value, positiv
FLP32_09	DMDFON	LOK	learning filter value, positiv
FLP32_10	DMDFON	LOK	learning filter value, positiv
FLP32_11	DMDFON	LOK	learning filter value, positiv
FLP32_12	DMDFON	LOK	learning filter value, positiv
FLP33_02	DMDFON	LOK	learning filter value, positiv
FLP33_03	DMDFON	LOK	learning filter value, positiv
FLP33_04	DMDFON	LOK	learning filter value, positiv
FLP33_05	DMDFON	LOK	learning filter value, positiv
FLP33_06	DMDFON	LOK	learning filter value, positiv



Variable	Source	Type	Description
FLP33_07	DMDFON	LOK	learning filter value, positiv
FLP33_08	DMDFON	LOK	learning filter value, positiv
FLP33_09	DMDFON	LOK	learning filter value, positiv
FLP33_10	DMDFON	LOK	learning filter value, positiv
FLP33_11	DMDFON	LOK	learning filter value, positiv
FLP33_12	DMDFON	LOK	learning filter value, positiv
FLP41_02	DMDFON	LOK	learning filter value, positiv
FLP41_03	DMDFON	LOK	learning filter value, positiv
FLP41_04	DMDFON	LOK	learning filter value, positiv
FLP41_05	DMDFON	LOK	learning filter value, positiv
FLP41_06	DMDFON	LOK	learning filter value, positiv
FLP41_07	DMDFON	LOK	learning filter value, positiv
FLP41_08	DMDFON	LOK	learning filter value, positiv
FLP41_09	DMDFON	LOK	learning filter value, positiv
FLP41_10	DMDFON	LOK	learning filter value, positiv
FLP41_11	DMDFON	LOK	learning filter value, positiv
FLP41_12	DMDFON	LOK	learning filter value, positiv
FLP42_02	DMDFON	LOK	learning filter value, positiv
FLP42_03	DMDFON	LOK	learning filter value, positiv
FLP42_04	DMDFON	LOK	learning filter value, positiv
FLP42_05	DMDFON	LOK	learning filter value, positiv
FLP42_06	DMDFON	LOK	learning filter value, positiv
FLP42_07	DMDFON	LOK	learning filter value, positiv
FLP42_08	DMDFON	LOK	learning filter value, positiv
FLP42_09	DMDFON	LOK	learning filter value, positiv
FLP42_10	DMDFON	LOK	learning filter value, positiv
FLP42_11	DMDFON	LOK	learning filter value, positiv
FLP42_12	DMDFON	LOK	learning filter value, positiv
FLP43_02	DMDFON	LOK	learning filter value, positiv
FLP43_03	DMDFON	LOK	learning filter value, positiv
FLP43_04	DMDFON	LOK	learning filter value, positiv
FLP43_05	DMDFON	LOK	learning filter value, positiv
FLP43_06	DMDFON	LOK	learning filter value, positiv
FLP43_07	DMDFON	LOK	learning filter value, positiv
FLP43_08	DMDFON	LOK	learning filter value, positiv
FLP43_09	DMDFON	LOK	learning filter value, positiv
FLP43_10	DMDFON	LOK	learning filter value, positiv
FLP43_11	DMDFON	LOK	learning filter value, positiv
FLP43_12	DMDFON	LOK	learning filter value, positiv
FLP51_02	DMDFON	LOK	learning filter value, positiv
FLP51_03	DMDFON	LOK	learning filter value, positiv
FLP51_04	DMDFON	LOK	learning filter value, positiv
FLP51_05	DMDFON	LOK	learning filter value, positiv
FLP51_06	DMDFON	LOK	learning filter value, positiv
FLP51_07	DMDFON	LOK	learning filter value, positiv
FLP51_08	DMDFON	LOK	learning filter value, positiv
FLP51_09	DMDFON	LOK	learning filter value, positiv
FLP51_10	DMDFON	LOK	learning filter value, positiv
FLP51_11	DMDFON	LOK	learning filter value, positiv
FLP51_12	DMDFON	LOK	learning filter value, positiv
FLP52_02	DMDFON	LOK	learning filter value, positiv
FLP52_03	DMDFON	LOK	learning filter value, positiv
FLP52_04	DMDFON	LOK	learning filter value, positiv
FLP52_05	DMDFON	LOK	learning filter value, positiv
FLP52_06	DMDFON	LOK	learning filter value, positiv
FLP52_07	DMDFON	LOK	learning filter value, positiv
FLP52_08	DMDFON	LOK	learning filter value, positiv
FLP52_09	DMDFON	LOK	learning filter value, positiv
FLP52_10	DMDFON	LOK	learning filter value, positiv
FLP52_11	DMDFON	LOK	learning filter value, positiv
FLP52_12	DMDFON	LOK	learning filter value, positiv
FLP53_02	DMDFON	LOK	learning filter value, positiv
FLP53_03	DMDFON	LOK	learning filter value, positiv
FLP53_04	DMDFON	LOK	learning filter value, positiv
FLP53_05	DMDFON	LOK	learning filter value, positiv
FLP53_06	DMDFON	LOK	learning filter value, positiv
FLP53_07	DMDFON	LOK	learning filter value, positiv
FLP53_08	DMDFON	LOK	learning filter value, positiv
FLP53_09	DMDFON	LOK	learning filter value, positiv
FLP53_10	DMDFON	LOK	learning filter value, positiv
FLP53_11	DMDFON	LOK	learning filter value, positiv
FLP53_12	DMDFON	LOK	learning filter value, positiv
FLP61_02	DMDFON	LOK	learning filter value, positiv
FLP61_03	DMDFON	LOK	learning filter value, positiv
FLP61_04	DMDFON	LOK	learning filter value, positiv
FLP61_05	DMDFON	LOK	learning filter value, positiv
FLP61_06	DMDFON	LOK	learning filter value, positiv
FLP61_07	DMDFON	LOK	learning filter value, positiv
FLP61_08	DMDFON	LOK	learning filter value, positiv
FLP61_09	DMDFON	LOK	learning filter value, positiv
FLP61_10	DMDFON	LOK	learning filter value, positiv
FLP61_11	DMDFON	LOK	learning filter value, positiv





Variable	Source	Type	Description
FLP61_12	DMDFON	LOK	learning filter value, positiv
FLP62_02	DMDFON	LOK	learning filter value, positiv
FLP62_03	DMDFON	LOK	learning filter value, positiv
FLP62_04	DMDFON	LOK	learning filter value, positiv
FLP62_05	DMDFON	LOK	learning filter value, positiv
FLP62_06	DMDFON	LOK	learning filter value, positiv
FLP62_07	DMDFON	LOK	learning filter value, positiv
FLP62_08	DMDFON	LOK	learning filter value, positiv
FLP62_09	DMDFON	LOK	learning filter value, positiv
FLP62_10	DMDFON	LOK	learning filter value, positiv
FLP62_11	DMDFON	LOK	learning filter value, positiv
FLP62_12	DMDFON	LOK	learning filter value, positiv
FLP63_02	DMDFON	LOK	learning filter value, positiv
FLP63_03	DMDFON	LOK	learning filter value, positiv
FLP63_04	DMDFON	LOK	learning filter value, positiv
FLP63_05	DMDFON	LOK	learning filter value, positiv
FLP63_06	DMDFON	LOK	learning filter value, positiv
FLP63_07	DMDFON	LOK	learning filter value, positiv
FLP63_08	DMDFON	LOK	learning filter value, positiv
FLP63_09	DMDFON	LOK	learning filter value, positiv
FLP63_10	DMDFON	LOK	learning filter value, positiv
FLP63_11	DMDFON	LOK	learning filter value, positiv
FLP63_12	DMDFON	LOK	learning filter value, positiv
FLP71_02	DMDFON	LOK	learning filter value, positiv
FLP71_03	DMDFON	LOK	learning filter value, positiv
FLP71_04	DMDFON	LOK	learning filter value, positiv
FLP71_05	DMDFON	LOK	learning filter value, positiv
FLP71_06	DMDFON	LOK	learning filter value, positiv
FLP71_07	DMDFON	LOK	learning filter value, positiv
FLP71_08	DMDFON	LOK	learning filter value, positiv
FLP71_09	DMDFON	LOK	learning filter value, positiv
FLP71_10	DMDFON	LOK	learning filter value, positive
FLP71_11	DMDFON	LOK	learning filter value, positive
FLP71_12	DMDFON	LOK	learning filter value, positive
FLP72_02	DMDFON	LOK	learning filter value, positiv
FLP72_03	DMDFON	LOK	learning filter value, positiv
FLP72_04	DMDFON	LOK	learning filter value, positiv
FLP72_05	DMDFON	LOK	learning filter value, positiv
FLP72_06	DMDFON	LOK	learning filter value, positiv
FLP72_07	DMDFON	LOK	learning filter value, positiv
FLP72_08	DMDFON	LOK	learning filter value, positiv
FLP72_09	DMDFON	LOK	learning filter value, positive
FLP72_10	DMDFON	LOK	learning filter value, positive
FLP72_11	DMDFON	LOK	learning filter value, positive
FLP72_12	DMDFON	LOK	learning filter value, positive
FLP73_02	DMDFON	LOK	learning filter value, positiv
FLP73_03	DMDFON	LOK	learning filter value, positiv
FLP73_04	DMDFON	LOK	learning filter value, positiv
FLP73_05	DMDFON	LOK	learning filter value, positiv
FLP73_06	DMDFON	LOK	learning filter value, positiv
FLP73_07	DMDFON	LOK	learning filter value, positiv
FLP73_08	DMDFON	LOK	learning filter value, positiv
FLP73_09	DMDFON	LOK	learning filter value, positive
FLP73_10	DMDFON	LOK	learning filter value, positive
FLP73_11	DMDFON	LOK	learning filter value, positive
FLP73_12	DMDFON	LOK	learning filter value, positive
FLP81_02	DMDFON	LOK	learning filter value, positiv
FLP81_03	DMDFON	LOK	learning filter value, positiv
FLP81_04	DMDFON	LOK	learning filter value, positiv
FLP81_05	DMDFON	LOK	learning filter value, positiv
FLP81_06	DMDFON	LOK	learning filter value, positiv
FLP81_07	DMDFON	LOK	learning filter value, positiv
FLP81_08	DMDFON	LOK	learning filter value, positiv
FLP81_09	DMDFON	LOK	learning filter value, positive
FLP81_10	DMDFON	LOK	learning filter value, positive
FLP81_11	DMDFON	LOK	learning filter value, positive
FLP81_12	DMDFON	LOK	learning filter value, positive
FLP82_02	DMDFON	LOK	learning filter value, positiv
FLP82_03	DMDFON	LOK	learning filter value, positiv
FLP82_04	DMDFON	LOK	learning filter value, positiv
FLP82_05	DMDFON	LOK	learning filter value, positiv
FLP82_06	DMDFON	LOK	learning filter value, positiv
FLP82_07	DMDFON	LOK	learning filter value, positiv
FLP82_08	DMDFON	LOK	learning filter value, positiv
FLP82_09	DMDFON	LOK	learning filter value, positive
FLP82_10	DMDFON	LOK	learning filter value, positive
FLP82_11	DMDFON	LOK	learning filter value, positive
FLP82_12	DMDFON	LOK	learning filter value, positive
FLP83_02	DMDFON	LOK	learning filter value, positiv
FLP83_03	DMDFON	LOK	learning filter value, positiv
FLP83_04	DMDFON	LOK	learning filter value, positiv
FLP83_05	DMDFON	LOK	learning filter value, positiv



Variable	Source	Type	Description
FLP83_06	DMDFON	LOK	learning filter value, positiv
FLP83_07	DMDFON	LOK	learning filter value, positiv
FLP83_08	DMDFON	LOK	learning filter value, positiv
FLP83_09	DMDFON	LOK	learning filter value, positive
FLP83_10	DMDFON	LOK	learning filter value, positive
FLP83_11	DMDFON	LOK	learning filter value, positive
FLP83_12	DMDFON	LOK	learning filter value, positive
FOSAT	DMDFON	AUS	state of fuel-on/-off adaptation in actual map range
FS11_02	DMDFON	LOK	filter value segment duration, operating range 11
FS11_03	DMDFON	LOK	filter value segment duration, operating range 11
FS11_04	DMDFON	LOK	filter value segment duration, operating range 11
FS11_05	DMDFON	LOK	filter value segment duration, operating range 11
FS11_06	DMDFON	LOK	filter value segment duration, operating range 11
FS11_07	DMDFON	LOK	filter value segment duration, operating range 11
FS11_08	DMDFON	LOK	filter value segment duration, operating range 11
FS11_09	DMDFON	LOK	filter value segment duration, operating range 11
FS11_10	DMDFON	LOK	filter value segment duration, operating range 11
FS11_11	DMDFON	LOK	filter value segment duration, operating range 11
FS11_12	DMDFON	LOK	filter value segment duration, operating range 11
FS12_02	DMDFON	LOK	filter value segment duration, operating range 12
FS12_03	DMDFON	LOK	filter value segment duration, operating range 12
FS12_04	DMDFON	LOK	filter value segment duration, operating range 12
FS12_05	DMDFON	LOK	filter value segment duration, operating range 12
FS12_06	DMDFON	LOK	filter value segment duration, operating range 12
FS12_07	DMDFON	LOK	filter value segment duration, operating range 12
FS12_08	DMDFON	LOK	filter value segment duration, operating range 12
FS12_09	DMDFON	LOK	filter value segment duration, operating range 12
FS12_10	DMDFON	LOK	filter value segment duration, operating range 12
FS12_11	DMDFON	LOK	filter value segment duration, operating range 12
FS12_12	DMDFON	LOK	filter value segment duration, operating range 12
FS13_02	DMDFON	LOK	filter value segment duration, operating range 13
FS13_03	DMDFON	LOK	filter value segment duration, operating range 13
FS13_04	DMDFON	LOK	filter value segment duration, operating range 13
FS13_05	DMDFON	LOK	filter value segment duration, operating range 13
FS13_06	DMDFON	LOK	filter value segment duration, operating range 13
FS13_07	DMDFON	LOK	filter value segment duration, operating range 13
FS13_08	DMDFON	LOK	filter value segment duration, operating range 13
FS13_09	DMDFON	LOK	filter value segment duration, operating range 13
FS13_10	DMDFON	LOK	filter value segment duration, operating range 13
FS13_11	DMDFON	LOK	filter value segment duration, operating range 13
FS13_12	DMDFON	LOK	filter value segment duration, operating range 13
FS21_02	DMDFON	LOK	filter value segment duration, operating range 21
FS21_03	DMDFON	LOK	filter value segment duration, operating range 21
FS21_04	DMDFON	LOK	filter value segment duration, operating range 21
FS21_05	DMDFON	LOK	filter value segment duration, operating range 21
FS21_06	DMDFON	LOK	filter value segment duration, operating range 21
FS21_07	DMDFON	LOK	filter value segment duration, operating range 21
FS21_08	DMDFON	LOK	filter value segment duration, operating range 21
FS21_09	DMDFON	LOK	filter value segment duration, operating range 21
FS21_10	DMDFON	LOK	filter value segment duration, operating range 21
FS21_11	DMDFON	LOK	filter value segment duration, operating range 21
FS21_12	DMDFON	LOK	filter value segment duration, operating range 21
FS22_02	DMDFON	LOK	filter value segment duration, operating range 22
FS22_03	DMDFON	LOK	filter value segment duration, operating range 22
FS22_04	DMDFON	LOK	filter value segment duration, operating range 22
FS22_05	DMDFON	LOK	filter value segment duration, operating range 22
FS22_06	DMDFON	LOK	filter value segment duration, operating range 22
FS22_07	DMDFON	LOK	filter value segment duration, operating range 22
FS22_08	DMDFON	LOK	filter value segment duration, operating range 22
FS22_09	DMDFON	LOK	filter value segment duration, operating range 21
FS22_10	DMDFON	LOK	filter value segment duration, operating range 21
FS22_11	DMDFON	LOK	filter value segment duration, operating range 21
FS22_12	DMDFON	LOK	filter value segment duration, operating range 21
FS23_02	DMDFON	LOK	filter value segment duration, operating range 23
FS23_03	DMDFON	LOK	filter value segment duration, operating range 23
FS23_04	DMDFON	LOK	filter value segment duration, operating range 23
FS23_05	DMDFON	LOK	filter value segment duration, operating range 23
FS23_06	DMDFON	LOK	filter value segment duration, operating range 23
FS23_07	DMDFON	LOK	filter value segment duration, operating range 23
FS23_08	DMDFON	LOK	filter value segment duration, operating range 23
FS23_09	DMDFON	LOK	filter value segment duration, operating range 23
FS23_10	DMDFON	LOK	filter value segment duration, operating range 23
FS23_11	DMDFON	LOK	filter value segment duration, operating range 23
FS23_12	DMDFON	LOK	filter value segment duration, operating range 23
FS31_02	DMDFON	LOK	filter value segment duration, operating range 31, cylinder 2
FS31_03	DMDFON	LOK	filter value segment duration, operating range 31
FS31_04	DMDFON	LOK	filter value segment duration, operating range 31
FS31_05	DMDFON	LOK	filter value segment duration, operating range 31
FS31_06	DMDFON	LOK	filter value segment duration, operating range 31
FS31_07	DMDFON	LOK	filter value segment duration, operating range 31
FS31_08	DMDFON	LOK	filter value segment duration, operating range 31
FS31_09	DMDFON	LOK	filter value segment duration, operating range 31





Variable	Source	Type	Description
FS53_04	DMDFON	LOK	filter value segment duration, operating range 53
FS53_05	DMDFON	LOK	filter value segment duration, operating range 53
FS53_06	DMDFON	LOK	filter value segment duration, operating range 53
FS53_07	DMDFON	LOK	filter value segment duration, operating range 53
FS53_08	DMDFON	LOK	filter value segment duration, operating range 53
FS53_09	DMDFON	LOK	filter value segment duration, operating range 53
FS53_10	DMDFON	LOK	filter value segment duration, operating range 53
FS53_11	DMDFON	LOK	filter value segment duration, operating range 53
FS53_12	DMDFON	LOK	filter value segment duration, operating range 53
FS61_02	DMDFON	LOK	filter value segment duration, operating range 61, cylinder 2
FS61_03	DMDFON	LOK	filter value segment duration, operating range 61
FS61_04	DMDFON	LOK	filter value segment duration, operating range 61
FS61_05	DMDFON	LOK	filter value segment duration, operating range 61
FS61_06	DMDFON	LOK	filter value segment duration, operating range 61
FS61_07	DMDFON	LOK	filter value segment duration, operating range 61
FS61_08	DMDFON	LOK	filter value segment duration, operating range 61
FS61_09	DMDFON	LOK	filter value segment duration, operating range 61
FS61_10	DMDFON	LOK	filter value segment duration, operating range 61
FS61_11	DMDFON	LOK	filter value segment duration, operating range 61
FS61_12	DMDFON	LOK	filter value segment duration, operating range 61
FS62_02	DMDFON	LOK	filter value segment duration, operating range 62, cylinder 2
FS62_03	DMDFON	LOK	filter value segment duration, operating range 62
FS62_04	DMDFON	LOK	filter value segment duration, operating range 62
FS62_05	DMDFON	LOK	filter value segment duration, operating range 62
FS62_06	DMDFON	LOK	filter value segment duration, operating range 62
FS62_07	DMDFON	LOK	filter value segment duration, operating range 62
FS62_08	DMDFON	LOK	filter value segment duration, operating range 62
FS62_09	DMDFON	LOK	filter value segment duration, operating range 62
FS62_10	DMDFON	LOK	filter value segment duration, operating range 62
FS62_11	DMDFON	LOK	filter value segment duration, operating range 62
FS62_12	DMDFON	LOK	filter value segment duration, operating range 62
FS63_02	DMDFON	LOK	filter value segment duration, operating range 63, cylinder 2
FS63_03	DMDFON	LOK	filter value segment duration, operating range 63
FS63_04	DMDFON	LOK	filter value segment duration, operating range 63
FS63_05	DMDFON	LOK	filter value segment duration, operating range 63
FS63_06	DMDFON	LOK	filter value segment duration, operating range 63
FS63_07	DMDFON	LOK	filter value segment duration, operating range 63
FS63_08	DMDFON	LOK	filter value segment duration, operating range 63
FS63_09	DMDFON	LOK	filter value segment duration, operating range 63
FS63_10	DMDFON	LOK	filter value segment duration, operating range 63
FS63_11	DMDFON	LOK	filter value segment duration
FS63_12	DMDFON	LOK	filter value segment duration, operating range 63
FS71_02	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 2
FS71_03	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 3
FS71_04	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 4
FS71_05	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 5
FS71_06	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 6
FS71_07	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 7
FS71_08	DMDFON	LOK	filter value segment duration, operating range 71, cylinder 8
FS71_09	DMDFON	LOK	filter value segment duration
FS71_10	DMDFON	LOK	filter value segment duration
FS71_11	DMDFON	LOK	filter value segment duration
FS71_12	DMDFON	LOK	filter value segment duration
FS72_02	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 2
FS72_03	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 3
FS72_04	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 4
FS72_05	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 5
FS72_06	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 6
FS72_07	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 7
FS72_08	DMDFON	LOK	filter value segment duration, operating range 72, cylinder 8
FS72_09	DMDFON	LOK	filter value segment duration
FS72_10	DMDFON	LOK	filter value segment duration
FS72_11	DMDFON	LOK	filter value segment duration
FS72_12	DMDFON	LOK	filter value segment duration
FS73_02	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 2
FS73_03	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 3
FS73_04	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 4
FS73_05	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 5
FS73_06	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 6
FS73_07	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 7
FS73_08	DMDFON	LOK	filter value segment duration, operating range 73, cylinder 8
FS73_09	DMDFON	LOK	filter value segment duration
FS73_10	DMDFON	LOK	filter value segment duration
FS73_11	DMDFON	LOK	filter value segment duration
FS73_12	DMDFON	LOK	filter value segment duration
FS81_02	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 2
FS81_03	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 3
FS81_04	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 4
FS81_05	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 5
FS81_06	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 6
FS81_07	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 7
FS81_08	DMDFON	LOK	filter value segment duration, operating range 81, cylinder 8



Variable	Source	Type	Description
FS81_09	DMDFON	LOK	filter value segment duration
FS81_10	DMDFON	LOK	filter value segment duration
FS81_11	DMDFON	LOK	filter value segment duration
FS81_12	DMDFON	LOK	filter value segment duration
FS82_02	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 2
FS82_03	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 3
FS82_04	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 4
FS82_05	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 5
FS82_06	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 6
FS82_07	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 7
FS82_08	DMDFON	LOK	filter value segment duration, operating range 82, cylinder 8
FS82_09	DMDFON	LOK	filter value segment duration
FS82_10	DMDFON	LOK	filter value segment duration
FS82_11	DMDFON	LOK	filter value segment duration
FS82_12	DMDFON	LOK	filter value segment duration
FS83_02	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 2
FS83_03	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 3
FS83_04	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 4
FS83_05	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 5
FS83_06	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 6
FS83_07	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 7
FS83_08	DMDFON	LOK	filter value segment duration, operating range 83, cylinder 8
FS83_09	DMDFON	LOK	filter value segment duration
FS83_10	DMDFON	LOK	filter value segment duration
FS83_11	DMDFON	LOK	filter value segment duration
FS83_12	DMDFON	LOK	filter value segment duration
FSE	DMDFON	LOK	actual filter value segment duration, for correction of segment duration
FSE11_02	DMDFON	LOK	filter value segment duration, for calculation, operating range 11, cylinder 2
FSE11_03	DMDFON	LOK	filter value segment duration, for calculation
FSE11_04	DMDFON	LOK	filter value segment duration, for calculation
FSE11_05	DMDFON	LOK	filter value segment duration, for calculation
FSE11_06	DMDFON	LOK	filter value segment duration, for calculation
FSE11_07	DMDFON	LOK	filter value segment duration, for calculation
FSE11_08	DMDFON	LOK	filter value segment duration, for calculation
FSE11_09	DMDFON	LOK	filter value segment duration, for calculation
FSE11_10	DMDFON	LOK	filter value segment duration, for calculation
FSE11_11	DMDFON	LOK	filter value segment duration, for calculation
FSE11_12	DMDFON	LOK	filter value segment duration, for calculation
FSE12_02	DMDFON	LOK	filter value segment duration, for calculation
FSE12_03	DMDFON	LOK	filter value segment duration, for calculation
FSE12_04	DMDFON	LOK	filter value segment duration, for calculation
FSE12_05	DMDFON	LOK	filter value segment duration, for calculation
FSE12_06	DMDFON	LOK	filter value segment duration, for calculation
FSE12_07	DMDFON	LOK	filter value segment duration, for calculation
FSE12_08	DMDFON	LOK	filter value segment duration, for calculation
FSE12_09	DMDFON	LOK	filter value segment duration, for calculation
FSE12_10	DMDFON	LOK	filter value segment duration, for calculation
FSE12_11	DMDFON	LOK	filter value segment duration, for calculation
FSE12_12	DMDFON	LOK	filter value segment duration, for calculation
FSE13_02	DMDFON	LOK	filter value segment duration, for calculation
FSE13_03	DMDFON	LOK	filter value segment duration, for calculation
FSE13_04	DMDFON	LOK	filter value segment duration, for calculation
FSE13_05	DMDFON	LOK	filter value segment duration, for calculation
FSE13_06	DMDFON	LOK	filter value segment duration, for calculation
FSE13_07	DMDFON	LOK	filter value segment duration, for calculation
FSE13_08	DMDFON	LOK	filter value segment duration, for calculation
FSE13_09	DMDFON	LOK	filter value segment duration, for calculation
FSE13_10	DMDFON	LOK	filter value segment duration, for calculation
FSE13_11	DMDFON	LOK	filter value segment duration, for calculation
FSE13_12	DMDFON	LOK	filter value segment duration, for calculation
FSE21_02	DMDFON	LOK	filter value segment duration, for calculation
FSE21_03	DMDFON	LOK	filter value segment duration, for calculation
FSE21_04	DMDFON	LOK	filter value segment duration, for calculation
FSE21_05	DMDFON	LOK	filter value segment duration, for calculation
FSE21_06	DMDFON	LOK	filter value segment duration, for calculation
FSE21_07	DMDFON	LOK	filter value segment duration, for calculation
FSE21_08	DMDFON	LOK	filter value segment duration, for calculation
FSE21_09	DMDFON	LOK	filter value segment duration, for calculation
FSE21_10	DMDFON	LOK	filter value segment duration, for calculation
FSE21_11	DMDFON	LOK	filter value segment duration, for calculation
FSE21_12	DMDFON	LOK	filter value segment duration, for calculation
FSE22_02	DMDFON	LOK	filter value segment duration, for calculation
FSE22_03	DMDFON	LOK	filter value segment duration, for calculation
FSE22_04	DMDFON	LOK	filter value segment duration, for calculation
FSE22_05	DMDFON	LOK	filter value segment duration, for calculation
FSE22_06	DMDFON	LOK	filter value segment duration, for calculation
FSE22_07	DMDFON	LOK	filter value segment duration, for calculation
FSE22_08	DMDFON	LOK	filter value segment duration, for calculation
FSE22_09	DMDFON	LOK	filter value segment duration, for calculation
FSE22_10	DMDFON	LOK	filter value segment duration, for calculation
FSE22_11	DMDFON	LOK	filter value segment duration, for calculation
FSE22_12	DMDFON	LOK	filter value segment duration, for calculation







Variable	Source	Type	Description
FSE72_12	DMDFON	LOK	filter value segment duration, for calculation
FSE73_02	DMDFON	LOK	filter value segment duration, for calculation
FSE73_03	DMDFON	LOK	filter value segment duration, for calculation
FSE73_04	DMDFON	LOK	filter value segment duration, for calculation
FSE73_05	DMDFON	LOK	filter value segment duration, for calculation
FSE73_06	DMDFON	LOK	filter value segment duration, for calculation
FSE73_07	DMDFON	LOK	filter value segment duration, for calculation
FSE73_08	DMDFON	LOK	filter value segment duration, for calculation
FSE73_09	DMDFON	LOK	filter value segment duration, for calculation
FSE73_10	DMDFON	LOK	filter value segment duration, for calculation
FSE73_11	DMDFON	LOK	filter value segment duration, for calculation
FSE73_12	DMDFON	LOK	filter value segment duration, for calculation
FSE81_02	DMDFON	LOK	filter value segment duration, for calculation
FSE81_03	DMDFON	LOK	filter value segment duration, for calculation
FSE81_04	DMDFON	LOK	filter value segment duration, for calculation
FSE81_05	DMDFON	LOK	filter value segment duration, for calculation
FSE81_06	DMDFON	LOK	filter value segment duration, for calculation
FSE81_07	DMDFON	LOK	filter value segment duration, for calculation
FSE81_08	DMDFON	LOK	filter value segment duration, for calculation
FSE81_09	DMDFON	LOK	filter value segment duration, for calculation
FSE81_10	DMDFON	LOK	filter value segment duration, for calculation
FSE81_11	DMDFON	LOK	filter value segment duration, for calculation
FSE81_12	DMDFON	LOK	filter value segment duration, for calculation
FSE82_02	DMDFON	LOK	filter value segment duration, for calculation
FSE82_03	DMDFON	LOK	filter value segment duration, for calculation
FSE82_04	DMDFON	LOK	filter value segment duration, for calculation
FSE82_05	DMDFON	LOK	filter value segment duration, for calculation
FSE82_06	DMDFON	LOK	filter value segment duration, for calculation
FSE82_07	DMDFON	LOK	filter value segment duration, for calculation
FSE82_08	DMDFON	LOK	filter value segment duration, for calculation
FSE82_09	DMDFON	LOK	filter value segment duration, for calculation
FSE82_10	DMDFON	LOK	filter value segment duration, for calculation
FSE82_11	DMDFON	LOK	filter value segment duration, for calculation
FSE82_12	DMDFON	LOK	filter value segment duration, for calculation
FSE83_02	DMDFON	LOK	filter value segment duration, for calculation
FSE83_03	DMDFON	LOK	filter value segment duration, for calculation
FSE83_04	DMDFON	LOK	filter value segment duration, for calculation
FSE83_05	DMDFON	LOK	filter value segment duration, for calculation
FSE83_06	DMDFON	LOK	filter value segment duration, for calculation
FSE83_07	DMDFON	LOK	filter value segment duration, for calculation
FSE83_08	DMDFON	LOK	filter value segment duration, for calculation
FSE83_09	DMDFON	LOK	filter value segment duration, for calculation
FSE83_10	DMDFON	LOK	filter value segment duration, for calculation
FSE83_11	DMDFON	LOK	filter value segment duration, for calculation
FSE83_12	DMDFON	LOK	filter value segment duration, for calculation
FZABGS		EIN	fault counter, summary, counts emission relevant misfirings of all cylinders
IDXFOB	DMDFON	LOK	index: shows actual map range (speed, load)
IDXFON	DMDFON	LOK	speed index operating range fuel-on adaptation
IDXFORL	DMDFON	LOK	load index operating range fuel-on adaptation
LUNW	DMDFON	LOK	Engine roughness for 1 camshaft revolution
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
R_SYN	GGDPG	EIN	Synchro schedule
TNST_W	BBSTT	EIN	time after end of start
TS01	DMDFON	LOK	segment duration cylinder 1
TS02	DMDFON	LOK	segment duration cylinder 2
TS03	DMDFON	LOK	segment duration cylinder 3
TS04	DMDFON	LOK	segment duration cylinder 4
TS05	DMDFON	LOK	segment duration cylinder 5
TS06	DMDFON	LOK	segment duration cylinder 6
TS07	DMDFON	LOK	segment duration cylinder 7
TS08	DMDFON	LOK	segment duration cylinder 8
TSK	DMDFON	AUS	corrected segment duration
TSK01	DMDFON	LOK	corrected segment duration cylinder 1
TSK02	DMDFON	LOK	corrected segment duration cylinder 2
TSK03	DMDFON	LOK	corrected segment duration cylinder 3
TSK04	DMDFON	LOK	corrected segment duration cylinder 4
TSK05	DMDFON	LOK	corrected segment duration cylinder 5
TSK06	DMDFON	LOK	corrected segment duration cylinder 6
TSK07	DMDFON	LOK	corrected segment duration cylinder 7
TSK08	DMDFON	LOK	corrected segment duration cylinder 8
TSK_M	DMDFON	LOK	monitor corrected segment duration
TSROH2_W	DMDTSB	EIN	second segment duration uncorrected (just for 2 control units)
TSROH_W	DMDTSB	EIN	segment duration uncorrected
TS_M	DMDFON	LOK	monitor segment duration
XS02	DMDFON	LOK	segment deviation, standardized
XS03	DMDFON	LOK	segment deviation, standardized
XS04	DMDFON	LOK	segment deviation, standardized
XS05	DMDFON	LOK	segment deviation, standardized
XS06	DMDFON	LOK	segment deviation, standardized
XS07	DMDFON	LOK	segment deviation, standardized









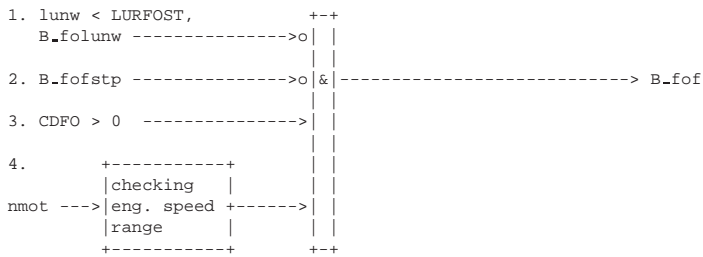


2. no misfires are detected (in this case all detection methods are taken into consideration) and the learning filter flmx does not drift away (flmx <= SLFOON, B\_fohold = 0). See chapter "healing"
3. no deactivation of misfire detection or fuel-on adaptation occurs (B\_mdstop=0, B\_fonstp=0).
4. no further conditions to deactivate fuel-on adaptation occur (see %DMDSTP).
5. The adaptation can be switched off by the code word CDFO. CDFO > 0: function active. By means of the code word CDFO the adaptation can also be reset (like after powerfail): CDFO -> 0, thereafter again CDFO > 0 to reactivate the adaptation.
6. the engine speed and the load lie within one of the operating ranges.

Since calculation is carried out asynchronously (virtually off-line) a retroactive masking is performed on the already stored values (for this look at "Course of the calculation": Favourable: retroactive masking for e.g. 2 camshaft revolutions)

### 2.2.2. Conditions for fuel-off adaptation resp. setting of B\_fof:

Overview:



A fuel-off adaptation is carried out if

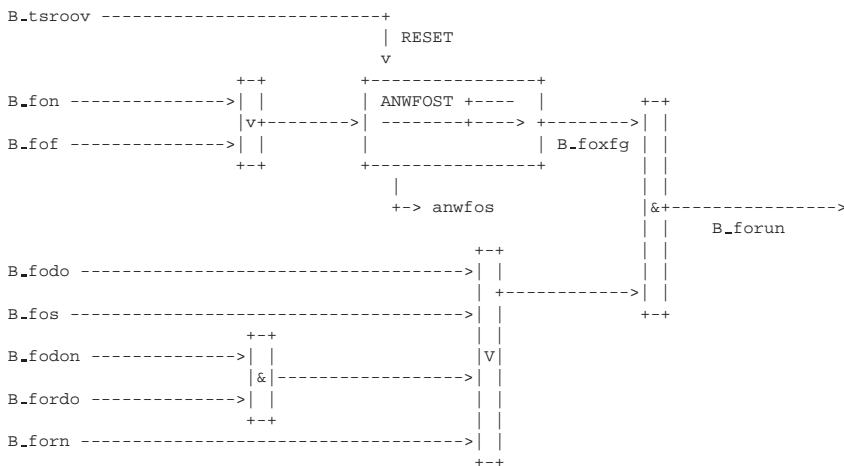
1. no strong segment time changes occur (lunw(n) <= LURPOST); B\_folunw = 0. (see fuel-on adaptation)
2. no deactivation of fuel-off-Adaptation occurs (B\_fofstp=0).
3. see above, as with B\_fon
4. there exists a corresponding engine speed range (set by KFCFO; value 4 in lowest operation range of the speed range => fuel cut-off range)

Since calculation is carried out asynchronously (virtually off-line) a retroactive masking is performed on the already stored values (for this look at "Course of the calculation": Favourable: retroactive masking for e.g. 2 camshaft revolutions)

### 2.2.3. Further conditions for the learning start (learning strategy):

Once the conditions for fuel-on (B\_fon) or fuel-off adaptation (B\_fof) have been fulfilled, ANWFOST camshaft revolutions are still waited for, until the learning starts (-> camshaft counter anwfos).

Due to the learning strategy, the learning may be blocked in a map range at a certain moment. An engine speed dominant range, for example, cannot learn until a dominant range has stabilized. A normal range cannot learn until the engine speed dominant range of the engine speed range has stabilized.  
(Description of the range characteristics see chapter 3.1)





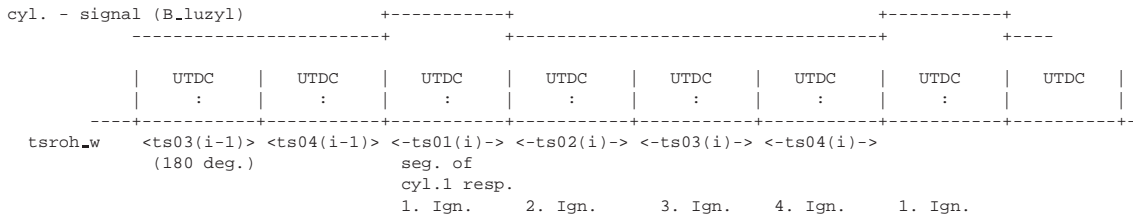
**2.3. Cylinder assignment of individual segments:**

During adaptation the segment of cylinder 1 (ts01, B<sub>mdzyl1</sub> = 1) is used as the reference (is not corrected). The other segments (for 4 cyl.: ts02, ts03, ts04) are corrected during the segment time calculation by the learned filter value fsexx-(Zdg)(n).

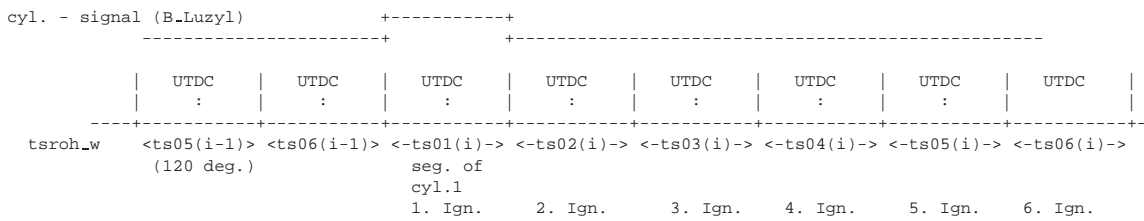
The chronological sequence of crankshaft segments (period of individual ignition intervals) and their designations are illustrated in the following diagrams:

**Example 4-cylinder engine:**

The cylinders are listed in their firing order.



**Example 6-cylinder engine:**



**2.4. Calculation of segment deviation and dynamic correction:** The calculation described below occurs at every camshaft revolution. The deviation between a computed value and a measured value (for 2 camshaft revolutions) is evaluated. The computed value is composed of the reference segment and a dynamic correction. (The dynamic correction is determined by linear interpolation and serves to compensate for an increase or reduction in engine speed.)

$$\text{Segment deviation} = \text{Reference segment} - \text{Measured value} + \text{Dynamic correction}$$

**Example 4-cylinder engine:**

$$ds02(i) = ts01(i) - ts02(i) + \frac{ts01(i+1) - ts01(i)}{zylza}$$

$$ds03(i) = ts01(i) - ts03(i) + \frac{2 * [ts01(i+1) - ts01(i)]}{zylza}$$

$$ds04(i) = ts01(i) - ts04(i) + \frac{3 * [ts01(i+1) - ts01(i)]}{zylza}$$

**2.5. Normalization of segment deviations:**

Subsequent division by the corresponding segment e.g. ts02(i) converts the deviation into an angle-proportional variable (independent of engine speed), which corresponds to the deviation of the segments.

$$xs02'(i) = \frac{ts02(i) + ds02(i)}{ts02(i)}$$

$$xs03'(i) = \frac{ts03(i) + ds03(i)}{ts03(i)}$$

$$xs04'(i) = \frac{ts04(i) + ds04(i)}{ts04(i)}$$



The values  $xs02'$ ,  $xs03'$ ... are displayed in deg. crankshaft.

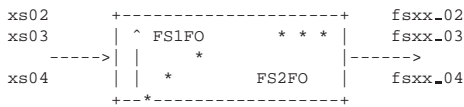
$$xs02(i) = \frac{ds02(i)}{ts02(i)}$$

$$xs02'(i) = 1 + xs02(i)$$

### 2.6. Filtering of segment deviation resp. calculation of filter values $fsxx_{-}(Zdg)(i)$ :

The normalized differential segment times  $xs*(i)$  are smoothed by a low-pass filter (filter factor FS1FO or FS2FO). The result represents the range-specific filter value  $fsxx_{-}(Zdg)(i)$ :  
[Zdg: from 2..zylza]

$$fsxx_{-}(Zdg)(i) = (1 - FS1/2FO) * fsxx_{-}(Zdg)(i-1) + (FS1/2FO) * xs(Zdg)(i)$$



$fsxx_{-}(Zdg)(i)$  is formed in each operating range from the current differential segment times.

The currently learning range is identified by the index  $idxfob$ .

The segment time filter values  $fsxx_{-}(Zdg)(i)$  are stored non-volatily in the RAM for each operating range. (Output of the filter values  $fsxx_{-}(Zdg)(i)$  in the unit deg. crankshaft.)

A restriction to plausible maximum values is performed:

$$-ALFO \leq fsxx_{-}(Zdg)(i) \leq ALFO \quad (\text{Unit: in deg. crankshaft as deviation from reference segment})$$

ALFO corresponds to the greatest possible deviation (sensor wheel tolerances and torsional vibrations).

The filter factors FS1FO resp. FS2FO are dictated by adjustable fixed values, whereby FS1FO resp. FS2FO are selected dependent on the progress of the adaptation:

FS1FO, if  $B_{forxx}=0$

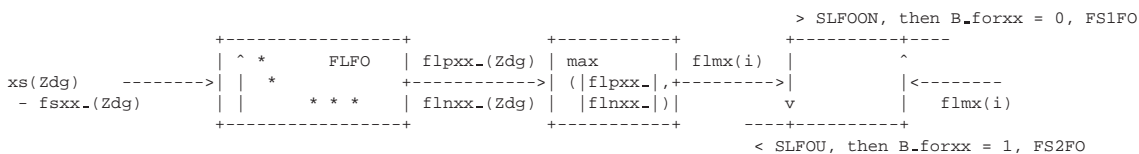
FS2FO, if  $B_{forxx}=1$

The correction of the segment times (with the filter values) takes into account the learning progress or adaptationstatus. Dependent on the progress, either the current filter value  $fsxx_{-}(Zdg)(i)$  or a filter value from the adjacent ranges is used. (See "Learning strategy")

The filter value used for segment time correction is designated is formed by interplation between the individual operating range filter values  $fsexx_{-}(Zdg)(i)$ .

### 2.7. Calculation of learning progress resp. calculation of $flpxx_{-}(Zdg)(i)/flnxx_{-}(Zdg)(i)$ and $flmx(i)$ :

Overview learning filter:



### Calculation of $flpxx_{-}(Zdg)(i)$ and $flnxx_{-}(Zdg)(i)$ :

To check whether adaptation is complete, 2 learning filter values exist for each filter value  $fsxx_{-}(Zdg)(i)$ .

That means 2 filter values are formed for each operating range.

The measure used here is the difference between the normalized segment time deviations  $xs(Zdg)(i)$  (= the current measured value) and the filtered values  $fsxx_{-}(Zdg)(i)$  (i.e. the values calculated so far).

The filter  $flpxx_{-}(Zdg)(i)$  starts at the maximum possible deviation ALFO,  $flnxx_{-}(Zdg)(i)$  starts at -ALFO.

The learning filters  $flpxx_{-}(Zdg)(i)$ ,  $flnxx_{-}(Zdg)(i)$  filter towards the diminishing deviation

$xs(Zdg)(i) - fsxx_{-}(Zdg)(i)$ . [Zdg: from 2..zylza]

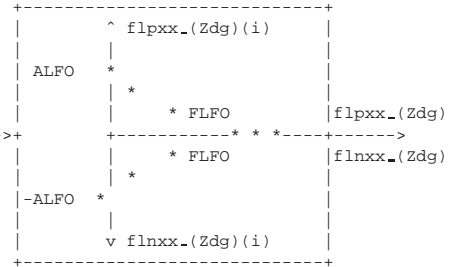
$$flpxx_{-}(Zdg)(i) = (1-FLFO) * flpxx_{-}(Zdg)(i-1) + FLFO * [xs(Zdg)(i) - fsxx_{-}(Zdg)(i)]$$



```
flnxx_(Zdg)(i) =
(1-FLFO) * flnxx_(Zdg)(i-1) + FLFO * [xs(Zdg)(i) - fsxx_(Zdg)(i)]
```

```
start. value: flpxx_(Zdg)(i) = ALFO          xs(Zdg)(i) - fsxx_(Zdg)(i)
              flnxx_(Zdg)(i) = -ALFO
```

flpxx\_(Zdg) and flnxx\_(Zdg) tend towards 0 during the adaptation.



ALFO corresponds to the maximum possible deviation (sensor wheel tolerances and torsional vibrations).

#### Formation of flmx(i), Setting of B\_forxx:

The absolute value is formed from the filter values flpxx\_(Zdg)(i) and flnxx\_(Zdg)(i) and then the greatest filter value flmx(i) (-> flmx = max ( |flpxx\_(Zdg)|, |flnxx\_(Zdg)|; maximum across all cylinders) is compared to the threshold values SLFOU (FW) and SLFOON (KL). SLFOON uses the same speed base points as KFCFO.

If the value flmx(i) lies above the threshold SLFOON, then B\_forxx = 0 (flmx > SLFOON).  
(for: fuel-on/fuel-off adaptation ready; xx: operating range)

If the value lies below the threshold SLFOU, adaptation is regarded as stabilized (respectively ready; flmx < SLFOU -> B\_forxx = 1). If flmx(i) then rises above the threshold SLFOON from below (flmx > SLFOON), the adaptation reacts as follows:

- if the actual range is a dominant range or a fuel cut-off range then the adaptation is restarted (reset), the reset counter flmxresz is incremented
- in other ranges B\_forxx is set to zero (B\_forxx = 0) and the adaptation is stopped (B\_fohold -> 1)

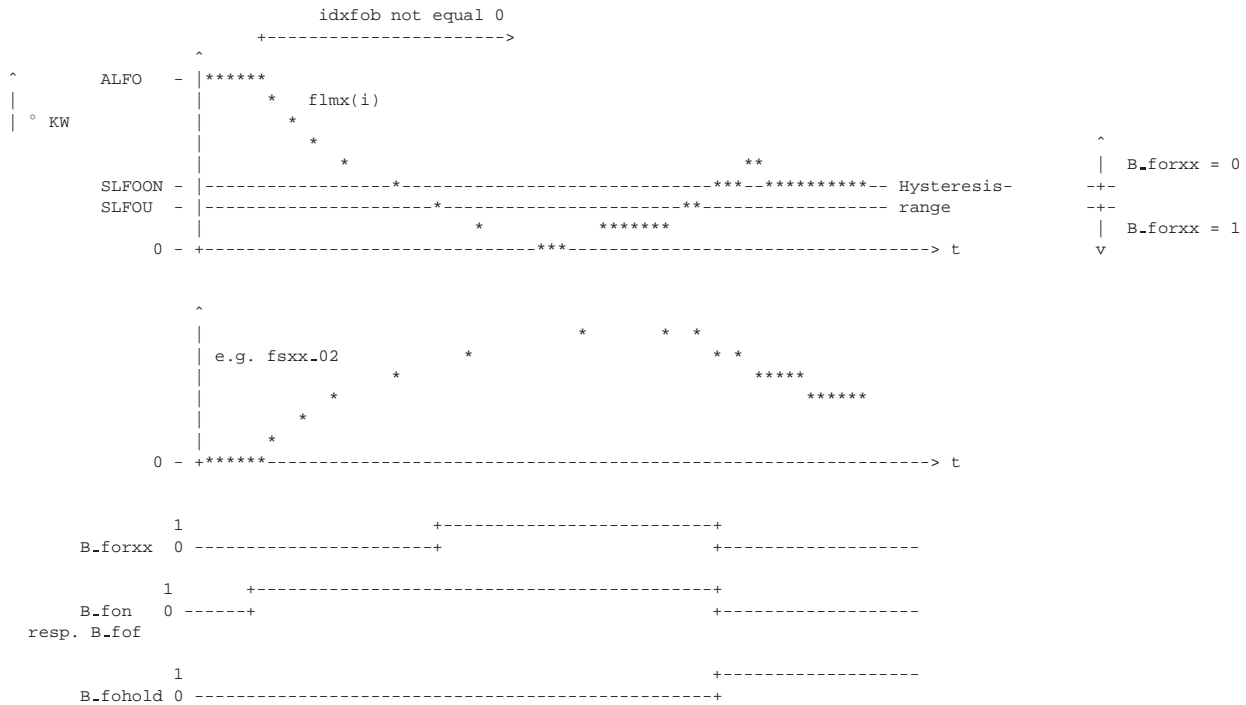
In case of small changes in flmx(i) (< SLFOON) the adaptation is still regarded as stabilized (B\_forxx = 1). There is thus a hysteresis range between SLFOU and SLFOON.

In addition to B\_forxx, in which the adaptation status of the corresponding range xx is stored, the bit B\_for is formed. B\_for shows the adaptation status of the current operating range. (B\_for is stored in the drum => measure B\_for\_m.)

The adaptation generates a status (fostat) by the status-bits (B\_fordo, B\_fornnn, B\_forxx and B\_ploknn). This status applies to the current operating range. The sensitivity of the misfire detection is adjusted dependent on the adaptation progress (fostat). Corresponding detection thresholds are assigned to each status (see %DMDLU).

If the conditions for the adaptation in the current operating range are fulfilled then B\_fon=1 (fuel-on adaptation) resp. B\_fof =1 (fuel-off adaptation) is set. Otherwise, if conditions are not fulfilled fuel-on/fuel-off adaptation: B\_fon/B\_fof=0 . The adaptation is active as soon as bit B\_forun is set (B\_fon resp. B\_fof = 1 and ANWFOST completed and learning strategy allows learning / see 2.2.3). In addition the bit B\_fodo is set, if the conditions for the adaptation in a dominant range (dominant fuel-on range or fuel cut-off range) are fulfilled. If a non-dominant range or no range is active B\_fodo = 0 applies.

Overview of temporal course:



Attention: In case the operating range is a dominant range or a fuel cut-off range, the entire adaptation is reset, if  $flmx > SLFOON$  (after stabilized adaptation), the reset counter  $flmxresz$  is incremented.

### 3. Learning resp. adaptation strategy:

#### 3.1. Definition resp. setting of the operating range status:

A status can be assigned to each range. The setting of the status is performed via the characteristic map KFCFO.

#### Value bit

- 1 0 means normal operating range:  
In this range adaptation is performed ( $B_{fon} = 1$ ) and the learned value is used for segment time correction (dependent on the learning progress).
- 2 1 means dominant range:  
Range which is frequently entered ( $B_{fodo} = 1$ ) and in which misfire should also be detected without adaptation. In the dominant range the first rough adaptation is performed which is spread to adjacent ranges (for  $B_{fodo} = 0 \rightarrow 1$ ).
- 4 2 means fuel cut-off range (fuel-off-range): Each fuel-off-range is automatically dominant. In a fuel cut-off range the load information is not relevant. Within the engine speed limits adjusted via KFCFO adaptation is only performed ( $B_{fodo} = 1$ ) if the condition  $B_{fof} = 1$  is set. It is only possible to define the lowest line (low load) of KFCFO as fuel cut-off range. The load base points of the lowest line are only of interest for the correction of the segment durations with the adaptation values. For the correction of segment durations the fuel cut-off ranges are treated like all other ranges. That means that the values learned during fuel cut-off are used for the correction of segment durations.
- 8 3 means dominant range within an engine speed range ("dominant n-range"):  
This range must be the first to be stabilized within an engine speed range. The adaptation values are then spread to the entire engine speed range (if a rough adaptation has already taken place). This range should frequently be entered and misfires must here be detected as accurately as possible in comparison to the other ranges of the engine speed range. (Favourable: high load. In each engine speed range at least one range of the type \*+2, \*+4 or \*+8 must be present. If the first learning phase has been terminated then the ranges of type \*+2, \*+4, \*+8 within an engine speed range have equal rights. (\*: can be 0 or 128)
- 16 4 means blocked range:  
In this range an adaptation is performed ( $B_{fon} = 1$ ), the filter values are calculated, however the bit  $B_{for}$  is not set in this range, that means the learned values are not used for the segment time correction. The value of the 1. learned dominant range of which learning has been terminated ( $\rightarrow$  spreading of the dominant range, phase 1) or of the 1. learned engine speed range of which learning has been terminated (phase 2) is included in the calculation.
- 128 7 means healing range. If misfire has been detected at first a healing range must be entered ( $B_{fohe} = 1$ ) before adaptation is continued. (Exception: in a fuel cut-off range it is also possible to learn if healing is active ( $B_{fohold} = 1$ )). Within a healing range misfire should always definitely be detected even without adaptation. Only combinations 128+1, 128+2, 128+8 are possible or useful. That means a healing range can only be a normal range, a dominant range within an engine speed range or a dominant range (a fuel cut-off range can not be defined as a healing range).





The label cfoxx indicates the characteristics of the range that is current for learning (e. g. cfoxx = 130, if the current range is a dominant healing range).

Example KFCFO

	13	23	33	43	53	63	73	83*	rl
128+1	128+1	128+8	8	8	8	8	8	8	^
12	22	32	42	52	62	72	82		
128+2	128+2	1	1	1	1	1	1		
11	21	31	41	51	61	71	81		
4	1	1	1	1	1	1	16		

B.fof -----> nmot

eng. speed eng. speed eng. speed eng. speed eng. speed eng. speed eng. speed eng. speed  
| range 1 | range 2 | range 3 | range 4 | range 5 | range 6 | range 7 | range 8 |

\*: Index: idxfob  
Status of operating range

### 3.2. Spreading of the first learned ranges to adjacent ranges (3-phase-adaptation):

The adaptation is subdivided into 3 phases:

Depending on the learning progress in these 3 phases the sensitivity of misfire detection is increased.

#### 1. phase: adaptation in the dominant range resp. fuel cut-off: (-> B.fordo=1)

At first a rough adaptation is performed during which the rough mechanical inaccuracies of the sensor wheel are learned. This first rough adaptation is stabilized if >= 1 dominant fuel-on range or fuel cut-off range has finished learning.(B.fordo=1). (Remark: if a fuel cut-off range is set then it is automatically regarded as being dominant.)

Principal picture:

after powerfail:

1 dominant range has finished learning:

rl	1	1	1	1	1	1	1	1	1
	1	1	1	1	1	1	1	1	1
	1	1	1	1	1	1	1	1	1

=====>

D	D	D	D	D	D	D	D	D	D
D	D	D	D	D	D	D	D	D	D
D	D	D	D	D	D	D	D	D	D

1: stands for factor = 1.0 in fs.fse., i.e.. no ts-correction, state after powerfail

D: complies to the filt. values of the 1. learned dominant range, which is used in the entire operating range for the segment time correction

Once the first dominant range has been learned (B.fordo=1) the values of this range are used for segment time correction in the entire operating range of the engine. These dominant values are spread to the entire engine operating range. This spreading resp. overwriting occurs only once as soon as flmx(i) is smaller than SLFOU (flmx(i) < SLFOU) in the dominant range. If the dominant range continues to adapt spreading to the adjacent ranges resp. overwriting of the adjacent ranges no longer occurs.

When other dominant ranges have finished learning, the adjacent ranges are no longer overwritten. In other words: Once the first dominant range has finished learning, the remaining ranges all adopt equal status regardless of whether they were previously dominant or non-dominant.

The dominant range of a speed range and a normal range can only learn if a dominant range is stabilized.

For the engine speed range in which the dominant operating range lies the bit B.forn\* = 1 is already set after the dominant range has stabilized. (see phase 2)(\* e.g. 01...08)

#### 2. phase: adaptation in an engine speed range: (-> B.forn01/02/03... = 1)

An engine speed range is considered to have stabilized if the dominant range of the engine speed range has stabilized.

The dominant range of a speed range can only learn if a dominant range is stabilized.

Example:

In the engine speed range 1 the range 12 is dominant.

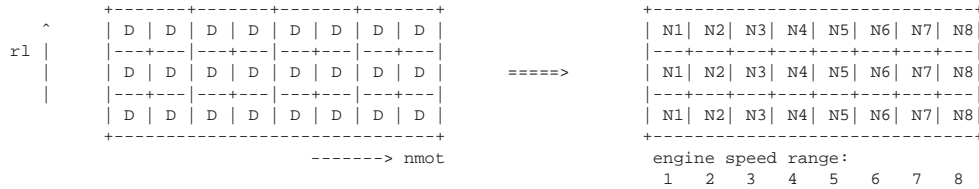
Then the engine speed range has stabilized (B.forn1 = 1), if: B.for12 = 1 applies.



Principal picture:

one dominant range has finished learning (phase 1 completed)

in each engine speed range at least 1 dominant range within the engine speed range has finished learning



N1: complies to the filter values which are used in engine speed range 1 for segment time correction.

As soon as a dominant range within the engine speed range has finished learning the learned filter values are used within this engine speed range for the segment time correction (spread to the various loads). In other words: The values learned in the dominant range of the engine speed range are spread to the entire engine speed range.

This spreading resp. overwriting occurs only once as soon as  $flmx(i) < SLFOU$  is in the dominant range of the engine speed range. If the dominant range continues to adapt spreading to the adjacent ranges resp. overwriting of the adjacent ranges no longer occurs.

The termination of the learning of the other non-dominant ranges of the engine speed range does not lead to an overwriting of the adjacent ranges. With other words: After the dominant range of the engine speed range has finished learning all ranges of the engine speed range adopt an equal status.

3. phase: Fine adaptation resp. adaptation in the according load/engine speed range: ( $\rightarrow B\_forxx = 1$ )

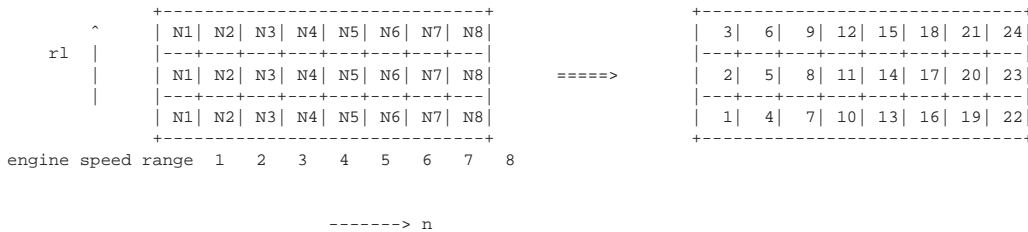
The fine adaptation has completely stabilized if in all load/engine speed ranges  $B\_forxx$  is set.

A normal range can only learn if a dominant range and the dominant range of the speed range is stabilized.

Principal picture:

one dominant range within each engine speed range has finished learning

all load/engine speed ranges have finished learning, fine adaptation is terminated



N1: complies to the filter values used in engine speed range 1- for segment time correction.

1...: complies to the filter values used in the according load/engine speed range for segment time correction.

As soon as an operating range has finished learning ( $flmx(i) < SLFOU$ ,  $B\_forxx = 1$ ), the learned filter values are used within this operating range for the segment time correction. If  $B\_forxx = 1$ , the filter values  $fsexx$  are spread together with the filter values  $fsxx$ . That means both filter values are identical (except quantization).

3.3. Detailed example for the 3-phase-adaptation:

The following diagram illustrates the engine operating range with the filter values used, after only the dominant range 21 has stabilized ( $B\_for21 = B\_fodo = 1$ ). [For the sake of simplicity the cyl. designations have been omitted and just 3x6 operation areas are shown.]



```

+---->  r1  -| fse21  13| fse21  23| fse21  33| fse21  43| fse21  53| fse21  63*| . . .
| +-->    ^  | fs13;  0 | fs23;  0 | fs33;  0 | fs43;  0 | fs53;  0 | fs63;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse21  12| fse21  22| fse21  32| fse21  42| fse21  52| fse21  62| . . .
| |      |  | fs12;  0 | fs22;  0 | fs32;  0 | fs42;  0 | fs52;  0 | fs62;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse21  11| fse21  21| fse21  31| fse21  41| fse21  51| fse21  61| . . .
| |      |  | fs11;  0 | =fs21;  1 | fs31;  0 | fs41;  0 | fs51;  0 | fs61;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      B_forn01=0  B_forn02=1  B_forn03=0  B_forn04=0  B_forn05=0  B_forn06=0
| |
| |-----> nmot
+----- calculated filter value resp. filter value used for segment time correction
+----- filter value learned in the range; adaptation status B_forxx
    
```

Now the dominant range 41 stabilizes within the engine speed range 4.  
The value learned in range 41 is spread to the engine speed range 4 and is there used for the segment time correction.

```

+---->  r1  -| fse21  13| fse21  23| fse21  33| fse41  43| fse21  53| fse21  63*| . . .
| +-->    ^  | fs13;  0 | fs23;  0 | fs33;  0 | fs43;  0 | fs53;  0 | fs63;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse21  12| fse21  22| fse21  32| fse41  42| fse21  52| fse21  62| . . .
| |      |  | fs12;  0 | fs22;  0 | fs32;  0 | fs42;  0 | fs52;  0 | fs62;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse21  11| fse21  21| fse21  31| fse41  41| fse21  51| fse21  61| . . .
| |      |  | fs11;  0 | =fs21;  1 | fs31;  0 | =fs41;  1 | fs51;  0 | fs61;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      B_forn01=0  B_forn02=1  B_forn03=0  B_forn04=1  B_forn05=0  B_forn06=0
| |
| |-----> nmot
+----- calculated filter value resp. filter value used for segment time correction
+----- filter value learned in the range; adaptation status B_forxx
    
```

When other ranges (including non-dominant ranges) have stabilized (B\_forxx=1), the now-learned filter value fsxx.(Zdg)(i) is used for segment time correction in the stabilized range. Hereafter: fsxx.(Zdg)(i) = fsxx.(Zdg)(i).

e.g.: ranges 11, 12, 21, 41 and 42 have stabilized (B\_for11 = B\_for12 = B\_for21 = B\_for41 = B\_for42 = 1)  
(Precondition: range 11 is the dominant range of engine speed range 1)

```

+---->  r1  -| fse11  13| fse21  23| fse21  33| fse41  43| fse21  53| fse21  63*| . . .
| +-->    ^  | fs13;  0 | fs23;  0 | fs33;  0 | fs43;  0 | fs53;  0 | fs63;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse12  12| fse21  22| fse21  32| fse42  42| fse21  52| fse21  62| . . .
| |      |  | =fs12;  1 | fs22;  0 | fs32;  0 | =fs42;  1 | fs52;  0 | fs62;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      -| fse11  11| fse21  21| fse21  31| fse41  41| fse21  51| fse21  61| . . .
| |      |  | =fs11;  1 | =fs21;  1 | fs31;  0 | =fs41;  1 | fs51;  0 | fs61;  0 |
| |      |  |-----|-----|-----|-----|-----|-----|
| |      B_forn01=1  B_forn02=1  B_forn03=0  B_forn04=1  B_forn05=0  B_forn06=0
| |
| |-----> nmot
+----- calculated filter value resp. filter value used for segment time correction
+----- filter value learned in the range; adaptation status B_forxx
    
```



### 3.4. Consideration of the learning/adaptation progress for the sensitivity of misfire detection:

Corresponding to the adaptation progress in the 3 adaptation phases the sensitivity of the misfire detection is increased. There are 4 sensitivity stages during misfire detection:

	status byte fostat:
- stage 3: after powerfail:	fostat = 3
- stage 2: after adaptation 1. phase:	fostat = 2
- stage 1: after adaptation 2. phase:	fostat = 1
- stage 0: after adaptation 3. phase and B_ploknn = 1: (see under plausibility check)	fostat = 0

For the current operating range (+ subrange) the adaptation puts a status information (fostat) at the disposal of the misfire detection (%DMDLU). From the status information which indicates the learning progress the misfire detection fixes the according LURMIN\* thresholds.

The bits B\_fordo, B\_fornnn, B\_forxx and B\_ploknn clearly indicate the adaptation status of the current operating range.

The table shows the definite assignment:

B_fordo	B_fornnn	B_forxx	B_ploknn	Status (fostat)
0	X	X	X	3
1	0	X	X	2
1	1	0	X	1
1	1	1	0	1
1	1	1	1	0

nn = current eng. speed range, xx = current operating range, X = not relevant

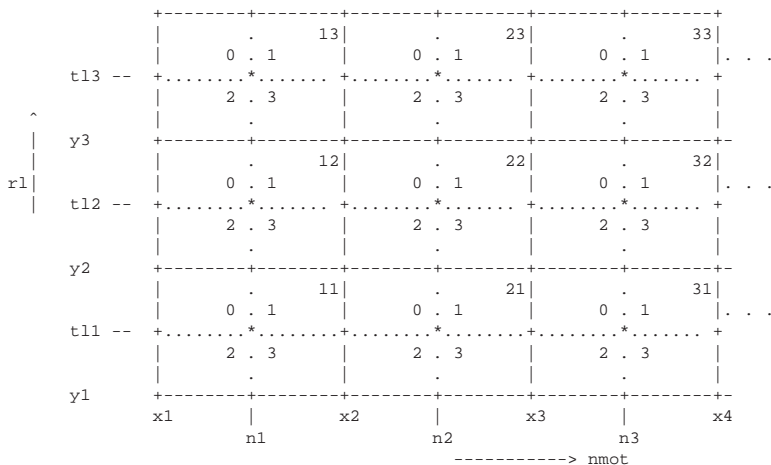
The assignment of the adaptation status (fostat) to the according LURMIN thresholds is described in %DMDLU.

fostat indicates the current adaptation status in the corresponding operating range.

Due to interpolation the adaptation state of the adjacent range has to be considered when fixing the status. (see example in app) For this an operating range is again subdivided into 4 equal parts (subranges). The subranges numbered from 0 to 3. When driving in the corresponding subrange each time the adaptation state of the adjacent subranges which lie outside the main range is checked. The least advanced status is then used. That means status of the current range = worst status from: current range, 3 adjoining ranges of the current range.

e.g.:

If driving in the main range 22, subrange 2, the main ranges 12, 11 and 21 are checked. If the learning progress of these adjacent main ranges 12, 11 and 21 is worse (no. of the status is larger) than in the main range 22 then the least advanced status is used.



\*: position of the adaptation mean values, from here interpolation is performed.

'.....': range limit subrange

'-----': " main range



### 3.5. Healing:

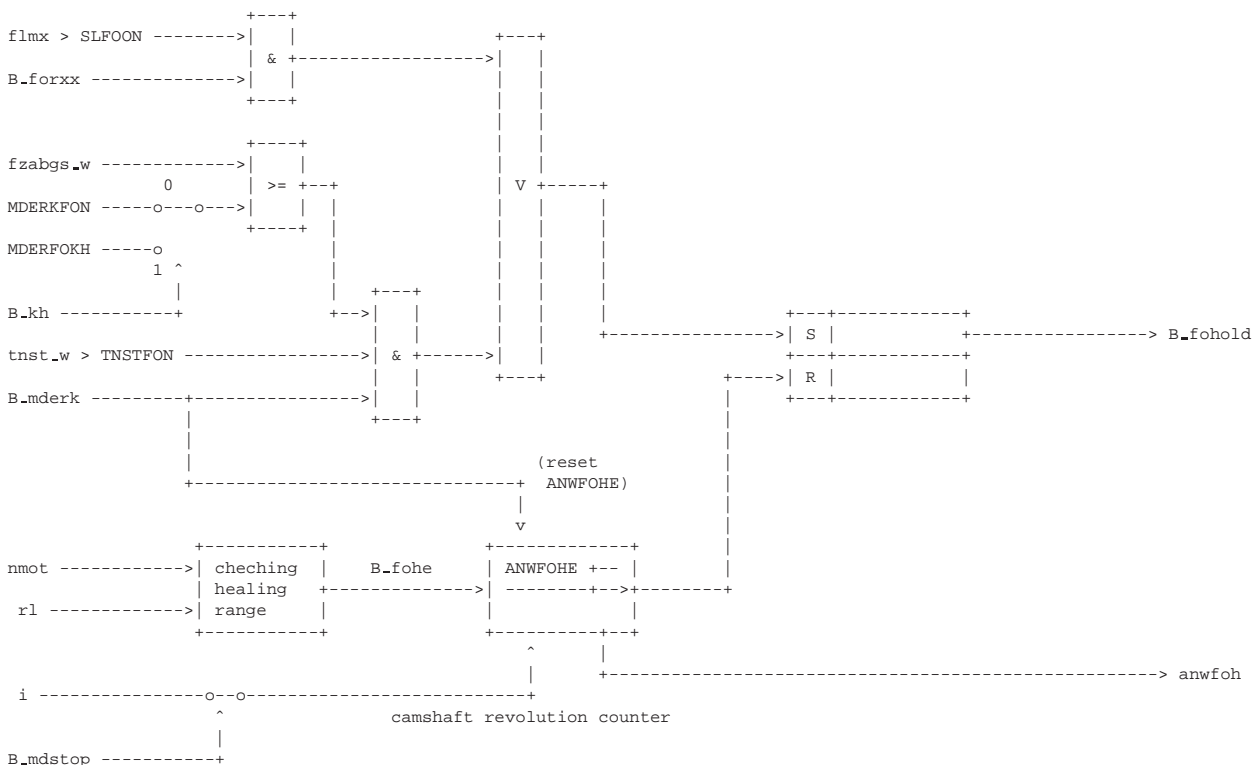
The filtering of the adaptation filters  $fs^*$  is stopped as soon as misfires are detected and the counter for misfires  $fzabgs$  (DMDMIL) is above the threshold  $MDERKFON$  (threshold  $MDERFOKH$  for  $B_{kh} = 1$  (catalytic converter heating)) and if  $tnst_w$  (time since engine start)  $> TNSTFON$  or if the learning filter  $flmx$  drifts away ( $flmx > SLFOON$ ). (If  $flmx$  rises above  $SLFOON$  ( $flmx > SLFOON$ ) within a dominant range or a fuel cut-off range then the adaptation gets restarted (reset of all ready-bits).)  $MDERKFON$ ,  $MDERFOKH$  indicates the number of misfires that can occur within a certain number of crankshaft rotations before the adaptation is stopped (see calculation of  $fzabgs$  in DMDMIL).

The learning filter recognizes the changes before the adaptation values drift away (-> important:  $FLFO = 4 * FS1FO$ ).

The filtering is reactivated only if healing in a healing range is finished. The stop of the adaptation occurs in the entire operating range except in fuel cut-off range (->  $B_{fohold} = 1$ ).

Healing is performed if while driving in a coherent healing range ( $B_{fohe} = 1$ ) no misfires were detected. For healing a coherent healing range must be entered constantly for  $ANWFOHE$  crankshaft revolutions (counter  $anwfoh$ ).

After the engine was turned off the healing status must be stored until the next engine start procedure.



Just in exceptional cases the thresholds  $MDERKFON$ ,  $MDERFOKH$ ,  $TNSTFON$  should be unequal to zero (see applikation hints). In case both inputs are "1" on the flip-flop then the reset has priority (e.g.  $flmx > SLFOON$ ,  $B_{forxx} = 1$ , and  $ANWFOHE$  completed).

The evaluation of the expression  $[(flmx > SLFOON) \& B_{forxx}]$  takes place before  $B_{forxx}$  is reseted after having exceeded the threshold  $SLFOON$ .

The deactivation is carried out retroactive. That means that when misfire is detected the values dating back a few camshaft revolutions are not used for the adaptation.

### 3.6 Plausibility check of the adaptation values:

The plausibility check should prevent that the learned misfires are taken into account for the calculation. Furthermore it should be prevented that any RAM changes (for example due to EMI stabilization) lead to error detections.

Misfires lead to load-dependent adaptation values. That means if misfires are learned larger adaptation values are obtained with increasing load resp. the differences between the adaptation values of one engine speed range are larger than during normal operating. Torsional vibrations do not necessarily show this load dependence.

The typical deviations during normal operating between the adaptation values of one engine speed range are stored in the characteristic line  $DFSEON$  in deg. crankshaft. The actual value of  $DFSEON$  that is used for the plausibility check is named  $dfsen$ .

The characteristic line has just as many n-base points as  $KFCFO$ .

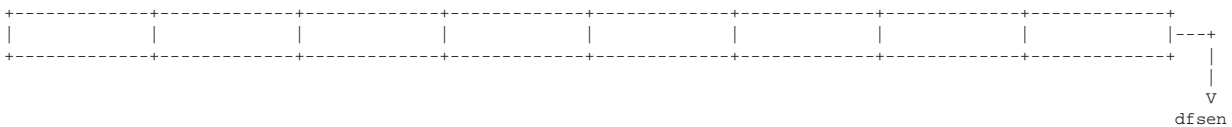


13	23	33	43	53	63	73	83	rl
FSE13_(Zdg)	FSE23_(Zdg)	FSE33_(Zdg)	FSE43_(Zdg)	FSE53_(Zdg)	FSE63_(Zdg)	FSE73_(Zdg)	FSE83_(Zdg)	^
12	22	32	42	52	62	72	82	
FSE12_(Zdg)	FSE22_(Zdg)	FSE32_(Zdg)	FSE42_(Zdg)	FSE52_(Zdg)	FSE62_(Zdg)	FSE72_(Zdg)	FSE82_(Zdg)	
11	21	31	41	51	61	71	81	
FSE11_(Zdg)	FSE21_(Zdg)	FSE31_(Zdg)	FSE41_(Zdg)	FSE51_(Zdg)	FSE61_(Zdg)	FSE71_(Zdg)	FSE81_(Zdg)	

-----> nmot

eng.speed	eng.speed	eng.speed	eng.speed	eng.speed	eng.speed	eng.speed	eng.speed
range 1	range 2	range 3	range 4	range 5	range 6	range 7	range 8

char. line DFSEFON:



The check should if possible be performed at least once for each background program run and this should be done independent of the current adaptation status.

Each time the maximum deviation of the FSE values is calculated via load for each engine speed range.

engine speed range 8:

$$dfse08 = \max[ \max(fse81\_02, fse82\_02, fse83\_02) - \min(fse81\_02, fse82\_02, fse83\_02), \max(fse81\_03, fse82\_03, fse83\_03) - \min(fse81\_03, fse82\_03, fse83\_03), \max(fse81\_04, fse82\_04, fse83\_04) - \min(fse81\_04, fse82\_04, fse83\_04), \dots, \max(fse81\_08, fse82\_08, fse83\_08) - \min(fse81\_08, fse82\_08, fse83\_08) ]$$

engine speed range 7:

$$dfse07 = \max[ \max(fse71\_02, fse72\_02, fse73\_02) - \min(fse71\_02, fse72\_02, fse73\_02), \max(fse71\_03, fse72\_03, fse73\_03) - \min(fse71\_03, fse72\_03, fse73\_03), \max(fse71\_04, fse72\_04, fse73\_04) - \min(fse71\_04, fse72\_04, fse73\_04), \dots, \max(fse71\_08, fse72\_08, fse73\_08) - \min(fse71\_08, fse72\_08, fse73\_08) ]$$

correspondingly:

$$dfse06 = \max[ \dots ]$$

$$dfse05 = \max[ \dots ]$$

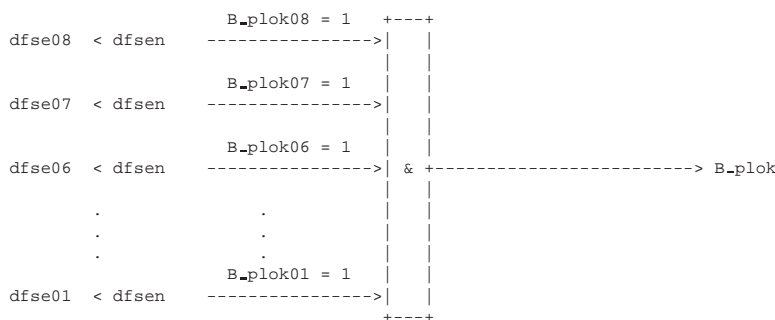
$$dfse04 = \max[ \dots ]$$

$$dfse03 = \max[ \dots ]$$

$$dfse02 = \max[ \dots ]$$

$$dfse01 = \max[ \dots ]$$

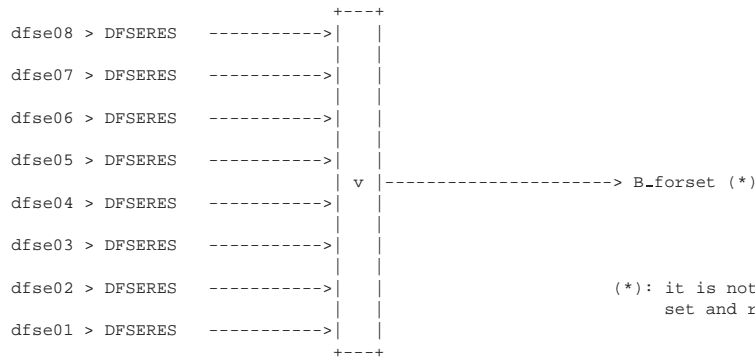
Checking of the plausibility:



If the plausibility condition in an engine speed range nn is not fulfilled (B\_ploknn=0) then the adaptation status (fostat) is not switched to 0 resp. reswitched from 0 to 1 (see table in chapter 3.4). The detection threshold of the misfire detection is adjusted correspondingly by %DMDLU.

B\_plokn shows if values in the actual speed range are plausible.

Should the deviations of the FSE values of an engine speed range differ largely, these may be caused by RAM overruns for example, then the adaptation is reseted (reset) and the reset counter dfseresz is incremented (complete reset of all values except reset counters, B\_forset = 1, -> fostat = 3).



(\*): it is not possible to measure B\_forset because it is set and reset in-between two calculation cycles

#### 4. Starting values and filter factors

After a "computer cold start", powerfail (B\_pwf: 1 -> 0), CDFON -> 0 the following values are predefined:

```

ds(Zdg)(i) = 0 usec
xs(Zdg)(i) = 0 °deg. KW
fsxx_(Zdg)(i) = fsxx_(Zdg)(i) = 0 deg. KW (complies to factor = 1.0)
    
```

```

flpxx_(Zdg)(i) = flmx(i) = ALFO deg. KW
flnxx_(Zdg)(i) = - ALFO deg. KW
    
```

```

dfseresz = 0;
flmxresz = 0;
    
```

Attention: If the reset is triggered by the function itself then the reset counters dfseresz and flmxresz are not set to zero.

#### APP DMDFON 6.40 Application hint

App.-suggestion for a 4-cyl. engine:

```

FS1FO:      0.005...0.01
FS2FO:      0.002
FLFO:       0.02..0.04 = 4 * FS1FO ; the learning filter must always be faster than the adaptation filter so that changes are
detected beforehand, before the adaptation values have drifted away.
At flmx > SLFOON the filtering is then immediately stopped. (reset in dominant and
fuel cut-off range)
The sensitivity of the misfire detection is switched to stage 1 (-> LURMIN1)
important: thus no more misfire detection is possible in this range,
result: misfires must always be detected before flmx > SLFOON
    
```

important: the filter factors of fluts should be faster (i.e. larger value) than FLFO so that the misfires are detected via fluts and the adaptation is stopped in time.  
lunw here serves as immediate stop trigger.

```

k = - (1/F) * ln (1-A);      A: 0..1, percentage of final value
                           k: number of filter steps
e.g.: F = 0.01, A = 0.99 (99 % of final value)
    
```

k = 460; (after 460 camshaft revolutions the adaptation has stabilized to 99 % of the final value, jump function presupposed as input)

```

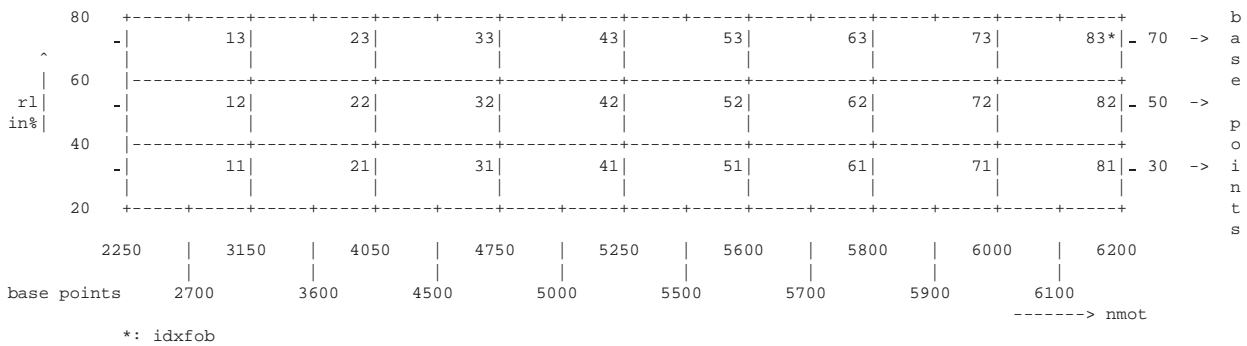
ALFO:       1,2 deg. crankshaft
SLFOU:      0,03 deg. crankshaft
SLFOON:     0,09 deg. crankshaft (at low speed higher, at high speed lower)
ANWFOST:    25
LURFOST:    15
    
```

```

DFSERES:    same as ALFO          (max. value, on which adaptation can be carried out)
MDERKFON:   0
MDERFOKH:   0
TNSTFON:    0
    
```

Prior to the application of KFCFO the systematic engine speed fluctuations in the entire operating range of different vehicles of the according project should be looked at.  
Here the engine speed dependance and load dependance of the adaptation values (fs\* resp. fse) is important.  
Depending on this KFCFO must be fixed with regard to the load and engine speed base points as well as the states of the individual ranges.

KFCFO:



The range limits always lie in the middle between the base points (not the other way round!).  
On the edge of the characteristic map the range limits are spread outwards as described in 1.2.

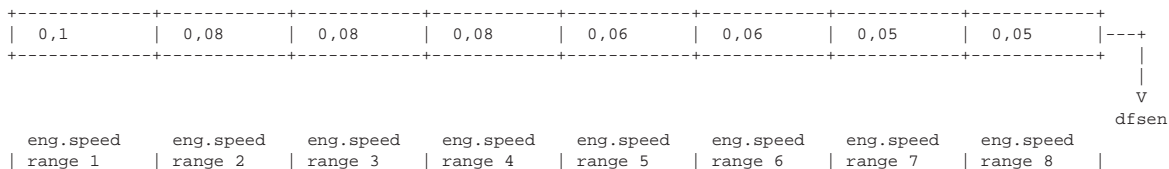
App. of KFCFO:

Dominant ranges should be positioned such that a stabilization of the adaptation values in the FTP75 test is possible. However this is not layed down by the legislator (CARB). For the certification a vehicle on which adaptation has already been terminated may be provided.

Operation ranges in which the adaptation values are not savely stabilized should be inhibited. Attention, in blocked ranges and partially in their adjacent ranges fostat does not reach 0 (see 3.4)!

In each engine speed range there must be at least one range of the type (value) \*+2, \*+4 or \*+8.  
If the first learning phase is completed then the ranges of types \*+2, \*+4 or \*+8 within a engine speed range adopt an equal status.  
(\*: can be 0 or 128)

Example-value characteristic line DFSEFON: (for vehicles with little torsional vibrations)



During application of DFSEFON it must always be taken into account what happens when misfires are learned in the various different operating ranges. The interrelation between the currently active characteristic line LURMIN\* is important.

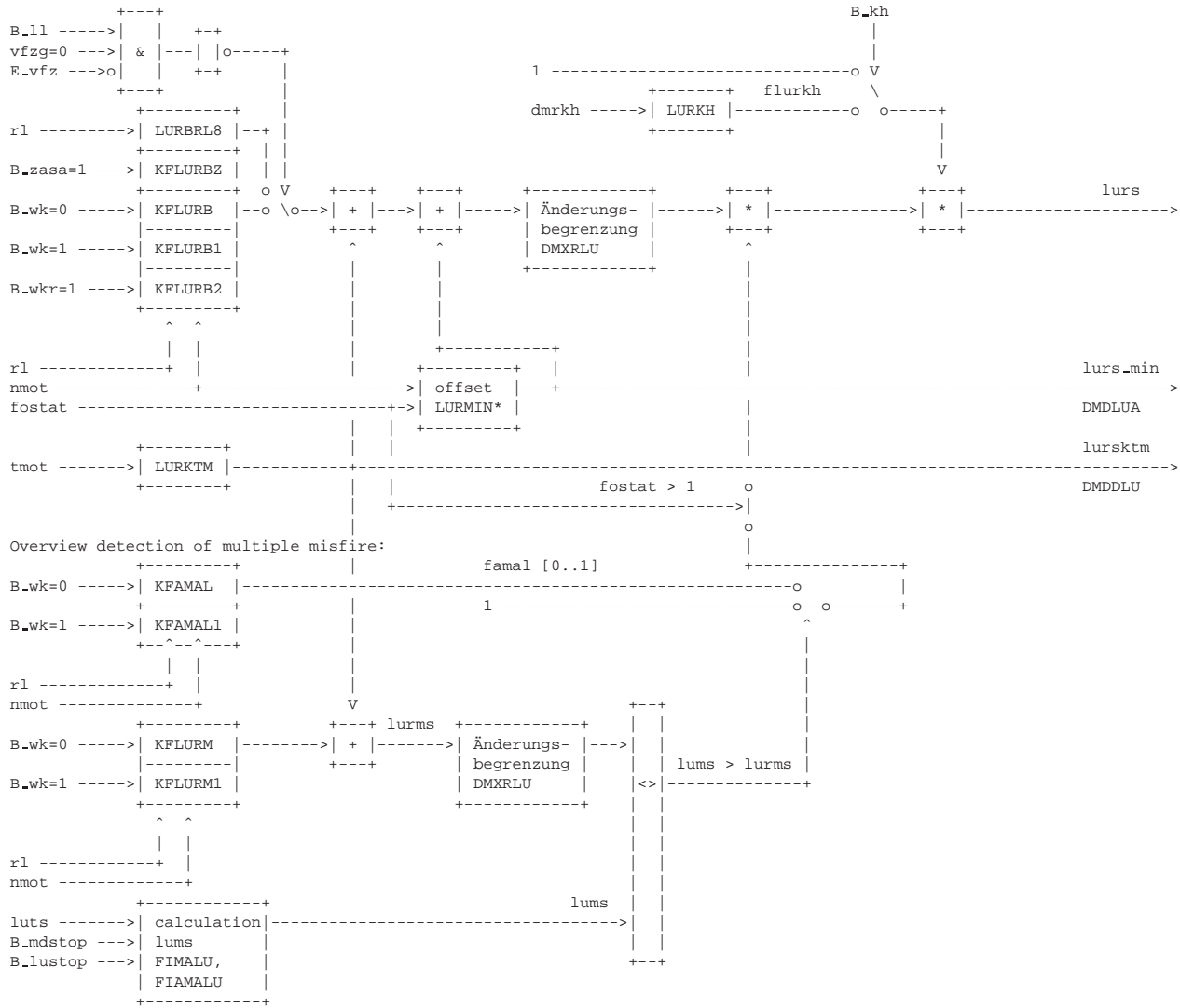
If the plausibility condition in an engine speed range nn is not fulfilled (B\_ploknn=0) the sensitivity of the misfire detection is worsened to stage 1 (LURMIN1).  
The sensitivity is worsened no further since only misfires are not detected during small loads. Misfires during higher loads should be detected even though the sensitivity is poor.  
Again during smaller load the deviation learned by a misfire is so small that by LURMIN1 no misdetection due to this error learning should be performed.

The sensitivity of the misfire detection is only set back to stage 1 if the plausibility check for all load ranges of an engine speed range has successfully been carried out (B\_ploknn=1).

Usually higher load ranges at high engine speeds may be entered much more often than at lower load ranges.







## ABK DMDLU 4.90 Abbreviations

Subscripts and reference points used:

- (n) = Crankshaft segments
- (i) = Camshaft revolutions; NW - Umdr.
- (j) = Crankshaft revolutions; KW - Umdr.
- (t) = Time

- tsk(n) corrected segment duration at the time n
- tsk(n+1) corrected segment duration at the time n+1
- luts(n) engine roughness - test value
- lurs(i) engine roughness reference
- lums(n) engine roughness mean value
- lurms(n) engine roughness mean value reference

- DMDLAD logical and temporary combination of results from different functions for misfire detection
- DMDDL differential imbalance
- DMDSTP stopconditions for misfire detection
- SY\_FLUQ quantization factor engine roughness computation; system variable.  
Variation only by means of a new DAMOS specification
- U crankshaft revolution
- d... difference
- zzyl cylinder number
- SY\_ZYLZA number of cylinders

Parameter	Source-X	Source-Y	Type	Description
ANALUN	NMOT		KL	number of combustions for deactivation after detected misfire
DMXRLU			FW	variation limitation for max. reduction of the engine roughness reference values
FIAMALU			FW	increase factor for filter multiple misfire detection
FIMALU			FW	filter factor multiple misfire detection
FLUV1			FW	switch for modification 1 - calculation of running irregularity
FLUV2			FW	switch for modification 2 - calculation of engine roughness
KFAMAL	NMOT	RL	KF	map reduction factor of the engine roughness reference value at multiple misfire



Parameter	Source-X	Source-Y	Type	Description
KFAMAL1	NMOT	RL	KF	map reduction factor of the engine roughness reference value at multiple misfire
KFLURB	NMOT	RL	KF	map for engine roughness - reference base value
KFLURB1	NMOT	RL	KF	map for engine roughness - reference base value
KFLURB2	NMOT	RL	KF	map for engine roughness - reference base value
KFLURBZ	NMOT	RL	KF	map for engine roughness base value, in case of ZAS
KFLURM	NMOT	RL	KF	reference base value map for engine roughness for misfire detection
KFLURM1	NMOT	RL	KF	reference base value map for engine roughness for misfire detection
LURBRL8	RL		KL	reference value for engine roughness, vehicle speed zero
LURKH	DMRKH		KL	dmrkh-depen. engine roughness reference correction value, during cat heating
LURKTM	TMOT		KL	Tmot-dependent engine roughness reference correcting value
LURMIN1	NMOT		KL	speed dependensy of engine roughness referenz minimum value 1
LURMIN2	NMOT		KL	speed dependensy of engine roughness referenz minimum value 2
LURMIN3	NMOT		KL	speed dependensy of engine roughness referenz minimum value 3
NFLUV			FW	rpm threshold for midification - calculation of running irregularity
P_ZYL			FW	distance for calculation arithm. mean value - DMDLU
TNALU			FW	duration of test-phase after detected misfire

Variable	Source	Type	Description
B_ANALU	DMDLU	AUS	condition for deactivation after first detected misfiring
B_ANALU_M	DMDLU	LOK	monitor, cond. for deactivation after first detected misfire
B_ANALU_M2	DMDLU	LOK	monitor, cond. for deactivation after first detected misfire, 2.ECU
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_DOPZUE	NLPH	EIN	Condition double ignition
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_LL	MSF	EIN	Condition idle
B_LUERK	DMDLU	AUS	condition for misfiring detected, from DMDLU
B_LUERK_M	DMDLU	LOK	monitor, condition for misfire detected in DMDLU
B_LUERK_M2	DMDLU	LOK	monitor, condition for misfire detected in DMDLU, 2.ECU
B_LUSTOP	DMDSTP	EIN	misfire detection stop
B_MASTER		EIN	Condition MASTER-ECU
B_MDSTOP	DMDSTP	EIN	misfire detection stop
B_OPTPHERK		EIN	condition suitable engine operating state for phase detection
B_TNALU	DMDLU	AUS	condition for active test phase after detected misfiring
B_TNALU_M	DMDLU	LOK	monitor, cond. for active test phase after detected misfire
B_TNALU_M2	DMDLU	LOK	monitor, cond. for active test phase after detected misfire, 2.ECU
B_WK		EIN	condition: converter lockup clutch closed
B_WKR		EIN	condition clutch controlled
B_ZASA		EIN	ZAS load switchover is active
DMRKH	KHMD	EIN	torque reserve for catalyzer heating
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
FAMAL	DMDLU	LOK	factor for reduction of LUR value at multiple misfire, from KFFAMALU
FLURKH	DMDLU	LOK	factor for reduction of LUR value at cat-heating, from KL LURKH
FOSTAT	DMDFON	EIN	state of fuel-on/-off adaptation in actual map range
LUMS	DMDLU	DOK	engine roughness mean value for multiple misfire detection
LUMS_M	DMDLU	LOK	monitor, engine roughness mean value for multiple misfire detection
LUMS_M2	DMDLU	LOK	monitor, engine roughness mean value for multiple misfire detection, 2.ECU
LURMS	DMDLU	DOK	cranking instability reference for multiple misfire detection -> compar to lums
LURMS_M	DMDLU	LOK	monitor, cranking instability reference for multi misfire detection, signed
LURMS_M2	DMDLU	LOK	monitor, cranking instability reference for multi misfire detection, signed, 2.
LURS	DMDLU	DOK	engine roughness reference value
LURSKTM	DMDLU	AUS	tmot-dependent offset for engine roughness value dlurs, signed
LURS_M	DMDLU	LOK	monitir engine roughness reference value
LURS_M2	DMDLU	LOK	monitir engine roughness reference value, 2.ECU
LURS_MIN	DMDLU	AUS	value of LUR in case of not finished sensor wheel adaptation, value from LURMIN*
LUTS	DMDLU	AUS	engine roughness test value
LUTS1	DMDLU	AUS	engine roughness test value, cylinder or ignition 1, signed
LUTS10	DMDLU	AUS	engine roughness test value, cylinder or ignition 10, signed
LUTS11	DMDLU	AUS	engine roughness test value, cylinder or ignition 11, signed
LUTS12	DMDLU	AUS	engine roughness test value, cylinder or ignition 12, signed
LUTS2	DMDLU	AUS	engine roughness test value, cylinder or ignition 2, signed
LUTS3	DMDLU	AUS	engine roughness test value, cylinder or ignition 3, signed
LUTS4	DMDLU	AUS	engine roughness test value, cylinder or ignition 4, signed
LUTS5	DMDLU	AUS	engine roughness test value, cylinder or ignition 5, signed
LUTS6	DMDLU	AUS	engine roughness test value, cylinder or ignition 6, signed
LUTS7	DMDLU	AUS	engine roughness test value, cylinder or ignition 7, signed
LUTS8	DMDLU	AUS	engine roughness test value, cylinder or ignition 8, signed
LUTS9	DMDLU	AUS	engine roughness test value, cylinder or ignition 9, signed
LUTS_M	DMDLU	LOK	monitir engine roughness test value
LUTS_M2	DMDLU	LOK	monitor engine roughness test value, 2.ECU
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SY_2SG	PROKON	EIN	system constant 2 motronic systems
TMOT	SWADAP	EIN	Engine temperature
TSK	DMDFON	EIN	corrected segment duration
VFZG	SWADAP	EIN	vehicle speed (km/h)
ZZYL	GGDPG	EIN	SW-cylinder counter



## FW DMDLU 4.90 Fixed Values

Parameter	Value	Description
DMXRLU		variation limitation for max. reduction of the engine roughness reference values
FIAMALU		increase factor for filter multiple misfire detection
FIMALU		filter factor multiple misfire detection
FLUV1		switch for modification 1 - calculation of running irregularity
FLUV2		switch for modification 2 - calculation of engine roughness
NFLUV		rpm threshold for midification - calculation of running irregularity
P_ZYL		distance for calculation arithm. mean value - DMDLU
TNALU		duration of test-phase after detected misfire

## FB DMDLU 4.90 Detailed description of function

### 1. Misfire detection

The following operating steps are performed for each measured segment, corrected by the fuel-on adaptation  
The data are processed asynchronously to the combustion cycle, after several segment data have been collected.

#### 1.1 Calculation of the engine roughness luts(n), Luts1(n), luts2(n), ... lutsSY\_ZYLZA(n)

The engine roughness is calculated in general according to the following formula:  
lut(n) is related to 1 crankshaft revolution (physical unit: (rev./s)<sup>2</sup>). The segment duration (physical unit: us)  
is therefore to be multiplied by zylza/2 each.

$$luts(n) = \frac{[tsk(n+1) - tsk(n)] - \text{compensation time}}{tsk(n)^3}$$

The calculated engine roughness value is also stored cylinder specific.

During ZAS-mode (B\_zasa=1) the engine roughness is calculated as follows:

$$luts(n) = \frac{[tsk(n+1) - tsk(n-1)] - (2 * \text{compensation time})}{tsk(n)^3}$$

The luts-values for the cylinders cut-off are set to 0.

#### 1.1.1 Calculation of compensation time according to the median procedure

For FLUV=1 and nmot<NFLUV the dynamic compensation time is calculated according to the median procedure.  
Median is defined as the mean value of a data sequence (based on the values).  
Medians are used for statistical evaluations, in order to eliminate outliers.  
The engine roughness must be calculated continuously for each segment. For processing, six measuring values are required.  
At first, 5 differences Dts1 to Dts5 are constructed of 2 consecutive segments.  
Calculated is the engine roughness value, which is related to the segment tsk(n).

$$\begin{aligned} Dts1 &= [tsk(n-1) - tsk(n-3)] / 2 \\ Dts2 &= tsk(n) - tsk(n-1) \\ Dts3 &= tsk(n+1) - tsk(n) \\ Dts4 &= tsk(n+2) - tsk(n+1) \\ Dts5 &= tsk(n+3) - tsk(n+2) \end{aligned}$$

The first differential value Dts corresponds to the mean value of two consecutive differences. By applying this procedure,  
it is also possible to detect misfire rates > 50%.

The 5 differences Dts1 to Dts5 are sorted, based on their value and then converted into the values DGts1 to DGts5.  
( DGts1 corresponds to the highest value).

$$\begin{aligned} DGts1 &= \text{highest value of Dts1 to Dts5} \\ DGts2 &= \text{second highest value of Dts1 to Dts5} \\ DGts3 &= \text{third highest value of Dts1 to Dts5} \\ DGts4 &= \text{fourth highest value of Dts1 to Dts5} \\ DGts5 &= \text{fifth highest value of Dts1 to Dts5} \end{aligned}$$

The engine roughness is calculated based on:

$$\text{compensation time} = DGts3 \quad \rightarrow \quad luts(n) = \frac{Dts3 - DGts3}{tsk(n)^3}$$

#### 1.1.2 Calculation of compensation time according to the arithmetical meanvalue

For FLUV1=0 and FLUV2=1 or for FLUV1=1 and nmot>NFLUV the compensation time is calculated according to the arithmetical  
meanvalue.

$$Dts6 = [tsk(n-p\_zyl+SY\_ZYLZA) - tsk(n-p\_zyl)] / SY\_ZYLZA; \quad p\_zyl = ((SY\_ZYLZA)/2)-1$$

The engine roughness is calculated based on:

$$\text{compensation time} = Dts6 \quad \rightarrow \quad luts(n) = \frac{Dts3 - Dts6}{tsk(n)^3}$$

#### 1.1.3 Quantization parameter FLUQ

The parameter SY\_FLUQ can be chosen, so that the optimum quantization of the engine roughness values are ensured.  
The choice of SY\_FLUQ = LUEXP (systemconstant variable)  
results with tsquant = TINCT (system constant variable)  
in a quantisation of luquant = LUQUANT (system constant variable)



1.1.4 Overview of the calculations of the compensation time:

FLUV1	FLUV2	n	calculation of compensation time
1	x	n < NFLUV	median
1	x	n > NFLUV	arithmetical mean-value
0	1	x	arithmetical mean-value

x: means not relevant here.

1.2 Detecting of multiple misfiring supplementary information lums(n)

If several cylinders are misfiring (e.g., also alternating one combustion/one misfire event), the calculated engine roughness values may be that low so that the reference value is not exceeded during misfiring and therefore, misfiring would not be detected. Based on this fact, the periodicity of the engine roughness value is used as additional information during multiple misfiring.

The engine roughness values are filtered based on the following equation:

$$lums(n) = (1 - FIMALU) * lums(n-1) + FIMALU * FIAMALU * ( | luts(n-1) - 0.5 * luts(n-2) - 0.5 * luts(n) | )$$

During deactivation at specific operating conditions (B\_mdstop=1, B\_lustop=1, see 1.5), the lums-calculation is going on, but starts after the deactivation with the value 0. Only in case of rough road detection using statistic lums is not initialized after disabling by B\_swe\_s.

During deactivation after a detected misfire (see 1.6) the filtering resp. the lums-calculation is stopped.

If both deactivations are valid simultaneously, B\_analu possesses the higher priority, e.g. lums is stopped and not set to 0.

In case of ZAS-mode (B\_zasa=1) lums is set to 0.

1.3 Calculation of the engine roughness reference value:

The engine roughness value lurs consists of a base value (KFLURB) and a coolant-temperature-dependent correction value LURKTM. The base value is determined by the map KFLURB for B\_wk=0, by the map KFLURB1 for B\_wk=1 and by the map KFLURB2 for B\_wkr=1. In case of ZAS-mode (B\_zasa=1) the base value is determined by the map KFLURBZ independant of B\_wk and B\_wkr. In case of idle an vehicle speed = 0 (and E\_vfz=0) the base value is determined by the load dependant characteristic line LURBRL8 (independant of B\_wk, B\_wkr, B\_zasa).

Furthermore, the correction value lursktm, determined by a characteristic line LURKTM, is added on the base value.

During cat-heating for better detection during the first 1000 crankshaft rev. the threshold lurs can be decreased by the factor flurkh. flurkh is calculated from the characteristic line LURKH, dependant on the difference torque dmrkh used for cat-heating.

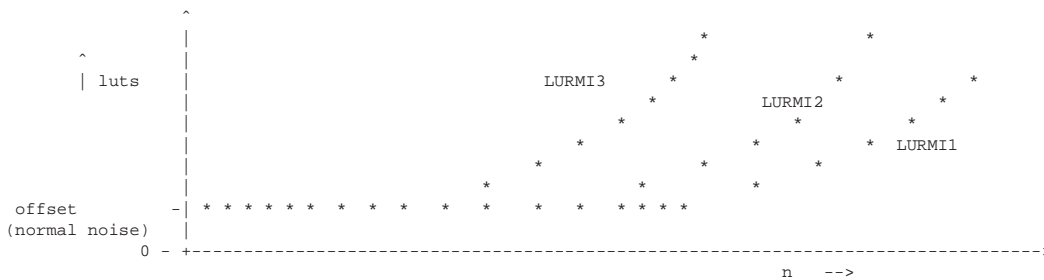
Offset to lurs of LURMIN\* in case of not yet performed resp. not completed adaptation. LURMIN1..3 are characteristic lines over the speed.

If the adaptation is not yet completed to the reference value lurs is added the minimum value LURMIN3. LURMIN3 must hold out the inaccuracy of the segment duration. If the adaptation is completed in a dominant range the reference value is increased by the value LURMIN2. LURMIN2 must hold out the speed and load dependeces. If the adaptation is completed in a speed-dominant range of the actual speed the reference value lurs is increased by the minimum value LURMIN1. LURMIN1 must hold out the load-dependance of the actual speed-range. If the adaptation is completed in the actual range and all values of the actual speed-range are plausible there is no further offset to lurs.

The offset to lurs for the actual range depends on fostat (see %DMDFON):

- fostat = 3: offset LURMIN3
- fostat = 2: offset LURMIN2
- fostat = 1: offset LURMIN1
- fostat = 0: no further offset of lurs

different characteristic lines of LURMI\*::



The new reference value lurs(i) is compared with the old reference value lurs(i-2). A change towards smaller reference values is limited by the variation constant DMXRLU. After 2 camshaft-rotations lurs can be decreased of DMXRLU.



#### 1.4 Determination if misfiring

Misfire detection is performed by comparing the engine roughness reference  $lurs(i)$  with the engine roughness value  $luts(n)$ . If  $luts > lurs$ , then a single misfire is detected. (exception during deactivation of  $B\_analu=1$  (see 1.6) and  $B\_mdstop=1$  and  $B\_lustop = 1$  (see %DMDSTP)).

In case  $lums(n)$  exceeds the value  $lurms(i)$ , then  $lurs$  is reduced by a  $n$ -/tl-dependant factor  $famal$  in case of completed adaptation ( $fostat=0$  or  $fostat = 1$ ).

The factor  $famal$  is got of a map over  $nmot$  and  $rl$  (KFAMAL in case of  $B\_wk=0$  and KFAMAL1 in case of  $B\_wk=1$ ). The threshold  $lurms$  results of a base value  $KFLURM$  and a coolant-temperature dependant offset  $lursktm$  (LURKTM). Changes towards smaller reference values are limited by the variation constant  $DMXRLU$ , see  $lurs$  (over 2 camshaft rotations).

$lum > lurms \Rightarrow lurs = lurs * famal[0..1] ; \text{ if } fostat = 0 \text{ V } fostat = 1$

#### 1.5 Deactivation in case of abnormal conditions

In case of rough road, high load- and speed-changes, engine-torque jumps, ... the misfire detection is deactivated to provide misdetections,  $B\_mdstop=1$  or  $B\_lustop=1$ .

The calculation of  $luts$  and  $lums$  goes on, so that the rough-road-detection with satistical methods (%DSWES) is able to go on. After the deactivation the calculation of  $luts$  and  $lums$  starts at 0 so there will be no 'past time information' in the filters.

In case of  $B\_mdstop=1$  or  $B\_lustop=1$  the bit  $B\_luerk$  is not set, independant from the comparson of  $luts > lurs$ .

#### 1.6 Deactivation after detected misfiring:

If misfiring is detected within the previous segment, then misfire detection is deactivated during the next ANALUN segments and  $B\_analu = 1$ . ANALUN is a characteristic line over speed. After this deactivation, a test phase with the duration of about  $> TNALU$  segments takes place and  $B\_tnalu=1$ .

If an additional misfire is detected during this test phase, then no further deactivation via ANALUN is carried out and the test phase remains active ( $B\_tnalu=1$ ). The test phase is completed after  $TNALU$  segments after the last detected misfire. If  $ANALUN = 0$ , then no deactivation after detected misfiring takes place.

By applying this measure, misdetection due to post-oscillation (which may be triggered by single misfiring) is suppressed. Continuous misfiring, however, is detected reliably.

The calculation and monitoring of  $luts$  is going on. Only the detection of misfire is suppressed. ( $B\_luerk=0$  even if  $luts>lurs$ ). The  $lums$ -calculation is stopped during  $B\_analu=1$ .

A deactivation also takes place if misfire is detected in %DMDDL and  $B\_analu = 1$  is set.

### APP DMDLU 4.90 Application hint

#### 1) Monitor function

For the application of the misfire detection, it is necessary, to synchronously monitor the segment time, the  $luts$ -value and several status bits. This is ensured with the monitor function.

For the description of the monitor-function and a list of related values see %DMDUE.

#### 2) SY\_FLUQ is a system variable, a variation is only possible by means of a new DAMOS specification.

#### 3) Function deactivation:

For application purposes the misfire detection can be deactivated by setting  $NMXALU = 0$  rpm in %DMDSTP.

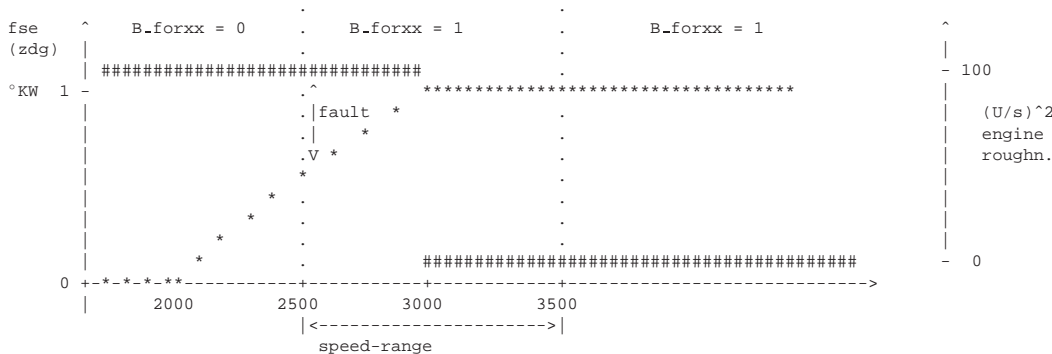
#### 4) Sensitivity of misfire detection:

LURMIN3: corresponds to the maximum possible faults (mechanical sensor wheel tolerances and torsional vibrations)  
e.g. +- 1,2°crankshaft

LURMIN2: corresponds to the max. possible faults over the speed (speed dependance of adaptation values)  
e.g. +- 0,15°crankshaft

LURMIN1: corresponds to the max. possible fault over the load (load dependance of adaptation values in each speed range)  
e.g. +- 0,1°crankshaft

LURMIN\*-expansion to neighbour ranges:



\*: fse value for ts-correction  
#: LURMIN\*-offset

#### 5) B\_analu and B\_tnalu:

$B\_analu$  and  $B\_tnalu$  of %DMDLU and %DMDDL are stored in one physical RAM-cell. So it is possible that both functions influence the other function and  $B\_analu$  and  $B\_tnalu$  are simultaneous in- and output.



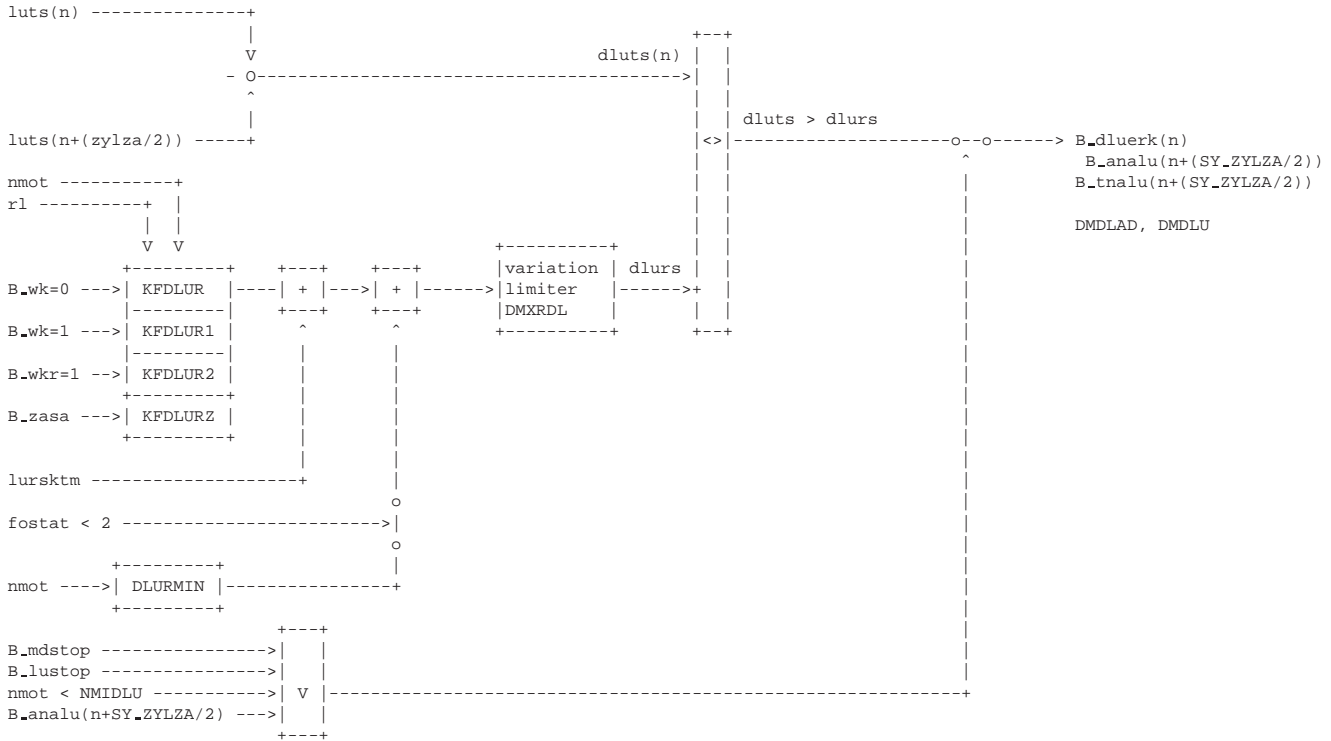
6) short test of function DMDDL

For a short validation of the function the engine roughness values luts\_ap can be compared in normal and in misfire mode (e. g. Mode 6 at ZAG). In areas of mean speed and load the luts\_ap values in case of misfire must be visible higher than in case of normal combustions.

## DMDDL 7.50 Diagnostic routine Misfire Detection, forming the diff. for irregular running

### FDEF DMDDL 7.50 Function definition

Overview DMDDL:



B\_analu, B\_tnalu is triggered or retriggered by luts or by dluts.

The whole misfire detection can be locked with the Eurocodeword CDMD.  
For B\_cdmd=0 the function DMDDL is locked, B\_dluerk, B\_analu and B\_tnalu are set to 0.  
For B\_cdmd=1 the function DMDDL is active.

This function is only active for engines with even cylinder numbers.  
For SY\_ZYLZA 0 odd B\_dluerk is set to 0.

In case of 2 ecu's (SY\_2SG = 1) the function %DMDDL is deactivated in the Master-ecu (B\_master = 1).

### ABK DMDDL 7.50 Abbreviations

Indices and reference points used:

(n)	Crankshaft segments		
luts(n)	Imbalance test variable, updating in synchro		
dluts(n)	Differential imbalance, updating in synchro		
dlurs	Differential imbalance reference value		
DMDLAD	logical and temporary combination of the results from different functions for misfire detection		
DMDLU	misfire detection with engine roughness		
DMDSTP	stop conditions for misfire detection		
SY_FLUQ	Quantization factor for imbalance calculation; system variable, change only possible via new DAMOS specification.		
U	Crankshaft revolution		
d...	Differential		
SY_ZYLZA	Number of cylinders		

Parameter	Source-X	Source-Y	Type	Description
DLURMIN	NMOT		KL	speed dependency of engine roughness referenz minimum value 1
DMXRDL			FW	variation limit for max. reduction of engine roughness reference value dlur
KFDLUR	NMOT	RL	KF	map engine roughness difference dluts referenz value
KFDLUR1	NMOT	RL	KF	map engine roughness difference dluts referenz value
KFDLUR2	NMOT	RL	KF	map engine roughness difference dluts referenz value
KFDLURZ	NMOT	RL	KF	map engine roughness difference dluts referenz value at ZAS (cylinder cut-off)
NMIDLU			FW	min. engine speed for deactivating misfire detection DMDDL



Variable	Source	Type	Description
B_ANALU	DMDLU	EIN	condition for deactivation after first detected misfiring
B_ANALU_M	DMDDLU	LOK	monitor, cond. for deactivation after first detected misfire
B_ANALU_M2	DMDDLU	LOK	monitor, cond. for deactivation after first detected misfire, 2.ECU
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_DLUERK	DMDDLU	AUS	condition for misfiring detected, from DMDDLU
B_DLUERK_M	DMDDLU	LOK	monitor, misfire detected in DMDDLU
B_DLUER_M2	DMDDLU	LOK	monitor, misfire detected in DMDDLU, 2.ECU
B_LUSTOP	DMDSTP	EIN	misfire detection stop
B_MASTER		EIN	Condition MASTER-ECU
B_MDSTOP	DMDSTP	EIN	misfire detection stop
B_WK		EIN	condition: converter lockup clutch closed
B_WKR		EIN	condition clutch controlled
B_ZASA		EIN	ZAS load switchover is active
DLURS	DMDDLU	LOK	engine roughness difference reference value
DLURS_M	DMDDLU	LOK	monitr, engine roughness difference reference value, signed, delayed output
DLURS_M2	DMDDLU	LOK	monitr, engine roughness difference reference value, signed, delayed out, 2.ECU
DLUTS	DMDDLU	LOK	difference engine roughness test value
DLUTS1	DMDDLU	AUS	difference engine roughness test value
DLUTS10	DMDDLU	AUS	difference engine roughness test value
DLUTS11	DMDDLU	AUS	difference engine roughness test value
DLUTS12	DMDDLU	AUS	difference engine roughness test value
DLUTS2	DMDDLU	AUS	difference engine roughness test value
DLUTS3	DMDDLU	AUS	difference engine roughness test value
DLUTS4	DMDDLU	AUS	difference engine roughness test value
DLUTS5	DMDDLU	AUS	difference engine roughness test value
DLUTS6	DMDDLU	AUS	difference engine roughness test value
DLUTS7	DMDDLU	AUS	difference engine roughness test value
DLUTS8	DMDDLU	AUS	difference engine roughness test value
DLUTS9	DMDDLU	AUS	difference engine roughness test value
DLUTS_M	DMDDLU	LOK	monitor, difference engine roughness test value, signed, delayed output
DLUTS_M2	DMDDLU	LOK	monitor, difference engine roughness test value, signed, delayed output, 2.ECU
FOSTAT	DMDFON	EIN	state of fuel-on/-off adaptation in actual map range
LURSKTM	DMDLU	EIN	tmot-dependent offset for engine roughness value dlurs, signed
LUTS	DMDLU	EIN	engine roughness test value
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SY_2SG	PROKON	EIN	system constant 2 motronic systems

### FW DMDDLU 7.50 Fixed Values

Parameter	Value	Description
DMXRDL		variation limit for max. reduction of engine roughness reference value dlur
NMIDL		min. engine speed for deactivating misfire detection DMDDLU





## FB DMDDL 7.50 Detailed description of function

### 1. Introduction:

The function described below allows the recognition of single and permanent misfires, and of non-symmetrical multiple misfires.

The quality of detection is independent of sensor wheel accuracy (crankshaft-synchronous segment time fluctuations), so symmetrical multiple misfires (also generating crankshaft-synchronous segment time fluctuations) cannot be recognized.

### 2. Calculation of differential imbalance dluts(n):

The imbalance values luts(n) and luts(n+(zylza/2)) belonging to the same crankshaft segment are subtracted.

$$dluts(n) = luts(n) - luts(n+(zylza/2))$$

If one of the two cylinders misfires, the differential dluts increases.

dluts is compared with the threshold value dlurs. dlurs is calculated relative to load and engine speed (8x8) via the map.

If the differential dluts(n) exceeds the threshold value dlurs, then combustion misfires occur.

If both cylinders 1 crankshaft revolution apart misfire, the differential dluts is approximated to 0 as in normal operation.

In case of ZAS-mode the engine roughness luts of the non-fired cylinders is equal to 0. So the dlut-calculation doesn't differ.

### 3. Calculation of reference value dlurs:

A base value is calculated from the load- and rpm-dependent map KFDLUR for B\_wk=0, KFDLUR1 for B\_wk=1 and KFDLUR2 for B\_wkr=1.

In case of ZAS-mode the map KFDLURZ is used independent of B\_wk and B\_wkr.

To this base value a tmot-dependent offset lursktm (from %DMDLU) is added.

Depending on the adaptation status (fostat >= 2) an offset will be added to the reference value.

Negative variations in the reference values are limited by the variation limiter DMXRDL (corresponds to DMXRLU, see %DMDLU),

i. e.  $dlurs(i-2) - dlurs(i) \leq DMXRDL$ .

### 4. Masking:

As with the basic functions (see %DMDUE), %DMDDL must also be masked under the same critical operating conditions:

Masking at B\_mdstop, B\_lustop

Masking at B\_analu

B\_analu can be triggered here either by dluts misfire detection or by luts misfire detection.

The ANALUN masking is deactivated with TNALU in the event of permanent misfires. (see %DMDLU)

Also the function DMDDL is masked for speed below the speed-dependant threshold NMIDLU.

In lower rpm-ranges instabil luts values can occur and will be probably subtracted or added by the dlut calculation.

Während einer der o.g. Ausblendungen wird die Differenzlaufunruhe dluts weiter berechnnet, bei dluts > dlurs wird jedoch nicht auf Aussetzer erkannt.

## APP DMDDL 7.50 Application hint

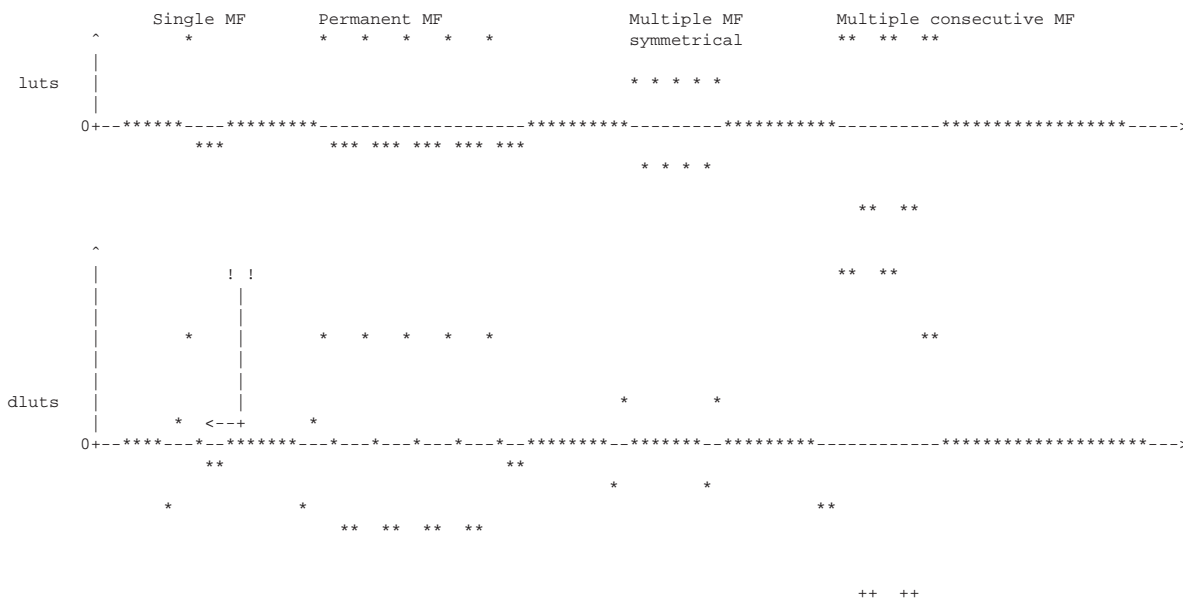
1. A PC simulation program (dmdsim.exe) is provided for the dluts calculation. (Off-line application)

2. For KFDLUR the values of KFLURB can be used in the 1st stage. Usually the values for the corresponding operating points should not overlap. However, the two maps can be used to adjust the sensitivity of the various methods to specific ranges.

3. To be noted in the application of KFDLUR:

Typical dluts curves:

e.g. 4-cylinder engine:

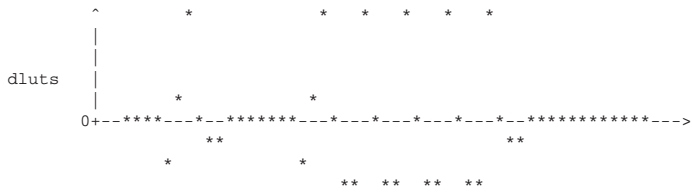
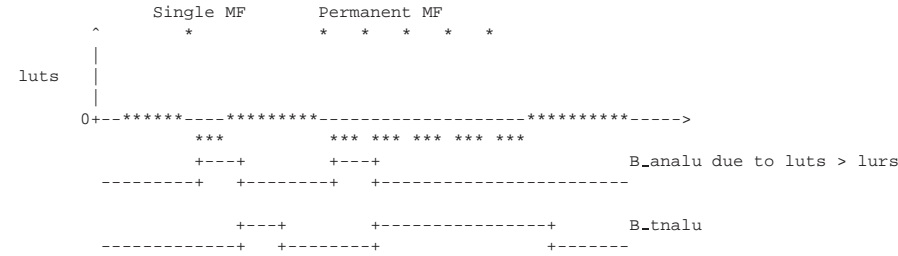


In the application of dlurs it must be noted that prior to the actual misfire, a smaller positive dluts value may occur. Therefore, dlurs must not be set to too small a value.

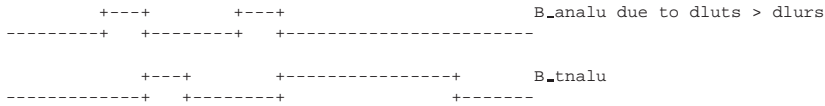


4. Peculiarities in B\_analu-masking due to the retroactive dluts calculation:

e.g. 4-cylinder engine: (prerequisite regarding luts: ZAD has stabilized)



If  $luts \leq lurs$  (luts has detected no misfire):



dluts(n) requires luts(n+2) for its calculation. (e.g. 4-cyl. engine). In the ECU, dluts(n) can thus only be calculated 2 ignitions later in retrospect. The correct arrangement (resetting by 2 ignitions) is produced via the monitor drum.

If B\_analu due to  $luts > lurs$  is already set at the time of the dluts(n) calculation, then no B\_analu is set with dluts.

Triggering of B\_analu due to  $dluts > dlurs$  can only occur 2 ignitions later (4-cyl. engine) because of the delayed calculation. B\_analu, B\_tnalu are thus shifted by 2 ignitions.

Because of the typical luts curve (see above, negative dluts) after a misfire, this is not critical.

5. DMXRDL should cut in slower than DMXRLU, i.e.  $\rightarrow DMXRLU > DMXRDL$ . Under dynamics (negative load change) the interference of luts may accumulate due to summation, which is why "mis-detections" can occur if cut-in is too fast. (Remark: Genuine misfires frequently occur here, but these should not be detected!)

DMXRDL should be applied especially slowly in vehicles with manual switch or turbocharged engines.

6. Re. monitor function:

For the application of msifire detection it is necessary that some values like dluts, dlurs, etc. are synchronized. This is ensured in the monitor-function. For the description of the monitor-function and a list of related values see %DMDUE.

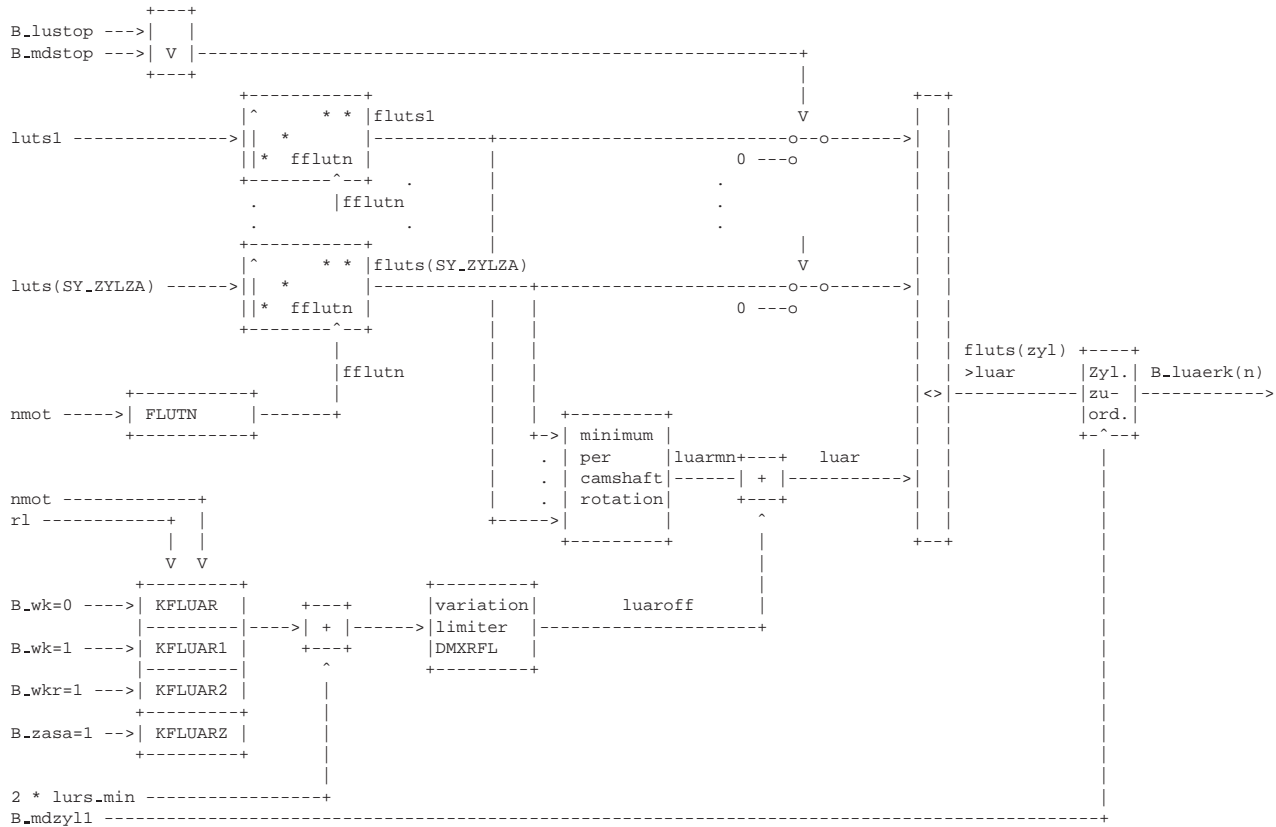
7. short test of function DMDDL

For a short test of the function the difference-engine-roughness value dluts can be compared in normal combustion mode and in misfire mode (e. g. Mode 6 at ZAG). In areas of mean speed and load a clear difference of dluts between normal and misfire mode must be visible.

## DMDLUA 4.30 Diagnostic routine Misfire Detection irregular running spacing

### FDEF DMDLUA 4.30 Function definition

Overview DMDLUA:



The entire functions for misfire detection can be locked with the Eurocodeword CDMD.  
For B\_cdmd=0 the function DMDLUA is locked and B\_luaerk is set to 0.  
For B\_cdmd=1 the function DMDLUA is active.

In case of 2 ecu's (SY\_2SG = 1) the function %DMDLUA is deactivated in the Master-ecu (B\_master = 1).

### ABK DMDLUA 4.30 Abbreviations

- (i) camshaft revolutions; NW-Umdr.
- (n) crankshaft segments
- zzyl cylinder number
- SY\_ZYLZA number of cylinders

Parameter	Source-X	Source-Y	Type	Description
DMXRFL			FW	limitation for max. reduction of the filter engine roughness reference values
FLUTN	NMOT		KL	filter factor running irregularity
KFLUAR	NMOT	RL	KF	map for engine roughness distance reference value
KFLUAR1	NMOT	RL	KF	map for engine roughness distance reference value
KFLUAR2	NMOT	RL	KF	map for engine roughness distance reference value
KFLUARZ	NMOT	RL	KF	map for engine roughness distance reference value at ZAS (cylinder cut-off)

Variable	Source	Type	Description
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_LUAERK	DMDLUA	AUS	condition for misfiring detected, with engine roughness distance, from DMDLUA
B_LUAERK_M	DMDLUA	LOK	monitor, misfire detected in DMDLUA
B_LUAER_M2	DMDLUA	LOK	monitor, misfire detected in DMDLUA, 2.ECU
B_LUSTOP	DMDSTP	EIN	misfire detection stop
B_MASTER		EIN	Condition MASTER-ECU
B_MDSTOP	DMDSTP	EIN	misfire detection stop
B_MDZYL1	DMDLUA	LOK	con. for cylinder ident. (f.t>TALUST),LU-calculation disabled (f.t<TALUST)
B_WK		EIN	condition: converter lockup clutch closed
B_WKR		EIN	condition clutch controlled
B_ZASA		EIN	ZAS load switchover is active
FFLUTN	DMDLUA	LOK	filter facot over speed for filtering the engine roughness
FLUTS1	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 1, signed
FLUTS10	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 10, signed
FLUTS11	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 11, signed
FLUTS12	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 12, signed
FLUTS2	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 2, signed
FLUTS3	DMDLUA	LOK	filter engine roughness test value, cylinder or inition 3, signed
FLUTS4	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 4, signed
FLUTS5	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 5, signed
FLUTS6	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 6, signed
FLUTS7	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 7, signed



Variable	Source	Type	Description
FLUTS8	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 8, signed
FLUTS9	DMDLUA	LOK	filter engine roughness test value, cylinder or ignition 9, signed
FLUTS_M	DMDLUA	LOK	monitr, filtered engine roughness test value, signed, delayed output
FLUTS_M2	DMDLUA	LOK	monitr, filtered engine roughness test value, signed, delayed output, 2.ECU
LUAR	DMDLUA	DOK	engine roughness distance reference value
LUARMN	DMDLUA	LOK	engine roughness distance reference value minimum
LUAROFF	DMDLUA	LOK	engine roughness distance reference value offset
LUAR_M	DMDLUA	LOK	monitor, engine roughness distance reference value, delayed output
LUAR_M2	DMDLUA	LOK	monitor, engine roughness distance reference value, delayed output, 2.ECU
LURS_MIN	DMDLU	EIN	value of LUR in case of not finished sensor wheel adaptation, value from LURMIN*
LUTS1	DMDLU	EIN	engine roughness test value, cylinder or ignition 1, signed
LUTS10	DMDLU	EIN	engine roughness test value, cylinder or ignition 10, signed
LUTS11	DMDLU	EIN	engine roughness test value, cylinder or ignition 11, signed
LUTS12	DMDLU	EIN	engine roughness test value, cylinder or ignition 12, signed
LUTS2	DMDLU	EIN	engine roughness test value, cylinder or ignition 2, signed
LUTS3	DMDLU	EIN	engine roughness test value, cylinder or ignition 3, signed
LUTS4	DMDLU	EIN	engine roughness test value, cylinder or ignition 4, signed
LUTS5	DMDLU	EIN	engine roughness test value, cylinder or ignition 5, signed
LUTS6	DMDLU	EIN	engine roughness test value, cylinder or ignition 6, signed
LUTS7	DMDLU	EIN	engine roughness test value, cylinder or ignition 7, signed
LUTS8	DMDLU	EIN	engine roughness test value, cylinder or ignition 8, signed
LUTS9	DMDLU	EIN	engine roughness test value, cylinder or ignition 9, signed
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SY_2SG	PROKON	EIN	system constant 2 motronic systems

### FW DMDLUA 4.30 Fixed Values

Parameter	Value	Description
DMXRFL		limitation for max. reduction of the filter engine roughness reference values

### FB DMDLUA 4.30 Detailed description of function

#### 1. Introduction

The described function as follows permits the detection of continuous misfiring in one or more cylinders. For this the cylinder individuell engine roughness luts(cyl) are filtered by a recursive low pass filter (fluts(cyl)) and are compared with an adapting threshold luar.

The detection ratio is nearly independant of the number of misfiring cylinders.

The detection ratio is dependant of the adaptation status (e.g. of the fuel-on adaptation).

Single misfire ( < 2 - 10 misfire per cylinder, according to fflutn) cannot be detected.

#### 2. Calculation of fluts(cyl)

The engine roughness luts(cyl)(i) are filtered cylinder individuell. The time constant ffluts is determined by a characteristic line FLUTN over speed.

$$\text{fluts}(zyl)(i) = (1 - \text{fflutn}) * \text{fluts}(zyl)(i-1) + \text{fflutn} * \text{luts}(zyl)(i)$$

During masking of misfire detection (B\_mdstop=1, B\_lustop=1) the filtered values fluts(cyl) are set to 0. After the masking (B\_md/lustop: 1 -> 0) the filtering begins at 0. Previous values are not considered.

In case of ZAS-mode (B\_zasa=1) the luts values of the cut-off cylinders are set to 0 so the corresponding fluts values are also 0 and the fluts calculation hasn't to be changed.

#### 3. Calculation of reference value luar

the reference value luar consists of a adapting minimum luarmin and an additive offset luaroff. The offset luaroff is calculated from the speed and load dependant map KFLUAR in case of B\_wk=0, of KFLUAR1 for B\_wk=1 and of KFLUAR2 for B\_wkr=1. In case of ZAS-mode luaroff is calculated from the map KFLUARZ independant of B\_wk and B\_wkr.

If the adaptation is not yet completed the offset value luaroff is increased by twice the value lurmin (from LURMIN\*, see %DMDLU).

Negative variations in the reference value are limited by the variation limiter DMXRFL (corresponding to DMXRFL in %DMDLU), i. e. luar(i-2) - luar(i) <= DMXRFL.

The minimum value luarmin is the minimum of all filtered values fluts(cyl) during one camshaft revolution.

#### 4. Determination if continuous misfire

Continuous misfire is determined with a comparison of the filtered fluts(cyl) and the referenc value luar. If fluts(cyl) exceeds the threshold luar misfire is detected in the corresponding cylinder.

The bit B\_luaerk(n) is set at the corresponding ignition.

### APP DMDLUA 4.30 Application hint

#### 1. Monitor-function

For application of misfire detection it is necessary to synchronously monitor some variables and several status bits. This is ensured with the monitor function.

For the description of the monitor-function and a list of the related values see %DMDUE.

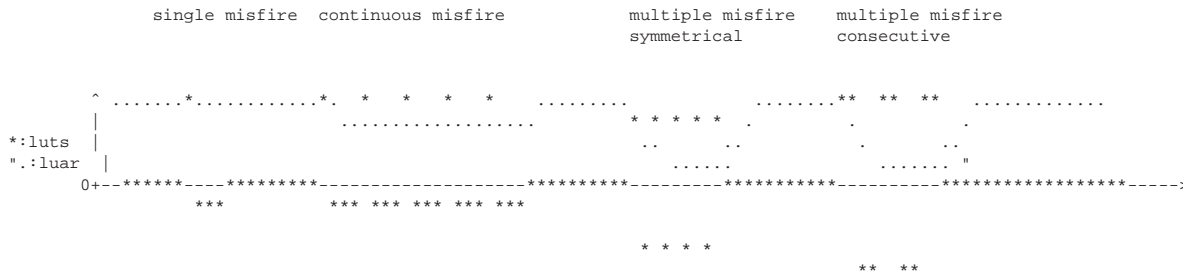


2. physical background:

During normal and misfire conditions the total amount of the luts values during one camshaft revolution is nearly equal to 0. During misfire in cylinder no. one e.g. the luts1 increases whereas the remaining luts2..lutsSY.ZYLZA decrease respectively become negative. The total amount of all luts values over one camshaft revolution is 0. This is also valid for misfire in multiple cylinders.

The distance between misfiring cylinder (positive luts) and firing cylinders (negative luts) is nearly the same and independant of the number of misfiring and firing cylinders.

Example 4-cylinder-engine:



3. Standard application values:

DMXRFL: 2 - 4 \* DMXRLU, dependant on fflutn, luar must be slower than fluts(cyl) to avoid misdetection during dynamic conditions.

FLUTN: 0.4 (lower rpm) ... 0.1 (higher rpm, > 4000/min)

KFLUAR: the values of KFLURN can be used in the 1st stage (see %DMDLU)

4. Difference between DMDLUA and lums (see %DMDLU)

lums serves espacilly for detection of symmetrical misfire. In this case lums shows advanteges at high cylinder engines. For 4-cyl.-engines DMDLUA ca be sufficient for detection of multiple misfire. So this function shall be applicated first and in case of non sufficient detection ratio lums shall be activated.

5. Improvement with DMDLUA:

- in case of poor and rough idling detection of continuous misfire can be protected with the function DMDLUA
- similar in case of unsystematical speed v variations (unsymmetrical distributed over all cylinders) during cold starting the misfire detection for continuous misfire can be protected. For this lurktm (see %DMDLU) isn't considered.
- DMDLUA is still now nonsensitive for post-oscillations. For that ANALU/TNALU aren't considered. Post-oscillations vary unsymmetrical over all cylinders (observe flutn, choose smaller -> 0,1)  
It must be tested if post-oscillations appear camshaft synchron. In this case the filters may run away. If the post-oscillations are not camshaft synchron they may disappear after filtering.

6. short test of function DMDLUA

For a short validation of the function the filtered engineroughness values fluts1..SY.ZYLZA can be compared in normal and in misfire mode (e. g. Mode 6 at ZAG). In areas of mean speed and load a high increasing of the fluts values of the misfiring cylinder must be visible.

## DMDSTP 9.90 Diagnostic of misfire detection : Stop conditions

### FDEF DMDSTP 9.90 Function definition

1. Overview : Function structure

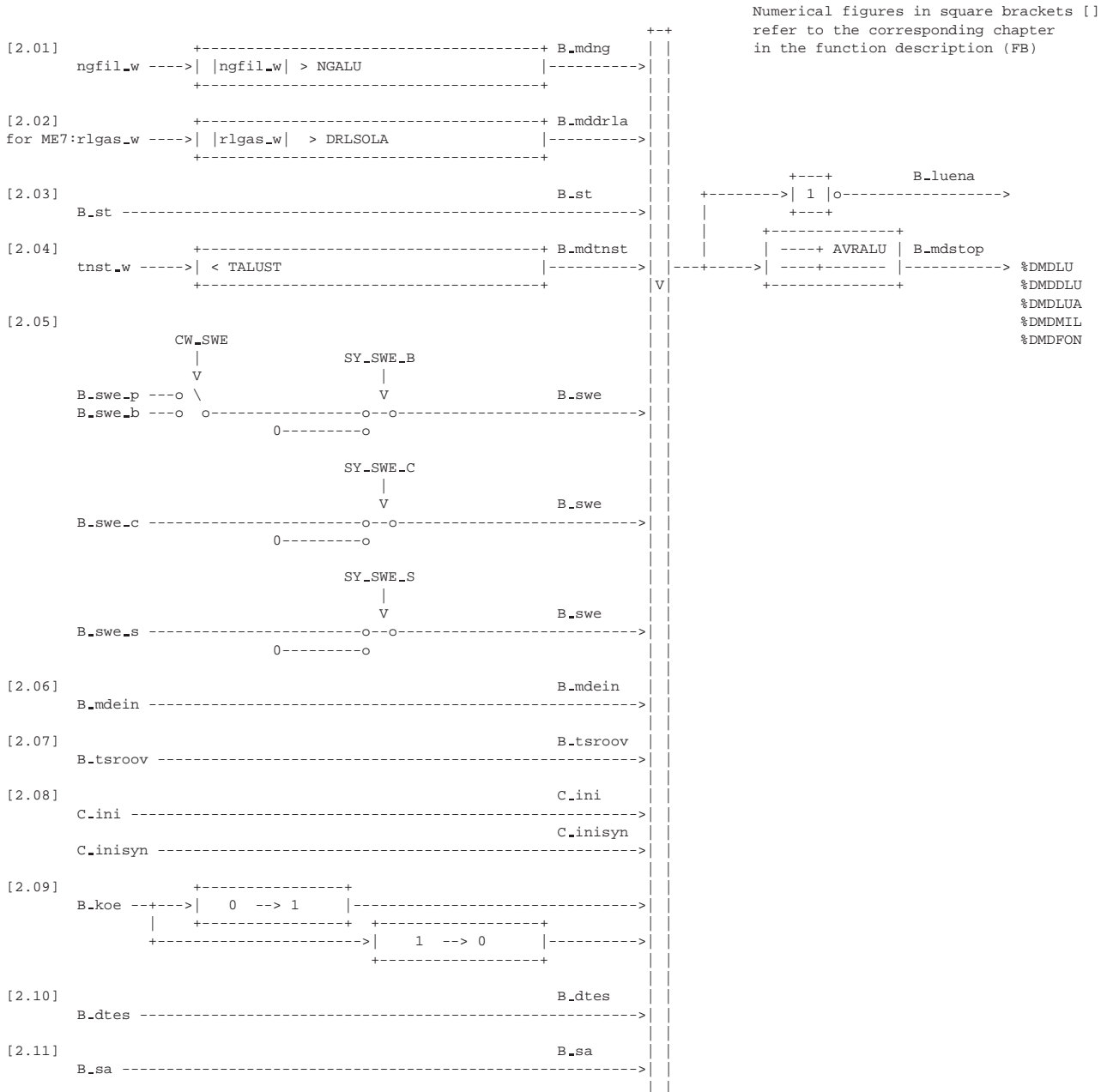
In the %DMDSTP all deactivation conditions for the functions of the misfire detection with regard to engine roughness (%DMDLU, %DMDLU, %DMDLUA and %DMDMIL) as well as the function of the fuel-on and fuel-off adaptation (%DMDFON) are evaluated. According to the following block diagram the %DMDSTP generates 4 different stop bits (B\_mdstop, B\_lustop, B\_fonstp and B\_fofstp), which each have a blocking effect on the mentioned function blocks:

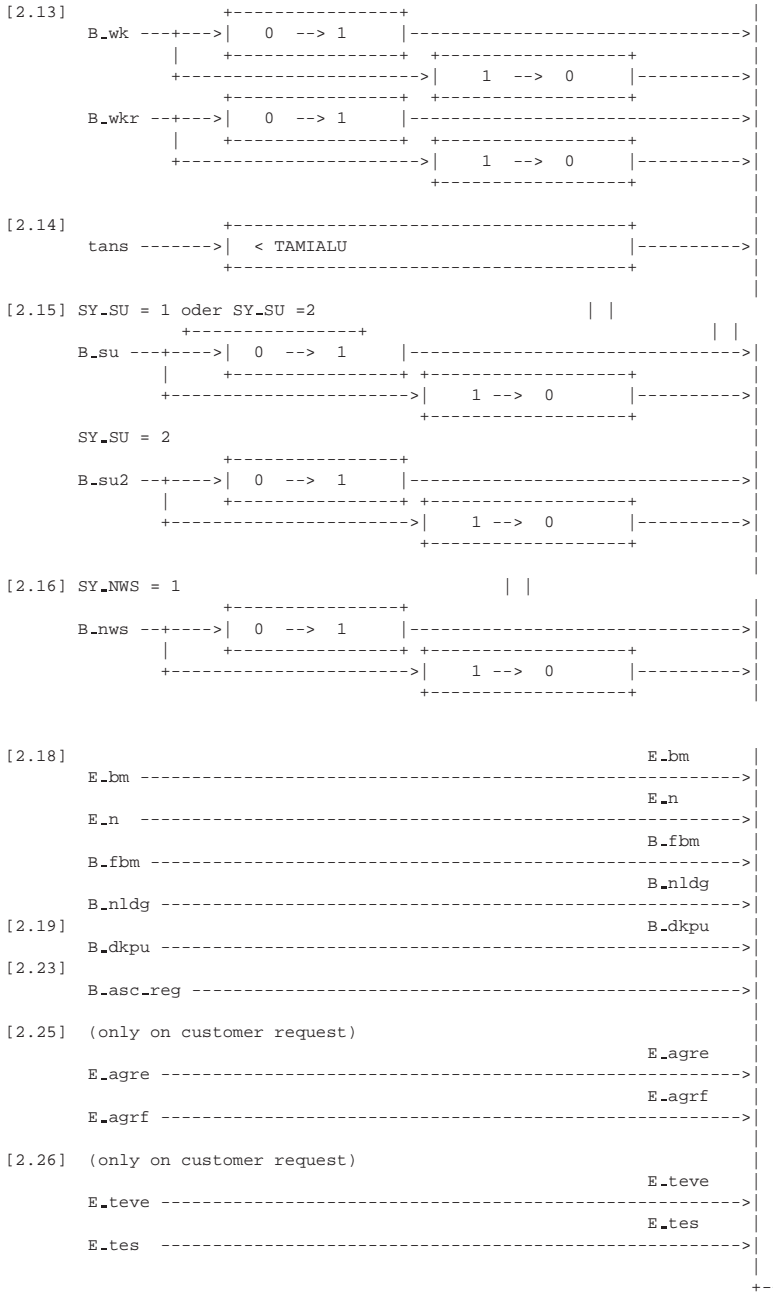


Via the Euro switch CDMD it is possible to switch off the functions of the misfire detection.  
If B\_cdmd=0 the function %DMDSTP is blocked.  
If B\_cdmd=1 the function %DMDSTP is active.

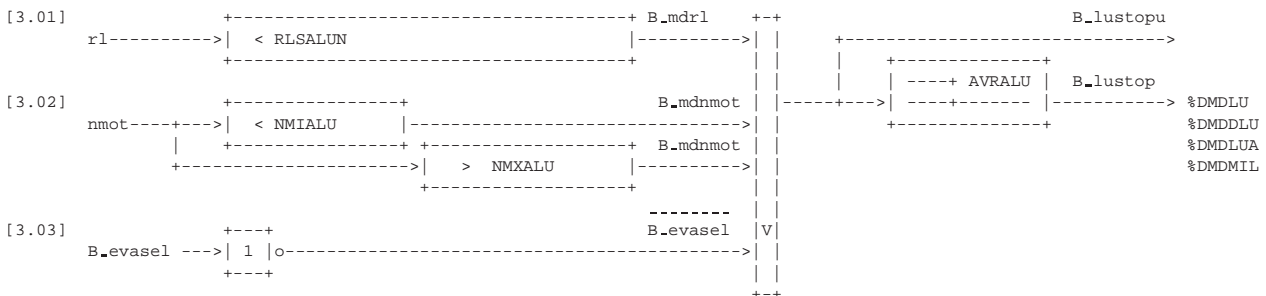


2. Formation of the stop bit : B\_mdstop for the deactivation of the functions : %DMDLU, %DMDDL, %DMDLUA, %DMDMIL and %DMDFON (fuel-on adaptation)  
[Nomenclature for cross coupling matrix : Partial function for common deactivation conditions DMDSTP MD]



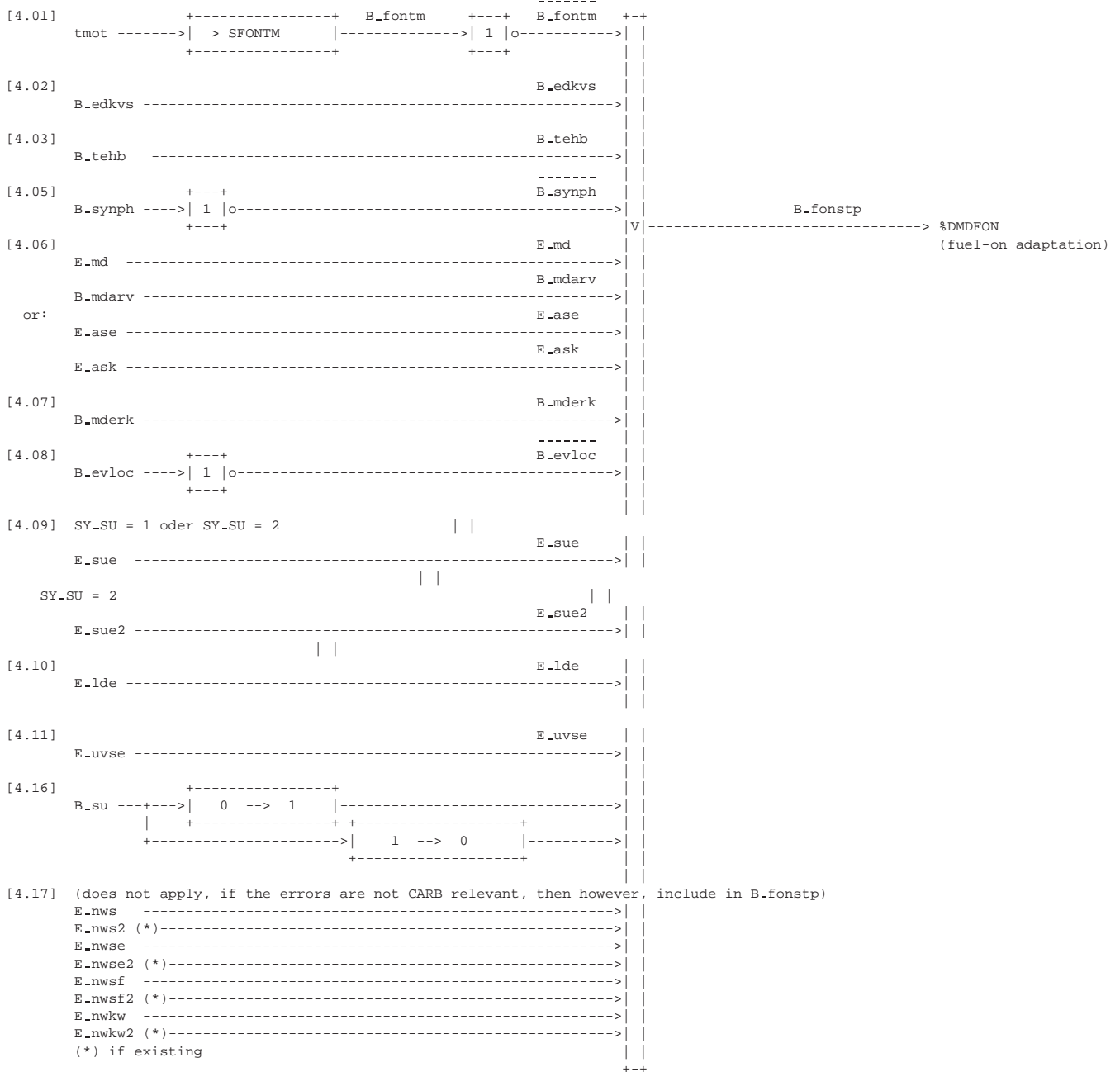


3. Formation of the stop bit : B\_lustop for the deactivation of the functions : %DMDLU, %DMDDL, %DMDLUA and %DMDMIL  
[Nomenclature for the cross coupling matrix : Partial function deactivation conditions specially for engine roughness  
DMDSTP LU]





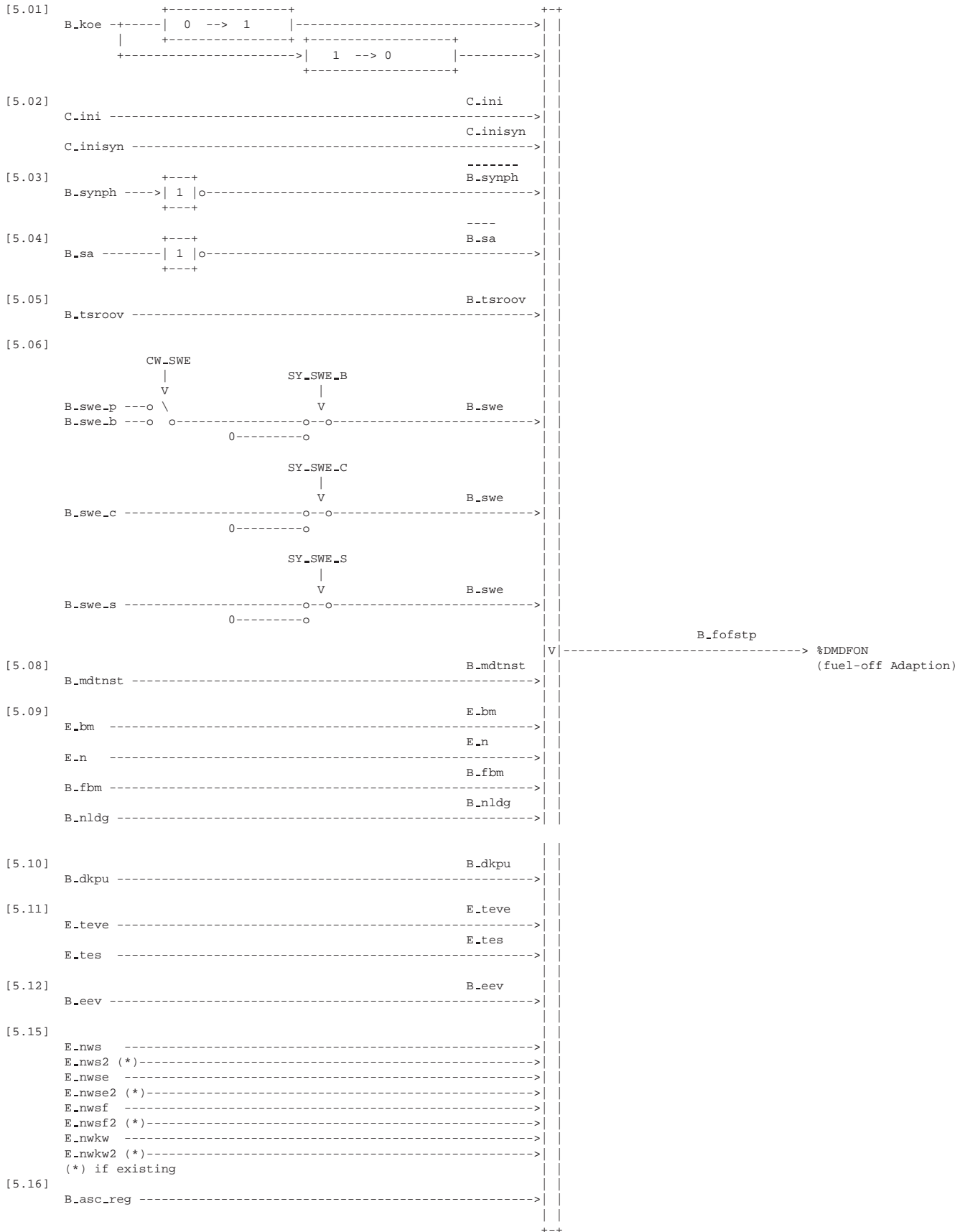
4. Formation of the stop bit : B\_fonstp for the deactivation of the function %DMDFON (fuel-on adaptation)  
[Nomenclature for cross coupling matrix : Partial function stop of the fuel-on adaptation DMDSTP FO]







5. Formation of the stop bit : B\_fofstp for the deactivation of the function %DMDFON (fuel-off adaptation)  
[Nomenclature for cross coupling matrix : Partial function stop of the fuel-off adaptation DMDSTP FF]





## ABK DMDSTP 9.90 Abbreviations

(n) = Crankshaft segments  
(t) = Time

Parameter	Source-X	Source-Y	Type	Description
AVRALU			FW	No. Camshaft-Revs/Combustions f. reactivation misfire detection a. disablement
CWSTPCNF			FW	code word disabeling criterion 1-> criterion active
DRLSOLA	RL		KL	Misfire Detection : load-dynamic treshold for deactivation
NGALUN	NMOT		KL	Misfire Detection : treshold for gradient of engine speed
NMIALU			FW	min. engine speed for deactivating misfire detection
NMXALU			FW	max. engine speed for deactivating misfire detection
RLSALULL			FW	Threshold load fuel cut-off detection for deactivating misfire detection in idle
RLSALUN	NMOT		KL	threshold load fuel cut-off detection for deactivating misfire detection
SFONTM			FW	threshold value tmot for fuel-on adaptation activ
SNM08DMUB	NMOT		SV (REF)	Datapoint distribution in DMD, 8 speed datapoints
SRL08DMUB	RL		SV (REF)	Datapoint distribution in DMD, 8 load datapoints
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_AGR			SYS (REF)	System constant AGR present
SY_ASR			SYS (REF)	system constant ASR present
SY_FANT			SYS (REF)	system constant increase of the fuel cut-off speed at tester intervention
SY_NWS			SYS (REF)	system constant camshaft control: none, 2 point, continous
SY_NWVAR			SYS (REF)	system constant for camshaft configuration
SY_PGRAD2			SYS (REF)	system constant: kind of the 2. phase signal
SY_SU			SYS (REF)	system constant: version of intake runner length adjuster
SY_SWE_B			SYS (REF)	system constant for rough road detection using PWM signal from ABS
SY_SWE_C			SYS (REF)	system constant for rough road detection using CAN
SY_SWE_S			SYS (REF)	system constant for rough road detection using engine roughness statistics
SY_TURBO			SYS (REF)	system constant for exhaust-gas turbocharger
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TALUST			FW	time for deactivating misfire detection after engine start
TAMIALU			FW	min. induction-air temperature for deactivating misfire-detection
VFZGADMD			FW	vehicle-speed threshold to deactivate the DMD at active brake intervention

Variable	Source	Type	Description
B_ASC_REG		EIN	CAN-message: ASC in action (with break intervention)
B_AUTGET	PROKON	EIN	condition automatic gearbox
B_BR2K	GGEGAS	EIN	Condition brakes actuated 2-channel detection
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DMBV		EIN	Active diagnosis: Torque comparsion cyl.-bank
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_EDKVS	DKVS	EIN	condition for adaption fault thresholds momentarily exceeded
B_EEV	DEVE	EIN	condition injector fault (power stage)
B_ENWS	DNWS	EIN	condition error camshaft control
B_ESGCAN		EIN	Condition error ecu-CAN for 2 ME-ecu's
B_EVASEL	AEVAB	EIN	Status:all local injector relevant to DASE are switched on
B_EVLOC	BGEVAB	EIN	Status: all injection valves are activated
B_FAAN		EIN	condition functional request for general speed increase
B_FAN		EIN	condition functional request for speed increase for quick trip
B_FBM	GGDPG	EIN	condition reference mark error => at least 1 tooth too few/many
B_FOFSTP	DMDSTP	AUS	condition fuel-off adaptation stopped
B_FOFSTPC		EIN	condition fuel-off adaptation stopped from 2nd ECU via CAN
B_FOFSTPT	DMDSTP	AUS	condition fuel-off adaptation stopped from 2nd ECU
B_FONSTP	DMDSTP	AUS	condition fuel-on adaptation stopped
B_FONSTPC		EIN	condition fuel-on adaptation stopped from 2nd ECU via CAN
B_FONSTPT	DMDSTP	AUS	condition fuel-on adaptation stopped from 2nd ECU
B_FONTM	DMDSTP	LOK	engine temperature high enough for fuel-on-adaption
B_KOE	KOS	EIN	Condition for AC-compressor ON
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_LL	MSF	EIN	Condition idle
B_LUENA	DMDSTP	LOK	Condition LU-calculation allowed (without time-delay)
B_LUSTOP	DMDSTP	AUS	misfire detection stop
B_LUSTOPC		EIN	misfire detection stop from 2nd ECU via CAN
B_LUSTOPT	DMDSTP	AUS	misfire detection stop from 2nd ECU
B_LUSTOPU	DMDSTP	LOK	Engine roughness calculation disabled , no time delay
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_MDDRLA	DMDSTP	LOK	Condition gradient of load for misfire detection
B_MDEIN	MDKOG	EIN	Condition actions on the torque are active
B_MDERK	DMDLAD	EIN	misfiring detected from multiple functions
B_MDNG	DMDSTP	LOK	Condition misfire detection gradient of engine speed
B_MDNMOT	DMDSTP	LOK	condition misfire detection high and low engine speed limit
B_MDRL	DMDSTP	LOK	Condition misfire detection low load-treshold
B_MDSTOP	DMDSTP	AUS	misfire detection stop
B_MDSTOPC		EIN	misfire detection stop from 2nd ECU via CAN
B_MDSTOPT	DMDSTP	AUS	misfire detection stop from 2nd ECU
B_MDTNST	DMDSTP	LOK	Condition misfire detection time after cranking
B_MILSTP	DMDSTP	AUS	statistic of misfire detection (%DMDMIL) stop
B_NLDG		EIN	condition limp-home function speed sensor
B_NWS	NWS	EIN	Condition camshaft control
B_NWS2		EIN	Tigger NWS valve 2



Variable	Source	Type	Description
B_PHSNL	NLPH	EIN	Condition phase search during phase sensor limp-home
B_SA	MDRED	EIN	Condition fuel cut-off
B_ST	SWADAP	EIN	condition for start
B_SU	SU	EIN	condition intake manifold switch-over
B_SU2	SU	EIN	condition intake manifold switch over, 2.flap
B_SWE_B		EIN	Condition rough road detected via a bit over CAN (from ABS-ECU)
B_SWE_C	DSWEC	EIN	Condition rough road detected from %DSWEC
B_SWE_P		EIN	Condition rough road detected via a PWM-Signal over CAN (from ABS-ECU)
B_SWE_S		EIN	Condition rough road detected from %DSWES
B_SYNPH	GGDPG	EIN	condition synchronization phase
B_TEB	TEB	EIN	condition for canister purge system with high canister load
B_TSROOV	DMDTSB	EIN	condition segment duration word overflow
B_WK		EIN	condition: converter lockup clutch closed
B_WKR		EIN	condition clutch controlled
DFP_AGRE		EIN	ECU int. fault path no.: EKR power stage
DFP_AGRF		EIN	ECU int. fault path no.: partial pressure EGR
DFP_BM		EIN	ECU int. fault path no.: reference mark
DFP_LDE		EIN	ECU int. fault path no.: electro pneumatic reversing valve power stage
DFP_MD		EIN	ECU int. fault path no.: misfire, multiple
DFP_N		EIN	ECU int. fault path no.: engine speed sensor
DFP_NWKW		EIN	ECU int. fault path no.: alignment between camshaft and crankshaft
DFP_NWKW2		EIN	ECU int. fault path no.: alignment between camshaft 2 and crankshaft
DFP_NWS		EIN	ECU int. fault path no.: camshaft control
DFP_NWS2		EIN	ECU int. fault path no.: camshaft control
DFP_NWSE		EIN	ECU int. fault path no.: camshaft control power stage
DFP_SUE		EIN	ECU-internal fault-path no.: Output-stage variable-tract intake manifold
DFP_SUE2		EIN	ECU int. fault path no.: Intake manifold valve 2
DFP_TES		EIN	Internal error path number evap system monitoring, pcv Struck open
DFP_TEVE		EIN	Internal fault path number: canister purge valve power stage
DFP_UVSE		EIN	Internal fault path number: power stage dump valve turbo
DFP_VFZ		EIN	ECU int. fault path no.: vehicle speed signal
E_AGRE		EIN	error flag: EGR power stage monitoring
E_AGRF		EIN	error flag: EGR flow monitoring
E_BM	DDG	EIN	error flag: reference mark sensor
E_LDE		EIN	error flag: electro pneumatic reversing valve (power stage)
E_MD	DMDMIL	EIN	Error flag: misfire, multiple
E_N	DDG	EIN	error flag: engine speed sensor
E_NWKW	DNWKW	EIN	error flag: alignment between camshaft and crankshaft
E_NWKW2	DNWKW	EIN	error flag: alignment between camshaft 2 and crankshaft
E_NWS	DNWS	EIN	error flag: camshaft control
E_NWS2	DNWS	EIN	error flag: camshaft control bank 2
E_NWSE	DNWSE	EIN	error flag: power stage of camshaft control valve
E_NWSE2		EIN	error flag: driver stage bank 2 of camshaft control valve
E_SUE		EIN	Errorflag: Power stage , Intake manifold valve
E_SUE2		EIN	Errorflag: Power stage, Intake manifold valve (bank2)
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_UVSE		EIN	error flag: power stage dump valve turbo
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
NGFIL_W	SWADAP	EIN	filtered engine-speed gradient
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RLGAS_W	BGRLG	EIN	gradient of air charge at one combustion cycle
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
TNST_W	BBSTT	EIN	time after end of start
VFZG	SWADAP	EIN	vehicle speed (km/h)

### FW DMDSTP 9.90 Fixed Values

Parameter	Value	Description
AVRALU		No. Camshaft-Revs/Combustions f. reactivation misfire detection a. disablement
CWSTPCNF		code word disabeling criterion 1-> criterion active
NMIALU		min. engine speed for deactivating misfire detection
NMXALU		max. engine speed for deactivating misfire detection
RLSALULL		Threshold load fuel cut-off detection for deactivating misfire detection in idle
SFONTM		threshold value tmot for fuel-on adaptation activ
TALUST		time for deactivating misfire detection after engine start
TAMIALU		min. induction-air temperature for deactivating misfire-detection
VFZGADM		vehicle-speed threshold to deactivate the DMD at active brake intervention

### FB DMDSTP 9.90 Detailed description of function

#### 1. Introduction

=====

With special operating conditions or errors of components, which lead to an increased engine roughness there, is a risk that an erroneous misfire detection or a mis-adaptation will be performed.  
So as to avoid this, the functions for the misfire detection and for the adaptation must be deactivated if the conditions mentioned below occur.



2. Formation of the stop bit B\_mdstop for deactivation of the functions : %DMDLU, %DMDLUA, %DMDMIL and %DMDFON (fuel-on adaptation)  
=====

If one of the following conditions is fulfilled then the stop bit B\_mdstop is set and the functions for the misfire detection by means of engine roughness (%DMDLU, %DMDLU, %DMDLUA and %DMDMIL) as well as the fuel-on adaptation (%DMDFON - fuel-on adaptation) are deactivated.  
Once the setting condition for B\_mdstop is no longer valid, the bit B\_mdstop is reset with a delay of AVRALU camshaft (NW) revolutions.

[2.01] Deactivation in case of engine speed dynamics, B\_mdng

For the detection of engine speed dynamics the absolute value of the filtered engine speed gradient |ngfil\_w| is compared to the characteristic line NGALU. If the characteristic line is exceeded B\_mdng = TRUE is set.

Remarks : - ngfil\_w is formed in %BGNG5.10 by filtering of the engine speed gradient ngas\_w.

So that ngfil\_w shows enough dynamic response, the filter time constant ZNGFIL there may not be chosen greater than 50ms.

- NGALU is a fixed characteristic line over the engine speed (8 base points, no interpolation)

[2.02] Deactivation in case of load dynamics, B\_mddrla

The detection of the load dynamics is performed differently, dependent on the ECU type (ME7 or M7):

ME7 : The absolute value of the load gradient |rlgas\_w| (formed via a working cycle) is compared to the characteristic line DRLSOLA. If the characteristic line is exceeded B\_mddrla = TRUE is set.

Remark : rlgas\_w is formed in the function %BGSRM (as from version 2.80)

Remark : DRLSOLA is a fixed characteristic line over the load (8 base points, no interpolation)

[2.03] Deactivation during engine start, B\_st

If B\_st = TRUE a deactivation is performed during engine start. (B\_st is generated in %BBSTT.)

[2.04] Deactivation for a time interval after end of start, B\_mdtntst

For a time interval TALUST after end of start the deactivation condition is fulfilled via the bit B\_mdtntst = TRUE.

Hint : According to the CARB legislation (1/97) deactivation may only be performed for 5s after end of start at the maximum.

[2.05] Deactivation in case of rough road condition, B\_swe

In case of detected rough road conditions, deactivation is performed via the bit B\_swe = TRUE. The deactivation is necessary, since the driving wheels can couple onto the drive shaft and thus also onto the crankshaft when driving across a rough road.

Because of several functions for rough road detection it is switched between several Bit dependant on the system constant value SY\_SWE\_S, SY\_SWE\_B, SY\_SWE\_C, CW\_SWE:

SY\_SWE\_B = 1 and CW\_SWE = 0: B\_swe\_b: vehicle wheel speed or wheel acceleration is evaluated in %BGRBS and %DSWEC

SY\_SWE\_B = 1 and CW\_SWE = 1: B\_swe\_p: pulse wide modulated signal comes via CAN (from the ABS-ECU)

SY\_SWE\_S = 1: B\_swe\_s: rough road detection is calculated from the statistic of the engine roughness values in %DSWES

SY\_SWE\_C = 1: B\_swe\_c: a rough road detected bit comes via CAN (from the ABS-ECU)

[2.06] Deactivation in case of active torque action, B\_mdein

In case of active torque action the deactivation condition is fulfilled via the bit B\_mdein = TRUE. A torque action can be triggered, e.g. by the following events:

- active ABS - control
- active ASR/PDR - control
- change of gears on automatic transmission

Remark : B\_mdein is generated in %MDKOG.

[2.07] Deactivation in case of segment time word overflow, B\_tsroov

If a word overflow occurs when forming the segment time, then B\_tsroov = TRUE and a deactivation takes place.

B\_tsroov is generated in %DMDTSB.

[2.08] Deactivation during the initialization phase, C\_ini, C\_inisyn

During the initialization phase C\_ini resp. C\_inisyn = TRUE applies.

[2.09] Deactivation when turning on or off the air conditioning compressor, B\_koe

When turning the air conditioning compressor on or off (positive and negative edge in B\_koe) a deactivation is performed.

[2.10] Deactivation in case of active canister purging diagnosis, B\_dtes

In case of active canister purging diagnosis (B\_dtes = TRUE) a deactivation is performed.

[2.11] Deactivation in case of fuel cut-off on overrun, B\_sa

During active fuel cut-off on overrun (B\_sa = TRUE) a deactivation is performed.

[2.13] Deactivation in case of a change of state of the torque converter lockup clutch, B\_wk, B\_wkr

In case of a change of state of the torque converter lockup clutch a deactivation is performed.

[2.14] Deactivation in case of inlet air temperature being too cold, tans

If the inlet air temperature (tans) falls short of the fixed value TAMIALU, then a deactivation is performed.

[2.16] Deactivation in case of camshaft adjustment, B\_nws

During the camshaft adjustment (positive or negative edge of B\_nws) a deactivation is performed.

[2.18] Deactivation in case of crankshaft reference mark error, E\_bm, E\_n, B\_fbm, B\_nldg

E\_bm : Reference mark error

E\_n : Error of the engine speed signal sensor, E\_n can be done without, if the condition is already included in E\_bm.

B\_fbm: Reference mark error ; one tooth too many or too little detected

In contrast to the above error bits, B\_fbm is set without time delay (debouncing and error memory access time).

B\_nldg: speed sensor emergency running (from %DDG10.10 on)



[2.19] Deactivation in case of non-synchronized throttle valve, B<sub>dkpu</sub>  
The fuel-off adaptation is deactivated, if there no valid information on the current position of the throttle valve.  
(B<sub>dkpu</sub> = 1 ; limp-home)

[2.23] Deactivation in case of ASR-, MSR-, ABS- or FDR-control, B<sub>asc.reg</sub>  
In addition to the torque action (B<sub>mdein</sub>) it covers the brake action.  
Possible bits are:  
- B<sub>asc.reg</sub>  
- B<sub>fdr</sub>  
- B<sub>eds</sub>  
- B<sub>asr</sub>

[2.25] Only on customer request : Deactivation in case of error in the exhaust gas recirculation system, E<sub>agre</sub>, E<sub>agrf</sub>  
E<sub>agre</sub> : Error in the power stage for triggering of EGR valve (from function %DAGRE)  
E<sub>agrf</sub> : Difference between actual and desired EGR partial pressure (from function %DAGRFR)  
In case of error, a too high EGR rate may result in a delayed combustion and thus in an increased engine roughness.

[2.26] Only on customer request : Deactivation in case of errors in the canister purging system, E<sub>teve</sub>, E<sub>tes</sub>  
E<sub>teve</sub> : Error canister purging valve power stage  
E<sub>tes</sub> : Error canister purging system  
In case of faulty open canister purging valve an increased engine roughness may result due to strong enrichment.

3. Formation of the stop bit : B<sub>lustop</sub> for the deactivation of the functions : %DMDLU, %DMDDL, %DMDLUA and %DMDMIL

=====

If one of the conditions to follow is fulfilled, then the stop bit B<sub>lustop</sub> is set and the functions for the misfire detection by means of engine roughness (%DMDLU, %DMDDL, %DMDLUA and %DMDMIL) are deactivated.  
Once the setting conditions for B<sub>lustop</sub> are no longer valid, the bit B<sub>lustop</sub> is reset with a delay of AVRALU NW revolutions.

[3.01] Deactivation below zero load, B<sub>mdrl</sub>  
If the engine load falls short of the characteristic line RLSALUN, then B<sub>mdrl</sub> = TRUE is set. RLSALUN is a characteristic line over the engine speed. ( 8 base points )

[3.02] Deactivation in case of too low / too high engine speed, B<sub>mdnmot</sub>  
If the engine speed lies outside of the value range [NMIALU ; NMXALU], the misfire detection is deactivated.

[3.03] Deactivation in case of injection switch-off, B<sub>evasel</sub>  
For certain operating conditions, for which the motronic actively cuts out the injection of one or several cylinders (B<sub>evasel</sub> = 0), the misfire detection must be deactivated.  
Possible causes for such cylinder cutouts are:  
- Maximum engine speed is exceeded  
- Maximum vehicle speed is exceeded  
- Torque reduction  
- Cylinder cutouts induced by workshop tester  
No deactivation of the misfire detection, however, is performed in the following events of a cylinder cutout:  
- Error in the power stage of an injector  
- Cylinder cutout due to detected misfire on a cylinder

4. Formation of the stop bit : B<sub>fonstp</sub> for the deactivation of the function %DMDFON (fuel-on adaptation)

=====

If one of the conditions to follow is fulfilled, then the stop bit B<sub>fonstp</sub> is set and the partial function for the fuel-on adaptation (%DMDFON) is deactivated.

[4.01] Deactivation in case of cold engine, B<sub>fontm</sub>  
The fuel-on adaptation is deactivated in case of a cold engine (B<sub>fontm</sub> = 0) due to the engine roughness resulting from this.

[4.02] Deactivation in case of error in the mixture formation, B<sub>edkvs</sub>  
The fuel-on adaptation is deactivated, if the adaptation error threshold in the mixture formation is exceeded (B<sub>edkvs</sub> = 1).

[4.03] Deactivation in case of canister purging with high charge, B<sub>tehb</sub>  
The fuel-on adaptation is deactivated in case of canister purging with high charge (B<sub>tehb</sub> = 1), since here there is a risk of increased engine roughness due to mixture enrichment.

[4.05] Deactivation in case of missing synchronization, B<sub>synph</sub>  
As long as there is no synchronization (B<sub>synph</sub> = 0), the fuel-on adaptation is deactivated.

[4.06] Deactivation in case of existing misfires, E<sub>md</sub>, B<sub>mdarv</sub> or E<sub>ase</sub>, E<sub>ask</sub>  
In case of DMDMIL1.xx:  
If a misfire error entry (E<sub>md</sub>=1) or a specific misfire rate (B<sub>mdarv</sub>=1) exist, then the fuel-on adaptation is deactivated.  
In case of DMDMIL3.xx:  
If a cat. damaging misfire error entry exists (E<sub>ask</sub>=1) or a emission rel. mirifre error entry exists (E<sub>ase</sub>=1) then the fuel-on adaptation is deactivated.

[4.07] Deactivation in case of detected misfires, B<sub>mderk</sub>  
With each detected misfire (B<sub>mderk</sub> = 1) the fuel-on adaptation is deactivated.

[4.08] Deactivation in case of injection switch-off, B<sub>evloc</sub>  
With each kind of active injection switch-off (B<sub>evloc</sub> = 0), the fuel-on adaptation is deactivated.

[4.09] Deactivation in case of power stage error during the intake manifold switch-over, E<sub>sue</sub> or E<sub>sue2</sub>

[4.10] Deactivation in case of error in the power stage of the wastegate, E<sub>lde</sub>  
(only on turbocharged engines)

[4.11] Deactivation in case of error in the power stage of the divert air valve, E<sub>uvse</sub>  
(only on turbocharged engines)



[4.16] Deactivation in case of intake manifold switch-over, B<sub>.su</sub>  
During the intake manifold switch-over (positive or negative edge of B<sub>.su</sub>) a deactivation is performed.

[4.17] Deactivation in case of errors of the camshaft adjustment resp. in case of incorrect assignment between NW and KW  
For projects, for which the following errors are CARB relevant it must each time be checked whether a deactivation shall be performed :

E<sub>.nws</sub> resp. E<sub>.nws2</sub> : General error in the system of the camshaft control  
E<sub>.nwse</sub> resp. E<sub>.nwse2</sub> : Error in the power stage of the camshaft adjustment  
E<sub>.nwsf</sub> resp. E<sub>.nwsf2</sub> : Camshaft control error detected by the diagnosis of the intake manifold pressure  
E<sub>.nwk</sub> resp. E<sub>.nwk2</sub> : Angle between camshaft and crankshaft is no longer correct

5. Formation of the stop bit : B<sub>.fofstp</sub> for the deactivation of the function %DMDFON (fuel-off adaptation)

=====

If one of the conditions to follow is fulfilled, then the stop bit B<sub>.fofstp</sub> is set and the partial function for the fuel-off adaptation (%DMDFON) is deactivated.

[5.01] Deactivation when turning on or off the air conditioning compressor, B<sub>.koe</sub>  
When turning the air conditioning compressor on or off (positive and negative edge in B<sub>.koe</sub>) a deactivation is performed.

[5.02] Deactivation during the initialization phase, C<sub>.ini</sub>, C<sub>.inisyn</sub>  
During the initialization phase C<sub>.ini</sub> resp. C<sub>.inisyn</sub> = TRUE applies.

[5.03] Deactivation in case of missing synchronization, B<sub>.synph</sub>  
As long as there is no synchronization (B<sub>.synph</sub> = 0), the fuel-on adaptation is deactivated.

[5.04] Deactivation when not in the overrun, B<sub>.sa</sub>  
The fuel-off adaptation is deactivated, if there is no overrun (B<sub>.sa</sub> = 0).

[5.05] Deactivation in case of segment time word overflow, B<sub>.tsroov</sub>  
If a word overflow occurs when forming the segment times, then B<sub>.tsroov</sub> = TRUE is set and a deactivation is performed.  
B<sub>.tsroov</sub> is generated in %DMDTSB.

[5.06] Deactivation in case of rough road condition, B<sub>.swe</sub>  
In case of detected rough road conditions, deactivation is performed via the bit B<sub>.swe</sub> = TRUE. The deactivation is necessary, since the driving wheels can couple onto the drive shaft and thus also onto the crankshaft when driving across a rough road.

Because of several functions for rough road detection it is switched between several Bit dependant on the system constant value SY<sub>.SWE.S</sub>, SY<sub>.SWE.C</sub>, SY<sub>.SWE.B</sub>, CW<sub>.SWE</sub>:

SY<sub>.SWE.B</sub> = 1 and CW<sub>.SWE</sub> = 0: B<sub>.swe.b</sub>: vehicle wheel speed or wheel acceleration is evaluated in %BGRBS and %DSWEC  
SY<sub>.SWE.B</sub> = 1 and CW<sub>.SWE</sub> = 1: B<sub>.swe.p</sub>: pulse wide modulated signal comes via CAN (from the ABS-ECU)  
SY<sub>.SWE.S</sub> = 1: B<sub>.swe.s</sub>: rough road detection is calculated from the statistic of the engine roughness values in %DSWES  
SY<sub>.SWE.C</sub> = 1: B<sub>.swe.c</sub>: a rough road detected bit comes via CAN (from the ABS-ECU)

[5.08] Deactivation for the time interval after end of start, B<sub>.mdtnst</sub>  
For a time interval TALUST after end of start the deactivation condition is fulfilled via the bit B<sub>.mdtnst</sub> = TRUE.  
[also see point 2.04]

[5.09] Deactivation in case of crankshaft reference mark error, E<sub>.bm</sub>, E<sub>.n</sub>, B<sub>.fbm</sub>, B<sub>.nldg</sub>  
E<sub>.bm</sub> : Reference mark error  
E<sub>.n</sub> : Error of the engine speed signal sensor, E<sub>.n</sub> can be done without, if the condition is already included in E<sub>.bm</sub>.  
B<sub>.fbm</sub>: Reference mark error ; one tooth too many or too little detected  
In contrast to the above error bits, B<sub>.fbm</sub> is set without time delay (debouncing and error memory access time).  
B<sub>.nldg</sub>: speed sensor emergency running (from %DDG10.10 on)

[5.10] Deactivation in case of non-synchronized throttle valve, B<sub>.dkpu</sub>  
The fuel-off adaptation is deactivated, if there is no valid information on the current position of the throttle valve.  
(B<sub>.dkpu</sub> = 1 ; limp-home)

[5.11] Deactivation in case of errors in the canister purging system, E<sub>.teve</sub>, E<sub>.tes</sub>  
E<sub>.teve</sub> : Error canister purging valve power stage  
E<sub>.tes</sub> : Error canister purging system  
In case of faulty open canister purging valve an increased engine roughness may result due to strong enrichment.

[5.12] Deactivation in case of diagnosis error injector, B<sub>.eev</sub>

[5.15] Deactivation in case of errors of the camshaft adjustment, s. 2.17

[5.16] Deactivation in case of ASC-, MSR-, ABS-control, B<sub>.asc\_reg</sub>, s. 2.23



## APP DMDSTP 9.90 Application hint

### 1) Monitor function

For the application it is necessary to be able to realize the status bits B\_mdstop, B\_lustop, B\_fonstp and B\_fofstp in a synchronized fashion. This is possible by means of a monitor function.  
The description of the monitor function can be found in %DMDUE.

### 2) with 2 ECUs:

On vehicles with two Electronic Control Units it must be checked on whether in case of an error in the load and temperature acquisition on one of the two ECUs, the engine bank for the other ECU in the misfire detection is interfered with.

### 3) The threshold value NMIALU (for deactivation in case of too low engine speeds) should not be chosen smaller than the minimum engine speed, which can still be realized due to the quantization tsquant.

### 4) Application of the characteristic lines NGALU and DRLSOLA

During the application of the characteristic lines NGALU and DRLSOLA it must be checked to what extent the gradients ngfil\_w as well as rlgas\_w respond to misfires.  
This check should mainly be performed in the range with low engine speed and high load (1000 - 1500 rpm ; 40-60% load ; continuous and multiple misfire). The threshold values must in any case be chosen larger than the maximum amplitudes of the corresponding gradients occurring during misfire operation.

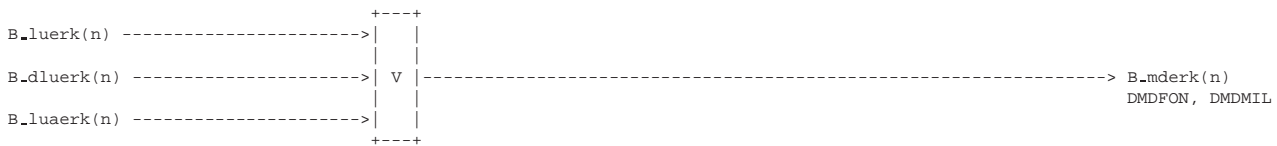
### 5) Short test for the check on whether function is active

- Set threshold NMIALU e.g. to 1400 rpm
- if the function is active it must apply: B\_mdstop = 1 for nmot < NMIALU (e.g. idling) and B\_mdstop = 0 if engine speed is kept above NMIALU

## DMDLAD 5.10 Logic and Delay; Logical operation, different blocks for misfire detection

### FDEF DMDLAD 5.10 Function definition

Overview DMDLAD:



The entire functions for misfire detection can be locked with the Eurocodeword CDMD.  
For B\_cdmd=0 the function DMDLAD is locked and B\_mderk and B\_mderkf are set to 0.  
For B\_cdmd=1 the function DMDLAD is active.

In case of 2 ecu's (SY\_2SG = 1) the function %DMDLAD is deactivated in the master-ecu (B\_master = 1).

### ABK DMDLAD 5.10 Abbreviations

Subscripts and reference points used:

(n) = crankshaft segments

SY\_ZYLZA = number of cylinders

Variable	Source	Type	Description
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_DLUERK	DMDDL	EIN	condition for misfiring detected, from DMDDL
B_LUAERK	DMDLUA	EIN	condition for misfiring detected, with engine roughness distance, from DMDLUA
B_LUERK	DMDLU	EIN	condition for misfiring detected, from DMDLU
B_MASTER		EIN	Condition MASTER-ECU
B_MDERK	DMDLAD	AUS	misfiring detected from multiple functions
SY_2SG	PROKON	EIN	system constant 2 motronic systems

### FW DMDLAD 5.10 Fixed Values

Parameter	Value	Description
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### FB DMDLAD 5.10 Detailed description of function

#### 1. Logical and temporal combination of the results different functions for misfire detection

The detection results several functions for misfire detection are combined.

It is the matter of the following functions and result signals:

- DMDLU -> B\_luerk
- DMDDL -> B\_dluerk
- DMDLUA -> B\_luaerk

All signals are set at the time/ignition when misfire is detected. So a cylinder identification and temporal association is possible (see %DMDMIL).

The result is a combined signal for detection and identification of misfire and for the stop of the adaptation (see %DMDFON).



1.1 Temporal synchronisation

The problem of the temporal synchronization is solved in the different functions themselves.  
e.g. at the calculation time  $n+(SY\_ZYLZA/2)$  the result bit B\_dluerk(n) is set retroactive.

1.2 Logical combination

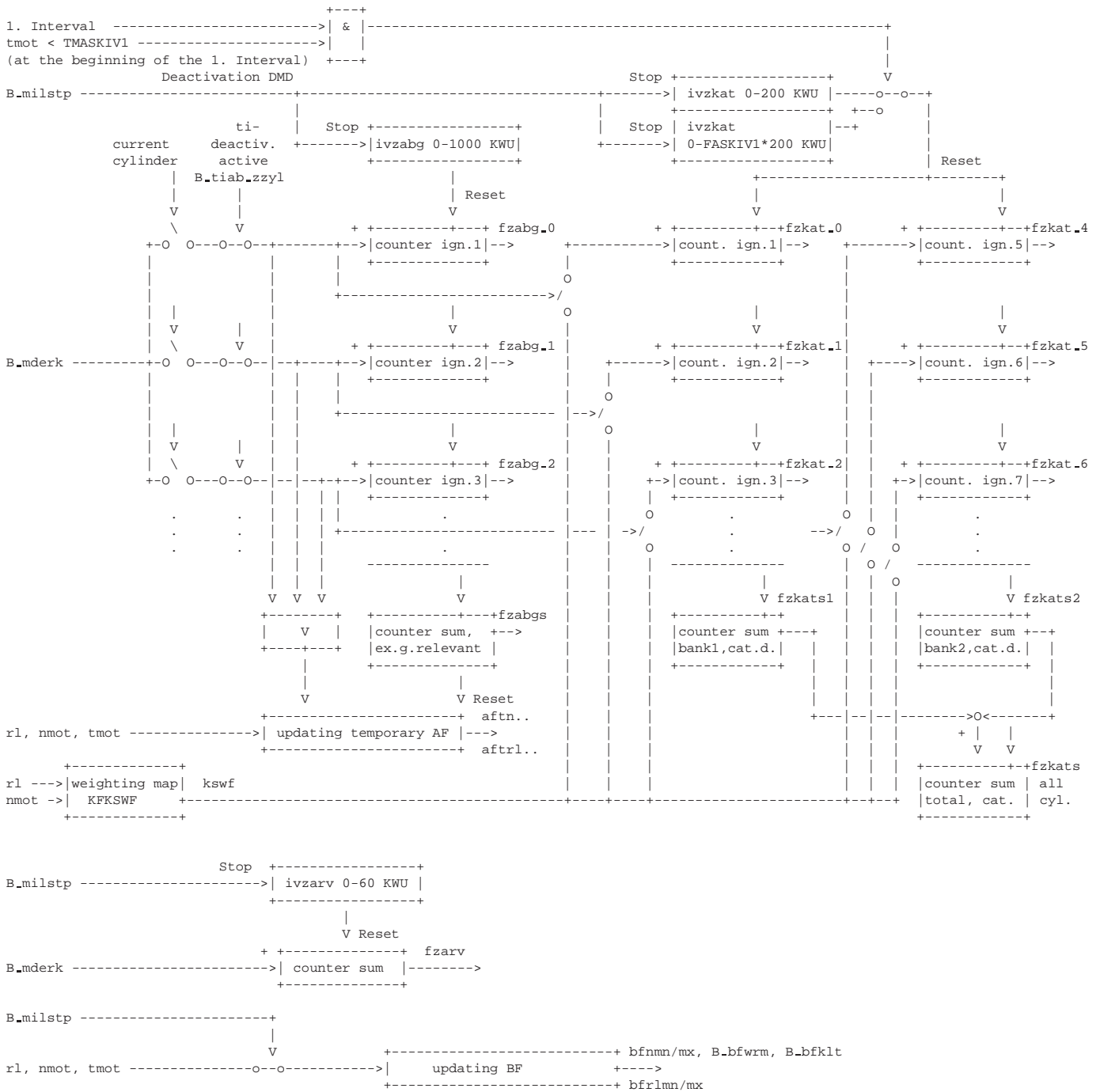
All temporal synchronized result signals (B\_luerk, B\_dluerk, B\_luaerk) are OR-combined. If at least one of these signals is set the output B\_mderk is set to 1.

APP DMDLAD 5.10 Application hint

DMDMIL 3.60 Fault treatment of misfire detection, control on MIL and rectification

FDEF DMDMIL 3.60 Function definition

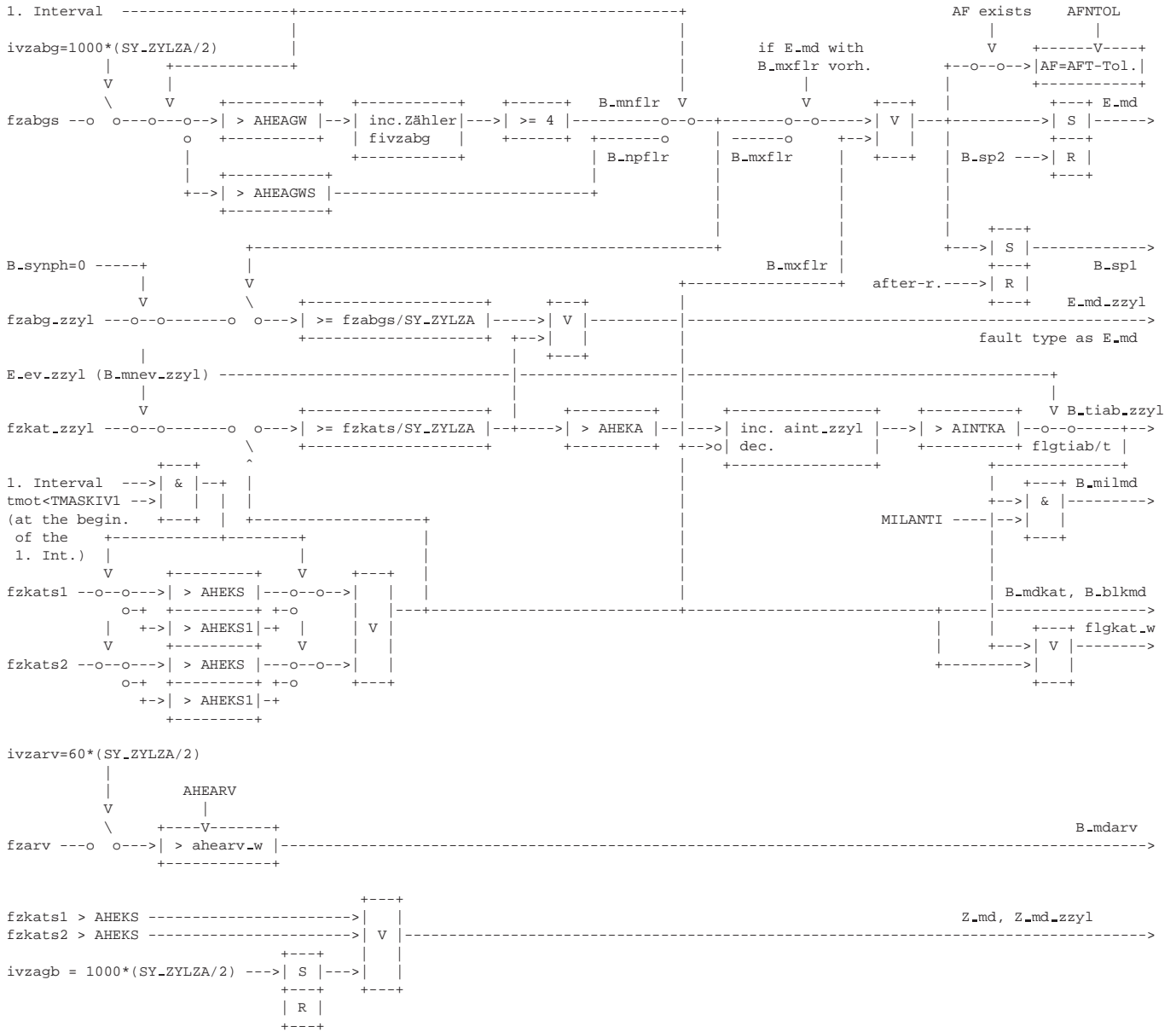
1. Fault counting algorithm



2.1. Fault detection

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During the after-run:



Ambient conditions: tfst (tank filling), rl (load), nmot (engine speed), tmot (engine temperature), B\_sch

The function DMDMIL can be blocked via the code word CDMD.

If B\_cdmd=0 the function is blocked, i.e. E\_md=0, E\_md\_zzyl=0, Z\_md=1, Z\_md\_zzyl=1.

If B\_cdmd=1 the function is active.



## ABK DMDMIL 3.60 Abbreviations

zzyl Cylinder number  
SY\_ZYLZA No. of cylinders  
BF Operating window engine operation  
AFT Temporary operating window with misfires  
AF Final operating window with misfires  
FSP Fault memory  
exh. fault Exhaust gas relevant fault  
cat. fault catalyst damaging fault  
Start fault exhaust gas relevant fault during the first interval after start

MD Misfire Detection (description for cross coupling matrix)  
ID Cylinder identification (description for cross coupling matrix)

Parameter	Source-X	Source-Y	Type	Description
AFNTOL			FW	tolerance for decreasing the misfire window in the speed range
AHEAGW			FW	misfire frequency at which emission limits occurs
AHEAGWS			FW	misfire frequency at which emission limits occurs
AHEARV			FW	misfire frequency at which other functions will be stopped
AHEKA			FW	misfire frequency at which fuel cutoff occurs
AHEKS			FW	misfire frequency at which catalyst damage occurs
AHEKS1			FW	misfire frequency at which catalyst damage occurs during first intervall
AINTKAN	NMOT		KL	number of interval misfire frequency at which ti- cutoff
AZYTIAB			FW	maximum number of cylinder with ti- cut off at which catalyst damage occurs
CDCMD	BLOKNR		KL	Code word CARB: misfire, multiple
CDCMD00	BLOKNR		KL	Code word CARB: misfire cyl. 0
CDCMD01	BLOKNR		KL	Code word CARB: misfire cyl. 1
CDCMD02	BLOKNR		KL	Code word CARB: misfire cylinder 2
CDCMD03	BLOKNR		KL	Code word CARB: misfire cylinder 3
CDCMD04	BLOKNR		KL	Code word CARB: misfire cylinder 4
CDCMD05	BLOKNR		KL	Code word CARB: misfire cylinder 5
CDCMD06	BLOKNR		KL	Code word CARB: misfire cylinder 6
CDCMD07	BLOKNR		KL	Code word CARB: misfire cylinder 7
CDCMD08	BLOKNR		KL	Code word CARB: misfire cylinder 8
CDCMD09	BLOKNR		KL	Code word CARB: misfire cylinder 9
CDCMD10	BLOKNR		KL	Code word CARB: misfire cylinder 10
CDCMD11	BLOKNR		KL	Code word CARB: misfire cylinder 11
CDTMD			FW	Code word tester: misfire, multiple
CDTMD00			FW	Code word tester: misfire cyl. 0
CDTMD01			FW	Code word tester: misfire cyl. 1
CDTMD02			FW	Code word tester: misfire cylinder 2
CDTMD03			FW	Code word tester: misfire cylinder 3
CDTMD04			FW	Code word tester: misfire cylinder 4
CDTMD05			FW	Code word tester: misfire cylinder 5
CDTMD06			FW	Code word tester: misfire cylinder 6
CDTMD07			FW	Code word tester: misfire cylinder 7
CDTMD08			FW	Code word tester: misfire cylinder 8
CDTMD09			FW	Code word tester: misfire cylinder 9
CDTMD10			FW	Code word tester: misfire cylinder 10
CDTMD11			FW	Code word tester: misfire cylinder 11
CWDMDE			FW	code word for EOBD-application DMDMIL (healing without window overlap)
FAINTEN			FW	number of interval for enabling ti - cutoff
FASKIV1			FW	factor for increasing the 1. cat-interval, misfire detection
KFKSWF	N	TL	KF	map for catalyst protection, weighting factors
MILANTI			FW	MIL is on during ti turn-off in 1. dcy
NLLM	TMOT		KL	desired engine speed
TMASKIV1			FW	temp. threshold for increasing 1. cat-interval, misfire detection
TMWUC			FW	engine temperture threshold for fulfilment "warm up cycle"

Variable	Source	Type	Description
AFNMN	DMDMIL	LOK	area of misfirings, minimum engine speed
AFNMX	DMDMIL	LOK	area of misfirings, maximum engine speed
AFRLMN	DMDMIL	LOK	area of misfirings, minimum load
AFRLMX	DMDMIL	LOK	area of misfirings, maximum load
AFTNMN	DMDMIL	LOK	area of misfirings, minimum engine speed, temporary
AFTNMX	DMDMIL	LOK	area of misfirings, maximum engine speed, temporary
AFRLMN	DMDMIL	LOK	area of misfirings, minimum load, temporary
AFRLMX	DMDMIL	LOK	area of misfirings, maximum load, temporary
AHEARV_W	DMDMIL	LOK	Misfiring frequency to reach suppression of other functions (from AHEARV
AINTKAMIN	DMDMIL	LOK	number of interval misfire frequency at which ti- cutoff, minimal value
AINT_0	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 1
AINT_1	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 2
AINT_10	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 11
AINT_11	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 12
AINT_2	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 3
AINT_3	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 4
AINT_4	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 5
AINT_5	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 6
AINT_6	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 7
AINT_7	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 8
AINT_8	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 9
AINT_9	DMDMIL	LOK	amount of catalyst damaging intervals for ignition 10
ANZAIINTEN	DMDMIL	LOK	number of interval after start for enabling ti- cutoff (200 crankshaft rev.)



Variable	Source	Type	Description
AZYCNT	DMDMIL	LOK	amount of deactivateg cylinders because of cat. damaging misfire
BFNMN	DMDMIL	LOK	area of engine operation, minimum engine speed
BFNMX	DMDMIL	LOK	area of engine operation, maximum engine speed
BFRLMN	DMDMIL	LOK	area of engine operation, minimum load
BFRLMX	DMDMIL	LOK	area of engine operation, maximum load
B_AFKLT	DMDMIL	LOK	window for misfiring, condition cold, TMOT<TMWUC
B_AFTKLT	DMDMIL	LOK	window for misfiring, temporary, condition cold, TMOT<TMWUC
B_AFTWRM	DMDMIL	LOK	window for misfiring, temporary, condition warm, TMOT>TMWUC
B_AFWRM	DMDMIL	LOK	window for misfiring, condition warm, TMOT>TMWUC
B_BFKLT	DMDMIL	LOK	window engine operation, condition cold, TMOT<TMWUC
B_BFWRM	DMDMIL	LOK	window engine operation, condition warm, TMOT>TMWUC
B_BLKMD	DMDMIL	AUS	MIL-trigger blinking controlled by misfire detection
B_CDMD	PROKON	EIN	function active per codeword CDMD
B_DCY	DDCY	EIN	condition for 'driving cycle' fulfilled
B_MDARV	DMDMIL	AUS	critical misfire rate detected
B_MDKAT	DMDMIL	AUS	cat. damaging misfire rate exceeded (for deactivation of other functions)
B_MILMD	DMDMIL	AUS	MIL-trigger on controlled by misfire detection, during ti turn-off
B_MILSTP	DMDSTP	EIN	statistic of misfire detection (%DMDMIL) stop
B_MNEV1C		EIN	Error type: short circuit to ground at power stage injector 1
B_MNEV2C		EIN	Error type: short circuit to ground at power stage injector 2
B_MNEV3C		EIN	Error type: short circuit to ground at power stage injector 3
B_MNEV4C		EIN	Error type: short circuit to ground at power stage injector 4
B_MNEV5C		EIN	Error type: short circuit to ground at power stage injector 5
B_MNEV6C		EIN	Error type: short circuit to ground at power stage injector 6
B_MNMD	DMDMIL	LOK	Fault type min.: misfire, multiple
B_MXMD	DMDMIL	LOK	Fault type max.: misfire, multiple
B_NPMD	DMDMIL	LOK	Fault type not plaus.: misfire, multiple
B_SP1	DMDMIL	AUS	FLC-trigger of misfire detection
B_SP2	DMDMIL	AUS	HLC-trigger of misfire detection
B_SYNPH	GGDPG	EIN	condition synchronization phase
B_TIAB0	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ignition 0
B_TIAB1	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ignition 1
B_TIAB10	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl. 10
B_TIAB11	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl. 11
B_TIAB2	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 2
B_TIAB3	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 3
B_TIAB4	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 4
B_TIAB5	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 5
B_TIAB6	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 6
B_TIAB7	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 7
B_TIAB8	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl/ign. 8
B_TIAB9	DMDMIL	AUS	ti-cutoff at catalyst damaging misfiring, cyl. 9
B_WUC	DWUC	EIN	condition for detected 'warm up cycle'
EEVMNC		EIN	Error type: short circuit to ground at power stage injector 1..8
E_EV		EIN	error flag: general injector fault (power stage)
E_EV1	DEVE	EIN	error flag: injection valve of cyl. 1
E_EV2	DEVE	EIN	error flag: injection valve of cyl. 2
E_EV3	DEVE	EIN	error flag: injection valve of cyl. 3
E_EV4	DEVE	EIN	error flag: injection valve of cyl. 4
E_EV5	DEVE	EIN	error flag: injection valve of cyl. 5
E_EV6	DEVE	EIN	error flag: injection valve of cyl. 6
E_EV7	DEVE	EIN	error flag: injection valve of cyl. 7
E_EV8	DEVE	EIN	error flag: injection valve of cyl. 8
E_MD	DMDMIL	AUS	Error flag: misfire, multiple
E_MD00	DMDMIL	AUS	Error flag: misfire ignition 0
E_MD01	DMDMIL	AUS	Error flag: misfire ignition 1
E_MD02	DMDMIL	AUS	Error flag: misfire ignition 2
E_MD03	DMDMIL	AUS	Error flag: misfire ignition 3
E_MD04	DMDMIL	AUS	Error flag: misfire ignition 4
E_MD05	DMDMIL	AUS	Error flag: misfire ignition 5
E_MD06	DMDMIL	AUS	Error flag: misfire ignition 6
E_MD07	DMDMIL	AUS	Error flag: misfire ignition 7
E_MD08	DMDMIL	AUS	Error flag: misfire ignition 8
E_MD09	DMDMIL	AUS	Error flag: misfire ignition 9
E_MD10	DMDMIL	AUS	Error flag: misfire ignition 10
E_MD11	DMDMIL	AUS	Error flag: misfire ignition 11
FIVZABG	DMDMIL	LOK	intervall counter emission relevant misfiring
FLGKAT_W	DMDMIL	LOK	state flag cat. damaging misfire rates or ti turn-off
FLGTIAB	DMDMIL	AUS	state flag ti turn-of by catalyst damaging misfiring rates
FLGTIABT	DMDMIL	AUS	state flag ti turn-of by catalyst damaging misfiring rates
FZABGS_W	DMDMIL	LOK	fault counter, summary, counts emission relevant misfirings of all cylinders
FZABG_W_0	DMDMIL	LOK	fault counter ign. 1, counts emission relevant misfirings of ignition 1
FZABG_W_1	DMDMIL	LOK	fault counter ign. 2, counts emission relevant misfirings of ignition 2
FZABG_W_10	DMDMIL	LOK	fault counter ign.11, counts emission relevant misfirings of ignition 11
FZABG_W_11	DMDMIL	LOK	fault counter ign.12, counts emission relevant misfirings of ignition 12
FZABG_W_2	DMDMIL	LOK	fault counter ign. 3, counts emission relevant misfirings of ignition 3
FZABG_W_3	DMDMIL	LOK	fault counter ign. 4, counts emission relevant misfirings of ignition 4
FZABG_W_4	DMDMIL	LOK	fault counter ign. 5, counts emission relevant misfirings of ignition 5
FZABG_W_5	DMDMIL	LOK	fault counter ign. 6, counts emission relevant misfirings of ignition 6
FZABG_W_6	DMDMIL	LOK	fault counter ign. 7, counts emission relevant misfirings of ignition 7
FZABG_W_7	DMDMIL	LOK	fault counter ign. 8, counts emission relevant misfirings of ignition 8
FZABG_W_8	DMDMIL	LOK	fault counter ign. 9, counts emission relevant misfirings of ignition 9



Variable	Source	Type	Description
FZABG_W_9	DMDMIL	LOK	fault counter ign.10, counts emission relevant misfirings of ignition 10
FZARV_W	DMDMIL	LOK	fault counter, counts misfirings of all cylinders
FZKATS1_W	DMDMIL	LOK	failure counter, summary, counts catalyst damaging misfiring of cylinder bank 1
FZKATS2_W	DMDMIL	LOK	failure counter, summary, counts catalyst damaging misfiring of cylinder bank 2
FZKATS_W	DMDMIL	LOK	fault counter, summary, counts catalyst damaging misfirings of all cylinders
FZKAT_W_0	DMDMIL	LOK	fault counter ign. 1, counts cat. damaging misfire of ignition 1
FZKAT_W_1	DMDMIL	LOK	fault counter ign. 2, counts cat. damaging misfire of ignition 2
FZKAT_W_10	DMDMIL	LOK	fault counter ign.11, counts cat. damaging misfire of ignition 11
FZKAT_W_11	DMDMIL	LOK	fault counter ign.12, counts cat. damaging misfire of ignition 12
FZKAT_W_2	DMDMIL	LOK	fault counter ign. 3, counts cat. damaging misfire of ignition 3
FZKAT_W_3	DMDMIL	LOK	fault counter ign. 4, counts cat. damaging misfire of ignition 4
FZKAT_W_4	DMDMIL	LOK	fault counter ign. 5, counts cat. damaging misfire of ignition 5
FZKAT_W_5	DMDMIL	LOK	fault counter ign. 6, counts cat. damaging misfire of ignition 6
FZKAT_W_6	DMDMIL	LOK	fault counter ign. 7, counts cat. damaging misfire of ignition 7
FZKAT_W_7	DMDMIL	LOK	fault counter ign. 8, counts cat. damaging misfire of ignition 8
FZKAT_W_8	DMDMIL	LOK	fault counter ign. 9, counts cat. damaging misfire of ignition 9
FZKAT_W_9	DMDMIL	LOK	fault counter ign.10, counts cat. damaging misfire of ignition 10
IVZABG_W	DMDMIL	LOK	interval counter for emission relevant faults (0 - 1000 crankshaft revolutions)
IVZAIN_T_W	DMDMIL	LOK	interval counter for enable of ti-cut off (0 - 200 crankshaft revs.)
IVZARV_W	DMDMIL	LOK	interval counter for misfires (0-60 crankshaft revolutions)
IVZKAT_W	DMDMIL	LOK	interval counter for catalyst damaging misfirings (0 - 200 crankshaft revs.)
KSWF	DMDMIL	LOK	catalyst protection weighting factors, from KFKSWF
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
TFST	GGFST	EIN	fuel level in tank
TMOT	SWADAP	EIN	Engine temperature
Z_MD	DMDMIL	AUS	Cycle flag: misfire, multiple
Z_MD00	DMDMIL	AUS	Cycle flag: misfire ignition 0
Z_MD01	DMDMIL	AUS	Cycle flag: misfire ignition 1
Z_MD02	DMDMIL	AUS	Cycle flag: misfire ignition 2
Z_MD03	DMDMIL	AUS	Cycle flag: misfire ignition 3
Z_MD04	DMDMIL	AUS	Cycle flag: misfire ignition 4
Z_MD05	DMDMIL	AUS	Cycle flag: misfire ignition 5
Z_MD06	DMDMIL	AUS	Cycle flag: misfire ignition 6
Z_MD07	DMDMIL	AUS	Cycle flag: misfire ignition 7
Z_MD08	DMDMIL	AUS	Cycle flag: misfire ignition 8
Z_MD09	DMDMIL	AUS	Cycle flag: misfire ignition 9
Z_MD10	DMDMIL	AUS	Cycle flag: misfire ignition 10
Z_MD11	DMDMIL	AUS	Cycle flag: misfire ignition 11

### FW DMDMIL 3.60 Fixed Values

Parameter	Value	Description
AFNTOL		tolerance for decreasing the misfire window in the speed range
AHEAGW		misfire frequency at which emission limits occurs
AHEAGWS		misfire frequency at which emission limits occurs
AHEARV		misfire frequency at which other functions will be stopped
AHEKA		misfire frequency at which fuel cutoff occurs
AHEKS		misfire frequency at which catalyst damage occurs
AHEKS1		misfire frequency at which catalyst damage occurs during first interval
AZYTIAB		maximum number of cylinder with ti- cut off at which catalyst damage occurs
CDTMD		Code word tester: misfire, multiple
CDTMD00		Code word tester: misfire cyl. 0
CDTMD01		Code word tester: misfire cyl. 1
CDTMD02		Code word tester: misfire cylinder 2
CDTMD03		Code word tester: misfire cylinder 3
CDTMD04		Code word tester: misfire cylinder 4
CDTMD05		Code word tester: misfire cylinder 5
CDTMD06		Code word tester: misfire cylinder 6
CDTMD07		Code word tester: misfire cylinder 7
CDTMD08		Code word tester: misfire cylinder 8
CDTMD09		Code word tester: misfire cylinder 9
CDTMD10		Code word tester: misfire cylinder 10
CDTMD11		Code word tester: misfire cylinder 11
CWDMDE		code word for EOBD-application DMDMIL (healing without window overlap)
FAINTEN		number of interval for enabling ti - cutoff
FASKIV1		factor for increasing the 1. cat-interval, misfire detection
MILANTI		MIL is on during ti turn-off in 1. dcy
TMASKIV1		temp. threshold for increasing 1. cat-interval, misfire detection
TMWUC		engine temperature threshold for fulfilment "warm up cycle"

### FB DMDMIL 3.60 Detailed description of function

In block diagrams fault type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by entering the entire status word of the fault path into the central diagnosis management DFPM. The bits E\_xyz, Z\_xyz, B\_mxyz etc. are contents of this status word. For error and cycle flags of external fault paths, which occur as inputs access methods, are available which read these informations directly from the fault path status managed in the DFPM.



For each fault path the following values are defined:

Status fault path xyz:       sfpxyz  
Error flag xyz:            E\_xyz (bit 0 in sfpxyz)  
Cycle flag xyz:            Z\_xyz (bit 1 in sfpxyz)  
Fault type xyz:            TYP\_xyz  
                          B\_mxyz  
                          B\_mxyz  
                          B\_sxyz  
                          B\_nxyz  
Clear fault path:         B\_clxyz  
Default value active:     B\_bkxyz  
Fault path code xyz:      CDTxyz  
Fault class xyz:         CLAxzy  
Fault intensity xyz:      TSFxyz  
CARB code xyz:          CDCxyz  
Table of ambient cond. xyz: FFTxyz  
Fault index xyz:         DFPxyz

The following fault paths are defined in this function definition:

MD = Misfires, total fault (multiple)  
MD01 = Misfires, ignition 1  
MD02 = Misfires, ignition 2  
MD03 = Misfires, ignition 3  
MD04 = Misfires, ignition 4  
MD05 = Misfires, ignition 5  
MD06 = Misfires, ignition 6  
MD07 = Misfires, ignition 7  
MD08 = Misfires, ignition 8  
MD09 = Misfires, ignition 9  
MD10 = Misfires, ignition 10  
MD11 = Misfires, ignition 11  
MD12 = Misfires, ignition 12

Fault memory relevant values of the function DMDMIL are assigned to the function-oriented selection of the function DFPM\_DMDMIL.

Precondition for the understanding of the misfire fault treatment is the FDEF %DFPM for the general fault treatment.

#### 1. Reaching of the misfire rate

Corresponding to the OBDII legislation of the CARB a distinction must be made between "exhaust gas relevant" misfires after start and while driving (misfires cause the exhaust emission standard to be exceeded by a factor of 1.5) and "cat. damaging" misfires (CAT is endangered).

##### 1.1 Exhaust gas relevant misfires

For the detection of exhaust gas relevant misfires the number of misfires which have occurred within an interval of 1000 crankshaft revolutions (KWU) are relevant. If the number of occurring misfires during this interval is so high that the exhaust emission standard is exceeded by a factor of 1.5, then the exhaust gas relevant misfire rate has been reached resp. exceeded.

An interval counter ivzabg counts the combustions during which the misfire detection and the statistical evaluation are active (B\_milstp=0). When reaching the maximum value of 1000 KWU (complies to 500 \* SY\_ZYLZA combustions) the interval counter ivzabg is reset.

If a misfire is detected during a combustion the total fault counter fزابg and the fault counters of the misfiring cylinders fزابg\_zzyl are increased by 1. The fault counters are reset at the end of the 1000 KWU interval.

Exhaust gas relevant misfires after start:

If the total fault counter fزابg exceeds the threshold value AHEAGWS at the end of the first interval after start, then exhaust gas relevant misfires exist after start and a fault entry is performed.

Exhaust gas relevant misfires while driving:

If the threshold value AHEAGW is in total exceeded 4 times by the total fault counter fزابg during the dcy (as from the 2. interval) then exhaust gas relevant misfires exist during the driving cycle and a fault entry is performed.

##### 1.2 Catalyst damaging misfires

For the detection of catalyst damaging misfires the number of misfires which have occurred during an interval of 200 KWU are relevant. If the number of misfires occurring during this interval is so high that the catalyst is endangered, then the catalyst damaging misfire rate has been reached resp. exceeded.

The first interval after start can be increased up to 1000 KWU via the factor FASKIV1, if the engine temperature tmot after start does not lie above the threshold TMASKIV1 (tmot is measured at the first calculating step of DMD). Since the catalyst is not at operating temperature when the engine is cold, no catalyst damage due to misfires can occur during the first 1000 KWU after start.

An interval counter ivzkat counts the combustions during which the misfire detection and the statistical evaluation are active (so B\_milstp=0). When reaching the maximum value of 200 KWU (complies to 100 \* SY\_ZYLZA combustions) the interval counter ivzkat is reset.



If a misfire is detected during a combustion the total fault counter `fzkats`, the total fault counters `fzkats1` and `fzkats2`, which are each assigned to a bank on separate exhaust systems, and the fault counters of the misfiring cylinders `fzkat_zzyl` are increased by the value `kswf`. `kswf` is calculated from the map `KFKSWF` over load and engine speed and it contains values which are weighted according to catalyst damage (large value with high engine speed and high load). The fault counters are reset at the end of the 200 KWU interval. As soon as one of the total fault counters `fzkats1` or `fzkats2` exceeds the threshold value `AHEKS` (or `AHEKS1` in the 1. prolonged interval), catalyst damaging misfires exist and a fault entry is made (not only at the end of the interval). As long as catalyst damaging misfires exist, i.e. `fzkats1` or `fzkats2` > `AHEKS`, the bit `B.blkmd` is set and the MIL flashes. Also the Bit `B.mdkat` is set. With this Bit other functions can be deactivated during cat. damaging misfiring. If at the end of the interval `fzkats1` and `fzkats2` < `AHEKS`, the bit `B.blkmd` and `B.mdkat` is reset and the MIL no longer flashes. In case of catalyst damage it is also indicated in the status byte `flgkat.w` as to which cylinder has catalyst damaging misfires. `flgkat.w` resp. the respective bit is reset after an interval without threshold value exceeding, however, remains set in case of ti cut-off.

#### Ti cut-off:

After `AINTKA` intervals, during which `fzkat_zzyl` > `AHEKA` and `fzkats1` or `fzkats2` > `AHEKS`, the injection of the respective cylinder is switched off, if the max. no. of cutout cylinders is not already given and if there is no injector fault at open valve. In case of 2 ECU's the injector fault with open valve (`E.ev_zzyl` with `B.mnev_zzyl`) of the master-ECU (`B.master=1`) is stored in the bit `B.mnevzzylt` and transferred via CAN to the slave-ECU. There it is evaluated as `B.mnevzzylc`. For this the cyl. fault counters `fzkat_zzyl` are compared with the threshold `AHEKA` in case of detected cat. misfires (`fzkats1` or `fzkats2` > `AHEKS`). If the threshold is exceeded the counter `aint_zzyl` is incremented, with `fzkats1` < `AHEKS` and `fzkats2` < `AHEKS` it is decremented. If `aint_zzyl` is greater than `AINTKA` - as long as no `AZITIAB`-cylinders have yet been switched off and also no injector fault with open valve yet exists at the misfiring cylinder (`E.evxx`, fault type `B.mnevxx`) - then the bit of the respective cylinder in `flgtiab` and the bit `B.tiab_zzyl` are set to 1, the injection is switched off and the counter of the cutout cylinder `azycnt` is increased by 1. In case of 2 ECU's (`SY_2SG=1`) the bits `B.tiab_zzyl` are stored in the 2 bytes `flgtiab` and `flgtiabt` where `flgtiab` corresponds to the slave-ECU (`B.master=0`) and `flgtiabt` corresponds to the master-ECU (`B.master=1`). `flgtiabt` is send via CAN to the master-ECU. For `AZITIAB` = 0 no cut-off takes place. The condition for ti-cut-off is checked immediately as `fzkats1/2` increases the threshold `AHEKS` (and not at the end of the intervall). The cut-off remains active until a new engine start is performed. During a deactivation the cylinder-individual fault counters of the cutout cylinders are no longer increased. If all misfiring cylinders have been cutout, misfires are no longer counted, `fzkats1` and `fzkats2` < `AHEKS`, and dependent on the `MILANTI` the MIL will change from flashing to off (`MILANTI=0`) or from flashing to on (`MILANTI=1`) in the 1. dcy and in the 2. dcy it will change from flashing to on. For the switch-off of the Lambda control see `%LREB` and for the switch-off of the full-load enrichment see `%RLASE`.

#### 1.3 Occurrence of misfire faults

If the misfire rate for a fault entry has been reached or exceeded, the bit `E.md` and the trigger `B.spl` are set. If no misfire window yet exists, then the temporary misfire window is decreased by the permitted tolerance and stored as final misfire window (see 3.). A cylinder identification is performed if `B.synph=1`. A cylinder is detected to be misfiring if the cylinder-individual fault counter `fzabg_zzyl` exceeds the mean value `fzabgs/SY_ZYLZA` or if the cylinder-individual fault counter `fzkat_zzyl` exceeds the mean value `fzkats/SY_ZYLZA`. The bit `E.md_zzyl` is also set for the misfiring cylinders. The bits `E.md` and `E.md_zzyl` remain set until the end of the first faultless dcy with window overlap.

Misfire faults are debounced via 2 driving cycles (dcy), that means if misfire faults occur for the first time a non-debounced fault entry is performed (pending fault memory entry).

- If misfire faults occur again during the next dcy, then the fault entry is debounced and the error lamp (MIL) comes on (resp. flashes in case of catalyst damaging misfires).
- If no misfire faults occur during a subsequent dcy and the dcy took place under similar conditions (regarding load, engine speed and engine temperature, window overlap s. 3.), then the pending fault memory entry is cleared (resp. remains visible to the customer service) and the misfire window is reset.
- If no window overlap is achieved during the subsequent dcy, then the pending fault memory entry is cleared after 80 dcy.

If a debounced fault entry exists and the MIL is on, then the MIL goes out after 3 faultless dcy with window overlap and the fault entry is cleared 40 warm-up cycles (wuc) later.

#### 1.4 Misfire rate for the switch-off of other ECU functions (e. g. `BBLDR`)

With exh. misfires, e.g. at 1000 rpm, the bit `E.md` is only set after 4 min. (4 \* 1000 KWU).

In order to enable a quicker reaction to misfires in other functions there is another counter, which counts the misfire rate in an interval of 60 KWU. If a certain misfire rate, e.g. 5% is exceeded within this interval, then the bit `B.mdarv` is set.

An interval counter `ivzarv` counts the combustions during which the misfire detection and the statistical evaluation are active (i.e. `B.milstp=0`). Once the maximum value of 60 KW revolutions has been reached (complies to 30 \* `SY_ZYLZA` combustions), the interval counter `ivzarv` is reset.

If misfiring is detected during a combustion, then the fault counter `fzarv` is increased by 1. At the end of the 60 KWU interval the fault counter is reset.

If the counter `fzarv` exceeds the value `ahearv_w` at the end of the interval, then the bit `B.mdarv` is set. If the threshold is undershot at the end of the interval, then the bit `B.mdarv` is reset. `ahearv_w` is set to `AHEARV` with the following 2 exclusions: `AHEARV[%]` < `AHEAGW[%]` then `ahearv_w` is set to `AHEAGW[%]`, `AHEARV[%]` > 10% then `ahearv_w` is limited to 10%. This is made because of other function may not be permanent deactivated without fault code entry.

#### 2. Setting and resetting of various state conditions

Faultless dcy:

`B.dcy` = 1 and  
`ivzabg` at least once = 0 (>1000 KWU) and  
`B.spl` = 0 (threshold value was not exceeded)

Fault trigger `B.spl`:

If `fzkats1` or `fzkats2` > `AHEKS` or at the end of the 1000 KWU interval `fzabgs` > `AHEAGW` / `AHEAGWS` (during 1. interval), then the trigger `B.spl` is set. `B.spl` remains set until the after-run has ended.

**Healing trigger B<sub>sp2</sub>:**

If the dcy was faultless and the window overlap was fulfilled, i.e.  $BF \geq AF$ , the healing trigger B<sub>sp2</sub> is set in the after-run. B<sub>sp2</sub> is set until the end of the after-run. Once B<sub>sp2</sub> was set 3 times the MIL will go out and the AF is reset. For EOBD-projects the healing trigger B<sub>sp2</sub> can be performed without checking window overlap (CWDME=1).

**Cycle bits Z<sub>md</sub>, Z<sub>md</sub>.zzyl:**

The cycle bits Z<sub>md</sub>, Z<sub>md</sub>.zzyl are set after the first 1000 KWU interval has elapsed or in case a fault already occurs beforehand, that means  $fzkats1$  or  $fzkats2 > AHEKS$ . The cycle bits remain set until the after-run has ended.

**Error bits E<sub>md</sub>, E<sub>md</sub>.zzyl:**

The error bits E<sub>md</sub>, E<sub>md</sub>.zzyl are set, if the no. of misfires for a fault entry has been reached ( $fzkats1$  or  $fzkats2 > AHEKS$ ;  $fzabgs > AHEAGWS$  in the 1. interval;  $fzabgs > AHEAGW$  at least 4x during the dcy). The error bits E<sub>md</sub>, E<sub>md</sub>.zzyl are reset at the end of a faultless dcy with window overlap.

**Clear bits B<sub>clmd</sub>, B<sub>clmd</sub>{SY\_ZYLZA}:**

By setting of the clear bits (call-up of the clearing process) all fault counters, interval counters, error and cycle bits, counters of the ti cut-off and the operating windows are reset.

**Operating window BF:**

The operating window BF is updated during the entire dcy if there is no cutout (s. %DMDSTP) and it begins with starting values.

**Temporary misfire window AFT:**

The temporary misfire window AFT is updated with each occurring misfire and it is reset at the end of the 1000 KWU intervals (reset to the starting values).

**Misfire window AF:**

After misfire faults have occurred for the first time the temporary misfire window is decreased by the permitted tolerance (20% load, 375 rpm) and stored in the final misfire window. The misfire window is reset in the after-run after 3 faultless dcy with window overlap at debounced entry or after 1 faultless dcy with window overlap or after 80 dcy without window overlap at non-debounced fault entry.

**Fault memory entry:**

Non-debounced entry: when the first misfire faults occur  
Debounced entry: when misfire faults occur during the 2. dcy or during a subsequent dcy, if a non-debounced misfire fault already exists.

Clearing of a non-debounced fault memory entry: after a faultless dcy with window overlap or after 80 dcy without window overlap (still remains visible to customer service)

Clearing of a debounced fault memory entry: 40 wuc after MIL turned off (still remains visible to customer service)

Fault type: with cat. faults: B<sub>mxflr</sub>, with exh. faults while driving: B<sub>mnflr</sub>, with exh. faults after start: B<sub>npflr</sub>.

The fault type B<sub>mxflr</sub> is not overwritten by any other fault type, the fault type B<sub>mnflr</sub> is not overwritten by the fault type B<sub>npflr</sub>.

**Output scantool (s. %TCSORT):**

- If only one cylinder is identified to be misfiring, then only the fault entry of the corresponding cylinder is output. The output of the total fault (E<sub>md</sub>) is then suppressed.
- If several cylinders are identified to be misfiring, then in any case the total fault is output as 'multiple fault'. The additional output of the cylinder-individual faults can be suppressed dependent on the data entered in TCSORT.

**B<sub>blkmd</sub>:**

The bit B<sub>blkmd</sub> directly triggers the flashing of the MIL. It is set if  $fzkats1 > AHEKS$  or  $fzkats2 > AHEKS$ . If this condition is no longer given at the end of the interval, then the bit B<sub>blkmd</sub> is reset.

**B<sub>mdkat</sub>:**

The bit B<sub>mdkat</sub> is set if  $fzkats1 > AHEKS$  or  $fzkats2 > AHEKS$ . If this condition is no longer given at the end of the interval then the Bit B<sub>mdkat</sub> is reset. With the Bit B<sub>mdkat</sub> other functions can be deactivated during cat. damaging misfiring.

**B<sub>milmd</sub>:**

The bit B<sub>milmd</sub> turns on the MIL directly, if ti cut-off exists and if MILANTI=1 (relevant only during 1.dcy, with pending fault memory entry)

**MIL:**

The MIL comes on during the 2. dcy with misfire faults and it goes out again after 3 faultless dcy with window overlap. In addition the MIL flashes, if the threshold for cat. misfires AHEKS is exceeded by  $fzkats1$  or  $fzkats2$ . During the first dcy with misfire faults the MIL flashes with cat. faults and it goes out again, if the cat. faults no longer exist. In the 2. and in the subsequent dcy with misfire faults the MIL flashes if cat. faults exist and it stays on if cat. faults no longer exist. With ti cut-off the MIL may also be on during the 1. dcy if MILANTI=1, although catalyst damage is no longer given.

**DFPM:**

DLC: is decremented if B<sub>wuc</sub>=1 in case of debounced error or B<sub>dcy</sub>=1 in case of pending error  
FLC: is decremented if B<sub>sp1</sub>=1 & Z<sub>md</sub>=1  
HLC: is decremented if B<sub>sp2</sub>=1 & Z<sub>md</sub>=1

**B<sub>mdarv</sub>:**

If a certain misfire rate is exceeded at the end of the 60 KWU interval, then B<sub>mdarv</sub> is set. If the misfire rate is undershot again, then B<sub>mdarv</sub> is reset again.

**flgtiab/t, B<sub>tiab</sub>.zzyl:**

With ti cut-off the bit B<sub>tiab</sub>.zzyl and the corresponding bit in flgtiab is set. In case of 2 ECU's the bits are stored in flgtiab (slave-ECU) and flgtiabt (master-ECU).

**flgkat\_w:**

With catalyst damage the corresponding bit of the misfiring cylinder in flgkat\_w is set.

### 3. Definition of operating windows

In order to turn off the MIL it is necessary to store the operating ranges load, engine speed and engine temperature, in which faults have occurred resp. have been detected.

For this the following operating windows are needed:

BF - operating window, is updated constantly (every 200ms) during the entire driving cycle, if DMD is active  
AFT - temporary misfire window, is updated with each misfire  
AF - final misfire window, taken over during the fault memory entry from the AFT

A window is defined by 5 parameters:

nmn = lowest engine speed            nmx = highest engine speed  
rlmn = lowest load                    rlmx = highest load  
and the warming up status (tmot < or > TMWUC)

#### 3.1 Starting values for range windows BF, AFT and AF:

bfnmn = FF (hex),            bfnmx = 0  
aftnmn = FF (hex),            aftnmx = 0  
afnmn = FF (hex),            afnmx = 0

bfrlmn = FF (hex), bfrlmx = 0  
aftrlmn = FF (hex), aftrlmx = 0  
afrlmn = FF (hex), afrlmx = 0

B\_bfwrn = 0,                    B\_bfklt = 0  
B\_aftwrn = 0,                    B\_aftklt = 0  
B\_afwrn = 0,                    B\_afklt = 0

#### 3.2 Operating window BF

This window is set to starting values at engine start. The updating is performed at active misfire detection (B\_milstp = 0, see %DMDSTP) during the entire engine cycle (until ignition off), independent of whether faults are detected or not.

Correction of the operating window (in the 200ms grid):

If nmot > bfnmx, then bfnmx = nmot,  
if nmot < bfnmn, then bfnmn = nmot,  
if rl > bfrlmx, then bfrlmx = rl,  
if rl < bfrlmn, then bfrlmn = rl,  
if tmot > TMWUC, then B\_bfwrn = 1,  
if tmot < TMWUC, then B\_bfklt = 1

#### 3.3 Misfire windows AF and AFT

Generally speaking the misfire window shows that range, in which misfires have occurred. A distinction is made here between a temporary and a final misfire window.

Updating of the temporary misfire window AFT:

The temporary AFT is updated with each (individual) misfire that is detected:

If n > aftnmx, then aftnmx = n,  
if n < aftnmn, then aftnmn = n,  
if rl > aftrlmx, then aftrlmx = rl,  
if rl < aftrlmn, then aftrlmn = rl,  
if tmot > TMWUC, then B\_aftwrn = 1,  
if tmot < TMWUC, then B\_aftklt = 1,  
(with B\_aftwrn = B\_aftklt = 1, then misfires first with tmot < TMWUC and thereafter with tmot > TMWUC)

After every 1000 KWU the AFT is reset to the starting values.

Updating of the final misfire window AF:

The contents of the temporary misfire window is decreased by the legally permitted tolerance and stored in the final misfire window during the first fault memory entry (exhaust gas resp. catalyst damaging faults).

afnmx = aftnmx - 375/2 rpm (\*)  
afnmn = aftnmn + 375/2 rpm (\*)

The misfire window is limited to idle speed, that means afnmn > NLLM(tmot).

(In case of misfire during idle speed decreases shortly. Therefore afnmn can be < NLLM(tmot). Healing is than only with 80 wuc possible in case of pending fault code because window overlap cannot be reached. NLLM comes from %LLR).

if afnmx < afnmn, then afnmx = afnmn = (afnmx+afnmn)/2

(\*): by the quantization of nmot with 40 rpm here 320/2 = 160 rpm are realized

The speed tolerance is given in AFNTOL. In older VS100-Versions AFNTOL can be applied.

CAUTION: AFNTOL must be 160 rpm !!!

afrlmx = 0.90 \* aftrlmx

afrlmn = 1.10 \* aftrlmn.

if afrlmx < afrlmn, then afrlmx = afrlmn = (afrlmx+afrlmn)/2

The temperature status is adopted without change

B\_afklt = B\_aftklt

B\_afwrn = B\_aftwrn

#### 3.4 Checking of the window overlap

Similar operating conditions are given, if

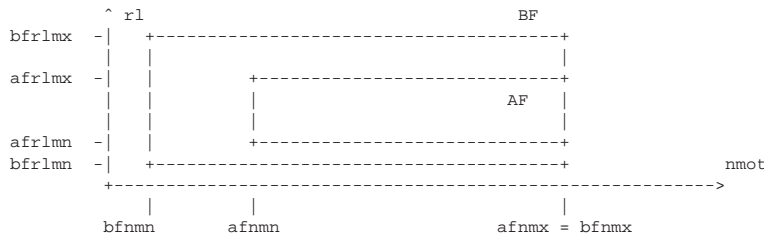
1. B\_bfwrn = B\_afwrn, if B\_afwrn = 1
2. B\_bfklt = B\_afklt, if B\_afklt = 1
3. bfrlmx >= afrlmx            and bfrlmn <= afrlmn
4. bfnmx >= afnmx            and bfnmn <= afnmn

that means the window condition is fulfilled if the operating window overlaps the misfire window (AF is included in the BF).



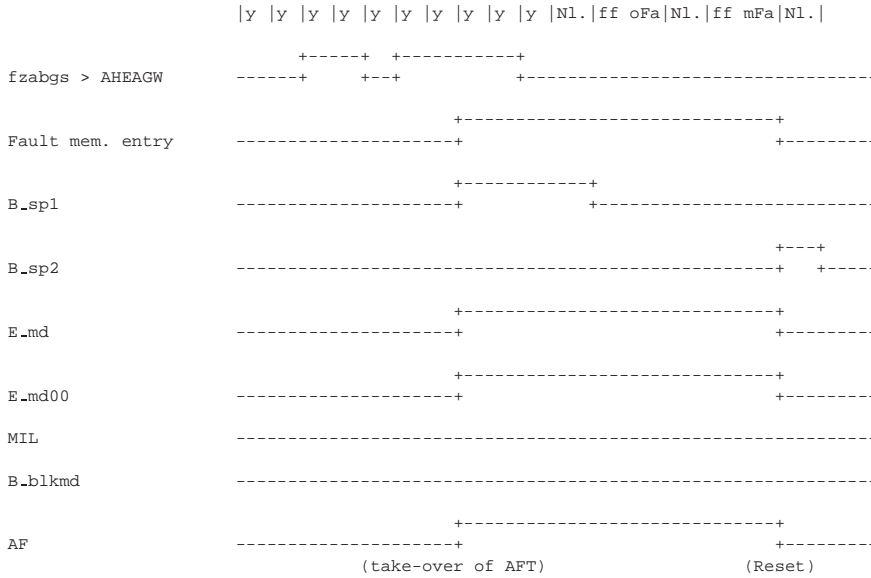


Example for a fulfilled window condition resp. window overlap:



#### 4. Flow charts

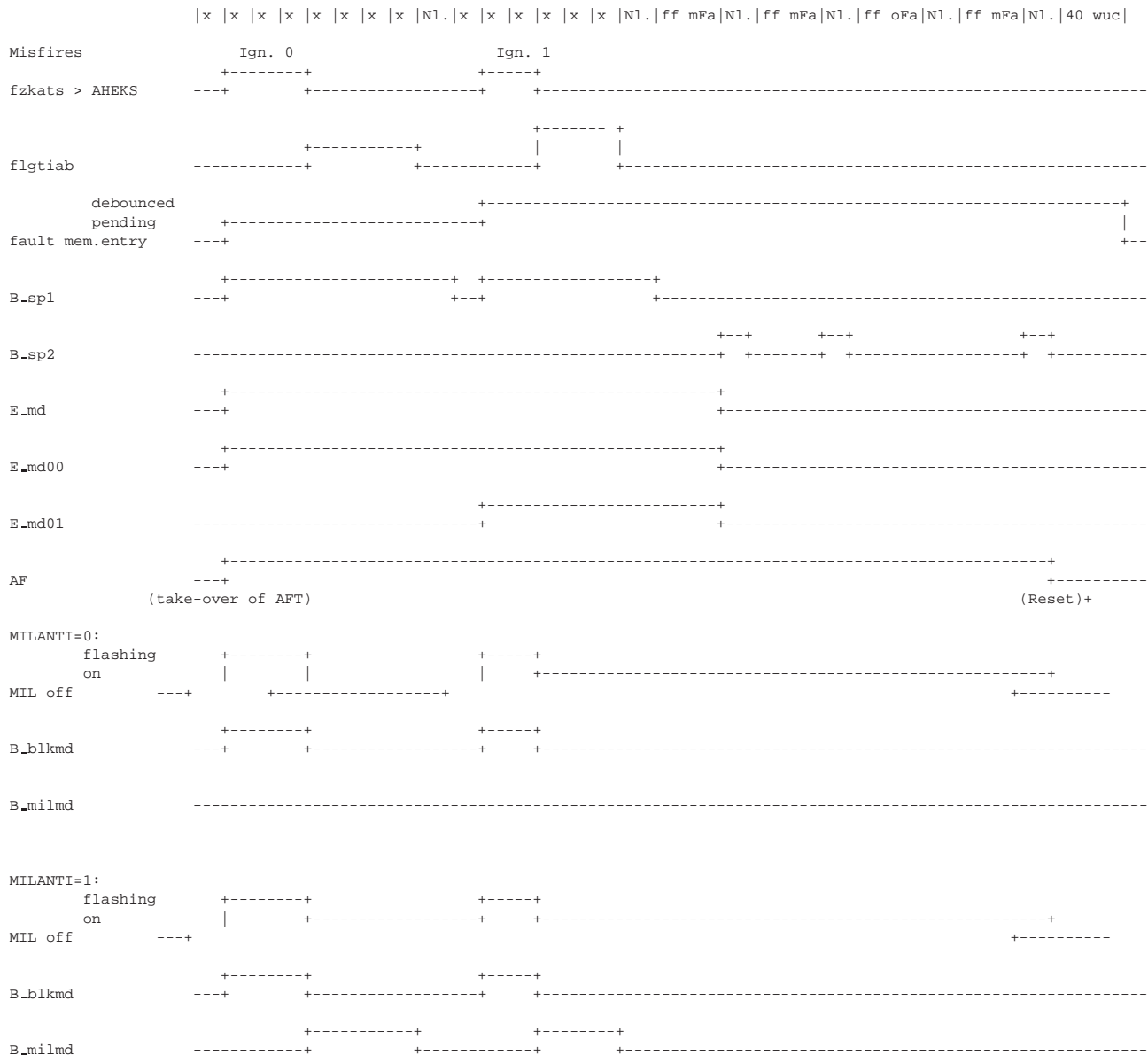
##### 4.1 Misfire in only 1 dcy



y: 1000 KWU interval  
Nl.: after-run  
ff mFa: faultless dcy with window overlap  
ff oFa: faultless dcy without window overlap

##### 4.2 Misfires in 2 dcy, exhaust gas relevant, during the dcy





x: 200 KWU interval  
Nl.: after-run  
ff mFa: faultless dcy with window overlap  
ff oFa: faultless dcy without window overlap  
wuc: warm-up cycle

### APP DMDMIL 3.60 Application hint

1. Classes of the fault types:  
CLAMD = 2  
CLAMD{SY\_ZYLZA} = 2  
ATTENTION: Since the flashing of the MIL is triggered directly, the class should not be changed.  
Otherwise the MIL will possibly flash without a fault entry having been made.
2. Quicktest of the function DMDMIL  
For a quick check of the function it is possible to measure the interval counters ivzabg and ivzkat as well as the fault counters fzkabgs and fzkats. The interval counters must count the combustions, during B.milstp=0. The fault counters must count each individual misfire that was detected (weighted in fzkats with kswf).
3. ATTENTION: In case of MILANTI=1 it is possible, that during a temp. error (during 1. dcy) the MIL is on but there is only in Mode 7 a fault code entry visible !!!  
To agree with the legislation MILANTI should be 0.

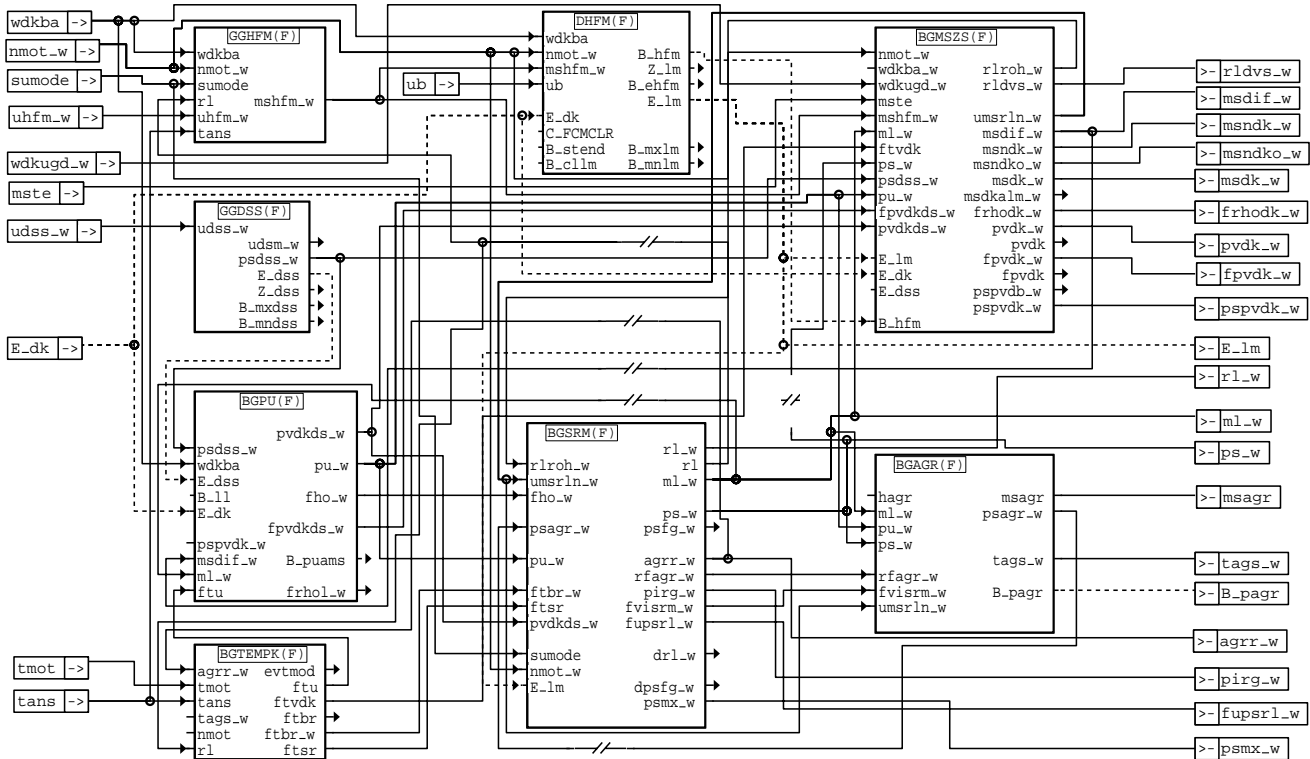
AHEARV: should correspond to 5% misfire during 60 crankshaft rotations.

AFNTOL: must be 160 U/min !!!



## EGFE 6.10 Input variables for charging detection

### FDEF EGFE 6.10 Function definition



egfe-egfe

### ABK EGFE 6.10 Abbreviations

Variable	Source	Type	Description
AGRR_W	EGFE	AUS	exhaust gas recirculation rate
B_CLLM	EGFE	LOK	condition: clear fault path main load sensor
B_EHFM	EGFE	LOK	condition: HFM error (without debounce)
B_HFM	EGFE	LOK	Condition: HFM ready to measure
B_LL	EGFE	LOK	Condition idle
B_MNDSS	EGFE	LOK	Condition: min-error manifold pressure sensor
B_MNLM	EGFE	LOK	Condition: min-error main load sensor
B_MXDSS	EGFE	LOK	Condition: max-error manifold pressure sensor
B_MXLM	EGFE	LOK	Condition: max-error main load sensor
B_PAGR	EGFE	AUS	egr calculation disabled
B_PUAMS	EGFE	LOK	Condition ambient pressure adaptation by comparing mshfm/msdk
B_STEND	EGFE	LOK	condition end of start
C_FCMCLR	EGFE	LOK	system state: reset fault memory
DPSFG_W	EGFE	LOK	delta fresh air partial pressure in manifold
DRL_W	EGFE	LOK	charge change (Word)
EVTMOD	EGFE	LOK	modelled temperature at inlet valve
E_DK	DDVE	EIN	Error flag: throttle position sensor
E_DSS	EGFE	LOK	error flag: Manifold absolute pressure
E_LM	EGFE	AUS	Error flag: main load sensor
FHO_W	EGFE	LOK	correction factor: altitude
FPVDK	EGFE	LOK	correction factor for pressure upstreams throttle
FPVDKS_W	EGFE	LOK	Factor pressure in front of throttle valve of pressure sensor (word)
FPVDK_W	EGFE	AUS	correction factor for pressure upstream of throttle valve, 16-bit
FRHODK_W	EGFE	AUS	factor correction air density for throttle valve flow f(intake air temp., altit.)
FRHOL_W	EGFE	LOK	Factor: air density f(intake air temp., altitude), 16-bit
FTBR	EGFE	LOK	factor: temperature correction in combustion chamber
FTBR_W	EGFE	LOK	factor: temperature correction in combustion chamber
FTSR	EGFE	LOK	correction factor for air temperature in the manifold
FTU	EGFE	LOK	factor: ambient temperature
FTVDK	EGFE	LOK	correction factor for temperature upstream of throttle valve
FUPSRL_W	EGFE	AUS	factor system related transformation pressure to load (16-Bit)
FVISRM_W	EGFE	LOK	integrator amplifier factor intake manifold modell
HAGR	EGFE	LOK	Stroke EGR valve
ML_W	EGFE	AUS	air mass flow filtered (Word)
MSAGR	EGFE	AUS	EGR mass flow into intake manifold
MSDIF_W	EGFE	AUS	mass flow difference mshfm_w - msdk_w
MSDKALM_W	EGFE	LOK	Mass flow over throttle (balance with HFM signal)
MSDK_W	EGFE	AUS	air-mass flow through throttle valve



Variable	Source	Type	Description
MSHFM_W	EGFE	LOK	air-mass flow HFM
MSNDKO_W	EGFE	AUS	norm leakage air mass flow through throttle blade
MSNDK_W	EGFE	AUS	standardised air mass flow through throttle valve
MSTE	BGTEV	EIN	mass flow purge control into the manifold
NMOT	EGFE	LOK	engine speed
NMOT_W	SWADAP	EIN	engine speed
PIRG_W	EGFE	AUS	partial pressure residual exhaust gas internal EGR (16-Bit)
PSAGR_W	EGFE	LOK	partial pressure EGR
PSDSS_W	EGFE	LOK	Intake manifold pressure measured with pressure sensor at manifold (DS-S)
PSFG_W	EGFE	LOK	fresh air partial pressure in manifold
PSMX_W	EGFE	AUS	maximum manifold pressure limitation for modeled manifold pressure
PSPVDB_W	EGFE	LOK	quotient:int.manif.press.divided by press.upstream of throttle valve limit
PSPVDK_W	EGFE	AUS	quotient: int.manif.pressure divided by pressure upstream of throttle valve
PS_W	EGFE	AUS	intake manifold pressure (absolute) (Word)
PU_W	EGFE	LOK	Ambient pressure
PVDK	EGFE	LOK	pressure in front of throttle
PVDKDS_W	EGFE	LOK	Pressure in front of throttle valve of pressure sensor (word)
PVDK_W	EGFE	AUS	pressure upstream of throttle valve, 16-bit
RFAGR_W	EGFE	LOK	relative load by external exhaust gas reduction
RL	EGFE	LOK	relative air charge
RLDVS_W	EGFE	AUS	relative air charge through throttle valves on intake manifold
RLROH_W	EGFE	LOK	relative air charge flowing into intake manifold
RL_W	EGFE	AUS	relative air charge (Word)
SUMODE	SU	EIN	status of the intake manifold switch over
TAGS_W	EGFE	AUS	EGR temperature on introduction into intake manifold
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
UB	SWADAP	EIN	battery voltage
UDSM_W	EGFE	LOK	Pressure sensor voltage averaged via a segment (word)
UDSS_W		EIN	Voltage pressure sensor manifold pressure (word)
UHFM_W		EIN	HFM voltage
UMSRLN_W	EGFE	LOK	calculation factor load to mass flow
WDKBA	GGDVE	EIN	throttle angle
WDKBA_W	EGFE	LOK	throttle angle with respect to lower mechanical stop
WDKUGD_W	BGMSZS	EIN	Throttle valve angle during which 95% charge is reached
Z_DSS	EGFE	LOK	cycle flag: Manifold absolute pressure
Z_LM	EGFE	LOK	cycle flag:load determination LMM/HLM/HFM

### FW EGFE 6.10 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

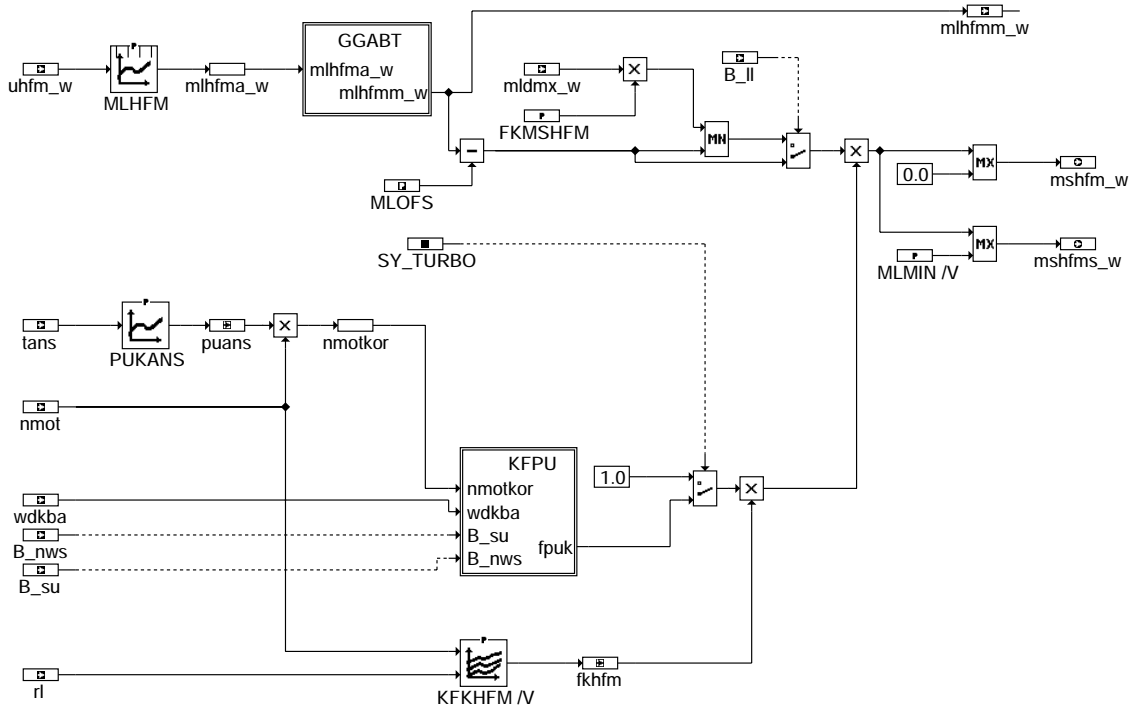
## FB EGFE 6.10 Detailed description of function

### APP EGFE 6.10 Application hint

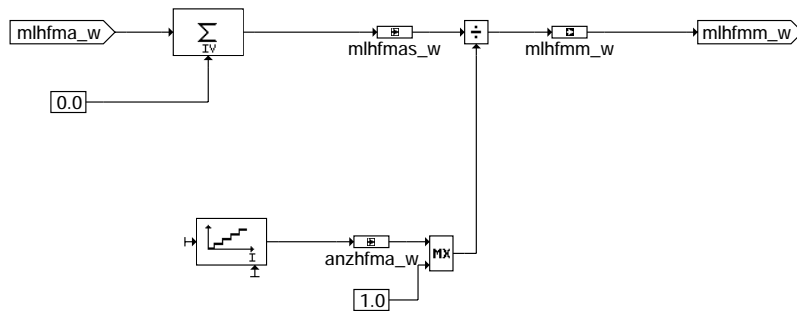
## GGHFM 57.30 Sensor signal, hot-film air-mass meter

### FDEF GGHFM 57.30 Function definition

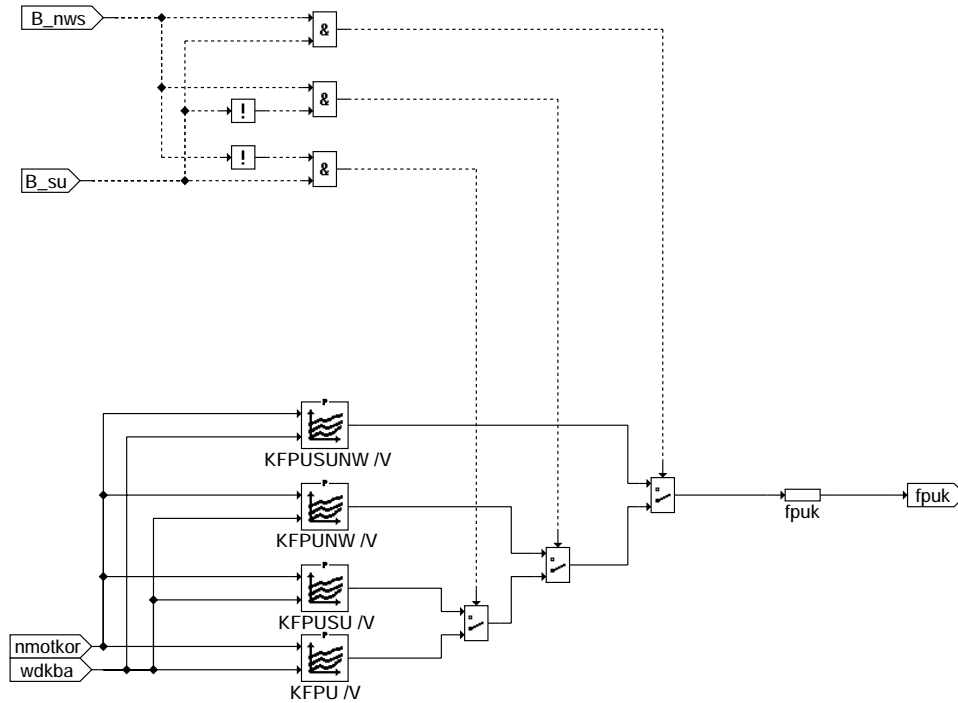
Source: GGHFM 57.20



#### gghfm-gghfm



#### gghfm-ggab



gghfm-kfpu

### ABK GGHFM 57.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FKMSHFM			FW	Correction factor for MIN selection with mshfm
KFKHFM	NMOT	RL	KF	HFM-correction characteristic map
KFPU	NMOTKOR	WDKBA	KF	pulsation characteristic map
KFPUNW	NMOTKOR	WDKBA	KF	pulsation map for camshaft control switch over
KFPUSU	NMOTKOR	WDKBA	KF	pulsation characteristic map at active variable intake system by smode=1
KFPUSUNW	NMOTKOR	WDKBA	KF	pulsation characteristic map at active variable intake system and camshaft cont.
MLHFM	UHFM_W		KL	air-mass meter characteristic line
MLMIN			FW	Minimum HFM air mass
MLOFS			FW (REF)	offset for characteristic line of air mass flow meter HFM 5
PUKANS	TANS		KL	correction of pulsation depending on intake air temperature
SY_TURBO			SYS (REF)	system constant for exhaust-gas turbocharger

Variable	Source	Type	Description
ANZHFM_A_W	GGHFM	LOK	number of HFM samplings over one synchro
B_LL	MSF	EIN	Condition idle
B_NWS	NWS	EIN	Condition camshaft control
B_SU	SU	EIN	condition intake manifold switch-over
FKHFM	GGHFM	LOK	correction factor for HFM
FPUK	GGHFM	LOK	correction factor for HFM in pulsation range
MLDMX_W	DHFM	EIN	Maximal air mass from map KFMLDMX
MLHFMA_S_W	GGHFM	LOK	cumulative air mass over one synchro
MLHFMA_W	GGHFM	LOK	air mass scanning value of HFM 16-bit
MLHFMM_W	GGHFM	AUS	mean HFM air mass value 16-Bit
MSHFMS_W	GGHFM	AUS	air mass flow HFM (signed)
MSHFM_W	GGHFM	AUS	air-mass flow HFM
NMOT	SWADAP	EIN	engine speed
NMOTKOR	GGHFM	LOK	engine speed correction
PUANS	GGHFM	LOK	pulsation correction as a function of tans
RL	SWADAP	EIN	relative air charge
TANS	SWADAP	EIN	Intake air temperature
UHFM_W		EIN	HFM voltage
WDKBA	GGDVE	EIN	throttle angle

### FW GGHFM 57.30 Fixed Values

Parameter	Value	Description
FKMSHFM		Correction factor for MIN selection with mshfm
MLMIN		Minimum HFM air mass

gghfm-kfpu

**FB GGHFM 57.30 Detailed description of function**

The air mass sensor (HFM) is scanned every lms. The scanned voltage is first linearised (MLHFM). The characteristic contains only positive values, for further calculation of the air mass flow. For this reason, when using a HFM5 an offset (MLOFS) for the reverse flow range must be taken into account when calculating the values for MLHFM. The calculated air mass values are then added together via a segment in a memory. Once per segment, at the beginning of the charge calculation, the totalled value is arithmetically averaged via the preceding segment, i.e. it is divided by the number of scans of the last segment and then the characteristic offset MLOFS is deducted. The value is then multiplied by a pulsation correction value taken from the map KPFP. This air mass flow is delivered to the output as a 16-bit value mshfm\_w and as an 8-bit value mshfm.

**APP GGHFM 57.30 Application hint**Procedure in application:  
-----

Linearisation characteristic of the HFM

Input/check of the linearisation characteristic of the HFM

- Characteristic dependent on size and design (hybrid/sensor) of the HFM used
- HFM2: Characteristic with positive air masses and MLOFS = 0 !!
- HFM5: Use characteristic with reverse flow range, i.e. pos. and neg. air masses, and additional offset (MLOFS = 200 kg/h)
- Interpolation is the same for HFM2 and for HFM5

When using a plug-in sensor variant the characteristic must be checked in conjunction with the fitting position used.

Prerequisites for application of the pulsation map  
-----

- Adaptation of the battery voltage correction TVUB, poss. determined by way of fuel measuring
- Neutralisation of all enrichments, i.e. set pre-control to Lambda=1 (e.g. KFLF); Pulsation correction initially neutralised (set KPFP to 1); Deactivate or increase psmax limitation

Application of the pulsation map  
-----

The pulsation map is used to compensate pulsation errors of the HFM; it is not intended to correct errors in the reverse flow range.

Definition of pulsation range:

Voltage oscillation of air mass sensor HFM &lt; 0.5V

Definition of reverse range:

Voltage of air mass sensor HFM &lt; 1.0

Adaptation of the pulsation map:

- Definition of the pulsation range; poss. distribution of interpolation points of the pulsation map for better coverage of the pulsation range

In fuel systems without constant differential pressure upstream of the injection valve (e.g. RLFS), i.e. where the pressure regulator does not operate against the intake manifold pressure as a reference pressure, this must be specially guaranteed for application of the pulsation map (connection of the pressure regulator to the intake manifold).

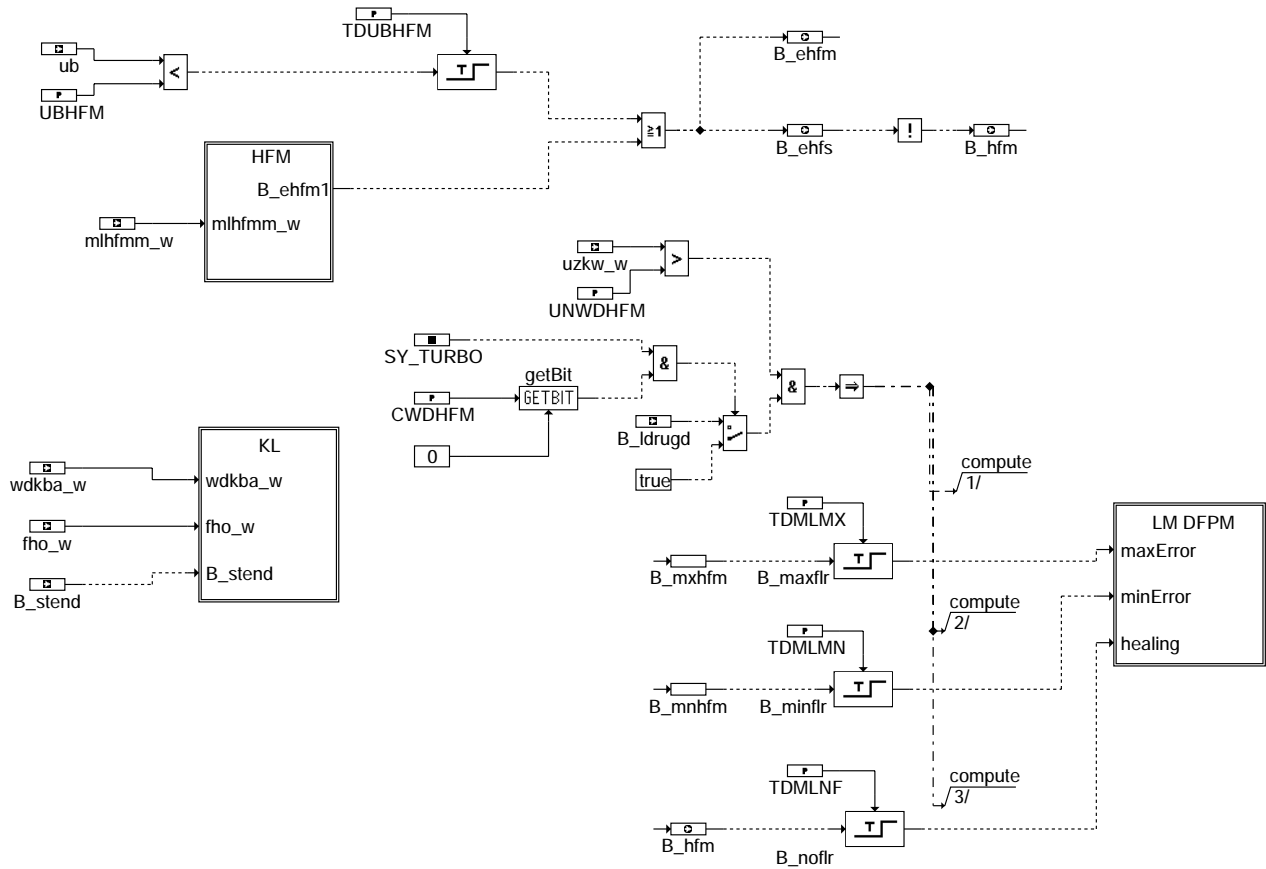
If this is not possible for technical reasons, the varying pressure differential upstream of the injection valve must be taken into account beforehand in a correction map (see note on RLFS systems).



## DHFM 63.80 Diagnosis; plausibility test hot film air flow sensor

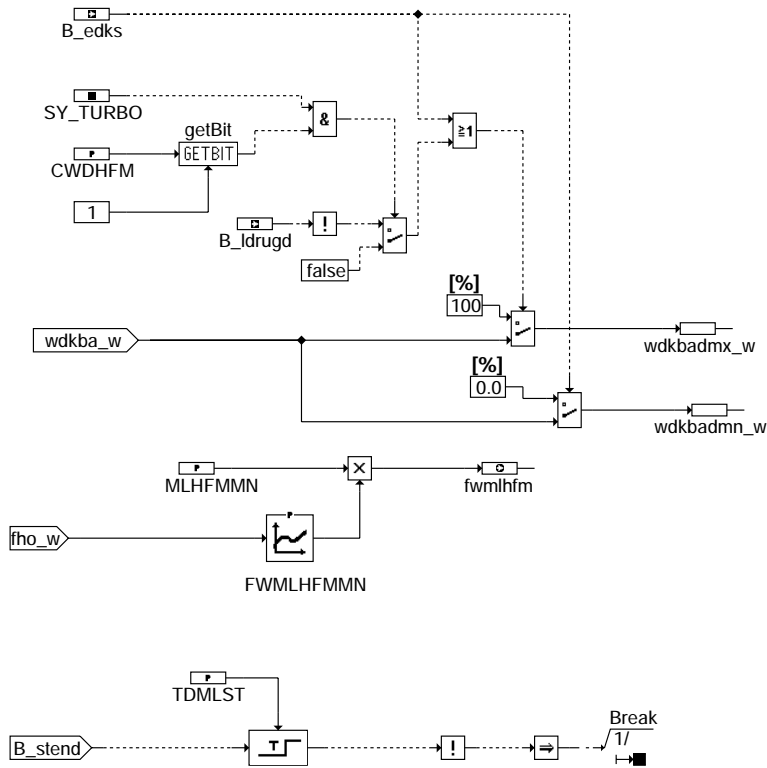
### FDEF DHFM 63.80 Function definition

Source: DHFM 63.70

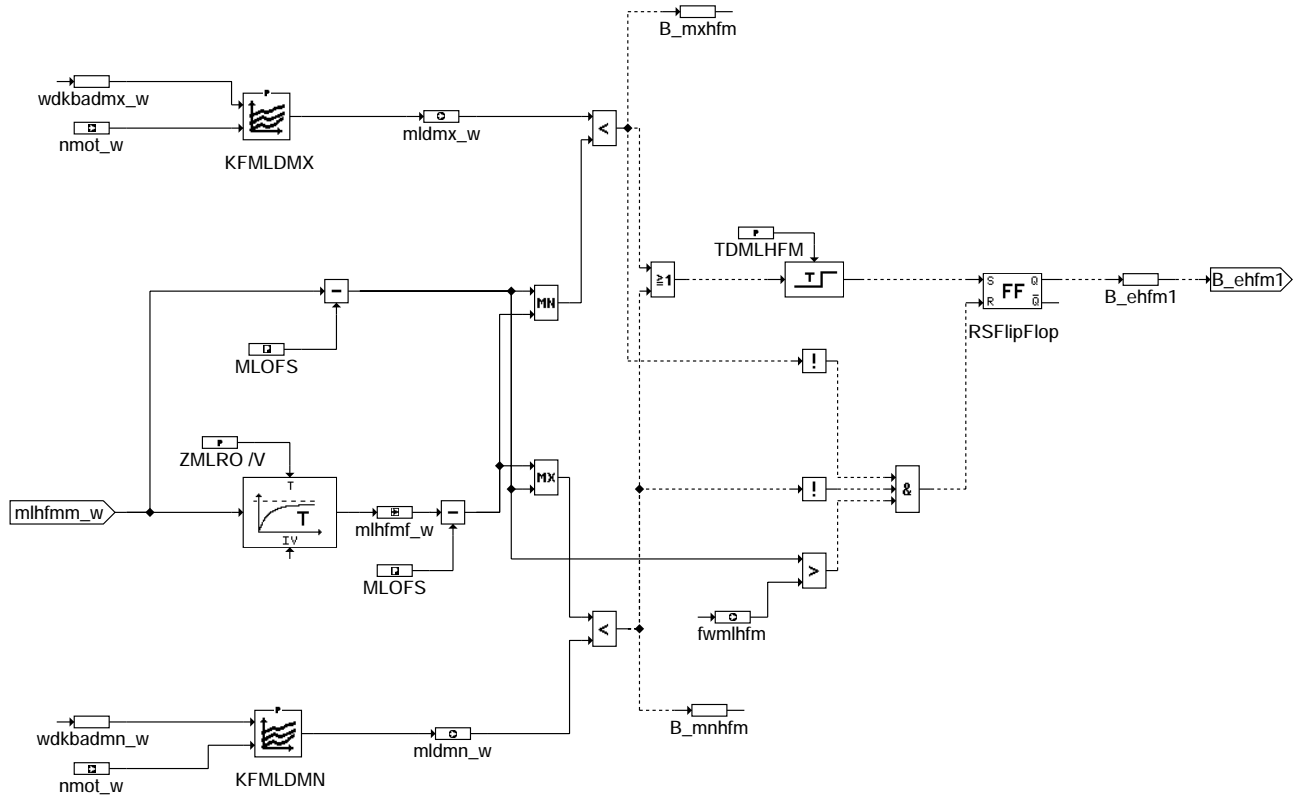


dhfm-dhfm

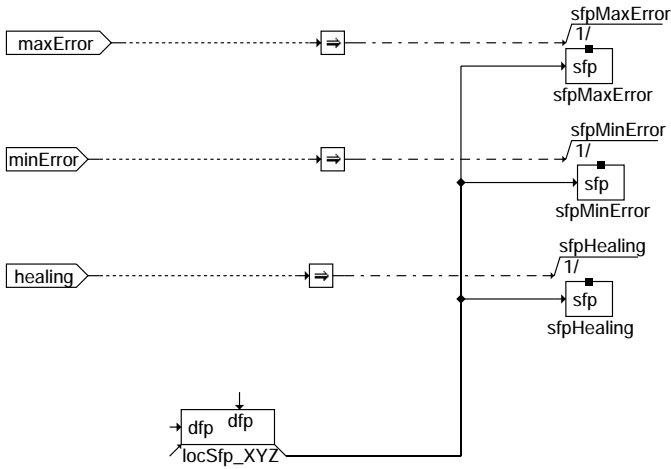
dhfm-dhfm



### dhfm-kl



### dhfm-hfm

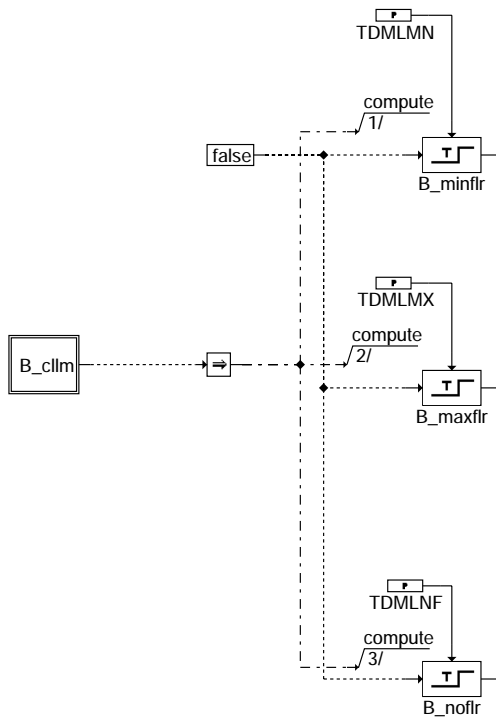


**Action Table for fault path \* in DFPM:**

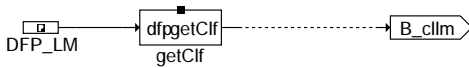
	E_*	Z_*	B_mx*	B_mn*
maxError:	S	S	S	R
minError:	S	S	R	S
Healing:	R	S	R	R

S: set R: reset

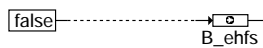
**dhfm-lm-dfpm**



**dhfm-fcmclr**



**dhfm-b-clxyz**



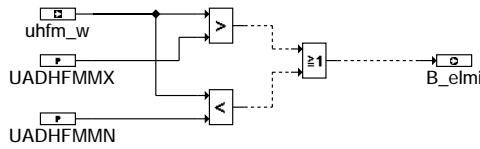
**dhfm-nachlauf**

dhfm-lm-dfpm

dhfm-fcmclr

dhfm-b-clxyz

dhfm-nachlauf



**dhfm-init**

"- (\*1) abweichend zur Beschaltung wird dieser Teil im Modul %DFPM realisiert."  
"- (\*2) Die durch C\_[\*] ausgelösten Aktionen (im Bild mit (\*2) markiert) werden in der Software in eigenen Prozessen abgearbeitet."

"- Maximalwert von wdkba z.B. bei 8Bit-wdkba --> FF Hex"

**Fehlerspeicherverwaltung:**  
-----

Status Fehlerpfad LM: SFPLM  
Errorflag LM: E\_lm  
Zyklusflag LM: Z\_lm  
Fehlerart LM: B\_mxl  
B\_mnl

Löschen Fehlerpfad: C\_fmclr & B\_cllm  
Fehlerpfad LM : CDTLM  
Fehlerklasse LM: CLALM  
Fehlerschwere LM: TSFLM  
Carb-Code LM: CDCLM  
Umweltbedingungen LM: FFTLM Umweltbedingungen siehe %DFFT

**ABK DHFM 63.80 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWDHFM			FW	Code word in DHFM
FVMLHFMMN	FHO_W		KL	Weighting factor for min. HFM air-mass threshold as a function of the altitude
KFMLDMN	WDKBADMN_W	NMOT_W	KF	air mass flow threshold for min. failure
KFMLDMX	WDKBADMX_W	NMOT_W	KF	air mass flow threshold for max. failure
MLHFMMN			FW	Min. HFM air-mass threshold to reset the min. fault
MLOFS			FW (REF)	offset for characteristic line of air mass flow meter HFM 5
SY_TURBO			SYS (REF)	system constant for exhaust-gas turbocharger
TDMLHFM			FW	Delay time for setting the bit B_hfm
TDMLMN			FW	debounce time for minimum fault detection air-mass meter
TDMLMX			FW	debounce time for maximum fault detection air-mass meter
TDMLNF			FW	debounce time air-mass meter diagnosis with o.k. status
TDMLST			FW	debounce time fault detection air-mass meter during start
TDUBHFM			FW	time of HFM-diagnosis at u < UBHFM
UADHFMMN			FW	minimum input voltage for HFM during Start
UADHFMMX			FW	maximum input voltage for HFM during start
UBHFM			FW	battery voltage threshold for switch to msdk
UNWDHFM			FW	camshaft rotations for debouncing diagnosis DHFM
ZMLRO			FW	time constant for low-pass-filter air mass flow

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B_BELM	DHFM	AUS	condition air flow sensor (MAFS/MAPS) request
B_BKLM	DHFM	AUS	Condition: main load sensor active
B_CLLM		EIN	condition: clear fault path main load sensor
B_EDKS	GGDVE	EIN	Condition fault in throttle-valve sensor
B_EHFM	DHFM	AUS	condition: HFM error (without debounce)
B_EHFM1	DHFM	LOK	condition: HFM error (without debounce)
B_EHFS	DHFM	AUS	Condition substitute value main charge sensor
B_ELMI	DHFM	AUS	Condition error massflow at initialisation
B_FTLM	DHFM	AUS	Condition fault entry by tester for air mass flow sensor (MAFS/MAPS)
B_HFM	DHFM	AUS	Condition: HFM ready to measure
B_LDRUGD		EIN	Condition unthrottled, Eneable from LDR
B_MNHFM	DHFM	LOK	Condition: Below lower plausibility threshold
B_MNLM	DHFM	AUS	Condition: min-error main load sensor
B_MXHFM	DHFM	LOK	Condition: Upper HFM plausibility threshold exceeded
B_MXLM	DHFM	AUS	Condition: max-error main load sensor
B_NPLM	DHFM	AUS	plausible-error main load sensor
B_SILM	DHFM	AUS	signal-error main load sensor
B_STEND	BBSTT	EIN	condition end of start
DFP_LM	DHFM	DOK	ECU-internal fault path no.: main-load sensor
E_LM	DHFM	AUS	Error flag: main load sensor
FHO_W	BGPU	EIN	correction factor: altitude
FVMLHFMM	DHFM	AUS	weighted MLHFMMN in dependence from fho
MLDMN_W	DHFM	AUS	Minimal air mass from map KFMLDMN



Variable	Source	Type	Description
MLDMX_W	DHFM	AUS	Maximal air mass from map KFMLDMX
MLHFMF_W	DHFM	LOK	Filtered air mass HFM mean value 16 Bit value
MLHFMM_W	GGHFM	EIN	mean HFM air mass value 16-Bit
NMOT_W	SWADAP	EIN	engine speed
SFPLM	DHFM	AUS	status fault path: main load sensor
UB	SWADAP	EIN	battery voltage
UHFM_W		EIN	HFM voltage
UZKW_W	GGDPG	EIN	revolution counter crankshaft
WDKBADMN_W	DHFM	LOK	Throttle-valve angle to address KFMLDMN
WDKBADMX_W	DHFM	LOK	Throttle-valve angle to address KFMLDMX
WDKBA_W	GGDVE	EIN	throttle angle with respect to lower mechanical stop
Z_LM	DHFM	AUS	cycle flag: load determination LMM/HLM/HFM

### FW DHFM 63.80 Fixed Values

Parameter	Value	Description
CWDHFM		Code word in DHFM
MLHFMMN		Min. HFM air-mass threshold to reset the min. fault
TDMLHFM		Delay time for setting the bit B_hfm
TDMLMN		debounce time for minimum fault detection air-mass meter
TDMLMX		debounce time for maximum fault detection air-mass meter
TDMLNF		debounce time air-mass meter diagnosis with o.k. status
TDMLST		debounce time fault detection air-mass meter during start
TDUBHFM		time of HFM-diagnosis at $u < UBHFM$
UADHFMMN		minimum input voltage for HFM during Start
UADHFMMX		maximum input voltage for HFM during start
UBHFM		battery voltage threshold for switch to msdk
UNWDHFM		camshaft rotations for debouncing diagnosis DHFM
ZMLRO		time constant for low-pass-filter air mass flow

### FB DHFM 63.80 Detailed description of function

Der Funktionsumfang umfasst folgende Teilbereiche:

#### Post-start stabilization

The diagnostic routine is only enabled following elapse of the debounce time TDMLST for suppression of the incorrect signal after the HFM2 (12V peak, turn-on preheating fault) has been turned on. Triggering for strat of the debounce time is realized by the condition B\_stend.

The same condition for enabling the diagnostic routine also applies for minimum faults

B\_mnlm, e.g. cable drop of KS to ground

B\_stend is set if  
mshfm is less than the speed-dependent threshold value MLDMN  
and  
the delay time TDMLST triggered by B\_stend has elapsed  
and then the  
debounce time TDMLMN (fault entry delay time for minimum fault) has elapsed.

B\_mx1m, e.g. KS to Ubatt

B\_mx1m is set if  
mshfm is greater than the speed and throttle valve-dependent threshold value KFMLDMX  
and  
the delay time TDMLST triggered by B\_stend has elapsed  
and then the  
debounce time TDMLMX (fault entry delay time for maximum fault) has elapsed.

In the case of a throttle valve fault (for E\_dk), KFMLDMX is addressed with the maximum DK angle, and only the upper threshold values apply as speed-dependent values.  
In the case of a throttle valve fault (for E\_dk), KFMLDMN is addressed with the minimum DK angle, and only the lowest threshold values apply as speed-dependent values.

B\_noflr

B\_noflr is set if  
no fault (Min-Max-Plaus)  
is detected  
with debounce time TDMLNF.



E\_lm  
-----  
Error flag is set after the respective debounce time for  
B\_minflr or B\_maxflr

Z\_lm  
-----  
Cycle flag is set for  
B\_minflr or B\_maxflr or B\_noflr

B\_ehfm  
-----  
This flag is set without debounce time for minimum or maximum fault, in order that a switchover to the  
standby load signal can be made immediately in the event of a fault.  
If for HFMS, the battery voltage is less than 11 Volts, then the HFM signal is no longer  
plausible and switch over to the standby filling signal is required by B\_ehfm=true.  
For HF2 the UBHF threshold is of no significance and must be dated such that  
no switchover to the standby filling signal occurs (i.e. UBHF=0)

B\_hfm  
-----  
The flag B\_hfm is set following start end (B\_stend) and subsequent elapse of TDMLST  
and signalizes the readiness of the HFM for measurement and operation. The filling detection is switched over from  
the standby filling signal to the main filling signal after the start by the flag B\_hfm.

Remarks:  
- Fault lamp control: 2 trps after (E\_lm & Z\_lm)  
- No faults are diagnosed on the hardware side  
- Refer also to %DVFL for fault memory management  
- C.ini for resetting of the cycle flag is described in more detail in %DFVL

## APP DHFM 63.80 Application hint

Stand by measure :

-----  
Switchover to secondary filling signal and standby value RLNOT for DK fault at the same time (is realized in the funct. %BGMSZS)

Different additional measures are possible depending on the project (see cross-reference matrix):

-----  
disable LR-adaption, >  
disable LLR characteristics and optional, > jeweils aktuelle Adaptionswerte gültig  
disable KR-adaption, >  
Tank venting in continuous operation (no prohibition for adaption)

Abgespeicherte Umweltbedingungen beim Auftreten des Fehlers

-----  
Für den Fall, daß der freeze-frame nicht über den Kundendienstdiagnosetester ausgelesen werden kann, empfehlen wir beim Auftreten  
des Fehler folgende Umweltbedingungen mit abzuspeichern.

1. Umweltwert nmot.u
2. Umweltwert tmot.u

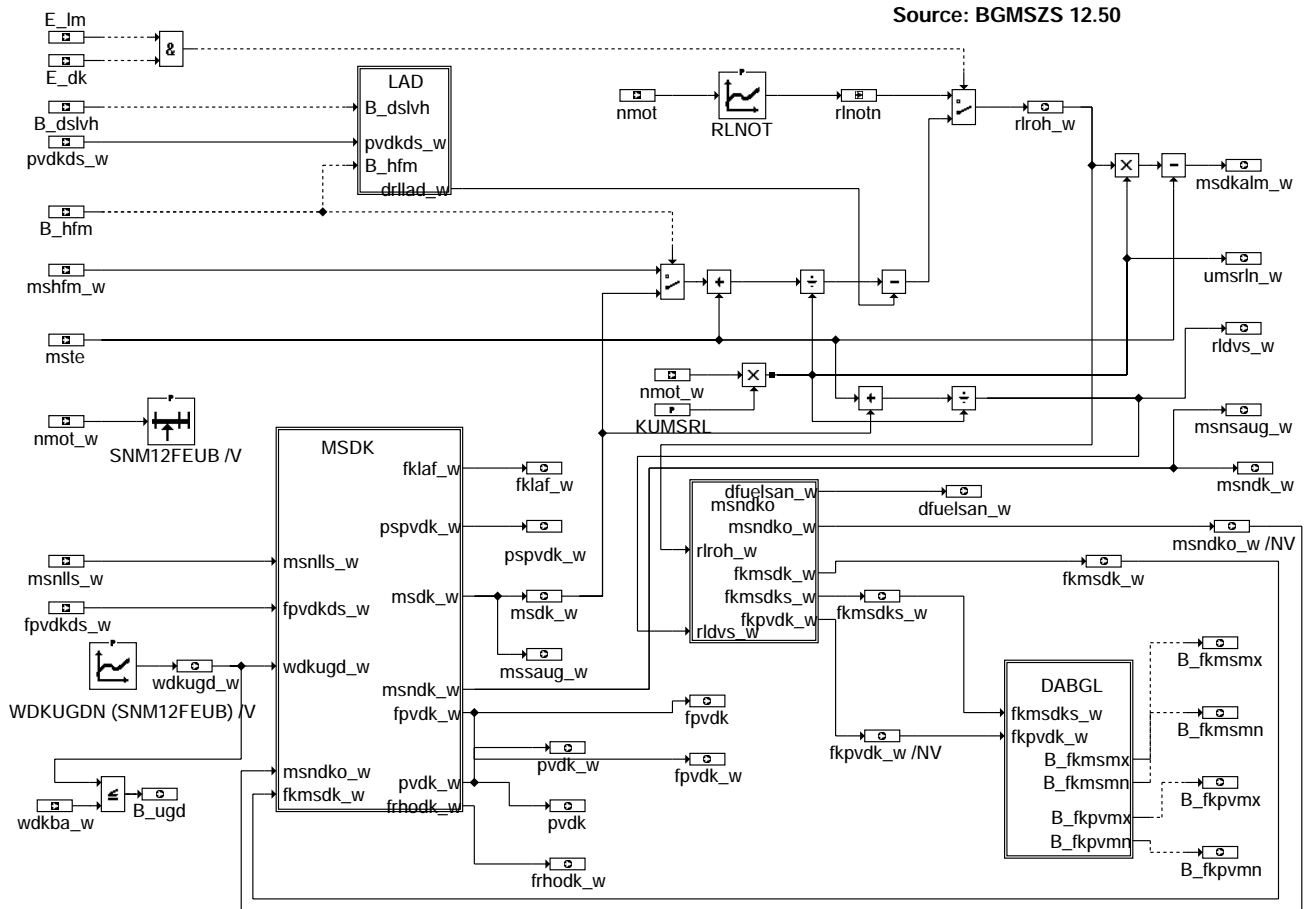
Kann der freeze-frame über den Kundendienstdiagnosetester ausgelesen werden, empfehlen wir zwei weitere (im freeze-frame nicht  
enthaltene Größen) als Umweltbedingungen mit abzuspeichern z.B. tans.u,wdkba.u. (Referenztablelle siehe %DFFT).

Anhaltswerte für Erstapplikation :

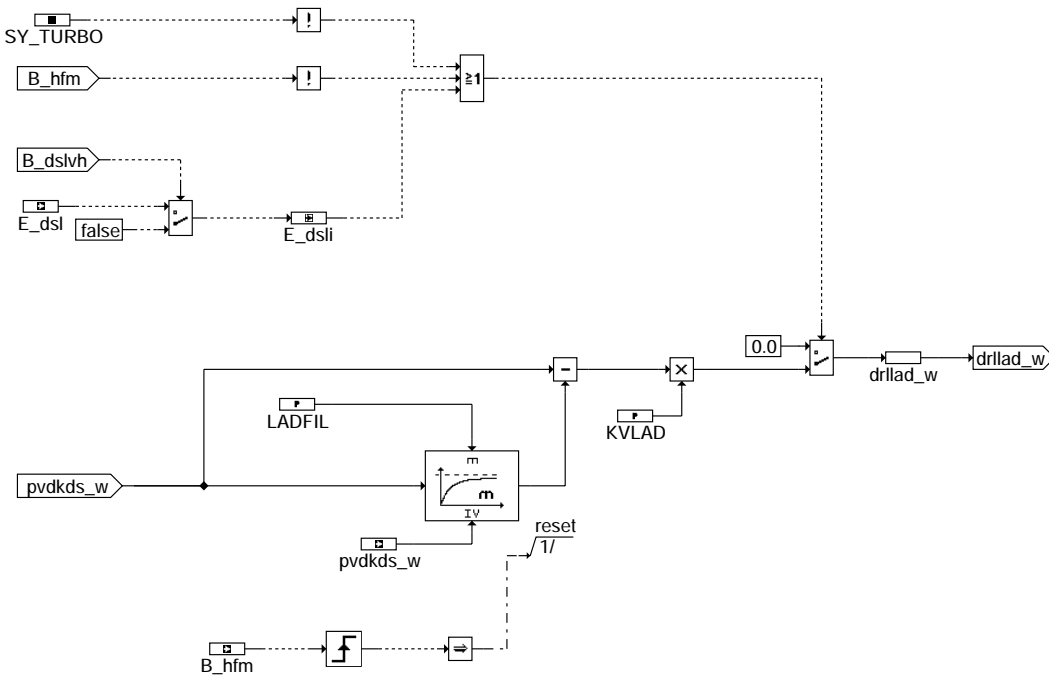
-----  
TDMLMN 0.3 sec possible drop in speed for connector falling off in the LL, without the automobile cutting out  
TDMLMX 0.3 sec  
TDMLNF 1.0 sec Stabilization behaviour of HFM following KS  
TDMLST 0.3 sec dependent on start with cable fallen off  
ZMLRO ca. 0.3 sec time constant from the intake manifold  
  
KFMLDMX Less than minimum air mass with closed LLS in trailing throttle  
KFMLDMN dsign approx. 20% above maximum possible air mass at full load

### BGMSZS 12.60 Calculation of mass flows into intake manifold

#### DFEF BGMSZS 12.60 Function definition



#### bgmszs-bgmszs

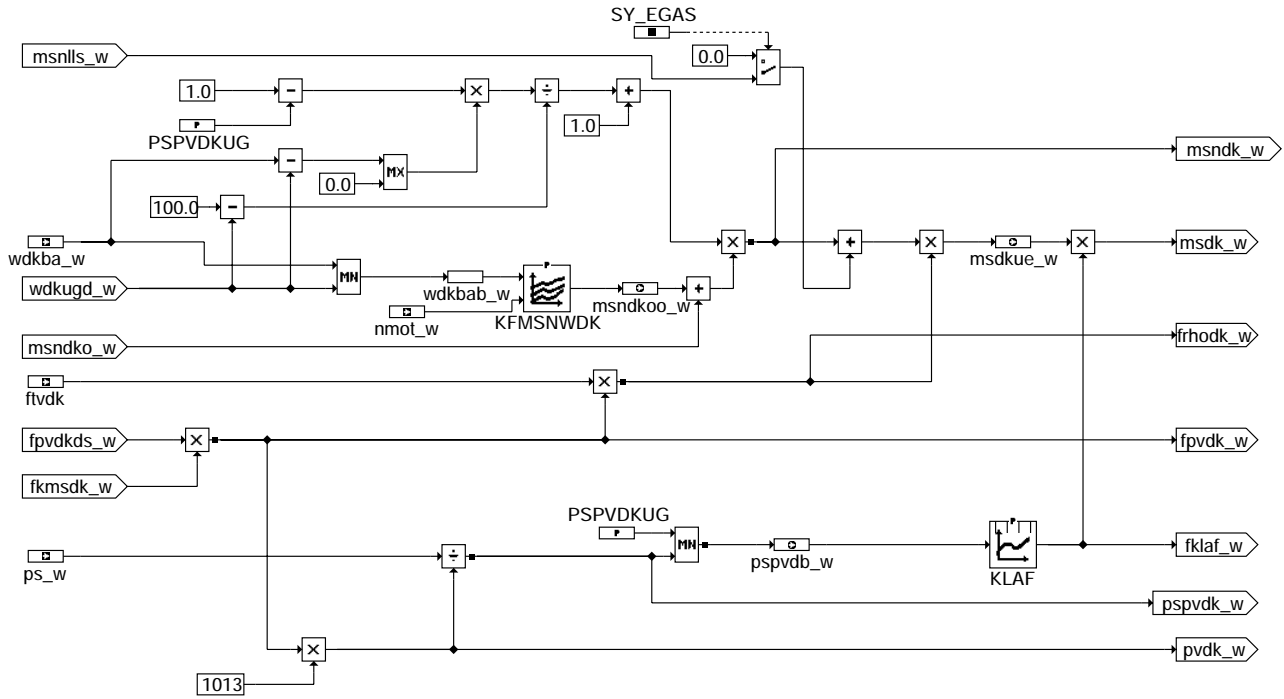


#### bgmszs-lad

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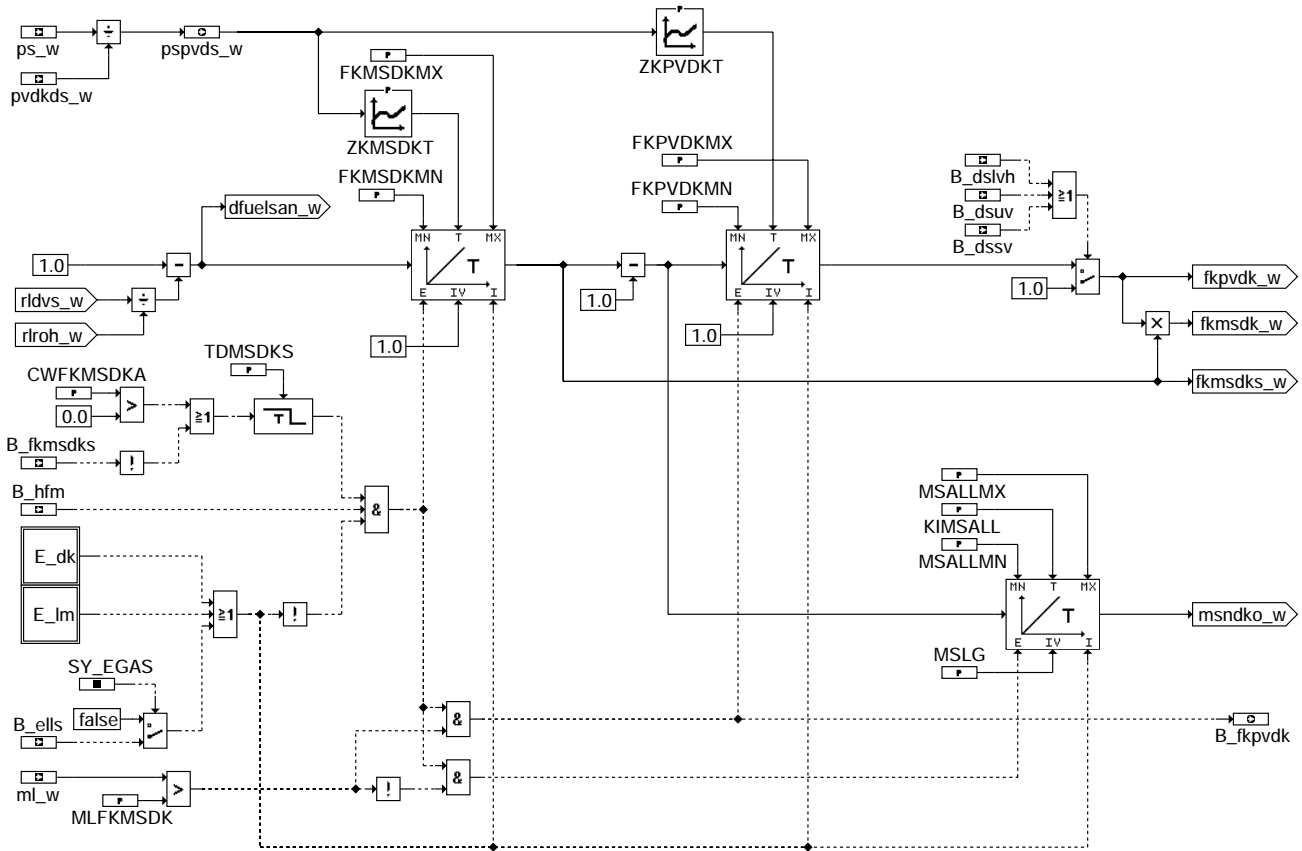
bgmszs-bgmszs

bgmszs-lad



bgmszs-msdk

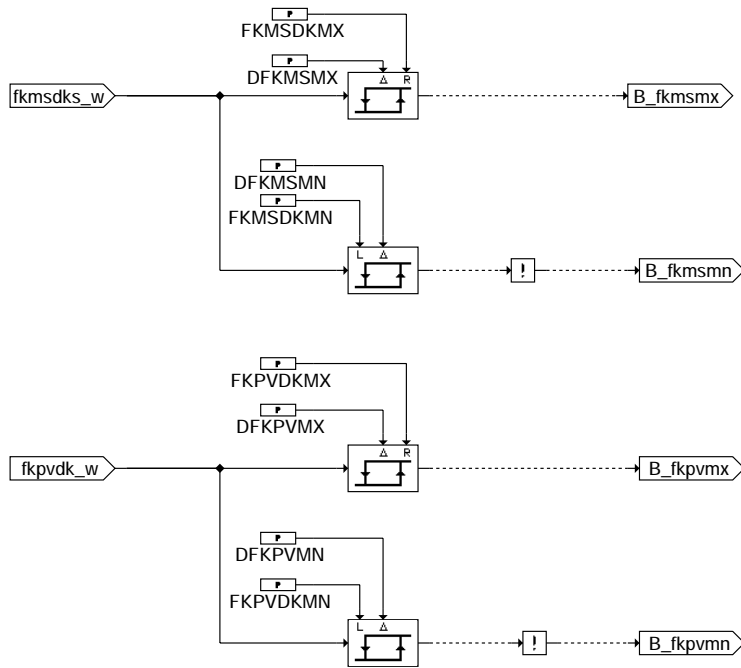
bgmszs-msdk



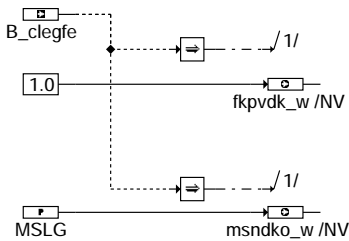
bgmszs-msndko

bgmszs-msndko





**bgmszs-dabgl**



**bgmszs-fcmclr**

**ABK BGMSZS 12.60 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWFKMSDKA			FW	codeword for mass-flow adaption activ
DFKMSMN			FW	Delta FKMSDKMN for resetting of B_fkmsmn
DFKMSMX			FW	Delta FKMSDKMX for resetting of B_fkmsmx
DFKPVMN			FW	Delta FKPVDKMN for resetting of B_fkpvmn
DFKPVMX			FW	Delta FKPVDKMX for resetting of B_fkpvmx
FKMSDKMN			FW	low limit for slow mass-flow correction of throttle valve
FKMSDKMX			FW	high limit for fast mass-flow correction of throttle valve
FKPVDKMN			FW	lower limit for mass-flow correction of throttle valve
FKPVDKMX			FW	high limit for mass-flow correction of throttle valve
KFMSNWDK	WDKBAB_W	NMOT_W	KF	Map for scaled mass flow over throttle valve
KIMSALL			FW	Correction value for idling air mass integrator for E gas
KLAF	PSPVDB_W		KL	characteristic of Saint-Venant
KUMSRL			FW	conversion constant from mass flow to relative air charge
KVLAD			FW	air charge correction caust by boost pressure dynamic
LADFIL			FW	boost pressure filtering for calculation of delta boost pressure
MLFKMSDK			FW	air flow threshold for multipl. adjustment of HFM and throttle air flow
MSALLMN			FW	Minimum idling air mass adaptation for E gas
MSALLMX			FW	Maximum idling air mass adaptation for E gas
MSLG			FW	Mass flow total leakage air
PSPVDKUG			FW	Ratio pspvd not reduced
RLNOT	NMOT		KL	limp-home relative air charge rl in case of E_DK and E_LM
SNM12FEUB	NMOT_W		SV	set points of WDKSMX, WDKUGDN
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_TURBO			SYS (REF)	system constant for exhaust-gas turbocharger
TDMSDKS			FW	Time delay for the bit B_fkmsdks
WDKUGDN	NMOT_W		KL	throttle angle necessary for 95 % of the maximum possible air charge
ZKMSDKT	PSPVDS_W		KL	integrator speed for fast constant mass-flow adaption
ZKPVDKT	PSPVDS_W		KL	integrator speed for slow constant mass-flow adaption



Variable	Source	Type	Description
B_CLEGFE		EIN	condition clear fault path EGFE
B_DSLVH		EIN	boost-pressure sensor is on the system
B_DSUV		EIN	intake-manifold pressure sensor is mounted
B_DSUV		EIN	ambient pressure sensor is mounted on the system
B_ELLS		EIN	Condition: error idle speed actuator
B_FKMSDKS	FUEDK	EIN	stop for integration of fkmsdk
B_FKMSMN	BGMSZS	AUS	Quick adaption of the mass flow fkmsdks at the lower arrester
B_FKMSMX	BGMSZS	AUS	Quick adaption of the mass flow fkmsdks at the upper arrester
B_FKPVDK	BGMSZS	AUS	Confiton for the release of the slow multiplicative load trim
B_FKPVMN	BGMSZS	AUS	Slow mass flow adaption fkpvdk at the lower arrester
B_FKPVMX	BGMSZS	AUS	Slow mass flow adaption fkpvdk at the upper arrester
B_HFM	DHFM	EIN	Condition: HFM ready to measure
B_PWF		EIN	Condition for powerfail
B_UGD	BGMSZS	AUS	condition: throttle angle greater or equal wdkugd
DFP_DK	BGMSZS	DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_LM	BGMSZS	DOK	ECU-internal fault path no.: main-load sensor
DFUELSAN_W	BGMSZS	AUS	Delta charge sensor to alpha/n-systems
DRLLAD_W	BGMSZS	LOK	dynamic part of relative air charge ri at turbo engine
E_DK	DDVE	EIN	Error flag: throttle position sensor
E_DSL		EIN	error flag: pressure sensor charging pressure
E_DSLI	BGMSZS	LOK	Error flag : Pressure sensor for turbo charge pressure , intern
E_LM	EGFE	EIN	Error flag: main load sensor
FKLAF_W	BGMSZS	AUS	Factor saint venant (KLAF)
FKMSDKS_W	BGMSZS	AUS	correction factor for fast mass flow signal
FKMSDK_W	BGMSZS	AUS	correction factor for mass-flow substitute load signal
FKPVDK_W	BGMSZS	AUS	correction factor for slow mass flow signal
FPVDK	BGMSZS	AUS	correction factor for pressure upstreams throttle
FPVDKDS_W	BGPU	EIN	Factor pressure in front of throttle valve of pressure sensor (word)
FPVDK_W	BGMSZS	AUS	correction factor for pressure upstream of throttle valve, 16-bit
FRHODK_W	BGMSZS	AUS	factor correction air density for throttle valve flow f(intake air temp.,alrit.)
FTVDK	SWADAP	EIN	correction factor for temperature upstream of throttle valve
ML_W	EGFE	EIN	air mass flow filtered (Word)
MSDKALM_W	BGMSZS	AUS	Mass flow over throttle (balance with HFM signal)
MSDKUE_W	BGMSZS	AUS	Air mass flow thru throttle body when overcritical pressure drop
MSDK_W	BGMSZS	AUS	air-mass flow through throttle valve
MSHFM_W	GGHFM	EIN	air-mass flow HFM
MSNDKOO_W	BGMSZS	AUS	Normalized mass flow over throttle without offset (word)
MSNDKO_W	BGMSZS	AUS	norm leakage air mass flow through throttle blade
MSNDK_W	BGMSZS	AUS	standardised air mass flow through throttle valve
MSNLLS_W		EIN	standardised air mass flow through idle speed actuator (word)
MSNSAUG_W	BGMSZS	AUS	standardized air mass flow through intake manifold (word)
MSSAUG_W	BGMSZS	AUS	air mass flow through intake manifold (word)
MSTE	BGTEV	EIN	mass flow purge control into the manifold
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
PSPVDB_W	BGMSZS	AUS	quotient:int.manif.press.divided by press.upstream of throttle valve limit
PSPVDK_W	BGMSZS	AUS	quotient: int.manif.pressure divided by pressure upstream of throttle valve
PSPVDS_W	BGMSZS	AUS	quotient manifold pressure/pressure before throttle plate
PS_W	EGFE	EIN	intake manifold pressure (absolute) (Word)
PVDK	BGMSZS	AUS	pressure in front of throttle
PVDKDS_W	BGPU	EIN	Pressure in front of throttle valve of pressure sensor (word)
PVDK_W	BGMSZS	AUS	pressure upstream of throttle valve, 16-bit
RLDVS_W	BGMSZS	AUS	relative air charge through throttle valves on intake manifold
RLNOTN	BGMSZS	LOK	Relative air charge when main and limp home signal error, depending on rpm
RLROH_W	BGMSZS	AUS	relative air charge flowing into intake manifold
UMSRLN_W	BGMSZS	AUS	calculation factor load to mass flow
WDKBAB_W	BGMSZS	LOK	wdkba_w limited (minimum selection between wdkba_w and wdkugd_w)
WDKBA_W	GGDVE	EIN	throttle angle with respect to lower mechanical stop
WDKUGD_W	BGMSZS	AUS	Throttle valve angle during which 95% charge is reached

### FW BGMSZS 12.60 Fixed Values

Parameter	Value	Description
CWFKMSDKA		codeword for mass-flow adaption activ
DFKMSMN		Delta FKMSDKMN for resetting of B_fkmsmn
DFKMSMX		Delta FKMSDKMX for resetting of B_fkmsmx
DFKPVMN		Delta FKPVDKMN for resetting of B_fkpvmn
DFKPVMX		Delta FKPVDKMX for resetting of B_fkpvmx
FKMSDKMN		low limit for slow mass-flow correction of throttle valve
FKMSDKMX		high limit for fast mass-flow correction of throttle valve
FKPVDKMN		lower limit for mass-flow correction of throttle valve
FKPVDKMX		high limit for mass-flow correction of throttle valve
KIMSALL		Correction value for idling air mass integrator for E gas
KUMSRL		conversion constant from mass flow to relative air charge
KVLAD		air charge correction caust by boost pressure dynamic
LADFIL		boost pressure filtering for calculation of delta boost pressure
MLFKMSDK		air flow threshold for multipl. adjustment of HFM and throttle air flow
MSALLMN		Minimum idling air mass adaptation for E gas
MSALLMX		Maximum idling air mass adaptation for E gas
MSLG		Mass flow total leakage air





the difference mass flow  $msdif (=mshfm-mssaug)$  is formed and fed to an integrator. For  $msdif=0$  the integrator provides the value  $fkmsdk=1$ , otherwise  $fkmsdk$  is different from 1. The factor  $fkmsdk$  is used to adjust the pressure upstream throttle valve  $pvdks$ . In this way  $mssaug$  is adapted to  $mshfm$ .

The integrator is activated only by operation ready load sensor (!E<sub>lm</sub>) and second load signal (!E<sub>dk</sub>), and furthermore the air mass  $m_l$  must exceed the threshold  $MLFKMSDK$ . the limitations of the integrator are given by  $FKPVDKMX$  and  $FKPVDKMN$ .

### APP BGMSZS 12.60 Application hint

The standardised flow through throttle valve  $KLAF$  is specified by physics, and is stored as a  $501 * 16$  bit table in the Eprom. The fine stepping from value to value is particularly necessary in the subcritical operating range, since the intake manifold model tends to oscillate if the stepping is spread too coarsely. The values table for the outflow characteristic  $KLAF$  can be requested as an EXCEL file from H.Pfitz K3/ESY5 Tel. 8502 if required.

!!!! The  $KLAF$  is stored only once for the entire project in the EPROM (FLASH), due to the available memory space!!!!

The  $KLAF$  input value is calculated in the relevant modules and transferred in a RAM cell. Then the corresponding output value of the  $KLAF$  is calculated using the transfer value, and the  $KLAF$  value is used for further calculations in the relevant software modules.

Characteristic  $MSNWDK$  for the standard mass flow through the throttle valve, dependent on the throttle angle  $wkba$ , will not always be supplied by the engine manufacturer. In this case the following measurement variables are required to determine the characteristic:

characteristic:

$wkba$  - Throttle angle referred to stop limit at closed throttle valve

$tans$  - Fresh-air temperature upstream of throttle valve

$pvdk$  - Pressure upstream of throttle valve = ambient pressure in induction engine

$ps$  - intake manifold pressure

$mshfm$  - Air mass flow at HFM

The measuring of the characteristic of throttle valve is described in E-Bericht K3/ESY 28/96.

there are the following relationships:

ECU term	E-Report term
$MSNWDK = \frac{mshfm}{fpvk * ftvdk * KLAF(pspvdk)}$	$= \frac{msd}{(pvd/p0) * (Wurzel(T0/Tvd)) * Psin}$
$fpvdk = pvd / 1013hPa$	$= pvd / 1013 hPa$

$ftvdk = \sqrt{273 / (tans + 273)}$  -> Square root of the standard temperature 273 Kelvins divided by the intake air temperatur (Kelvin)

$KLAF$  - The value of  $KLAF$  as function of the ratio between the intake manifold pressure and the pressure upstreams of throttle valve.

Values for initialize:

LADFIL = 0.25

KVLAD = 0.35 %/hPa

MSALLMN = 0 kg/h

MSALLMX = 12 kg/h

KIMSALL = .01

$KLAF$  is specified by physic

**MSNDK:** during application there must be a measured actuator characteristic.

for production application a desired value for actuator characteristic  $MSNDK$  has to be specified.

the characteristic  $MSNDK$  has to be correctected, so that at closed throttle valve ( $wkba = 0$ ) the air mass flow through the valve is zero ( $MSNWDK = 0$  kg/h).

**MSLG:** during application the leakage air mass flow at closed throttle valve is entered in  $MSLG$ .

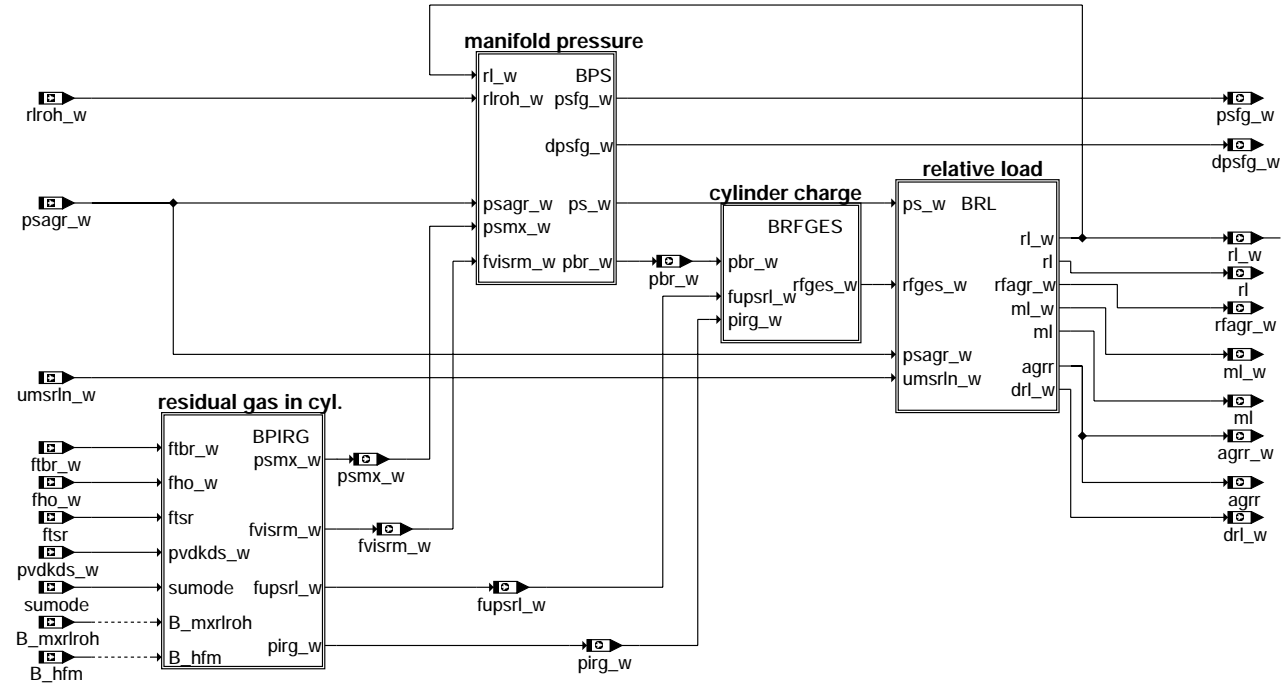
for production application the leakage air mass flow specified in the  $TKU$  is entered in  $MSLG$

## BGSRM 17.30 Model of intake manif. for calc. relative air charge and intake manif. pressure

### FDEF BGSRM 17.30 Function definition

BGSRM: Übersicht

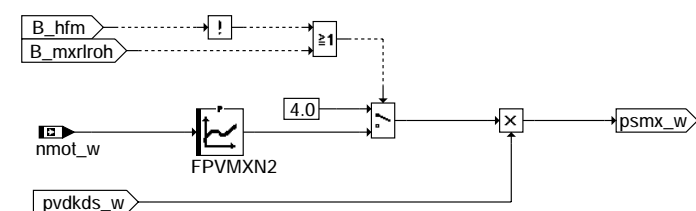
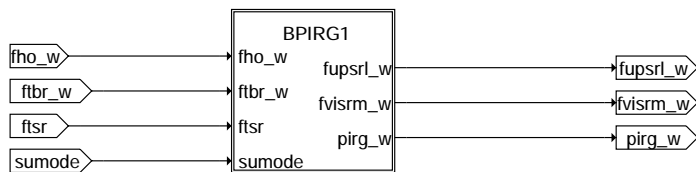
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#### bgsrm-bgsrm

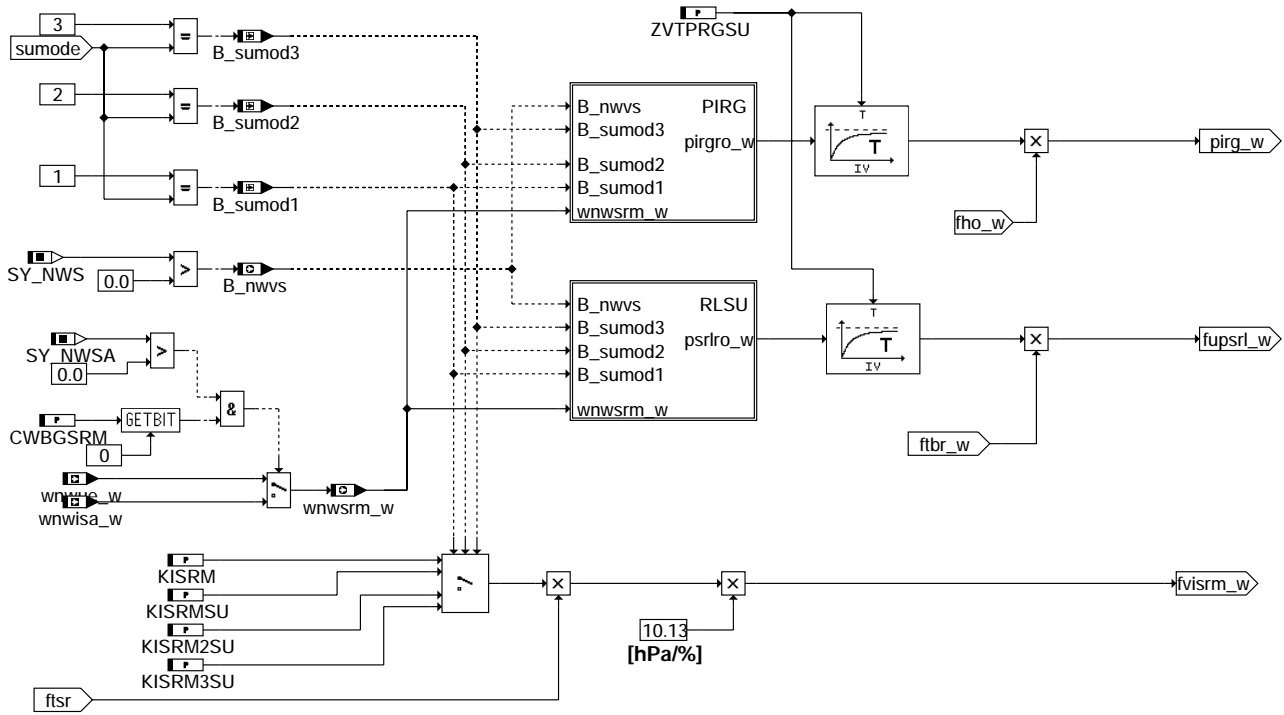
BPIRG: Berechnung max. Saugrohrdruck, internes Restgas, Umrechnungsfaktor Druck --> Füllung und Integratorverstärkung

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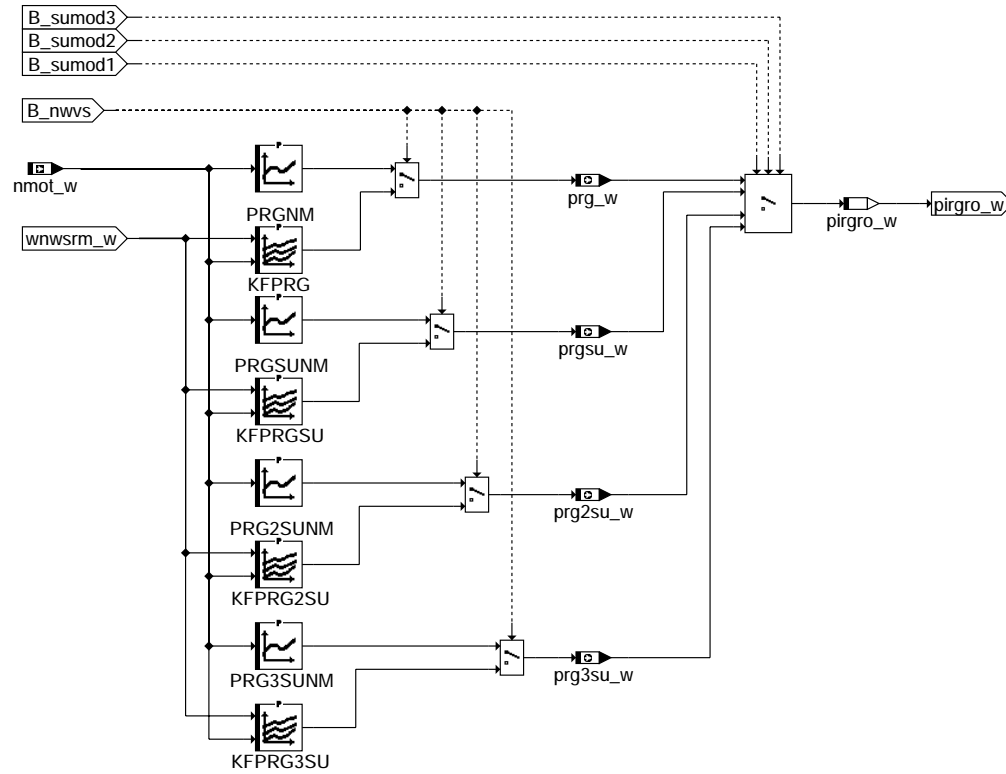
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**BPIRG1: Berechnung internes Restgas, Umrechnungsfaktor Druck --> Füllung und Integratorverstärkung**



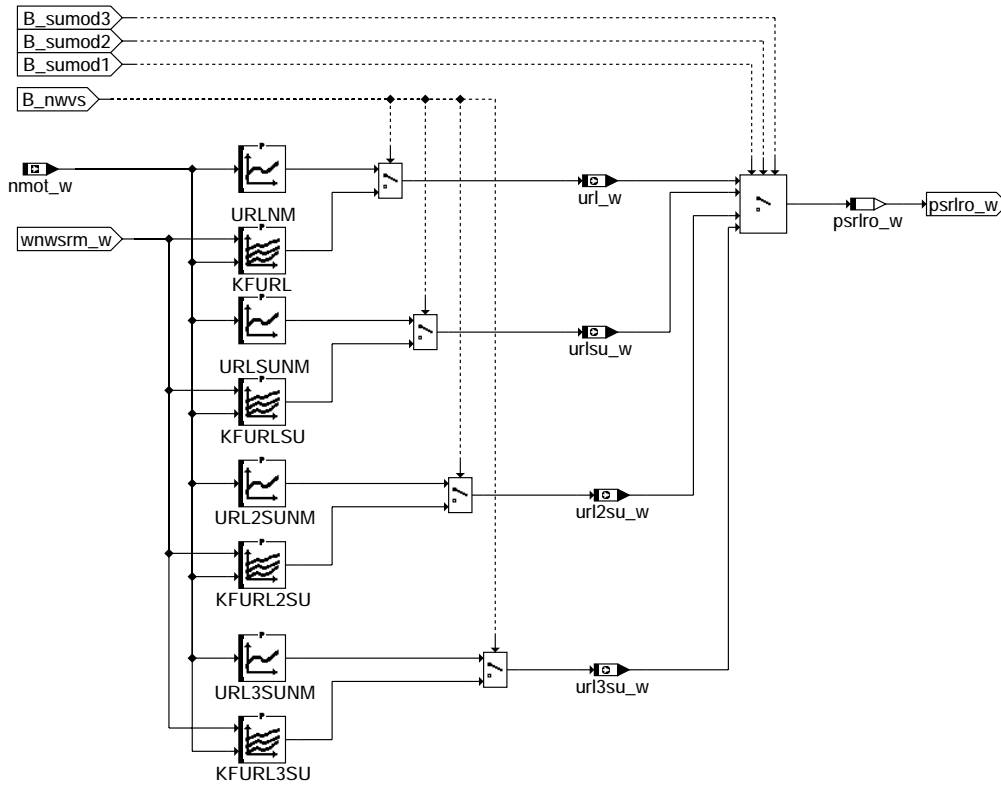
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**PIRG: Berechnung internes Restgas**



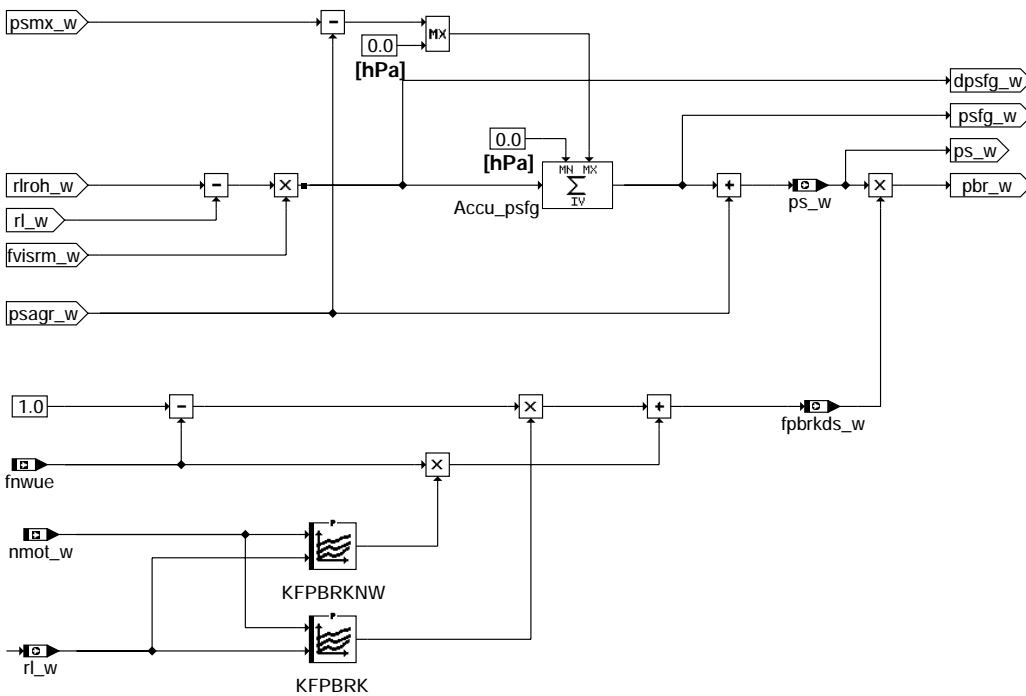
**bgsrm-pirg**

PIRG: Berechnung Umrechnungsfaktor Druck --> Füllung



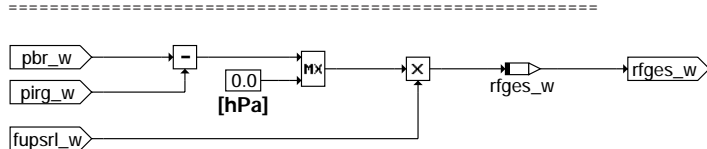
bgstrm-risu

BPS: Berechnung Saugrohr- und Brennraumdruck



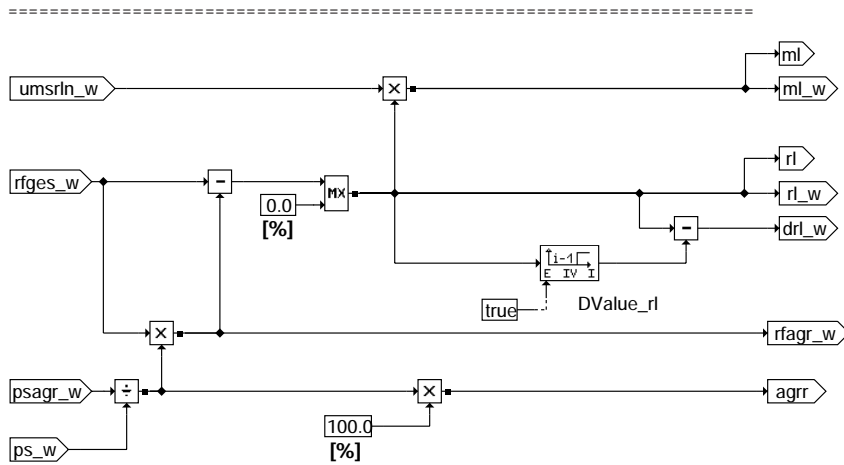
bgstrm-bps

**BRFGES: Berechnung Brennraumfüllung ohne internes Restgas**



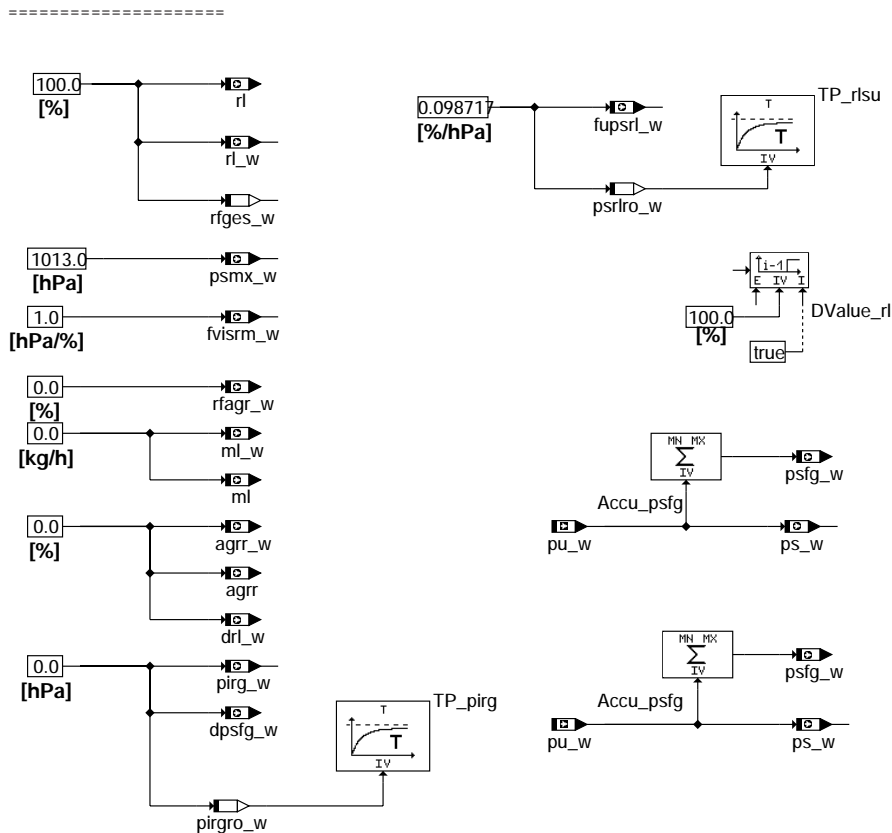
**bgasm-brfges**

**BRL: Berechnung Frischluftbrennraumfüllung, AGR-Rate und Luftmassenstrom**



**bgasm-brl**

**INIT: Initialisierung**



**bgasm-init**

**ABK BGSRM 17.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWBGSRM			FW	code word in BGSRM
FPVMXN2	NMOT_W		KL	factor for pressure ratio maximum with secondary last sensor
KFPBRK	NMOT_W	RL_W	KF	factor to correct pressure at combustion chamber
KFPBRKNW	NMOT_W	RL_W	KF	factor to correct pressure at combustion chamber by active Camshaft control
KFPRG	WNWSRM_W	NMOT_W	KF	internal partial exhaust gas pressure dependent on camshaft adjustment sumode=0





Parameter	Source-X	Source-Y	Type	Description
KFPRG2SU	WNWSRM_W	NMOT_W	KF	internal partial exhaust gas pressure depent on camshaft adjustment sumode=2
KFPRG3SU	WNWSRM_W	NMOT_W	KF	internal partial exhaust gas pressure dpent on camshaft adjustment sumode=3
KFPRGSU	WNWSRM_W	NMOT_W	KF	internal partial exhaust gas pressure dependent on camshaft adjustment sumode=1
KFURL	WNWSRM_W	NMOT_W	KF	conversion factor from ps->rl dependent on camshaft adjustment sumode=0
KFURL2SU	WNWSRM_W	NMOT_W	KF	conversion factor from ps->rl dependent on camshaft adjustment sumode=2
KFURL3SU	WNWSRM_W	NMOT_W	KF	conversion factor from ps->rl dependent on camshaft adjustment sumode=3
KFURLSU	WNWSRM_W	NMOT_W	KF	conversion factor from ps->rl dependent on camshaft adjustment sumode=1
KISRM			FW	integrator speed constant for intake manifold model
KISRM2SU			FW	integrator speed constant for intake manifold model by sumode=2
KISRM3SU			FW	integrator speed constant for intake manifold model by sumode =3
KISRMSU			FW	integrator speed constant for intake manifold model by sumode=1
PRG2SUNM	NMOT_W		KL	internal exhaust-gas part. press. dependent on the speed at active SU (2nd flap)
PRG3SUNM	NMOT_W		KL	inter. exhaust-gas part. press. dependent on speed at active SU (1st + 2nd flap)
PRGNM	NMOT_W		KL	internal exhaust-gas partial pressure dependent on the speed
PRGSUNM	NMOT_W		KL	inter. exhaust-gas partial press. dep. on speed in case of active SU (1st flap)
SY_NWS			SYS (REF)	system constant camshaft control: none, 2 point, continous
SY_NWSA			SYS (REF)	system constant camshaft control outlet
URL2SUNM	NMOT_W		KL	conversion factor from ps->rl dependent on nmot_w for active SU (2nd flap)
URL3SUNM	NMOT_W		KL	conversion factor from ps->rl dependent on nmot_w for active SU (1st + 2nd flap)
URLNM	NMOT_W		KL	conversion factor from ps->rl dependent on nmot_w
URLSUNM	NMOT_W		KL	conversion factor from ps->rl dependent on nmot_w for active SU (1st flap)
ZVTPRGSU			FW	time constant for low pass filtering by intake manifold flaps dynamic

Variable	Source	Type	Description
AGRR	BGSRM	AUS	exhaust gas recirculation rate
AGRR_W	BGSRM	AUS	exhaust gas recirculation rate
B_HFM	DHFM	EIN	Condition: HFM ready to measure
B_MXRLROH		EIN	condition maximum selection for rloh has been fulfilled
B_NWVS	BGSRM	AUS	condition camshaft adjustment (continuous or 2-step) exists
B_SUMOD1	BGSRM	LOK	condition variable intake manifold sumode=1
B_SUMOD2	BGSRM	LOK	condition variable intake manifold sumode=2
B_SUMOD3	BGSRM	LOK	condition variable intake manifold sumode=3
DPSFG_W	BGSRM	AUS	delta fresh air partial pressure in manifold
DRL_W	BGSRM	AUS	charge change (Word)
FHO_W	BGPU	EIN	correction factor: altitude
FNWUE	NWS	EIN	Weighting factor camshaft overlap
FPBRKDS_W	BGSRM	AUS	factor for determination of combustion chamber pressure
FTBR_W	BGTEMPK	EIN	factor: temperature correction in combustion chamber
FTSR	BGTEMPK	EIN	correction factor for air temperature in the manifold
FUPSRL_W	BGSRM	AUS	factor system related transformation pressure to load (16-Bit)
FVISRM_W	BGSRM	AUS	integrator amplifier factor intake manifold modell
ML	BGSRM	AUS	air mass flow
ML_W	BGSRM	AUS	air mass flow filtered (Word)
NMOT_W	SWADAP	EIN	engine speed
PBR_W	BGSRM	AUS	Calculated combustion chamber pressure
PIRGRO_W	BGSRM	LOK	unfilter value for partial pressure residual gas internal EGR
PIRG_W	BGSRM	AUS	partial pressure residual exhaust gas internal EGR (16-Bit)
PRG2SU_W	BGSRM	AUS	raw value of partial pressure residual gas internal EGR at active SU flap (2nd)
PRG3SU_W	BGSRM	AUS	raw val. of part. press. residual gas internal EGR at active SU flap (1st + 2nd)
PRGSU_W	BGSRM	AUS	raw value of part. press. residual gas internal EGR at active SU flap (1st flap)
PRG_W	BGSRM	AUS	raw value of part. press. residual gas internal EGR when no SU-flap is switched
PSAGR_W	BGAGR	EIN	partial pressure EGR
PSFG_W	BGSRM	AUS	fresh air partial pressure in manifold
PSMX_W	BGSRM	AUS	maximum manifold pressure limitation for modeled manifold pressure
PSRLRO_W	BGSRM	LOK	factor for conversion pressure in cylinder filling
PS_W	BGSRM	AUS	intake manifold pressure (absolute) (Word)
PU_W	BGPU	EIN	Ambient pressure
PVDKDS_W	BGPU	EIN	Pressure in front of throttle valve of pressure sensor (word)
RFAGR_W	BGSRM	AUS	relative load by external exhaust gas reduction
RFGES_W	BGSRM	LOK	total relative charge (including EGR)
RL	BGSRM	AUS	relative air charge
RLROH_W	BGMSZS	EIN	relative air charge flowing into intake manifold
RL_W	BGSRM	AUS	relative air charge (Word)
SUMODE	SU	EIN	status of the intake manifold switch over
UMSRLN_W	BGMSZS	EIN	calculation factor load to mass flow
URL2SU_W	BGSRM	AUS	factor for conversion from pressure to charge for active SU flap (2nd)
URL3SU_W	BGSRM	AUS	factor for conversion from pressure to charge at active SU flaps (1st + 2nd)
URLSU_W	BGSRM	AUS	factor for conversion from pressure to charge for active SU flap (1st)
URL_W	BGSRM	AUS	factor for conv. from press. to charge in case of default pos. of manifold flaps
WNWISA_W		EIN	actual shifting angle of the outlet camshaft
WNWSRM_W	BGSRM	AUS	selec. between wnwue and wnwisa for addressing of the maps for pirg and fupsr1
WNWUE_W	NWS	EIN	camshaft overlap angle of inlet and outlet valve opening

### FW BGSRM 17.30 Fixed Values

Parameter	Value	Description
CWBGSRM		code word in BGSRM
KISRM		integrator speed constant for intake manifold model
KISRM2SU		integrator speed constant for intake manifold model by sumode=2
KISRM3SU		integrator speed constant for intake manifold model by sumode =3



Parameter	Value	Description
KISRMSU		integrator speed constant for intake manifold model by sumode=1
ZVTPRGSU		time constant for low pass filtering by intake manifold flaps dynamic

### FB BGSRM 17.30 Detailed description of function

The intake manifold model calculates the air charge in the combustion chamber from the air mass flowing into the intake manifold.

An integrator simulates the storage of the intake manifold. It integrates the difference between the in-flowing relative charge  $rl_{roh}$  and the extracted relative air charge  $rl$  using the integrator constant  $KISRM$ , and delivers the standardised air mass in the intake manifold at its output. The integrator is calculated in synchro. This acts like a multiplication of the input variables by the engine speed. If the relative charges are used instead of the air mass flows as input signals, the result obtained at the output is an intake manifold air mass.

With the temperature correction factor  $ftsr$  and the value for standard pressure  $1013hPa$  the partial intake manifold pressure of air mass and internal residual gas at a given air mass temperature in the combustion chamber is calculated from the air mass. With an external EGR system, the partial pressure  $agrp-w$ , generated by the external EGR, is added on. This produces the total intake manifold pressure, which represents an important intermediate variable for other functions.

With the engine extraction equation  $rl = (ps - pigr) * fupsrl * (100\% - agrr)$  the extracted relative air charge  $rl$  is calculated from the intake manifold pressure. In this way the relationship between the air charge  $rl$  and the intake manifold pressure can be described by a straight line, calculated from the offset  $pigr$  and the slope characteristic starting value  $KFPSURL$ . With active exhaust gas recirculation (EGR) the total charge signal  $rfges$  is corrected to the relative air charge  $rl$  by multiplying-in the EGR rate.

The offset is interpreted as residual gas  $pigr$ , which remains in the combustion chamber. The offset is dependent on the engine speed  $nmot$  and the overlap angle  $wnwue$  at systems with camshaft control. If the camshaft position is between the two extremes of camshaft control, offset value  $pigr$  is calculated by linear interpolation as function of  $wnwue$ .

As the ambient pressure falls, the proportion of residual gas falls. The offset is therefore reduced by the altitude factor  $fho$ .

The slope of the straight line at standard temperature is also dependent on the engine speed and the overlap angle  $wnwue$  at systems with camshaft control. The slope is calculated by the same method as the offset. For calculation of the intake manifold pressure  $ps$  to the relative air charge, the current air temperature in the combustion chamber must additionally be taken into account. This is done using the factor  $ftbr$ . The faktor  $fupsrl = ftbr * KFPSURL$  takes into account all influences on the slope in translation of pressure into air charge. The factor  $fupsrl$  is also provided for other functions.

With an external EGR system the calculation from intake manifold pressure to air charge delivers the total charge  $rfagr$  including the EGR portion.

The extracted air mass  $rl$  is reduced by the EGR rate  $agrr$ . Then:  $rl = rfagr * (1 - agrr)$ .

$rl$  is fed back to the input of the integrator as the extracted air charge.  $rl$  is the central variable for calculation of the injection. The extracted air mass flow  $ml$  is obtained from the product of engine speed,  $rl$  and the constant  $KUMSRL$ .

The incorporation of the EGR partial pressure into the intake manifold model allows for calculation of the EGR portion of the combustion chamber charge with the appropriate timing. The associated integrator for simulation of the storage behaviour of the intake manifold referred to the EGR charge is to be found in the function  $BGAGR$ .



## APP BGSRM 17.30 Application hint

### assumptions:

Constant KUMSRL in Funktion BGMSZS must be defined.  
Function BGTEMPK is applicated

for application stationary conditions of intake manifold pressure model:  
pneumatic filtered measuring of intake manifold pressure.

for application dynamical effects of intake manifold pressure modell:  
fast intake manifold pressure measuring (time constant of pressure sensor: <10ms ; sampling rate < 4ms)

### application data for first steps:

zkorr	z.....number of cylinders:.....4 - 8
KISRM = -----	VH.....engine capacity
Vs/VH * z	Vs.....volume of intake manifold (from throttle blade to inlet valve) ..typ. 1.5 .. 3.0 * VH
	zkorr...Faktor for correction.....0.90 at z = 4
	0.92 at z = 5
	0.95 at z = 6
	1.00 at z > 6

example.: z = 4, Vs/VH = 2.2 --> KISRM = 0.1023

KFPRG = 50 hPa at complet map  
KFURL = 0.1 %/hPa at complet map  
FPVMXN = 1.20 (disable limitation of intake manifold pressure)

### FPVMXN is applicated after KFPU application:

FPVMXN is the measured intake manifold pressure at full opend throttle valve as function of engine speed corrected by a factor of 1.1.

!!! attention: fpvdk has to correspond with the actual ambient pressure divided by 1013 hPa !!!

if there is a ambient pressure sensor DSUOFS an DSUGRAD must be correct.

if there is a adaptation FPVDMN and FPVDMX must be actual ambient pressure divided by 1013 hPa.

### application of KFPRG and KFURL:

Measuring of intake manifold pressure ps at steps of 100 hPa, relative air charge rl\_w, and ftbr at steps of engine speed nmot and at the two positions of camshaft control represented by the overlap angle wnwue.

The values rl = f(ps) at one engine speed and one camshaft control position are drawing in a diagramm.

Then a regression straight line is calculated for the values. The offset at position rl = 0 divided by fho is the value KFPRG at position nmot, wnwue.

The gradient of the regression straight line divided by a mean value of ftbr is the value KFURL at position nmot,wnwue.

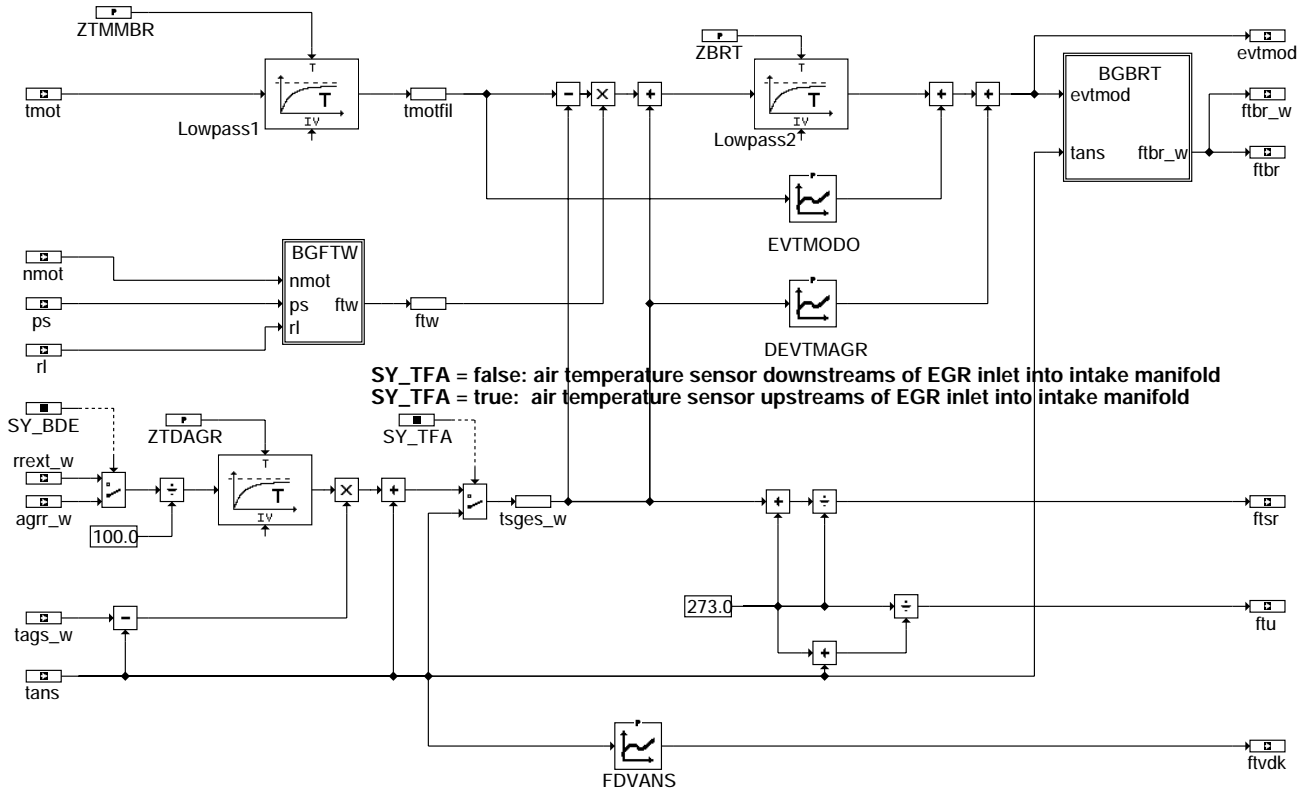
### application of intake manifold dynamic:

Measuring of relative air charge (rl\_w), intake manifold pressure measured with sensor (psmes) and calculated bei ECU (ps\_w) varation of KSIRM, so that the characteristic curves of psmes and ps\_w ar conform.

## BGTEMPK 10.40 Calculation of temperature compensation for intake manifold

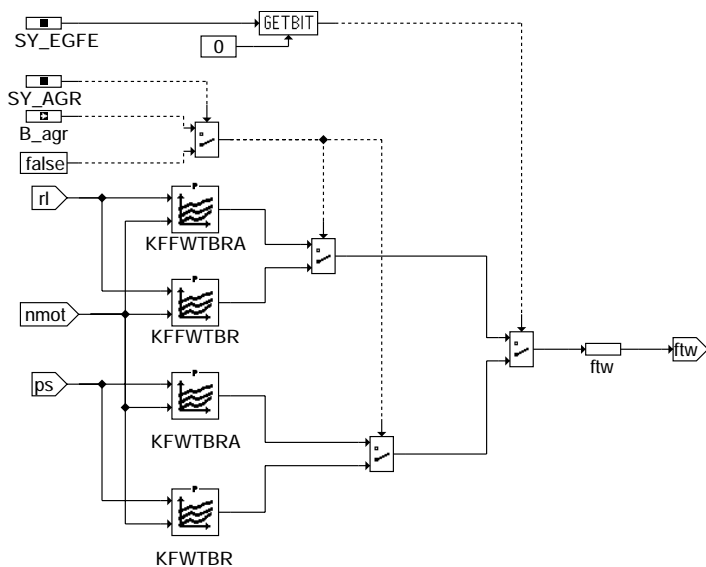
### FDEF BGTEMPK 10.40 Function definition

Source: BGTEMPK 10.40



bgtempk-bgtempk

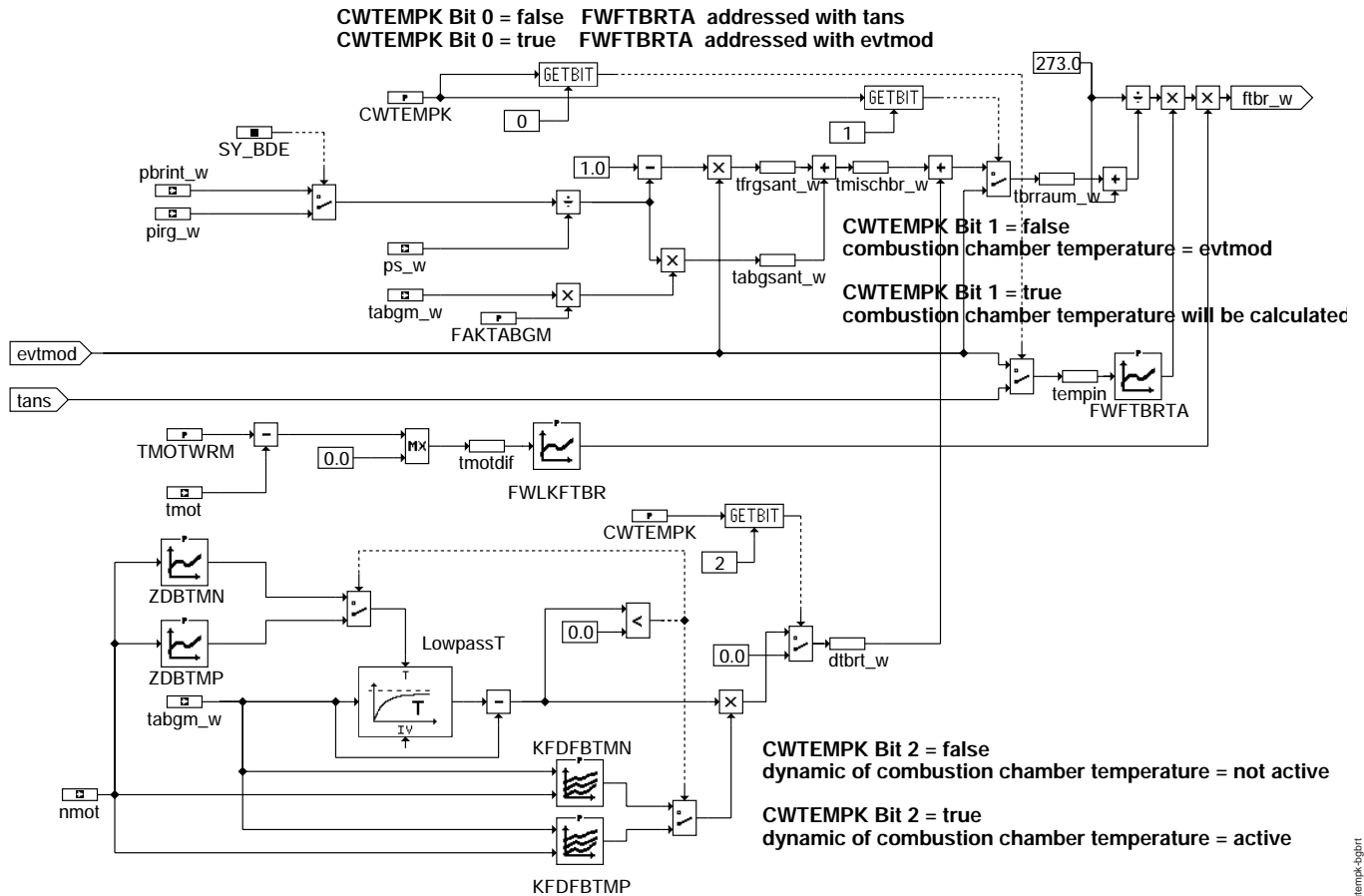
SY\_EGFE Bit 0 = false -> speed density  
 SY\_EGFE Bit 0 = true -> HFM



bgtempk-bgftw

bgtempk-bgtempk

bgtempk-bgftw



bgtempk-bgbrt

### ABK BGTEMPK 10.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWTEMPK			FW	code word for addressing FWFTBRTA depending on (tans/evtmod)
DEVTMAGR	TSGES_W		KL	offset for evtmod depending on tsges_w at high tans caused by EGR
EVTMOD	TMOTFIL		KL	offset for evtmod depending on filtered engine temperature
FAKTABGM			FW	weigh factor for tabgm (exhaust temp) for calculate stationary combustion cham
FDVANS	TANS		KL	Temperature factor for air at throttle valve
FWFTBRTA	TEMPIN		KL	Weighting for ftbr as a function of tans
FWLKFTBR	TMOTDIF		KL	warm up correction for combustion chamber model
KFDFBTMN	TABGM_W	NMOT	KF	dynamic factor for combustion chamber temperatur model negativ gradient
KFDFBTMP	TABGM_W	NMOT	KF	dynamic factor for combustion chamber temperatur model positiv gradient
KFFWTBR	RL	NMOT	KF	Weighting factor for combustion chamber temperature model
KFFWTBRA	RL	NMOT	KF	Weighting factor for combustion chamber temperature model B_agr=true
KFWTBR	PS	NMOT	KF	Weighting factor Tans/Tmot for combustion chamber temperature model
KFWTBRA	PS	NMOT	KF	Weighting factor Tans/Tmot for combustion chamber temperature model B_agr=true
SY_AGR			SYS (REF)	System constant AGR present
SY_BDE			SYS (REF)	system constant GDI
SY_EGFE			SYS (REF)	system constant input variable for charge detection
SY_TFA			SYS (REF)	configuration for installtion position for intake-air sensor
TMOTWRM			FW	engine temperature for warm engine
ZBRT			FW	time constant for combustion chamber temp. model
ZDBTMN	NMOT		KL	time constant combustion chamber temperatur model for negativ gradient
ZDBTMP	NMOT		KL	time constant combustion chamber temperatur model for positiv gradient
ZTDAGR			FW	time constant for temperature dynamics for EGR add-on - shutdown
ZTMMBR			FW	time constant, engine temperature for combustion chamber temp. model
Variable	Source		Type	Description
AGR_R_W	EGFE		EIN	exhaust gas recirculation rate
B_AGR			EIN	Condition AGR active
DTBRT_W	BGTEMPK		LOK	combustion chamber temperature dynamik part
EVTMOD	BGTEMPK		AUS	modelled temperature at inlet valve
FTBR	BGTEMPK		AUS	factor: temperature correction in combustion chamber
FTBR_W	BGTEMPK		AUS	factor: temperature correction in combustion chamber
FTSR	BGTEMPK		AUS	correction factor for air temperature in the manifold
FTU	BGTEMPK		AUS	factor: ambient temperature
FTVDK	BGTEMPK		AUS	correction factor for temperature upstream of throttle valve
FTW	BGTEMPK		LOK	factor weighting of temperature tmot, tans
NMOT	SWADAP		EIN	engine speed



Variable	Source	Type	Description
PBRINT_W		EIN	Partial pressure (inert gas + air) in combustion compart through internal EGR
PIRG_W	EGFE	EIN	partial pressure residual exhaust gas internal EGR (16-Bit)
PS		EIN	intake manifold pressure (absolute)
PS_W	EGFE	EIN	intake manifold pressure (absolute) (Word)
RL	SWADAP	EIN	relative air charge
RREXT_W		EIN	Residual-gas rate (inert gas + air) over external EGR
TABGM_W	ATM	EIN	Exhaust gas temperature in front of the catalyzer from model (Word)
TABGSANT_W	BGTEMPK	LOK	statory combustion chamber temperature evoked via Inertgas
TAGS_W	EGFE	EIN	EGR temperature on introduction into intake manifold
TANS	SWADAP	EIN	Intake air temperature
TBRRaum_W	BGTEMPK	LOK	total combustion chamber temperature stationary and dynamik part
TEMPIN	BGTEMPK	LOK	temperature input (addressing from FWFTBRTA)
TFRGSANT_W	BGTEMPK	LOK	stationary combustion chamber temperature evoked via fresh air
TMISCHBR_W	BGTEMPK	LOK	stationary combustion chamber temperature
TMOT	SWADAP	EIN	Engine temperature
TMOTDIF	BGTEMPK	LOK	difference from actual engine temperature to warm engine temperature
TMOTFIL	BGTEMPK	LOK	filtered engine temperature
TSGES_W	BGTEMPK	LOK	intake manifold temp. (after EGR introduction)

### FW BGTEMPK 10.40 Fixed Values

Parameter	Value	Description
CWTEMPK		code word for addressing FWFTBRTA depending on (tans/evtmod)
FAKTABGM		weigh factor for tabgm (exhaust temp) for calculate stationary combustion cham
TMOTWRM		engine temperature for warm engine
ZBRT		time constant for combustion chamber temp. model
ZTDAGR		time constant for temperature dynamics for EGR add-on - shutdown
ZTMMBR		time constant, engine temperature for combustion chamber temp. model



## FB BGTEMPK 10.40 Detailed description of function

This temperature compensation supplies the combustion-chamber temperature factor (ftbr) at the output. This is used for the conversion from intake-manifold pressure to air mass. The general gas equation  $p \cdot V = m \cdot R \cdot T$  gives the relationship between the pressure  $P$  and air mass  $m$ .  $V$  is the volume,  $R$  the property of the air (air factor = isentropic exponent) and  $T$  corresponds to the air temperature.

The intake-air temperature sensor is usually mounted in the air filter container or in the intake manifold. In order to take both constellations occurring in practice into account, allowance for the location of the intake air temperature sensor is accordingly made by the system byte SY\_TFA. The rise in temperature due to the mass flow from the exhaust-gas recirculation (EGR) flow is automatically measured as well if the temperature sensor is mounted downstream of the point of introduction.

In this case, the data assignment for the parameter SY\_TFA, as defined in the %PROKON function, must be set to false.

If the temperature sensor is mounted upstream of the intake point (e.g. it is in the air filter container) without any consideration for the EGR rate, then the same intake-air temperature would be always be measured irrespective of whether this is with or without EGR. Entering SY\_TFA = true in %PROKON means that, depending on the EGR rate, the modeled intake temperature is added to the temperature measured at the point of introduction. This then corresponds to the temperature modeled for the mixed gas (after intake by the EGR system).

The temperature needed for the calculation is however the temperature of the air in the combustion chamber. A fresh-gas temperature equivalent to the temperature near to the inlet valve is formed using the temperature model. Though the modeled fresh-gas temperature can assume different values in the process here depending on the air flow ratio  $r_l$ , the modeled temperature, evtmod, will however always lie between the engine temperature and the intake-air temperature for weighting factors  $ftw \leq 1$ .

If it applies for the weighting factor that  $ftw > 1$ , then the modeled temperature evtmod is greater than  $t_{mot}$ . The map KKWTRB weights the difference between  $t_{mot}$  and  $t_{ans}$  ( $t_{motfil} - t_{sges}$ ).

The low pass in the TMOT branch prevents the modeled air temperature from increasing too quickly during engine warm-up.

Adjustment to a new thermal equilibrium (air temperature close to the inlet valve) for load changes occurs within seconds.

The second low pass with the time constant ZBRT takes this into account and prevents any abrupt change in the modeled air temperature in the event of a sudden change in the load.

In systems with EGR, the EGR rate is adjusted by a low-pass filter (ZTDAGR) such that the inclusion of the modeled intake temperature into the intake manifold, tags, will dynamically correspond to reality and that this will not take place abruptly.

The modeled intake-air temperature is converted into Kelvin. Scaling is based on 273 Kelvin (0 degrees Celsius). A combustion-chamber temperature factor (ftbr) is made available at the output for further charging-detection calculations.

The temperature factor ftbr is used for the conversion of air mass to intake-manifold pressure.

The temperature factor ftu is used to convert the charge-air mass to a charge-air pressure during boost-pressure control.

A root  $t_{norm}/t_{ans}$  value is made available in the characteristic curve FDVANS to calculate the mass flowing over the throttle valve.

The combustion chamber temperature factor, ftbr, is corrected by multiplication with the characteristic curve FWFTRTA.

Addressing the characteristic can be either by the code word CWTEMPK, bit 0 = false, intake-air temperature (tans)

or by CWTEMPK, bit 0 = true, the modeled temperature, evtmod, at the inlet valve.

Notes on the correct selection for addressing can be found in the application hints given in this FDEF.

A differentiation is made in the system configuration SY\_EGFE between HFM-based or pressure-based charging detection (KFWTBR and KFFWTBR respectively). The value for SY\_EGFE is defined in %PROKON and is hardware-dependent.

In pressure systems with EGR, a switchover to the weighting map KFWTBRA is made when  $B_{agr} = true$ . In HFM systems with EGR, switchover is made to the map KFFWTBRA when  $B_{agr} = true$ . Using the characteristic FWLKFTRB, the combustion-chamber temperature factor ftbr can be adjusted by multiplication as a function of the difference between TMOTWRM and the current engine temperature (during warm-running).

A further feature is the steady-state calculation of the combustion-chamber temperature in that CWTEMPK, bit 1 = true takes the mixing ratio into consideration both for the fresh gas and residual gas in the combustion chamber as well as for the gas temperature. The exhaust-gas temperature, tabgm, shall be applied before activating this steady-state calculation of the combustion-chamber temperature. evtmod is taken as the steady-state combustion-chamber temperature when bit 1 = false in the code word CWTEMPK. A dynamic portion from the RAM cell dtbrt is then added to the steady-state portion of ftbr.

This sub-function should only be activated by bit 2 = true of the code word CWTEMPK for a pressure-based charging detection.

Any transitional compensation is to be deactivated. Subsequent adjustment of dtbrt for different loads and speeds is such that lambda deviations due to load changes are as close to 1 as possible.

The time constant for the differentiator is ZDBTMN. The height of the jump can be adjusted using KFDFBTMP for a negative gradient of tabgm (positive load change). In this context, the same applies for ZDBTMP and KFDFBTMP for a positive gradient of tabgm (negative load change). An adjustment can also be made by multiplication with the characteristic curve FWLKFTRB as a function of the difference between the current  $t_{mot}$  and TMOTWRM of the ftbr. A data assignment deviating from the neutral value becomes necessary if, although the ratio for the modeled to the measured intake-manifold pressure is OK for an engine warm from operation, larger differences occur between the modeled and the measured intake-manifold pressure during warm-running.

## APP BGTEMPK 10.40 Application hint

A thermocouple shall be installed in the intake manifold close to the inlet valve for application of the temperature model.

This is necessary in order to adjust the model temperature at the output of the low pass filter with the time constant ZBRT to the temperature of the intake manifold. Attention is to be paid here that the thermocouple is mounted such that its tip is in the middle of the manifold cross-section. This is to prevent radiant heat from non-permissible falsification of the measurement result.

The adjustment of map KFFWTBR is performed at the datapoints defined for  $n_{mot}$  and  $r_l$  ( $n_{mot}$  and  $ps$  for pressure-based systems).

Entering the weighting factor in the map KFFWTBR for an engine warm from operation and for the different air-flow rates ( $r_l$  or  $ps$ ) is such that the model temperature evtmod agrees with the temperature as measured by the thermocouple.

The time constant ZBRT shall be chosen such that for a load change, the newly adjusted model temperature changes at the same time as the intake-air temperature is measured at the thermocouple. In practice, measurements need to be performed for different jumps in the load and at several engine speeds. A mean value for ZBRT is then to be chosen from the thereby determined time constants.

The time constant ZTMMBR can only be checked while the engine is still warm from operation, whereby adjustment of the time constant is shall be adjusted such that the model temperature agrees with the air temperature actually measured (thermocouple) for the previously matched weighting map KFFWTBR. Several warm-up runs are normally necessary to adjust the time constant.

The time constant ZTDAGR shall be adjusted to give the best dynamic agreement at the different EGR rates for the modeled inlet-air temperature, tags, with the true inlet-air temperature as measured by the thermocouple.

Attention shall be paid in systems with EGR that a switchover to KFFWTBRA or KFWTBRA respectively is made when  $B_{agr} = true$ . The data assignment has to be the same for KFWTBR and KFWTBRA if there is no difference between systems with EGR and systems without EGR.

If during warming-up, a value for evtmod is measured that is higher than the engine temperature,  $t_{mot}$ , then, depending on the engine



temperature, an engine-temperature offset can be added to this from the characteristic curve EVTMOD0. This allows evtmod's during engine warm-up that are higher than tmot. The offset must be 0 for an engine already warm from running. Temperatures at the inlet valve higher than tmot can be attributable to e.g. a larger valve overlap. Basic data assignment shall be neutral with 0 deg. The characteristic curve is activated at very high intake-air temperatures tans > tmot. This can occur during active EGR at high engine speeds and high EGR rates for example. Activating the characteristic curve can also show model temperatures (evtmod) that are higher than tmot or tans. Without EGR, the data assignment for the characteristic curve shall be neutral. By changing the quantization of the maps KFFWTBR and KFWTBR from the previous 0...1 to 0...2 (new), evtmod temperatures higher than tmot are possible as well.

Values for initial application

```

KFFWTBR      Turbo engine 0, aspirating engine 0.2 (factor > 1 --> evtmod = > as tmot)
KFWTBR       Turbo engine 0, aspirating engine 0.2 (factor > 1 --> evtmod = > as tmot)
KFFWTBRA     Turbo engine 0, aspirating engine 0.2 (factor > 1 --> evtmod = > as tmot)
KFWTBRA      Turbo engine 0, aspirating engine 0.2 (factor > 1 --> evtmod = > as tmot)
    
```

Assign data for weighting factors KFWTBR and KFFWTBR at nmot = 0 and rl = 100% (for key ON = Terminal 15 on) as for idling.

Data assignment for difference between ftw Kl.15 (key ON) and engine's idle speed shall be as small as possible.

KFDFBTMN	tabgm_w---	0	200	400	600	800	1000
	nmot						
	v						
	800	0.2	0.2	0.2	0.2	0.2	0.2
	1000	0.1	0.1	0.1	0.1	0.1	0.1
	1500	0.1	0.1	0.1	0.1	0.1	0.1
	2000	0.1	0.1	0.1	0.1	0.1	0.1
	2500	0.1	0.1	0.1	0.1	0.1	0.1
	3000	0.2	0.2	0.2	0.2	0.2	0.2
	3500	0.2	0.2	0.2	0.2	0.2	0.2
	4000	0.0	0.0	0.0	0.0	0.0	0.0

KFDFBTMP	tabgm_w---	0	200	400	600	800	1000
	nmot						
	v						
	800	0.7	0.7	0.7	0.7	0.7	0.7
	1000	0.7	0.7	0.7	0.7	0.7	0.7
	1500	0.7	0.7	0.7	0.7	0.7	0.7
	2000	0.7	0.7	0.7	0.7	0.7	0.7
	2500	0.7	0.7	0.7	0.7	0.7	0.7
	3000	0.7	0.7	0.7	0.7	0.7	0.7
	3500	0.0	0.0	0.0	0.0	0.0	0.0
	4000	0.0	0.0	0.0	0.0	0.0	0.0

ZDBTMN	nmot --->	800	1000	1500	2000	2500	3000	3500	4000
		2.0	7.0	5.0	3.0	1.0	2.0	1.0	0.1

ZDBTMP	nmot --->	800	1000	1500	2000	2500	3000	3500	4000
		0.8	2.0	0.7	0.5	0.2	0.2	0.1	0.1

FAKTABGM 1 Weighting factor tabgm (modeled exhaust-gas temperature)

FWLKFTBR 1 1 = Neutral data assignment (warm-up not corrected) = basic data assignment

TMOTWRM 90 degrees Celsius (basic data assignment value)

CWTEMPK Bit 0 = false FWFTBRTA addressed with tans  
 Bit 0 = true FWFTBRTA addressed with evtmod (recommended)  
 Bit 1 = false Stationary determination of combustion-chamber temperature not active (recommended)  
 Bit 1 = true Stationary determination of combustion-chamber temperature active  
 Bit 2 = false Dynamic calculation of combustion-chamber temperature not active (recommended)  
 Bit 2 = true Dynamic calculation of combustion-chamber temperature active (activate only for pressure systems)

ZTMMBR approx. 300 sec

ZBRT approx. 2 - 5 sec

FDVANS see table below

ZTDAGR approx. 10 sec

FWFTBRTA !!!!! Attention: Carefully read notes on data assignment!!!!!!

EVTMOD0 Basic data assignment neutral shall be with 0 degrees  
 If during warm-up, an evtmod is measured that is greater than the engine temperature tmot, then, depending on the engine temperature, an engine-temperature offset can be added to this from the characteristic curve EVTMOD0.  
 Thus evtmod's higher than tmot are possible during engine warm-up.  
 The offset must be 0 for an engine already warm from running.  
 Temperatures at the inlet valve higher than tmot can be attributable to e.g. a larger valve overlap.





DEVTMAGR Basic data assignment shall be neutral with 0 deg.  
The characteristic curve is activated at very high intake-air temperatures  $tans > tmtot$ .  
This can occur in active EGR at high engine speeds and high EGR rates for example.  
Activating the characteristic curve can show model temperatures (evtmod) that are higher than  $tmtot$  or  $tans$ . Without EGR, the data assignment for the characteristic curve shall be neutral.

The intake-air temperature correction is stored as factor in the characteristic curve FDVANS. It is addressed with  $tans$  [ $^{\circ}C$ ]. This characteristic curve is needed to correct the density at the throttle valves.

$$FDVANS = \sqrt{T0[K]/TANS[K]} \quad \text{Base temperature } T0 \text{ is } 0^{\circ}C = 273 \text{ K, i.e. } ftans (0^{\circ}C) = 1.0$$

Characteristic curve with 8 datapoints to be used for the intake-air temperature:

TANS	-40	-20	0	20	30	40	50	80
FDVANS	1.0824	1.0388	1.0	0.9653	0.9492	0.9339	0.9194	0.8794

FWFTBRATA Data assignment for initial application of BGTEMPK with " root characteristic FWFTBRATA".  
For  $tans = 0$  deg. C, assign 1.0 as data (neutral) for FWFTBRATA.  
Addressing FWFTBRATA shall be via evtmod for a new BGTEMPK application.  
That means the code word CWTEMPK must be = 1.

$$FWFTBRATA = \sqrt{TANS[K]/T0[K]} \quad \text{Base temperature } T0 \text{ is } 0^{\circ}C = 273 \text{ K, i.e. } ftans (0^{\circ}C) = 1.0$$

Characteristic curve with 14 datapoints to be used for modeled air temperature near to the inlet valve:

EVTMOD	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	90
FWFTBRATA	0.923	0.943	0.962	0.981	1.0	1.018	1.034	1.053	1.072	1.087	1.104	1.12	1.137	1.153

!!!! ATTENTION APPLICATION ENGINEERS !!!!!

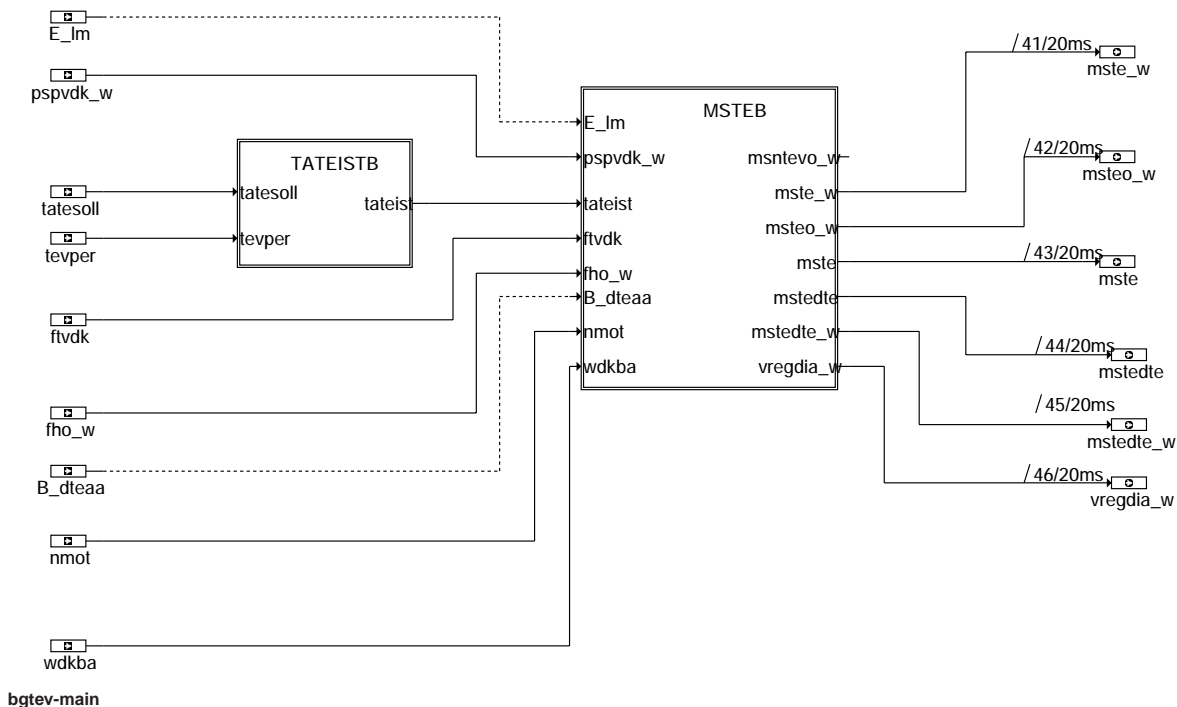
If the initial charging-detection application was performed without the root characteristic FWFTBRATA and adjustment was subsequently made for a cold start or for UK-SEFI, then the data assignment shall be 1.0 for the entire corrective characteristic curve FWFTBRATA.

If the basic application was performed with the BGTEMPK 9.10 then the data assignment for the code word CWTEMPK shall be 1.0 because FWFTBRATA was addressed with  $tans$  in this FDEF.

## BGTEV 1.70 Calculation variable, mass flow TEV

### FDEF BGTEV 1.70 Function definition

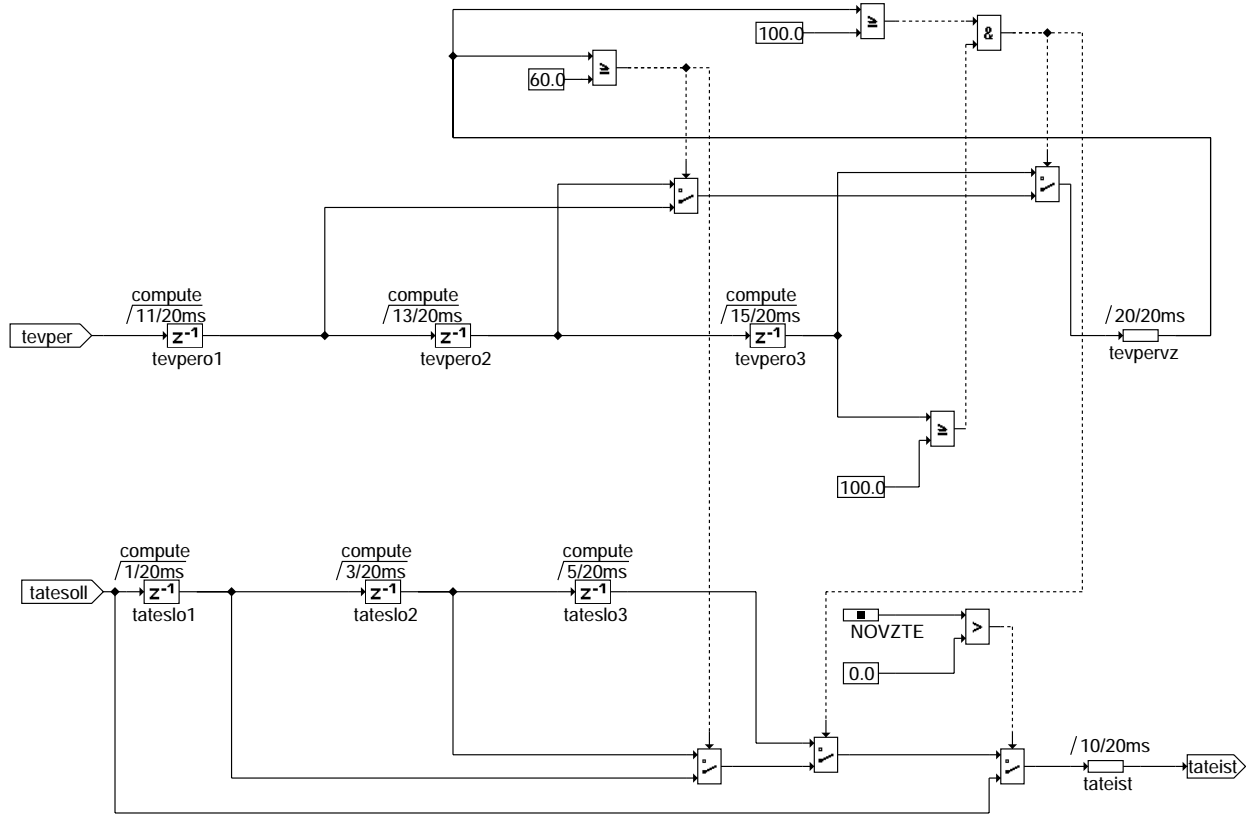
BGTEV: Function BGTEV:



bgtev-main

bgtev-main

TATEISTB: Function part TATEISTB - Calculation of the actual duty cycle:

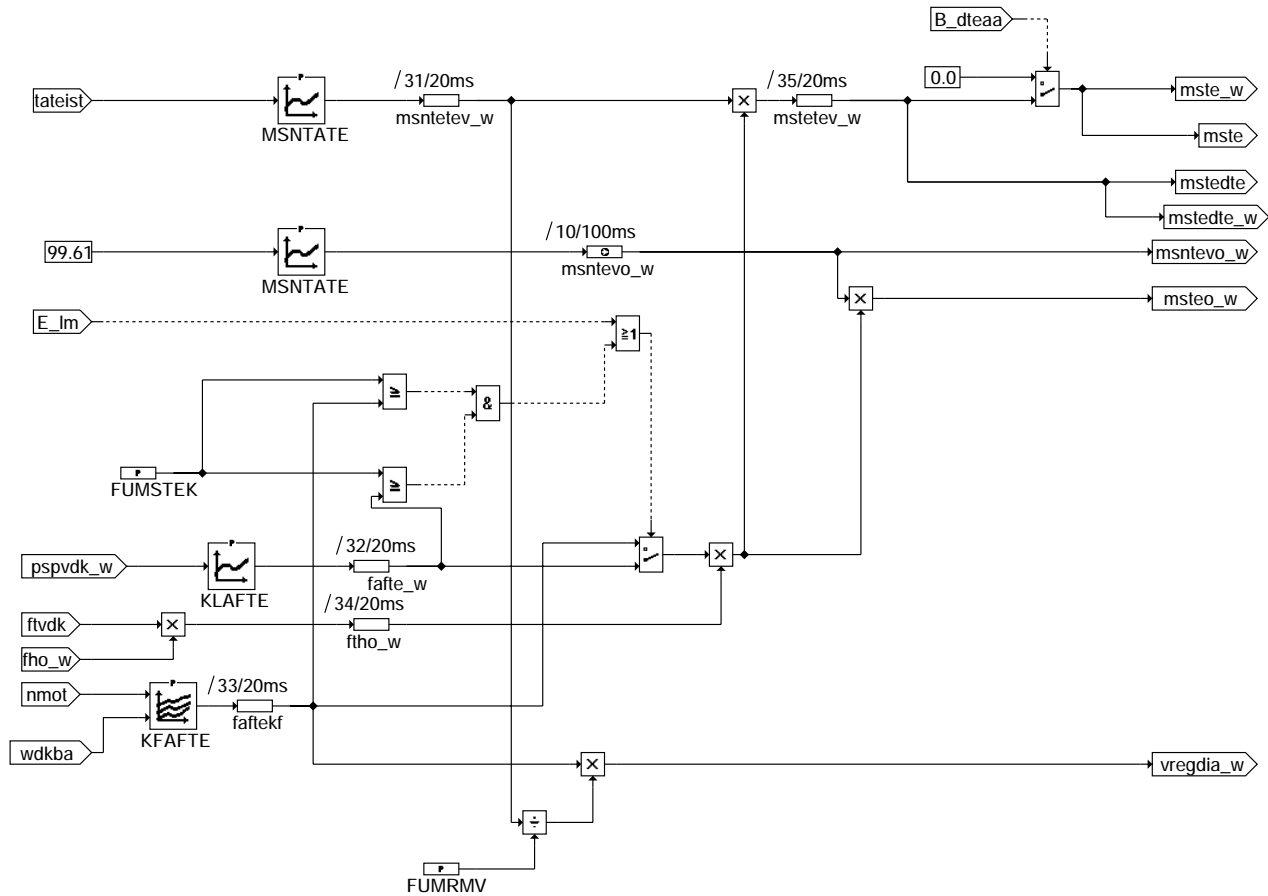


bgtev-tateistb

bgtev-tateistb



MSTEB: Function part MSTEB - Calculation of the PCV mass flow:



bgtev-msteb

### ABK BGTEV 1.70 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FUMRMV			FW	factor for density of the air
FUMSTEK			FW	factor for switching over to map-calculation of the mass-flow through the PCV
KFAFFE	NMOT	WDKBA	KF	map flow-characteristic of PCV (incl. PCV charcoal-canister line)
KLAFFE	PSPVDK_W		KL	characteristic of Saint-Venant of purge control valve an line AKF-TEV
MSNTATE	TATEIST		KL	Characteristic standardized mass flow through TEV
NOVZTE			FW	code word for desired duty cycle not delay

Variable	Source	Type	Description
B_DTEAA	DTEV	EIN	Condition diagnosis CPV by opening the CPV active
C_JNI	SWADAP	EIN	ECU-condition for initialisation
E_LM	EGFE	EIN	Error flag: main load sensor
FAFTEKF	BGTEV	LOK	factor flow through PCV: value from characteristic map
FAFTE_W	BGTEV	LOK	factor flow through PCV
FHO_W	BGPU	EIN	correction factor: altitude
FTHO_W	BGTEV	LOK	factor temperature and altitude depending correction of mass flow
FTVDK	SWADAP	EIN	correction factor for temperature upstream of throttle valve
MSNTETEV_W	BGTEV	LOK	normalized mass flow PCV (16 bit)
MSNTEVO_W	BGTEV	AUS	normalized mass flow through the complete open PCV
MSTE	BGTEV	AUS	mass flow purge control into the manifold
MSTEDTE	BGTEV	AUS	purge mass flow for DTEV
MSTEDTE_W	BGTEV	AUS	purge mass flow for DTEV (word)
MSTEO_W	BGTEV	AUS	Mass flow the 100 % opened TEV
MSTETEV_W	BGTEV	LOK	mass flow through the purge control valve
MSTE_W	BGTEV	AUS	mass flow purge control into the manifold
NMOT	SWADAP	EIN	engine speed
PSPVDK_W	EGFE	EIN	quotient: int.manif.pressure divided by pressure upstream of throttle valve
R_T20		EIN	Time schedule 20 ms
TATEIST	BGTEV	LOK	actual duty-cycle of the PCV
TATESLO1	BGTEV	LOK	desired dirty cycle of the PVC (delay of one calculation frame)
TATESLO2	BGTEV	LOK	desired dirty cycle of the PVC (delay of two calculation frames)
TATESLO3	BGTEV	LOK	desired dirty cycle of the PVC (delay of three calculation frames)
TATESOLL	GKRA	EIN	desired duty cycle of the PCV
TEVPER	ATEV	EIN	periode time of purge control valve
TEVPERO1	BGTEV	LOK	periode time of purge control valve delay of one calculation frame
TEVPERO2	BGTEV	LOK	periode time of purge control valve delay of two calculation frames



Variable	Source	Type	Description
TEVPERO3	BGTEV	LOK	periode time of purge control valve delay of three calculation frames
TEVPERVZ	BGTEV	LOK	delayed period time of the PCV
VREGDIA_W	BGTEV	AUS	gas volume flow through the purge control valve: for fuel tank diagnosis
WDKBA	GGDVE	EIN	throttle angle

### FW BGTEV 1.70 Fixed Values

Parameter	Value	Description
FUMRMV		factor for density of the air
FUMSTEK		factor for switching over to map-calculation of the mass-flow through the PCV
NOVZTE		code word for desired duty cycle not delay

### FB BGTEV 1.70 Detailed description of function

#### Introduction:

The section BGTEV calculates the mass flow (mste resp. mste\_w) which flows into the intake manifold via the purge control valve (PCV). Mste is included in the calculation in the load acquisition as additional air charge. In the canister purge control function mste\_w is needed for the later calculation of the ti-correction (rkte\_w). Furthermore the possible volume flow through a fully opened valve is needed (msteo\_w) for the canister purge control function.

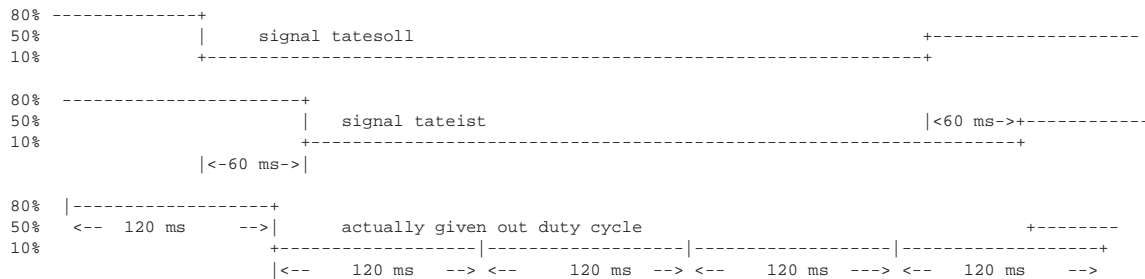
For the canister diagnosis a value of the volume flow PCV is needed which is independent of HFM tolerances. This value is also formed in BGTEV (vregdia\_w). Vregdia\_w is the product from the standardized mass flow PCV in the over-critical (msntetev) with the output value of a characteristic map over engine speed and throttle valve angle (KFAFTE) divided by the density of air (FUMRMV).

It is assumed that pure air flows through the PCV. In case of charged activated carbon filter, therefore, the HC molecules which flow through the PCV are considered just like air molecules. The thus resulting charge error can, however, be neglected when taking into consideration that at the max. only approx. 1/46 of the entire volume flow flowing into the intake manifold can consist of fuel particles. So in the extreme case (HC-conc. = 1) a charge error of approx. 2% at 50% fuel proportion canister purge control is obtained.

#### Calculation of the actual duty cycle on the PCV (tateist):

For the calculation of the mass flow through the purge control valve at first the "current, actual" duty cycle at the PCV must be calculated. For this it is assumed that the PCV-timer takes over the desired duty cycle in the mean delayed by half a period. With the thus delayed duty cycle (tateist) the current mass flow mste\_w is calculated.

Example: The PCV closes (resp. opens) e.g. at decreasing load (increasing load) with a period of 120 ms in the mean 60 ms later than is demanded by the requirement (tatesoll). By the delay by 60 ms tateist takes into consideration the mean "retarding" of the PCV.





Example for the calculated delay of the signal tateist and for the actually given out duty cycle Tatesoll

The calculation of tateist in detail:

The duty cycle tatesoll as well as the period are stored delayed up to 3-times (in the 20 ms grid) as a RAM-cell.

Remark: Apart from values for the duty cycle also values for the period need to be stored in order to be able to take into consideration that the PCV-timer each time processes the period transferred in the past and thus a change from a large period to a small period can only be taken over after the large period has passed.

The variable delayed period (tevpervz) is inquired upon:

- if tevpervz < 60 ms then the value of tevper (tevper(-1)) delayed by only one calculation cycle is used
- if tevpervz >= 60 ms but also <= 100 ms then the value of tevper (tevper(-2)) delayed by two calculation cycles is used
- if tevpervz >= 100 ms and at the same time also tevper(-3) >= 100 ms then tevper(-3) is used.

This additional And-inquiry is necessary so that in case of a period jump from e.g. tevper = 30 ms to tevper = 120 ms at first after one calculation cycle the 120 ms, but then again the 30 ms are given for a calculation cycle as delayed duty cycle tevpervz.

For the calculation of the delayed duty cycle it is now only necessary to give the selection conditions for the period also to the switches for the selection of the corresponding 1-,2-,3-times delayed duty cycle. Thus the value for tateist can be obtained from tatesoll.

Important: The switch is operated only after the calculation of tateist.

With the codeword "NOVZTE" the delay of tatesoll can be switched off.

Calculation of the mass flow into the intake manifold (mste\_w):  
-----

Principally two different calculation types for the mass flow through the purge control valve must be distinguished:

- a) The calculation derived from the KLAFFE - characteristic line
- b) The calculation derived from a characteristic map KFAFFE over the engine speed and the throttle valve angle

to a) The mass flow through a valve depends on the quotient of the pressures ps\_w/pvdk\_w = pspvdk\_w. Because of the long pipes there is needed a special KLAFFE for the PCV flow.

to b) It cannot be ruled out that while being at full load ps\_w/pvdk\_w is slightly wrong. That causes big deviations in mste\_w if the KLAFFE is still used for calculation. Furthermore local small vacuums can occur (Bernoulli) due to flow effects on the PCV. Here it may be necessary to switch-over to an adjusted characteristic map value. In the characteristic map KFAFFE (characteristic map outflow purge control valve) the actually measured values of the mass flow through the PCV (incl. pipe) must be stored pressure- and altitude-corrected and divided by MSNTATE. So to speak KFAFFE contains the individual flow rate characteristics for PCV and pipe. KFAFFE has just as KLAF values between 0 and 1.0. So as to obtain a harmonic quantization with fafte\_w the value range, however, is [0... < 2].

Remark: The mass flow at given external temperature and at given pressure can be measured by means of a "mass flow meter". With this and from the determined characteristic line (MSNTATE) the values of the individual flow rate function PCV + pipe can be calculated.

$$KFAFFE = mstetev\_measured / MSNTATE / (ftho\_w)$$

$$- ftho\_w = \text{correction temperature} = \sqrt{273 \text{ K} / \text{tans}} \quad \text{and correction pressure} = pu / 1013 \text{ hPa}$$

The change-over from the value determined under a) and the value determined under b) is performed as soon as the KLAFFE as well as once the characteristic map value from KFAFFE lies below the threshold FUMSTTEK.

Thus it is achieved that close to full load the characteristic map value is given out. However, in case of lower intake manifold pressures the value calculated from the HFM-signal which is also correct with regard to dynamics is used.

With B\_dteaa = TRUE the mass flow mste\_w is set Zero to switch off the consideration of the purge mass flow in the complete system. (load detection, throttle activation, purge control function). This is important for the diagnosis of the purge valve, because the effect of valve opening should cause a reaction in the system (idle control closes the throttle, Lambda controller corrects Lambda deviation).

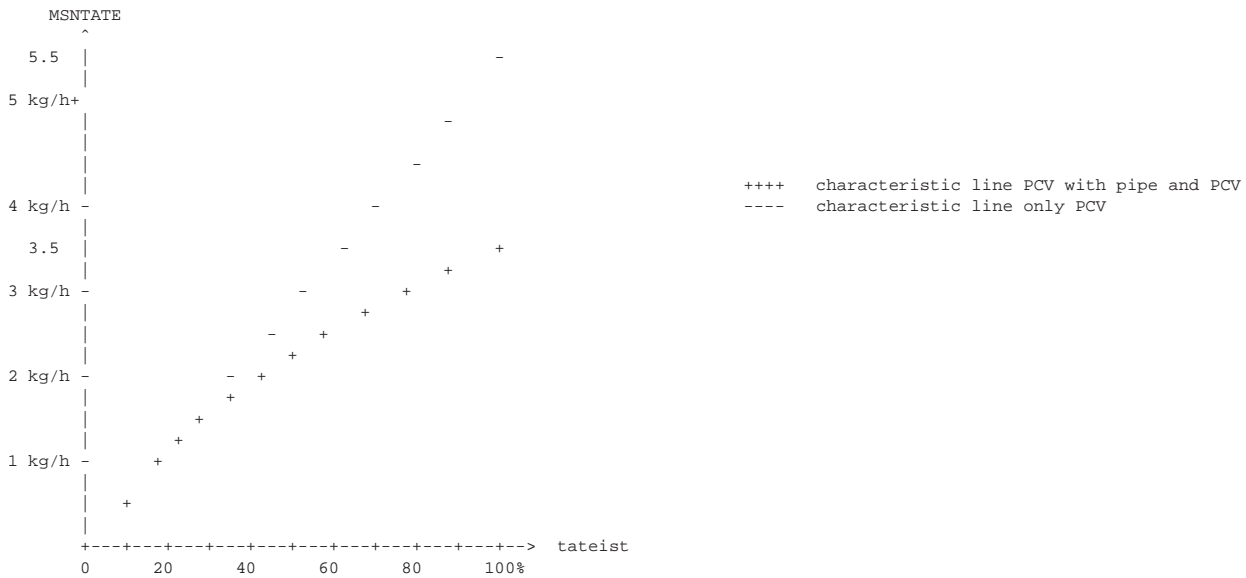
Examples from the application (MSNTATE and KLAFFE) - Taking into consideration the flow resistance of the pipe "ACF-PCV":  
-----

Duty cycle-dependent correction:

By the freely adjustable opening characteristic MSNTATE any PCV-characteristic line can be taken into consideration. In addition it can be considered that with a high flow resistance of the pipes and of the ACF also in case of a linear characteristic of the PCV a curved characteristic line msntetev\_w = f(tate) is obtained.



Example for MSNTATE for a PCV with mass flow 5.5 kg/h (without pipe, without ACF) and 3.5 kg/h with ACF and pipe

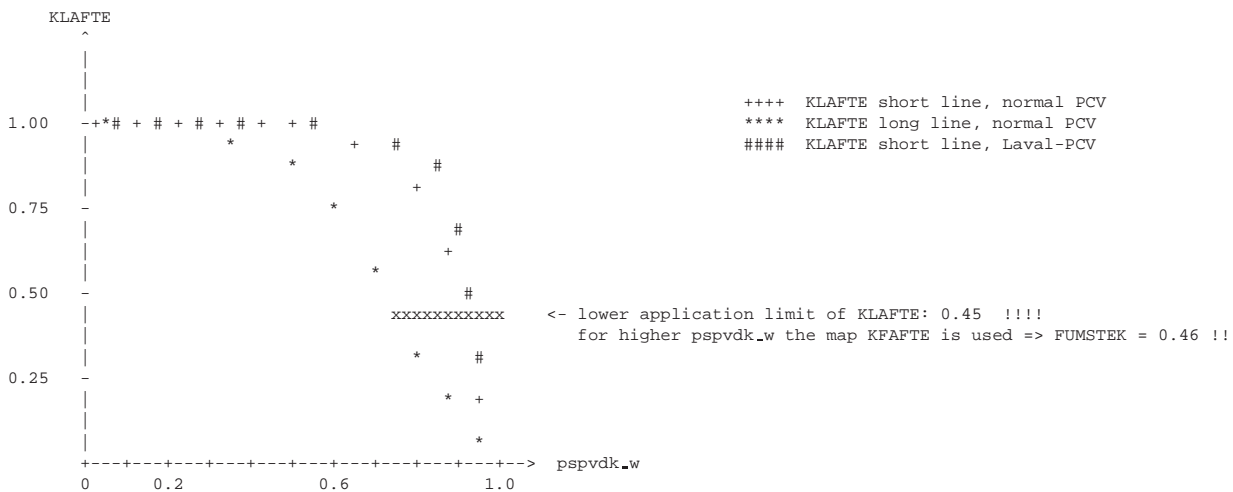


Example of a characteristic line MSNTATE (correction is dependent on duty cycle).  
Characteristic line measured at very low intake manifold pressure ( $p_{s/pu} < 0.3$ )

From this example it becomes obvious:

- The pipe upstream of the PCV and the ACF markedly reduce the mass flow (5.5 kg/h  $\rightarrow$  3.5 kg/h)
- The linear characteristic line over the duty cycle becomes curved.

Example for the KLAFFE:



After having selected the best value of the flow rate characteristic (faftekf or fafte\_w) for the corresponding operating state the selected value is corrected with regard to altitude and pressure (multiplication by ftho\_w). The thus corrected value is multiplied by msntetev\_w. The duty cycle-dependent mass flow through the PCV is obtained.

In a later version of the BGTEV also the pipe PCV-intake manifold can be taken into consideration (storage effect).

In this BGTEV msntetev\_w is identical to the output value mste\_w.

Apart from the current flow rate also the flow rate through the fully opened PCV is needed in the TEB. Msteo\_w is calculated from MSTATE if 100% (resp. 99.61% = FF HEX) is assumed as input.

## APP BGTEV 1.70 Application hint

Values for the "initial application":

- FUMSTEK = 0.46

- FUMRMV = 1.3

- MSNTATE - base points/ values	0	11.1	22.2	33.3	44.4	55.5	66.6	77.7	88.8	100	[%]
	0	0.634	1.269	1.903	2.537	3.1718	3.80664	4.441	5.07500	5.72	[kg/h]

KFAFTE:

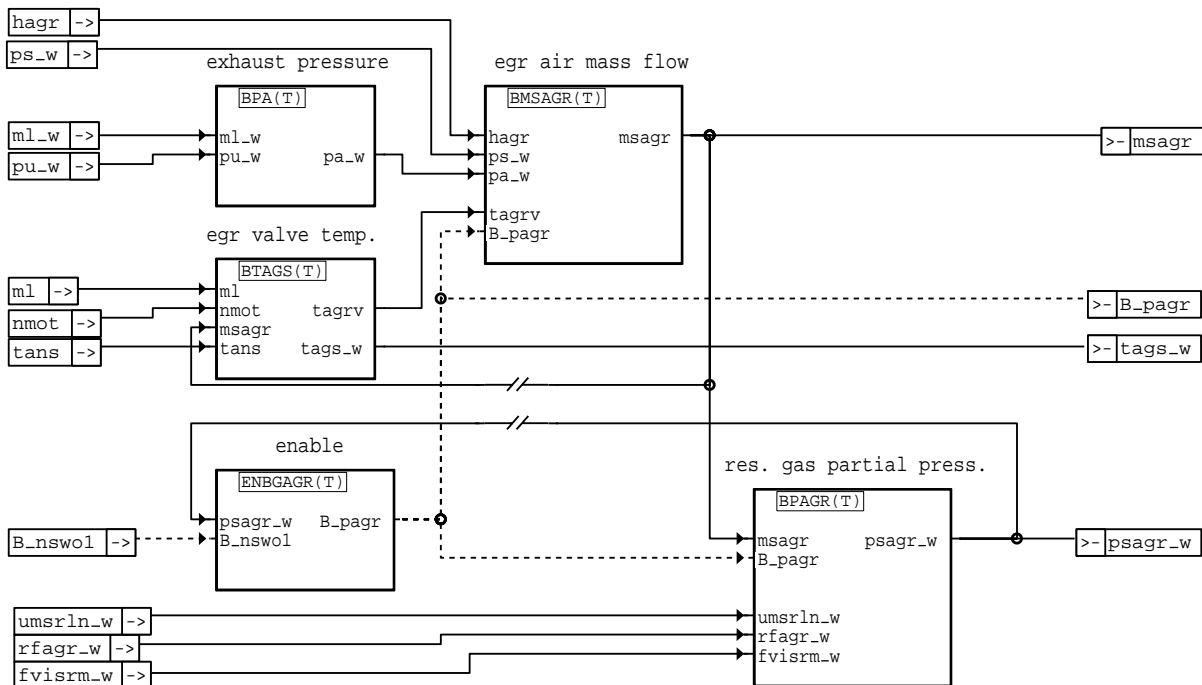
wkba / nmot	600	800	1000	1400	1800	2400	3000	3500	4000	5000 rpm
4%	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
10%										
16%	0.60	0.80	0.90	1.00	1.00	1.00	1.00	1.00	1.00	1.00
24%										
34%	0.20	0.50	0.80	0.95	1.00	1.00	1.00	1.00	1.00	1.00
45%										
55%	0.05	0.1	0.40	0.60	0.85	0.90	0.95	1.00	1.00	1.00
65%										
80%	0.01	0.02	0.08	0.15	0.40	0.50	0.60	0.70	0.75	0.80
99.61%	0.01	0.01	0.04	0.08	0.20	0.25	0.30	0.35	0.40	0.45

KLAFTE see under %FB.

## BGAGR 1.40 Correction air charge calculation by exhaust gas recirculation

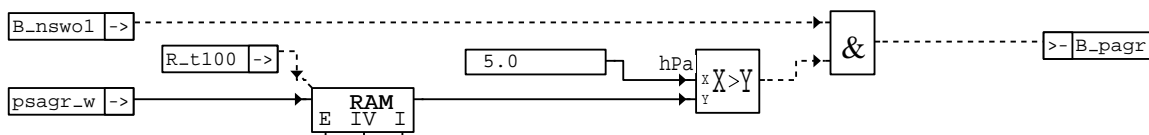
### FDEF BGAGR 1.40 Function definition

BGAGR: functional overview



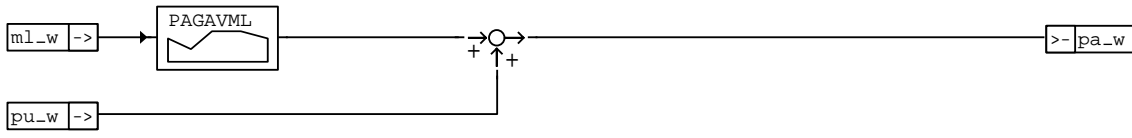
### bgagr-bgagr

ENBGAGR: enable condition



### bgagr-enbgagr

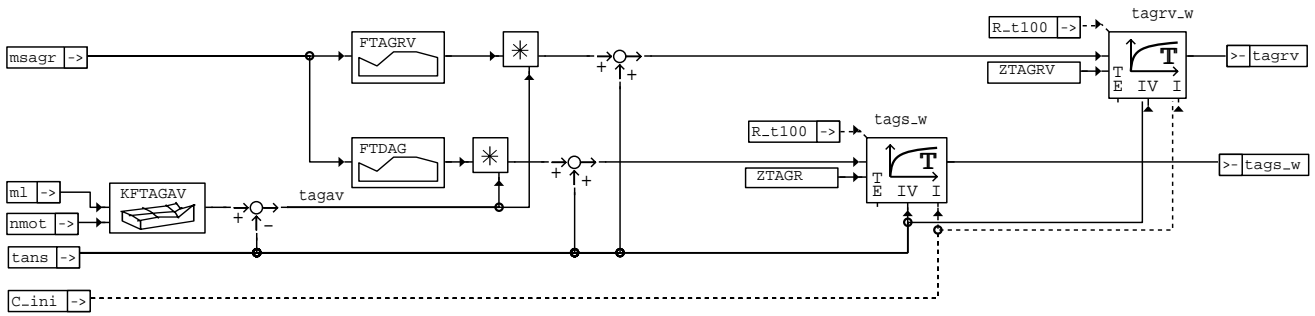
BPA: calculation of exhaust pressure



bgagr-bpa

### bgagr-bpa

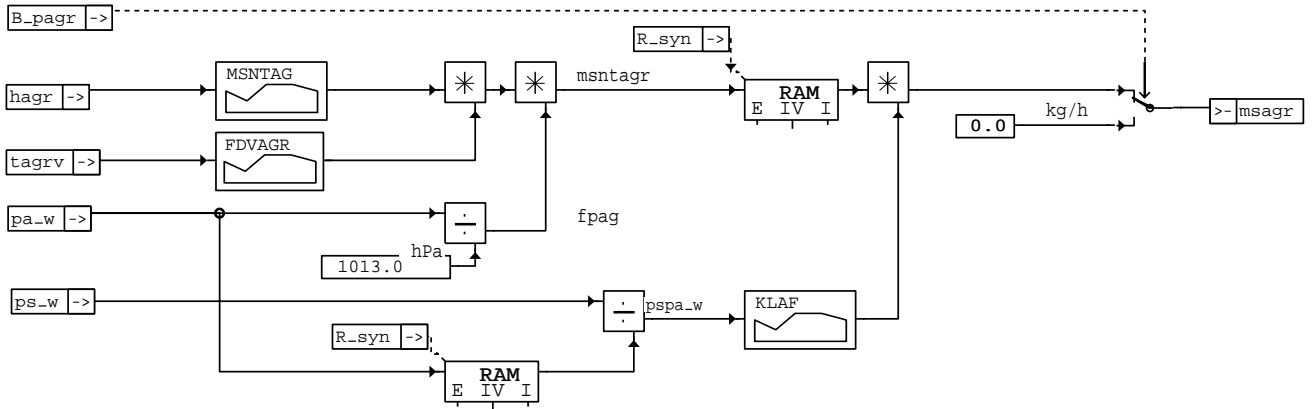
BTAGS: calculation of egr valve temperature



bgagr-btags

### bgagr-btags

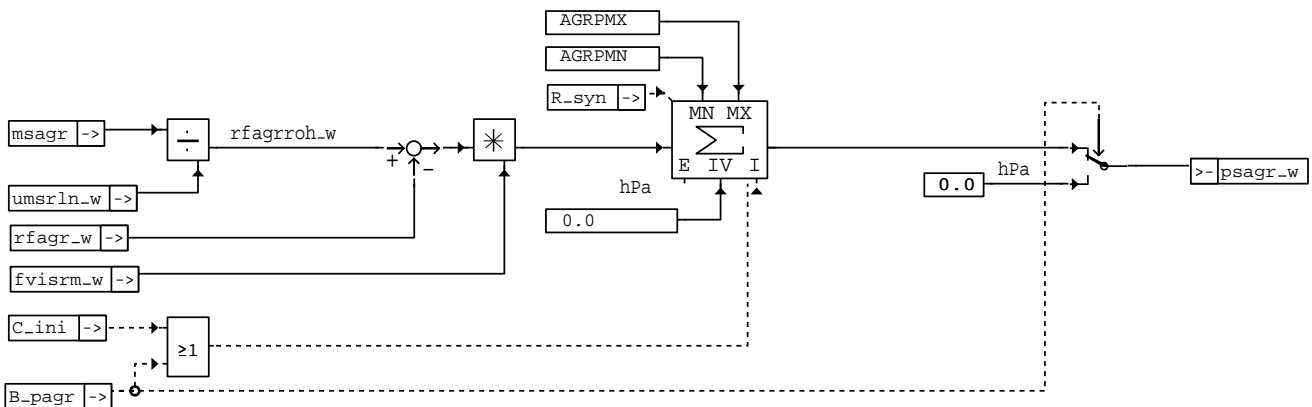
BMSAGR: calculation of egr air mass flow



bgagr-bmsagr

### bgagr-bmsagr

BPAGR: calculation of EGR partial pressure inside manifold



bgagr-bpagr

### bgagr-bpagr





## ABK BGAGR 1.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
AGRPMN			FW	minimum EGR partial pressure
AGRPMX			FW	maximum EGR partial pressure
FDVAGR	TAGRV		KL	factor temperature for flow through EGR valve
FTAGRV	MSAGR		KL	Factor for temperature drop from EGR_pipe to EGR_valve
FTDAG	MSAGR		KL	factor for temperature drop on EGR line
KFTAGAV	ML	NMOT	KF	EGR temperature at outlet valve
KLAF	PSPA_W		KL	characteristic of Saint-Venant
MSNTAG	HAGR		KL	EGR mass flow standardised
PAGAVML	ML_W		KL	exhaust gas pressure at outlet valve
ZTAGR			FW	time constant for EGR temperature model
ZTAGRV			FW	Time constant for EGR temperature model EGR valve

Variable	Source	Type	Description
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_PAGR	BGAGR	AUS	egr calculation disabled
C_JNI	SWADAP	EIN	ECU-condition for intialisation
FPAG	BGAGR	DOK	factor: exhaust gas pressure
FVISRM_W	BGSRM	EIN	integrator amplifier factor intake manifold modell
HAGR	EGAG	EIN	Stroke EGR valve
ML	SWADAP	EIN	air mass flow
ML_W	EGFE	EIN	air mass flow filtered (Word)
MSAGR	BGAGR	AUS	EGR mass flow into intake manifold
MSNTAGR	BGAGR	DOK	aktual supersonic EGR mass flow
NMOT	SWADAP	EIN	engine speed
PA_W	BGAGR	LOK	absolute pressure exhaust manifold
PSAGR_W	BGAGR	AUS	partial pressure EGR
PS_W	EGFE	EIN	intake manifold pressure (absolute) (Word)
PU_W	BGPU	EIN	Ambient pressure
RFAGRROH_W	BGAGR	DOK	EGR charge portion into intake manifold
RFAGR_W	BGSRM	EIN	relative load by external exhaust gas reduction
R_SYN	GGDPG	EIN	Synchro schedule
R_T100		EIN	Time schedule 100 ms
TAGAV	BGAGR	DOK	EGR temperature at point of outlet valve
TAGRV	BGAGR	LOK	EGR valve temperature
TAGRV_W	BGAGR	DOK	EGR valve temperature (Word)
TAGS_W	BGAGR	AUS	EGR temperature on introduction into intake manifold
TANS	SWADAP	EIN	Intake air temperature
UMSRLN_W	BGMSZS	EIN	calculation factor load to mass flow

## FW BGAGR 1.40 Fixed Values

Parameter	Value	Description
AGRPMN		minimum EGR partial pressure
AGRPMX		maximum EGR partial pressure
ZTAGR		time constant for EGR temperature model
ZTAGRV		Time constant for EGR temperature model EGR valve

## FB BGAGR 1.40 Detailed description of function

The section BGAGR calculates the EGR mass flow into the intake manifold. The EGR temperature necessary for the calculation is determined in a temperature model.

The manufacturer of the EGR valve supplies a characteristic which can be translated into characteristic MSNTAG. The EGR standardised mass flow should be dependent on the targeted duty factor in MSNTAG. The standard conditions are: EGR mass flow at atemperature of 0 degrees Celsius, ratio of pressure downstream to pressure upstream of valve < 0.52 corresponds to supercritical. Pressure upstream of valve = 1013hPa.

The mass flow is adapted to the actual pressure conditions via the characteristic KLAF (standardised flow through a valve), which is addressed with the ratio pspag of intake manifold pressure ps to exhaust gas pressure pag. The exhaust gas counterpressure is composed from the ambient pressure pu and the pressure loss in the exhaust gas system, which must be measured in the application phase and stored in characteristic PAGAVML. The pressure loss increases as the air flow through the engine increases. PAGAVML is therefore dependent on ml. The pressure correction factor fpag is used to adapt to the actual pressure upstream of the valve.

The characteristic FDVAGR corrects the standardized EGR mass flow to the EGR mass flow at actually temperature at inlet of intake manifold in dependent of the modelled EGR temperature

The standard EGR mass flow is calculated with the corrections described into the actual mass flow msagr, which flows through the EGR valve.

## APP BGAGR 1.40 Application hint

The standardised flow through throttle valve KLAF is specified by physics, and is stored as a 501 \* 16 bit table in the Eprom. The fine stepping from value to value is particularly necessary in the subcritical operating range, since the intake manifold model tends to oscillate if the stepping is spread too coarsely.

The values table for the outflow characteristic KLAF can be requested as an EXCEL file from H.Pfitz K3/ESY5 Tel. 8502 if required.

!!!! The KLAF is stored only once for the entire project in the EPROM (FLASH), due to the available memory space!!!!

The KLAF input value is calculated in the relevant modules and transferred in a RAM cell. Then the corresponding output value of the KLAF is calculated using the transfer value, and the KLAF value is used for further calculations in the relevant software modules.

Characteristic FDVAGR for density correction of the EGR mass flow as function of tags[°C]

$$FDVAGR = \sqrt{\frac{T_0}{T}} \quad \text{standard temperature } T_0 \text{ ist } 0^\circ\text{C} = 273\text{K} \rightarrow f_{tags} (0^\circ\text{C}) = 1.0$$

Values for characteristic FDVAGR:

tags	-40	0	40	100	200	300	400	700
FDVAGR	1.0824	1.0	0.9339	0.8555	0.7597	0.6902	0.6369	0.5296

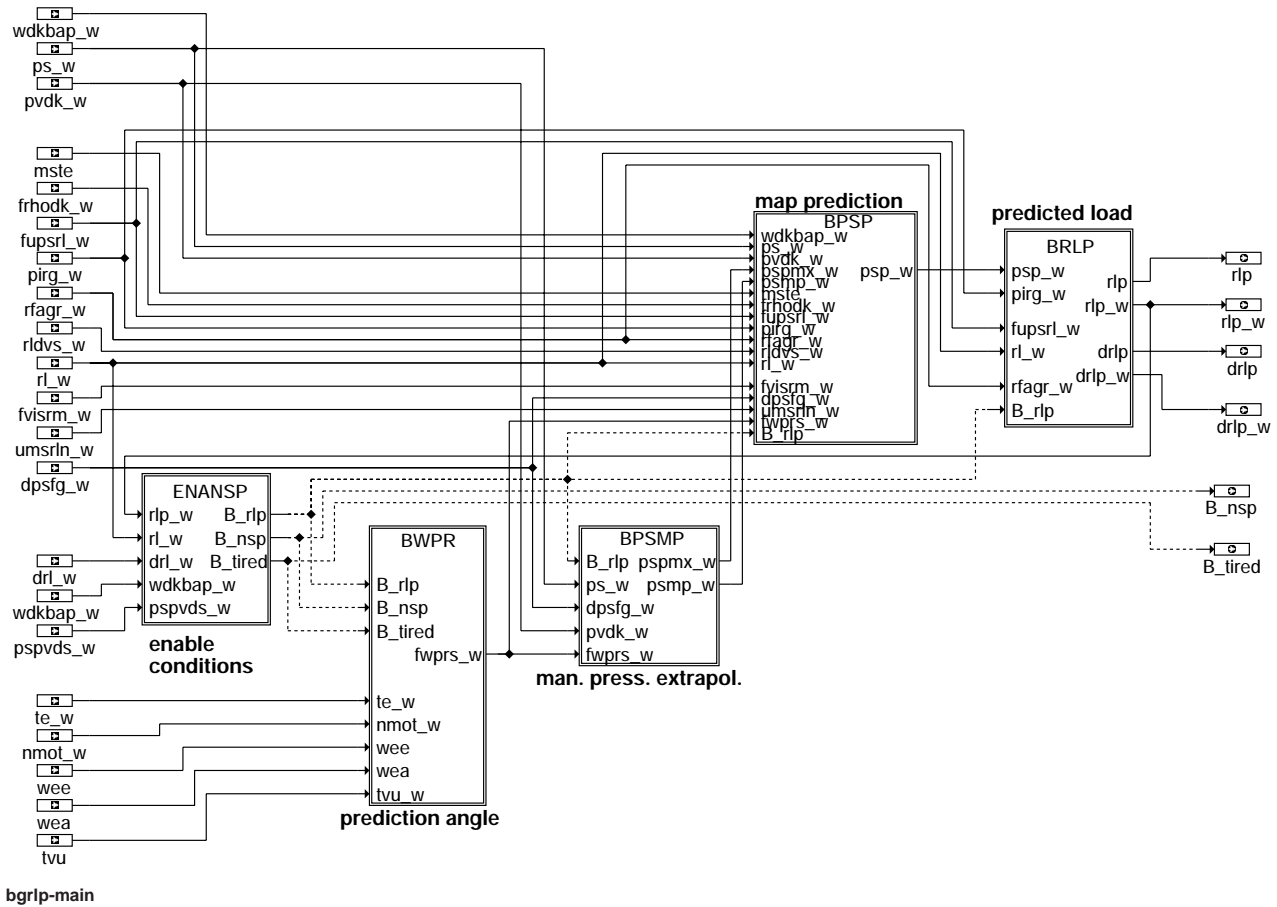
For application:

function disable: agrvp\_w = 0 see function GGAGRV, or MSNTAG = 0 completely --> msagr = 0  
PAGRMX = PAGRMN = 0 --> psagr\_w = 0 hPa

## BGRLP 4.50 Calculation variable rlp: predicted air charge

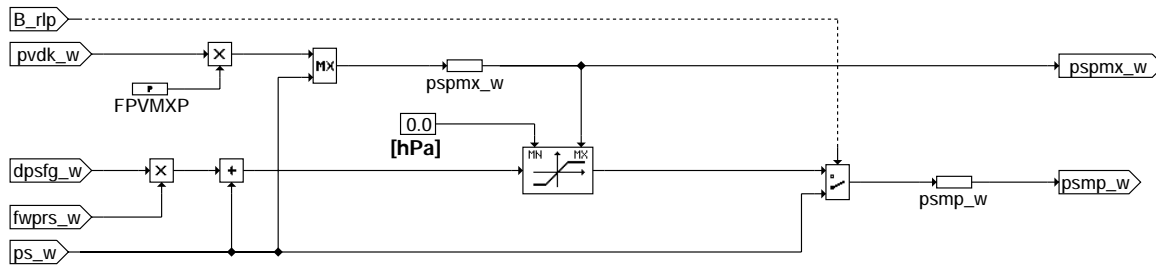
### FDEF BGRLP 4.50 Function definition

BGRLP: Overview - load prediction



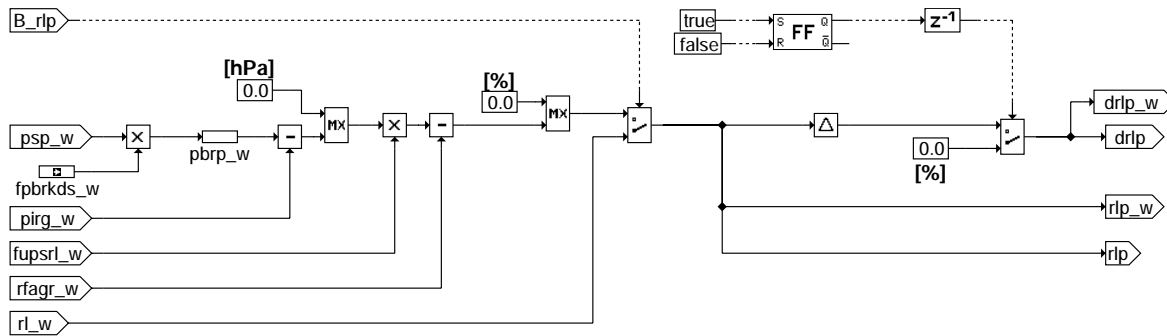


BPSMP: 1. Inlet manifold pressure extrapolation



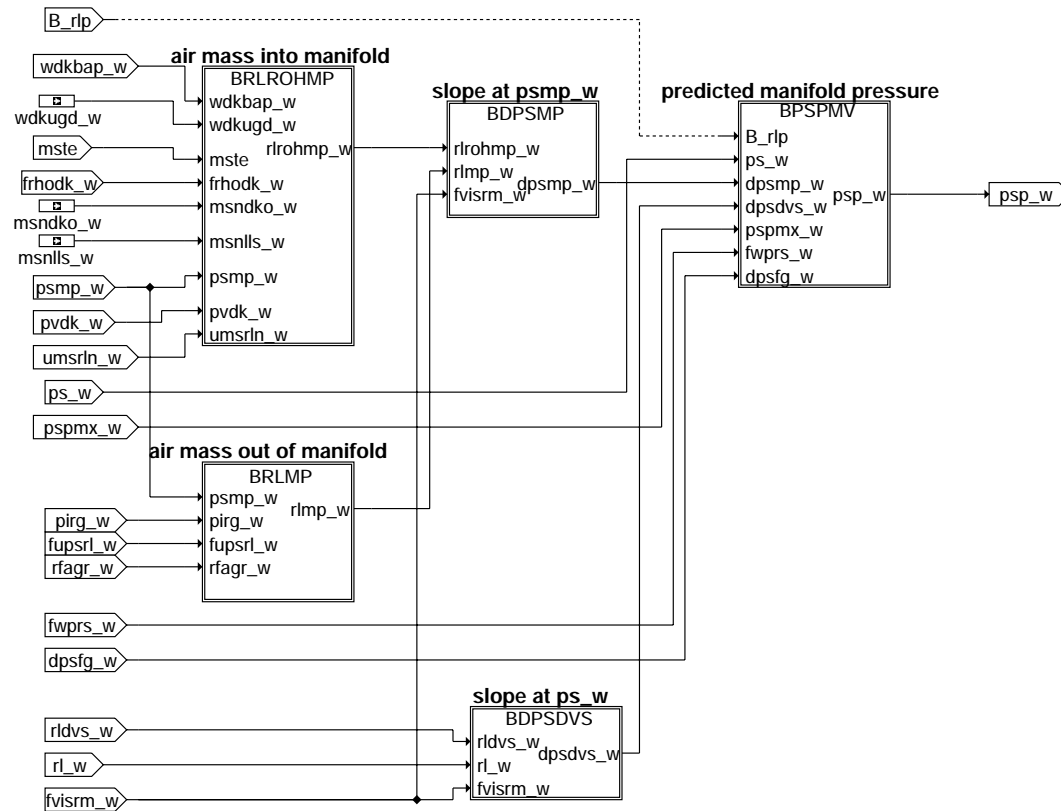
**bgrlp-bpsmp**

BRLP: Calculation of predetermined air charge rlp\_w



**bgrlp-brlp**

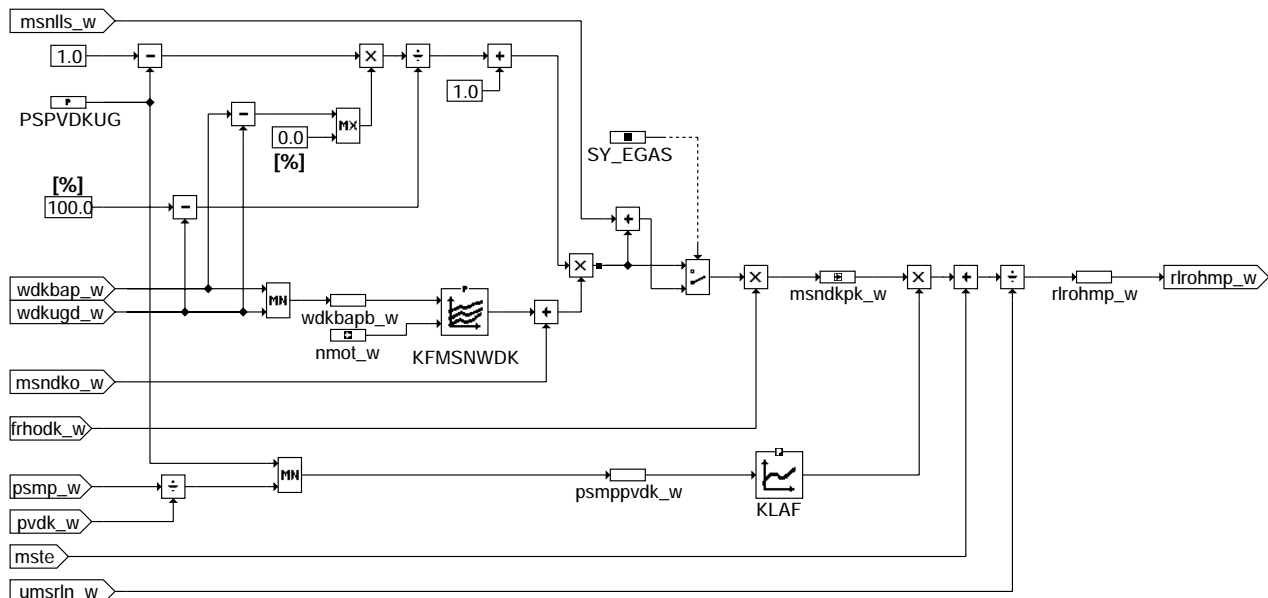
BPSP: Calculation of predetermined inlet manifold pressure psp\_w



**bgrlp-bpsp**

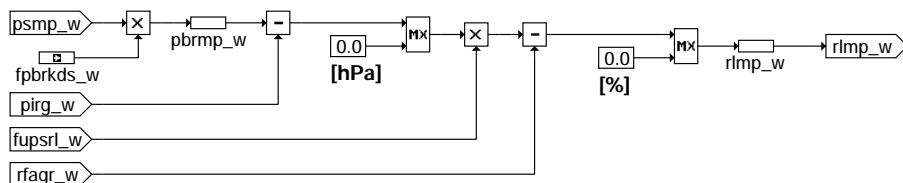


BRLROHMP: Air mass flowing into the inlet manifold at  $psmp\_w$



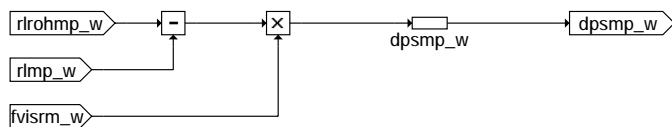
### bgrlp-brrohmp

BRLMP: Air mass flowing out of the inlet manifold at  $psmp\_w$



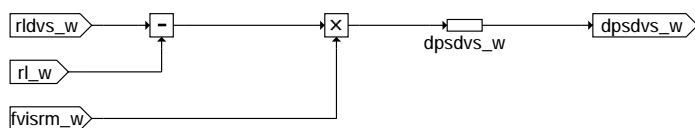
### bgrlp-brimp

BDPSMP: Inlet manifold pressure gradient at  $psmp\_w$



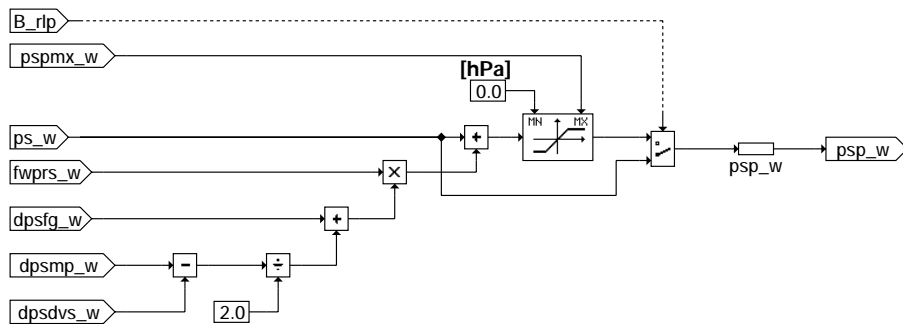
### bgrlp-bdpsmp

BDPSDVS: Inlet manifold pressure gradient at  $ps\_w$



### bgrlp-bdpsdvs

BPSPMV: Calculation of predetermined inlet manifold pressure with the average of  $dps\_w$  and  $dpsmp\_w$



### bgrlp-bpspmv



## ABK BGRLP 4.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CBGRLP			FW	Code word configuration function BGRLP
DRLDYNU			FW	drl threshold value for te post injection/reduction
DRLMIN			FW	Minimal charge change for triggering of post injection
DTEPRU			FW	delta-te threshold for post injection/ti-reduction detected
DWPR			FW	Delta prediction angle without post injection/ti-reduction
DWPRNSP			FW	Delta prediction angle at post injection release
FPVMXP			FW	factor for pressure ratio maximum for load prediction
KFMNSWDK	WDKBAPB_W	NMOT_W	KF	Map for scaled mass flow over throttle valve
KLAF	PSMPPVDK_W		KL (REF)	characteristic of Saint-Venant
PSPVDKUG			FW	Ratio pspvdk not reduced
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TNSURLP			FW	Time rl prediction suppression in post-start
WPRMX			FW	maximum prediction angle
Variable	Source		Type	Description
B_DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B_LL	MSF		EIN	Condition idle
B_NSP	BGRLP		AUS	condition for post-injection
B_NSWO2	PROKON		EIN	condition engine speed > NSWO2
B_RLP	BGRLP		LOK	condition for load prediction
B_RLPNS	BGRLP		LOK	Enable condition load prediction after cranking
B_ST	SWADAP		EIN	condition for start
B_STEND	BBSTT		EIN	condition end of start
B_TIRED	BGRLP		AUS	Condition reduction of active injections
B_JGDSP	BGRLP		LOK	condition predicted set value throttle angle near full load
DPSDVS_W	BGRLP		LOK	Delta intake manifold pressure from throttle valves (Word)
DPSFG_W	BGSRM		EIN	delta fresh air partial pressure in manifold
DPSMP_W	BGRLP		LOK	delta extrapolated intake manifold pressure (Word)
DRLP	BGRLP		AUS	delta predicted load for injection time calculation
DRLP_W	BGRLP		AUS	delta predicted load for injection time calculation (word)
DRL_W	SWADAP		EIN	charge change (Word)
E_DK	DDVE		EIN	Error flag: throttle position sensor
FPBRKDS_W	BGSRM		EIN	factor for determination of combustion chamber pressure
FRHODK_W	EGFE		EIN	factor correction air density for throttle valve flow f(intake air temp.,altit.)
FUP SRL_W	EGFE		EIN	factor system related transformation pressure to load (16-Bit)
FVISRM_W	BGSRM		EIN	integrator amplifier factor intake manifold modell
FWPRS_W	BGRLP		LOK	Factor prediction angle with respect to segment
GRUNDWERT			EIN	space between SW reference mark to TDC in °KW
MSNDKO_W	EGFE		EIN	norm leakage air mass flow through throttle blade
MSNDKPK_W	BGRLP		LOK	normalized predicted corrected mass flow over throttle (word)
MSNLLS_W			EIN	standardised air mass flow through idle speed actuator (word)
MSTE	BGTEV		EIN	mass flow purge control into the manifold
NMOT_W	SWADAP		EIN	engine speed
PBRMP_W	BGRLP		LOK	extrapolated combustion chamber pressure (Word)
PBRP_W	BGRLP		LOK	predicted combustion chamber pressure (Word)
PIRG_W	EGFE		EIN	partial pressure residual exhaust gas internal EGR (16-Bit)
PSMPPVDK_W	BGRLP		LOK	predicted manifold pressure/pressure upstream throttle plate
PSMP_W	BGRLP		LOK	extrapolated intake manifold pressure (Word)
PSPMX_W	BGRLP		LOK	maximum predicted intake manifold pressure
PSPVDS_W	BGMSZS		EIN	quotient manifold pressure/pressure before throttle plate
PSP_W	BGRLP		LOK	predicted intake manifold pressure (Word)
PS_W	EGFE		EIN	intake manifold pressure (absolute) (Word)
PVDK_W	EGFE		EIN	pressure upstream of throttle valve, 16-bit
RFAGR_W	BGSRM		EIN	relative load by external exhaust gas reduction
RLDVS_W	EGFE		EIN	relative air charge through throttle valves on intake manifold
RLMP_W	BGRLP		LOK	rel. extrapolated air charge (Word)
RLP	BGRLP		AUS	rel. air charge predicted for injection calculation
RLP_W	BGRLP		AUS	rel. air charge predicted for injection calculation (Word)
RLROHMP_W	BGRLP		LOK	Relative air filling intake manifold flow for intake manifold pres. psmpp_w(Word)
RL_W	EGFE		EIN	relative air charge (Word)
TE_W			EIN	effective injection time (word)
TVU			EIN	supply of voltage correction
UMSRLN_W	BGMSZS		EIN	calculation factor load to mass flow
VWKW	BGRLP		LOK	crankshaft angular speed
WDKBAPB_W	BGRLP		LOK	predicted limited throttle angle wdkbl for ti-calculation (Word)
WDKBAP_W	BGWDKM		EIN	predicted throttle angle wdkbl for ti-calculation (Word)
WDKUGD_W	BGMSZS		EIN	Throttle valve angle during which 95% charge is reached
WEA	ESVW		EIN	anglemark injection break off
WEE	ESVW		EIN	angle injection-end in normal operation
WESSBM			EIN	angle: intake valve closes late until reference mark
WPR	BGRLP		LOK	Calculated injection angle for load prediction
WPRNSP	BGRLP		LOK	Calculated injection angle for load prediction for behind injection



## FW BGRLP 4.50 Fixed Values

Parameter	Value	Description
CBGRLP		Code word configuration function BGRLP
DRLDYNU		drl threshold value for te post injection/reduction
DRLMIN		Minimal charge change for triggering of post injection
DTEPRU		delta-te threshold for post injection/ti-reduction detected
DWPR		Delta prediction angle without post injection/ti-reduction
DWPRNSP		Delta prediction angle at post injection release
FPVMXP		factor for pressure ratio maximum for load prediction
PSPVDKUG		Ratio pspvk not reduced
TNSURLP		Time rl prediction suppression in post-start
WPRMX		maximum prediction angle

## FB BGRLP 4.50 Detailed description of function

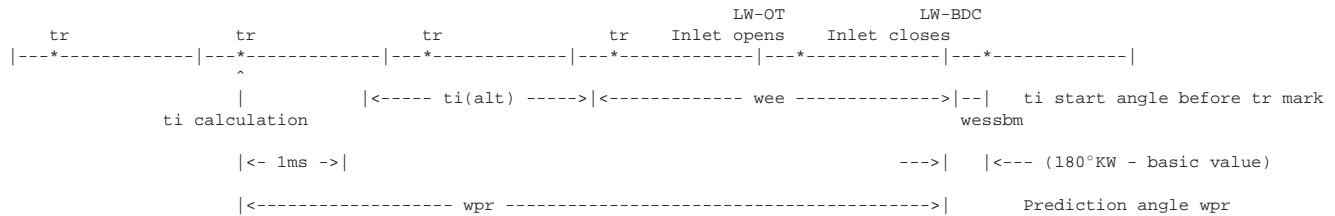
Prediction of the injection calculation load:

The charge cycle BDC determines the air charge of the des cylinder largely irrespective of the camshaft control times, since the pressure between the inlet manifold and the cylinder is balanced.  
The load signal rl\_w is based on the current inlet manifold pressure ps\_w and describes the air charge of the currently inducting cylinder.  
Since there is a time lag until the LW-BDC of the cylinder belonging to the currently calculated ti, the inlet manifold pressure can still change greatly.  
Based on a future Dk actual angle wdcbap\_w and knowing the differential crank angle to LW-BDC (prediction angle wpr), the inlet manifold pressure at LW-BDC psp\_w can now be pre-calculated.

The whole prediction of the injection calculation load can be switched off with CBGRLP[bit 0 = 0].

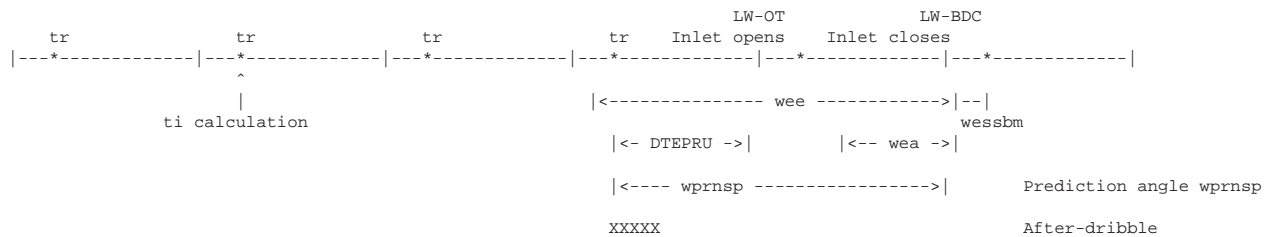
### 1. Standard case without after-dribble / intermediate dribble or ti reduction enable

The crank angle from tr mark to ignition TDC (basic value) is 108 °KW in this case



First the crank angle between the current load -/ti calculation in the synchro at a tr mark and the charge cycle BDC of the corresponding cylinder is determined (--> prediction angle wpr). The first step is to determine the angle between tr mark and ti start + lms (= estimated synchro calculation time).  
This angle is rounded up to whole segments (720°KW/SY\_ZYLZA), giving the number of whole segments between ti calculation and tr mark of the cylinder under consideration.  
The air mass message for 1 segment means that rl\_w can be directly timed to the tr mark;  
But then 180°KW - basic value (tr mark v. ignition TDC) must be deducted to give the angle difference from the moment of load measurement to LW BDC (= Prediction angle wpr).

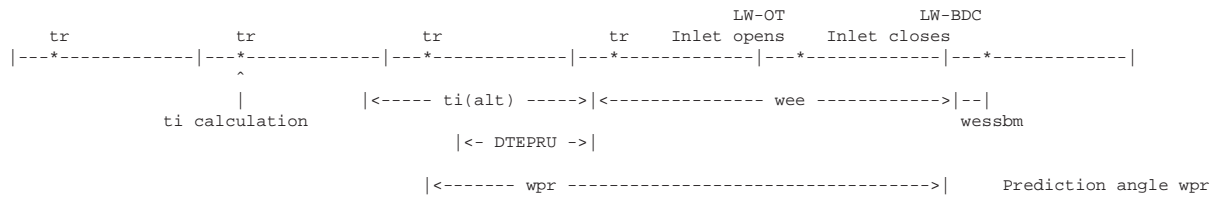
### 2. with after-dribble / intermediate dribble enable



If the predicted load rlp\_w is significantly greater than the current load rl\_w (--> DRLDYNU), the intermediate/after-dribble mechanism of the CIFDI is enabled (B\_nsp = 1).  
Since extension of ongoing injections or additional after-dribble is now allowed, the KW prediction angle used is the last update opportunity at a tr mark and the inlet closing crankshaft of the cylinder concerned.  
It is assumed that the ti for one cylinder can then still be updated if a time of at least DTEPRU (typically 5 ms) remains from the end of the ti calculation to the termination of angle injection wea (see %EA), enabling a viable intermediate dribble length.  
This special treatment of the prediction angle wpr where B\_nsp = 1 can be prevented by CBGRLP[biz 1 = 0].



3. With ti reduction enable:



If the predicted load `rlp_w` is significantly smaller than the current load `rl_w` ( $\rightarrow$  DRLDYNU), the ti reduction mechanism of the CIFI is enabled (`B_tired = 1`).

Since a ti reduction of ongoing injections is now allowed, the crankshaft prediction angle `wprnsp` used is the last update opportunity at a `tr` mark and the inlet closing crankshaft of the cylinder concerned.

The last update opportunity is selected in such a way that at least one more injection time (to be shortened) of DTEPRU (typically 5 ms) remains.

This special treatment of the prediction angle `wpr` at `B_tired = 1` can be prevented by `CBGRLP[biz 2 = 0]`.

At start, when moving from start to after-start, and shortly after start-end, `rlp_w` is supplied with the direct main load signal `rl_w`.

Prediction can also be completely switched off with `CBGRLP[biz 0 = 0]`.

### APP BGRPLP 4.50 Application hint

Requirements:

- Static main load detection correct
- Ancillary load detection correct, i.e. `msdk_w` must match `mshfm_w`
- Dynamic load detection correct, i.e. `ps_w` matches statically and dynamically measured inlet manifold pressure profile
- Tidal air angle as late as possible (fuel flight time before inlet opening = approx. 8ms with normal injector installation)
- Injection termination angle as late as possible (approx. fuel flight time before charge cycle BDC)
- Gap between tidal air angle and injection termination angle so large that intermediate/after-dribble still have room N dynamic too ( $>= 4ms$ ); otherwise the CIFI cannot initiate any after-dribble!!
- Tidal air angle as late as possible (fuel flight time before inlet opens = approx. 8ms with normal injection valve installation)
- Injection termination angle as late as possible (approximate fuel flight time before charge cycle BDC)
- Gap between tidal air angle to injection termination large enough for space for intermediate and after-dribble even with N dynamic ( $>= 4ms$ ); otherwise CIFI cannot initiate any after-dribble!!
- Dk prediction correctly applied (see `%BGWDKM`)
- NSWO2 threshold in `%PROKON`  $>= 4500$  rpm

Pre-assignment of parameters:

- Threshold for after-dribble /ti reduction enable DRLDYNU = 1.5 %
- Threshold for minimum space after-dribble/ti reduction DTEPRU = 5 ms
- Prediction suppression time in after-start TNSURLP = 5 s
- Configuration CBGRLP = 11 i.e. even in unthrottled operation prediction on, ti after-dribble enabled, ti-reduction off
- Delta prediction angle in standard case DWPR = 0 °KW
- Delta prediction angle in after-dribble enable DWPRNSP = 0 °KW
- Max. prediction angle WPRMX = 1530 °KW
- Factor `pvdK` for psp delimitation FPVMXP = 1.1

Switching off the function:

- Configuration CBGRLP = 2 i.e. prediction off, ti after-dribble enabled

Procedure:

- This function was developed to minimize the application effort; so there is nothing more to do!!
- If lean peaks still occur during acceleration after the above parameter pre-assignment, this can be compensated by increasing the prediction angle using DWPR or DWPRNSP.

Functions affected:

- Transition compensation

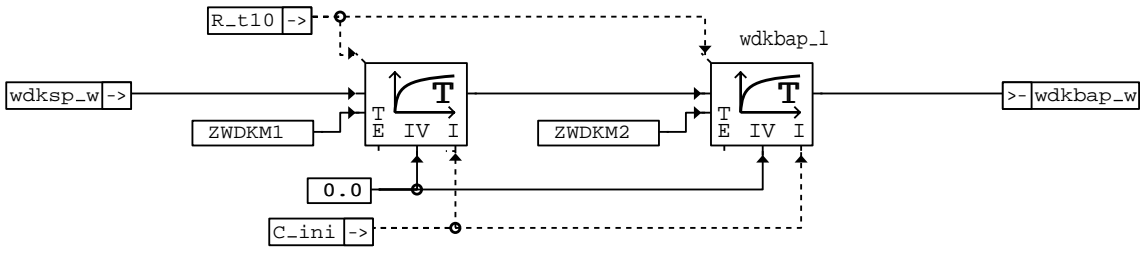
Since the prediction corrects the updating errors of the injection calculation load detection, also controlling the after-dribble-/and ti reduction of the CIFI, the transition compensation application is greatly influenced; the load prediction must therefore be applied before the transition compensation.





## BGWDKM 1.0 Calculation of throttle angle model

### FDEF BGWDKM 1.0 Function definition



bgwdkm-bgwdkm

### ABK BGWDKM 1.0 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ZWDKM1			FW	1. time constant throttle angle model
ZWDKM2			FW	2. time constant throttle angle model
Variable	Source		Type	Description
C_JNI	SWADAP		EIN	ECU-condition for intialisation
R_T10			EIN	Time schedule 10 ms
WDKBAP_L	BGWDKM		LOK	predicted throttle angle wdkbl for ti-calculation (Long)
WDKBAP_W	BGWDKM		AUS	predicted throttle angle wdkbl for ti-calculation (Word)
WDKSP_W	FUEDKSA		EIN	predicted desired throttle angle

### FW BGWDKM 1.0 Fixed Values

Parameter	Value	Description
ZWDKM1		1. time constant throttle angle model
ZWDKM2		2. time constant throttle angle model

### FB BGWDKM 1.0 Detailed description of function

Task of the function:

Calculation of an advancing Dk actual angle wdkbap\_w from the advancing Dk nominal angle wdksp\_w.

Benefits:

By knowing the future Dk actual angle, very rapid changes in the air filling can be calculated despite an unavoidable dead time between load detection and the actual air filling of the cylinders; combustion misfiring is thereby avoided for extreme dynamics (see %BGRLP).

Realization:

The dynamics of the Dk actuator (without overshoot) are simulated by 2 PT1 members connected in series; the model Dk actual angle corresponds to the stationary nominal value for the Dk angle.

## APP BGWDKM 1.0 Application hint

### Prerequisites:

- Dk position regulator applied and stable (i.e. no overshoot in the Dk actual angle !);  
An overshoot of the Dk actual angle cannot be simulated !!

### Application tools:

- VS100

### Pre-assignment of parameters:

- Time constants Dk angle model: ZWDKM1 = 0.01 s, ZWDKM2 = 0.03 s
- Dead time in the Dk nominal value path (see %FUEDK) TVWDKS = 0.02 s

### Shutdown of the function:

- TVWDKS (see %FUEDK) = 0.0 s
- ZWDKM1 = ZWDKM2 = 0.0 s,  
i.e. simulated Dk actual value corresponds to the Dk nominal value

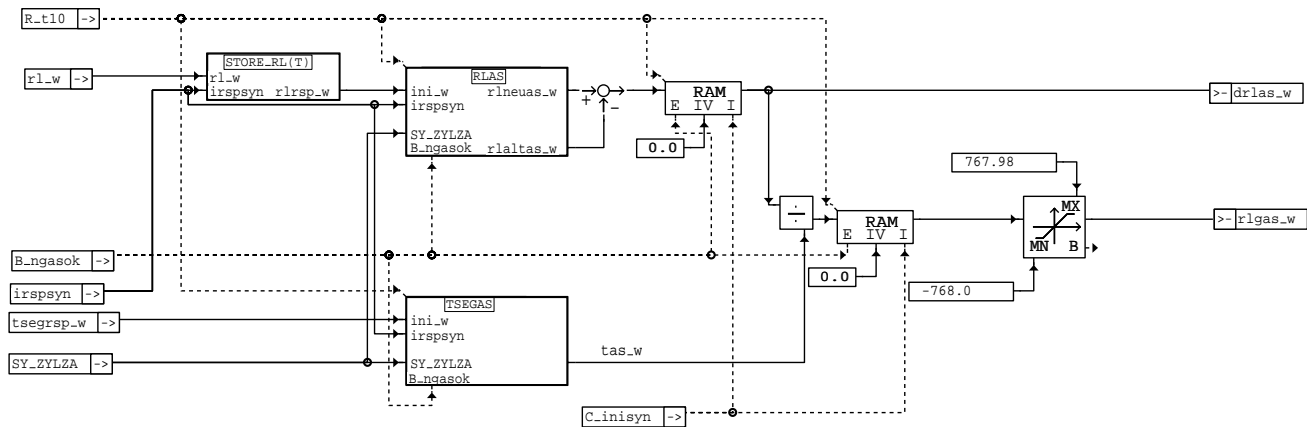
### Method of proceeding:

- Dead time in the Dk nominal value path (see %FUEDK) TVWDKS = 0.0 s
- Perform Dk nominal value jumps  
Possibility a: by applying a voltage to the pedal input  
Possibility b: by switching over in %FUEDK to Dk nominal value requirement using code word CWMDAPP and WDKSAPP; different Dk nominal values can be realized by paging in the VS100 measurements menu
- Comparison of measured Dk actual value wdkba\_w with the estimated Dk actual value wdkbap\_w;  
Optimization in the agreement by adaptation of ZWDKM1 and ZWDKM2
- Reset the dead time in Dk nominal value path back to the original value (see %FUEDK) TVWDKS = 0.02 s).

## BGR LG 1.10 RL-GRADIENT

### FDEF BGR LG 1.10 Function definition

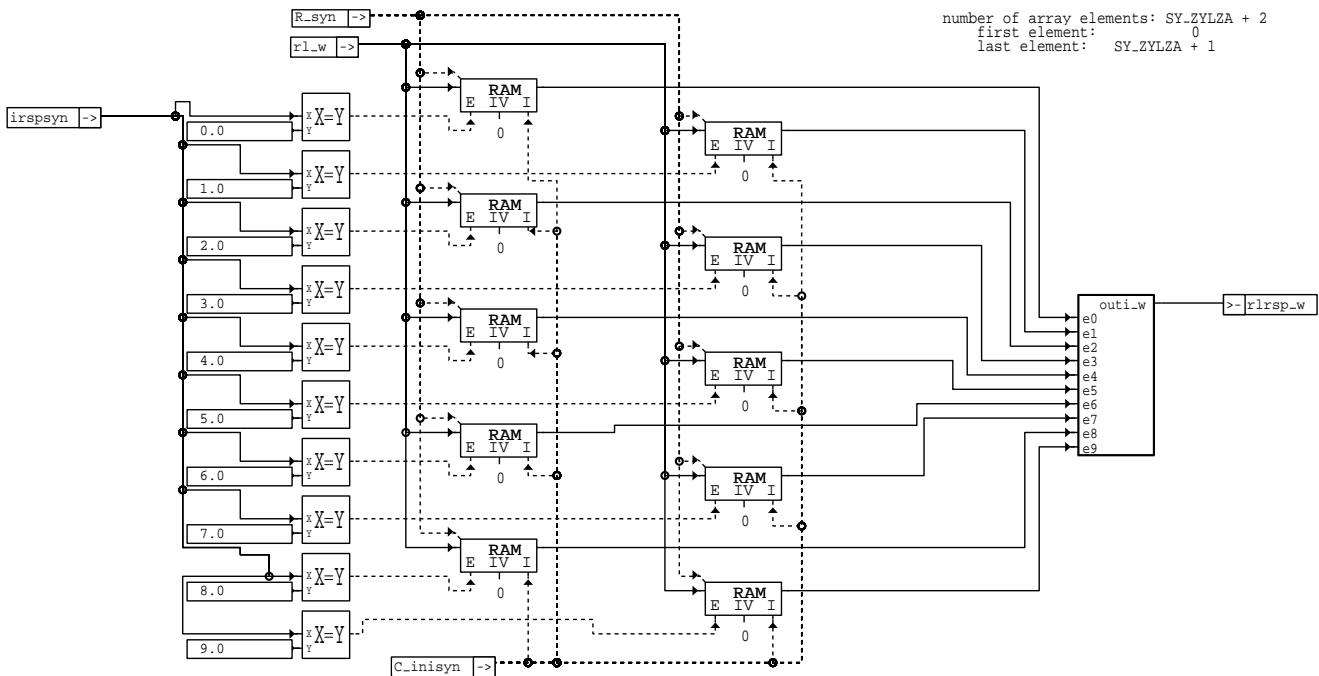
RLGAS: Calculation of the Charge Gradient rlgas\_w over one Working Cycle



bgrlg-bgrlg

bgrlg-bgrlg

STORE\_RL: Storage of the Charge in the Segment Cycle



bgrlg-store-rl

### ABK BGRLG 1.10 Abbreviations

Variable	Source	Type	Description
B_NGASOK	BGNG	EIN	condition memory array for ngas calculation valid
C_INISYN	BGNG	EIN	ECU-condition for intialisation of angle synchronization
DRLAS_W	BGRLG	AUS	change of air charge at one combustion cycle
IRSPSYN	BGNG	EIN	index to address memory of tsegrsp_w, nmotrsp_w, rls_p_w
RLGAS_W	BGRLG	AUS	gradient of air charge at one combustion cycle
RLRSP_W	BGRLG	LOK	Begin of ring buffer , relative charge
RL_W	EGFE	EIN	relative air charge (Word)
R_SYN	GGDPG	EIN	Synchro schedule
R_T10	BGNG	EIN	Time schedule 10 ms
SY_ZYLZA	PROKON	EIN	system constant number of cylinders
TAS_W	BGRLG	LOK	time during one working cycle for rlgas_w
TSEGRSP_W	BGNG	EIN	Begin of ring buffer for segment time

### FW BGRLG 1.10 Fixed Values

Parameter	Value	Description
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### FB BGRLG 1.10 Detailed description of function

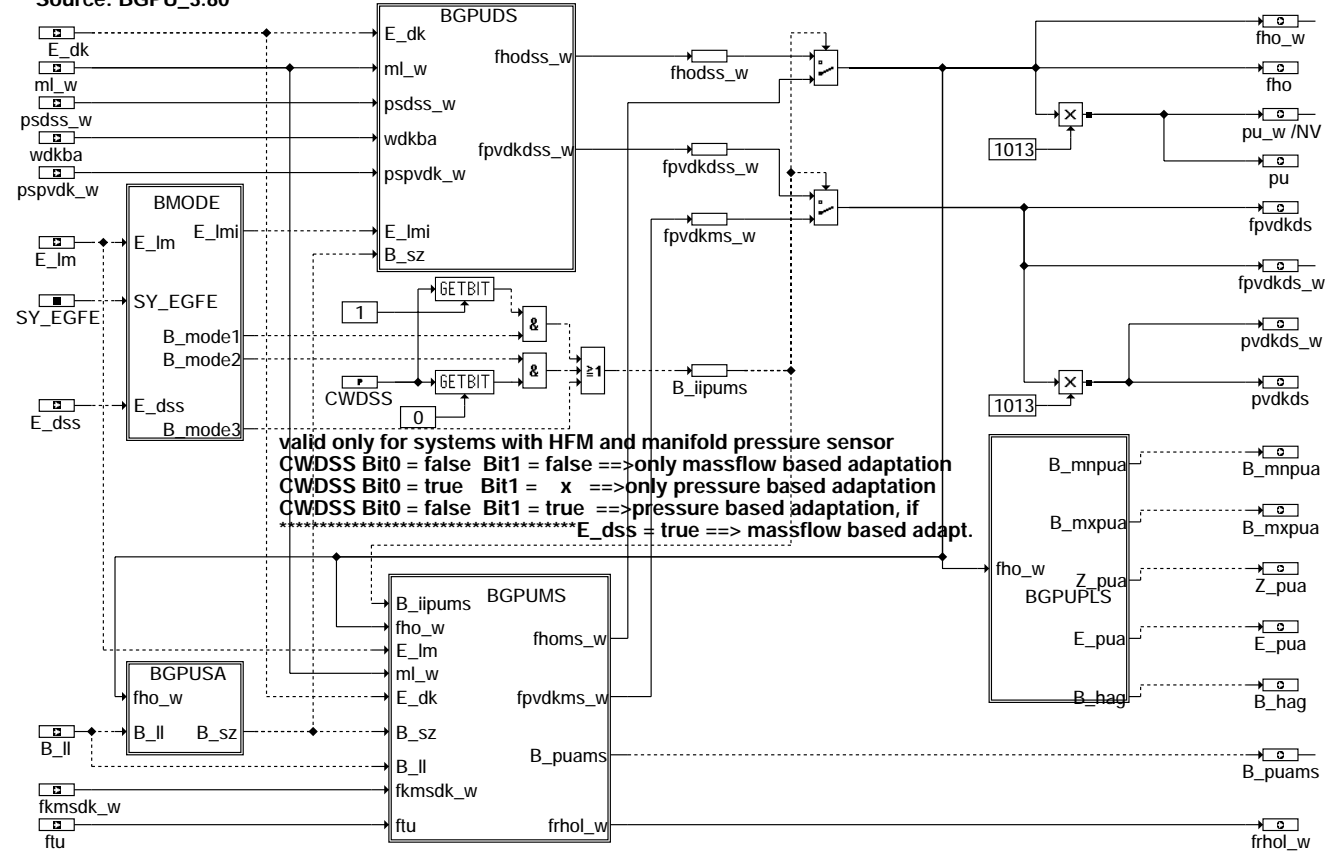
In the function RLGAS a charge gradient over one working cycle is formed for knock and misfire detection. For this, the current value of rl\_w (STORE\_RL) and the segment time tseg\_w (STORE\_TSEG) are entered into a ring buffer store segment-synchronously. The pointer irspsyn points to the position of the last entry in the ring buffer store. The size of the ring buffer store is SY\_ZYLZA + 2 values. The charge difference drlas\_w for one working cycle is calculated in the time cycle. The difference is obtained from the charge at that position in the ring buffer store to which irspsyn points minus the charge prior to SY\_ZYLZA ignitions. The period of time of one working cycle (time for 1 camshaft revolution) tas\_w is calculated by adding the individual segment times starting from irspsyn for SY\_ZYLZA ignitions. By a division of the charge change drlas\_w by the time tas\_w needed for this, the charge gradient over one working cycle is obtained.

## APP BGRLG 1.10 Application hint

## BGPU 3.100 Calculation value ambient pressure

### FDEF BGPU 3.100 Function definition

Source: BGPU\_3.80

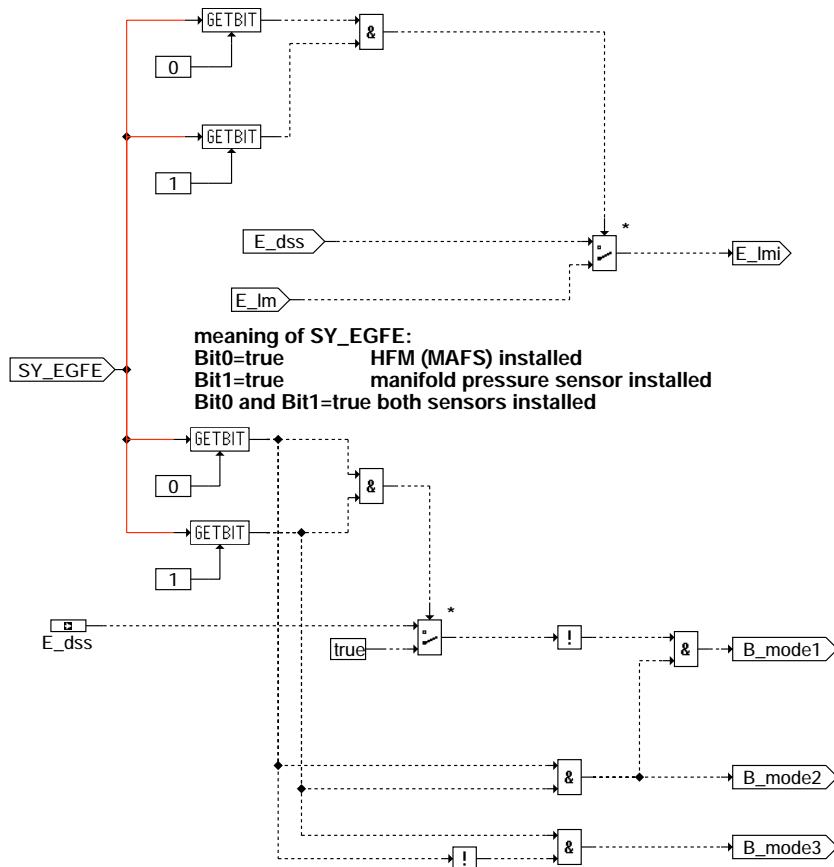


valid only for systems with HFM and manifold pressure sensor  
 CWDSS Bit0 = false Bit1 = false ==> only massflow based adaptation  
 CWDSS Bit0 = true Bit1 = x ==> only pressure based adaptation  
 CWDSS Bit0 = false Bit1 = true ==> pressure based adaptation, if  
 \*\*\*\*\* E\_dss = true ==> massflow based adapt.

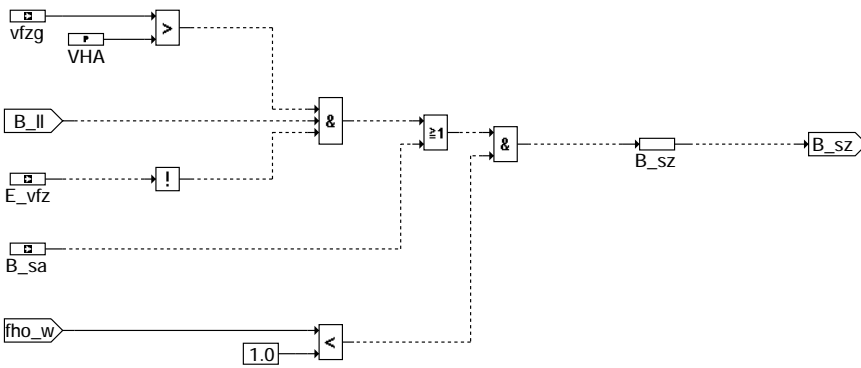
bgpu-bgpu

bgpu-bgpu

please note: these switches (\*) have to be realised by preprocessor



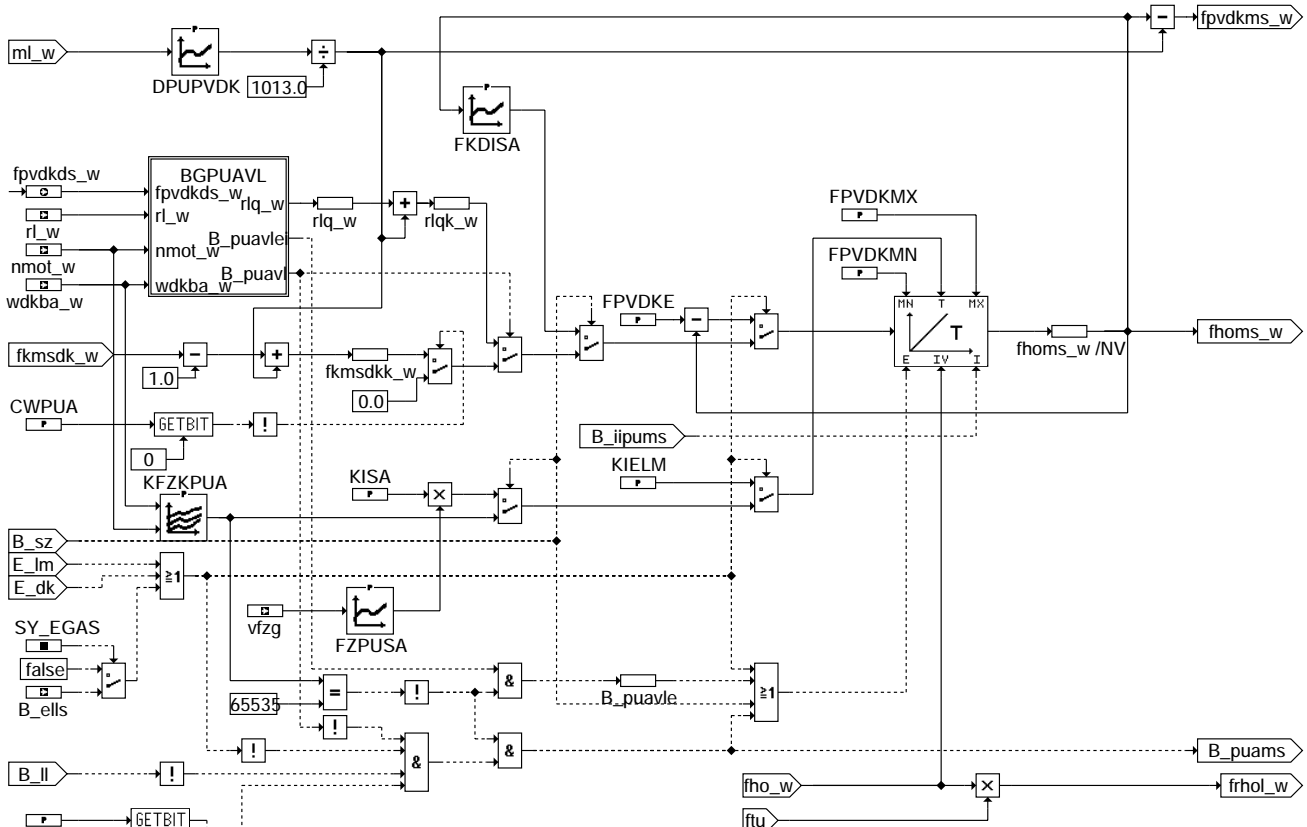
**bgpu-bmode**



**bgpu-bgpusa**

bgpu-bmode

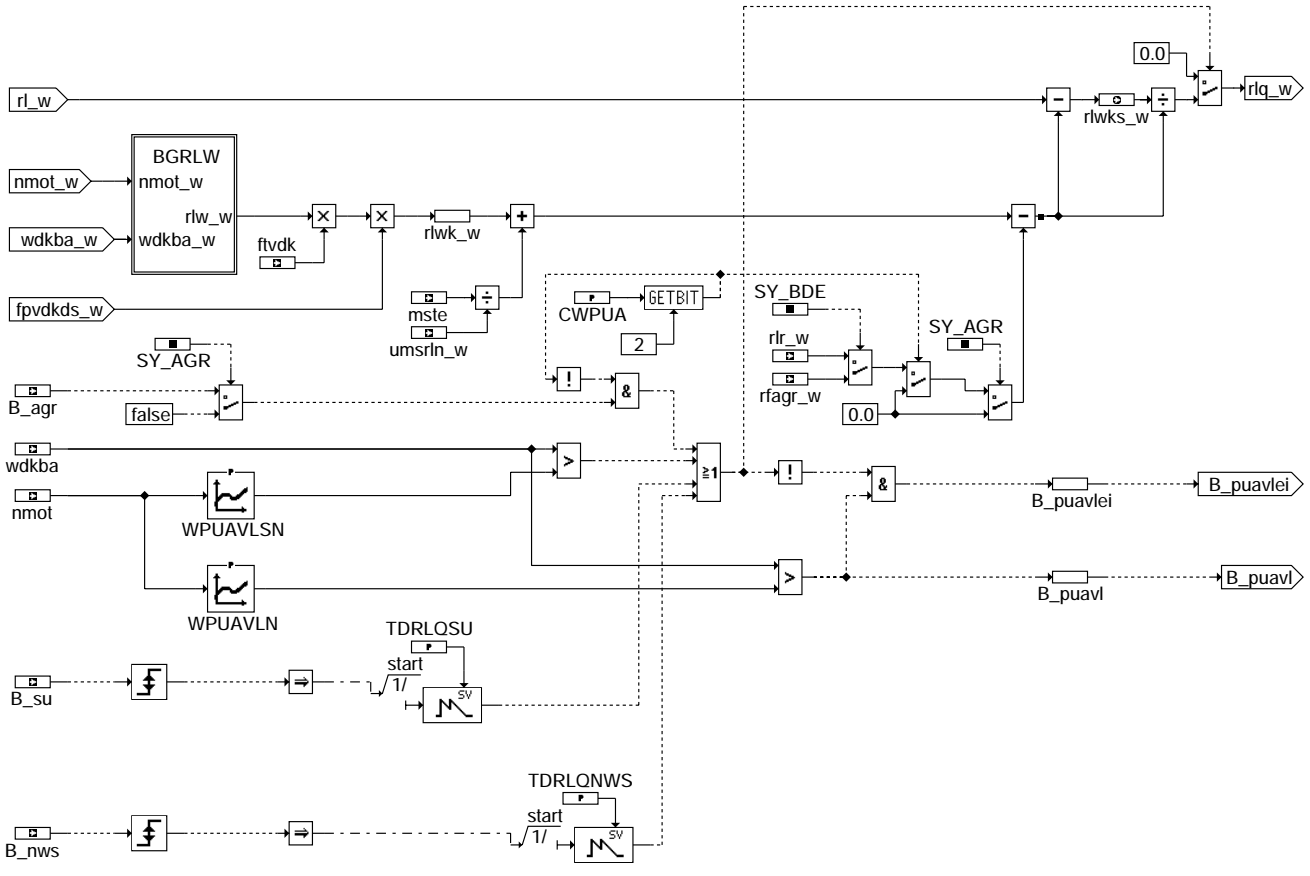
bgpu-bgpusa



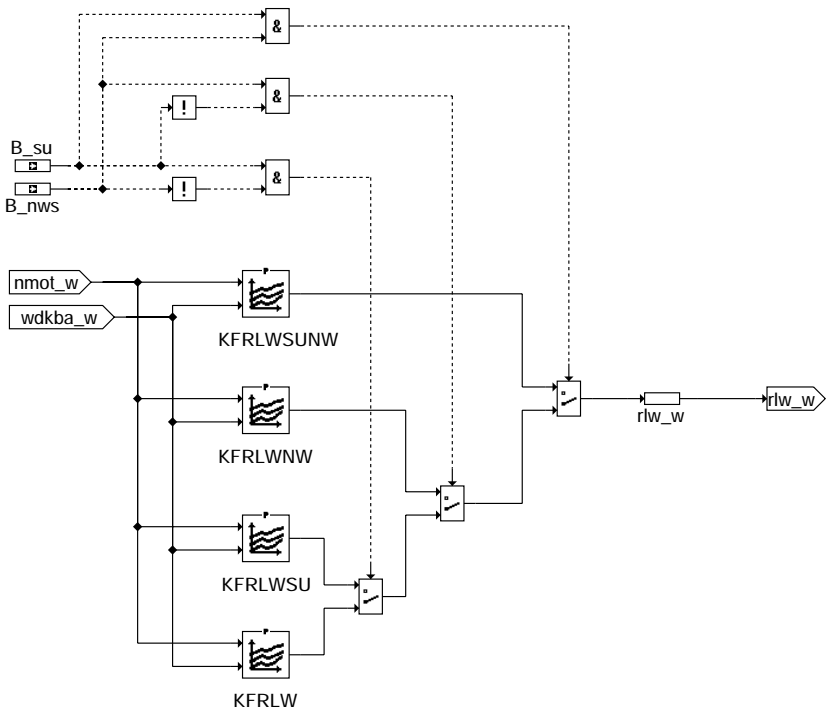
**CWPUA Bit0 = false and Bit1 = false --> massflow adaption until pspvdk=0.95 if WPUAVLN=100%**  
**CWPUA Bit0 = false and Bit1 = false --> massflow- and at wide open throttle rl/rlw-adaption if WDKBA > WPUAVLN**  
**CWPUA Bit0 = true and Bit1 = false --> only rl/rlw adaption if WDKBA > WPUAVLN**  
**CWPUA Bit0 = false and Bit1 = true --> only massflow adaption until WOT if WPUAVLN=100%**

bgpu-bgpums

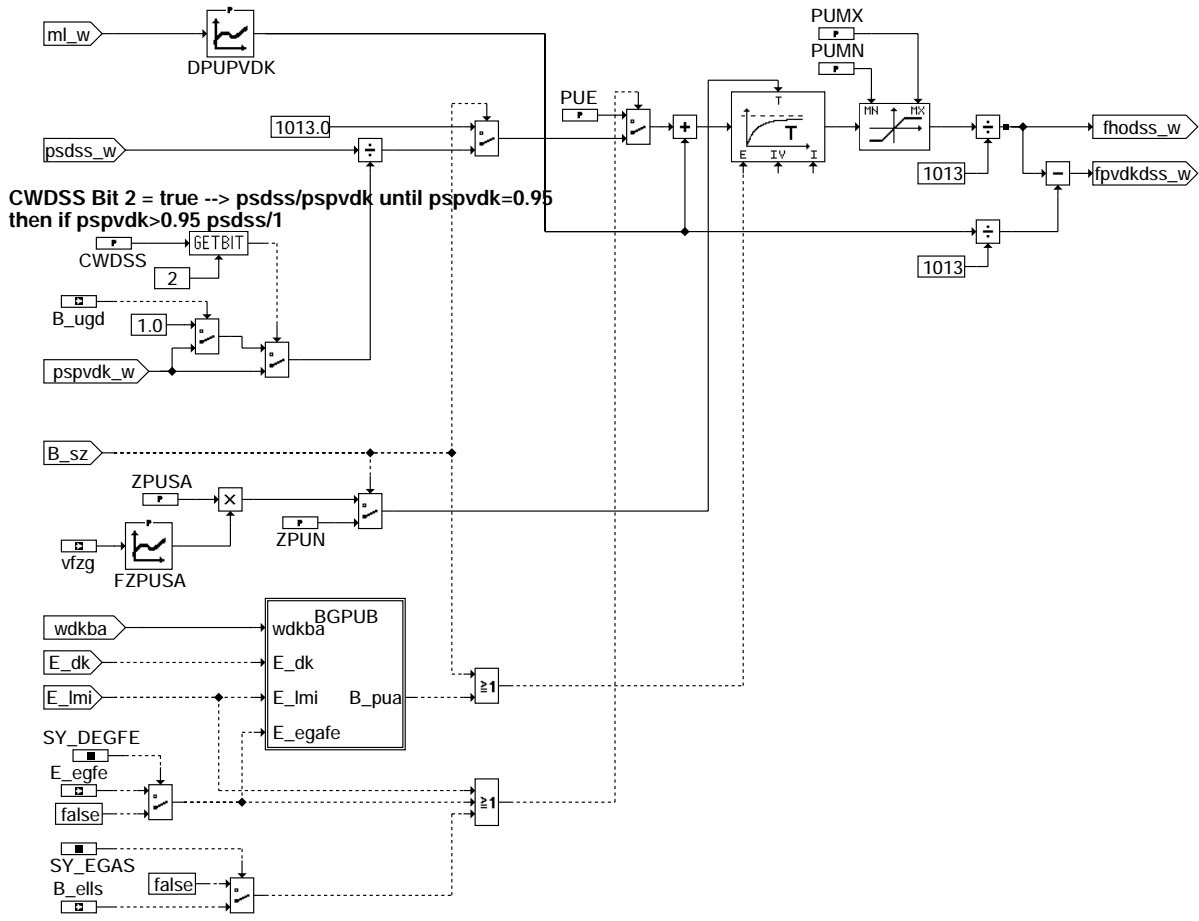
bgpu-bgpums



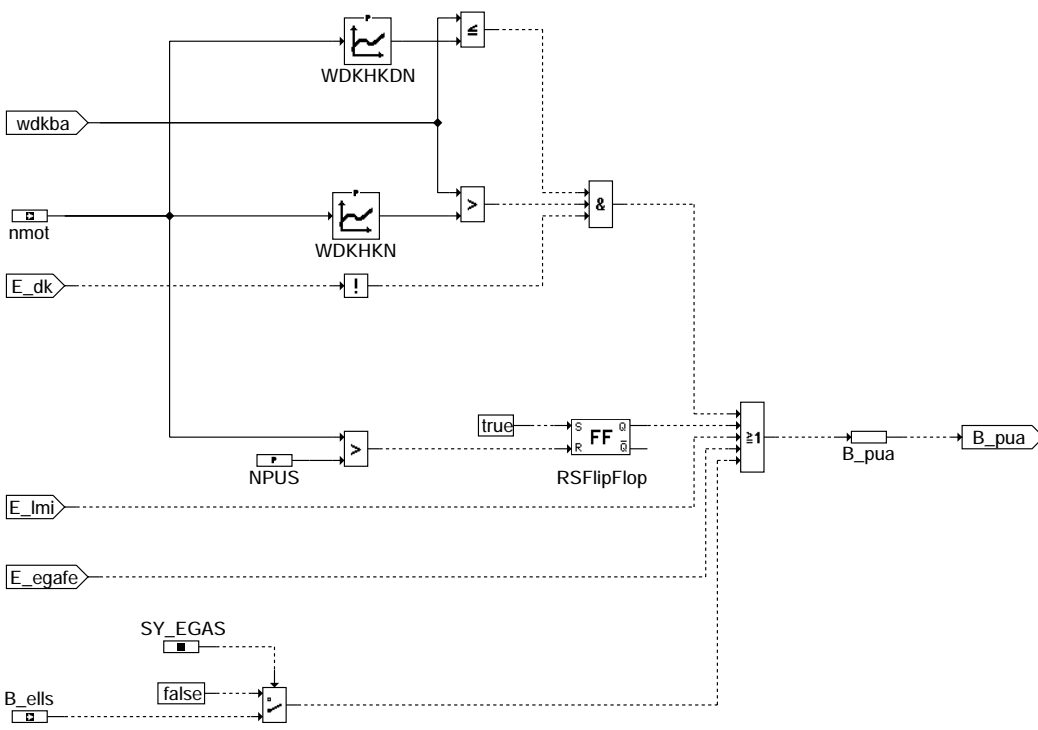
### bgpu-bgpuavi



### bgpu-bgrlw



**bgpu-bgpuds**

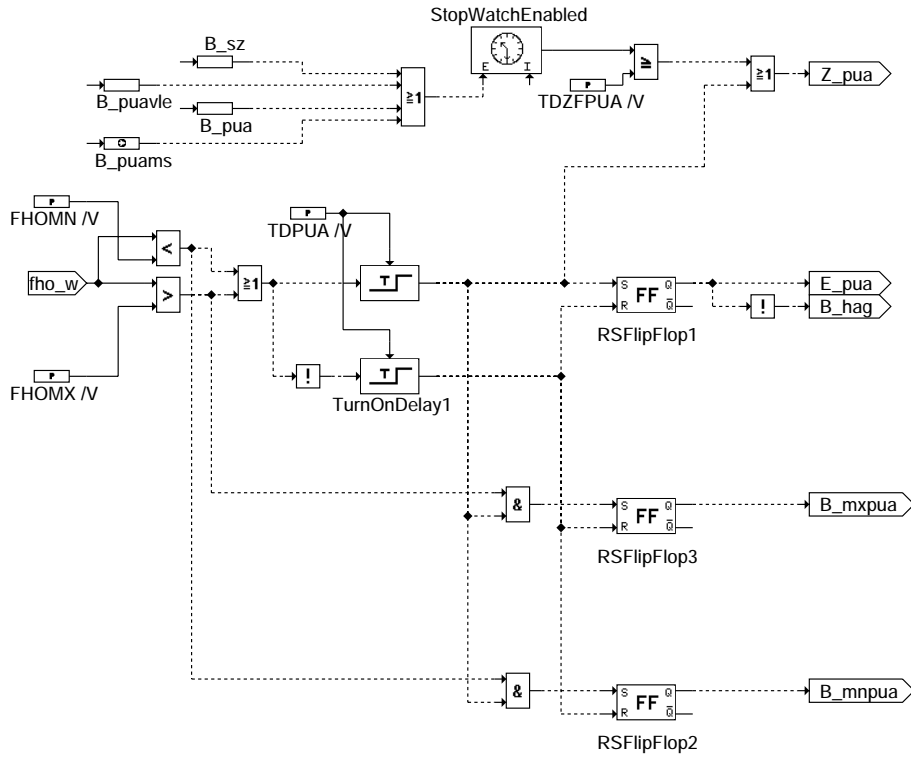


**bgpu-bgpud**

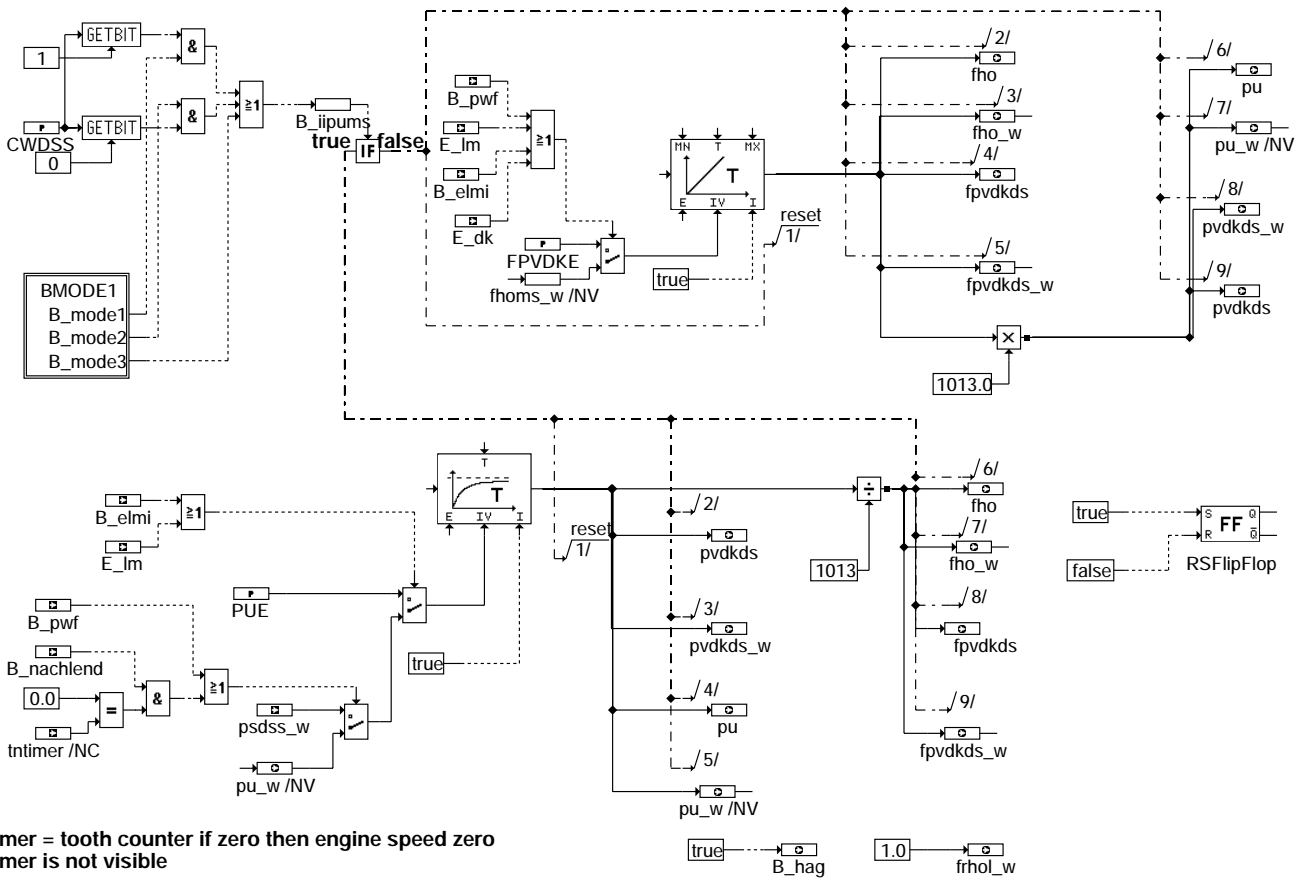
bgpu-bgpuds

bgpu-bgpud





**bgpu-bgpupls**



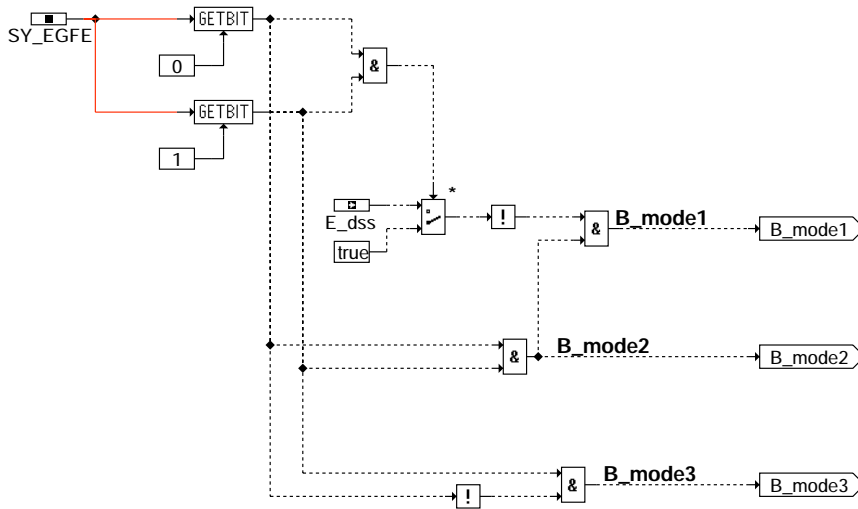
**tntimer = tooth counter if zero then engine speed zero**  
**tntimer is not visible**

**bgpu-init**



please note: these switches (\*) have to be realised by preprocessor

meaning of SY\_EGFE:  
 Bit0=true HFM (MAFS) installed  
 Bit1=true manifold pressure sensor installed  
 Bit0 and Bit1=true both sensors installed



### bgpu-bmode1

"- (\*1) deviant to the circuit this part is realized in the module %DFPM."

"- (\*2) The actions triggered by C-[\*] (marked in the diagram with (\*2)) are processed in the software in separate processes."

#### Fault Memory Management:

```
-----
Status fault path PUA: SFPPUA
Error flag PUA:      E_pua
Cycle flag PUA:     Z_pua
Fault type PUA:     B_mxpua
                   B_mnpua
```

```
Clear fault path:    C_fmclr & B_clpua
Fault path PUA :    CDTPUA
Fault class PUA:    CLAPUA
Fault severity PUA: TSPPUA
Carb code PUA:     CDCPUA
Ambient conditions PUA: FFTDSU
```

```
Ambient: U1PUA nmot_u
          U2PUA rl_u
```

### ABK BGPU 3.100 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWDSS			FW	Code word ambient pressure adaptation via pressure sensor at the intake manifold
CWPUA			FW	Code word ambient pressure adaptation
DPUPVDK	ML_W		KL	pressure difference pu-pvdK
FHOMN			FW	minimum factor for diagnosis of altitude correction
FHOMX			FW	maximum factor for diagnosis of altitude correction
FKDISA	FHOMS_W		KL	faktor difference for integrator ambient pressure during fuel cut off
FPVDKE			FW	default value, pressure upstream of throttle valve
FPVDKMN			FW	lower limit for pressure upstream of throttle valve
FPVDKMX			FW	upper limit for pressure upstream of throttle valve
FZPUSA	VFZG		KL	correction faktor time constant ambient pressure adaptation during fuel cut-off
KFRLW	NMOT_W	WDKBA_W	KF	rlw-map from throttle valve angle
KFRLWNW	NMOT_W	WDKBA_W	KF	rlw-map from throttle valve angle during variable camshaft
KFRLWSU	NMOT_W	WDKBA_W	KF	rlw-map from throttle valve angle during manifold switch over
KFRLWSUNW	NMOT_W	WDKBA_W	KF	rlw-map from throttle valve angle during manifold switch over and active var. ch
KFZKPUA	WDKBA_W	NMOT_W	KF	time constant for ambient pressure
KIELM			FW	Integrator coefficient for ambient pressure counter during E_lm=true
KISA			FW	Integrator coefficient for ambient pressure counter during fuel cut-off
NPUS			FW	Deactivation threshold for ambient pressure adaptation during start
PUE			FW	substitute value for ambient pressure in case of sensor failure
PUMN			FW	Ambient pressure limitation minimum
PUMX			FW	Ambient pressure limitation maximum
SY_AGR			SYS (REF)	System constant AGR present
SY_BDE			SYS (REF)	system constant GDI
SY_DEGFE			SYS (REF)	system constant diagnosis input values load monitoring
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_EGFE			SYS (REF)	system constant input variable for charge detection
TDPUA			FW	debounce time for error entry, ambient pressure adaption
TDRLQNWS			FW	disable time for ambient pressure adaptation after switch camshaft

bgpu-bmode1



Parameter	Source-X	Source-Y	Type	Description
TDRLQSU			FW	disable time for ambient pressure adaptation after switch manifold flap
TDZFPUA			FW	time delay for setting cycle flag for ambient pressure adaptation
VHA			FW	Speed threshold for altitude adaptation
WDKHKDN	NMOT		KL	High threshold throttle plate for altitude adaptation
WDKHKN	NMOT		KL	Low threshold throttle plate for altitude adaptation
WPUAVLN	NMOT		KL	Throttle valve angle as of which VL ambient pressure adaptation is active
WPUAVLSN	NMOT		KL	Throttle valve angle as of which VL ambient pressure adaptation is blocked
ZPUN			FW	Time constant ambient pressure adaptation during normal operating
ZPUSA			FW	Time constant ambient pressure adaptation during fuel cut-off
Variable	Source		Type	Description
B_AGR			EIN	Condition AGR active
B_ELLS			EIN	Condition: error idle speed actuator
B_ELMI	DHFM		EIN	Condition error massflow at initialisation
B_HAG	BGPU		AUS	condition altitude adaptation valid
B_IPUMS	BGPU		LOK	condition initialisation mass flow adaptation
B_LL	MSF		EIN	Condition idle
B_MNPUA	BGPU		AUS	Condition: min-error ambient pressure adaptation
B_MXPUA	BGPU		AUS	Condition: max-error ambient pressure adaptation
B_NACHLEND	MOTAUS		EIN	condition ECU switch off delay regularly finished
B_NWS	NWS		EIN	Condition camshaft control
B_PUA	BGPU		LOK	Condition ambient pressure adaptation active
B_PUAMS	BGPU		AUS	Condition ambient pressure adaptation by comparing mshfm/msdk
B_PUAVL	BGPU		LOK	Condition ambient pressure adaptation at WOT
B_PUAVLE	BGPU		LOK	Condition ambient pressure adaptation at WOT enable
B_PUAVLEI	BGPU		LOK	Condition ambient pressure adaptation at WOT enable internal
B_PWF			EIN	Condition for powerfail
B_SA	MDRED		EIN	Condition fuel cut-off
B_SU	SU		EIN	condition intake manifold switch-over
B_SZ	BGPU		LOK	Condition fuel cut-off counter during altitude correction
B_UGD	BGMSZS		EIN	condition: throttle angle greater or equal wdkugd
E_DK	DDVE		EIN	Error flag: throttle position sensor
E_DSS			EIN	error flag: Manifold absolute pressure
E_EGFE	DEGFE		EIN	Error flag: input parameters for charging detection
E_LM	EGFE		EIN	Error flag: main load sensor
E_PUA	BGPU		AUS	error flag: ambient pressure adaptation
E_VFZ	EGAG		EIN	Error flag: vehicle speed signal
FHO	BGPU		AUS	Correction factor altitude
FHODSS_W	BGPU		LOK	correction factor: altitude manifold pressure based
FHOMS_W	BGPU		LOK	correction factor: altitude mass flow based
FHO_W	BGPU		AUS	correction factor: altitude
FKMSDKK_W	BGPU		LOK	correction factor for mass-flow substitute load signal after calc.from DPUPVDK
FKMSDK_W	BGMSZS		EIN	correction factor for mass-flow substitute load signal
FPVDKDS	BGPU		AUS	Factor pressure in front of throttle valve of pressure sensor
FPVDKDSS_W	BGPU		LOK	Factor pressure in front of throttle valve based of manifold pressure
FPVDKDS_W	BGPU		AUS	Factor pressure in front of throttle valve of pressure sensor (word)
FPVDKMS_W	BGPU		LOK	Factor pressure in front of throttle valve of mass flow based ambient press.adap
FRHOL_W	BGPU		AUS	Factor: air density f(intake air temp., altitude), 16-bit
FTU	BGTEMPK		EIN	factor: ambient temperature
FTVDK	SWADAP		EIN	correction factor for temperature upstream of throttle valve
ML_W	EGFE		EIN	air mass flow filtered (Word)
MSTE	BGTEV		EIN	mass flow purge control into the manifold
NMOT	SWADAP		EIN	engine speed
NMOT_W	SWADAP		EIN	engine speed
PSDSS_W			EIN	Intake manifold pressure measured with pressure sensor at manifold (DS-S)
PSPVDK_W	EGFE		EIN	quotient: int.manif.pressure divided by pressure upstream of throttle valve
PU	BGPU		AUS	Ambient pressure
PU_W	BGPU		AUS	Ambient pressure
PVDKDS	BGPU		AUS	Pressure in front of throttle valve of pressure sensor
PVDKDS_W	BGPU		AUS	Pressure in front of throttle valve of pressure sensor (word)
RFAGR_W	BGSRM		EIN	relative load by external exhaust gas reduction
RLQK_W	BGPU		LOK	Quotient rlw/rl density-corrected behind summation of DPUPVDK
RLQ_W	BGPU		LOK	Quotient rlw/rl density-corrected
RLR_W			EIN	relative air-load over int. and ext. EGR
RLWKS_W	BGPU		AUS	sum corrected rel. air charge from auxiliary load signal (Word)
RLWK_W	BGPU		LOK	corrected rel. air charge from auxiliary load signal (Word)
RLW_W	BGPU		LOK	relative air charge from auxiliary load signal (Word)
RL_W	EGFE		EIN	relative air charge (Word)
TNTIMER			EIN	tooth counter not recordable with VS100
UMSRLN_W	BGMSZS		EIN	calculation factor load to mass flow
VFZG	SWADAP		EIN	vehicle speed (km/h)
WDKBA	GGDVE		EIN	throttle angle
WDKBA_W	GGDVE		EIN	throttle angle with respect to lower mechanical stop
Z_PUA	BGPU		AUS	cycle flag: ambient pressure adaptation



## FW BGPU 3.100 Fixed Values

Parameter	Value	Description
CWDSS		Code word ambient pressure adaptation via pressure sensor at the intake manifold
CWPUA		Code word ambient pressure adaptation
FHOMN		minimum factor for diagnosis of altitude correction
FHOMX		maximum factor for diagnosis of altitude correction
FPVDKE		default value, pressure upstream of throttle valve
FPVDKMN		lower limit for pressure upstream of throttle valve
FPVDKMX		upper limit for pressure upstream of throttle valve
KIELM		Integrator coefficient for ambient pressure counter during E <sub>lm</sub> =true
KISA		Integrator coefficient for ambient pressure counter during fuel cut-off
NPUS		Deactivation threshold for ambient pressure adaptation during start
PUE		substitute value for ambient pressure in case of sensor failure
PUMN		Ambient pressure limitation minimum
PUMX		Ambient pressure limitation maximum
TDPUA		debounce time for error entry, ambient pressure adaptation
TDRLQNW		disable time for ambient pressure adaptation after switch camshaft
TDRLQSU		disable time for ambient pressure adaptation after switch manifold flap
TDZFPUA		time delay for setting cycle flag for ambient pressure adaptation
VHA		Speed threshold for altitude adaptation
ZPUN		Time constant ambient pressure adaptation during normal operating
ZPUSA		Time constant ambient pressure adaptation during fuel cut-off

## FB BGPU 3.100 Detailed description of function

An ambient pressure adaptation is realized by means of this function. In the process a switch to two physically different adaptation methods is performed via the system constant SY\_EGFE Bit0 and Bit1.

If SY\_EGFE Bit0 = false and Bit1 = true (SY\_EGFE Bit0=B<sub>hfm</sub> and Bit1=B<sub>dssv</sub>) the ambient pressure is determined from a pressure sensor mounted in the intake manifold. This kind of ambient pressure adaptation is used for a pressure-sensor-based charge sensing (p-system).

If SY\_EGFE Bit0 = true and Bit1 = false the ambient pressure is learned from the output value of the "fast integrator" (fkmsdk). This means that the difference between the two charge signals mshfm and msdk<sub>w</sub>, which is outputted as factor in the output value of fkmsdk serves for the ambient pressure adaptation. This method is used for the ambient pressure adaptation on aspirating engines with HFM but without ambient pressure sensor.

If SY\_EGFE Bit0 = true and Bit1 = true, the ambient pressure adaptation can either be pressure-sensor-based or mass-flow-based. Here the pressure-sensor-based adaptation should be given preference.

By the code word CWDSS the following selection can be made in the process:

CWDSS	Bit0	Bit1	
	false	false	---> only mass-flow ambient-pressure-based pu-adaptation
	true	x	---> only pressure-based pu-adaptation
	false	true	---> pressure-based pu-adaptation when E <sub>dss</sub> =true switch-over to mass-flow-based pu-adaptation

Bit2 CWDSS is only relevant at pressure-sensor-based ambient pressure adaptation.  
Bit2 initial data entered --> false Only in special cases may Bit2=true (fast integrator at pspvdk > 0.95 stop and active Pu-adaptation in this range)  
If Bit2=true theoretical fault worst-case 50 hPa = 500 m

When SY\_EGFE Bit0 = true and Bit1 = false (EGFE=01) the following applies:

An altitude factor resp. the pressure upstream throttle valve, which added to the pressure drop at the air filter DPUPVDK corresponds to the ambient pressure can be learned by comparing the secondary charge signal (msdk) with the main charge signal (mshfm). The comparison of the two charge signals is, however, not performed in this module but in the function %BGMSZS.

The secondary charge path is adjusted to the main charge path by the correction factor fkmsdk via the so-called "fast integrator". This is realized by a feedback of the integrator output to the secondary charge signal. In the temporal mean and with correct application of the secondary charge signal the correction factor fkmsdk will be equal to 1.

Description of the physical effect of the ambient pressure adaptation on mass flow comparison:

When driving at high altitude the secondary charge signal remains constant, the main charge signal becomes smaller and smaller due to decreasing air density with increasing altitude. The "fast integrator" controls this deviation of the two charge signals down to zero in the function BGMSZS. At e.g. 2000 m above sea level the mean correction factor fkmsdk would be at 0.8. The correction factor fkmsdk is now transferred to the function BGPU for the formation of the ambient pressure. There, the input of the ambient pressure integrator is set to the value fkmsdk minus 1. The ambient pressure integrator runs at about 1/10th of the adaptation speed of the "fast integrator". A deviation of the two mass flows, which lasts for longer, is thereby interpreted as ambient pressure change. The output of the integrator keeps on changing until the two mass flows (mshfm/msdk) have matched via the output values fpvdks and pvdkds in the function BGMSZS. The "fast integrator" in BGMSZS then has the value 1 in the temporal mean as output value fkmsdk. The factor pressure upstream throttle valve and the factor altitude are available at the output of the ambient pressure adaptation. The pressure upstream throttle valve, which corresponds to the ambient pressure, is calculated by a multiplication by the standard pressure (1013hPa). The factors FPVDKMX and FPVDKMN represent a limitation of the upper and of the lower adaptation range. The output value of the integrator after power fail or in case of a fault of one of the two charge signals can be defined by the factor FPVDKE.

The ambient pressure adaptation speed is adjusted dependent on engine speed and throttle angle via the map KFZKPUA.

With code word CWPUA=0 at first a switch to the already described mass-flow-based ambient pressure adaptation is performed. If then the condition wdkba > WPUAVLN = true (e.g. at pspvdk >= 0.9) the rl/rlw-based ambient pressure adaptation is switched to.

With code word CWPUA=1 and WPUAVLN = 100 % always (in the entire operating range) the rl/rlw-based ambient pressure adaptation is active. On engines with manifold switchover resp. camshaft adjustment depending on the operating state different rlw maps exist, which take the influencing of the charge into consideration via intake-manifold flap resp. camshaft adjustment. The following a/n maps are active:

no manifold switchover and camshaft adjustment active	KFRLW
manifold switchover active	KFRLWSU
camshaft adjustment active	KFRLWNW
manifold switchover and camshaft adjustment active	KFRLWSUNW



It is recommendable to activate the rl/rlw adaptation at a pressure ratio of approx. 0,9 at the latest, however, at pspvdk 0,95. Attention needs to be paid here, that the two adaptation methods are enabled in the desired adaptation range via the map KFZKPUA. Generally it always applies to rl/rlw adaptation that it can be blocked in pulsation ranges via the characteristic WPUAVLNS. Furthermore attention needs to be paid that the desired adaptation range is enabled via KFZKPUA. This applies to the rl/rlw pu-adaptation as well as to the mass-flow-based ambient pressure adaptation. With CWPUA Bit1=true and active fast integrator CWFKMSDKA=1 (%BGMSZS fast integrator also active in VL) the mass-flow-based ambient pressure adaptation can also be used in the vicinity of full load. Here it must be ensured that in the pulsation range at VL no too large ambient pressure deviations occur (altitude test). On ME7 systems this kind of ambient pressure adaptation is not recommendable, since sudden deviations from main to secondary charge signal can lead to unsteadiness of the throttle valve movement in the vicinity of full load.

When SY.EGFE Bit0 = false and Bit1 = true (EGFE=2) the following applies:

The factor ambient pressure adaptation (fpvdkds resp. fho) serves to adjust functions to the altitude (e.g. start control, correction of load signal). The ambient pressure factor is determined via a measurement of the manifold pressure in operating and map ranges, in which the manifold pressure approximately corresponds to the ambient pressure. The first manifold pressure measurement is performed during start, if C\_ini is fulfilled and if the engine speed is still below a threshold value (NPUS). The second adaptation range lies from characteristic WDKHKN until WDKHKDN is reached when the throttle angles are exceeded. Above WDKHKN the measured manifold pressure corresponds to the ambient pressure. This fact is made use of when learning the ambient pressure. By the division of manifold pressure/pressure upstream throttle valve the ambient pressure is determined also from the manifold pressure of a throttled engine (manifold pressure is < than ambient pressure). Up to which manifold pressure this method calculates a sufficiently exact ambient pressure, needs to be determined with each project. If the determined ambient pressure e.g. >= +/- 70 hpa deviates from the actual value, the ambient pressure adaptation needs to be blocked for even smaller throttle angles at this engine speed (with WDKHKN). On engines with little pulsation the fast integrator can also be enabled if pspvdk >= 0,95. The characteristic WDKHKDN must then be set to 100%; bit 2 of CWDSS must then be false (psdss is always divided by pspvdk). On engines, which have critical pulsation it is possible to block the adaptation when pspvdk=0.95 is reached by means of the characteristic WDKHKDN. Disadvantage of this being that no adaptation will be performed during a long uphill drive at full load. By CWDSS Bit2=true a switchover to psdss/1 is performed when pspvdk=0.95 is reached. Attention needs to be paid here that the characteristic WDKHKDN does not prohibit the adaptation; set value everywhere to 100%. Adaptation at full load is also performed with this configuration. The theoretical worst-case deviation shortly after pspvdk >0.95 has been reached here is 50 hPa = 500m, with increasing pspvdk this fault becomes smaller until it equals zero when pspvdk=1 is reached.

The time constant of the low pass varies as follows:

The initialization value is ZPUSA.

The low pass for the filtering of the manifold pressure signal psdss/pspvdk is filtered with the time constant ZPUN during normal operating.

With detected altitude (fho<1) the adaptation factor increases with the time constant ZPUSA during fuel cut-off or during idling at correspondingly valid vehicle speed (B\_ssz). Thus it is achieved that during long downhill driving and with closed throttle valve (during which no adaptation is possible) the altitude factor is corrected in the direction of a lesser altitude. With B\_ssz=true the low pass filter travels from the current value to the standard value 1013 hPa with the time constant ZPUSA. This means, that e.g. at 3000 m above sea level a quicker control down to low altitude is performed if the condition B\_ssz=true than at 500 m above sea level. By this behavior, large slope gradients at high altitude and small slope gradients at low altitude, a usual mountain profile is taken into account.

A plausibility check on the fho signal is performed in the subfunction BGPUPLS independent of which ambient pressure adaptation method is active. If the altitude factor fho is less than the fixed value FHOMN or greater than the fixed value PHOMX, the error bit E\_pua is set to true after the delay time TDPUA. Inverse to E\_pua the flag altitude adaptation valid B\_hag is set to false. This information is inquired upon in the EGR valve and secondary air valve diagnosis.

The pressure drop at the air filter element is taken into consideration via the characteristic DPUPVDK dependent on the air mass flow ml for both methods of the ambient pressure adaptation (pressure sensor and mass flow based). The values for the pressure drop at the air filter element differ for each project and must be determined at various air flow rates. Attention must be paid here that an air filter and an air filter container intended for the series production are used.

## APP BGPU 3.100 Application hint

The pressure-sensor-based ambient pressure adaptation is realized by an evaluation of the manifold pressure. The mass flow through the throttle valve is corrected by the generated output signals.

The measured manifold pressure approximately corresponds to the ambient pressure in the range close to full load at wide-open throttle valve and during start at low engine speeds. By a division of the manifold pressure by the pressure ratio pspvdk it is possible to determine the pressure upstream throttle valve and thus the ambient pressure.

Definition of the adaptation range:

- Define adaptation range (when entering 65535 the adaptation is disabled) KFZKPUA such that the difference between adapted and real ambient pressure is never more than 10%.  
The ambient pressure adaptation may not be active during idle resp. in a range close to idle psvdk < 0,5 or if WDKBA < 10%.
- Record manifold pressure during start and define engine speed threshold NPUS such that the manifold pressure corresponds to the ambient pressure up to this engine speed.

Adjustment of the time constants:

- Choose time constant ZPUN that slow that small deviations of the pressure, which constantly occur while driving are only slightly corrected  
-> Limit: Altitude factor fho must still be reliably corrected during fast driving at altitude drag fault < 30 hPa  
-> Guidance value: Learning of a delta pu = 30 hPa within approx. 15 sec

Adjustment of the fuel cut-off counter:



- Set ZPUSA and KISA for slow downhill driving  
-> Guidance value: Setting to an altitude difference per time of 1 m/sec

Guidance values for the initial application at pressure-sensor-based ambient pressure adaptation partial function BGPUDS:

PUMX : 1250 hPa  
PUMN : 350 hPa  
PUE : 1000 hPa  
NPUS : 400 rpm  
ZPUSA : approx. 2000 sec  
ZPUN : approx. 160 sec

WDKHKN : At different engine speeds enter values such that faults psdss/pu are 10% at the maximum.  
Guidance values for initial data: Determine throttle angle at corresponding engine speed base points in WDKHKN, at which the pressure ratio ps/pu <= 0.525 (over critical).

if CWDSS Bit 2 = false the fast integrator must have been enabled in the VL-range CWFKMSDKA=1 (%BGMSSZS)

WDKHKDN : Enter 100% into entire characteristic. If an unlearning can be detected in one ambient pressure adaptation range, this range can be blocked by according data being entered into WDKHKDN (wdkbl < WDKHKDN pu-adaptation blocked)

if CWDSS Bit 2 = true then

WDKHKDN : Enter 100% into entire characteristic. Then adaptation is enabled also when pspvdk => 0.95  
When pspvdk => 0.95 is exceeded a switchover from psdss/pspvdk to psdss/1 is performed via B\_ugd.  
If an unlearning can be detected in one ambient pressure adaptation range, this range can be blocked by according data being entered into WDKHKDN (wdkbl < WDKHKDN pu-adaptation blocked)

Guidance values for initial application of mass-flow and rl/rlw ambient pressure adaptation partial function BGPUMS and BGRWL:

FPVDKMX : 1.25  
FPVDKMN : 0.35

FKDISA : fhoms\_w -> 0.0 0.499 0.5 0.6 0.7 0.8 0.95 1.00  
0.1 0.1 0.1 0.1 0.1 0.1 0.1 0  
(FKDISA=0.001 integrator slow, FKDISA=2 integrator fast)

KISA : 1500 s (KISA=1 integrator fast, KISA=65535 integrator slow)  
KIELM : 150 s (KIELM=1 integrator fast, KIELM=65535 integrator slow)  
FPVDKE : 1.0

KFZKPUA	wdkba_w -->	0	5	10	15	20	30	35	40	60	70	80	100
	nmot_w												
	v												
	6000	65535	65535	65535	65535	65535	66	66	66	66	66	66	66
	5000	65535	65535	65535	65535	65535	66	66	66	66	66	66	66
	4000	65535	65535	65535	65535	65535	66	66	66	66	66	66	66
	3000	65535	65535	65535	65535	65535	66	66	66	66	66	66	66
	2000	65535	65535	65535	65535	65535	66	66	66	66	66	66	66
	1500	65535	65535	65535	66	66	66	66	66	66	66	66	66
	1000	65535	65535	65535	66	66	66	66	66	66	66	66	66
	800	65535	65535	65535	65535	65535	65535	65535	65535	65535	65535	65535	65535

(KFZKPUA=65535 integrator stop, KFZKPUA=1 integrator fast)

Enter 66 everywhere in KFZKPU with rl/rlw-based ambient pressure adaptation. With this type of adaptation the adaptation is enabled via the characteristic WPUAVLN. The adaptation is blocked via the characteristic WPUAVLSN.

- KFRLW : With charge-correct application of the main signal path transfer the according rl-value to each base point of KFRLW when B\_su and B\_NWS = false. (Set ambient pressure to day pressure, temperature model must have been adjusted).  
Adjust DPUPVDK, then with currently set pu and charge-correctly adjusted secondary charge signal  
rlqk\_w must be 0 for each base point
- KFRLWSU : With charge-correct application of the main signal path transfer the according rl-value to each base point of KFRLWSU when B\_su = true and B\_NWS = false. (Set ambient pressure to day pressure, temperature model must have been adjusted).  
Adjust DPUPVDK, then with currently set pu and charge-correctly adjusted secondary charge signal  
rlqk\_w must be 0 for each base point
- KFRLWNW : With charge-correct application of the main signal path transfer the according rl-value to each base point of KFRLWNW when B\_su = false and B\_NWS = true. (Set ambient pressure to day pressure, temperature model must have been adjusted).  
Adjust DPUPVDK, then with currently set pu and charge-correctly adjusted secondary charge signal  
rlqk\_w must be 0 for each base point
- KFRLWSUNW : With charge-correct application of the main signal path transfer the according rl-value to each base point of KFRLWSUNW when B\_su and B\_NWS = true. (Set ambient pressure to day pressure, temperature model must have been adjusted).  
Adjust DPUPVDK, then with currently set pu and charge-correctly adjusted secondary charge signal  
rlqk\_w must be 0 for each base point

Example for WPUAVLN only mass-flow-based adaptation

WPUAVLN : nmot -> 800 1000 1500 2000 2500 3000 3500 4000 4500 5000 5550 6000

fill all base points with 100 then rl/rlw adaptation never becomes active

(Since the start of the ambient pressure adaptation takes place at wdkba > characteristic value of WPUAVLN



!! enter data into KFZKPUA such that mass flow based adaptation starts as from desired throttle angle)  
CWPUA = 0

Example for WPUAVLN mass-flow-based and rl/rlw adaptation

WPUAVLN : nmot -> 800 1000 1500 2000 2500 3000 3500 4000 4500 5000 5550 6000  
Enter throttle angle at pspvdk 0,90 for each engine speed base point

(In the chosen example start of the ambient pressure adaptation at wdkba > characteristic value of WPUAVLN

!! enter data into KFZKPUA such that integrator is enabled as from mass-flow-based adaptation up to and including  
rl/rlw adaptation (pspvdk<0,9).  
CWPUA = 0

Example for WPUAVLN only rl/rlw adaptation

WPUAVLN : nmot -> 800 1000 1500 2000 2500 3000 3500 4000 4500 5000 5550 6000  
12 15 18 20 22 24 28 30 35 35 35 35

(In the chosen example start of the ambient pressure adaptation at wdkba > characteristic value of WPUAVLN

!! Important: Ambient pressure adaptation will only adapt if time constant is not equal to 65535 in KFZKPUA)  
CWPUA = 1

Example for WPUAVLSN pu-adaptation rl/rlw based from 1500- 2000 rpm at > 60 %DK blocked

WPUAVLSN : nmot -> 800 1000 1500 2000 2500 3000 3500 4000 4500 5000 5550 6000  
100 100 60 60 60 100 100 100 100 100 100 100

(In the chosen example stop of the ambient pressure adaptation at wdkba > 60 deg. from nmot 1500 rpm to 2500 rpm  
The rl/rlw adaptation is enabled without limits if it says 100 in the entire characteristic line)

TDRLQSU : approx. 2 sec  
TDRLQNSW: approx. 2 sec

Guidance values for the initial application independent of the type of ambient pressure adaptation:

FHOMX : 1.2  
FHOMN : 0.4

TDZFPUA : Adjust time 150 sec such that incorrect ambient pressure adaptation will stabilize during the emission test.  
(On engines with large displacement do not choose TDZFPUA too large, since cycle flag is then not set during  
the emission test [Reason being that vehicle is operated at such small throttle angles that the ambient pressure  
adaptation is only enabled for e.g. 50 seconds during the entire test] set TDZFPUA = 40 seconds in given example)

DPUPVDK : Pressure drop at air filter element with varying air mass flows (ml) set up between idle value and ml  
value at maximum engine speed (extremely project-dependent)  
(if value is unknown enter 0 into DPUPVDK, then the pressure upstream throttle valve is the same as ambient pressure)

FZPUSA: Base points vfzg 20 40 50 60 70 80 90 100  
Values .... 1.0....

the speed-dependent intervention at fuel cut-off is  
switched off by this.

TDPUA : 200 ms  
VHA : 15 km/h

## BGRML 1.20 Calculation Value of Relative Air Mass according to SAE J1979 Mode \$01 + \$02 PID

### DFEF BGRML 1.20 Function definition

SY\_TURBO = 0:

```

ml_w ----->| : +-----> rml (Q: 1 Byte, 0 ... FF hex)
                +-----
                ^
fpvdk_w ----->| * +-----
                +-----
                ^
MLMAX -----+
    
```

SY\_TURBO = 1:

```

ml_w ----->| : +-----> rml (Q: 1 Byte, 0 ... FF hex)
                +-----
                ^
MLMAX -----+
    
```

### ABK BGRML 1.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
MLMAX			FW	maximum air-quantity for load calculation SAE J1979
SY_TURBO			SYS	system constant for exhaust-gas turbocharger



Variable	Source	Type	Description
FPVDK_W	EGFE	EIN	correction factor for pressure upstream of throttle valve, 16-bit
ML_W	EGFE	EIN	air mass flow filtered (Word)
RML	BGRML	AUS	relative air mass (calc. load value) acc. to SAE J1979

### FW BGRML 1.20 Fixed Values

Parameter	Value	Description
MLMAX		maximum air-quantity for load calculation SAE J1979

### FB BGRML 1.20 Detailed description of function

Areas of utilization such as e.g. the SCAN TOOL transfer according to SAE J1979 necessitate the variable "relative air mass" (rml), also referred to as "Calculated Load Value" (CLV) in the SAE J1979. In accordance to SAE J1979 the formula is:

$$CLV = \frac{\text{Current airflow}}{\text{Peak airflow (@sea level)}} * \frac{\text{Atmospheric pressure (@sea level)}}{\text{Barometric pressure}} * 100 \%$$

Derived from this the following results

a) for an aspirating engine (SY\_TURBO = 0):

$$rml = \frac{ml\_w}{MLMAX * fpvdk\_w} * 100\%$$

b) for a turbo engine (SY\_TURBO = 1):

$$rml = \frac{ml\_w}{MLMAX} * 100\%$$

On systems with turbo charger the inclusion of altitude correction factors is dropped!

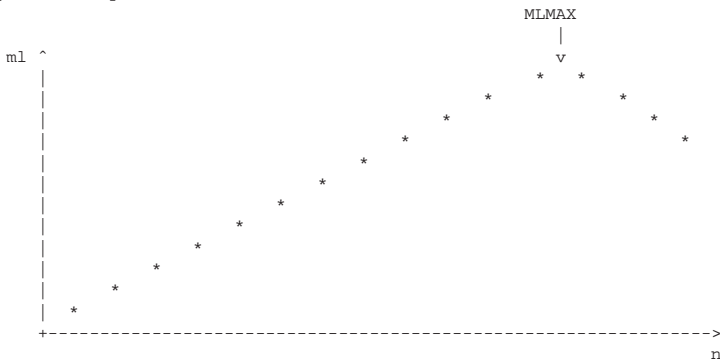
The calculation of rml is performed for a) + b) with the quantization 0 ... 255 dec corresponds to 0 ... 100 % .  
The calculation is to be performed every 100 ms.

### APP BGRML 1.20 Application hint

Determination of MLMAX:

MLMAX corresponds to the peak airflow of the engine at fully open throttle valve and high engine speed.  
The value MLMAX is usually known to engine manufacturers and is to be adjusted in agreement with the customer.

Example (with open throttle valve):



## EGTE 1.0 Input variables for recording the temperature

### FDEF EGTE 1.0 Function definition

Responsible:

### ABK EGTE 1.0 Abbreviations

### FW EGTE 1.0 Fixed Values

Parameter	Value	Description
-----------	-------	-------------



## FB EGTE 1.0 Detailed description of function

There is no text for this FDEF !!!!

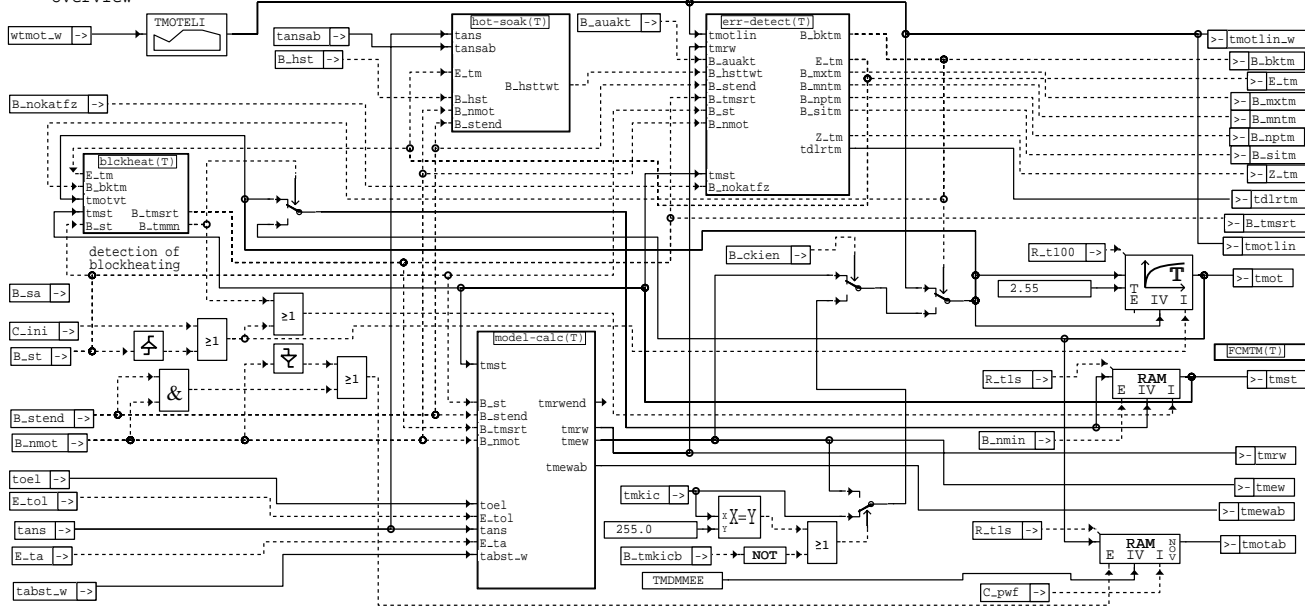
Responsible:

## APP EGTE 1.0 Application hint

## GGTFM 40.60 Signal engine temperature sensor

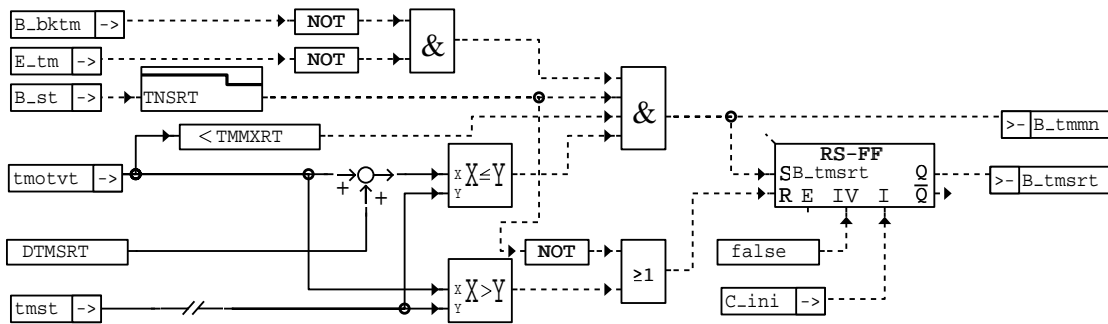
### FDEF GGTFM 40.60 Function definition

overview



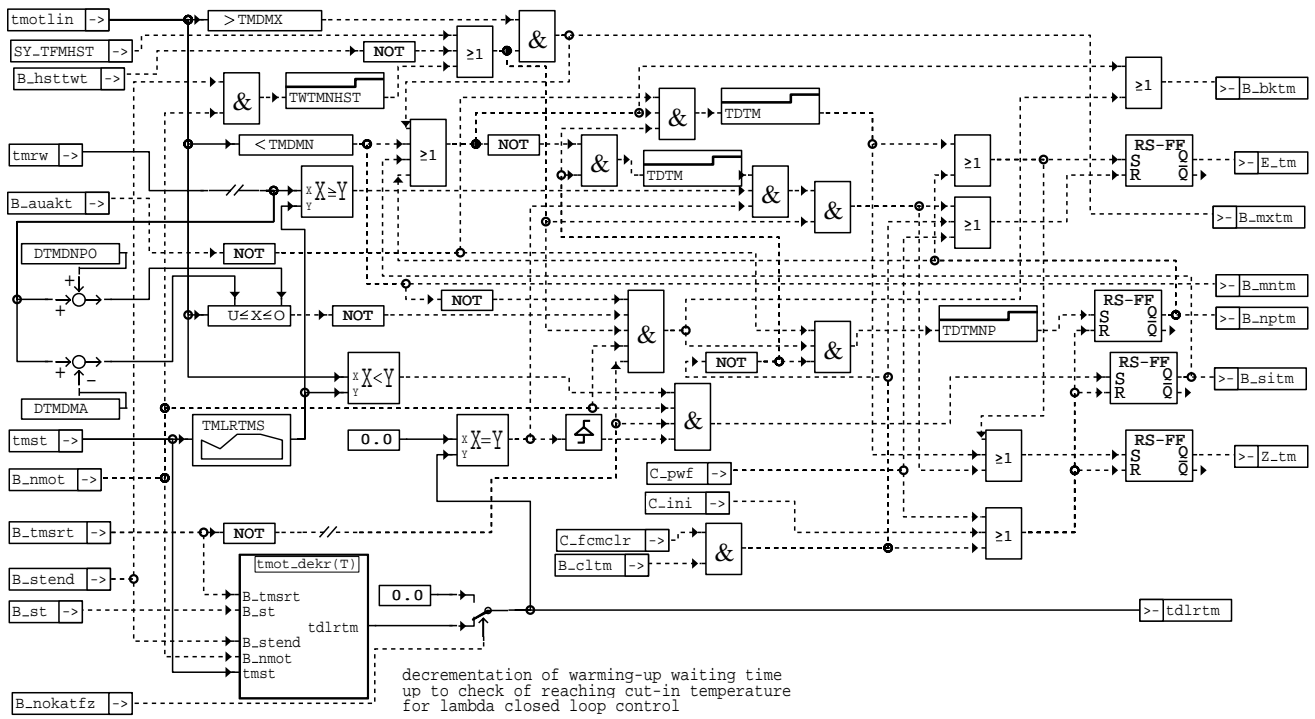
ggtfm-ggtfm

### detection of blockheater



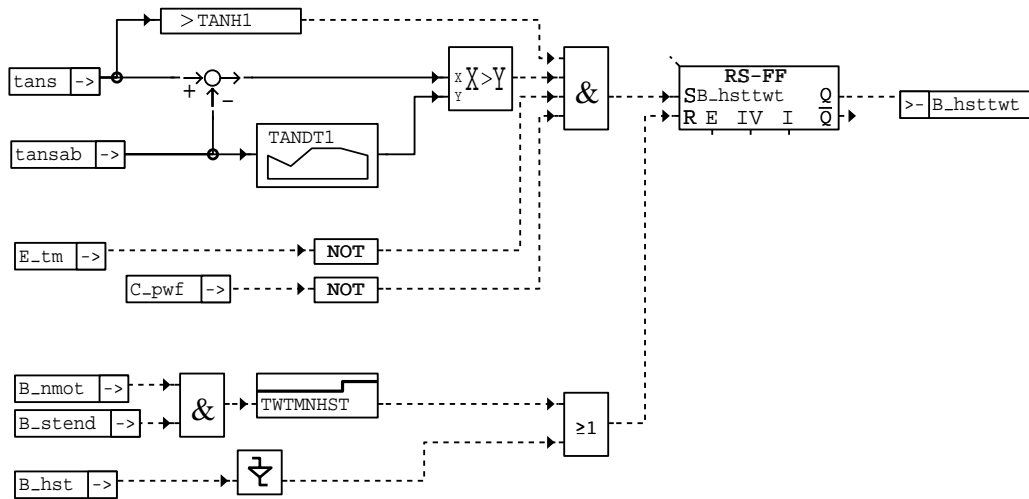
ggtfm-blockheat

section for error detection



ggfm-err-detect

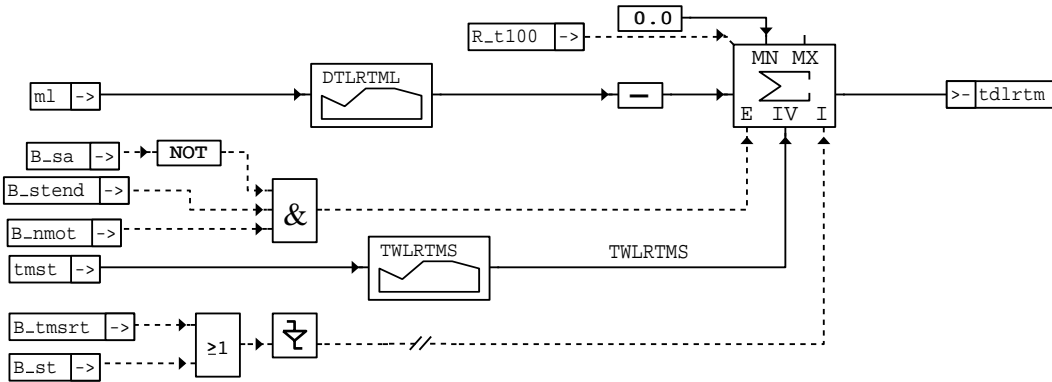
ggfm-err-detect



ggfm-hot-soak

ggfm-hot-soak

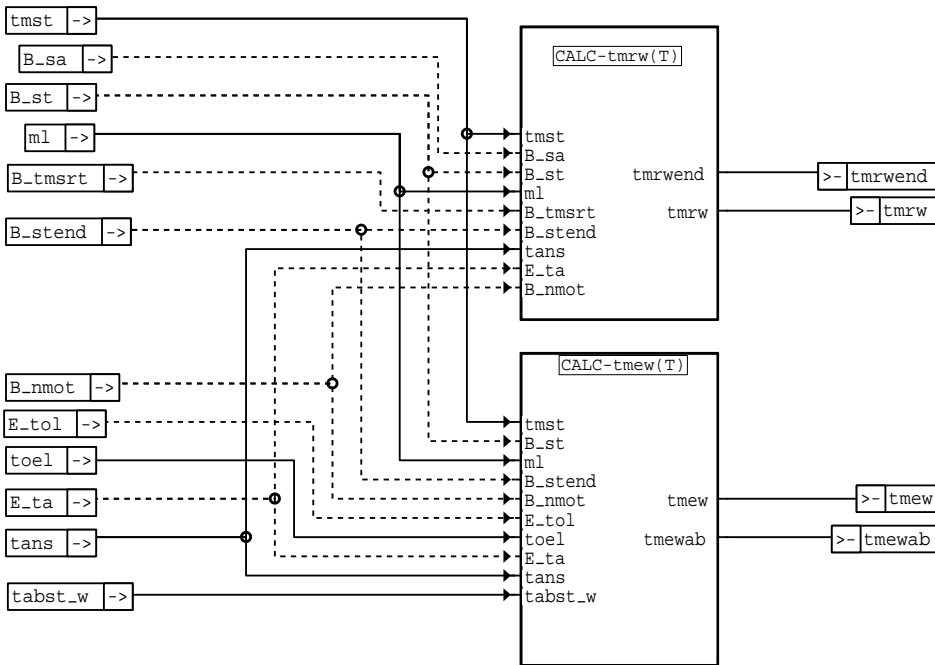
initialization and control of  
warming-up waiting time counter



ggtfm-tmot-dekr

**ggtfm-tmot-dekr**

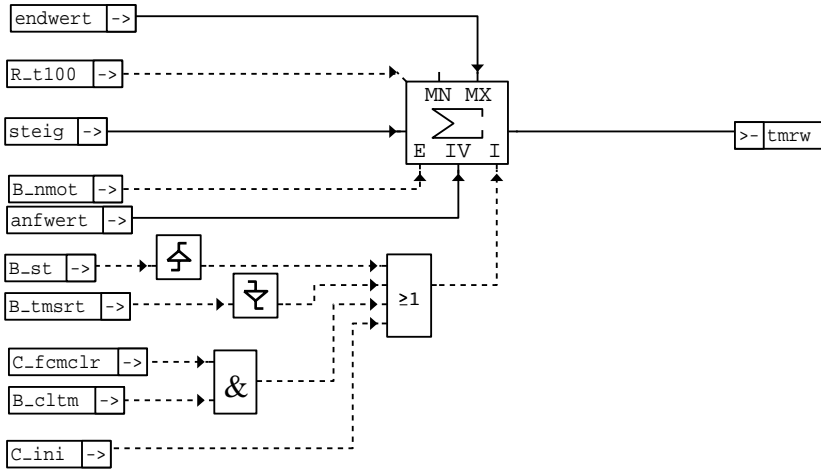
model calculations for engine coolant temperature (overview)



ggtfm-model-calc

**ggtfm-model-calc**

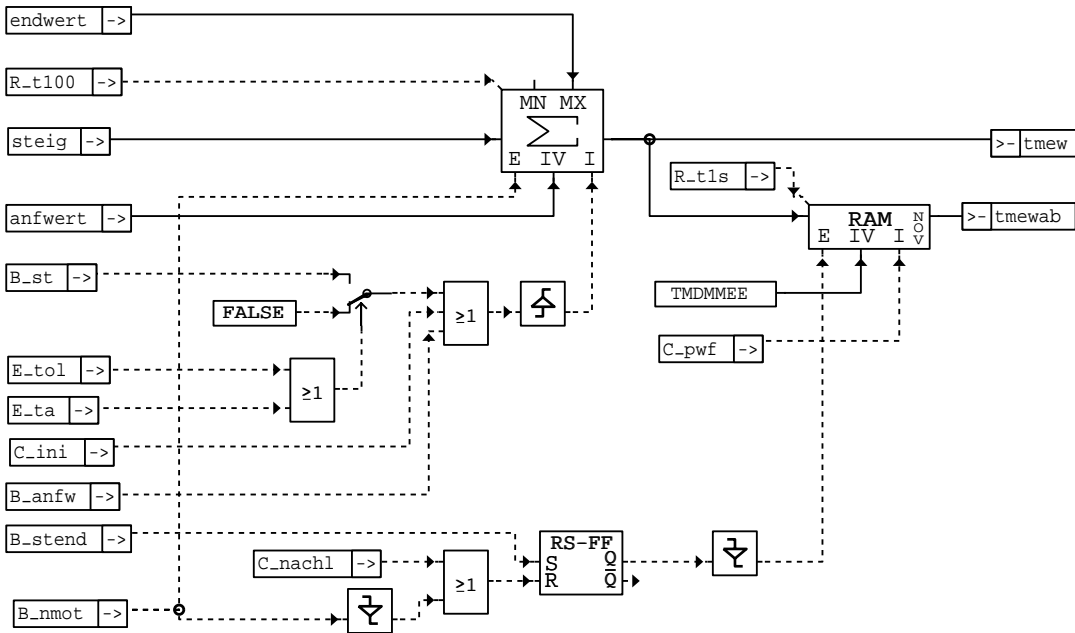
### reference temperature: initialization and control block



ggtfm-ref-temp-mod

#### ggtfm-ref-temp-mod

### substitute temperature: initialization and control block



ggtfm-subst-temp-mod

#### ggtfm-subst-temp-mod

Fault memory management:  
-----

Status fault path TMOT: SFPTM  
Error flag TMOT: E\_tm  
Cycle flag TMOT: Z\_tm  
Fault type TMOT: B\_mxtm  
B\_mntm  
B\_nptm  
B\_sitm



Reset fault path: C\_fmclr & B\_cltm  
Fault path TMOT : CDTM  
Fault class TMOT: CLATM  
Fault rate TMOT: TSFTM  
Carb Code TMOT: CDCTM  
Freeze frame table TMOT: FFTM

## ABK GGTFM 40.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCTM	BLOKNR		KL	code word CARB: engine coolant temperature TMOT
CDTTM			FW	code word tester: engine temperature
CLATM			FW	error class: engine coolant temperature TMOT
DTLRML	ML		KL	proportion factor to decrease waiting time up to tmot-threshold for closed loop
DTMDMA			FW	start offset for engine temperature model
DTMDNPO			FW	offset on engine temperature model to upper threshold for non-plausibility
DTMSRT			FW	difference of engine cool.temp.to starttemp.for retriggering models (blockheater)
FABSTT	TABST_W		KL	Factor parking time for model temperature
FFTTM	BLOKNR		KL	freeze frame table: engine temperature TMOT
KFDTMRS	ML	TMRW	KF	char.line for gradient of engine coolant temp. during cutoff for reference model
KFDTMTE	ML	TMEW	KF	char. map for gradient of engine coolant temperature in substitute temp. model
KFDTMTR	ML	TMRW	KF	char. map for gradient of engine coolant temperature in reference model
KFDTMTU	ML	TUM	KF	char. map for correction gradient of engine coolant temp. at low warming up
TADMM			FW	1. step width (time) for engine temperature model
TANDT1	TANSAB		KL	delta threshold intake air temperature for hot start
TANH1			FW	intake air temperature - threshold hot start
TDTM			FW	debouncing time, engine temperature sensor
TDTMMA			FW	delay time load value engine temperature model
TDTMNP			FW	debouncing time, engine temperature sensor signal not plausible
TMDMMA			FW	begin temperature for engine temperature model
TMDMMAT	TABST_W		KL	Default temperature dependent on parking time during TDTMMA
TMDMMAU			FW	lower start temperature from tans for engine temperature model
TMDMMEE			FW	final temperature for substitute value of engine temperature
TMDMMER			FW	final temperature for reference value of engine temperature
TMDMN			FW	minimum engine temperature
TMDMX			FW	maximum engine temperature
TMLRTMS	TMST		KL	engine temp. threshold for lambda control depending on cranking temp. tmst
TMMXRT			FW	max. engine cool.temp. for retriggering models (blockheater-detection)
TMOTELI	WTMOT_W		KL	engine temperature calculation, inverse function
TNSRT			FW	max. time after start to retrigger calculation of engine temperature model
TSFTM			FW	fault active time: engine coolant temperature sensor TMOT
TUMDET			FW	substitute value of ambient (-air) temperature for engine coolant temp. model
TWLRMTS	TMST		KL	waiting time up to check engine temp. signal exceeding threshold for closed loop
TWTMNHST			FW	waiting time for max.-range check of TMOT following hot soak start

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B_ABSTNLG		EIN	condition soak time calculation via ECM-afterturn is valid
B_ANFW	GGTFM	LOK	condition drive away support activated
B_AUAKT		EIN	condition emission check active
B_BKTM	GGTFM	AUS	condition backup value for engine coolant temperature
B_CKIEN		EIN	condition CAN transfer from instrument cluster enabled
B_CLTM		EIN	condition clear fault path engine coolant temperature TMOT
B_HST	ESSTT	EIN	condition hot start
B_MNTM	GGTFM	AUS	fault type: minimum value of engine coolant temperature
B_MXTM	GGTFM	AUS	fault type: maximum value of engine coolant temperature exceeded
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_NOKATFZ		EIN	condition: no cat vehicle
B_NPTM	GGTFM	AUS	Error type: engine coolant temperature signal not plausible to model
B_SA	MDRED	EIN	Condition fuel cut-off
B_SITM	GGTFM	AUS	Error type: coolant temperature below threshold to cut in lambda closed loop
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_TMKICB		EIN	condition engine temperature from instrument message can be evaluated
B_TMMN	GGTFM	LOK	Condition: blockheater detected
B_TMSRT	GGTFM	AUS	condition: retriggering engine temperature model after start
CW_TABST		EIN	code word to influence initialization of substitute value by switch off time
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_NACHL		EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP	EIN	ECU-condition powerfail intialisation
E_TA	GGTFA	EIN	error flag: TANS
E_TM	GGTFM	AUS	Error flag: engine temperature tmot
E_TOL		EIN	Error flag: oil temperature
ML	SWADAP	EIN	air mass flow
R_T100		EIN	Time schedule 100 ms
R_T1S		EIN	Time schedule 1 s
SFPTM	GGTFM	AUS	status fault path: engine coolant temperature TMOT
SY_TFMA	PROKON	EIN	system constant: intake air temperature signal available (initial. GGTFM)
SY_TFMHST		EIN	sastem constant:
SY_TFMO	PROKON	EIN	system constant: engine oil temperature signal available (initial. GGTFM)
SY_TFUMG	PROKON	EIN	system constant: ambient temperature sensor present



Variable	Source	Type	Description
TABST_W	BGTABST	EIN	soak time
TANS	SWADAP	EIN	Intake air temperature
TANSAB	GGTFA	EIN	Intake air temperature when engine is shut-off
TDLRTM	GGTFM	AUS	remaining time up to check of tmot-signal exceeding threshold for closed loop
TMEW	GGTFM	AUS	model-based substitute value for engine temperature signal in case of error
TMEWAB	GGTFM	AUS	Engine temperature default value from model when parking
TMKIC		EIN	engine temperature from instrument message
TMOT	GGTFM	AUS	Engine temperature
TMOTAB	GGTFM	AUS	engine coolant temperature at engine stop or cut-off cranking
TMOTLIN	GGTFM	AUS	Engine coolant temperature, linearised and calculated
TMOTLIN_W	GGTFM	AUS	Engine coolant temperature, linearised and calculated, 16bit word
TMOTVT	GGTFM	LOK	engine coolant temperature at low-pass input
TMRW	GGTFM	AUS	model-based reference value for plausibility check of engine temperature signal
TMRWEND	GGTFM	LOK	final value for the reference value of the engine temperature model
TMST	GGTFM	AUS	engine temperature at start
TOEL		EIN	Oil temperature
TUM	GGTFM	LOK	ambient (air) temperature
WTMOT_W		EIN	ADC result of engine temperature sensor 10 bit
Z_TM	GGTFM	AUS	cycle flag: engine temperature TMOT

### FW GGTFM 40.60 Fixed Values

Parameter	Value	Description
CDTTM		code word tester: engine temperature
CLATM		error class: engine coolant temperature TMOT
DTMDMA		start offset for engine temperature model
DTMDNPO		offset on engine temperature model to upper threshold for non-plausibility
DTMSRT		difference of engine cool.temp.to starttemp.for retriggering models (blockheater)
TADMM		1. step width (time) for engine temperature model
TANH1		intake air temperature - threshold hot start
TDTM		debouncing time, engine temperature sensor
TDTMMA		delay time load value engine temperature model
TDTMNP		debouncing time, engine temperature sensor signal not plausible
TMDMMA		begin temperature for engine temperature model
TMDMMAU		lower start temperature from tans for engine temperature model
TMDMEE		final temperature for substitute value of engine temperature
TMDMMER		final temperature for reference value of engine temperature
TMDMN		minimum engine temperature
TMDMX		maximum engine temperature
TMMXRT		max. engine cool.temp. for retriggering models (blockheater-detection)
TNSRT		max. time after start to retrigger calculation of engine temperature model
TSFTM		fault active time: engine coolant temperature sensor TMOT
TUMDETM		substitute value of ambient (-air) temperature for engine coolant temp. model
TWTMNHST		waiting time for max.-range check of TMOT following hot soak start
Immediate constant		
ZFTMOT = 2.4 s (realization with 2.55 sec)		

### FB GGTFM 40.60 Detailed description of function

Description of the overview and detection of blockheating:

Under normal circumstances, the engine temperature tmot is established from the input signal utmot linearized via TMOTELI. In the event of an error, which is determined via the fault detection, there is an immediate switchover to a substitute temperature which is computed from a model. The fault detection tests for plausibility of the temperature course as well as testing the minimum and maximum values.

That temperature initially sampled is stored as engine start temperature (under tmst), to be refreshed at the beginning of start.

A start with pre-heated block is supposed according to the measured temperature curve during a one-shot timeout after start (TNSRT). As long as the engine temperature is determined to be lower than the value initially measured (in this case B\_tmsrt =true is valid), the value for engine start temperature is refreshed up to its minimum as preparation for retriggering models. As soon as these conditions disappear, the calculations of the minimum plausibility limit (reference temperature model) resp. the waiting time up to check exceeding cut-in temperature for lambda closed loop control will be released.

In order to receive a "turn-off ignition" temperature, the validated temperature value is stored cyclically in a permanent-RAM cell named tmotab under normal operation conditions after end-of-start; restoring additionally during start up to any break.

Description of the fault detection:

If the linearized engine temperature tmotlin exceeds the maximum or minimum plausibility limits, B\_maxflr and B\_minflr are set respectively, as are the error and cycle flags after the debounce time TDTM has elapsed.

A plausibility check of the engine temperature is performed by a comparison of the measured engine temperature tmotlin with a reference temperature tmrw. The reference temperature tmrw which is continually updated is reduced by the safety margin DTMDMA and compared with the temperature determined. If this does not increase by the amount expected (e.g. parallel circuit or short circuit to a plausible potential), the error flag is set is set after the same debounce time TDTM as above. During the retrigger phase induced by blockheating, the plausibility check is precautionarily disabled.

Furthermore, it is checked whether the engine temperature exceeds the switch-on threshold for lambda closed loop control. The engine temperature must exceed this threshold after a given period of time which depends on the engine starting temperature. The processing of the waiting time  $t_{dlrtm}$  is influenced depending on the air mass flow. Decreasing of the waiting time is stopped during fuel cutoff mode in particular. If the temperature threshold to cut in lambda control is not reached within the time this period has elapsed, the  $B\_signal=1$  is set and a fault entry is made by  $E\_tm$ . As the waiting time until attainment of the cut-in threshold is itself dependent on this temperature, the waiting time must be adjusted accordingly to a change in the temperature threshold. The error path  $B\_signal$  is suppressed after a start with the block heater as long as the conditions for this are present ( $B\_tmsrt=1$ ).

The cycle flag is set immediately upon occurrence of a fault  $E\_tm$ . The cycle flag is set without a fault entry, not only after expiration of the waiting time  $t_{dlrtm}$  but also when the reference temperature  $tmrw$  has reached the cut-in temperature for lambda closed loop control.

The error flag is reset by  $B\_noflr$ , if there is no fault present for the debounce time TDTM. This debounce time is necessary in order that at scattered interferences on e.g. a broken line will not always be detected as being in order.

**B\_maxflr:** - low input voltage by short circuit to ground  
The picked up signal by the RB's standard NTC engine temperature sensor permit the direct information of an unplausible temperature range above TMDMX.

**B\_minflr:** - high input voltage by cable drop or short circuit to supply voltage  
For the circuitry variant without  $R\_parallel$ , this threshold must be disabled, i.e.  $TMDMN=00h$ .

**B\_plaus:** - increase in the engine temperature is not plausible

**B\_signal:** - engine temperature threshold to enable lambda closed loop control not attained after the waiting period

#### Model temperatures:

By the creation of a model, a reference temperature for the diagnosis and a substitute temperature, which is employed, if a fault condition exists, are established. Both model temperatures' characteristic lines are independent of each other.

#### Description of the reference temperature:

Beginning with the measured starting temperature, the reference temperature is updated after a delay time TADMM with a (rising or falling) gradient map-dependent on the air mass flow and the temperature level currently computed. The increase of the model temperature is limited by an upper final value  $tmrwend$ . This final value is derived from the maximum of TMDMMER and the engine temperature threshold to cut in the lambda closed loop control.

Unlike the versions up to 25.xx, possible drops in the engine temperatures or very low rises, such as can occur for example for very low ambient temperatures and operations near to idling/fuel cutoff, are taken into account in the calculation of the reference temperature; i.e. temperature gradients (= gradient S) with a negative sign can be stored in the map KFDIMTR resp. in the characteristic line KLDTMRS, that is selected during fuel cutoff.

#### Description of the substitute temperature:

The substitute temperature is established similar to the reference temperature. They differ however in the following points: In order to prevent an incorrect selection in case of a later detected non-plausibility of  $tmotlin$ , initialization here is not done by starting temperature. Instead of this the initial value is taken from the engine oil temperature, if this signal is available and correct, otherwise from the intake air temperature  $tans$ . Finally a substitute value TMDMMA is taken in case of an error  $E\_ta$  or if no TANS-sensor is present. The initial value taken from  $tans$  is also limited to TMDMMA as required.

The earliest possible detection of an unplausible  $Tmot$  value (following the first AD conversion or for the  $E\_tm$  already set from the previous cycle) leads to the selection of a substitute value. Unlike the versions up to 25.xx, calculations are permitted to reduce the substitute temperature for operations near idling (negative temperature gradients are hence also possible in the map KFDTMTE).







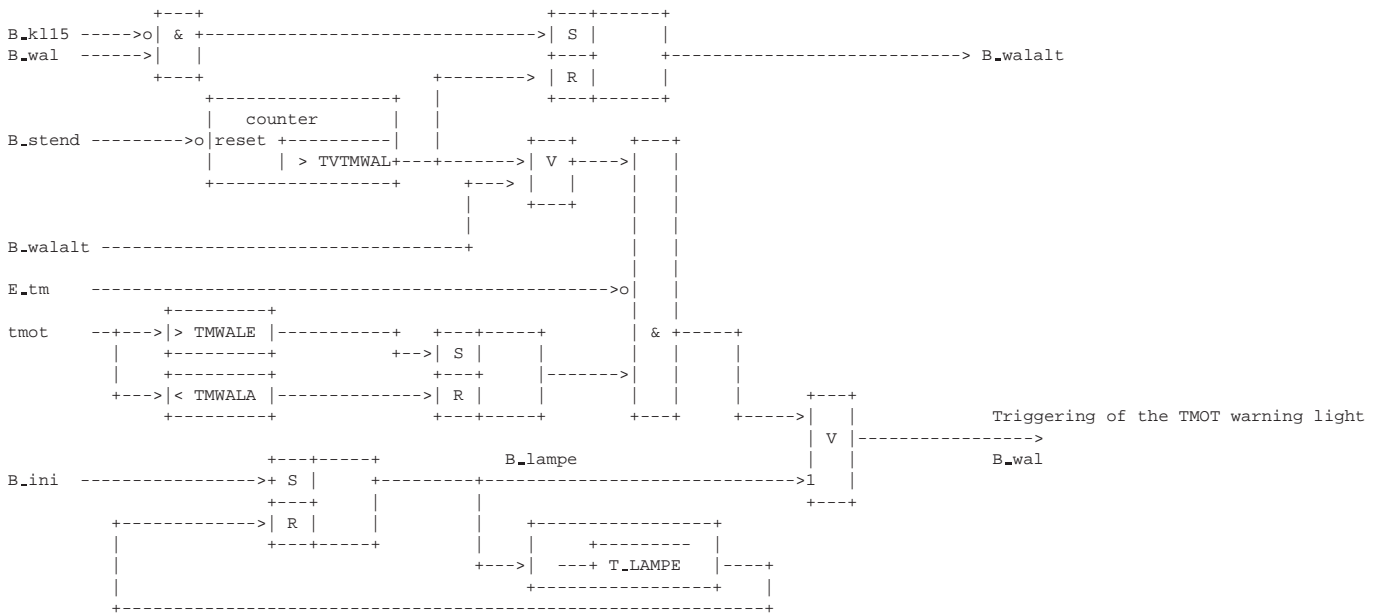
## FB GGPOEL 5.30 Detailed description of function

Die Funktion liest den Öldruckschalter (S\_poell) ein und gibt das Ergebnis über CAN an das Armaturenbrett aus. Der Schalter zeigt an, ob der Öldruck ein bestimmtes Niveau überschritten hat. Dieser Druck kann nur bei laufendem Motor erreicht werden. Wird er jedoch schon bei stehendem Motor angezeigt (S\_poell = TRUE), wird auf einen defekten Schalter geschlossen. Es wird nach Ablauf der Entprellzeit TDEPOEL ein Fehler im Fehlerspeicher abgelegt. Der Fehler wird nur bei Drehzahlen <= NPMOL1 geprüft und ggf. geheilt. Bei gesetztem Fehler E\_poel wird, wie bei zu niedrigem Druck, die Öldruckwarnlampe angesteuert.

## APP GGPOEL 5.30 Application hint

## ATWAL 3.20 Output engine temperature warning lamps

### FDEF ATWAL 3.20 Function definition



### ABK ATWAL 3.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TMWALA			FW	Engine temperature threshold for switching off of warning lamp "too hot"
TMWALE			FW	Engine temperature threshold for switching on of warning lamp "too hot"
TVTMWAL			FW	Delay time after start when the TMOT warning lamp is switched on
T_LAMPE			FW	lamp on time after system start

Variable	Source	Type	Description
B_JNI		EIN	Condition initialization
B_LAMPE	ATWAL	AUS	Lamps on condition after system start for dashboard test
B_STEND	BBSTT	EIN	condition end of start
B_WAL	ATWAL	AUS	Condition switch on warning light in the dashboard
B_WALALT	ATWAL	LOK	Condition warning light when Key Off
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
TMOT	SWADAP	EIN	Engine temperature

### FW ATWAL 3.20 Fixed Values

Parameter	Value	Description
TMWALA		Engine temperature threshold for switching off of warning lamp "too hot"
TMWALE		Engine temperature threshold for switching on of warning lamp "too hot"
TVTMWAL		Delay time after start when the TMOT warning lamp is switched on
T_LAMPE		lamp on time after system start



## FB ATWAL 3.20 Detailed description of function

The TMOT warning light is installed in the dashboard and is triggered when TMOT becomes greater than an adjustable value (TMWALE). The correct operation of the warning light is checked by triggering it for the time T\_LAMPE while terminal 15 is switched on and with the engine at standstill (when T\_LAMPE = FFhex it applies: Permanently on until end of start). When the engine is turned off (key off) the current value of B\_wal is stored in the permanent RAM (B\_walalt). To prevent a possible incorrect triggering by stored heat of the engine, the warning light is only triggered after an adjustable time after end of start. If the light was already triggered when the engine was last turned off (B\_walalt = TRUE), this blocking time is ignored.

## APP ATWAL 3.20 Application hint

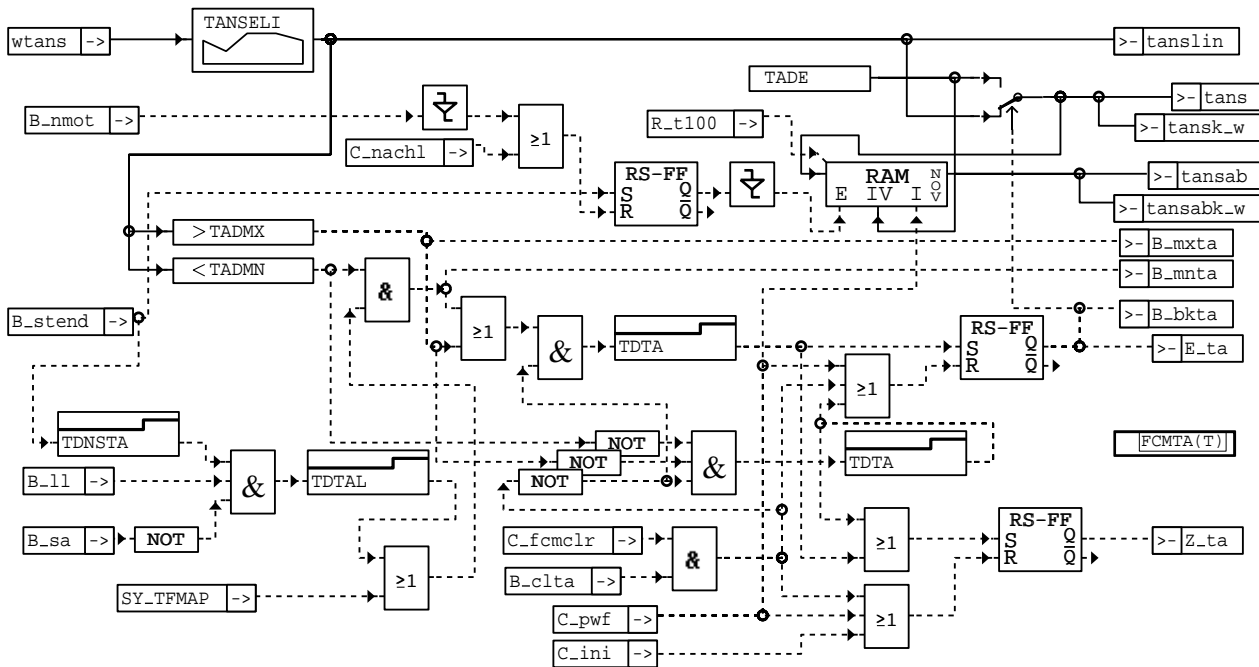
Value Range / Initial Entering of Data into the Adjustable Labels:

TMWALE: 100 deg.....125 deg. / 120 deg.  
 TMWALA: 100 deg.....125 deg. / 118 deg.  
 TVTMWAL: 0 sec.....204 sec / 30 sec  
 T\_LAMPE: 0 sec.....25.5 sec / 4 sec (Remark: T\_LAMPE = 25.5 sec corresponds to light permanently on with engine at standstill)

## GGTFA 15.50 Diagnosis; intake air temperature sensor

### DDEF GGTFA 15.50 Function definition

GGTFA acquisition and diagnostic checks of signal from intake air temperature input



### ggfta-ggfta

Fault memory management:

Status fault path TANS: SFPTA  
 Error flag TANS: E\_ta  
 Cycle flag TANS: Z\_ta  
 Fault type TANS: B\_mxta  
                   B\_mnta  
                   B\_npta  
                   B\_sita

Reset fault path: C\_fmclr & B\_clta  
 Fault path TANS : CDTTA  
 Fault class TANS: CLATA  
 Fault rate TANS: TSFTA  
 Carb Code TANS: CDCTA  
 Freeze frame table TANS: FFTTA



## ABK GGTFA 15.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCTA	BLOKNR		KL	code word CARB: intake air temperature
CDTTA			FW	code word tester: intake-air temperature
CLATA			FW	error class: intake air temperature TANS
FFTTA	BLOKNR		KL	freeze frame table: air intake temperature TANS
TADE			FW	substitute value air temperature in case of fault
TADMN			FW	intake-air temperature min.
TADMX			FW	intake-air temperature max.
TANSELI	WTANS		KL	intake air temperature calculation, inverse function
TDNSTA			FW	exhaust manifold warming time from start, for TANS - Diagnostic
TDTA			FW	time for diagnosis intake air temperature sensor
TDTAL			FW	intake-air temperature error detection/time-out from B_LL = 1
TSFTA			FW	fault active time: intake air temperature sensor TANS
Variable	Source		Type	Description
BLOKNR			EIN	DAMOS source for block number
B_BKTA	GGTFA		AUS	condition backup value for intake air temperature
B_CLTA			EIN	condition clear fault path intake air temperature TANS
B_LL	MSF		EIN	Condition idle
B_MNTA	GGTFA		AUS	fault type: minimum value of intake air temperature TANS
B_MXTA	GGTFA		AUS	fault type: maximum value of intake air temperature TANS exceeded
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_SA	MDRED		EIN	Condition fuel cut-off
B_STEND	BBSTT		EIN	condition end of start
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_NACHL			EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
E_TA	GGTFA		AUS	error flag: TANS
R_T100			EIN	Time schedule 100 ms
SFPTA	GGTFA		AUS	status fault path: air intake temperature TANS
SY_TFMAP	PROKON		EIN	system constant: intake air temp.sensor with shunt resistor in input circuitry
TANS	GGTFA		AUS	Intake air temperature
TANSAB	GGTFA		AUS	Intake air temperature when engine is shut-off
TANSABK_W	GGTFA		AUS	Intake air temperature when engine is shut-off in Kelvin
TANSK_W	GGTFA		AUS	Intake air temperature in Kelvin
TANSLIN	GGTFA		AUS	intake air temperature, linearised and calculated
WTANS			EIN	ADC-value for intake air temperature
Z_TA	GGTFA		AUS	cycle flag: intake air temperature

## FW GGTFA 15.50 Fixed Values

Parameter	Value	Description
CDTTA		code word tester: intake-air temperature
CLATA		error class: intake air temperature TANS
TADE		substitute value air temperature in case of fault
TADMN		intake-air temperature min.
TADMX		intake-air temperature max.
TDNSTA		exhaust manifold warming time from start, for TANS - Diagnostic
TDTA		time for diagnosis intake air temperature sensor
TDTAL		intake-air temperature error detection/time-out from B_LL = 1
TSFTA		fault active time: intake air temperature sensor TANS

## FB GGTFA 15.50 Detailed description of function

Following function description for version TANS-NTC circuitry with pullup-R and with parallel resistor to TANS-sensor (e.g. 2,87 kOhms resp. 36,5 kOhms) --> SY\_TFMAP=1 !

Fault detection (set Errorflag E.ta)

Directly scanning of exceeding the threshold values is practicable without any additional conditions.

Debouncing times overlap electric disturbance by coupling on the lines as well as line-conducted faults or short loose contacts.

In a tolerance calculation the following fault cases were observed:

- Short circuit at sensor input (E.A.TANS) to UBat/5V : Sampling maximum value of utans --> tanslin below TADMN.  
Generally sensor or/and printed circuit board parts melted in event of short-circuit to UB; damages in case of short circuits to 5V dependent on temperature resp. current on occurrence of fault!
- Short circuit at sensor input (E.A.TANS) to ground : Sampling minimum value of utans --> tanslin above TADMX.  
Taking into account voltage drops and other uncertainties, the threshold should be choosen corresponding to a value of a regular intake air temperature of more than approx. 125 deg.C (does not occur).
- Interruption of sensor lines : Sampling high value of utans --> tanslin exceeding TADMN  
Assuming a shunt at the sensor input (E.A.TANS) of RN = 500 kOhms, a fault under those conditions corresponds to a plausible intake air temperature of less than -35 deg.C.

Faults are only cleared after a debouncing time to prevent switchover to faulty plausible values, e.g. resulting from electrical interference coupled in the cable, when dropped off.

Cycle flag Z.ta is set either as soon as a fault is detected or, in case of no fault, after all branches of the test have been run through.



Following function description for version TANS-NTC circuitry with pullup-R only (e.g. 1kOhm), no parallel resistor to TANS-sensor --> SY\_TFMAP=0 !

Fault detection (set Errorflag E\_ta)

Directly scanning of exceeding of threshold values is only practicable for maximum limit without additional conditions. Debouncing times overlap electric disturbance by coupling on the lines as well as line-conducted faults or short loose contacts. In a tolerance calculation the following fault cases were observed:

- Short circuit at sensor input (E.A.TANS) to UBat/5V : Sampling maximum value of utans --> tanslin below TADMN.  
Generally sensor or/and printed circuit board parts melted in event of short-circuit to UB; damages in case of short circuits to 5V dependent on temperature resp. current on occurrence of fault!
- Short circuit at sensor input (E.A.TANS) to ground : Sampling minimum value of utans --> tanslin above TADMX.  
Taking into account voltage drops and other uncertainties, the threshold should be chosen corresponding to a value of a regular intake air temperature of more than approx. 140 deg.C (does not occur).
- Interruption of sensor lines : Sampling high value of utans --> tanslin exceeding TADMN (?)  
Assuming a shunt at the sensor input (E.A.TANS) of  $R_N = 500 \text{ kOhm}$ , a fault under those conditions corresponds to a plausible intake air temperature of (-30 ..-32) deg.C. That won't be low enough for cold-starts in many applications.  
In order to diagnose this fault, additional conditions (as waiting time TDNSTA after end-of-start elapsed, idling for time TDOTAL at a minimum and no fuel cutoff) are scanned and, if matched, enable to assume safely, that the TANS sensor must output a higher value as a result of heat transmission from the engine. Otherwise --> below TADMN.

Faults are only cleared after a debouncing time to prevent switchover to faulty plausible values, e.g. resulting from electrical interference coupled in the cable, when dropped off.

Cycle flag Z\_ta is set either as soon as a fault is detected or, in case of no fault, after all branches of the test have been run through.

#### APP GGTF 15.50 Application hint

Checking of the tanslin < TADMN fault detection, which can occur as a consequence of a short circuit to supply voltage or a break, may only be provoked by a break; applying battery voltage may cause the NTC sensor to be damaged !

Reference values for RB-TANS standard sensor circuitry with shunt resistor

(under above mentioned dimensioning  $R_{vor} = 2,87 \text{ kOhms}$  ,  $R_{par} = 36,5 \text{ kOhms}$ ):

TADMX approx. 125 deg.C ; TADMN approx. -35 deg.C (tolerance!) ; TADE 20 deg.C ; TDTA approx. 200 msec

Reference values for RB-TANS standard sensor circuitry without shunt resistor

(under above mentioned dimensioning  $R_{vor} = 1 \text{ kOhm}$  , no  $R_{par}$ ):

TADMX ca. 140 deg.C ; TADMN ca. -30 deg.C (Toleranz!) ; TADE 20 deg.C ; TDTA ca. 200 msec , TDNSTA ca. 4 min

## EGAK 3.0 Input values of exhaust value of catalyst

### FDEF EGAK 3.0 Function definition

zuständig:

### ABK EGAK 3.0 Abbreviations

### FW EGAK 3.0 Fixed Values

Parameter	Value	Description
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### FB EGAK 3.0 Detailed description of function

Beschreibung fehlt !!!!

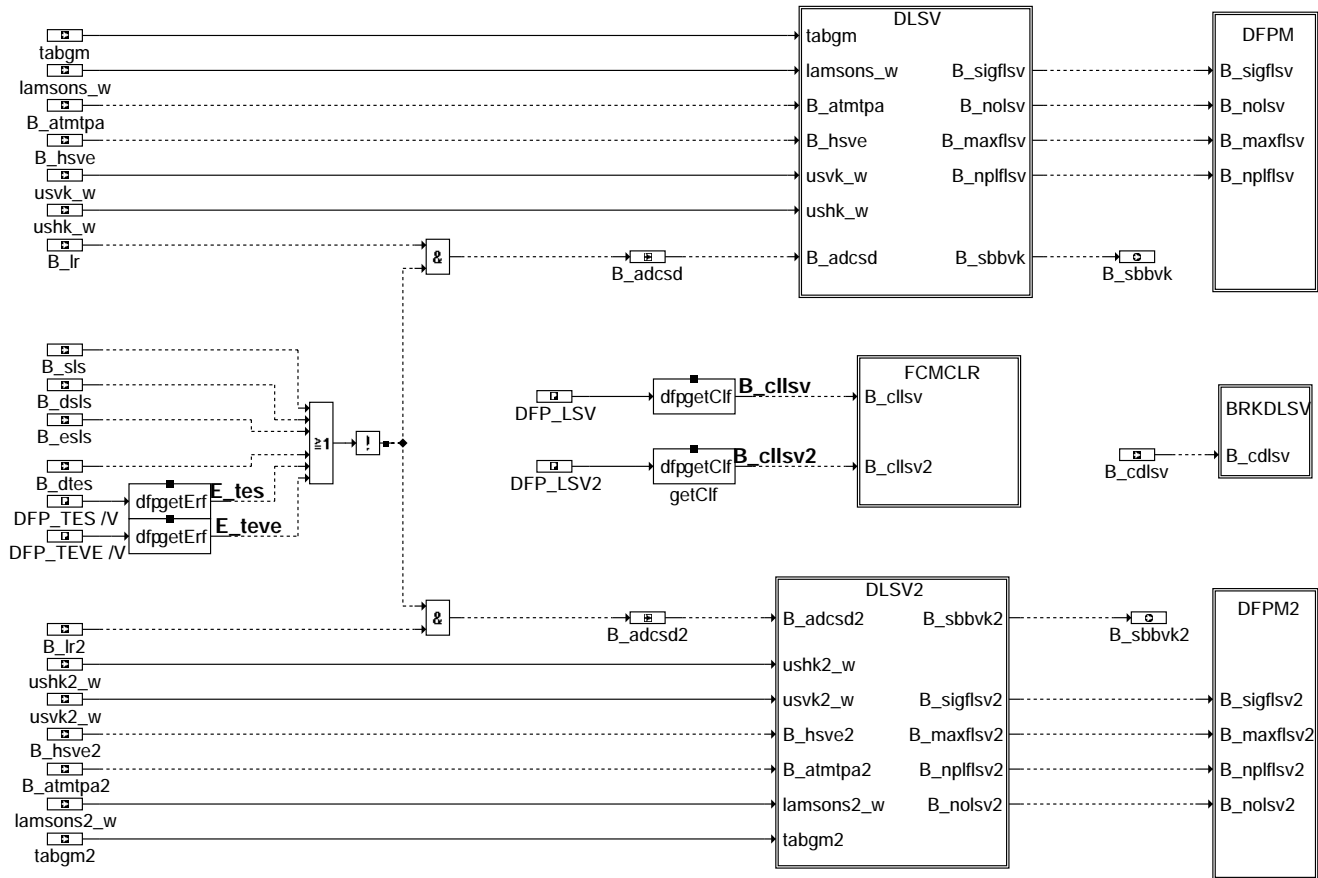
zuständig:

## APP EGAK 3.0 Application hint

## DLSV 32.60 Diagnosis; Readiness for operation of sensor upstream catalyst

### FDEF DLSV 32.60 Function definition

MAIN: Übersicht und Darstellung der elektrischen Sonden-Diagnose vor KAT

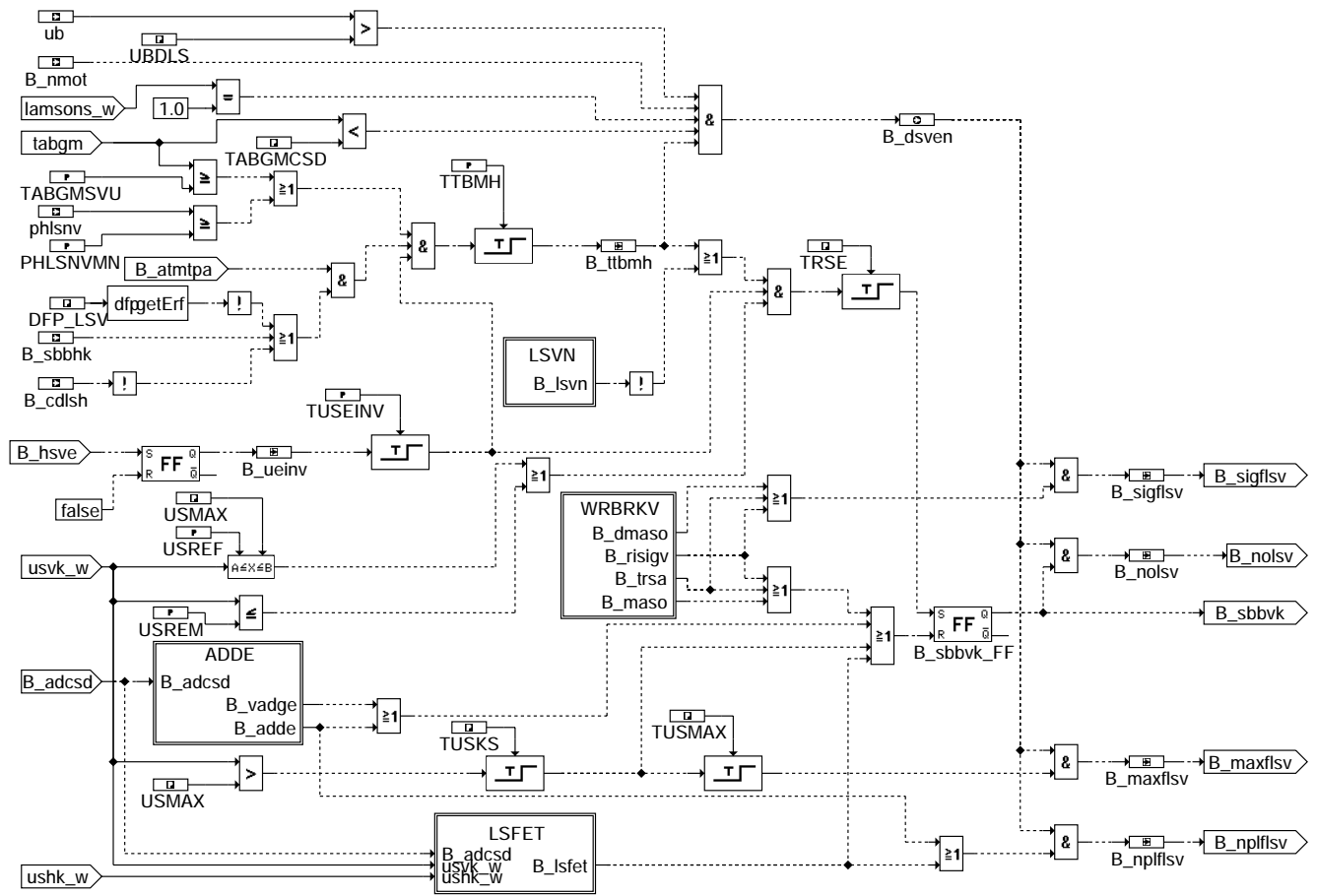


dlsv-main

dlsv-main



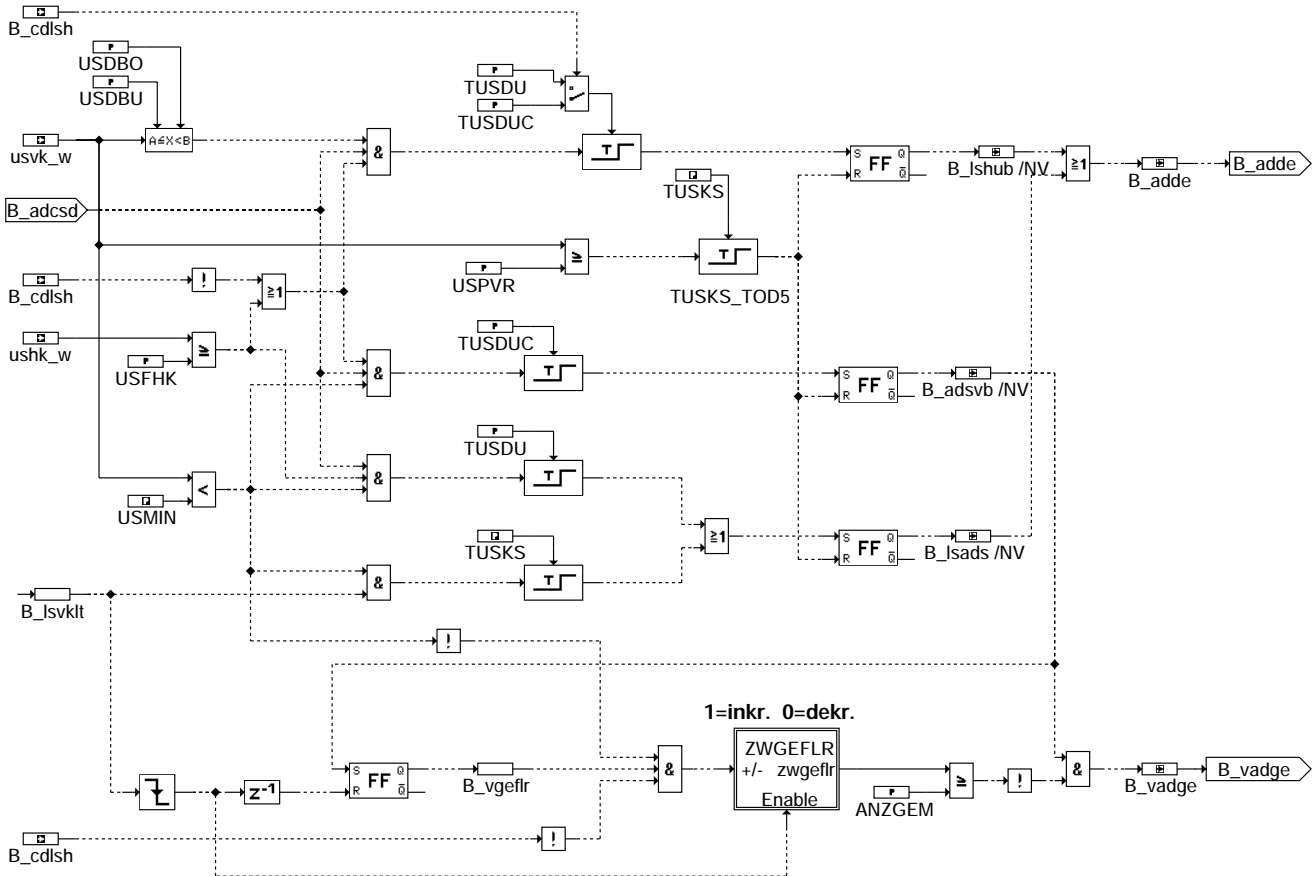
DLSV: Funktion



dlsv-dlsv

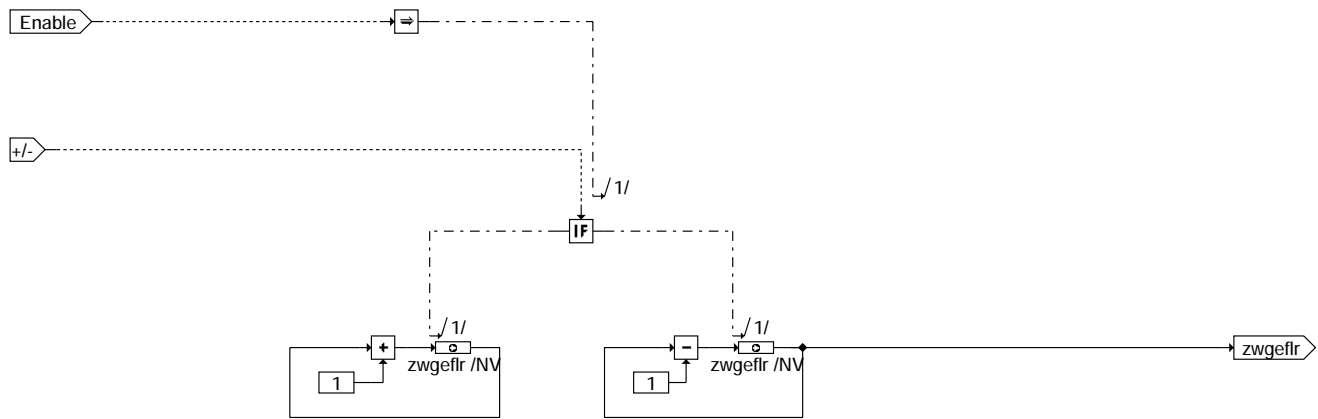
dlsv-dlsv

ADDE: Erkennung Adernschluß und Sonde mit begrenztem Spannungshub



dlsv-adde

ZWGEFLR: Ereigniszähler für Europa-Version zur Unterscheidung Adernschluß oder Gemischfehler

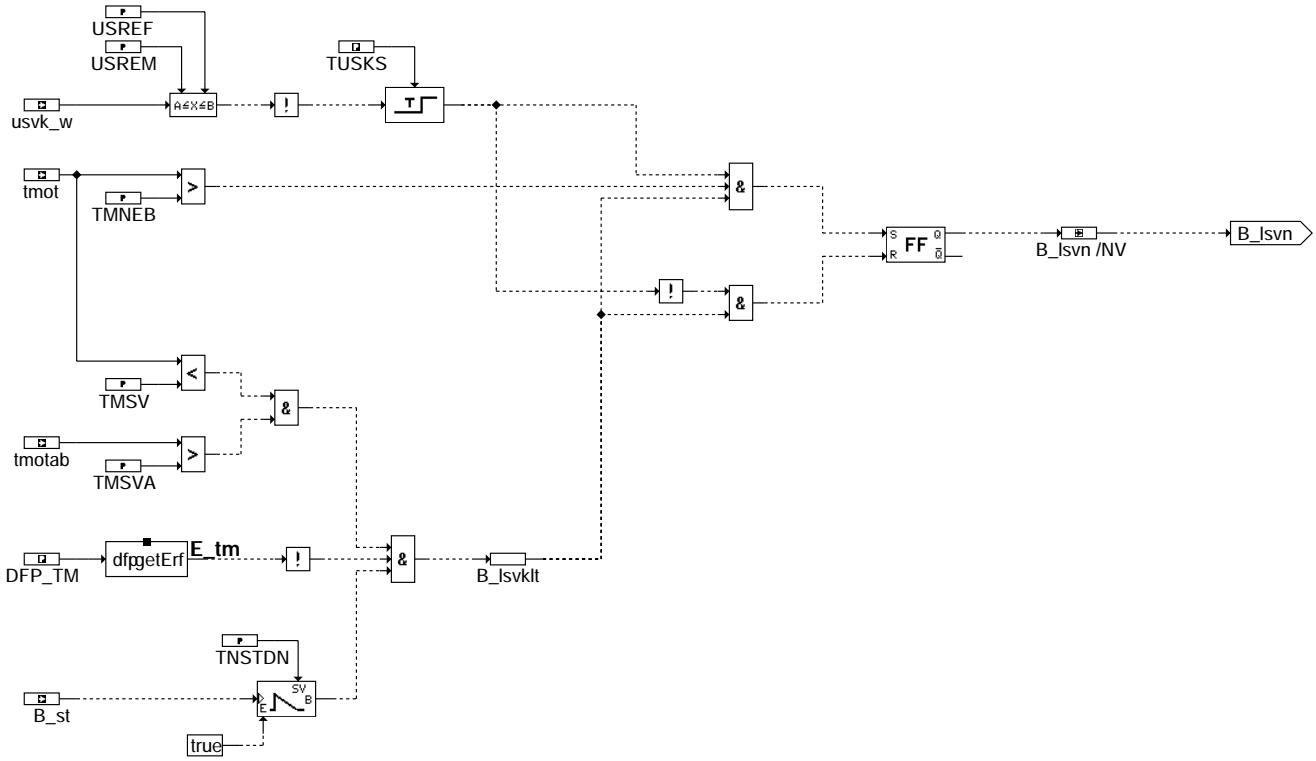


dlsv-zwgefir



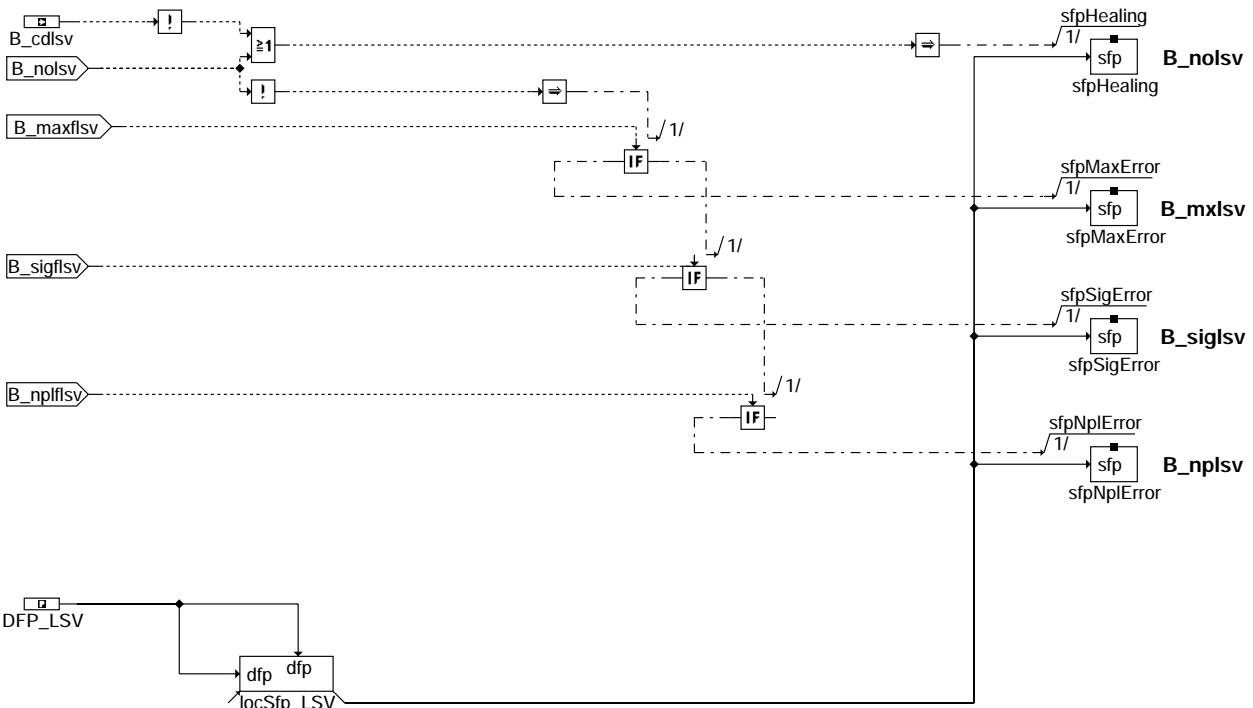


LSVN: Erstellung der Kaltbedingung B\_lsvkit (kalte Sonde) und Erkennung Nebenschlußnch UBatt und SG-Masse bei Kalter Sonde



**dlsv-lsvn**

DFPM: Fehlerverwaltung DLSV



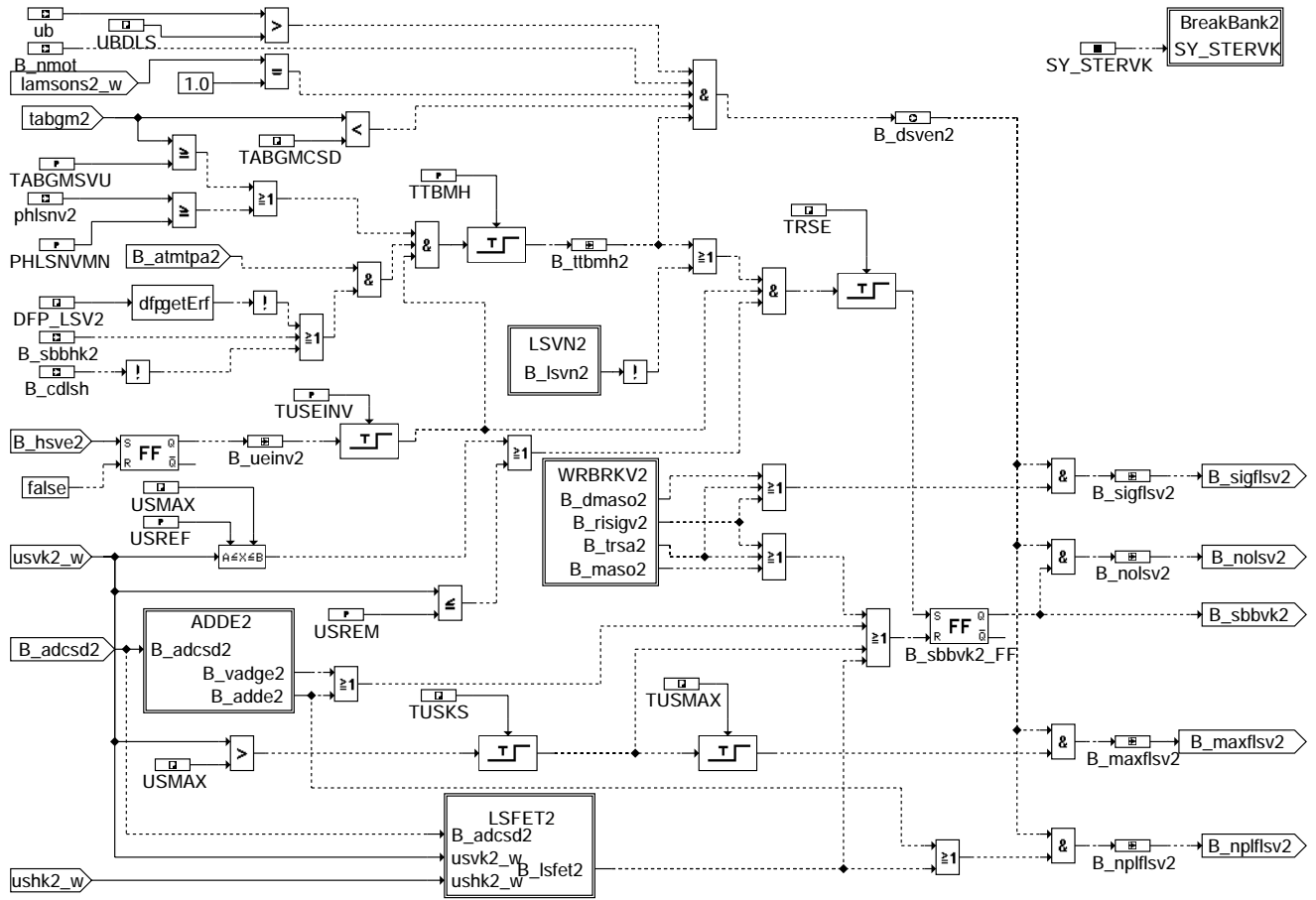
**E\_lsv = 1 if B\_mxflsv or B\_sigflsv or B\_nplsv is set**  
**E\_lsv = 0 if B\_nolsv is set**

**Z\_lsv = 1 if B\_nolsv or B\_mxflsv or B\_sigflsv or B\_nplsv is set**

**dlsv-dfpm**

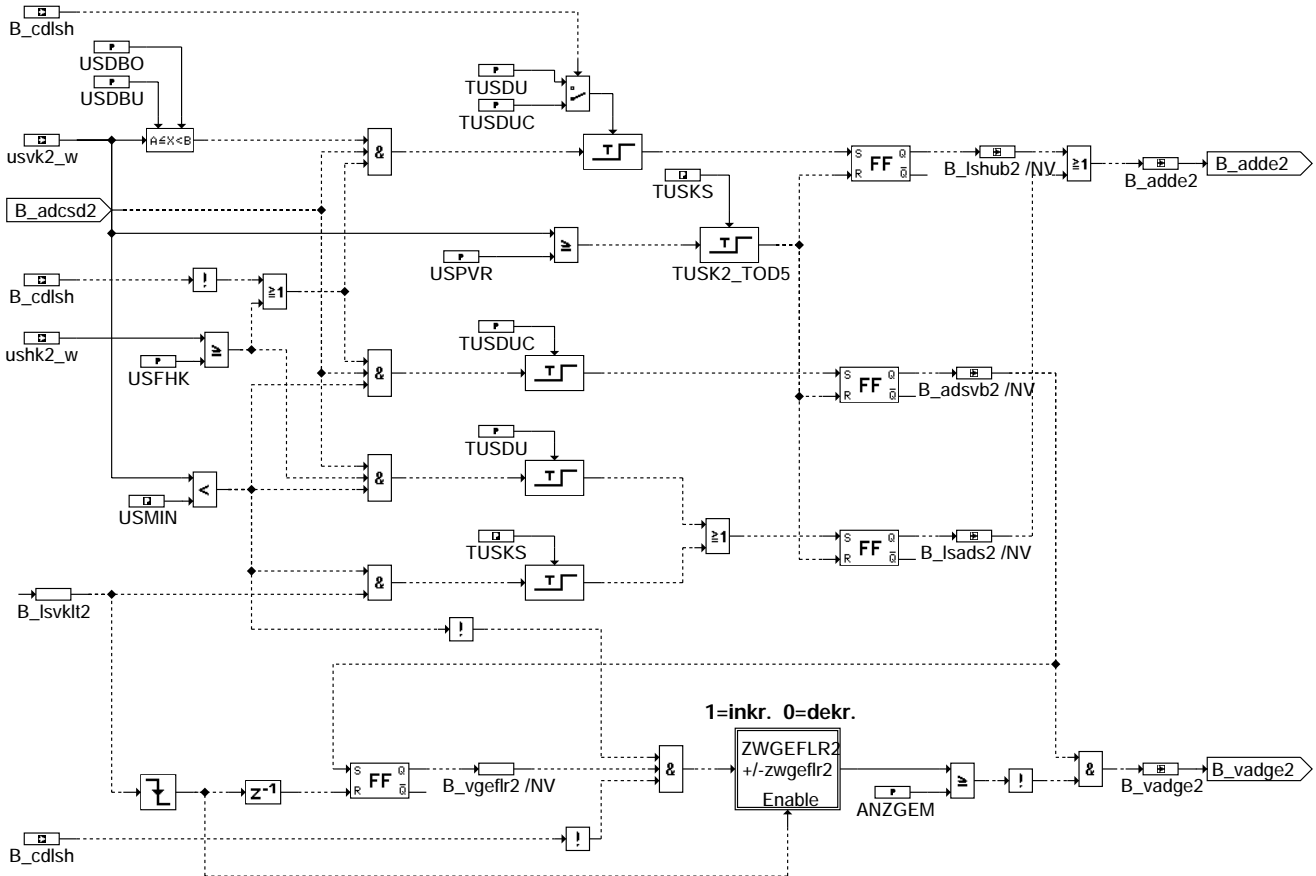


DLSV2: Funktion Bank2



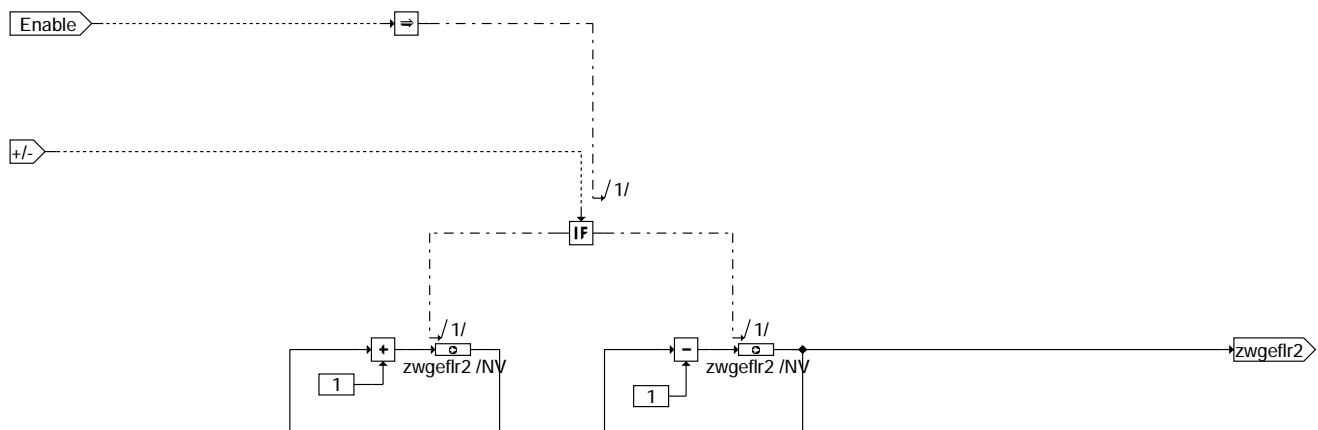


ADDE2: Erkennung Adernschluß und Sonde mit begrenztem Spannungshub Bank2



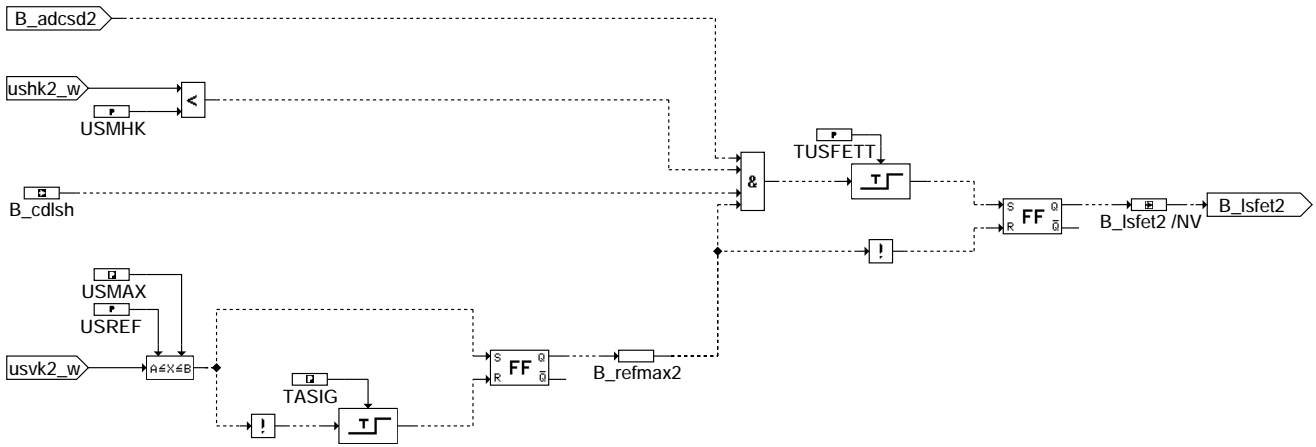
dlsv-adde2

ZWGEFLR2: Ereigniszähler für Europa-Version zur Unterscheidung Adernschluß oder Gemischfehler Bank2



dlsv-zwgefir2

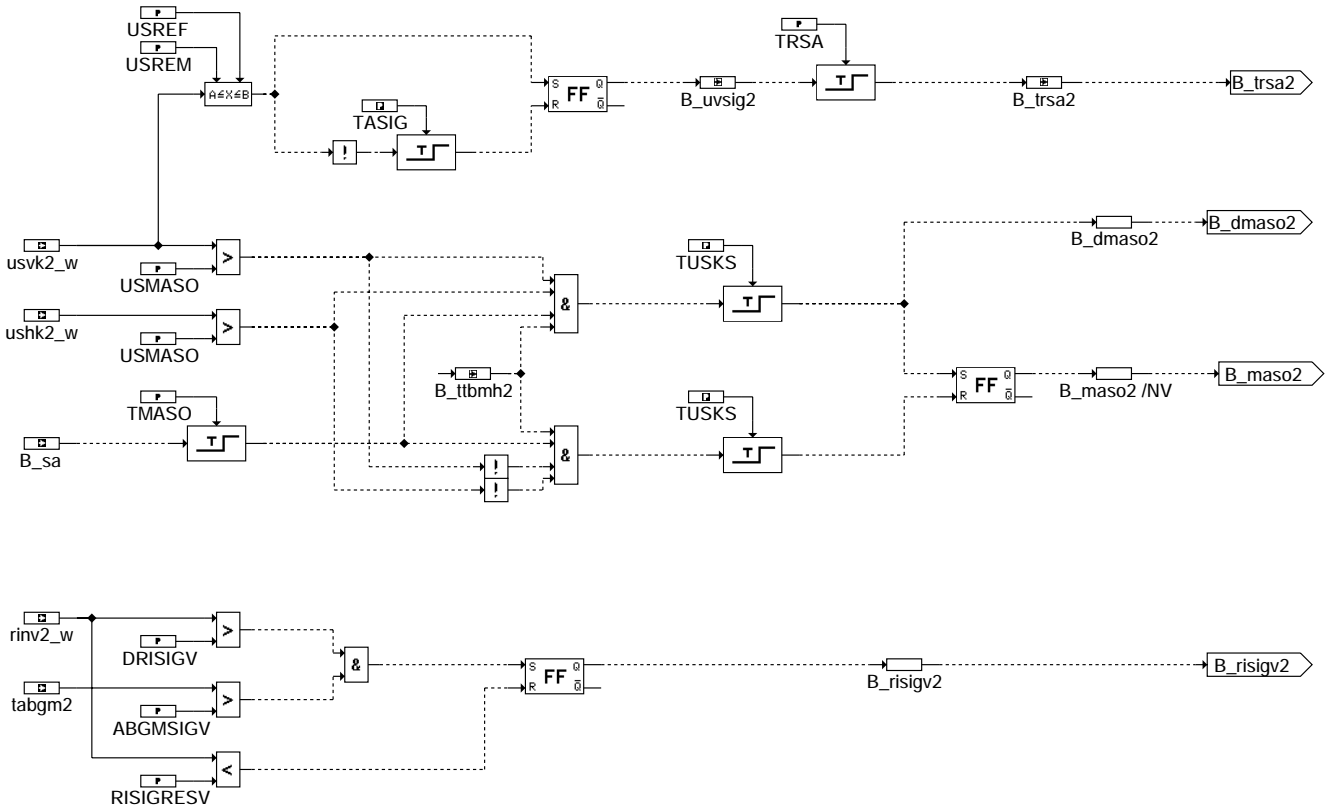
L5FET2: Erkennung Nebenschluß nach Ubatt und Kabelbruch der Sondenmasse einer planaren Sonde Bank2



dlsv-lsfet2

dlsv-lsfet2

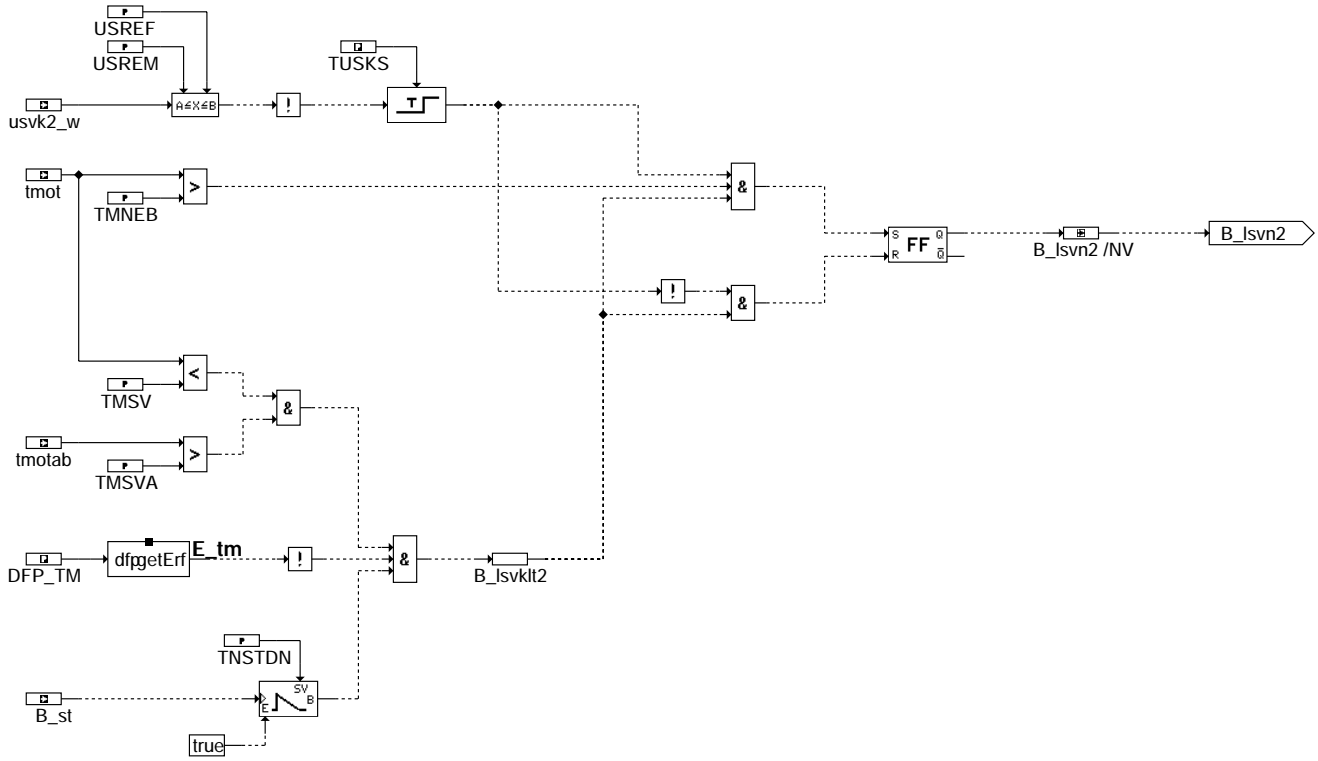
WRBRK2: Erkennung Signalunterbrechung; Erkennung Abfall gemeine Sondenmasse; Erkennung Unterbrechung Sondenmasse einer plan. Sonde



dlsv-wrbrk2

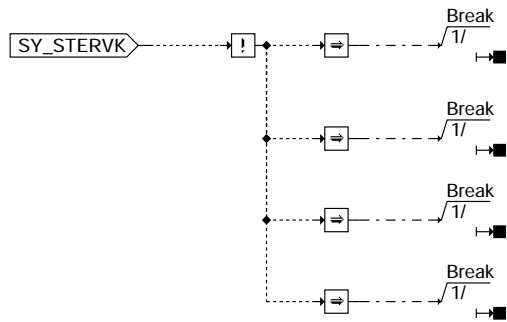
dlsv-wrbrk2

L SVN2: Erstellung der Kaltbedingung B\_lsvklt (kalte Sonde) und Erkennung Nebenschlußnach UBatt und SG-Masse bei Kalter Sonde Bank2



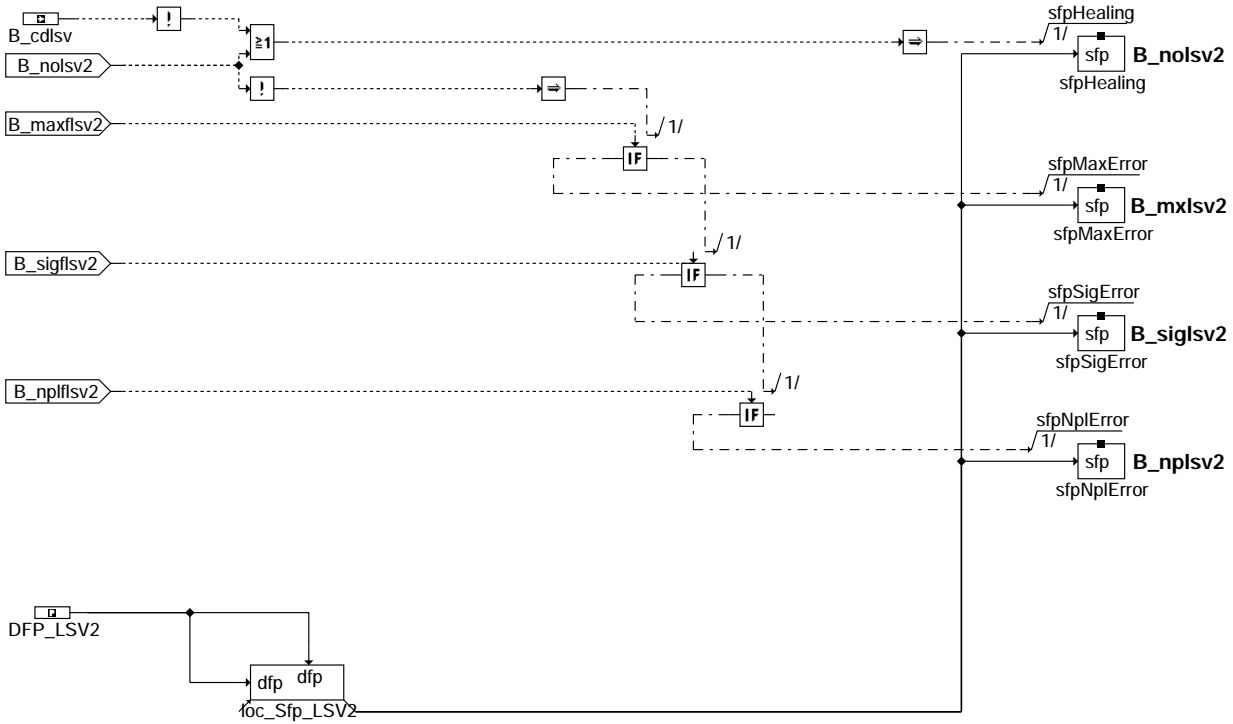
### dlsv-lsvn2

BreakBank2: SY\_STERVK



### dlsv-breakbank2

DFPM2: Fehlerverwaltung DLSV

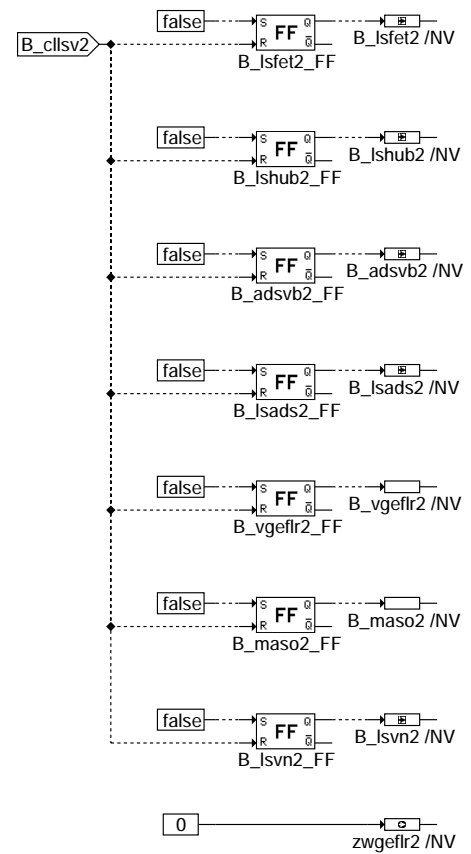
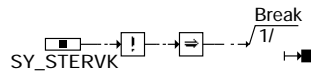
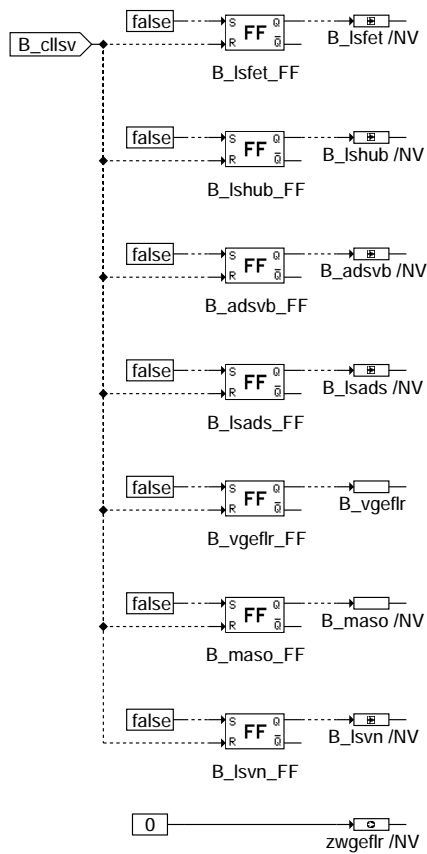


E\_Isv2 = 1 if B\_mxlsv2 or B\_siglsv2 or B\_nplsv2 is set  
 E\_Isv2 = 0 if B\_nolsv2 is set  
 Z\_Isv2 = 1 if B\_nolsv2 or B\_mxlsv2 or B\_siglsv2 or B\_nplsv2 is set

dlsv-dfpm2

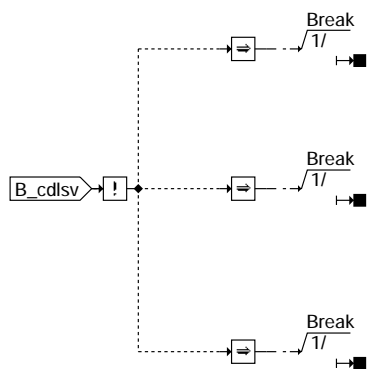
dlsv-dfpm2

FCMCLR: Fehlerspeicher löschen



dlsv-fcmclr

BRKDLSV: Abschalten der Funktion



Bei B\_cdlsv = 0 wird Funktion DLSV nicht gerechnet

dlsv-brkdlsv

In block diagrams fault type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the fault path xyz back into the central diagnosis management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external fault paths which occur as inputs, access methods are available which read these informations directly from the fault path status managed in the DFPM.



For each fault path "lsv" of this diagnosis function the following values are defined:

	Bank 1	Bank 2
Status fault path lsv:	sfplsv	sfplsv2
Error flag xyz:	E_lsv	E_lsv2
Cycle flag xyz:	Z_lsv	Z_lsv2
Fault type xyz:	TYP_lsv: (B_mxplsv, B_silsv, B_nplsv)	TYP_lsv2: (B_mxplsv2, B_silsv2, B_nplsv2)
Clear fault path:	B_cllsv	B_cllsv2
Default value active:	B_bklsv (optional)	B_bklsv2 (optional)
Fault path code lsv:	CDTlsv	CDTlsv2
Fault class lsv:	CLAlsv	CLAlsv2
Fault intensity lsv:	TSFlsv	TSFlsv2
CARB CODE lsv:	CDClsv	CDClsv2
Table of ambient cond. lsv:	FFTlsv	FFTlsv2

## ABK DLSV 32.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ABGMSIGV			FW	threshold for exhaust temp. for wiring-interruption with Ri-diagnosis upstr. cat
ANZGEM			FW	number of mixture fault
CDKLSV2			FW	code word customer: lambda sensor downstream cat
CDTlsv2			FW	code word tester: lambda sensor 2 upstream catalyst [018]
CLALSV2			FW	fault class: O2 sensor bank 2 pre cat
DRISIGV			FW	diagnosis threshold for Ri sensor for signal disconnection pre cat
PHLSNVMM			FW	minimal normalised heating-power-diagnosis sensor pre catalyst
RISIGRESV			FW	threshold for reset wiring-interruption with Ri-diagnosis upstr. cat
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TABGMCSVD			FW (REF)	threshold for exhaust temperature for measuring CSD
TABGMVSUV			FW	temp. threshold from exhaust temp. modell for diagn. sensor upstream
TASIG			FW (REF)	Time for the deactiv.of interf. peaks outside of range for det.of signal interr.
TMASO			FW	time after fuel cut off for commen open sensor ground
TMNEB			FW	Engine temprature threshold for measurement of sensor shunt pre cat
TMSV			FW	engine temp. threshold for recognition cold start for measuring sensor upstream
TMSVA			FW	threshold for engine switch-off temp. for measuring cooling sensor upstream cat
TNSTDN			FW	time after start for diagnosis shunt resistance fault (monoflop)
TRSA			FW	monitoring time closed-loop control (upstream CAT) -> sensor off
TRSE			FW (REF)	monitoring time -> closed-loop control on
TSFLSV2			FW	fault active time: lambda sensor catalyst upstream, bank 2
TTBMH			FW	period for theoretical operation readiness of sensor with heating
TUSDU			FW	time delay for detec. intercore short circ. and sensor with limit. volt. up.cat
TUSDUC			FW	delay time code for detec. wire-to-wire sh. circ. of the oxyg. sens. upstr. cat
TUSEINV			FW	Delay time for condition Lambda sensor ready bit
TUSFETT			FW	time delay for detec. current leakage to Ubatt upstream cat
TUSKS			FW (REF)	delay time for short circuit detection on the oxygen sensor
TUSMAX			FW (REF)	monitoring time for Usmax
UBDLS			FW (REF)	battery voltage threshold for release the sensor diagnosis
USDBO			FW	upper limit wire-to-wire detection and defective O2-sensor limited voltage range
USDBU			FW	lower limit wire-to-wire detection and defective O2-sensor limited voltage range
USFHK			FW	sensor voltage threshold for detection 'rich' downstream cat
USMASO			FW	sensor voltage threshold for commen open sensor ground
USMAX			FW (REF)	threshold for short circuit of sensor to Ubatt
USMHK			FW	sensor voltage threshold for detection 'rich' downstream cat
USMIN			FW (REF)	threshold for short circuit of sensor to ground
USPVR			FW	threshold for reset of fault "potential offset" of sensor upstream cat
USREF			FW	threshold for operation readiness of sensor at rich mixture (upstream CAT)
USREM			FW	threshold for operation readiness of sensor at lean mixture (upstream CAT)

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B_ADCSD	DLSV	LOK	condition for test of short-circuit and CSD
B_ADCSD2	DLSV	LOK	condition for test of short-circuit and CSD bank2
B_ADDE	DLSV	LOK	condition short circuit or defective sensor with limited voltage amplitude
B_ADDE2	DLSV	LOK	condition short circuit or defective sensor bank2 with limited voltage amplitude
B_ADsvB	DLSV	LOK	prohibition operating readiness because of SC wire-to-wire
B_ADsvB2	DLSV	LOK	prohibition operating readiness because of SC wire-to-wire bank2
B_ATMTPA	ATM	EIN	condition temperature upstream catalyst exceeds dew-point
B_ATMTPA2	ATM	EIN	condition temperature upstream catalyst exceeds dew-point2
B_BELSV	DLSV	AUS	Condition: function request for elctr. diag. sensor voltage upstream cat
B_BELSV2	DLSV	AUS	Condition: function request for elctr. diag. sensor voltage upstream cat bank2
B_BKLSV	DLSV	AUS	Condition: lambda sensor upstream cat. active
B_BKLSV2	DLSV	AUS	Condition: lambda sensor upstream cat. active bank2
B_CDLSH	PROKON	EIN	function active per codeword CDLSH
B_CDLSV	PROKON	EIN	function active per codeword CDLSV
B_CLLSV		EIN	Delete fault path in DLSV.
B_CLLSV2		EIN	Delete fault path in DLSV. Bank2
B_DMASO	DLSV	LOK	condition common lamda sensor ground open "dynamic"
B_DMASO2	DLSV	LOK	condition common lambda sensor ground open "dynamic" bank2
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DSVEN	DLSV	AUS	condition enable sensor diagnosis upstream catalyst
B_DSVEN2	DLSV	AUS	condition enable sensor diagnosis upstream catalyst bank2
B_DTES	GKRA	EIN	Condition for active diagnosis of canister purge system





Variable	Source	Type	Description
B_ESLS		EIN	Condition secondary air fault by wrong air mass flow
B_FTLSV	DLSV	AUS	Condition fault entry by tester for lambda sensor upstream cat
B_FTLSV2	DLSV	AUS	Condition fault entry by tester for lambda sensor upstream cat bank2
B_HSVE	HLS	EIN	condition for lambda sensor heating-switch upstream cat on
B_HSVE2	HLS	EIN	condition for lambda sensor2 heating-switch upstream cat on
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LSADS	DLSV	LOK	condition for lambda sensor upstream cat SC wire to wire
B_LSADS2	DLSV	LOK	condition for Lambda sensor upstream cat wire to wire bank2
B_LSFET	DLSV	LOK	condition for sensor voltage current leakage to UBatt upstream cat
B_LSFET2	DLSV	LOK	condition for sensor voltage current leakage to UBatt upstream cat bank2
B_LSHUB	DLSV	LOK	condition for lambda sensor upstream cat with restricted signal amplitude
B_LSHUB2	DLSV	LOK	condition for lambda sensor upstream cat with restricted sensor voltage bank 2
B_LSVKLT	DLSV	LOK	condition cold oxygen sensor upstream catalyst
B_LSVKLT2	DLSV	LOK	condition cold oxygen sensor upstream catalyst bank2
B_LSVN	DLSV	LOK	condition leakage resistance at cold oxygen sensor upstream catalyst
B_LSVN2	DLSV	LOK	Condition leakage resistance at cold sensor upstream catalyst
B_MASO	DLSV	LOK	condition common lambda sensor ground open
B_MASO2	DLSV	LOK	condition common lambda sensor ground open on bank 2
B_MAXFLSV	DLSV	LOK	Short circuit to battery voltage at O2 sensor pre cat
B_MAXFLSV2	DLSV	LOK	Short circuit to battery voltage at O2 sensor pre cat Bank 2
B_MNLSV	DLSV	AUS	Condition for fault type "minimum value" upstream cat detected
B_MNLSV2	DLSV	AUS	Condition for fault type "minimum value" upstream cat detected bank2
B_MXLSV	DLSV	AUS	Condition for fault type "maximum value" upstream cat detected
B_MXLSV2	DLSV	AUS	Condition for fault type "maximum value" upstream cat detected bank2
B_NMOT	GGDFG	EIN	condition engine speed: n > NMIN
B_NOLSV	DLSV	LOK	Condition diagnosis finished with o.k. upstream cat report
B_NOLSV2	DLSV	LOK	Condition diagnosis finished with o.k. upstream cat report bank2
B_NPLFLSV	DLSV	LOK	Short circuit between cables at O2 sensor pre cat
B_NPLFLSV2	DLSV	LOK	Short circuit between cables at O2 sensor pre cat bank 2
B_NPLSV	DLSV	AUS	Condition fault type "value not plausible" detected
B_NPLSV2	DLSV	AUS	Condition fault type "value not plausible" detected bank2
B_PWF		EIN	Condition for powerfail
B_REFMAX	DLSV	LOK	Condition O2-sensor voltage in plausible area between USREF and USMAX,pre cat
B_REFMAX2	DLSV	LOK	Condition O2-sensor voltage in plausible area between USREF and USMAX ,bank2
B_RISIGV	DLSV	LOK	Condition signal disconnection of sensor ground with Ri-diagnosis
B_RISIGV2	DLSV	LOK	Condition signal disconnection of sensor ground with Ri-diagnosis, bank 2
B_SA	MDRED	EIN	Condition fuel cut-off
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_SBBVK	DLSV	AUS	condition for lambda sensor upstream cat ready for operation
B_SBBVK2	DLSV	AUS	condition oxygen sensor upstream cat. bank2 ready for operation
B_SIGFLSV	DLSV	LOK	Signal interruption at O2 sensor upstream cat
B_SIGFLSV2	DLSV	LOK	Signal interruption at O2 sensor upstream cat bank 2
B_SILSV	DLSV	AUS	condition for fault type 'signal missing' upstream cat detected
B_SILSV2	DLSV	AUS	condition for fault type 'signal missing' upstream cat detected bank2
B_SLS	AK	EIN	Condition for active secondary air
B_ST	SWADAP	EIN	condition for start
B_TRSA	DLSV	LOK	Condition wiring interruption for sensor upstream catalyst
B_TRSA2	DLSV	LOK	Condition wiring interruption for sensor downstream catalyst bank 2
B_TTBMH	DLSV	LOK	condition theoretical lambda sensor operation readiness with heating
B_TTBMH2	DLSV	LOK	condition theoretical lambda sensor operation readiness with heating bank2
B_JEINV	DLSV	LOK	Condition: preparation of setting the O2 sensor ready condition
B_JEINV2	DLSV	LOK	Condition: preparation of setting the O2 sensor ready condition bank 2
B_JVVSIG	DLSV	LOK	Condition O2 sensor voltage pre cat in voltage band for signal interruption
B_JVVSIG2	DLSV	LOK	Condition O2 sensor voltage pre cat in voltage band for signal interruption ba.2
B_VADGE	DLSV	LOK	condition suspect for short circuit or mixture failure
B_VADGE2	DLSV	LOK	condition suspect of short-circuit or mixture failure on bank 2
B_VGEFLR	DLSV	LOK	condition suspicion of mixture fault
B_VGEFLR2	DLSV	LOK	condition suspicion of mixture fault bank 2
DFP_LSV	DLSV	DOK	ECU int. fault path no.: electrical diagnosis for lambda sensor upstream cat.
DFP_LSV2	DLSV	DOK	ECU int. fault path no.: electr. diagnos. for lambda sensor upstream cat. bank 2
DFP_TES	DLSV	DOK	Internal error path number evap system monitoring, pcv Struck open
DFP_TEVE	DLSV	DOK	Internal fault path number: canister purge valve power stage
DFP_TM	DLSV	DOK	Internal fault path number: engine temperature
E_LSV	DLSV	AUS	error flag: lambda sensor upstream catalyst
E_LSV2	DLSV	AUS	error flag: lambda sensor upstream catalyst
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
LAMSONS2_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
PHLSNV	HLS	EIN	normalized heating power of lambda sensor upstream of catalyst
PHLSNV2	HLS	EIN	normalized heating power of lambda sensor 2 upstream of catalyst
RINV2_W	GGLSV	EIN	Actual value of internal resistance of lambda sensor 2, pre ca
RINV_W	GGLSV	EIN	Actual value of internal resistance of lambda sensor,pre cat (word)
SFPLSV	DLSV	AUS	status fault path: diagnosis of lambda sensor upstream of catalyzer
SFPLSV2	DLSV	AUS	status fault path:
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TMOT	SWADAP	EIN	Engine temperature
TMOTAB	GGTFM	EIN	engine coolant temperature at engine stop or cut-off cranking



Variable	Source	Type	Description
UB	SWADAP	EIN	battery voltage
USHK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst 2
USHK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst
USVK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst
ZWGEFLR	DLSV	AUS	counter value of mixture fault
ZWGEFLR2	DLSV	AUS	counter value of mixture fault bank 2
Z_LSV	DLSV	AUS	cycle flag: lambda sensor upstream of catalyst
Z_LSV2	DLSV	AUS	cycle flag: 2nd lambda sensor upstream of catalyst

Abbreviations and terminology

CSD 'chemical shift down' lowered sensor characteristic line due to poisoning  
ECU,SG Electronic control unit  
SC,KS Short circuit

Abbreviations for cross coupling matrix:

Partial function sensor operating readiness - outputs: SB=sensor operating readiness  
- Inputs: S/SB=block/sensor operating readiness

Partial function sensor diagnosis - Outputs: SD=sensor diagnosis  
F/SD=flip-flop sensor diagnosis  
- Inputs: S/SD=block/sensor diagnosis  
B/SD=condition/sensor diagnosis

**FW DLSV 32.60 Fixed Values**

Parameter	Value	Description
ABGMSIGV		threshold for exhaust temp. for wiring-interruption with Ri-diagnosis upstr. cat
ANZGEM		number of mixture fault
CDKLSV2		code word customer: lambda sensor downstream cat
CDTLV2		code word tester: lambda sensor 2 upstream catalyst [018]
CLALV2		fault class: O2 sensor bank 2 pre cat
DRISIGV		diagnosis threshold for Ri sensor for signal disconnection pre cat
PHLSNVMM		minimal normalised heating-power-diagnosis sensor pre catalyst
RISIGRESV		threshold for reset wiring-interruption with Ri-diagnosis upstr. cat
TABGMSVU		temp. threshold from exhaust temp. modell for diagn. sensor upstream
TMASO		time after fuel cut off for commen open sensor ground
TMNEB		Engine temperature threshold for measurement of sensor shunt pre cat
TMSV		engine temp. threshold for recognition cold start for measuring sensor upstream
TMSVA		threshold for engine switch-off temp. for measuring cooling sensor upstream cat
TNSTDN		time after start for diagnosis shunt resistance fault (monoflop)
TRSA		monitoring time closed-loop control (upstream CAT) -> sensor off
TSFLSV2		fault active time: lambda sensor catalyst upstream, bank 2
TTBMH		period for theoretical operation readiness of sensor with heating
TUSDU		time delay for detec. intercore short circ. and sensor with limit. volt. up.cat
TUSDUC		delay time code for detec. wire-to-wire sh. circ. of the oxyg. sens. upstr. cat
TUSEINV		Delay time for condition Lambda sensor ready bit
TUSFETT		time delay for detec. current leakage to Ubatt upstream cat
USDBO		upper limit wire-to-wire detection and defective O2-sensor limited voltage range
USDBU		lower limit wire-to-wire detection and defective O2-sensor limited voltage range
USFHK		sensor voltage threshold for detection 'rich' downstream cat
USMASO		sensor voltage threshold for commen open sensor ground
USMHK		sensor voltage threshold for detection 'rich' downstream cat
USPVR		threshold for reset of fault "potential offset" of sensor upstream cat
USREF		threshold for operation readiness of sensor at rich mixture (upstream CAT)
USREM		threshold for operation readiness of sensor at lean mixture (upstream CAT)

**FB DLSV 32.60 Detailed description of function**

Introduction:

The diagnosis function serves the purpose to detect all possible wiring faults of the Lambda sensor. Output signals are: the fault bit E\_lsv, the cycle bit Z\_lsv and the sensor operating readiness bit B\_sbbvk.

The following fault types are transferred to the fault management logic: ( B\_maxflsv (KS\_UBat), B\_sigflsv (wiring interruption, sensor heating defective), B\_nplflsv (wire-to-wire SC or O2 sensor with limited voltage amplitude). B\_minflsv is not transferred since a short-circuit to electronic ground is tantamount to wire-to-wire SC.

These fault types are stored in a flip-flop in the permanent RAM and they are transferred to the fault memory as B\_mxflsv (SC-UBat), B\_mnlsv (0), B\_silsv (wiring interruption); B\_nplsv (wire-to-wire SC).

Generally, a transfer to the fault management can only take place (B\_dsvn = 1) if the dew point end B\_atmtpa = 1 is exceeded and thus the sensor heating is switched on with B\_hsve =1 and if a sensor-specific time TUSEINV has elapsed and hence was permanently switched on for at least the time TTBMH (that means especially not dutycycled). At the same time the battery voltage ub may not lie below the threshold UBDLS, lamsons\_w must be equal to 1 and the exhaust gas temperature from the model must be less than the threshold TABGMCSO. With the bit B\_cdlsv = 0 the entire diagnosis function DLSV is switched off.



## Requirements for a properly working diagnosis function:

The described diagnosis and detection of operating readiness of the sensor can only be performed, if a potential-free sensor, a sensor evaluation circuit with reverse voltage source and a two-level Lambda control is used. The function can only be used in combination with the function %HLS.

## Operating readiness:

The internal resistance of the the cold sensor is very high so that the voltage of the sensor evaluation circuit always remains within a given range (independent of the mixture), determined by the reverse-voltage source (USREM < usvk\_w < USREF). With increasing sensor temperature, the internal resistance decreases and the sensor voltage dominates the reverse voltage source. Due to the steep sensor characteristic, the sensor voltage is always different to the reverse voltage, so that the voltage of the evaluation circuit leaves the range USREM < usvk\_w < USREF. The operating readiness of the sensor is not only, like so far, switched on via the sensor parameters. Only once the time TUSEINV has elapsed the operating readiness can be detected, if the following applies permanently for at least the time t = TRSE to the voltage usvk:  
USREF <= usvk\_w <= USMAX or usvk <= USREM. During the time TUSEINV all interferences which cause an early turn-on are suppressed. Furthermore, the faults 'wire-to-wire SC' as well as 'defective sensor with limited voltage amplitude' (B\_nplsv) may not exist in the lower lean turn-on range.

If the time TUSEINV is adjusted towards zero then a too early turn-on is prevented, like so far, by means of the current leak detection, if with a highly restrictive current leak to U\_Bat or to ECU ground the Lambda control is erroneously activated (formation of B\_lsvn see below: "+/- detection current leakage for cold sensor"). Readiness for operation can only be set, if either the sensor voltage is outside of the window USREM < usvk\_w < USREF and there is no current leak or if the sensor has been heated for a sufficient time.

In this second case, operating readiness is only set if the sensor heating has been turned on for the time TTBMH without any interruption.

The operating readiness of the sensor is reset in case of all detected faults of the sensor upstream catalyst. In case of initialization (C\_ini = 1) the operating readiness is generally reset.

## Possible faults:

If the sensor heating has been turned on (B\_hsvs = 1) without any interruption for the time TTBMH, then it can be assumed that, with properly working sensor heating, the sensor has a low impedance (high impedance shunt does not affect sensor signal) and, theoretically, the sensor should therefore be ready for operation.

If the sensor voltage usvk remains within the voltage range USREM < usvk\_w < USREF, the flip-flop B\_uvsvig is set. When leaving this voltage range this flip-flop B\_uvsvig is again reset. The reset is performed after a delay by the time TASIG.

If influence peaks (e.g. clocked heating), which lie outside the voltage range, take place on the sensor voltage in case of wiring interruption (sensor voltage within the range), then they are deactivated by the time TASIG and the flip-flop B\_uvsvig is not reset. If the flip-flop B\_uvsvig remains set for longer than the time TRSAH (sensor voltage within the range), then a wiring interruption or a defective sensor heating is assumed. The fault (B\_silsv) is reported.

In case of an interruption of the common sensor ground (sensor grounds of the individual sensors are, however, connected) an undefined sensor voltage in the plausible voltage range is obtained, so that a Lambda control is no longer possible. This interruption can be detected with warm sensor (the time TTBMH has elapsed) during fuel cut-off (B\_sa = 1) after the time TMASO, if the sensor voltages usvk and ushk exceed the threshold value USMASO. After the interference suppression time TUSKS a flip-flop B\_maso is set and the operating readiness B\_sbbvk is switched off. The fault (B\_silsv1) is set via the trigger B\_dmaso. During the next trip B\_sbbvk remains switched off and E\_lsv is set in the fault management, since the B\_nolsv cannot be reset via B\_maso in the permanent RAM. Only during the next check in the fuel cut-off phase B\_sa the fault "open sensor ground" is either confirmed again or reset in case of healing B\_maso, if the sensor voltages usvk and ushk are less than USMASO for the time TMASO. By resetting B\_maso, B\_nolsv = 1 and thus the E\_lsv is reset. The cycle flag Z\_lsv is only then set again. By means of B\_dmaso it is prevented that the MIL lamp is triggered prior to the check "open sensor ground" during the 2. trip.

If the voltage of the evaluation circuit permanently exceeds the value USMAX for longer than the time TUSKS then there is a short circuit of the sensor signal lead to the supply voltage. The operation readiness B\_sbbvk is reset after the time TUSKS. Once the time TUSMAX has elapsed the fault B\_mx1sv is reported.

If the voltage of the evaluation circuit lies permanently longer than the time TUSFETT between the voltage range USREF <= usvk\_w <= USMAX with defined low-resistance current leak 2...3 kOhm and with active control B\_lr = 1, and if also the sensor voltage ushk downstream of catalyst lies below the threshold USMHK, then with not turned on Euro code bit (Euro version) B\_cd1sh = 1, the flip-flop B\_lsfet is set in the permanent RAM and the operation readiness B\_sbbvk is reset. The fault B\_nplsv is set. Only once the sensor voltage usvk lies outside of the voltage range USREF <= usvk\_w <= USMAX, is the flip-flop B\_lsfet reset and the fault B\_nplsv is cleared via B\_nolsv = 1.

A defective sensor with limited voltage amplitude is indicated (B\_lshup=1) if the evaluation voltage in case of B\_adc1=1 lies within the limits USDBU <= usvk < USDBO for the time TUSDU (without any interruption) and if in addition the sensor voltage downstream of catalyst (ushk\_w) in the rich range lies above the threshold USFHK. The fault B\_nplsv is set in the permanent RAM via the flip-flop B\_lshub and via B\_adde and the operation readiness B\_sbbvk is reset.

In addition the setting of the operation readiness (B\_sbbvk) is prevented in the lower lean turn-on range.

Only once the sensor voltage usvk leaves the window USDBU <= usvk\_w < USDBO, this flip-flop is reset again.

In case of a defective sensor downstream catalyst it is not possible to detect a defective sensor upstream catalyst.

A simultaneously occurring fault of the upstream and downstream sensor is not assumed.



#### Generating a cold bit (B.lsvklt)

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With sufficient cooling down of the exhaust system the sensor is cold, so that in case of start the evaluation voltage is determined by the reverse voltage. Such a start is definitely given, if during the starting procedure the engine temperature lies below the threshold TMSV and if in addition the engine was turned off at a temperature above TMSVA. Additionally no tmot-fault may exist.

If all above-mentioned conditions are fulfilled then the monoflop TNSTDN is triggered with the start bit. The duration of the cold bit is determined with the adjustable time TNSTDN.

On the Euro version there is no sensor downstream catalyst. With the code word CDLSH = 0 (Euro version) the time TUSDU is switched to a marginally greater time TUSDUC, and checking of the threshold USPHK is set to "1" via an OR gate. The time TUSDUC may not be chosen too high, since otherwise the mixture adaptation controller will deviate too much in case of a defective sensor.

With a short circuit between sensor signal and ground or with a defective fuel supply system (e.g. reduced system pressure, leakage), the sensor voltage upstream catalyst (usvk) lies around 0 Volt below the lean threshold USMIN. In order to distinguish these two faults the evaluation is performed by means of 2 flip-flops in the Euro Version.

#### Detection of wire-to-wire SC with OBD II version:

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If the sensor voltage upstream catalyst lies below the lean threshold USMIN and the sensor voltage downstream catalyst does not lie above the threshold USPHK with above-mentioned fault, then a mixture fault is assumed, that means the operating readiness of the sensor is not switched off and the mixture adaptation has a chance to compensate for this fault. If the mixture adaptation controller in the process reaches the limit then, consequently, this fault will be reported by the mixture adaptation.

A wire-to-wire SC between sensor signal and ground lead is detected, if the following applies:

The evaluation voltage for B.adcsd=1, i.e. for active Lambda control (B.lr = 1) and switched off secondary air (B.sls = 0) and secondary air diagnosis (B.dsls = 0 or B.esls), as well as the "not set" error flags of the secondary air pump (E.slpe = 0; E.slp = 0), and the "not set" error flags of the canister purge control (E.tes = 0; E.teve = 0), lies below the limits of the threshold USMIN without interruption, while at the same time the sensor voltage downstream catalyst (ushk) remains in the rich area above the threshold USPHK for the time TUSDU. Via a flip-flop B.lsad in the permanent RAM and via B.adde the operating readiness upstream catalyst (B.sbbvk) is reset and in the lower lean turn-on band the setting of the operating readiness is prevented. The fault B.nplsv is set.

A wire-to-wire SC is also immediately detected, if during start with cold sensor (B.lsvklt = 1), the sensor voltage lies below the threshold USMIN. The flip-flop B.lsad in the permanent RAM is set and once the time TTBMH has elapsed the fault B.plaus is indicated. Only once the sensor voltage usvk lies above the threshold USPVR, this flip-flop is reset.

Thus an additional information on whether a mixture fault or a wire-to-wire SC is present can be obtained during the start with cold sensor.

#### Detection of wire-to-wire SC with Europe version:

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On the Europe version the sensor downstream catalyst is not installed. With the code word CDLSH = 0 (Euro version) a switch from the time TUSDU to the marginally greater time TUSDUC is performed and the inquiry on the threshold USPHK is set to the value = 1 by means of an OR-gate.

A wire-to-wire SC during start with cold sensor (B.lsvklt = 1) is immediately detected, if the sensor voltage lies below the threshold USMIN.

In the process the sensor operating readiness is blocked via the flip-flop (B.lsad=1) and B.adde and the fault B.plaus is set once the time TTBMH has elapsed.

If the sensor voltage lies below the threshold USMIN for longer than the time TUSDUC without interruption, with active Lambda control (B.lr = 1) and switched off secondary air (B.sls = 0) and secondary air diagnosis (B.dsls = 0; B.esls), as well as with the "not set" error flags of the secondary air pump (E.slpe = 0; E.slp = 0) and the "not set" error flags of the canister purge control (E.tes = 0; E.teve = 0), then the flip-flop B.adsvb=1 is set in the permanent RAM, the operating readiness upstream catalyst (B.sbbvk) is reset via B.vadge and the setting of the operating readiness is prevented in the lower lean turn-on band. Simultaneously the flip-flop B.vgef1r=1 is set in the permanent RAM.

At first the operating readiness is only blocked on suspicion and no fault is indicated, since it is not yet known whether there is a wire-to-wire SC or a mixture fault.

However, if during the next cold start (B.lsvklt=1) the sensor voltage of the cold sensor does not lie below USMIN, but at the reverse voltage 450 mV, then a mixture fault is assumed. The flip-flop's B.adsvb und B.lsad remains set, if ushk,w not exceeds the threshold USPVR. the flip-flop in the permanent RAM with B.vgef1r remains set. The event counter zwgef1r is incremented by 1, by a delay of one operating step once the cold bit B.lsvklt=1 has elapsed. Thereafter the flip-flop B.vgef1r is reset after the delay of one operating step.

The given mixture fault is incremented by 1 after each cold start and the quantity is compared to ANZGEM. Once the quantity of measured mixture faults is reached, B.vadge=0 and thus the operating readiness B.sbbvk of the sensor is no longer reset.

For the mixture adaptation control %LRA it is now possible to correct the mixture fault. This mixture fault can then possibly be indicated via %DKVS.

For the healing (B.vgef1r is not set) the event counter is each time incremented by 1, if during cold start B.lsvklt=1 there is no mixture fault.

#### Early detection of current leakage with a cold sensor

-----

A high impedance current leakage must be detected in order to:

- prevent a premature turn-on of the Lambda control (formation of B.lsvn)
- provide maximum heating current after start without interruption for high impedance current leakage.

A detected current leakage is stored in a permanent RAM, buffered with a flip-flop (current leakage => B.lsvn = 1).

It is set, if with a cold sensor (B.lsvklt=1), the voltage is outside the band USREF <= usvk.w <= USREM longer than for the debouncing time TUSKS. It is reset accordingly at a following cold start if the voltage is again within the window.

Operating readiness of the upstream sensor is only released if either no current leakage has been detected, or the sensor heating has been turned on for longer than TTBMH without interruption. In the second case, high impedance current leakage does not affect the sensor voltage.

The current leakage detection can be switched off during the emission test if the engine temperature threshold TMNEB is chosen > 50°C.

Thereafter only the turn-on delay TUSEINV has an effect, i.e. if the sensor voltage lies outside of the window USREF <=usvk <=USREM during this time, then no turn-on of the operating readiness takes place.

If TMNEB is chosen < 20°C then the current leakage detection is fully effective during the emission test, i.e. with detected current leakage the operation readiness B.sbbvk is turned on only once the time TTBMH has elapsed.



**Fault healed:**

-----  
If the sensor heating is permanently on for longer than the time TTBMH and if the operation readiness B\_sbbvk is set, then, most likely, there is no fault.

**Fault management:**

-----  
From the three fault types the fault flag and the cycle flag is created. The cycle flag, however, is also set after each no-fault resp. healing-trigger and it is reset after each ECU initialization C\_ini. If an error is detected as having been healed (B\_nolsv = 1), then the fault flag is reset. By the fault management logic the CARB lamp is only triggered if after 2 trips the cycle flag and the fault flag are each set.

**APP DLSV 32.60 Application hint**

Guidance values:

- TUSKS : 100 ms
- TNSTDN : 1 s
- TRSE : 200 ms
- TRSA : 5 s
- TUSDU : 10 s
- TUSFETT: 10 s
- TASIG : 60 ms
- DRISIGV: 20000 Ohm
- RISIGRESV: 1000 Ohm
- TUSDUC : 20 s
- TMASO : 3 s
- TUSMAX : 5 s
- USFHK : 500 mV
- USMHK : 100 mV
- TTBMH : 90 s
- TMSPV : 40 °C
- TMSPVA : 60 °C
- TABGMCSO: 800 °C
- TABGMSVU: 600 °C
- PHLSNVMN: 0.8
- ANZGEM : 4
- UBDLS : 11 V
- USMASO : 200 mV (if all grounds of sensors seperately go to ECU, then is this function not required and USMASO can be dated with 1.2V).

TUSEINV : less than the turn-on time of the operation readiness by a factor of 0.7 if USREF or USREM are exceeded resp. undershot (5 ..20s).  
 TMNEB : --> > 50 °C: Current leakage detection is switched off. During the time TUSEINV a current leakage is suppressed. (Use on the planar sensor LSF4.7)  
 --> < 20 °C: Current leakage detection is fully effective during the emission test, i.e. in case of a detected current leakage, the operation readiness is turned on only after the time TTBMH.

The voltage band is briefly summarized in the following diagram.

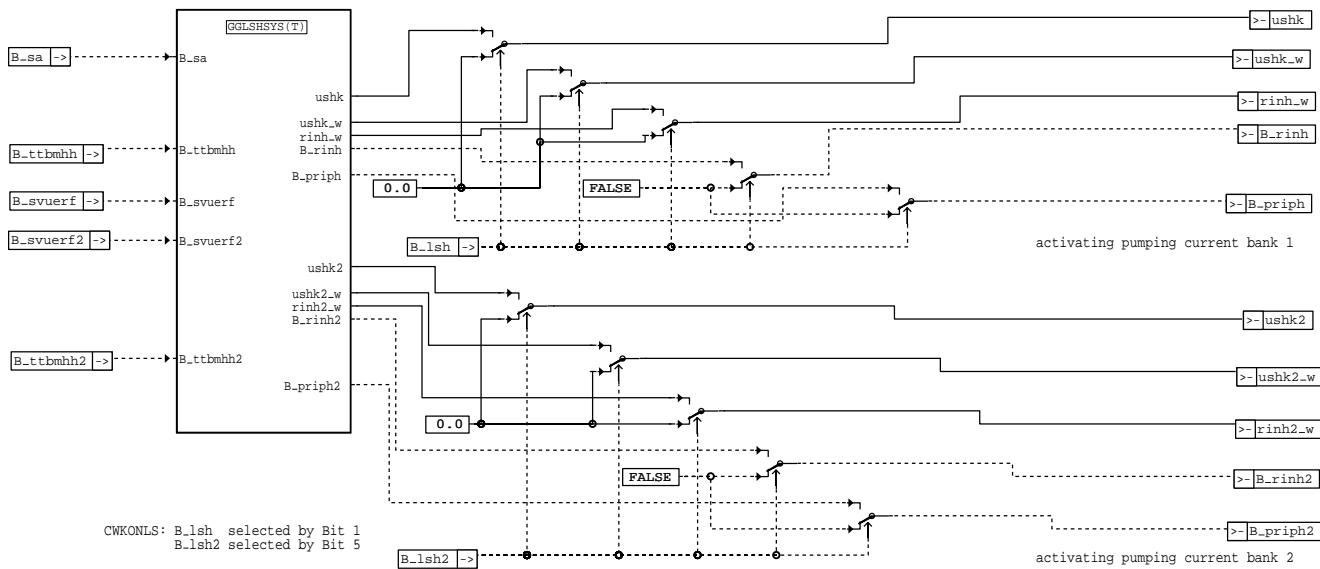
Practical numerical values are indicated

usvk_w	^	U_ADC	U_Sonde
USMAX	SC to U_Bat	= 1.50 V	1.50 V
	+-----+   Defined low impedance current leakage   to UBatt +-----+		
USREF	Operating readiness after t > TRSE(=200ms) sensor cold / signal interruption	= 0.600 V	0.600 V
USR	----- Control threshold / Sensor heating defective after t > TRSA(=5s)	= 0.450 V	0.450 V
USREM	Operating readiness after t > TRSE, if no wire-to-wire SC or SC of sensor ground to ECU ground	= 0.400 V	0.400 V
USDBO	+-----+   Defective sensor with restricted signal   amplitude +-----+	= 0.400 V	0,400 V
USDBU	+-----+	= 0.060 V	0.060 V
USMASO	+-----+   Interruption of the common sensor ground +-----+	= 0.200 V	0.200 V
USMIN	+-----+   Wire-to-wire SC +-----+	= 0.060 V	0.060 V

## GGLSH 3.30 Sensor variable for lambda sensor downstream of catalytic converter

### FDEF GGLSH 3.30 Function definition

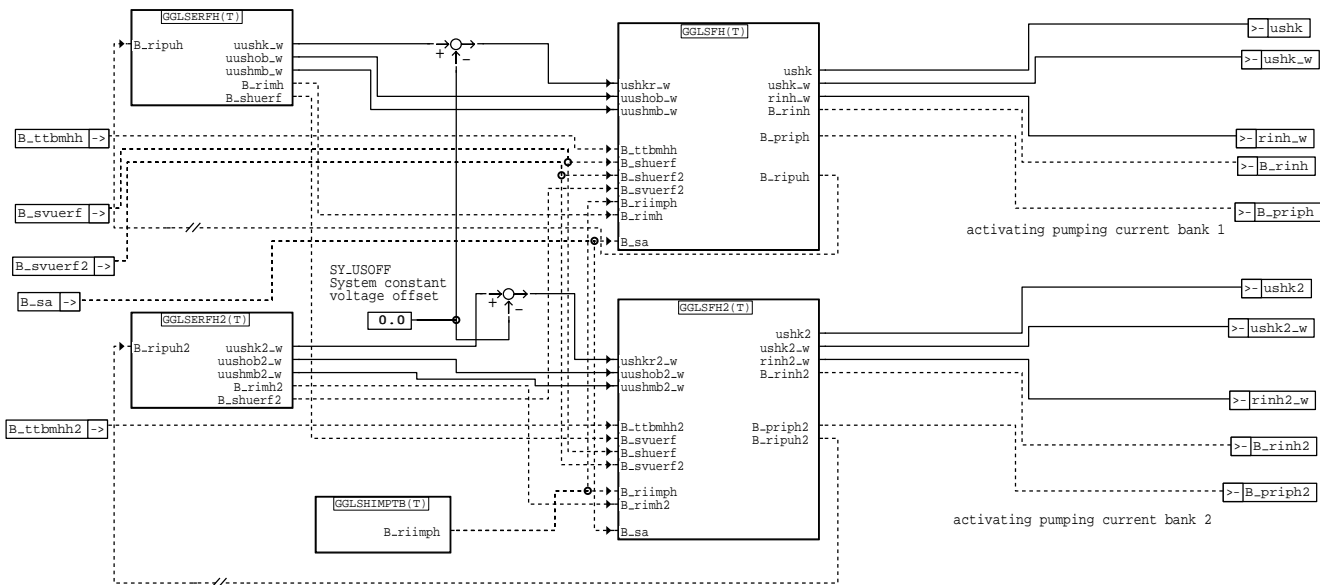
GGLSH: Analysis of configuration bit



gglsh-gglsh

### gglsh-gglsh

GGLSHSYS: Overview and description sensor voltage detection, bank1 and bank2

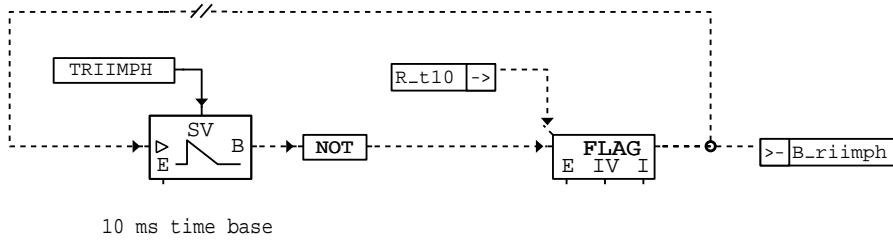


gglsh-gglshsys

### gglsh-gglshsys

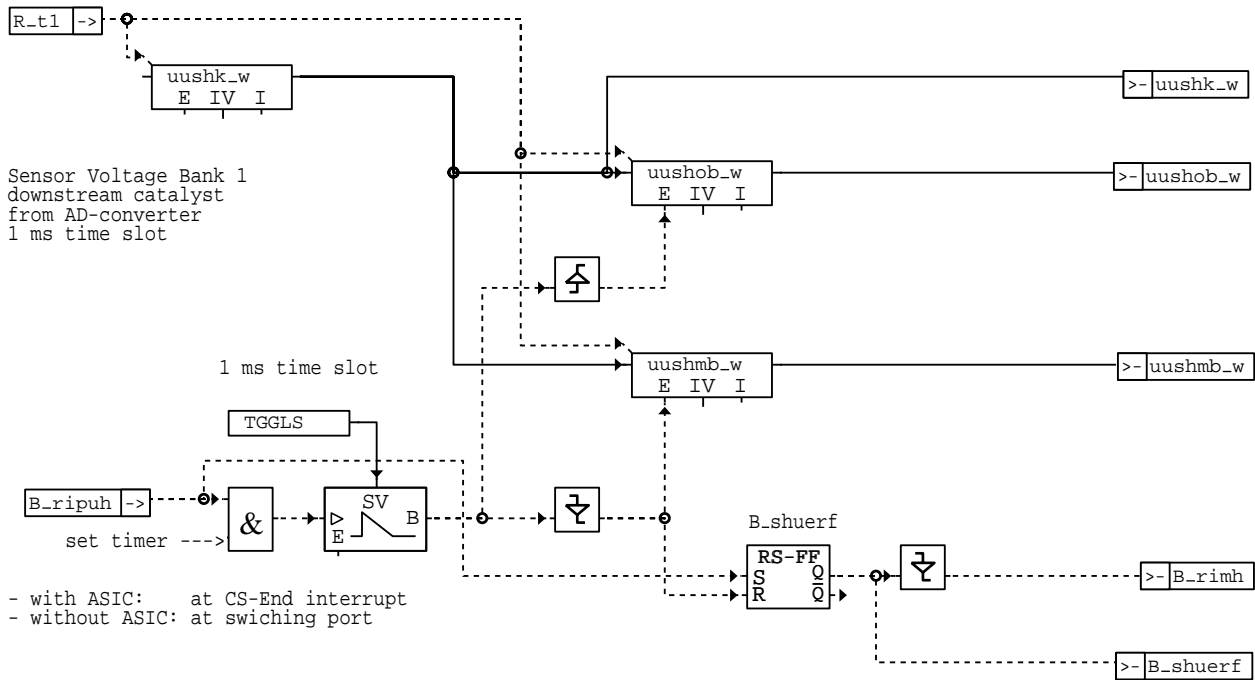


GGLSHIMPTP: Generating pumping time intervals for bank1 and bank2



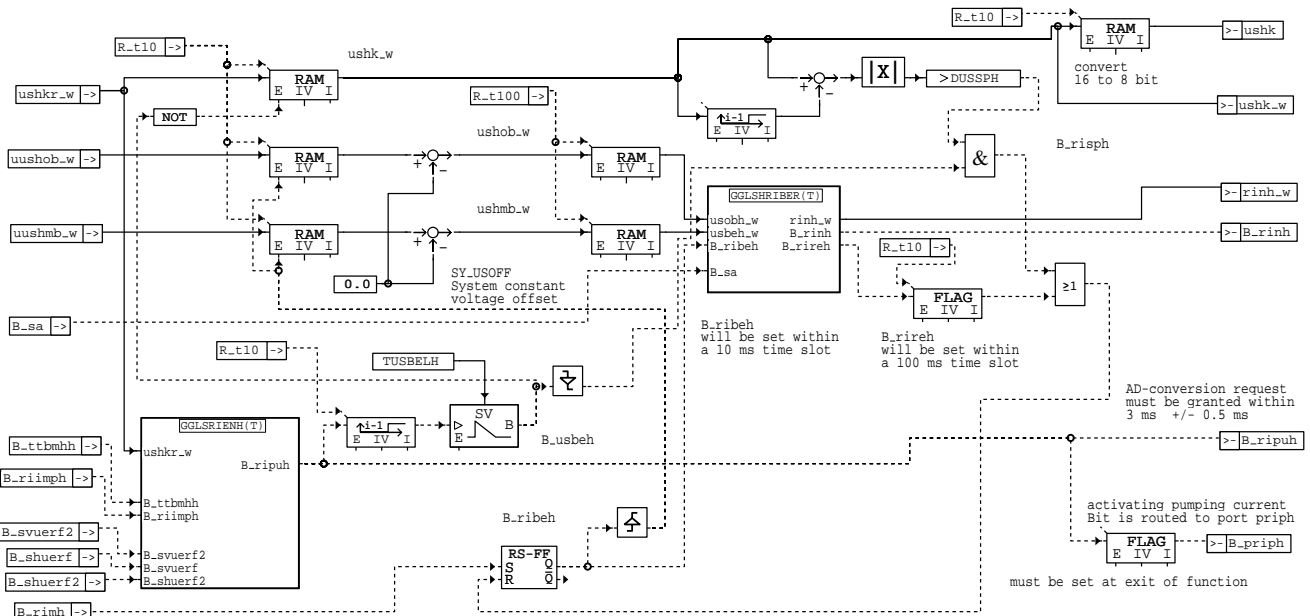
gglsh-gglshimptb

GGLSERFH: Measuring the sensor voltage in the 1 ms cycle with and without load, bank1



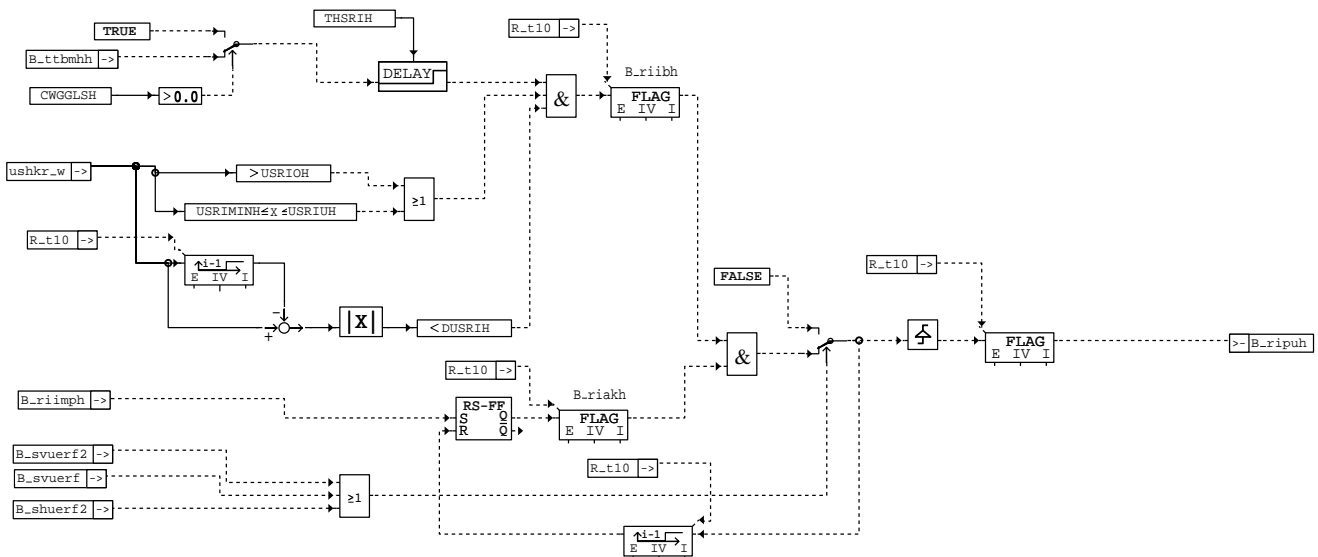
gglsh-gglserfh

GGLSFH: Transfer of the measured values without load after pumping into 100 ms cycle, bank 1



### gglsh-gglshf

GGLSRIENH: Enabling of Ri-measurement, bank 1

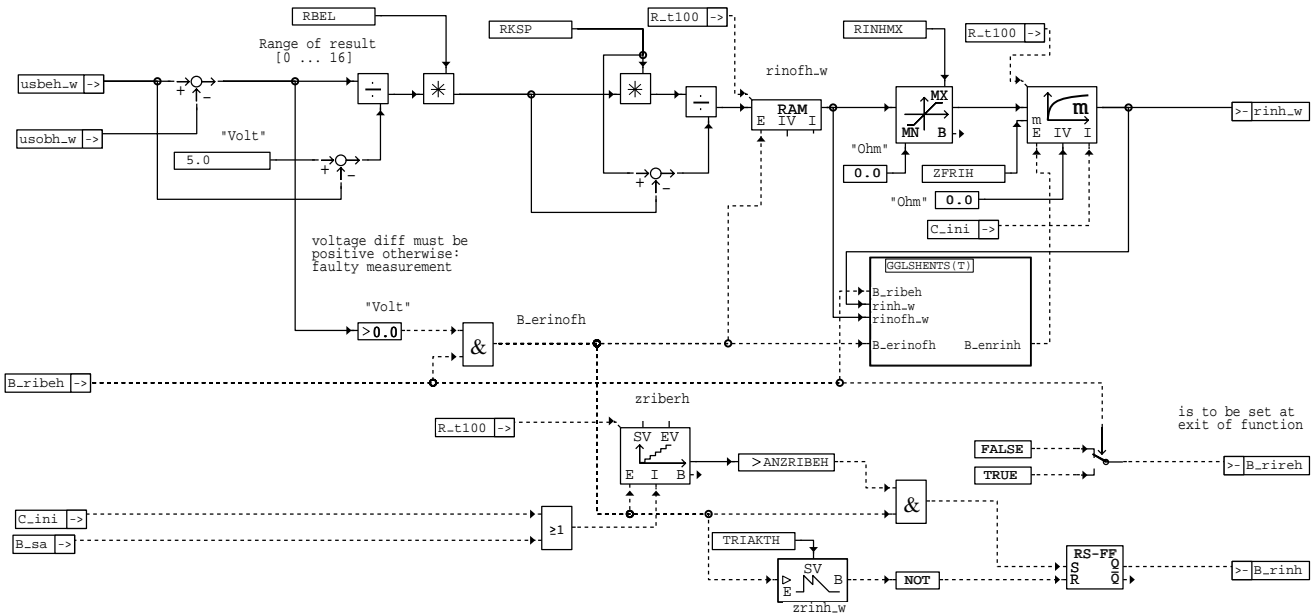


### gglsh-gglshrieh



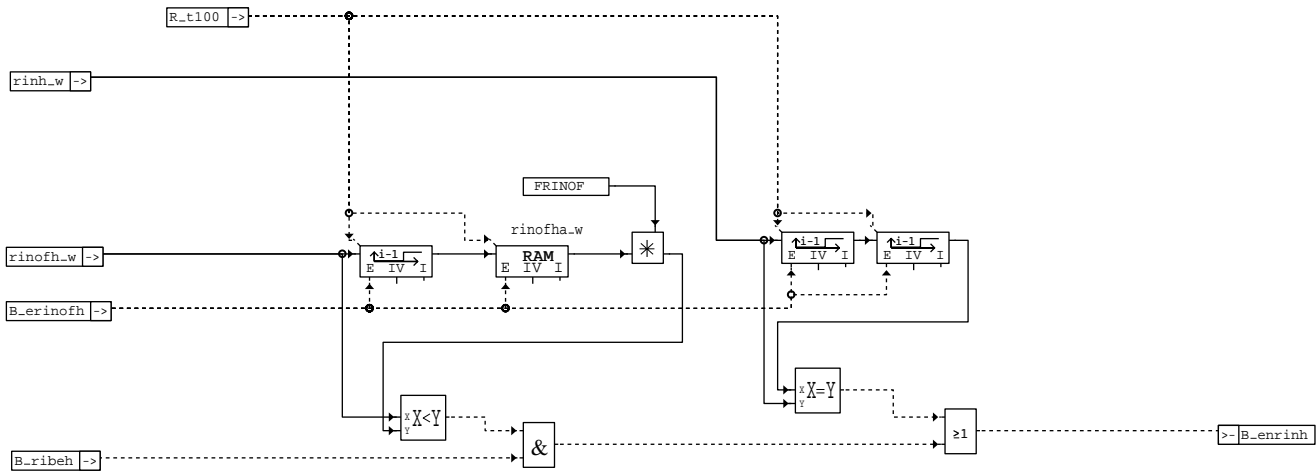


GGLSHRIBER: Calculation of Ri and statistical evaluation, bank 1



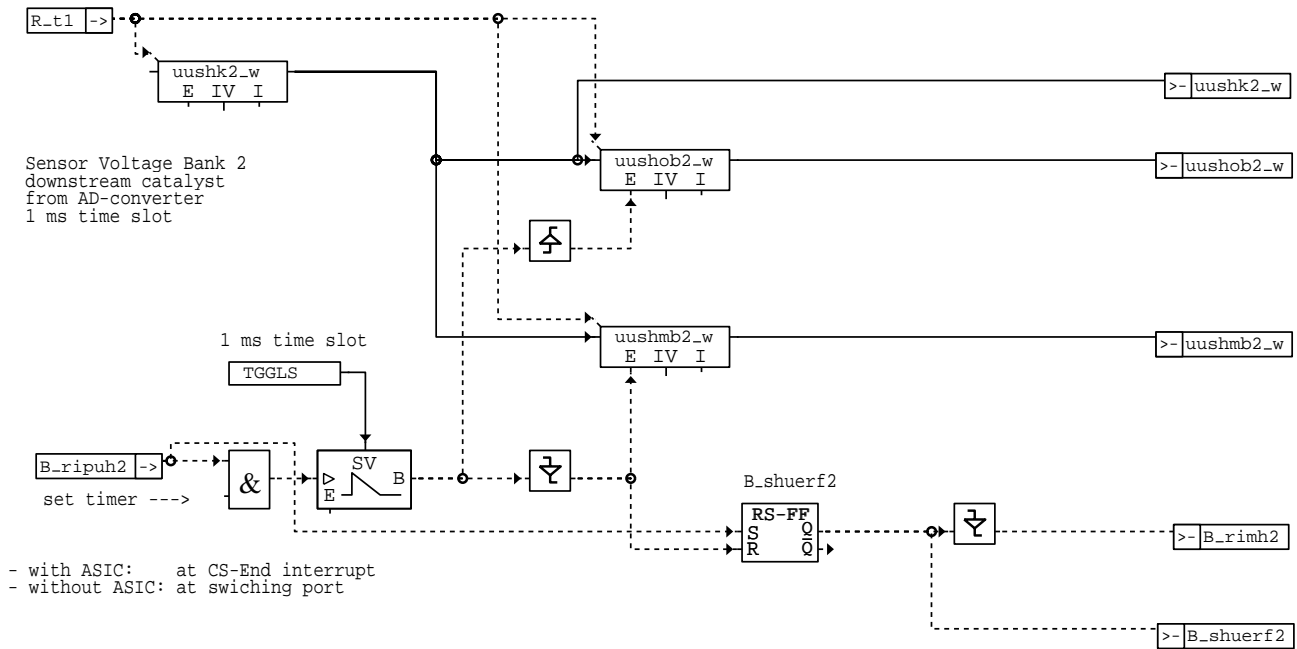
gglsh-gglshriber

GGLSHENTS: Additional interference suppression of Ri-measurement and formation of enable for the Ri-filter, bank1



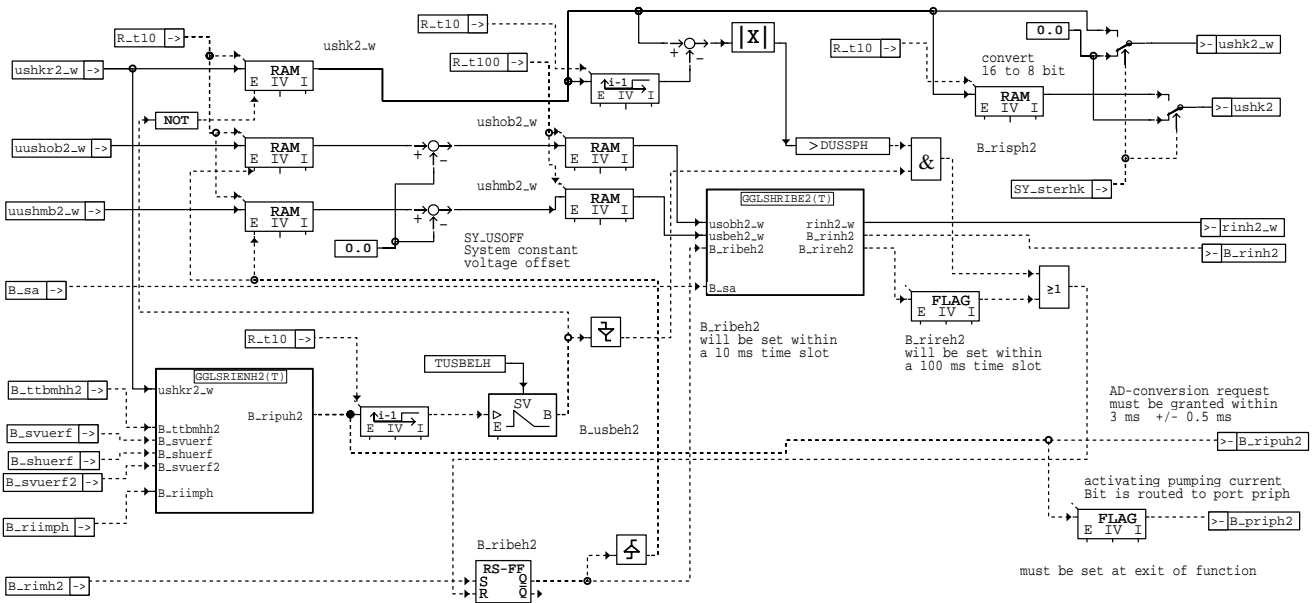
gglsh-gglshents

GGLSERFH2: : Measuring the sensor voltage in the 1 ms cycle with and without load, bank2



**gglsh-gglserfh2**

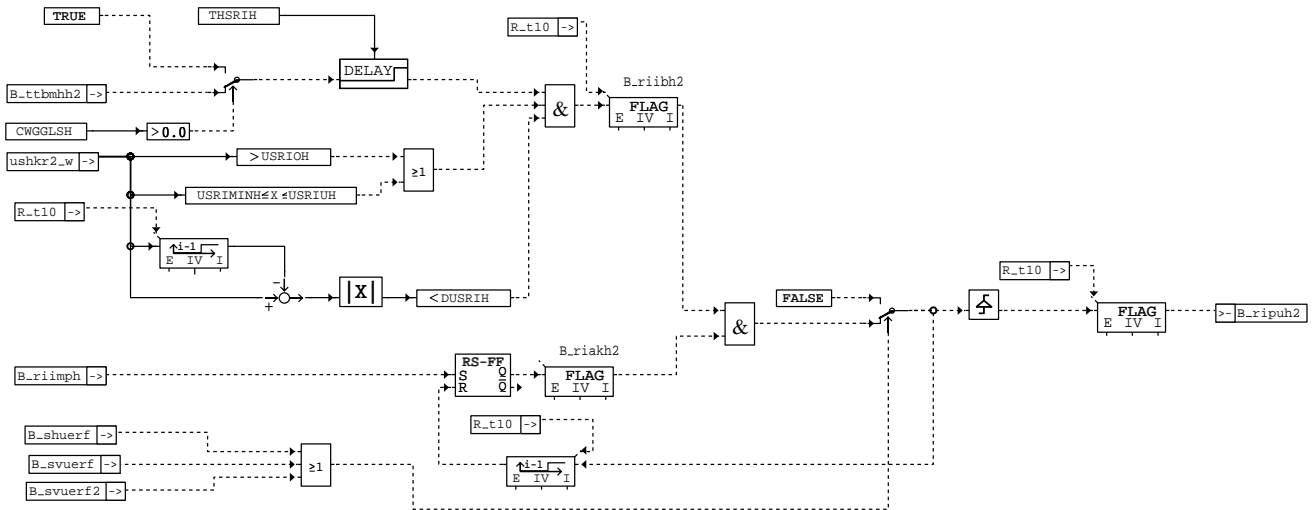
GGLSFH2: Transfer of the measured values without load after pumping into 100 ms cycle, bank 2



**gglsh-gglsfh2**

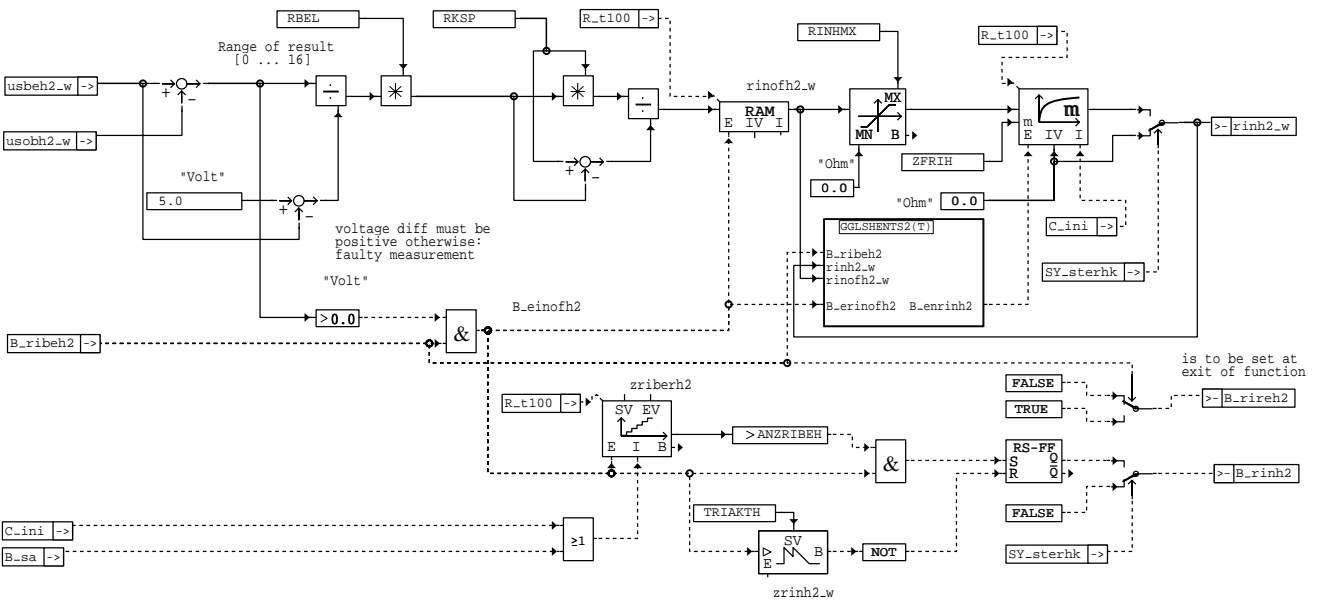


GGLSRIENH2: Enabling of Ri-measurement, bank 2



gglish-gglsrieh2

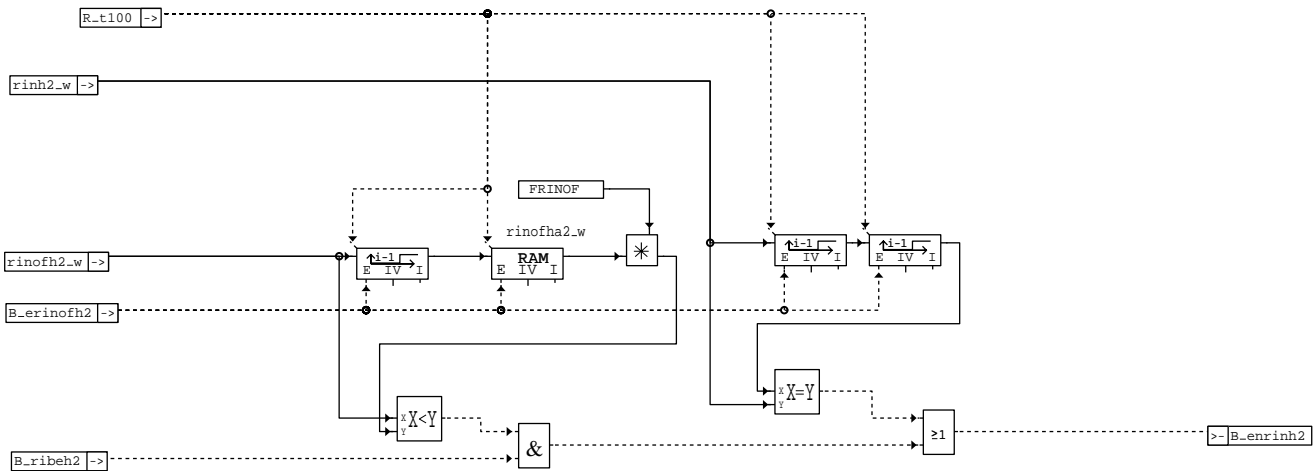
GGLSHRIBE2: Calculation of Ri and statistical evaluation, bank 2



gglish-gglsrhibe2



GGLSHENTS2: Additional interference suppression of Ri-measurement and formation of enable for the Ri-filter, bank2



gglsh-gglshents2

### ABK GGLSH 3.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ANZRIBEH			FW	Number of Ri.calculations downstream catalyst
CWGGLSH			FW	code word for Ri-evaluation for sensor downstr. of cat (not full heating)
DUSRIH			FW	Delta sensor volt. downstream cat betw. new and old value in grid for Ri-measur.
DUSSPH			FW	Delta sensor volt. rear cat between new and 2 old val. for sensor jump knowledge
FRINOF			FW	Factor for validation of old Ri-value without filter
RBEL			FW	On-load resistance for pump current generation
RINHMX			FW	Limit internal resistance Ri of the Nernst sensor downstream cat to max. value
RKSP			FW	Resistance between congruent voltage and sensor signal
TGGLS			FW	Time needed for ADC after interrupt in the function calculator (Asic)
THSRIH			FW	Time del. readiness of Ri-measure. after switched on sensor heat. downstream cat
TRIAKTH			FW	Time needed for Ri-calculation up to date downstream catalyst
TRIIMPH			FW	Time needed for pump impulse for both banks downstream catalyst
TUSBELH			FW	Time for holding of the sensor voltage after on-load impulse downstream catalyst
USRIMINH			FW	Minimum voltage threshold for Ri-measurement of the sensor downstream catalyst
USRIOH			FW	Upper voltage threshold for Ri-measurement of the sensor downstream catalyst
USRIUH			FW	Lower voltage threshold for Ri-measurement of the sensor downstream catalyst
ZFRIH			FW	Attenuation factor for the internal resistance Ri Nernst filter downstream cat

Variable	Source	Type	Description
B_ENRINH	GGLSH	LOK	Condition enable for Ri-Nernst with filter post cat
B_ENRINH2	GGLSH	LOK	Condition enable for Ri-Nernst with filter post cat bank 2
B_ERINOFH	GGLSH	LOK	Condition enable for Ri-Nernst without filter post cat
B_ERINOFH2	GGLSH	LOK	Condition enable for Ri-Nernst without filter post cat bank 2
B_LSH	PROKON	EIN	Cond. lambda sensor inst. downstr. of cat., 2. sensor downst. of outlet (Bank1)
B_LSH2	PROKON	EIN	Cond. lambda sensor inst. downstr. of cat., 2. sensor downst. of outlet (Bank2)
B_PRIIPH	GGLSH	AUS	Condition switch port for pump impulse downstream catalyst
B_PRIIPH2	GGLSH	AUS	Condition switch port for pump impulse downstream catalyst bank2
B_RIBEH	GGLSH	LOK	Condition calculate internal resistance Ri for sensor downstream catalyst
B_RIBEH2	GGLSH	LOK	Condition calculate internal resistance Ri for sensor downstream cat. bank2
B_RIIMPH	GGLSH	LOK	Condition impuls for pumping current downstream catalyst
B_RIMH	GGLSH	LOK	Cond. (adc-trigger) for measuring of loaded sensor voltage downstream catalyst
B_RIMH2	GGLSH	LOK	Cond. (adc-trigger) for measuring of loaded sensor voltage downstream cat. bank2
B_RINH	GGLSH	AUS	Condition internal resistance of Ri-measur. of sensor active downstream cat.
B_RINH2	GGLSH	AUS	Condition internal resist. of Ri-meas. sensor active downstream cat. bank2
B_RIPUH	GGLSH	LOK	Condition pumping current for sensor downstream catalyst
B_RIPUH2	GGLSH	LOK	Condition pumping current for sensor downstream catalyst bank2
B_RIREH	GGLSH	LOK	Condition result for internal resistance Ri for sensor downstream catalyst
B_RIREH2	GGLSH	LOK	Condition result for internal resistance Ri for sensor downstream catalyst bank2
B_SA	MDRED	EIN	Condition fuel cut-off
B_SHUERF	GGLSH	LOK	Condition sensor voltage post cat measured
B_SHUERF2	GGLSH	LOK	Condition sensor voltage post cat measured bank 2
B_SVUERF		EIN	Condition sensor voltage pre cat measured
B_SVUERF2		EIN	Condition sensor voltage pre cat measured bank 2
B_TTBMH	DLSH	EIN	cond. theoretical lambda sensor operation readiness downstr. cat with heating
B_TTBMH2	DLSH	EIN	cond. theoretical lambda sens. operat. readiness downstr. cat with heating bank2
C_JNI	SWADAP	EIN	ECU-condition for intialisation
RINH2_W		AUS	Act. value (word) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH_W	GGLSH	AUS	Actual value (word) internal res. Ri-Nernst cell lambda sensor downstream cat
RINOFH2_W	GGLSH	LOK	Internal resistance (word) Ri Nernst without filtering downstream cat bank2
RINOFH_W	GGLSH	LOK	Internal resistance (word) Ri Nernst without filtering downstream catalyst
R_T1		EIN	Time schedule 1 ms
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms



Variable	Source	Type	Description
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
USBEH2_W	GGLSH	LOK	Voltage (word) lambda sensor loaded with resistance downstream catalyst bank2
USBEH_W	GGLSH	LOK	Voltage (word) lambda sensor loaded with resistance downstream catalyst
USHK	GGLSH	AUS	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	AUS	output voltage oxygen sensor downstream catalyst 2
USHK2_W	GGLSH	AUS	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst 2
USHKR2_W	GGLSH	LOK	Voltage (word) lambda sensor raw value downstream catalyst bank2
USHKR_W	GGLSH	LOK	Voltage (word) lambda sensor raw value downstream catalyst bank2
USHK_W	GGLSH	AUS	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst
USOBH2_W	GGLSH	LOK	Voltage (word) lambda sensor without load downstream catalyst bank2
USOBH_W	GGLSH	LOK	Voltage (word) lambda sensor without load downstream catalyst
UUSHK2_W	GGLSH	LOK	ADC-voltage lambda sensor downstream catalyst bank2 (word)
UUSHK_W	GGLSH	LOK	ADC-voltage lambda sensor downstream catalyst (word)
UUSHMB2_W	GGLSH	LOK	Voltage (word, 1 ms-time slot) sensor with resistor loaded, downstream cat bank2
UUSHMB_W	GGLSH	LOK	Voltage (word, 1 ms-time slot) O2-sensor with resistor loaded, downstream cat
UUSHOB2_W	GGLSH	LOK	ADC voltage (word, 1 ms-time slot) O2-sensor unloaded downstream cat bank2
UUSHOB_W	GGLSH	LOK	ADC voltage (word, 1 ms-time slot) O2-sensor unloaded downstream cat

### FW GGLSH 3.30 Fixed Values

Parameter	Value	Description
ANZRIBEH		Number of Ri.calculations downstream catalyst
CWGGLSH		code word for Ri-evaluation for sensor downstr. of cat (not full heating)
DUSRIH		Delta sensor volt. downstream cat betw. new and old value in grid for Ri-measur.
DUSSPH		Delta sensor volt. rear cat between new and 2 old val. for sensor jump knowledge
FRINOF		Factor for validation of old Ri-value without filter
RBEL		On-load resistance for pump current generation
RINHMX		Limit internal resistance Ri of the Nernst sensor downstream cat to max. value
RKSP		Resistance between congruent voltage and sensor signal
TGGLS		Time needed for ADC after interrupt in the function calculator (Asic)
THSRIH		Time del. readiness of Ri-measure. after switched on sensor heat. downstream cat
TRIAKTH		Time needed for Ri-calculation up to date downstream catalyst
TRIIMPH		Time needed for pump impulse for both banks downstream catalyst
TUSBELH		Time for holding of the sensor voltage after on-load impulse downstream catalyst
USRIMINH		Minimum voltage threshold for Ri-measurement of the sensor downstream catalyst
USRIOH		Upper voltage threshold for Ri-measurement of the sensor downstream catalyst
USRIUH		Lower voltage threshold for Ri-measurement of the sensor downstream catalyst
ZFRIH		Attenuation factor for the internal resistance Ri Nernst filter downstream cat



## FB GGLSH 3.30 Detailed description of function

### 1. Introduction:

The sensor function GGLSH is used to detect and quantize the sensor voltage downstream catalyst, and to generate a pump current while at the same time the internal resistance  $R_i$  of the Nernst sensor is determined.

The LSF8 sensor is not equipped with a reference air volume and therefore, it requires a constant pump current which transports oxygen towards the reference electrode. In the present sensor function, the sensor voltage is periodically pulsed by means of a pump current (0.5 mA for 10 ms) so that the sensors LSF8 sensor is fully compatible to the sensors LSH and LSF4. Thus the sensor diagnosis' do not need to be changed. The sensors LSH and LSF4 have an air reference and actually do not need a pump current. However, if a pulsed pump current is used on these sensors, the internal resistance  $R_i$  can be determined. By the internal resistance an indirect check is performed in the heater diagnosis DHL5 on whether the sensor heater is o.k. In case of defect sensor heating or strongly reduced heating performance at low exhaust gas temperatures the internal resistance increases markedly.

### 2. Enable sensor function by configuration bit (GGLSH):

The sensor function can be enabled by means of the code word CWKONLS, provided the corresponding bits for the sensor installed upstream of the catalyst have been set. Bank1 can be enabled by means of bit 1 if  $B_{_lsh} = 1$ ; Bank2 is enabled via bit 5 if  $B_{_lsh2} = 1$  (sum = 34).

### 3. Generation of pump pulse (current impulse) GGLSRIENH:

An instable multi-vibrator with the output  $B_{_riimph}$  is used to generate a pump impulse. The multi-vibrator supplies an impulse with the duration of 10 ms after an adjustable timer TRIIMPH has passed. This impulse  $B_{_riimph}$  sets the flip-flop  $B_{_riakh}$ , i.e. the pumping current is updated. One timer only is used for both banks.

A pumping current with the condition  $B_{_ripuh} = 1$  can be performed if the sensor voltage lies within the permitted permissible voltage ranges ( $B_{_riibh} = 1$ ) and if the condition  $B_{_ttbmhh} = 1$  from %DLSV was continuously active for a time longer than THSRIH. The condition  $B_{_ttbmhh}$  from %DLSH can be disabled by the codeword CWGGLSH in order that  $R_i$  can be measured for application purpose even before end of dewpoint (refer to Application Note).

A permitted voltage range for permissible pumping current exists if the sensor voltage  $usvkr_w$

"- is greater than USRIOH in the rich range"

"- lies between USRIMNH and USRIUH in the lean range"

"- the gradient of the sensor voltage (difference between new value and old value (i-1) in the 10 ms cycle) is less than the " threshold value DUSRIH

After the pumping current was enabled  $B_{_ripuh} = 1$  the flip-flop  $B_{_riakh}$  is reset in the next 10 ms grid (i-1) so that the period for pumping current is exactly 10 ms.

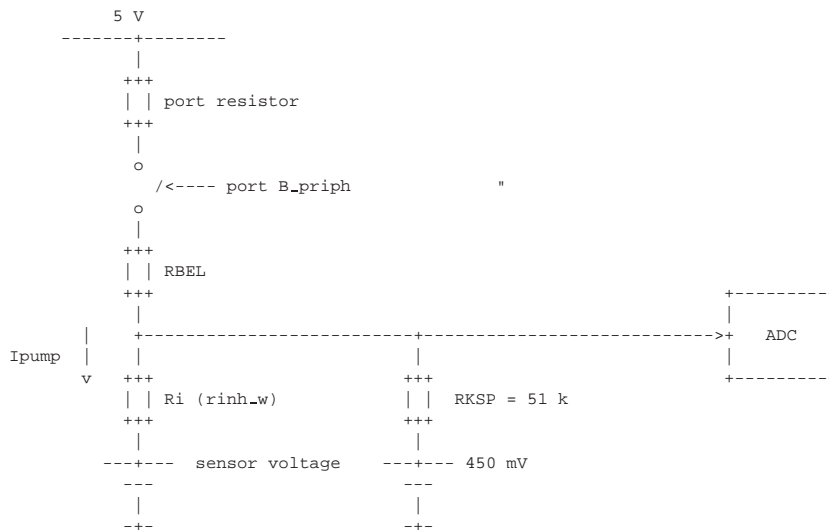
To maintain a correct current balance for the sensor LSF8, a timer TRIIMPH ( $B_{_riimph} = 1$ , i.e. pump impulse is necessary) has passed and if at the same time sensor voltages occur in the not permitted voltage range ( $USRIUH < ushkr_w < USRIOH$ ) the triggering of the pump impulse is at first forbidden and stored as information in the flip-flop  $B_{_riakh}$ . Only once the non permitted voltage range is left immediately afterwards  $B_{_ripuh} = 1$  is set in the permitted voltage range and by doing so the pump impulse is triggered.

There must be a definite relationship between unloaded and loaded sensor voltage for a sensor in the 10 ms grid. This requirement is met by only one sensor being allowed to be pumped in the 10 ms grid.

$B_{_ripuh}$  cannot be used to pump current if the sensor voltage at bank2 upstream of catalyst, or the voltages downstream of catalyst are momentarily being detected by  $B_{_shuerf2}$ , or  $B_{_svuerf}$  and  $B_{_svuerf2}$  respectively.

Via  $B_{_ripuh}$  a port is switched with the bit  $B_{_priph} = 1$  so that a pump current of 0,5 mA can flow for 10 ms from the 5V voltage supply and through a fixed defined resistor RBEL.

### Hardware:





#### 4. Transfer of the sensor voltage measured values (with and without load) into the 100 ms cycle for the Calculation of Ri

It is important for the calculation of the internal resistance Ri of the sensor that the sensor voltages with load and without load are read within one 10 ms cycle. This can be achieved if prior to the on-load impulse the unloaded sensor voltage uushk\_w is read via the ADC and if during the on-load impulse (10 ms) after approx. 3 ms the loaded sensor voltage uushb\_w is read via the ADC.

After the pump impulse was triggered B\_ripuh = 1 the sensor voltage ushkr\_w is held at the old value via a timer TUSBELH during the following 10 ms grid (i-1) so that the increased loaded sensor voltage cannot have an effect.

##### 4.1 Measuring the loaded and unloaded sensor voltage in the 1 ms time frame (GGLSERFH):

The ADC value of the sensor voltage is sampled in the 1 ms-time frame and is stored as the word uushk\_w in the RAM. If a permissible pump impulse B\_ripuh follows, then the unloaded voltage uuvob\_w is stored by setting the timer TGGLS with a positive edge. After elapse of the time TGGLS, the loaded sensor voltage uuvob\_w is stored is then retained in the 1 ms time frame with the negative edge. Setting the pump impulse B\_ripuh will also set the Flip-Flop B\_shuerf in the 1 ms frame, i.e. for the sensor upstream of the catalyst at bank1, the requirement is set that only the the sensor voltage will be measured here. TGGLS is reset following elapse of the timer by the negative edge of this detection Flip-Flop B\_shuerf. It must be ensured that the order of the bank calculation is observed (first bank1 and then bank2).

##### 4.2 Transfer of loaded and unloaded sensor voltage from the 1 ms time frame in 10 ms and 100 ms time frames (GGLSFH):

The condition B\_rimh is set by resetting the Flip-Flop B\_shuerf with the negative edge. The Flip-Flop B\_ribeh is set by B\_rimh for transfer to the 10 ms and 100 ms time frames. The unloaded sensor voltage uushob\_w and the loaded sensor voltage uushmb\_w are transferred into a RAM in the 10 ms time frame with the positive edge of this Flip-Flop. The increase from sensor grounding, SY\_USOFF, that is specific to the control unit, is subtracted from the unloaded sensor voltage uushob\_w or loaded sensor voltage uushmb\_w and then receives the unloaded sensor voltage ushob\_w and the loaded sensor voltage ushmb\_w in the 10 ms time. These are then transferred in the 100 ms time frame to the RAM, usobh\_w and usbeh\_w respectively. The increase in the sensor grounding, SY\_USOFF, that is specific to the control unit is then also subtracted in the 1 ms-time frame from the ADC voltage and stored in the 10 ms-time frame as the raw value in the RAM ushkr\_w (word). This 16 bit sensor voltage ushkr\_w is converted to the 8 bit format (ushk) for additional use in sensor diagnostics and lamda control.

##### Ri-calculation (rinofh\_w)

The internal resistance Ri' of the sensor is calculated from:

$$Ri' = \frac{usbeh\_w - usobh\_w}{5V - usbeh\_w} * RBEL$$

Corrected by the counter-resistance RKSP in the hardware Ri results:

$$Ri = \frac{Ri' * RKSP}{RKSP - Ri'} = rinofh\_w$$

This Ri value is given in the 100 ms-time frame by setting the Flip-Flop B\_ribeh = 1 and is limited to RINHMx.

The following measures are performed in order to prevent the loaded sensor voltage from being used during a jump of the sensor voltage in the 10 ms-impulse:

- If, especially during the rich-to-lean jump, the difference between the sensor voltage usbeh\_w (with load) and the sensor voltage usobh\_w (without load) is less than zero, then the B\_erinofh is not set and Ri is not computed.
- If, especially during the lean-to-rich jump, the absolute value of the difference between old and new sensor voltage exceeds DUSSPH after the timer TUSBELH has elapsed in the 10 ms cycle, then the flop-flop B\_ribeh is reset prematurely; this causes Ri not to be calculated.

Thereafter rinofh\_w is filtered through an event filter with the attenuation factor ZFRIH so that the filtered internal resistance rinh\_w of the sensor is obtained. -----> Event filter :  $y[k] = y[k-1] + ZFRIH(x[k] + y[k-1])$

After the calculation of the internal resistance a flag is set in the 10 ms grid via B\_rireh = 1 (Ri-calculation terminated) and the flip-flop B\_ribeh is reset.

##### 4.3 Additional interference suppression of Ri measurements and formation of enable for the Ri filter (GGLSHENTS):

In the new unfiltered new value of Ri (rinofh\_w) is greater by a factor FRINOF than the old Ri value rioffh\_w, then B\_enrinh is not set and hence the calculated value is transferred to the filter. In order than an increase in the internal resistance Ri is possible during sensor cooling (new Ri value is greater than the old value vby the factor FRINOF), the transfer of rinofh\_w to the filter is enabled by B\_enrinh = 1 after measuring 2 Ri values.

The Ri-calculations B\_ribeh are added-up by means of a counter zrriberh. If the number of Ri-calculations is greater than ANZRIBEH then a flip-flop B\_rinh is set, which indicates to the heater diagnosis the state that the calculation of the internal resistance is active and up to date. ANZRIBEH = 3/ZFRIH is chosen.

As soon as the counter starts a retriggerable timer zrinh\_w is triggered, whose timer time is chosen at TRIAKTH = 4\*TRIMPH. Once the timer has passed zrinh\_w = 0 the flip-flop B\_rinh is reset (resistance value rinh\_w is not updated). If within the period TRIAKTV again current Ri-calculations are performed (B\_ribeh = 1), then this timer zrinh\_w is continuously started again so that the condition B\_rinh is currently active.



Course of the ADC-sequence:



## APP GGLSH 3.30 Application hint

SY\_USOFF

The fixed value voltage difference between sensor ground and electronic ground can adjustable with a system constant SY\_USOFF and it must be adjusted ECU-specific by the software.

Example: If the voltage between sensor ground and electronic ground is 0.268V the SY\_USOFF must be adjusted to 0.268V.

Corresponding to the hardware design SY\_USOFF becomes 0V; 0,268V or 0,714V.

Typical application values:

THSRIH = 10 s  
TUSBELH = 60 ms  
TRIIMPH = 2 s  
TRIAKTHH = 4\*TRIMPH = 8 s  
ZFRIH = 0.3  
ANZRIBEH = 3/ZFRIH = 10  
RBEL = 8.45 KOhm  
RKSP = 51 KOhm  
RINHMX = 100 KOhm  
USRIOH = 490 mV  
USRIOH = 410 mV  
USRIMIN = 60 mV  
DUSRIOH = 25 mV  
UBDLS > 11 V  
DUSSPH = 200 mV  
TGGLS = 3 ms  
FRINOF = 1.5

CWGGLSH = 0 -----> Code word = 0 : Ri is only calculated after end of dewpoint for full heating power (series)  
= 1 : Ri can be measured as high-resistance for application during the phase of dewpoint

CWKONLS : -----> Code word in % PROKON : Sensors present upstream of the catalyst ---> Bank1: B\_lsv by Bit 0 = 1  
Bank2: B\_lsv2 by Bit 4 = 16  
(gives 17 as the sum)

Sensors present downstream of the catalyst --> Bank1: B\_lsh by bit 1 = 2  
Bank2: B\_lsh2 by bit 5 = 32  
(gives 34 as the sum)

For all 4 installed seensors: CWKONLS = 51

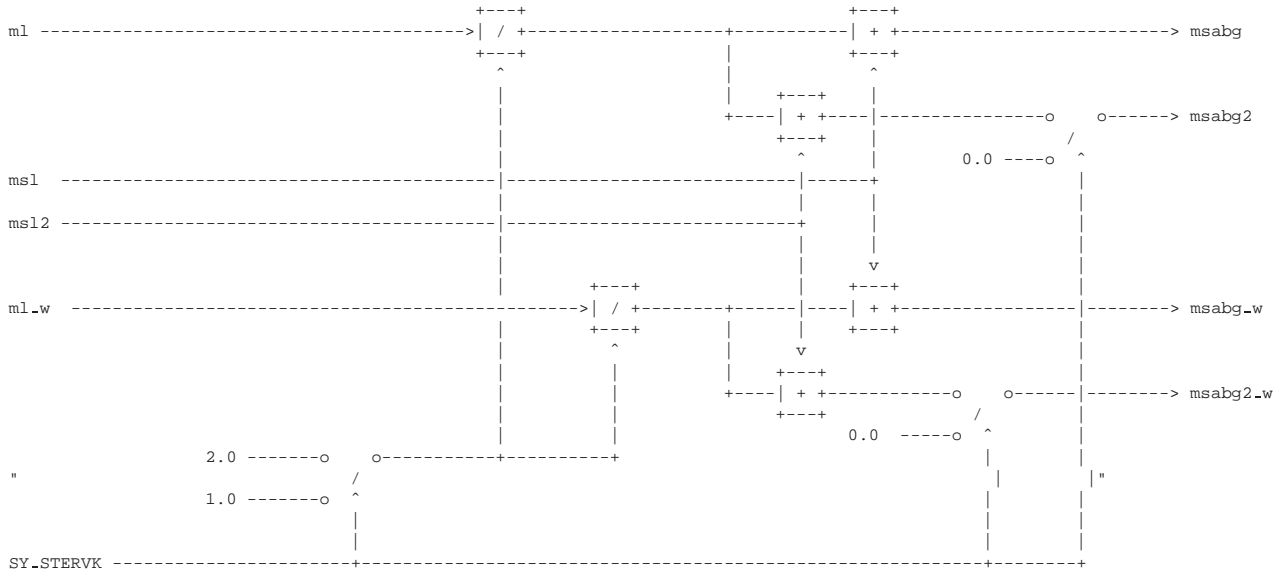
## BGMSABG 2.10 Calculation of exhaust emission mass flow - bank-dependent

### FDEF BGMSABG 2.10 Function definition

Provision for exhaust emission flow quantity:

In the basic version, the air mass ml is distributed throughout the active exhaust emission banks.





### ABK BGMSABG 2.10 Abbreviations

Variable	Source	Type	Description
ML	SWADAP	EIN	air mass flow
MLBB	BGMSABG	AUS	air mass flow filtered (Byte), bank1 related
MLBB2	BGMSABG	AUS	air mass flow filtered (Byte), bank2 related
MLBB2_W	BGMSABG	AUS	air mass flow filtered (Word), bank2 related
MLBB_W	BGMSABG	AUS	air mass flow filtered (Word), Bank1 related
ML_W	EGFE	EIN	air mass flow filtered (Word)
MSABG	BGMSABG	AUS	exhaust gas mass flow filtered, bank 1
MSABG2	BGMSABG	AUS	exhaust gas mass flow filtered, bank 2
MSABG2_W	BGMSABG	AUS	exhaust gas mass flow filtered (Word), bank 2
MSABG_W	BGMSABG	AUS	exhaust gas mass flow filtered (Word), bank 1
MSL	EIN	EIN	secondary air mass flow
MSL2	EIN	EIN	secondary air mass, bank 2

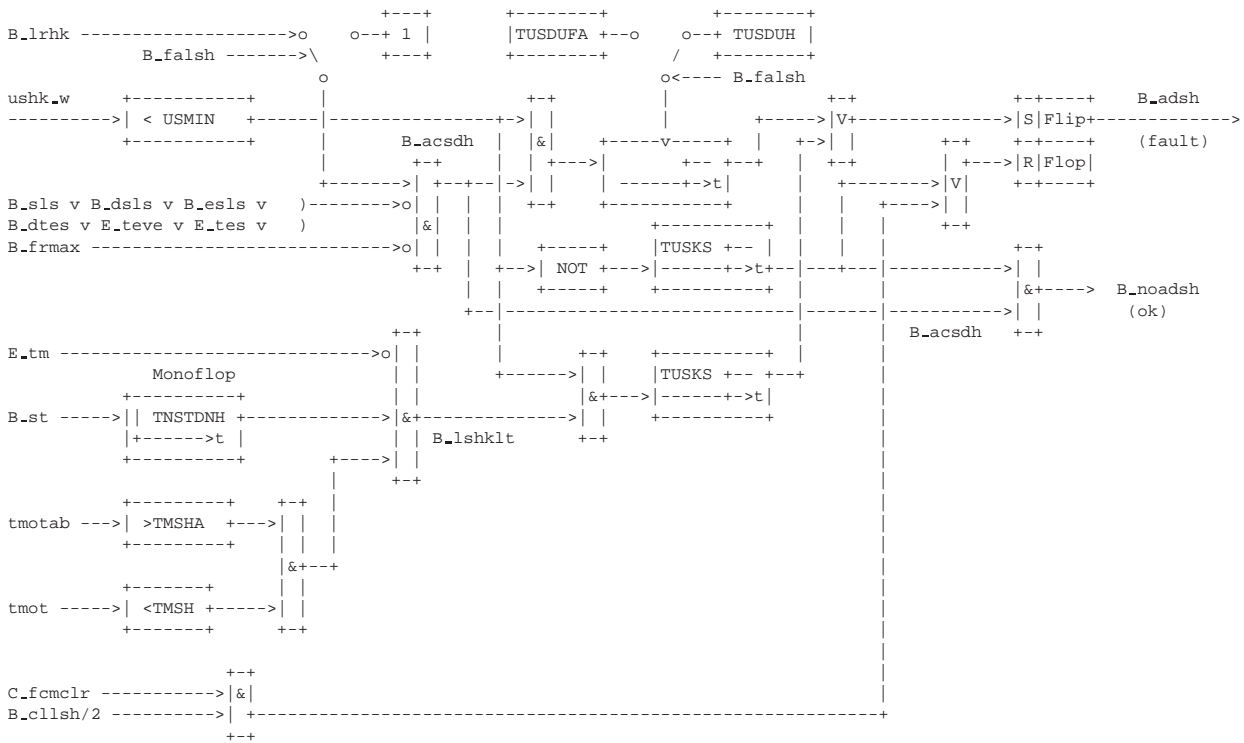
### FW BGMSABG 2.10 Fixed Values

Parameter	Value	Description



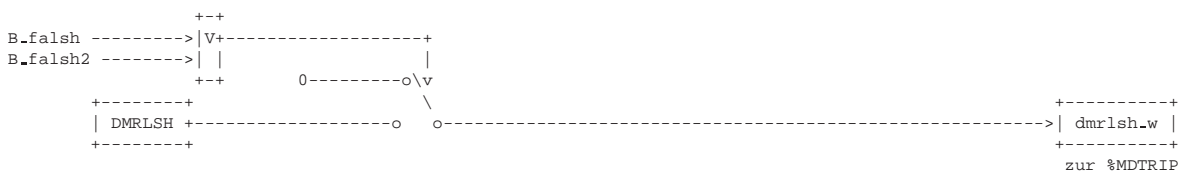


Detection wire-to-wire)

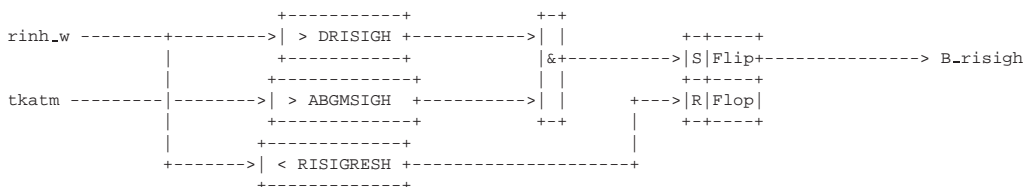


With STEREO-control additionally the following labels apply for bank2: ushk2; B\_lrhk2; B\_sbbhk2; Z\_lsh2; E\_lsh2; B\_dshen2; B\_usrhk2; B\_ueinh2; B\_adsh2; B\_adshs2; B\_acsdh2; lamsons2.w; tkatm2; B\_uhsig2; B\_trsah2; B\_falsh2, lamelsh2.w; rinh2.w; B\_atmpk2; B\_hshe2; B\_framax2; B\_noadsh2

Moment-reserve for shorttest



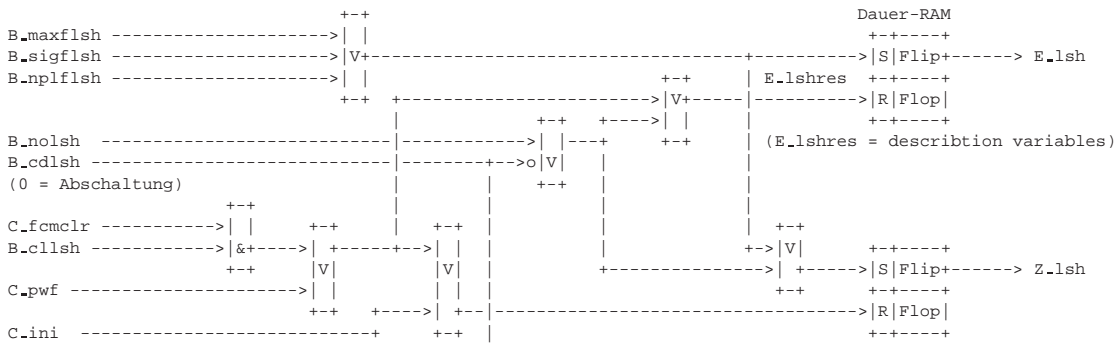
Wire-interruption of sensor ground ( planar sensor)



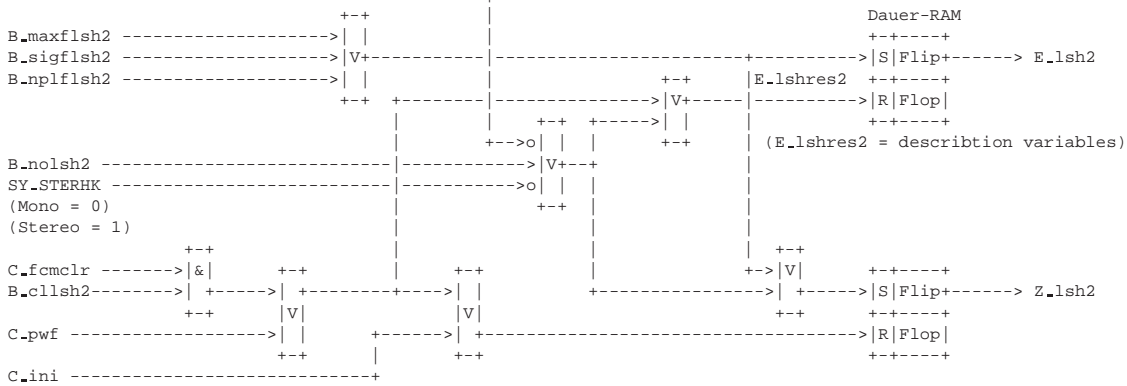


Fault management for DLSH:

(Bank1)



(Bank2)







Parameter	Source-X	Source-Y	Type	Description
RISIGRESH			FW	threshold for reset wiring-interruption with Ri-diagnosis downstr. cat
TABGMCS			FW	threshold for exhaust temperature for measuring CSD
TASIG			FW	Time for the deactiv.of interf. peaks outside of range for det.of signal interr.
TMSH			FW	engine temp. threshold for recognition cold start for measur. sensor downstream
TMSHA			FW	threshold for engine switch-off temp. for measur. cooling sensor downstream cat
TNSTDNH			FW	time after start for diagnosis wire-to-wire (monoflop)
TRSAFA			FW	monitoring time closed-loop control (downstream CAT) funct. requ. for Short trip
TRSAH			FW	monitoring time closed-loop control (downstream CAT) -> sensor off
TRSE			FW	monitoring time -> closed-loop control on
TSFLSH			FW	fault active time: lambda sensor catalyst downstream
TSFLSH2			FW	fault active time: lambda sensor catalyst downstream, bank 2
TTBMH			FW	period for theoretical operation readiness of sensor with heating
TUSDUFA			FW	time delay for detec. interc. short circuit sens. downstr.(func. rec.short-trip)
TUSDUH			FW	time delay for detection intercore short circuit l. sensor downstr. cat.
TUSEINH			FW	Delay time for turn-on of readiness for operation by sensor downstream of cat.
TUSKS			FW	delay time for short circuit detection on the oxygen sensor
TUSMAX			FW	monitoring time for Usmax
TUSTAL			FW	Delay for detection'wire to wire connection' after 'empty fuel tank for O2 po.ct
UBDLS			FW	battery voltage threshold for release the sensor diagnosis
USMAX			FW	threshold for short circuit of sensor to Ubat
USMIN			FW	threshold for short circuit of sensor to ground
USREFH			FW	threshold for operation readiness of sensor downstream CAT at rich mixture
USREMH			FW	threshold for operation readiness of sensor downstream CAT at lean mixture

Variable	Source	Type	Description
B_ACS	DLSH	LOK	condition for test of short-circuit and CSD catalyst downstream
B_ACS	DLSH	LOK	condition for test of short-circuit and CSD catalyst downstream bank 2
B_ADS	DLSH	LOK	condition for short-circuit downstream sensor
B_ADS	DLSH	LOK	condition for short-circuit for downstream sensor bank 2
B_ADS	DLSH	LOK	condition for short-circuit "set" downstream sensor
B_ADS	DLSH	LOK	condition for short-circuit "set" downstream sensor bank 2
B_ATM	ATM	EIN	condition temperature downstream catalyst exceeds dew-point
B_ATM	ATM	EIN	condition temperature downstream catalyst exceeds dew-point2
B_CDLS	PROKON	EIN	function active per codeword CDLSH
B_CLLS		EIN	Clear fault path in DLSH
B_CLLS		EIN	Clear fault path in DLSH, bank 2
B_DSHEN	DLSH	LOK	condition enable sensor diagnosis downstream catalyst
B_DSHEN	DLSH	LOK	condition enable sensor diagnosis downstream catalyst bank2
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DTES	GKRA	EIN	Condition for active diagnosis of canister purge system
B_ESLS		EIN	Condition secondary air fault by wrong air mass flow
B_FA		EIN	condition general function request
B_FALSH		EIN	condition function request downstream oxygen sensor diagnosis
B_FALSH		EIN	condition function request downstream oxygen sensor diagnosis bank2
B_FRMAX	LR	EIN	lambda control sets bit when lambda controller reaches its limit FRMAX
B_FRMAX	LR	EIN	lambda control sets bit when lambda control reaches it limit FRMAX, bank2
B_HSHE	HLS	EIN	condition for lambda sensor heating-switch downstream cat on
B_HSHE	HLS	EIN	condition for lambda sensor2 heating-switch downstream cat on
B_LRHK	LRHK	EIN	condition for lambda closed loop control downstream cat
B_LRHK	LRHK	EIN	condition for lambda closed loop control downstream cat (bank 2)
B_LSHKL	DLSH	LOK	condition cold oxygen sensor downstream catalyst
B_MAXFLSH	DLSH	LOK	Short-circuit to UBatt on sensor downstream catalyst detected
B_MAXFLSH	DLSH	LOK	Short-circuit to UBatt on sensor downstream catalyst detected, bank 2
B_MXLSH	DLSH	AUS	Condition for fault type "maximum value" downstream cat detected
B_MXLSH	DLSH	AUS	Condition for fault type "maximum value" downstream cat detected bank2
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_NOADSH	DLSH	LOK	condition for no short-circuit downstream sensor
B_NOADSH	DLSH	LOK	condition for no short-circuit downstream sensor bank2
B_NOLSH	DLSH	AUS	Condition diagnosis finished with o.k. downstream cat report
B_NOLSH	DLSH	AUS	Condition diagnosis finished with o.k. downstream cat report bank2
B_NPLFLSH	DLSH	LOK	Wire-to-wire SC on sensor downstream catalyst detected
B_NPLFLSH	DLSH	AUS	Wire-to-wire SC on sensor downstream catalyst detected bank 2
B_RISIGH	DLSH	LOK	Condition signal disconnection of sensor ground with Ri-diagnosis, post cat
B_RISIGH	DLSH	LOK	Condition signal disconnection of sensor ground with Ri-diagnosis post cat Bank2
B_SBBHK	DLSH	AUS	condition for lambda sensor downstream cat ready for operation
B_SBBHK	DLSH	AUS	condition for lambda sensor downstream cat ready for operation bank2
B_SIGFLSH	DLSH	LOK	Signal interruption (wiring interruption) on sensor downstream catalyst detectet
B_SIGFLSH	DLSH	LOK	Signal interruption (wiring interruption) on sensor downstr.cat.detectet bank 2
B_SILSH	DLSH	AUS	condition for fault type 'signal missing' downstream cat detected
B_SILSH	DLSH	AUS	condition for fault type 'signal missing' downstream cat detected bank2
B_SLS	AK	EIN	Condition for active secondary air
B_ST	SWADAP	EIN	condition for start
B_STERHK		EIN	condition Stereo Lambda control behind catalyst
B_TAL	GGFST	EIN	Condition tank empty or reserve
B_TALVAL	GGFST	EIN	condition ; bit empty tank valid
B_TRSAH	DLSH	LOK	Condition wiring interruption for sensor downstream catalyst
B_TRSAH	DLSH	LOK	Condition wiring interruption for sensor downstream catalyst, bank 2
B_TTBMH	DLSH	AUS	cond. theoretical lambda sensor operation readiness downstr. cat with heating
B_TTBMH	DLSH	AUS	cond. theoretical lambda sens. operat. readiness downstr. cat with heating bank2
B_JEINH	DLSH	LOK	Cond.: Prepar. to turn on the sensor readiness for operation downstream of cat.
B_JEINH	DLSH	LOK	Cond.: Prepar. to turn on the sensor readiness for operat. downstr. of cat.Bank2



Variable	Source	Type	Description
B_UHSIG	DLSH	LOK	Con.sensor voltage downstr.cat.in the voltage range for signal interrupt.
B_UHSIG2	DLSH	LOK	Con.sensor voltage downstr.cat.in the voltage range for signal interrupt., bank2
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DMRLSH_W	DLSH	AUS	torque reserve for lambda sensor diagnosis downstream cat
E_LSH	DLSH	AUS	error flag: lambda sensor downstream cat
E_LSH2	DLSH	AUS	Errorflag: Lambda-Sensor downstream bank2
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
LAMELSH2_W	DLSH	AUS	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMELSH_W	DLSH	AUS	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMSONS2_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
RINH2_W	GGLSH	EIN	Act. value (word) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH_W	GGLSH	EIN	Actual value (word) internal res. Ri-Nernst cell lambda sensor downstream cat
SFPLSH	DLSH	AUS	status fault path:
SFPLSH2	DLSH	AUS	status fault path:
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TMOT	SWADAP	EIN	Engine temperature
TMOTAB	GGTFM	EIN	engine coolant temperature at engine stop or cut-off cranking
TYP_LSH	DLSH	AUS	Fault type: lambda sensor 1 downstream
TYP_LSH2	DLSH	AUS	Fault type: lambda sensor 2 downstream
UB	SWADAP	EIN	battery voltage
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
Z_LSH	DLSH	AUS	cycle-flag: lambda sensor downstream cat
Z_LSH2	DLSH	AUS	cycle-Flag: Lambda-sensor downstream cat bank2

Abbreviations and terminology

CSD 'chemical shift down' lowered sensor characteristic line due to poisoning  
 ECU,SG Electronic Control Unit  
 SC,KS Short-circuit

Abbreviations for cross coupling matrix:

Partial function sensor operating readiness - outputs: SB=sensor operating readiness  
 - inputs: S/SB=block/sensor operating readiness  
 Partial function sensor diagnosis - outputs: SD=sensor diagnosis  
 - inputs: S/SD=block/sensor diagnosis  
 B/SD=condition/sensor diagnosis  
 F/SD=flip-flop/sensor diagnosis

**FW DLSH 26.50 Fixed Values**

Parameter	Value	Description
ABGMSIGH		threshold for exh. temp. for wiring-interruption with Ri-diagnosis downstr. cat
CDTLSH		code word tester: lambda sensor downstream catalyst [012]
CDTLSH2		code word tester: lambda sensor 2 downstream catalyst, cyl.row 2 [020]
CLALSH		fault class: O2 sensor downstream catalyst
CLALSH2		fault class: O2 sensor downstream catalyst bank 2
DLAMELSH		Delta Lamda setpoint for electrical sensor diagnosis downstr. catal. (quicktrip)
DMRLSH		torque reserve for diagnosis lambdasensor downstream cat
DRISIGH		diagnosis threshold for Ri sensor for signal disconnection post cat
RISIGRESH		threshold for reset wiring-interruption with Ri-diagnosis downstr. cat
TABGMCSD		threshold for exhaust temperature for measuring CSD
TASIG		Time for the deactiv.of interf. peaks outside of range for det.of signal interr.
TMSH		engine temp. threshold for recognition cold start for measur. sensor downstream
TMSHA		threshold for engine switch-off temp. for measur. cooling sensor downstream cat
TNSTDNH		time after start for diagnosis wire-to-wire (monoflop)
TRSAFA		monitoring time closed-loop control (downstream CAT) funct. requ. for Short trip
TRSAH		monitoring time closed-loop control (downstream CAT) -> sensor off
TRSE		monitoring time -> closed-loop control on
TSFLSH		fault active time: lambda sensor catalyst downstream
TSFLSH2		fault active time: lambda sensor catalyst downstream, bank 2
TTBMH		period for theoretical operation readiness of sensor with heating
TUSDUFA		time delay for detec. interc. short circuit sens. downstr.(func. rec.short-trip)
TUSDUH		time delay for detection intercore short circuit l. sensor downstr. cat.
TUSEINH		Delay time for turn-on of readiness for operation by sensor downstream of cat.
TUSKS		delay time for short circuit detection on the oxygen sensor
TUSMAX		monitoring time for Usmax
TUSTAL		Delay for detection'wire to wire connection' after 'empty fuel tank for O2 po.ct
UBDLS		battery voltage threshold for release the sensor diagnosis
USMAX		threshold for short circuit of sensor to Ubat



Parameter	Value	Description
USMIN		threshold for short circuit of sensor to ground
USREFH		threshold for operation readiness of sensor downstream CAT at rich mixture
USREMH		threshold for operation readiness of sensor downstream CAT at lean mixture





## FB DLSH 26.50 Detailed description of function

### Introduction:

The diagnostic function must detect all electrical connection faults of the lambda sensor. Output signals are the fault bit E\_lsh, the cycle bit Z\_lsh and the bit for sensor operation readiness B\_sbbhk.

The fault types, B\_maxflsh (KS\_UBat), B\_sigflsh (wiring interruption, sensor heating defective), B\_nplflsh (wire-to-wire SC) and a signal for fault healing (B\_nolsh) are passed to the fault management logic. These fault types are stored in a flip-flop in the permanent RAM and they are transferred to the fault memory as B\_mxflsh (SC-UBat), B\_silsh (wiring interruption); B\_nplsh (wire-to-wire SC).

Generally, a transfer to the fault management can only take place (B\_dshen = 1) if the dew point end downstream catalyst B\_atmtpk = 1 is exceeded and thus the sensor heating is switched on with B\_hshe = 1 and if a sensor-specific time TUSEINH has elapsed and hence was permanently switched on for at least the time TTBMH (that means especially not dutycycled). At the same time the battery voltage ub may not lie above the threshold UBDSL, lamsons\_w must be equal to 1 and the exhaust gas temperature from the model must be less than the threshold TABGMCS and B\_nmot mußt be equal to 1 (nmot < NMIN).

With the bit B\_cdlsh = 0 the entire diagnostic function %DLSH is switched off. With the bit SY\_STERHK = 0 a switch-over from Stereo to Mono can be performed.

### Preconditions for the diagnostic function

The diagnosis and the detection of sensor readiness for operation can only be carried out in this form, if a potential-free sensor and a sensor evaluation circuit with a reverse voltage source are used. The function can only be used in conjunction with the function %HLS.

### Operation readiness:

The internal resistance of the cold sensor is very high so that the voltage of the sensor evaluation circuit always remains within a given range (independent of the mixture), determined by the reverse-voltage source (USREMH < ushk < USREFH). With increasing sensor temperature, the internal resistance decreases and the sensor voltage dominates the reverse voltage source. Due to the steep sensor characteristic, the sensor voltage is always different to the reverse voltage, so that the voltage of the evaluation circuit leaves the range USREMH < ushk < USREFH. The operating readiness of the sensor is not only, like so far, switched on via the sensor parameters. Only once the time TUSEINH has elapsed the operating readiness can be detected, if the following applies permanently for at least the time t = TRSE to the voltage ushk:

USREFH <= ushk <= USMAX or ushk <= USREMH. During the time TUSEINH all interferences which cause an early turn-on are suppressed. Furthermore, the fault 'wire-to-wire SC' (B\_nplsh) may not exist in the lower turn-on range.

If the sensor heating has been turned on without any interruption for at least the time TTBMH (B\_ueinh=1), then it can be assumed that, with properly working sensor heating, the sensor has a low impedance (high impedance shunt does not affect sensor signal) and, theoretically, the sensor should therefore be ready for operation. If the sensor voltage then is still within the voltage range USREMH < ushk < USREFH without interruption for longer than the time TRSAH, then a wiring interruption or a defective sensor heating is assumed (B\_silsh).

The operation readiness B\_sbbhk is reset for all detected faults of the sensor downstream catalyst. The operation readiness is generally reset for initialization (C\_ini = 1).

As long as the sensor is cold, neither a fault is present nor is the sensor ready for operation.

### Possible faults:

If the sensor voltage ushk remains within the voltage range USREMH < ushk < USREFH, the flip-flop B\_uhsig is set. When leaving this voltage range this flip-flop B\_uhsig is again reset. The reset is performed after a delay by the time TASIG. If influence peaks (e.g. clocked heating), which lie outside the voltage range, take place on the sensor voltage in case of wiring interruption (sensor voltage within the range), then they are deactivated by the time TASIG and the flip-flop B\_uhsig is not reset. If the flip-flop B\_uhsig remains set for longer than the time TRSAH (sensor voltage within the range), then a wiring interruption or a defective sensor heating is assumed. The fault B\_silsh is reported.

If the voltage of the evaluation circuit is permanently above the value USMAX for longer than the time TUSKS, then there is a SC of the sensor signal wire to UBatt. The fault B\_mxflsh is reported.

The fault detection delayed by the time TUSKS serves as a safeguard against interferences.

There is a wire-to-wire SC between sensor signal and ground lead, if the following applies:

The evaluation voltage for B\_acsdh = 1, i.e. for active Lambda control (B\_lrhk = 1) and switched off secondary air (B\_sls = 0) and secondary air diagnosis (B\_dsls = 0 ; B\_dtes = 0 and B\_esls = 0), as well as the "not set" error flag of the secondary air pump (E\_slpe = 0), and the "not set" error flags of the canister purge control (E\_tes = 0; E\_teve = 0), lies below the threshold USMIN without interruption for longer than the time TUSDUH.

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The fault B\_nplsh is set by the flip-flop B\_adsh in the permanent RAM. If a wire-to-wire SC is still present at the following start, then the closed-loop Lambda control is prohibited in the lower lean turn-on range by the stored fault. The flip-flop is only reset once the sensor voltage ushk is above the threshold USMIN.

If a wire-to-wire SC is already present during a start, then the threshold USREMH is undershot and the operating readiness B\_sbbhk is set, so that B\_lrhk can become active. Thus it is ensured that a wire-to-wire SC can be detected during start.

A wire-to-wire SC is also immediately detected, if during start with cold sensor (B\_lshklt=1), the sensor voltage lies below the threshold USMIN. The flip-flop B\_adsh in the permanent RAM is set and once the time TTBMH has elapsed the fault B\_plaus is indicated. Only once the sensor voltage ushk lies above the threshold USMIN, this flip-flop is reset.

Thus an additional information on whether a mixture fault or a wire-to-wire SC is present can be obtained during the start with cold sensor.

A defective sensor with lowered sensor characteristic (CSD ---> characteristic shift down) is detected in %DLSAHK. The fault B\_mnflsh is set to 0.



Short trip test (function is requested by a tester)

In case a tester is connected (B\_fa = 1) the diagnostic function "DLSH" is blocked until the specific request (B\_falsh = 1) is made. For this function request the large times TRSAH and TUSDUH are switched to markedly smaller times TRSAFA and TUSDUFA, so that a short trip test becomes possible. In order to detect a wire-to-wire SC the control readiness B\_lrhk of the downstream controller is set to the value 1 by B\_falsh = 1.

So that the sensor voltage ushk downstream catalyst lies outside the checked voltage bands (throughput of the catalyst is low due to low load) an enrichment by DLAMELSH is performed by B\_falsh = 1 in %LAMKO.

The sensor voltage downstream catalyst ushk is then definitely above 500 mV, so that all possible faults (wiring interruption and wire-to-wire SC) can be checked.

If ushk lies above the threshold USPHK, then a wire-to-wire SC test is also possible upstream of catalyst in %DLSV.

No fault, fault healed:

If the sensor heating was permanently switched on for longer than the time TBMH and if the operating readiness B\_sbbhk is set and if the sensor voltage ushk lies above the control threshold usrhk (B\_usrhk = 0), then it is very likely that there is no fault. A trigger B\_nolsh is sent to the fault management.

Fault management:

From the three fault types the error flag and the cycle flag are created. The cycle flag, however, is also set after each no-fault resp. healing-trigger and it is reset after each ECU initialization C\_ini. If an error is detected as having been healed (B\_nolsh), then the error flag is reset. By the fault management logic the CARB lamp is only triggered if after 2 trips the cycle flag and the error flag are each set.

### APP DLSH 26.50 Application hint

Useful application values:

- TUSKS : 100 ms
- TRSE : 200 ms
- TRSAH : 600 s
- TUSDUH : 80 s (duration must be chosen a little shorter than the longest uninterrupted active control readiness B\_lrhk in the FTP75 test)
- TUSDUFA: 50 s
- TRSAFA : 50 s
- TBMH : 90 s (time 10s longer than injection secondary air pump)
- TUSEINH : 5 .. 20 s dependent on sensor type (smaller than switch-on time in the HT test in the FTP75 by a fact. 0.7)
- TASIG : 60 ms
- UBDLS : 11 V
- TABGMCS: 700° C
- DLAMELSH: 0.05 dependent on catalyst size

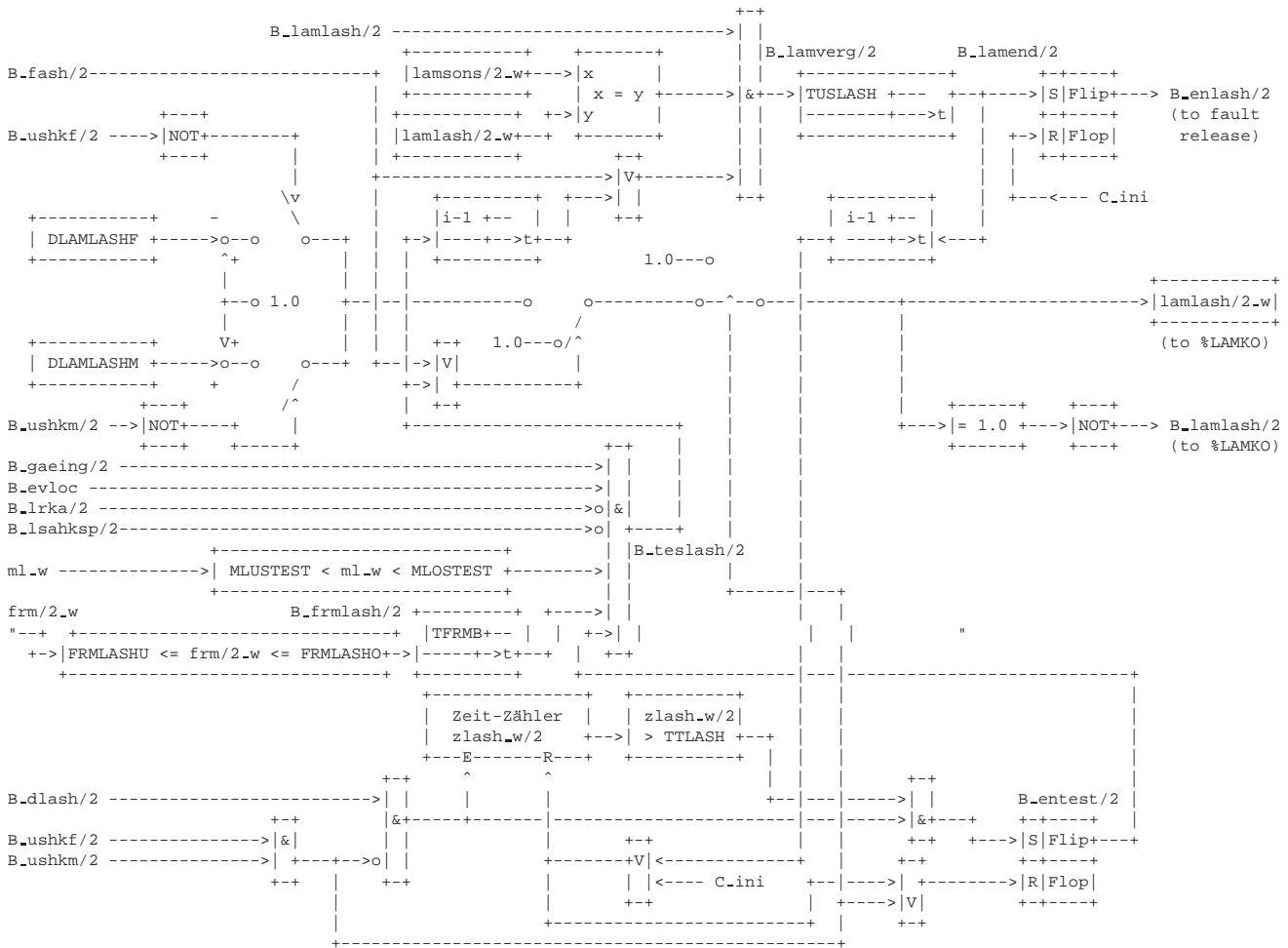
In the following diagram the voltage values, which are to be adjusted are entered.

ushk	SC to U_Bat	U_ADC	U_Sonde
USMAX	Release of operation readiness after t > TRSE (=200ms)	= 1.50 V	1.50 V
USREFH	Signal interruption or sensor cold (sensor heating defective) after t > TRSAH (=600s)	= 0.600 V	0.600 V - Control thresh. KFUSRHK
USREMH	release of operation readiness after t > TRSE (=200ms)	= 0.500 V	0.500 V
USMIN	wire-to-wire SC, if t > TUSDUH (=40 s)	= 0.400 V	0.400 V
		= 0.060 V	0.060 V

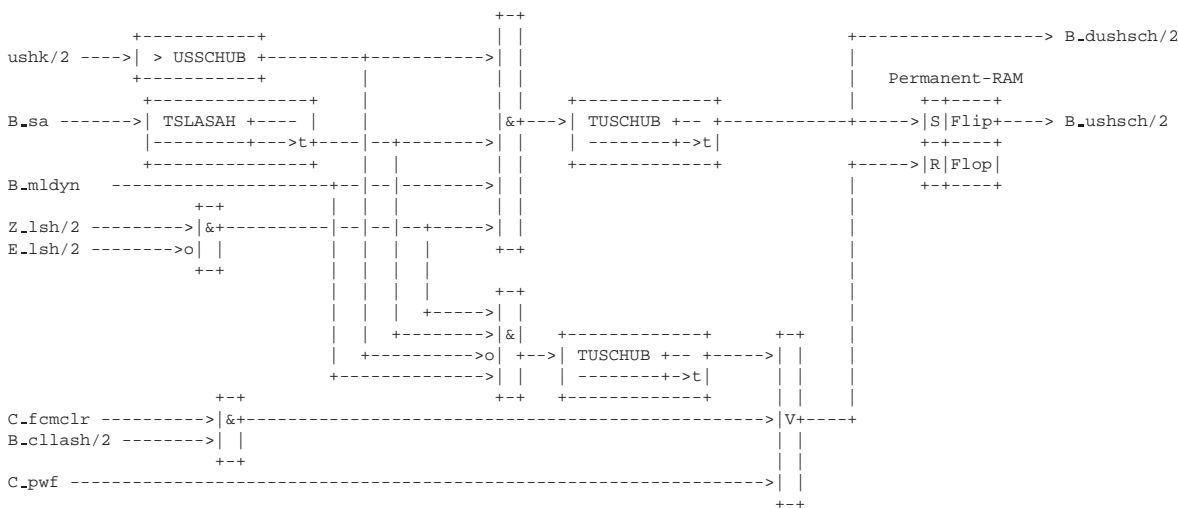




### Test function for oscillation check with Lambda adjustment in %LAMKO

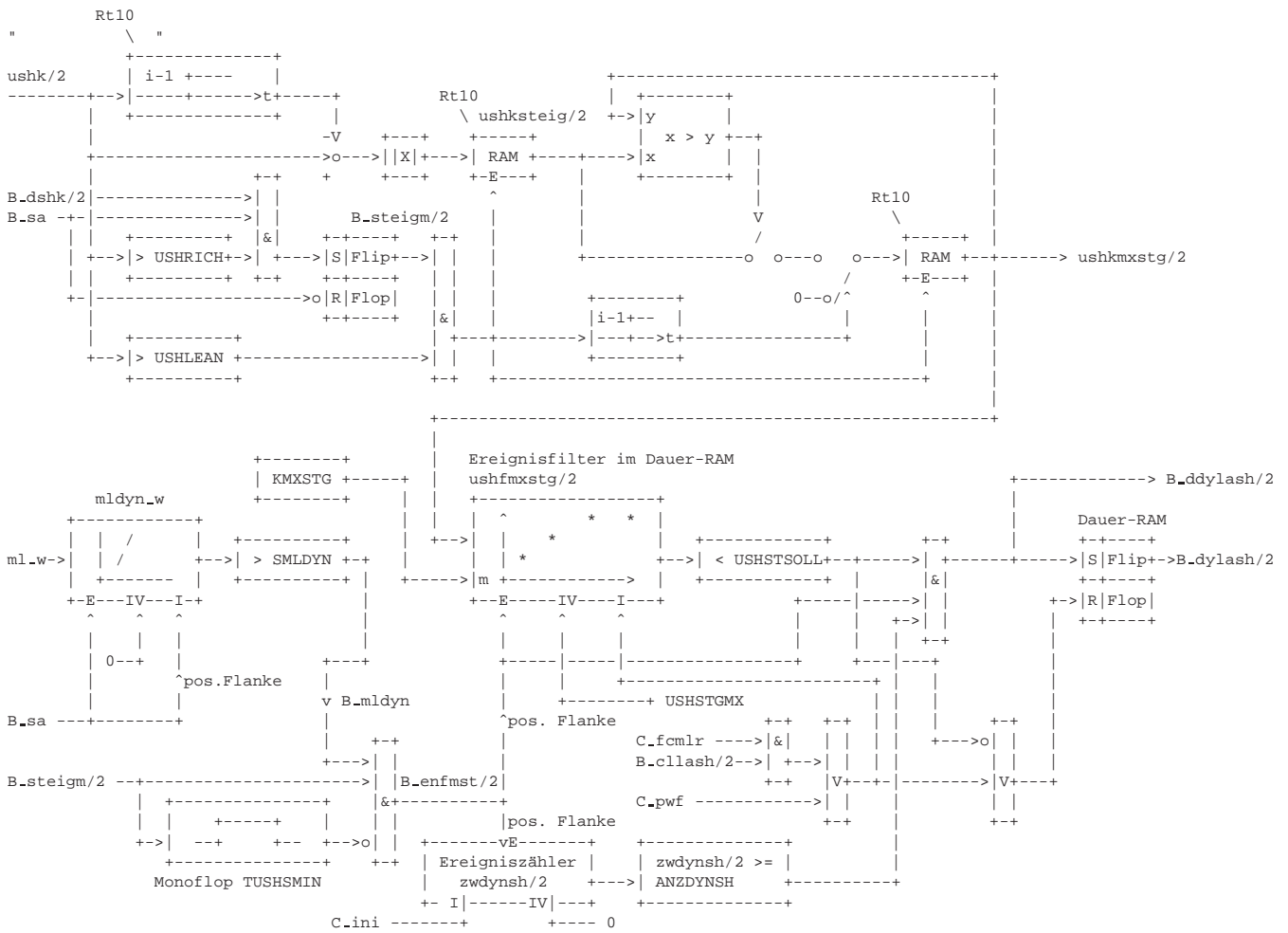


### Checking of the sensor voltage downstream catalyst during fuel cut-off



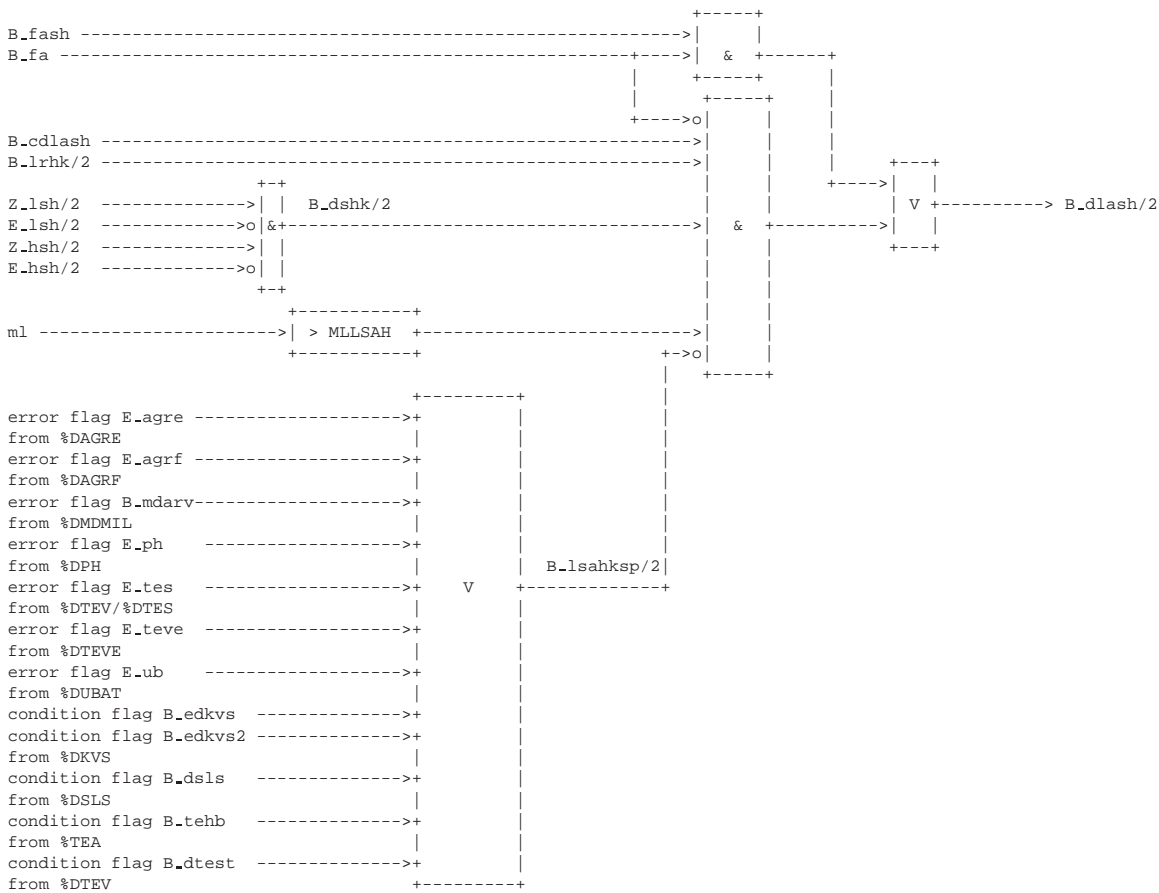


Checking of the sensor dynamics downstream catalyst during fuel cut-off





Release function of the oscillation check downstream catalyst







For each fault path "lash" of this diagnosis function the following values are defined:

	Bank 1	Bank 2
Status fault path lash	sfplash	sfplash2
Error flag lash	E_lash	E_lash2
Cycle flag lash	Z_lash	Z_lash2
Fault type lash	TYP_lash:(B_mxlash, B_mnlash, B_nplash)	TYP_lash2:(B_mxlash2, B_mnlash2, B_nplash2)
Clear fault path:	B_cllash	B_cllash2
Default value active:	B_bklash (optional)	B_bklash2 (optional)
Fault path code lash:	CDTlash	CDTlash2
Fault class lash:	CLAlash	CLAlash2
Fault intensity lash:	TSFlash	TSFlash2
CARB CODE lash	CDClash	CDClash2
Table of ambient cond. lash:	FFTlash	FFTlash2

## ABK DLSAHK 6.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ANZDYNSH			FW	Amount of dynamic measurement for swinging check of sensor post cat
ANZERDYH			FW	amount of error measurements for sensor dynamics at fuel cut-off downstream cat.
ANZERSCH			FW	amount of error measurements for sensor voltage at fuel cut-off downstream cat.
CDCLASH	BLOKNR		KL	code word CARB: lambda sensor aging downstream cat
CDCLASH2	BLOKNR		KL	code word CARB: lambda sensor aging downstream cat, Cyl.row 2
CDLASH			FW	code word O2-sensor aging diagnosis (SHK) in OBDII mode (invers => Europe mode)
CDTLASH			FW	code word tester: lambda sensor aging downstream catalyst [017]
CDTLASH2			FW	code word tester: lambda sensor aging downstream catalyst, cyl.row 2 [023]
CIDLSCHE			FW	comp.ID for single test of measurement at fuel cut-off for sensor downstream cat
CIDLSCHE2			FW	comp.ID for single test of meas. at fuel cut-off for sensor downstream cat bank2
CIDLSDY			FW	comp.ID for single test of dyn. meas. at fuel cut-off for sensor downstream cat.
CIDLSDY2			FW	comp.ID single test of dyn. meas. at fuel cut-off sensor downstream cat. bank2
CIDSHKF			FW	component ID for single test of rich voltage downstream catalyst
CIDSHKF2			FW	component ID for single test of rich voltage downstream catalyst bank2
CIDSHKM			FW	component ID for single test of lean voltage downstream catalyst
CIDSHKM2			FW	component ID for single test of lean voltage downstream catalyst bank2
CLALASH			FW	fault class: O2 sensor aging post cat
CLALASH2			FW	Fault class: Lambda-sensor aging downstream of catalytic converter, bank 2
CWDLASHK			FW	code word for test aging of O2-sensor post cat
CWLSHA			FW	
DLAMLASHF			FW	Delta Lambda set point (rich) for the test oscillation check downstream
DLAMLASHM			FW	Delta Lambda set point (lean) for the test oscillation check downstream
DMRLASH			FW	torque reserve for diagnosis monitoring ageing lambdasensor downstream Kat
FFTLASH	BLOKNR		KL	Table ambient conditions for Lambda sensor downstream catalyst
FFTLASH2	BLOKNR		KL	Table ambient conditions Lambda sensor downstream catalyst bank2
FRMLASHO			FW	upper threshold for mean value of lamda control factor
FRMLASHU			FW	lower threshold for mean value of lamda control factor
KMXSTG			FW	Filter constant for filter max. gradient for sensor downstream catalyst
MLLASH			FW	Air mass threshold for oscillation check downstream catalyst
MLOSTEST			FW	upper air mass threshold for start of test oscillation check downstream catalyst
MLUSSTG			FW	Air mass threshold for dynamic check downstream catalyst
MLUSTEST			FW	lower air mass threshold for start of test oscillation check downstream catalyst
SMLDYN			FW	air mass threshold for sensor dynamic downstream KAT
TABGSTG			FW	threshold for exhaust temperature dynamic-measuring
TFRMB			FW	time delay for detect. the mean value of lamda control factor within thresholds
TLASH			FW	time delay for reset lamlash_w if lamsons_w is not lamlash_w
TRIPFASH			FW	minimum time for active close loop regulation pre catalyst
TSALASH			FW	Time after fuel cut-off for the checking of the sensor downstream catalyst
TSFLASH			FW	fault active time: lambda sensor ageing catalyst downstream
TSFLASH2			FW	fault active time: lamda sesor ageing catalyst downstream, bank 2
TTLASH			FW	Time for voltage of O2 sensor post cat lower/higher than desired threshold
TUSCHUB			FW	Delay time for interference peaks at thrust detection of the rear oxygen sensor
TUSDYN			FW	Delay time for the detection of dynamic sensor faults downstream catalyst
TUSENLASH			FW	time for duration until lean/rich detection is allowed
TUSHSMIN			FW	Minimum time for measuring the gradient for enable filter
TUSLASH			FW	Test time for duration enrichment/enleanment downstream catalyst
TUSSA			FW	delay time after crossing the control threshold downstream cat
USHLEAN			FW	Threshold for lean volt. for reset dynamic measurement of sensor downstream cat.
USHRICH			FW	Threshold for rich volt. for valid dyn. measurement of sensor downstream cat.
USHSTGMX			FW	Value for maximum gradient for initial value of filter
USHSTSOLL			FW	Threshold for permitted gradient of the sensor voltage downstream catalyst
USSCHUB			FW	Threshold for sensor voltage downstream catalyst after fuel cut-off

Variable	Source	Type	Description
B_ABGSTG	DLSAHK	LOK	condition modeltemperature (tkatm od. tanhkm_w) is above threshold
B_ABGSTG2	DLSAHK	LOK	condition modeltemp. (tkatm od. tanhkm_w) is above threshold bank2
B_CDLASH	PROKON	EIN	function active per codeword CDLASH
B_CLLASH		EIN	Delete fault path in DLSA
B_CLLASH2		EIN	Delete fault path in DLSA Bank2
B_CWLSHDYN		EIN	cond. disabling of partial func. dynamics check of sensor downstream cat. %DLSAHK
B_CWLSHSCHE		EIN	cond. disabling of partial func. fuel cut-off for sensor downstream cat. %DLSAHK
B_DDYLASH	DLSAHK	LOK	Condition sensor downstream catalyst dynamically slow
B_DDYLASH2	DLSAHK	LOK	Condition sensor downstream catalyst dynamically slow 'dynamical' bank2





Variable	Source	Type	Description
B_DIDYSCH	DLSAHK	LOK	cond. disable dynamics measurement and make available measured values for Mode 6
B_DIDYSCH2	DLSAHK	LOK	cond. disable dyn. measurement and make available measured val. for Mode 6 bank2
B_DISCH	DLSAHK	LOK	cond. disable fuel cut-off measurement and make avail. measured val. for Mode 6
B_DISCH2	DLSAHK	LOK	cond. disable fuel cut-off measurement and make avail. measured val. Mode 6 bank2
B_DLASH	DLSAHK	LOK	active diagnosis: oxygen sensor aging downstream catalyst function
B_DLASH2	DLSAHK	LOK	active diagnosis: oxygen sensor aging downstream catalyst (cylinder row 2)
B_DSHK	DLSAHK	LOK	Condition diagnosis in %DLSH and %DHLS finished with o.k. downstream cat report
B_DSHK2	DLSAHK	LOK	Cond. diagnosis in %DLSH and %DHLS finished with o.k. downstr. cat report bank2
B_DSL		EIN	condition for active diagnosis of secondary air system
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_DUSHSCH	DLSAHK	LOK	Cond. threshold sen. downst. cat. during fuel cut-off not undershot 'dynamical'
B_DUSHSCH2	DLSAHK	LOK	Cond. threshold sen. downst. cat. during fuel cut-off not undershot 'dyn.' bank2
B_DYLASH	DLSAHK	LOK	Condition sensor downstream catalyst dynamically slow 'static'
B_DYLASH2	DLSAHK	LOK	Condition sensor downstream catalyst dynamically slow 'static' bank2
B_EDKVS	DKVS	EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS	EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_ENFMST	DLSAHK	LOK	Condition enable for filter, take over maximum of the gradient
B_ENLASH	DLSAHK	LOK	Condition test for oscillation check terminated, release cycle bit
B_ENLASH2	DLSAHK	LOK	Condition test for oscillation check terminated, release cycle bit bank2
B_EVLOC	BGEVAB	EIN	Status: all injection valves are activated
B_FASH		EIN	condition diagnosis oxygen sensor aging downstream catalyst function request
B_FASH2		EIN	condition diag. oxygen sensor aging downstream catalyst function request bank2
B_FRMLASH	DLSAHK	LOK	condition mean value of lambda control factor within threshold
B_FRMLASH2	DLSAHK	LOK	condition mean value of lambda control factor within threshold bank2
B_GAEING		EIN	condition basic adaption Bank 1 steady state
B_GAEING2		EIN	condition for adaptive lambda pilot control 2 successful
B_LAMEND	DLSAHK	LOK	Condition end of the Lambda adjustment in %LAMKO
B_LAMEND2	DLSAHK	LOK	Condition end of the Lambda adjustment in %LAMKO bank2
B_LAMLASH	DLSAHK	LOK	Condition for enleanment in %LAMKO
B_LAMLASH2	DLSAHK	LOK	Condition for enleanment in %LAMKO bank2
B_LAMVERG	DLSAHK	LOK	Condition comparison of desired Lambda in %DLSAHK with %LAMKO corresponding
B_LAMVERG2	DLSAHK	LOK	Cond. comparison of desired Lambda in %DLSAHK with %LAMKO corresponding bank2
B_LRHK	LRHK	EIN	condition for lambda closed loop control downstream cat
B_LRHK2	LRHK	EIN	condition for lambda closed loop control downstream cat (bank 2)
B_LSAHKSP	DLSAHK	LOK	flag for general disabling conditions for DLSAHK
B_LSAHKSP2	DLSAHK	LOK	flag for general disabling conditions for DLSAHK bank2
B_MAXLASH	DLSAHK	LOK	Condition for "max.value" for oscillat. check downst.cat detec.
B_MAXLASH2	DLSAHK	LOK	Condition for "max.value" for oscillat. check downst.cat detec. bank2
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_MINLASH	DLSAHK	LOK	Condition for "min. value" of oscillation check downstr. cat detec.
B_MINLASH2	DLSAHK	LOK	Condition for "min. value" of oscillation check downstr. cat detec. bank2
B_MLDYN	DLSAHK	LOK	Condition for minimal air mass in fuel cut off for dynamic measurement
B_MLUSTEST	DLSAHK	LOK	condition ml is within threshold
B_MNLASH	DLSAHK	AUS	Condition for fault type "min. value" of oscillation check downstr. cat detec.
B_MNLASH2	DLSAHK	AUS	Condition for fault type "min. value" of oscill. check downstr. cat detec. bank2
B_MXLASH	DLSAHK	AUS	Condition for fault type "max.value" for oscillat. check downst.cat detec.
B_MXLASH2	DLSAHK	AUS	Condition for fault type "max.value" for oscillat. check downst.cat detec. bank2
B_NDYLASH	DLSAHK	LOK	Condition no Dynamic Error at fuel cut off for sensor downstream catalyst
B_NDYLASH2	DLSAHK	LOK	Condition No Dynamic Error During Acceleration for sensor downstream of catalyst
B_NESCH	DLSAHK	LOK	Condition No Sensor Voltage Error During Acceleration
B_NESCH2	DLSAHK	LOK	Condition No Sensor Voltage Error During Acceleration Bank2
B_NOLASH	DLSAHK	LOK	Condition diagnosis oscillation check finished with o.k. report
B_NOLASH2	DLSAHK	LOK	Condition diagnosis oscillation check finished with o.k. report bank2
B_NPLASH	DLSAHK	AUS	Error typ 'value not plausible' for swinging check post cat
B_NPLASH2	DLSAHK	AUS	Error typ 'value not plausible' for swinging check post cat bank 2
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_STEIGM	DLSAHK	LOK	Condition measure gradient of the sensor signal
B_STEIGM2	DLSAHK	LOK	Condition measure gradient of the sensor signal bank2
B_TEHB	TEB	EIN	condition for canister purge system with high canister load
B_TESLASH	DLSAHK	LOK	Condition perform test for check of the sensor downstream catalyst
B_TESLASH2	DLSAHK	LOK	Condition perform test for check of the sensor downstream catalyst bank2
B_TRFASH	DLSAHK	LOK	Condition Short trip started for oszilation check of O2-sensor post cat
B_TRFASH2	DLSAHK	LOK	Condition Short trip started for oszilation check of O2-sensor bank 2
B_USHKF	DLSAHK	LOK	Condition sensor voltage downstream cat. "Rich" (set point exceeded)
B_USHKF2	DLSAHK	LOK	Condition sensor voltage downstream catalyst "Rich" (set point exceeded) bank2
B_USHKM	DLSAHK	LOK	Condition sensor voltage downstream catalyst "Lean" (set point undershot)
B_USHKM2	DLSAHK	LOK	Condition sensor voltage downstream catalyst "LEAN" (set point undershot) bank2
B_USHSCH	DLSAHK	LOK	Cond. threshold sen. downst. cat. during fuel cut-off not undershot 'statical'
B_USHSCH2	DLSAHK	LOK	Cond. threshold sen. downst. cat. during fuel cut-off not undershot 'stat.'bank2
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DMRLASH_W	DLSAHK	AUS	torque reserve for lambda sensor ageing diagnosis downstream cat
E_AGRE		EIN	error flag: EGR power stage monitoring
E_AGRF		EIN	error flag: EGR flow monitoring
E_HSH	DHLSHK	EIN	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK	EIN	error flag: lambda sensor heating downstream cat on the right
E_LASH	DLSAHK	AUS	error flag: lambda sensor aging downstream cat
E_LASH2	DLSAHK	AUS	error flag: lambda sensor aging downstream cat (cylinder row 2)
E_LSH	DLSH	EIN	error flag: lambda sensor downstream cat
E_LSH2	DLSH	EIN	Errorflag: Lambda-Sensor downstream bank2



Variable	Source	Type	Description
E_PH	DPH	EIN	error flag: phase sensor
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_JUB	GGUB	EIN	error flag: power supply voltage UB
FRM2_W	LR	EIN	fast mean value of lambda control factor bank 2(word)
FRMTRIP2_W	DLSAHK	LOK	Mean value of fr-factor for short trip of oszillation check
FRMTRIP_W	DLSAHK	LOK	Mean value of fr-factor for short trip of oszillation check
FRM_W	LR	EIN	fast mean value of lambda control factor (word)
LAMFRM2_W	DLSAHK	LOK	Lambda offset from mean value lambda regulation factor bank 2
LAMFRM_W	DLSAHK	LOK	Lambda offset from mean value lambda regulation factor
LAMLASH2_W	DLSAHK	AUS	Desired Lambda for test oscillation check downstream catalyst bank2
LAMLASH_W	DLSAHK	AUS	Desired Lambda for test oscillation check downstream catalyst
M6CLSCH	DLSAHK	AUS	Mode 6-Memory: Comp. ID sensor voltage during fuel cut-off downstream cat.
M6CLSCH2	DLSAHK	AUS	Mode 6-Memory: Comp. ID sensor voltage during fuel cut-off downstream cat. bank2
M6CLSDY	DLSAHK	AUS	Mode 6-Memory: Comp. ID dynamic response measurement for sensor downstream cat
M6CLSDY2	DLSAHK	AUS	Mode 6-Memory: Comp. ID dyn. resp. measurement for sensor downstream cat. bank2
M6CSHKF	DLSAHK	AUS	Mode 6-Memory: Comp. ID rich volt. for sensor downstream cat.(osci. test)
M6CSHKF2	DLSAHK	AUS	Mode 6-Memory: Comp. ID rich volt. for sensor downstream cat.(osci. test) bank2
M6CSHKM	DLSAHK	AUS	Mode 6-Memory: Comp. ID lean volt. for sensor downstream cat.(osci. test)
M6CSHKM2	DLSAHK	AUS	Mode 6-Memory: Comp. ID lean volt. for sensor downstream cat.(osci. test) bank2
M6SLSCH	DLSAHK	AUS	Mode 6-Memory: Threshold sensor voltage during fuel cut-off downstream cat.
M6SLSCH2	DLSAHK	AUS	Mode 6-Memory: Threshold sensor volt. during fuel cut-off downstream cat. bank2
M6SLSDY	DLSAHK	AUS	Mode 6-Memory: Threshold dynamic response measurement for sensor downstream cat.
M6SLSDY2	DLSAHK	AUS	Mode 6-Memory: Threshold dyn. resp. measurement for sensor downstream cat. bank2
M6SSHKF	DLSAHK	AUS	Mode 6-Memory: Threshold rich volt. for sensor downstream cat.(osci. test)
M6SSHKF2	DLSAHK	AUS	Mode 6-Memory: Threshold rich volt. for sensor downstream cat.(osci. test) bank2
M6SSHKM	DLSAHK	AUS	Mode 6-Memory: Threshold lean volt. for sensor downstream cat.(osci. test)
M6SSHKM2	DLSAHK	AUS	Mode 6-Memory: Threshold lean volt. for sensor downstream cat.(osci. test) bank2
M6WLSCH	DLSAHK	AUS	Mode 6-Memory: Measured value sensor voltage during fuel cut-off downstream cat.
M6WLSCH2	DLSAHK	AUS	Mode 6-Mem.: Measured value sensor volt. during fuel cut-off downst. cat. bank2
M6WLSDY	DLSAHK	AUS	Mode 6-Mem.: Measured value dyn. resp. measurement for sensor downst. cat.
M6WLSDY2	DLSAHK	AUS	Mode 6-Mem.: Measured value dyn. resp. measurement for sensor downst. cat. bank2
M6WSHKF	DLSAHK	AUS	Mode 6-Mem.: Measured value rich volt. for sensor downst. cat.(osci.test)
M6WSHKF2	DLSAHK	AUS	Mode 6-Mem.: Measured value rich volt. for sensor downst. cat.(osci.test) bank2
M6WSHKM	DLSAHK	AUS	Mode 6-Mem.: Measured value lean volt. for sensor downstr. cat.(osci.test)
M6WSHKM2	DLSAHK	AUS	Mode 6-Mem.: Measured value lean volt. for sensor downstr. cat.(osci.test) bank2
MLDYN_W	DLSAHK	LOK	integrated air mass at fuel cut off
ML_W	EGFE	EIN	air mass flow filtered (Word)
SFPLASH	DLSAHK	AUS	status fault path:
SFPLASH2	DLSAHK	AUS	status fault path:
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TYP_LASH	DLSAHK	AUS	Fault type: lambda sensor aging downstream
TYP_LASH2	DLSAHK	AUS	Fault type: lambda sensor aging downstream bank2
USHFMXSTG	DLSAHK	LOK	Filtered maximum gradient of the sensor voltage downstream catalyst
USHFMXSTG2	DLSAHK	LOK	Filtered maximum gradient of the sensor voltage downstream catalyst bank2
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
USHKMXSTG	DLSAHK	LOK	Maximum gradient of the sensor voltage downstream catalyst
USHKMXSTG2	DLSAHK	LOK	Maximum gradient of the sensor voltage downstream catalyst bank2
USHKSTEIG	DLSAHK	LOK	Gradient of the sensor voltage downstream catalyst
USHKSTEIG2	DLSAHK	LOK	Gradient of the sensor voltage downstream catalyst bank2
USRHK	LRHK	EIN	momentary control threshold for downstream lambda control
USRHK2	LRHK	EIN	momentary control threshold for downstream lambda control, bank2
ZERDYSH	DLSAHK	LOK	counter for error of the dynamics measurement at fuel cut-off
ZERDYSH2	DLSAHK	LOK	counter for error of the dynamics measurement at fuel cut-off bank2
ZERSCH	DLSAHK	LOK	counter for error measurements (sensor voltage threshold not undershot)
ZERSCH2	DLSAHK	LOK	counter for err. meas.(sensor volt.threshold not undershot)at fuel cut-off,bank2
ZLASH2_W	DLSAHK	LOK	Time counter for sensor voltage downstream cat. above/below the set point bank2
ZLASH_W	DLSAHK	LOK	Time counter for the sensor voltage downstream cat. above/below the set point
ZWDYNSH	DLSAHK	LOK	Counter for amount of dynamic measurement for O2 sensor post cat
ZWDYNSH2	DLSAHK	LOK	Counter for amount of dynamic measurement for O2 sensor post cat bank 2
Z_HSH	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat
Z_HSH2	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat, cylinder row 2
Z_LASH	DLSAHK	AUS	cycle flag of lambda sensor aging downstream cat
Z_LASH2	DLSAHK	AUS	cycle flag of lambda sensor aging downstream cat, cylinder row 2
Z_LSH	DLSH	EIN	cycle-flag: lambda sensor downstream cat
Z_LSH2	DLSH	EIN	cycle-Flag: Lambda-sensor downstream cat bank2
Parameter	Value		Description
ANZDYNSH			Amount of dynamic measurement for swinging check of sensor post cat
ANZERDYH			amount of error measurements for sensor dynamics at fuel cut-off downstream cat.
ANZERSCH			amount of error measurements for sensor voltage at fuel cut-off downstream cat.
CDLASH			code word O2-sensor aging diagnosis (SHK) in OBDII mode (invers => Europe mode)
CDTLASH			code word tester: lambda sensor aging downstream catalyst [017]
CDTLASH2			code word tester: lambda sensor aging downstream catalyst, cyl.row 2 [023]
CIDLSCH			comp.ID for single test of measurement at fuel cut-off for sensor downstream cat
CIDLSCH2			comp.ID for single test of meas. at fuel cut-off for sensor downstream cat bank2
CIDLSDY			comp.ID for single test of dyn. meas. at fuel cut-off for sensor downstream cat.
CIDLSDY2			comp.ID single test of dyn. meas. at fuel cut-off sensor downstream cat. bank2



Parameter	Value	Description
CIDSHKF		component ID for single test of rich voltage downstream catalyst
CIDSHKF2		component ID for single test of rich voltage downstream catalyst bank2
CIDSHKM		component ID for single test of lean voltage downstream catalyst
CIDSHKM2		component ID for single test of lean voltage downstream catalyst bank2
CLALASH		fault class: O2 sensor aging post cat
CLALASH2		Fault class: Lambda-sensor aging downstream of catalytic converter, bank 2
CWDLSAHK		code word for test aging of O2-sensor post cat
CWLSHA		
DLAMLASHF		Delta Lambda set point (rich) for the test oscillation check downstream
DLAMLASHM		Delta Lambda set point (lean) for the test oscillation check downstream
DMRLASH		torque reserve for diagnosis monitoring ageing lambdasensor downstream Kat
FRMLASHO		upper threshold for mean value of lamda control factor
FRMLASHU		lower threshold for mean value of lamda control factor
KMXSTG		Filter constant for filter max. gradient for sensor downstream catalyst
MLLASH		Air mass threshold for oscillation check downstream catalyst
MLOSTEST		upper air mass threshold for start of test oscillation check downstream catalyst
MLUSSTG		Air mass threshold for dynamic check downstream catalyst
MLUSTEST		lower air mass threshold for start of test oscillation check downstream catalyst
SMLDYN		air mass threshold for sensor dynamic downstream KAT
TABGSTG		threshold for exhaust temperature dynamic-measuring
TFRMB		time delay for detect. the mean value of lamda control factor within thresholds
TLASH		time delay for reset lamlash_w if lamsons_w is not lamlash_w
TRIPFASH		minimum time for active close loop regulation pre catalyst
TSALASH		Time after fuel cut-off for the checking of the sensor downstream catalyst
TSFLASH		fault active time: lambda sensor ageing catalyst downstream
TSFLASH2		fault active time: lamda sesor ageing catalyst downstream, bank 2
TTLASH		Time for voltage of O2 sensor post cat lower/higher than desired threshold
TUSCHUB		Delay time for interference peaks at thrust detection of the rear oxygen sensor
TUSDYN		Delay time for the detection of dynamic sensor faults downstream catalyst
TUSENLASH		time for duration until lean/rich detection is allowed
TUSHSMIN		Minimum time for measuring the gradient for enable filter
TUSLASH		Test time for duration enrichment/enleanment downstream catalyst
TUSSA		delay time after crossing the control threshold downstream cat
USHLEAN		Threshold for lean volt. for reset dynamic measurement of sensor downstream cat.
USHRICH		Threshold for rich volt. for valid dyn. measurement of sensor downstream cat.
USHSTGMX		Value for maximum gradient for initial value of filter
USHSTSOLL		Threshold for permitted gradient of the sensor voltage downstream catalyst
USSCHUB		Threshold for sensor voltage downstream catalyst after fuel cut-off

## FB DLSAHK 6.50 Detailed description of function

### Introduction:

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The task of the diagnosis function is to check the voltage level of the sensor downstream catalyst.

1. Oscillation check: If the sensor signal constantly remains below or above the set point, then the pilot control (%LRHK, %LRSHK) will enrich or enlean the mixture until the limit stop is reached by means of the integral controller (limiting values of the integral component are exceeded). The sensor upstream catalyst, which is absolutely o.k., is in this case erroneously detected to be defective.
2. Checking during fuel cut-off: The sensor voltage must fall short of a defined voltage threshold.
3. Dynamics check during fuel cut-off: A dynamically slow sensor can be detected by measuring the ascending gradients.

### Release function:

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The release function of the oscillation check for the sensor downstream catalyst is only active B\_dlash = 1, if the general release conditions B\_lashksp = 0 are given and if the electrical and the heater diagnosis for the sensor downstream catalyst have successfully been terminated B\_dshk = 1 and if the air mass ml has exceeded a certain threshold (MLLSAH) as well as the pilot control downstream catalyst B\_lrhk = 1 being turned on.

### Oscillation check downstream catalyst:

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The two flip-flops B\_ushkf and B\_ushkm are reset by C\_ini. They may be set again until the cycle bit Z\_lash = 1 at operating readiness B\_sbbhk = 1 and the delay time TUSENLASH are set, if ushk >= usrhk and ushk <= usrhk are each given for longer than the time TUSSA.

The sensor downstream catalyst is o.k., if the sensor voltage is greater than or equal to the set point usrhk of the pilot control and the controller moves into the direction "lean" (B\_ushkf = 1) and if ushk is less than or equal to the set point usrhk and the controller moves into the direction "rich" (B\_ushkm = 1).

If the sensor voltage ushk during control operation (B\_lrhk = 1 and B\_dlash = 1) remains below or above the set point usrhk (one of the flip-flops B\_ushkf or B\_ushkm is not set) for longer than the time TTLASH, then by a controlled enrichment or enleanment by means of a test function it is checked, whether the sensor voltage can be moved above or below the set point usrhk.

If the counter zlash\_w during control operation downstream catalyst has exceeded the time TTLSAH, then the flip-flop B\_entest is set. Thereafter, with sufficient air mass flow MLUSTEST < ml < MLOSTEST, without catalyst "deoxidization" B\_lrka = 0, no fault flags B\_lsahksp = 0 as well as B\_evloc = 1 (no fuel cut-off) and also the mean value frm\_w of lambda control is inside the thresholds FRMLASHO and FRMLASHU for the time TFRMB the bit B\_teslash is set.

With this bit a switch is closed, by which dependent on set rich/lean flip-flop (B\_ushkf or B\_ushkm), the delta Lambda value



DLAMLASH which is added or subtracted from Lambda 1.0, is passed to the RAM lamlash\_w. In addition the condition B\_lamlash is set in case the Lambda is not equal to 1. For the Lambda coordination %LAMKO the Lambda value lamlash\_w to be adjusted and the condition B\_lamlash are given. Thereafter lamlash\_w over lamsons\_w (Lambda set point) is included in the calculation in the fuel path in %GR. The triggering to Lambda "rich" or "lean" is therefore only performed into one direction, dependent on which flip-flop B\_ushkf or B\_ushkm is set.

Simultaneously the bit B\_lamvergl is set by the B\_teslash delayed by one clock pulse and the performed comparison of lamlash\_w with lamsons\_w from %LAMKO and B\_lamlash set from Lambda not equal to 1.

The controlled enrichment resp. enleanment and the test time TUSLASH are interrupted during a fuel cut-off phase or if ml < MLUSTEST.

If the sensor voltage ushk moves below or above the set point value usrhk (both flip-flops B\_ushkf and B\_ushkm are set) during the test time TUSLASH, then the test is aborted, by setting the Lambda equal to 1 by means of another switch. The condition B\_nolash = 1 (no fault) is set.

If one of the flip-flops B\_ushkf or B\_ushkm is not set once the test time TUSLASH has elapsed and the set trigger B\_lamend, then the flip-flop B\_enlash for the fault release is set by B\_lamend = 1 and the dynamic fault trigger B\_maxlash or B\_minlash can be set.

The cycle flag Z\_lash and the error flag E\_lash are set via B\_maxlash or B\_minlash.

Simultaneously the timer counter z\_lash\_w and the flip-flop B\_entest are reset by means of B\_lamend = 1, which is delayed by one clock pulse. With the reset of B\_entest it is ensured, that the test procedure is switched off, if the sensor is defect.

Since B\_enlash always remains set during a trip after the first test procedure for the fault release, a fault entry can only be performed with active Lambda control, i.e. B\_dlash = 1. This means that when a fault occurs during the test procedure (e.g. heating E\_hsh = 1) and thus one of the flip-flops B\_ushkf or B\_ushkm cannot be set, then this fault is not accepted, since B\_dlash is not set after the test procedure.

Until to the next trip the counters are reset again by C\_ini, so that the test procedure can start again.

#### Short trip for oscillation check:

With connected scan tool and B\_fa = 1 the oscillation check is blocked. The quick test is performed with B\_fash = 1, by switching through DLAMLASHF (enrichment) or DLAMLASHM (enleanment) via the switch and by setting B\_lamlash = 1. If both flip-flops B\_ushkf and B\_ushkm have already been set prior to the quick test having been started, then DLAMLASHF/LAMLASHM is not switched through and lamlash\_w remains set at 1.0. The sensor downstream catalyst is o.k. then. The short trip must be performed for longer than the time TUSLASH, so that in case a fault is possibly present (B\_ushkf or B\_ushkm not set) B\_enlash can be set for the fault release.

#### Checking of the sensor voltage downstream catalyst during fuel cut-off

After a fuel cut-off duration TSALSAH has elapsed and no electrical sensor fault from %DLSH (Z\_lsh = 1 and E\_lsh = 0, the sensor is sufficiently hot) a check is performed during fuel cut-off, on whether the sensor voltage ushk falls short of a threshold USSCHUB. If the sensor voltage during fuel cut-off remains greater than the threshold USSCHUB, then the bit B\_dushsch is set by the trigger and the flip-flop B\_ushsch is set in the permanent RAM. The fault B\_minlash is set by the bit B\_dushsch = 1. The delay time TUSCHUB is only for suppression of interference peak from the sensor voltage.

During normal operating a setting of the cycle bit Z\_lash is independent of this check and therefore it must not be waited for the start of a fuel cut-off duration. This is important on vehicles with automatic transmission, on which a fuel cut-off rarely occurs.

By setting the flip-flop B\_ushsch in the permanent RAM it is achieved that during the 2. trip the bit B\_nolash cannot be set and thus also not the cycle bit Z\_lash. The error flag E\_lash remains set. The cycle bit can only be set during the next check in the fuel cut-off phase B\_sa, by either this fault being confirmed again of by the flip-flop B\_ushsch in the permanent RAM being reset in case of healing, if the sensor voltage ushk falls short of the threshold USSCHUB.

B\_nolash = 1 results from the resetting of B\_ushsch and thus also the error flag E\_lash is reset.

By means of the trigger B\_dushsch it is avoided that the MIL lamp is triggered prior to this fuel cut-off check during the 2. trip.

#### Checking of the sensor dynamics downstream catalyst during fuel cut-off

If the sensor downstream catalyst is dynamically slow, then a "bad" catalyst can be detected as being "good" (avkat small).

With a measurement of the sensor edge times it is not possible to differentiate, also during fuel cut-off, between a dynamically good and bad sensor, especially in case of a bad catalyst.

Dynamically good and bad sensors, however, can be detected more easily, if the maximum ascending gradient of the sensor voltage is determined during fuel cut-off.

The ascending gradient ushksteig (absolute value from new-old value of the sensor voltage ushk) is measured, if during fuel cut-off (B\_sa = 1) the sensor downstream catalyst is o.k. with regard to heater diagnosis and electrical diagnosis and if the sensor voltage is greater USHRICH and greater USHLEAN. The measurement of the ascending gradient is aborted, if the sensor voltage ushk < USHLEAN or if B\_sa = 0. With B\_sa = 0 the flip-flop B\_steigm is reset. For each measurement during fuel cut-off the maximum ascending gradient ushkmxstg is calculated again. This value is only passed (B\_enfmst=1) on to an event filter ushfmxstg, if the fuel cut-off duration B\_sa (B\_steigm = 1) is present for a minimum duration TUSHSMIN and if the integrated air mass during fuel cut-off has exceeded a threshold value SMLDYN.

In the event of powerfail C\_pwf or clear fault path B\_cllash the initial value USHSTGMX is written into the event filter in the permanent RAM.

The filter constant amounts to KMXSTG. If with a dynamically slow sensor the filter value ushfmxstg is less than the limiting value USHSTSOLL, then the flip-flop B\_dylash in the permanent RAM is set and about the trigger B\_ddylash=1 fault B\_nplsh in the permanent RAM and the error E\_lash in the permanent RAM are set. B\_dylash and B\_ddylash can only be set, if after start it takes place a certain number ANZDYNH of dynamic measurements (transient effect from event filter ushfmxstg).

The fault B\_nplsh resp. E\_lash has healed again, if after a sufficient fuel cut-off duration the maximum ascending gradient ushfmxstg is again greater than the threshold value USHSTSOLL.

During normal operating a setting of the cycle bit Z\_lash is independent of this check and therefore it must not be waited for the start of a fuel cut-off duration. This is important on vehicles with automatic transmission, on which a fuel cut-off rarely occurs.

By setting the flip-flop B\_dylash in the permanent RAM it is achieved that during the 2. trip the bit B\_nolash cannot be set and thus also not the cycle bit Z\_lash. The error flag E\_lash remains set. The cycle bit can only be set during the next check in the fuel cut-off phase B\_sa with sufficient fuel cut-off duration (B\_enfmst = 1), by either this fault being confirmed again of by the flip-flop B\_dylash in the permanent RAM being reset in case of healing.

B\_nolash = 1 results from the resetting of B\_dylash and thus also the error flag E\_lash is reset.



By means of the trigger B\_ddylash it is avoided that the MIL lamp is triggered prior to this fuel cut-off check during the 2. trip.

**Fault management:**  
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The error flag E\_lash and the cycle flag Z\_lash are set by means of the trigger from the 3 fault types B\_maxlash, B\_minlash and B\_ddylash. The cycle flag Z\_lash is also set by no-fault B\_nolash and it is reset during each Electronic Control Unit initialization C\_ini. The cycle flag and the error flag are also reset via the clear bit B\_cllash.

With the code bit B\_cdlash = 0 the entire function DLSAHK is switched off and the error flag E\_lash is reset and the cycle flag Z\_lash is set.

The fault triggers B\_maxlash, B\_minlash and B\_ddylash also set the fault flip-flops B\_mxplash, B\_mnlash and B\_nplash in the permanent RAM. These can only be reset again via no-fault B\_nolash resp. E\_lashres.

**General DLSAHK turn-on conditions**  
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For the DLSAHK the following cross-connections with other OBD II diagnosis functions are relevant:

Function:		Processed by means of:
DAGRE	Diagnosis EGR power stage	B_lsahksp
DAGRF	Diagnosis EGR	B_lsahksp
DASE	Diagnosis misfire detection (emission relevant)	B_lsahksp
DEV	Diagnosis injectors	LRVK and LRHK
DHFM	Diagnosis load sensing	E_lm directly
DHLS	Diagnosis sensor heating	B_lsahksp
DKVS	Diagnosis fuel supply system	B_lsahksp
DLSH	Diagnosis downstream lambda sensor	LRHK
DPH	Diagnosis phase sensor	B_lsastp
DLSL	Diagnosis secondary air system	B_dsls
DTEV/DTES	Diagnosis canister purge valve	B_lsahksp
DTEVE	Diagnosis canister purge valve - power stage	B_lsahksp
DUBAT	Diagnosis UBAT	B_lsahksp

**APP DLSAHK 6.50 Application hint**

**Application hints**

The oscillation check sensor downstream catalyst can be switched off by the bit B\_cdlash:

(B\_cdlash=0) --> oscillation check blocked, E\_lash/2 = 0, Z\_lash/2 = 1  
(B\_cdlash=1) --> oscillation check active

**Preconditions for DLSAHK application:**

The two sensor Lambda control (LC or LCS upstream catalyst and Nernst sensor downstream catalyst) and the transient control must have been completely adjusted.

**Application values:**

TUSSA	2 s	
TFRMB	3 s	
TUSENLASH	30 s	
TUSLASH	10 s	dependent on catalyst size
TSALASH	5 s	dependent on catalyst size
TTLASH	100 s	dependent on catalyst size
DLAMLASF	0.10	dependent on catalyst size
DLAMLASM	0.07	dependent on catalyst size
FRMLASSHO	1.035	
FRMLASHU	0.975	
TUSHSMIN	3 s	dependent on catalyst size
TUSCHUB	200 ms	
USHRICH	550 mV	
USHLEAN	100 mV	
USHTEST	100 mV	
USSCHUB	100 mV	
USHSTSOLL	5 mV/ms	
USHSTGMX	70 mV/ms	
KMXSTG	0.5	
MLLASH	50 kg/h	choose such that the flow in the catalyst is as large as possible
MLUSTEST	20 kg/h	above mass flow during idling
MLOSTEST	120 kg/h	
SMLDYN	15 g	dependent on catalyst size
ANZDYN	4	number of dynamic tests dependent from vehicle (manual/automatic transmission)
DMRLASH	7%	for short-trip: choose such that the flow in the catalyst is as large as possible ml >= MLLASH



## DLSSA 14.80 Signal output from lambda sensors

### FDEF DLSSA 14.80 Function definition

Signal output for labda sensor upstream catalyst with conventional lambda control (SY\_STETLR := FALSE)  
=====

While the Lambda sensor aging diagnosis (%DLSA) is active, the Lambda sensor signal upstream catalyst can be considered as being characteristic for the quality of the mounted Lambda sensor upstream catalyst as far as shape and frequency are concerned. By the given Lambda sensor signal, output parameters are continuously calculated, like with the cycle duration monitoring for the upstream Lambda sensor. These parameters describe the shape of the upstream Lambda sensor signal. The calculated parameters together with the integrator value atv of th downstream control and the cycle duration of the upstream Lambda sensor and various constants are then outpitted via a tester interface. For the sensor voltage downstream catalyst the min. and max. values as well as the mean control threshold are sent to the tester if requested. The parameters to be calculated, their value range as well as the quantization which is to be used are described by the SAE standard J1979.

Function block diagram:

Is calculated for SY\_STETLR :=FALSE

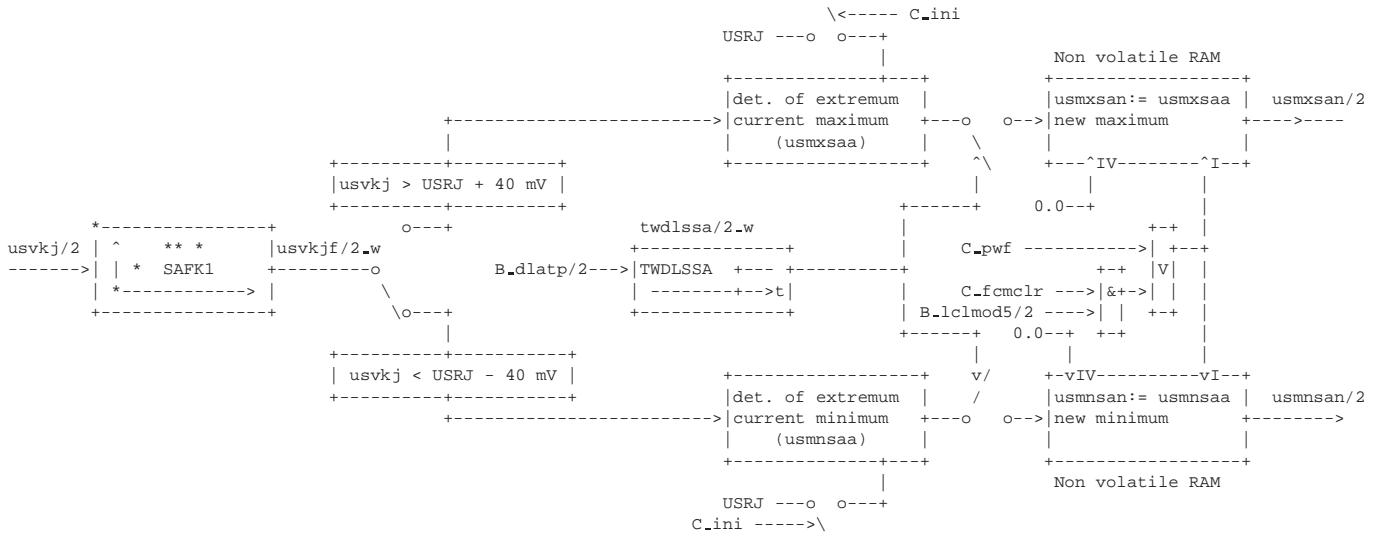
tfrn_w/2	+-----+   time of the usvkj from the     positive to the negative edge   +-----+	tuspnf/2
B_dlatp/2	+-----+   Determination of the max. value     of the upstr. sensor voltage   +-----+	usmxsan/2
(Enable flag for the cycle duration monitoring of the %DLSA, is also used for enabling of the DLSSA)	+-----+   Determination of the min. value     of the upstr. sensor voltage   +-----+	usmnsan/2
atv/2 (manipulated variable of LRHK)	+-----+   conversion to output format   +-----+	atvfett/2
tpsvkmf/2_w (cycle duration of the SVK)	+-----+   conversion to output format   +-----+	tpsvlssa/2
USR (ZPR-control threshold, %LR)	+-----+   conversion to output format   +-----+	USRJ
usvk/2 (upstream sensor voltage)	+-----+   Subtraction of the neg. offset   +-----+	usvkj/2
USMNSAMN (lower limiting value for minimum usvkj)		USMNSAMN
USMNSAMX (upper limiting value for minimum usvkj)		USMNSAMX
USMXSAMN (lower limiting value for maximum usvkj)		USMXSAMN
USMXSAMX (upper limiting value for maximum usvkj)		USMXSAMX
TUSPNMN (lower threshold value for the time betw. pos. and neg. edge)		TUSPNMN
TUSPNMX (upper threshold value for the time betw. pos. and neg. edge)		TUSPNMX
ATVFETTO (upper limiting value for atvfett)		ATVFETTO
ATVFETTU (lower limiting value for atvfett)		ATVFETTU
ATVMAGO (upper limiting value for the atvmager)		ATVMAGO
ATVMAGU (lower limiting value for the atvmager)		ATVMAGU
TPSVKMN (lower limiting value for the cycle duration)		TPSVKMN
TPSVKMX (upper limiting value for the cycle duration)		TPSVKMX



Determination of the minimum and maximum sensor voltage upstream catalyst:

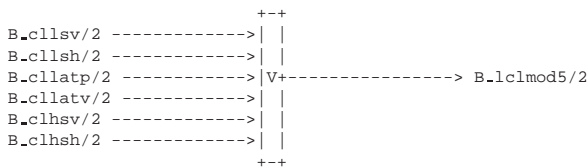
=====

will be calculated for SY\_STETLR := FALSE



Delete fault path DLSSA caused from different functions:

=====



Signal output for labda sensor upstream catalyst with continous lambda control (SY\_STETLR := TRUE)

=====

During active oxygen sensor aging diagnosis the sensor signal (shape and frequency) can be considered as characteristic for the quality of the installed upstream sensor. By means of the present section DLSSA, several parameters are calculated continuously (like cycle duration monitoring of the upstream sensor). These parameters describe the characteristic of the upstream Lambda sensor signal. The calculated values are provided via a tester interface, together with the correction value of the downstream controller, the dynamic property value of the upstream continuous sensor and different constants by a tester interface.

Block diagram of the function:



dynlsu_w / dynlsu2_w	value of dynamic sensor property conversion 16 --> 8 Bit	dynlsu/2
B_dylsu / B_dylsu2		
(release flag for dynamic test LSU monitoring of %DLSU, additionally used for release of %DLSSALRS)		
dlahi_w / dlahi2_w (correction factor of LRHK)	conversion to output standard	dlahisa/2
lamsons_w / lamsons2_w (control threshold %LRS)	conversion to output standard	lamsosa/2
lamsoni_w / lamsoni2_w (lambda upstr. catalyst)	conversion to output standard	lamsisa/2
	subtraction of neg. offset	
LAMSSAMN (lower limit for lambda upstream cat. lamsonij_w)		LAMSSAMN
LAMSSAMX (upper limit for lambda upstream cat. lamsonij_w)		LAMSSAMX
DLAHISATU (lower limit for control value dlahij_w)		DLAHISATO
DLAHISATO (upper limit for control value dlahij_w)		DLAHISATU
DYNLSUTO (upper threshold for dynamic value LSU)		DYNLSUTO
DYNLSUTU (lower threshold for dynamic value LSU)		DYNLSUTU

Function block diagram : Sensor downstream catalyst

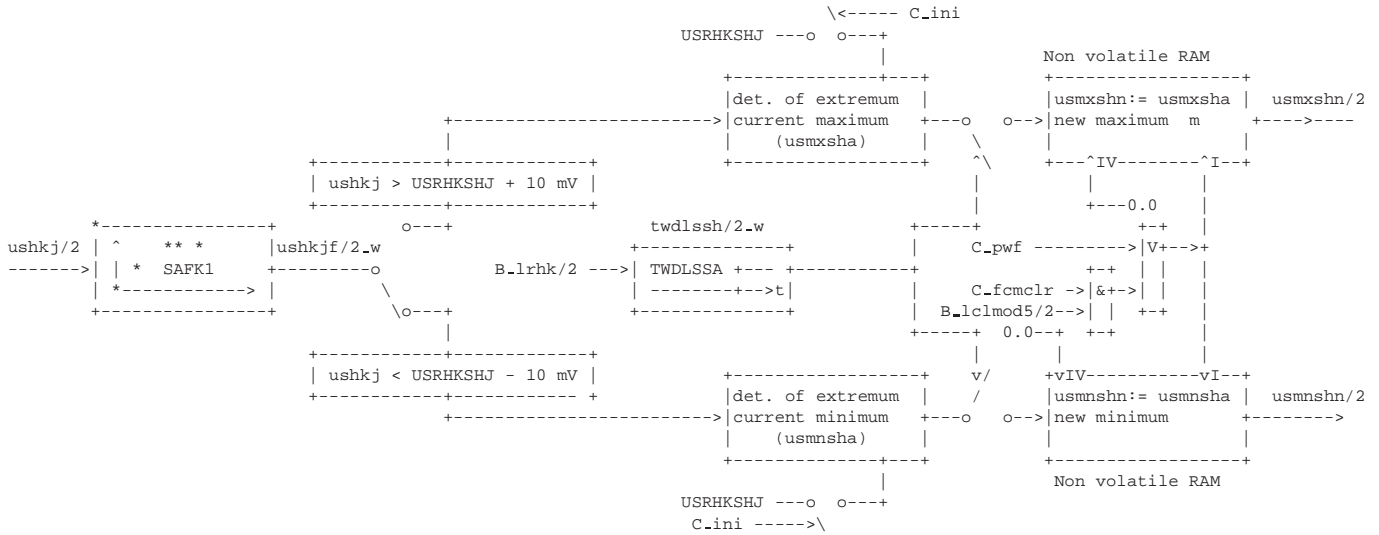
B_lrhk /2		usmxshn/2
	Determination of the max. value of the downstr. sensor voltage	
		usmshn/2
	Determination of the min. value of the downstr. sensor voltage	
ushk/2 (downstream sensor voltage)	Conversion to output format	ushkj/2
USRHKSJHJ (mean control threshold downstream catalyst)		USRHKSJHJ
USMNSHMN (lower limiting value for minimum ushkj)		USMNSHMN
USMNSHMX (upper limiting value for minimum ushkj)		USMNSHMX
usmxshmn (lower limiting value for maximum ushkj)		USMXSHMN
usmxshmx (upper limiting value for maximum ushkj)		USMXSHMX



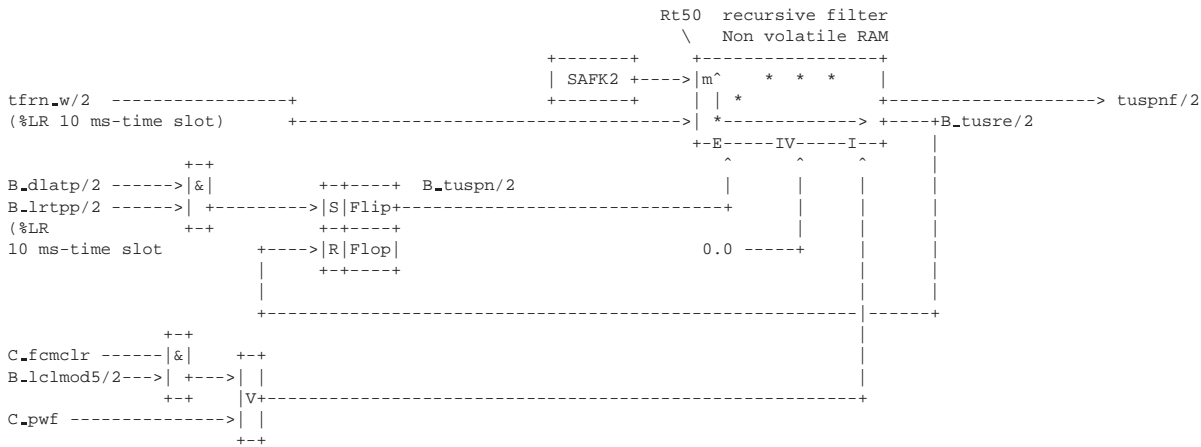


Determination of the minimum and maximum sensor voltage downstream catalyst:

will be calculated for SY-STETLR := TRUE / FALSE



Calculation of the time between crossing the threshold negative to positive and positive to negative upstream catalyst:



### ABK DLSSA 14.80 Abbreviations

The input values for the conventional control are defined in %LR, %LRHK and %DLSSA. The corresponding input values for the continuous control are defined in %LRS, %LRSHK, %GGLSU and %DLSU. The local values and the output values need to be defined anew for the Lambda sensor signal output.

Parameter	Source-X	Source-Y	Type	Description
ATVFETTO			FW	upper threshold for atvfett, CARB tester, DLSSA
ATVFETTU			FW	lower threshold for atvfett, CARB tester, DLSSA
ATVMAGO			FW	upper threshold for atvmager, CARB tester, DLSSA
ATVMAGU			FW	lower threshold for atvmager, CARB tester, DLSSA
DLAHISATO			FW	upper threshold for dlahisa, CARB tester, DLSSALRS
DLAHISATU			FW	lower threshold for dlahisa, CARB tester, DLSSALRS
DYNLSUTO			FW	upper threshold for dynlsusa, CARB tester, DLSSALRS
DYNLSUTU			FW	lower threshold for dynlsusa, CARB tester, DLSSALRS
LAMSSAMN			FW	lower threshold for lamsosa and lamsisa, CARB tester, DLSSALRS
LAMSSAMX			FW	upper threshold for lamsosa and lamsisa, CARB tester, DLSSALRS
SAFK1			FW	filter constant 1 for lambda sensor signal access
SAFK2			FW	filter constant 2 for lambda sensor signal access
TPSVKMN			FW	minimum cycle duration of upstream lambda sensor, DLSSA
TPSVKMX			FW	maximum cycle duration of upstream lambda sensor, DLSSA
TUSPNMN			FW	min. time of the sensor voltage between pos. and neg. slope
TUSPNMX			FW	max. time of the sensor voltage between pos. and neg. slope
TWDLSSA			FW	minium test duration for DLSSA extreme value evaluation
USIVMAXH			FW	Init value for max.sensor volt. downstr. cat. after powerfail/clear fault memory
USIVMAXV			FW	Init value for max. sensor volt. upstr. cat. after powerfail/clear fault memory
USIVMINH			FW	Init value for min.sensor volt. downstr. cat. after powerfail/clear fault memory



Parameter	Source-X	Source-Y	Type	Description
USIVMINV			FW	Init value for min. sensor volt. upstr. cat. after powerfail/clear fault memory
USMNSAMN			FW	max. detected sensor voltage for signal output (min. plaus. value)
USMNSAMX			FW	min. detected sensor voltage for signal output (max. plaus. value)
USMNSHMN			FW	max. detected sensor voltage downstr. cat. for signal output (min. plaus. value)
USMNSHMx			FW	min. detected sensor voltage downstr. cat. for signal output (max. plaus. value)
USMXSAMN			FW	max. detected sensor voltage for signal output (min. plaus. value)
USMXSAMX			FW	max. detected sensor voltage for signal output (max. plaus. value)
USMXSHMN			FW	max. detected sensor voltage downstr. cat. for signal output (min. plaus. value)
USMXSHMX			FW	max. detected sensor voltage downstr. cat. for signal output (max. plaus. value)
USR			FW	controller threshold for lambda control upstream catalyst
USRHKSH			FW	controller threshold for lambda control downstream catalyst, DLSSA display
USRHKSHJ			FW	controller threshold for lambda control downstream catalyst, DLSSA display
Variable	Source		Type	Description
ATV	LRHK		EIN	current integrator value of lambda control downstream cat
ATV2	LRHK		EIN	current integrator value of lambda control downstream cat 2
ATVFETT	DLSSA		AUS	atv shifting to 'rich', DLSSA
ATVFETT2	DLSSA		AUS	atv shifting to 'rich', DLSSA (bank2)
ATVMAGER	DLSSA		AUS	atv shifting to 'lean', DLSSA
ATVMAGER2	DLSSA		AUS	atv shifting to 'lean', DLSSA (bank2)
B_DLATP	DLSA		EIN	condition for active diagnosis: lambda sensor aging TP
B_DLATP2	DLSA		EIN	condition for active diagnosis: lambda sensor aging TP (cylinder row 2)
B_LCLMOD5	DLSSA		LOK	Clear nonvolatile RAM of DLSSA
B_LCLMOD52	DLSSA		LOK	Clear nonvolatile RAM of DLSSA
B_LRHK	LRHK		EIN	condition for lambda closed loop control downstream cat
B_LRHK2	LRHK		EIN	condition for lambda closed loop control downstream cat (bank 2)
B_LRTPP	LR		EIN	Periodic time valid, static cond. for %LR (amplitude/periodic time) = TRUE
B_LRTPP2	LR		EIN	static condition for lambda controller (amplitude/periodic time) bank2
B_TUSPN	DLSSA		LOK	Condition time between sensor transitions tfrn_w (%LR) valid
B_TUSPN2	DLSSA		LOK	Condition time between sensor transitions tfrn2_w (%LR) valid
B_TUSRE	DLSSA		LOK	Condition result for filtered half period for sensor upstream cat
B_TUSRE2	DLSSA		LOK	Condition result for filtered half period for sensor upstream cat bank2
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
DLAHI2_W			EIN	I-portion of the continuous LRHK2
DLAHISA	DLSSA		AUS	I part LRSHK, signal output DLSSA (SY_STETLR := TRUE), bank 1
DLAHISA2	DLSSA		AUS	I part LRSHK, signal output DLSSA (SY_STETLR := TRUE), bank 2
DLAHI_W			EIN	I-portion of the LRSHK
DYNLSU2_W			EIN	Dynamical value of the LSU, bank 2
DYNLSUSA	DLSSA		AUS	signal output DLSSA: dynamic value LSU, bank 1
DYNLSUSA2	DLSSA		AUS	signal output DLSSA: dynamic value LSU, bank 2
DYNLSU_W			EIN	Dynamical value of the LSU
LAMSISA	DLSSA		AUS	Signal output DLSSA: measured value lambda, bank 1
LAMSISA2	DLSSA		AUS	Signal output DLSSA: measured value lambda, bank 2
LAMSONI2_W			EIN	Lambda actual value
LAMSONI_W			EIN	Lambda actual value
LAMSONS2_W	LAMSOLL		EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL		EIN	required lambda referred to lambda sensor fitting location
LAMSOSA	DLSSA		AUS	Signal output DLSSA: lambda set value %LRS, bank 1
LAMSOSA2	DLSSA		AUS	Signal output DLSSA: lambda set value %LRS, bank 2
SY_STETLR	PROKON		EIN	System constant condition continuous Lambda control present
TFRN2_W	LR		EIN	time duration lambda controller negativ slope, bank 2
TFRN_W	LR		EIN	time duration lambda controller negativ slope
TPSVKMF2_W	DLSA		EIN	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (word)
TPSVKMF_W	DLSA		EIN	filtered cycle duration of sensor signal upstream cat. (word)
TPSVLSA2	DLSSA		AUS	cycle duration (sensor signal upstream cat) for DLSSA (bank2)
TPSVLSSA	DLSSA		AUS	cycle duration (sensor signal upstream cat) for DLSSA
TPSVLSSA2	DLSSA		AUS	cycle duration (sensor signal upstream cat) for DLSSA (bank2)
TUSPNF	DLSSA		AUS	filtered time between positive and negative usvk slope, DLSSA
TUSPNF2	DLSSA		AUS	filtered time between positive and negative usvk slope, DLSSA (bank2)
TWDLSSA2_W	DLSSA		LOK	timer of minimum test duration for DLSSA-extreme evaluation bank2
TWDLSSA_W	DLSSA		LOK	timer of minimum test duration for DLSSA-extreme evaluation
TWDLSSH2_W	DLSSA		LOK	timer of minimum test duration for DLSSA-extreme evaluation downstream cat bank2
TWDLSSH_W	DLSSA		LOK	timer of minimum test duration for DLSSA-extreme evaluation downstream cat
USHK	GGLSH		EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH		EIN	output voltage oxygen sensor downstream catalyst 2
USHKJ	DLSSA		LOK	output voltage oxygen sensor downstream catalyst without offset, DLSSA, bank 1
USHKJ2	DLSSA		LOK	output voltage oxygen sensor downstream catalyst without offset, DLSSA, bank 2
USHKJF2_W	DLSSA		LOK	filterd output voltage oxygen sensor downstream cat without offset, DLSSA (bank2)
USHKJF_W	DLSSA		LOK	filterd output voltage oxygen sensor downstream catalyst without offset, DLSSA
USMNSAA	DLSSA		LOK	minimum established sensor voltage value upstream cat (old), DLSSA, bank 1
USMNSAA2	DLSSA		LOK	minimum established sensor voltage value upstream cat (old), DLSSA, bank 2
USMNSAN	DLSSA		AUS	minimum established sensor voltage value upstream cat (new), DLSSA
USMNSAN2	DLSSA		AUS	minimum established sensor voltage value upstream cat (new), DLSSA (bank2)
USMNSHA	DLSSA		LOK	minimum established sensor voltage value upstream cat (old), DLSSA, bank 1
USMNSHA2	DLSSA		LOK	minimum established sensor voltage value upstream cat (old), DLSSA, bank 2
USMNSHN	DLSSA		AUS	minimum established sensor voltage value downstream cat (new), DLSSA
USMNSHN2	DLSSA		AUS	minimum established sensor voltage value downstream cat (new), DLSSA
USMXSAA	DLSSA		LOK	maximum established sensor voltage value upstream cat (old), DLSSA, bank 1
USMXSAA2	DLSSA		LOK	maximum established sensor voltage value upstream cat (old), DLSSA, bank 2
USMXSAN	DLSSA		AUS	maximum established sensor voltage value upstream cat (new), DLSSA
USMXSAN2	DLSSA		AUS	maximum established sensor voltage value upstream cat (new), DLSSA (bank2)



Variable	Source	Type	Description
USMXSHA	DLSSA	LOK	maximum established sensor voltage value upstream cat (old), DLSSA, bank 1
USMXSHA2	DLSSA	LOK	maximum established sensor voltage value upstream cat (old), DLSSA, bank 2
USMXSHN	DLSSA	AUS	maximum established sensor voltage value downstream cat (new), DLSSA
USMXSHN2	DLSSA	AUS	maximum established sensor voltage value downstream cat (new), DLSSA
USRJ	DLSSA	AUS	lambda control threshold without offset, DLSSA
USVK	GGLSV	EIN	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyst 2
USVKJ	DLSSA	AUS	output voltage oxygen sensor upstream catalyst without offset, DLSSA
USVKJ2	DLSSA	AUS	output voltage oxygen sensor upstream catalyst without offset, DLSSA (Bank2)
USVKJF2_W	DLSSA	LOK	filtered output voltage oxygen sensor upstream cat. without offset, DLSSA (bank2)
USVKJF_W	DLSSA	LOK	filtered output voltage oxygen sensor upstream catalyst without offset, DLSSA

Parameter	Value	Description
ATVFETTO		upper threshold for atvfett, CARB tester, DLSSA
ATVFETTU		lower threshold for atvfett, CARB tester, DLSSA
ATVMAGO		upper threshold for atvmager, CARB tester, DLSSA
ATVMAGU		lower threshold for atvmager, CARB tester, DLSSA
DLAHISATO		upper threshold for dlahisa, CARB tester, DLSSALRS
DLAHISATU		lower threshold for dlahisa, CARB tester, DLSSALRS
DYNLSUTO		upper threshold for dynlsusa, CARB tester, DLSSALRS
DYNLSUTU		lower threshold for dynlsusa, CARB tester, DLSSALRS
LAMSSAMN		lower threshold for lamsosa and lamsisa, CARB tester, DLSSALRS
LAMSSAMX		upper threshold for lamsosa and lamsisa, CARB tester, DLSSALRS
SAFK1		filter constant 1 for lambda sensor signal access
SAFK2		filter constant 2 for lambda sensor signal access
TPSVKMN		minimum cycle duration of upstream lambda sensor, DLSSA
TPSVKMX		maximum cycle duration of upstream lambda sensor, DLSSA
TUSPNMN		min. time of the sensor voltage between pos. and neg. slope
TUSPNMX		max. time of the sensor voltage between pos. and neg. slope
TWDLSSA		minium test duration for DLSSA extreme value evaluation
USIVMAXH		Init value for max.sensor volt. downstr. cat. after powerfail/clear fault memory
USIVMAXV		Init value for max. sensor volt. upstr. cat. after powerfail/clear fault memory
USIVMINH		Init value for min.sensor volt. downstr. cat. after powerfail/clear fault memory
USIVMINV		Init value for min. sensor volt. upstr. cat. after powerfail/clear fault memory
USMNSAMN		max. detected sensor voltage for signal output (min. plaus. value)
USMNSAMX		min. detected sensor voltage for signal output (max. plaus. value)
USMNSHMN		max. detected sensor voltage downstr. cat. for signal output (min. plaus. value)
USMNSHMX		min. detected sensor voltage downstr. cat. for signal output (max. plaus. value)
USMXSAMN		max. detected sensor voltage for signal output (min. plaus. value)
USMXSAMX		max. detected sensor voltage for signal output (max. plaus. value)
USMXSHMN		max. detected sensor voltage downstr. cat. for signal output (min. plaus. value)
USMXSHMX		max. detected sensor voltage downstr. cat. for signal output (max. plaus. value)
USR		controller theshold for lambda control upstream catalyst
USRHKSH		controller theshold for lambda control downstream catalyst, DLSSA display
USRHKSHJ		controller theshold for lambda control downstream catalyst, DLSSA display

## FB DLSSA 14.80 Detailed description of function

Data to be calculated for the Lambda sensor signal output for the conventional control:

```
tuspnf: Time of the sensor voltage between positive and negative edge
usmxsan: maximum detected sensor voltage value for signal output upstream catalyst
usmnsan: minimum detected sensor voltage value for signal output upstream catalyst
usmxshn: maximum detected sensor voltage value for signal output downstream catalyst
usmshn: minimum detected sensor voltage value for signal output downstream catalyst
atvfett: Integrator manipulated variable for the pilot control towards RICH
atvmager: Integrator manipulated variable for the pilot control towards LEAN
tpsvlssa: Cycle duration of the sensor signal upstream catalyst for signal output
usrj: Control threshold of the Lambda control (without offset)
usvkj: Sensor voltage upstream catalyst without negative voltage offset
```

Data to be calculated for the Lambda sensor signal output for the continuous control:

```
dlahisa: Integrator control variable of the downstream control
```

Data to be calculated for the Lambda sensor downstream catalyst:

```
usrhkshj: Control threshold of the pilot control downstream catalyst (without offset)
ushkj: Sensor voltage downstream catalyst (without offset)
```

1. Determination of the minimum and maximum sensor voltage upstream (SY\_STETLR := FALSE) /downstream catalyst

With initialization C.ini the RAM-cells for the old maximum (usmxsaa resp. usmxsha) and for the old minimum (usmnsaa resp. usmnsa) are set to the starting value USRJ resp. USRHKSHJ.

The RAM-cells for the new maximum (usmxsan resp.usmxshn) and for the new minimum (usmnsan resp. usmshn) are reset with powerfail.

The new extremums (minimum resp. maximum of the Lambda sensor voltage upstream and downstream catalyst) are output via the tester interface.

While driving the absolute minimum resp. maximum is formed within a n-,tl-range, which is preset by the %DLSA.



The current extremum is entered into the RAM-cell "old maximum" resp. "old minimum". The purpose of the filters is to smooth the input signal usvkj and ushkj.

The extremums are formed according to the following principal:

If the sensor voltage usvkjf\_w resp. ushkjf\_w is greater than the presently stored positive peak value usmxsaa resp. usmxsha, then it is overwritten by the currently filtered sensor voltage usvkj resp. ushkj.

If the sensor voltage usvkj resp. ushkj is less than the presently stored negative peak value usmnsaa resp. usmnsha, then it is overwritten by the currently filtered sensor voltage usvkj resp. ushkj.

As long as the enable flag of the %DLSSA cycle duration monitoring (B\_dlatp) or of active closed loop B\_lrhk remains set for longer than the time TWDLSSA (engine is in a defined nmot-, rl-range), the new extremum is always overwritten by the current old extremum and thus made available to the tester interface. The output signal (usmnsan resp. usmnshn as well as usmxsan resp. usmxshn), however, remains active, i.e. it does not remain frozen for good at an extreme value.

## 2. Calculation of the time between positive and negative edge upstream catalyst (SY\_STETLR := FALSE)

By the section %LR the total time of a controller cycle tpsvkmf\_w is calculated summing the positive integrator time tfrp\_w and the negative integrator time tfrn\_w. tfrn\_w is the time for the positive half cycle of the lambda control and is exactly the time requested by the SCAN-tool. For (B\_dlatp AND B\_lrtpp) = TRUE the most recent time tfrn\_w will be taken as input to the recursive filter. As B\_lrtpp is calculated in the 10 ms time slot the Bit status is buffered by the Flip Flop B\_tuspn. This Flip Flop will be reset at the end of the filter calculation using the Bit B\_tusre. The RAM used with the recursive filter is located in a non volatile RAM. The filter constant is SAFK2.

## 3. I-part of the downstream control (SY\_STETLR := FALSE)

The output value atv of the integrator is given in 40ms increments as absolute value in atvfett and atvmager. This conversion is necessary since atv is a signed-byte value and can contain positive as well as negative values, however, the CARB tester interface only allows positive values. For this reason this value is entered into atvfett, if atv contains a positive value and atvmager is zero in this case. If the value of atv is negative this value is entered as absolute value into atvmager and atvfett is set to zero.

The quantization between atv (see %LRHK) and atvfett resp. atvmager (40ms) differs! The limiting values for atvfett are ATVFETTO and ATVFETTU, for atvmager the limiting values are ATVMAGO and ATVMAGU.

## 4. Cycle duration (SY\_STETLR := FALSE)

The cycle duration of the Lambda sensor signal upstream catalyst (tpsvkmf\_w) is quantized with 10ms, for the DLSSA the cycle duration (tpsvlssa) needs to be quantized with 40ms. The value tpsvkmf determined in the %LR must therefore be converted accordingly for the DLSSA. The limiting values for tpsvkmf\_w are TPSVKMN and TPSVKMX.

## 5. Control threshold, sensor voltage upstream catalyst (SY\_STETLR := FALSE)

The control threshold USR and the sensor voltage upstream catalyst must be converted for the DLSSA output to the CARB tester, since a negative voltage offset is included in the calculation of the BOSCH conversion formula. However, this offset is not provided in the SAE1979. This means that this offset must be subtracted from the constant USR and from the variables usvk. The resulting values are USRJ and usvkj. The conversion formula is the same in both cases.

## 6. Integrator control variable of downstream control (%LRSHK) (SY\_STETLR := TRUE)

The absolute value of the integrator output value dlahi\_w is stored in dlahisa (0.0039/increment). This conversion is required as dlahi\_w is considered a two-byte value. Furthermore, dlahi\_w may contain positive and negative values. The limits for dlahisa are DLAHISATO and DLAHISATU. However, according to CARB, only unsigned values are permitted. Therefore a offset of HEX 80 is added to dlahisa.

## 7. Dynamic value dynlsu for the LSU (SY\_STETLR := TRUE)

The dynamic properties of the LSU are characterized by the value dynlsu calculated by the section %DLSU. dynlsu\_w is converted to the Byte-value dynlsusa. The limits for dynlsusa are DYNLSUTU and DYNLSUTO.

## 8. Threshold value for downstream sensor (SY\_STETLR := TRUE/FALSE)

The threshold value USRHKSHJ and the downstream sensor signal voltage must be converted for the DLSSA output, before it is transferred to the CARB tester, since a negative voltage offset is considered in the BOSCH conversion formula (this offset is not considered in SAE 1979). That means that this offset must be subtracted from the variable ushk, which then results in the values ushkj. In either case the conversion formula is the same. The representative controller threshold USRHKSHJ is directly defined as fixed value and output to the tester.

## 9. DLSSA output routine:

The following values are outputted via the tester interface:

Sensor upstream catalyst (SY\_STETLR := FALSE)

tuspnf: filtered time of the sensor voltage between positive and negative edge  
usmxsan: maximum detected sensor voltage value for signal output  
usmnsan: minimum detected sensor voltage value for signal output  
atvfett: TV shift towards RICH  
atvmager: TV shift towards LEAN  
tpsvlssa: averaged cycle duration of the sensor signal upstream catalyst  
usrj: control threshold from %LR (without offset)  
USMNSAMN: minimum detected sensor voltage value for signal output (min. plaus. value)  
USMNSAMX: maximum detected sensor voltage value for signal output (max. plaus. value)  
USMXSAMN: maximum detected sensor voltage value for signal output (min. plaus. value)  
USMXSAMX: minimum detected sensor voltage value for signal output (max. plaus. value)  
TUSPNMN: minimum time of the sensor voltage between positive and negative edge





Test ID \$00: output upstream sensor , LSU-Type, conventional control (SY\_STETLR := TRUE)

selected by date3/bit 0 (bank 1 /sensor 1)  
selected by date3/bit 4 (bank 2 /sensor 1)====> stereo

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20
output yes/no	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   1

following ID's used -----^

Test-ID \$20:

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	21 22 23 24 25 26 27 28	29 2A 2B 2C 2D 2E 2F 30	31 32 33 34 35 36 37 38	39 3A 3B 3C 3D 3E 3F 40
output yes/no	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   1

following ID's used -----^

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	41 42 43 44 45 46 47 48	49 4A 4B 4C 4D 4E 4F 50	51 52 53 54 55 56 57 58	59 5A 5B 5C 5D 5E 5F 60
output yes/no	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   1

following ID's used -----^

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	61 62 63 64 65 66 67 68	69 6A 6B 6C 6D 6E 6F 70	71 72 73 74 75 76 77 78	79 7A 7B 7C 7D 7E 7F 80
output yes/no	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   1

following ID's used -----^

By user definable test-id's

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	81 82 83 84 85 86 87 88	89 8A 8B 8C 8D 8E 8F 90	91 92 93 94 95 96 97 98	99 9A 9B 9C 9D 9E 9F A0
output yes/no	1   1   1   1   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0

L L D D  
A A Y L  
M M N A  
S S L H  
I O S I  
S S U S  
A A S A  
J J A J  
J

no following ID's -----^

Test-ID \$A0, Test-ID \$C0 und Test-ID \$E0:

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	x1 x2 x3 x4 x5 x6 x7 x8	x9 xA xB xC xD xE xF x0	x1 x2 x3 x4 x5 x6 x7 x8	x9 xA xB xC xD xE xF x0
output yes/no	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0	0   0   0   0   0   0   0   0



Test ID \$00: output downstream catalystr (SY\_STETLr := TRUE/FALSE):  
 selected by date3/bit 1 (bank 1 /sensor 2)  
 selected by date3/bit 5 (bank 2 /sensor 2) =====> stereo

	DATA-A	DATA-B	DATA-C	DATA-D
TEST ID	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20
output yes/no	1 1 0 0 0 0 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
	U U	U U		
	S S	S S		
	R R	M M	n o f o l l o w i n g	I D ' s
	H H	N X		
	K K	S S		
	S S	H H		
	H H	N N		
	J J			

Test ID \$20:

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	21 22 23 24 25 26 27 28	29 2A 2B 2C 2D 2E 2F 30	31 32 33 34 35 36 37 38	39 3A 3B 3C 3D 3E 3F 40
output yes/no	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0

Test ID \$40, test ID \$60, test ID \$80, test ID \$A0, test ID \$C0 and test ID \$E0:

	DATA-A	DATA-B	DATA-C	DATA-D
TEST-ID	x1 x2 x3 x4 x5 x6 x7 x8	x9 xA xB xC xD xE xF x0	x1 x2 x3 x4 x5 x6 x7 x8	x9 xA xB xC xD xE xF x0
output yes/no	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0

### APP DLSSA 14.80 Application hint

FW name                      typical value

ATVFETTO	1.2 s
ATVFETTU	0 s
ATVMAGO	1.2 s
ATVMAGU	0 s
SAFK1	0.1
SAFK2	0.1
TPSVKMN	0.3 s
TPSVKMX	3 s
TUSPNMN	0.15 s
TUSPNMX	1.5 s
TWDLSSA	10 s
USMNSAMN	0.005 V
USMNSAMX	0.4 V
USMXSAMN	0.5 V
USMXSAMX	1.05V
USMNSHMN	0.005 V
USMNSHMX	0.4V
USMXSHMN	0.5 V
USMXSHMX	1.05 V

FW name                      typical value

DLAHISATO	0.05
DLAHISATU	-0.05
DYNLSUTU	0.3
DDYNLSTO	4,0
SAFK2	0.1
TWDLSSA	10 s
LAMSSAMN	0.7
LAMSSAMX	2.0

Assignment DLSSA parameter - tester interface

Nernst- sensor upstream catalystr



Test ID	test value	min. Limit	max. Limit
\$01	usrj	-	-
\$02	usrj	-	-
\$07	usmnsan	USMNSAMN	USMNSAMX
	usmnshn	USMNSHMN	USMNSHMX
\$08	usmxsan	USMXSAMN	USMXSAMX
	usmxshn	USMXSHMN	USMXSHMX
\$09	tuspnf	TUSPNMN	TUSPNMX
\$30	atvfett	ATVFETTU	ATVFETTO
\$31	atvmager	ATVMAGU	ATVMAGO
\$32	tpsvlssa	TPSVKMN	TPSVKMX

## LSU- sensor upstream catalyst

\$81	lamsisa	LAMSSAMN	LAMSSAMX
\$82	lamsosa	LAMSSAMN	LAMSSAMX
\$83	dynlsusa	DYNLSUSATU	DDYNLSUSATO
\$84	dlahisa	DLAHISATU	DLAHISATO

## Nernst- sensor downstream catalyst

Test ID	test value	min. Limit	max. Limit
\$01	usrhkshj	-	-
\$02	usrhkshj	-	-
\$07	usmnshn	USMNSHMN	USMNSHMX
\$08	usmxshn	USMXSHMN	USMXSHMX

The test IDs \$00, \$20, \$40, \$60, \$80, \$A0, \$C0 and \$E0 are used for the output management.

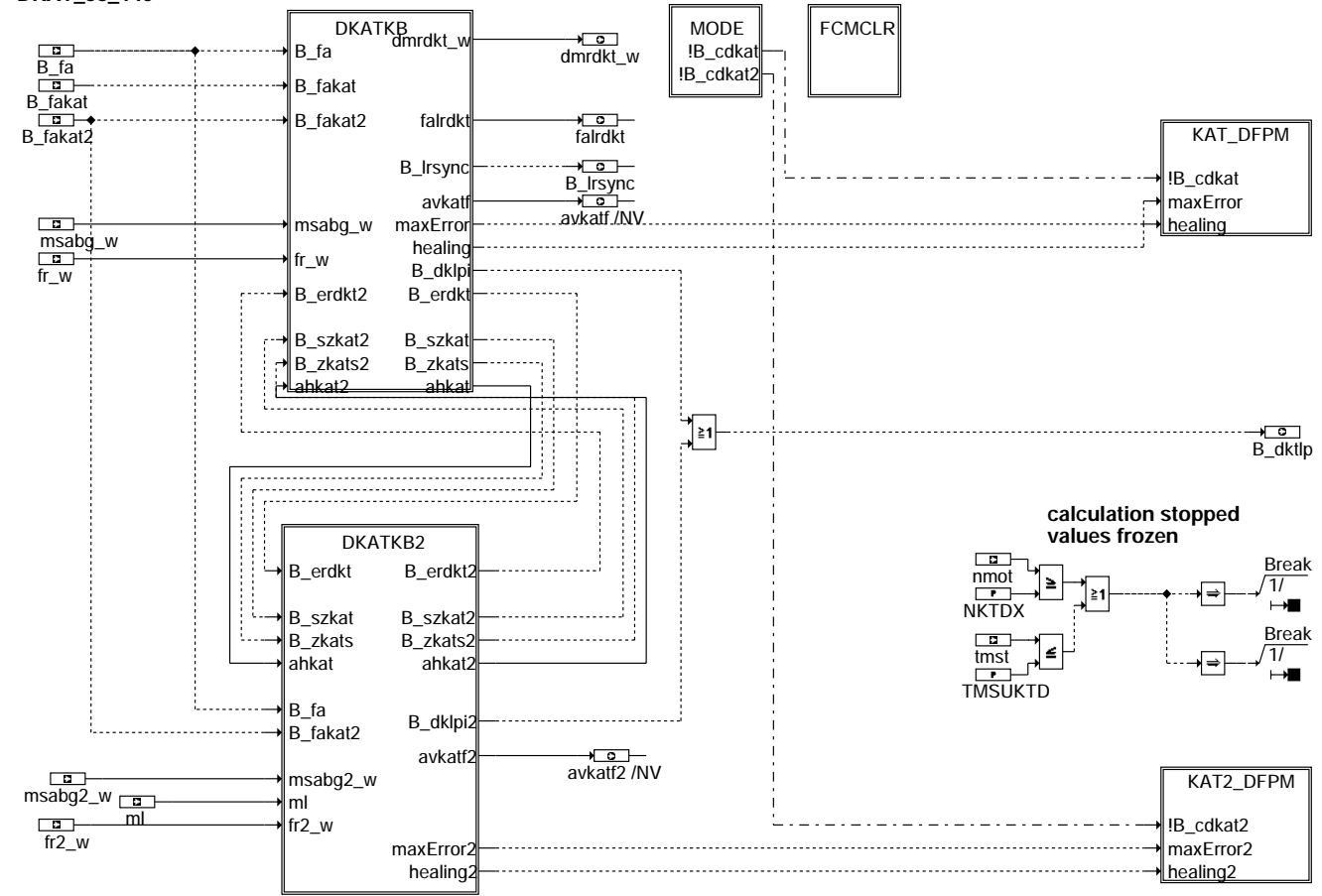


## DKAT 58.140 Diagnosis; catalyst conversion

### FDEF DKAT 58.140 Function definition

DKAT : Katalysatorüberwachungsfunktion Bank 1 und 2

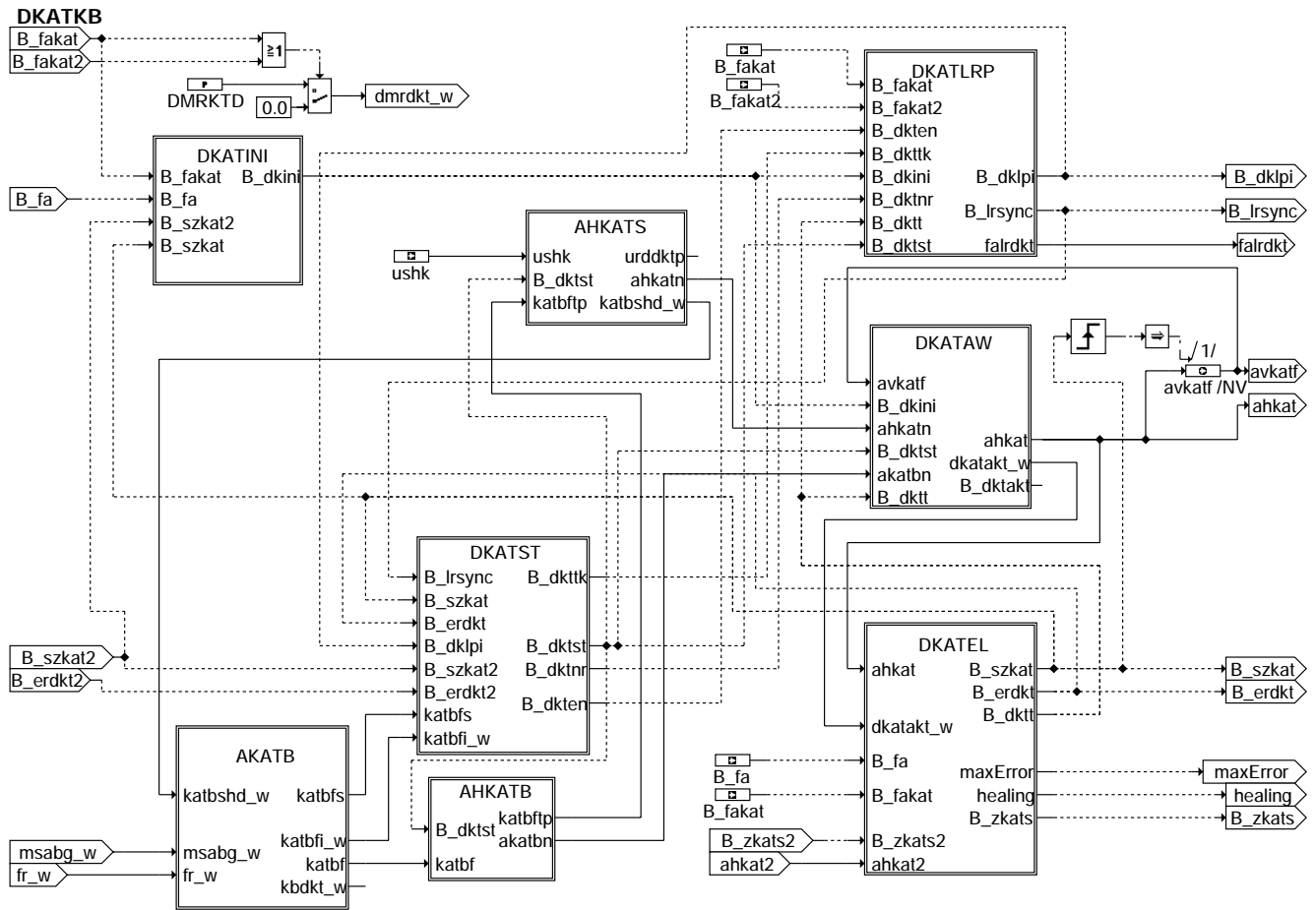
#### DKAT\_58\_140



dkat-main

dkat-main

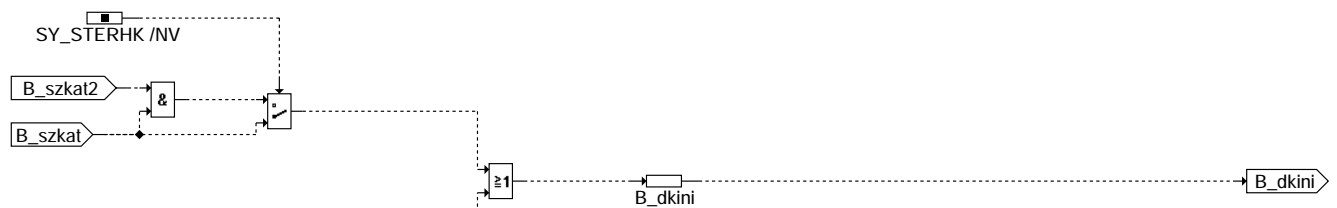
DKATKB : Katalysatorüberwachungsfunktion Bank 1



**dkat-dkatkb**

DKATINI : Initialisierung Bank 1

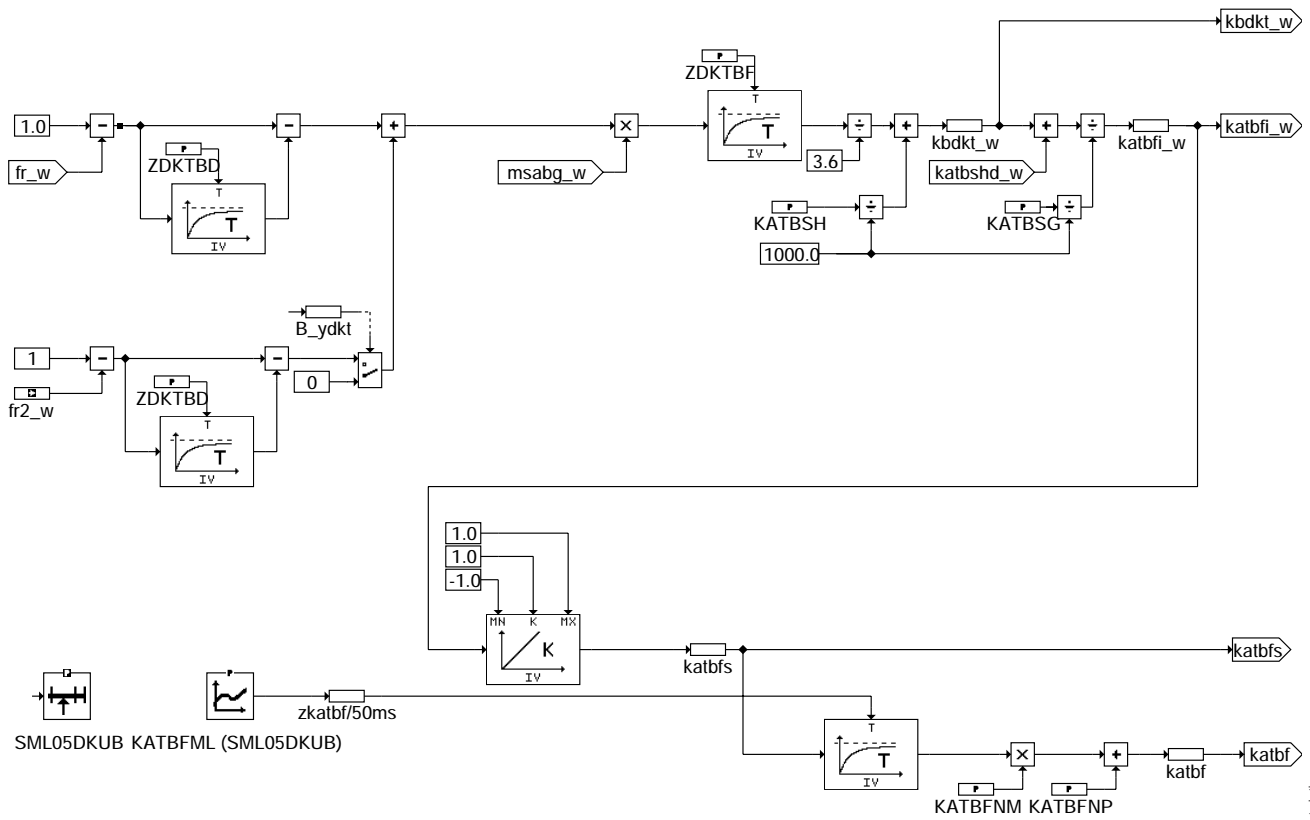
**DKATINI**



**dkat-dkatini**

AKATB : Aufbereitung des Katbelastungssignales Bank 1

## AKATB

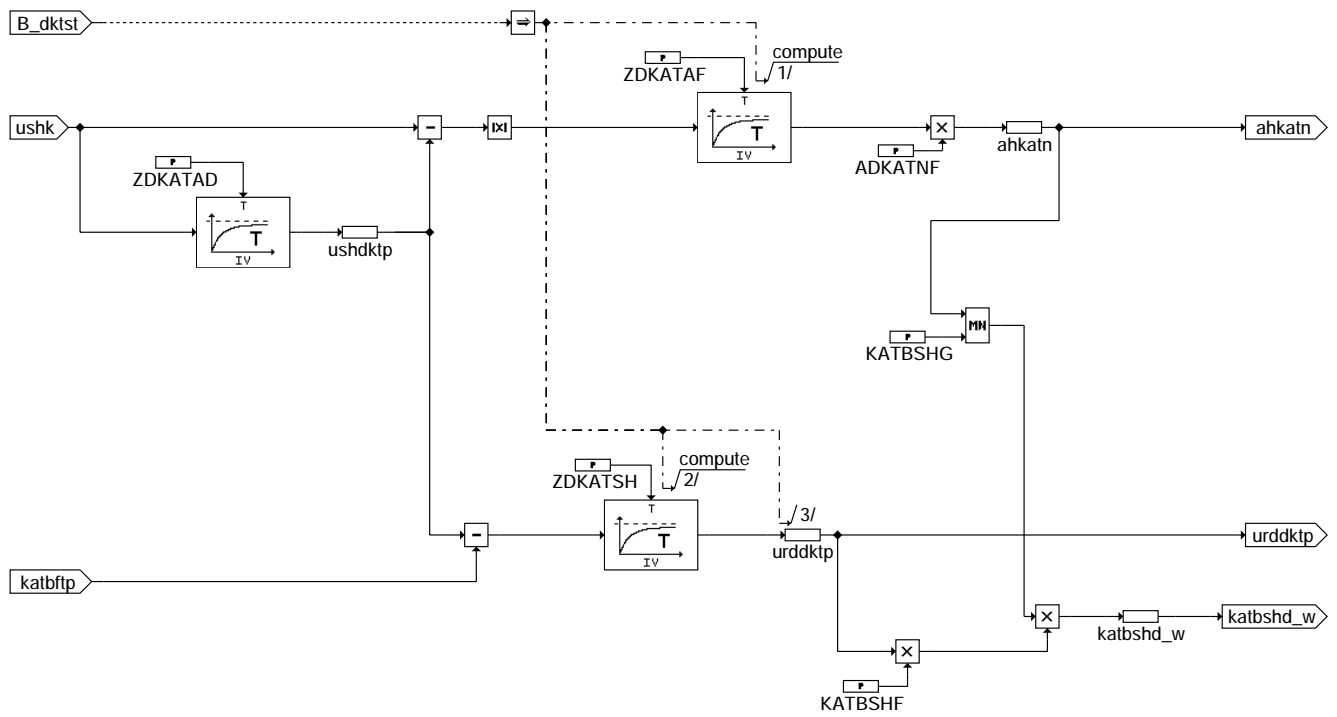


dkat-akatb

## dkat-akatb

AHKATS : Amplitudenaufbereitung in Abhängigkeit von der Sondenspannung Bank 1

## AHKATS

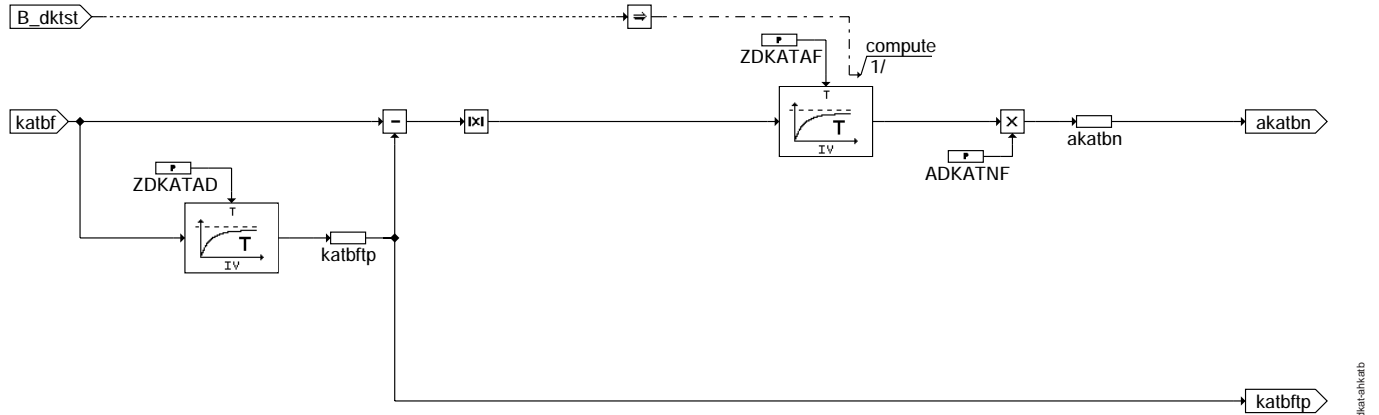


dkat-ahkats

## dkat-ahkats

AHKATB : Amplitudenaufbereitung in Abhängigkeit vom Katbelastungssignal Bank 1

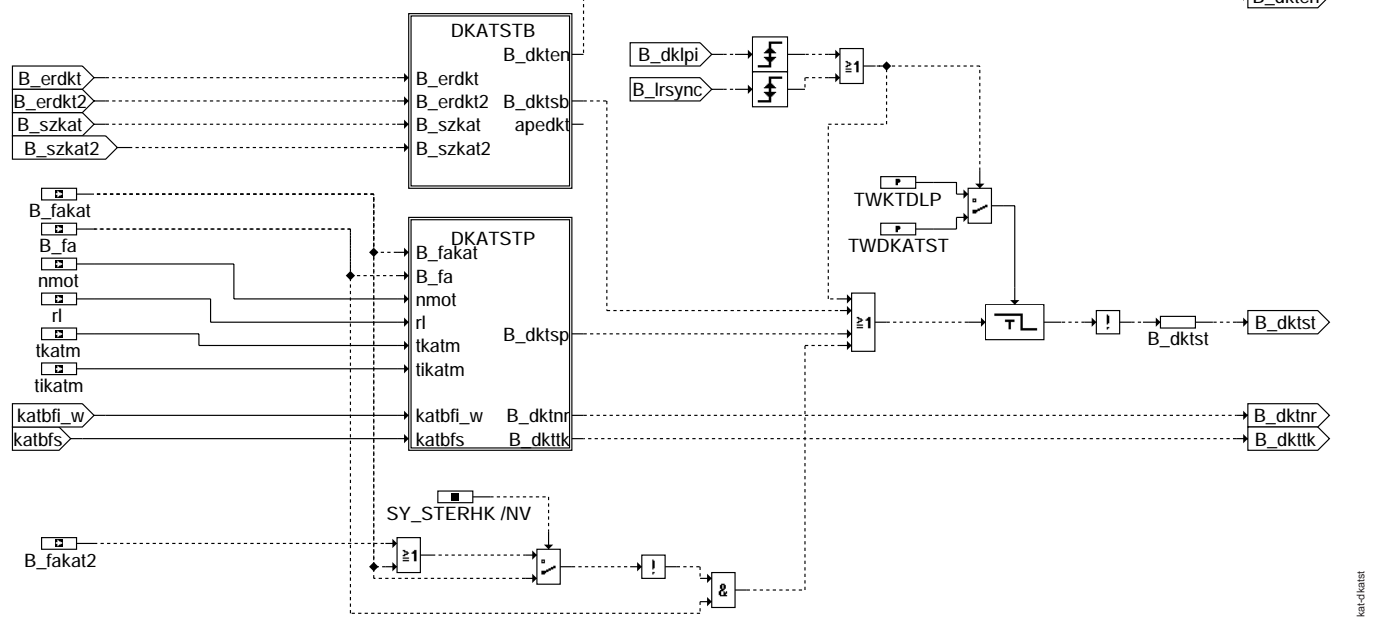
### AHKATB



### dkat-ahkatb

DKATST : Aufbereitung der Stoppbedingung Bank 1

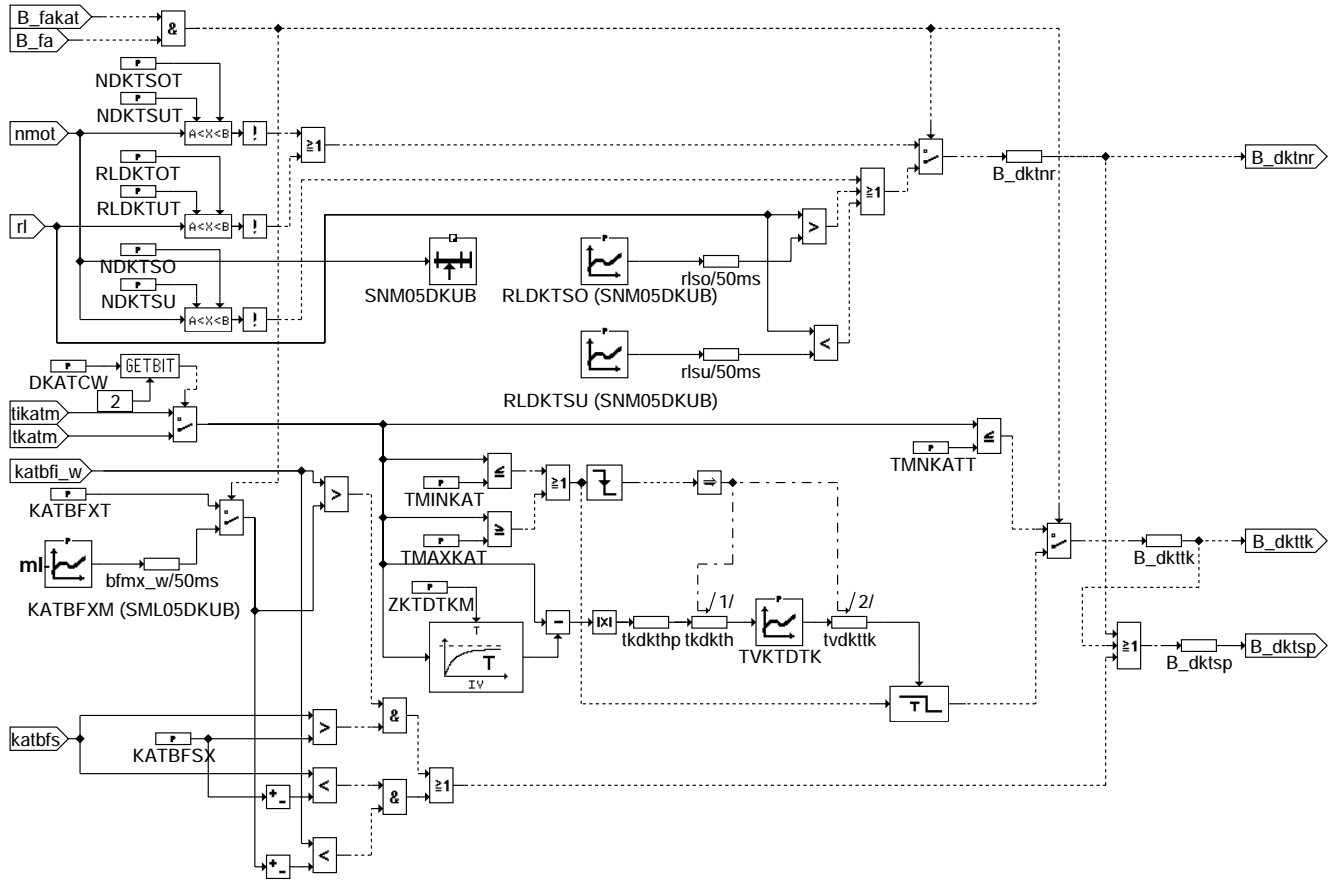
### DKATST



### dkat-dkatst

DKATSTP : Physikalische Stoppkriterien Bank 1

## DKATSTP



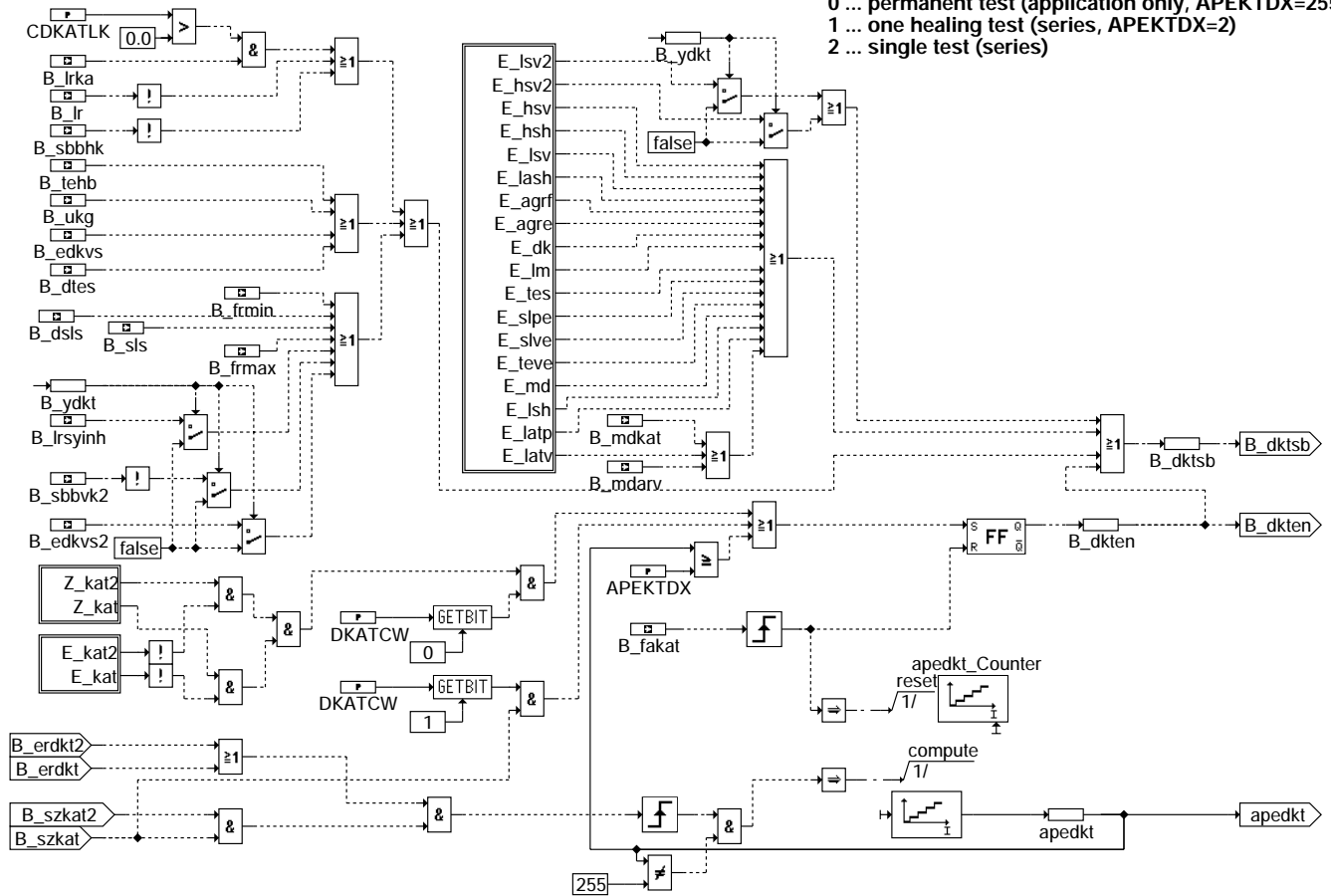
dkat-dkatstp

dkat-dkatstp



DKATSTB : Bankspezifische Stoppkriterien Bank 1

### DKATSTB



### DKATCW:

- 0 ... permanent test (application only, APEKTDX=255)
- 1 ... one healing test (series, APEKTDX=2)
- 2 ... single test (series)

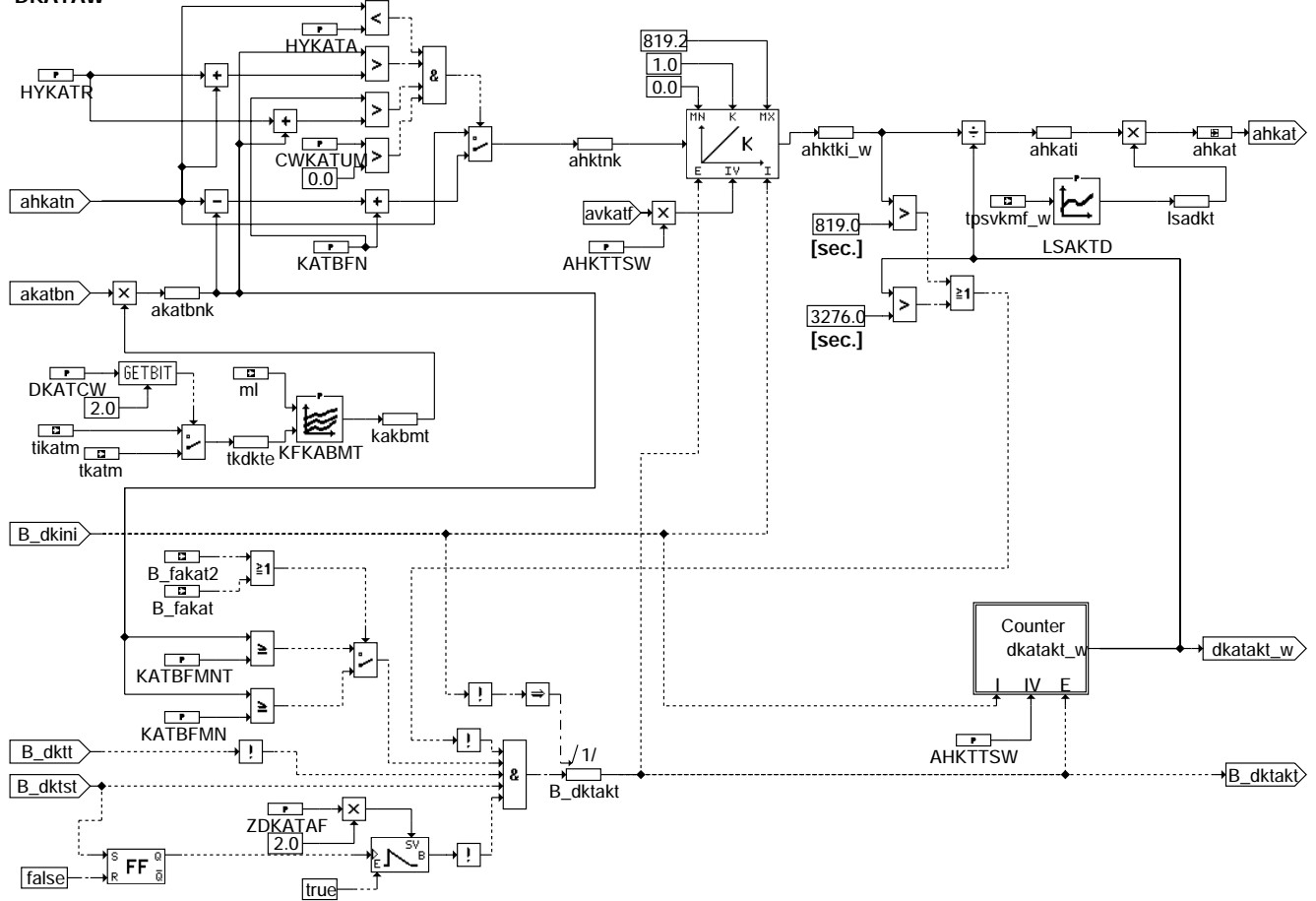
dkat-dkatstb

dkat-dkatstb



DKATAW : Signalauswertung Bank 1

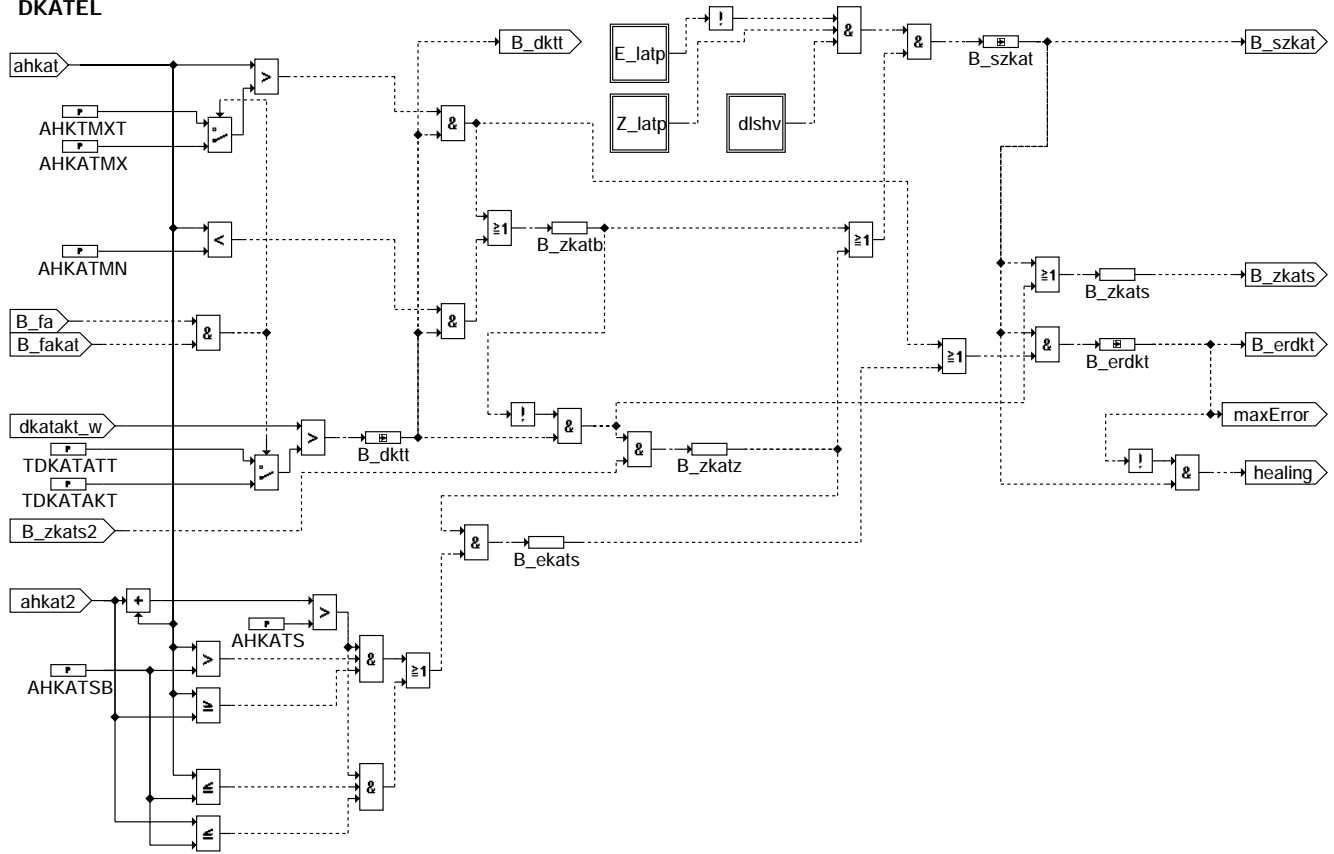
## DKATAW



## dkat-dkataw

DKATEL : Setzen der Error- und Zyklusflags Bank 1

## DKATEL

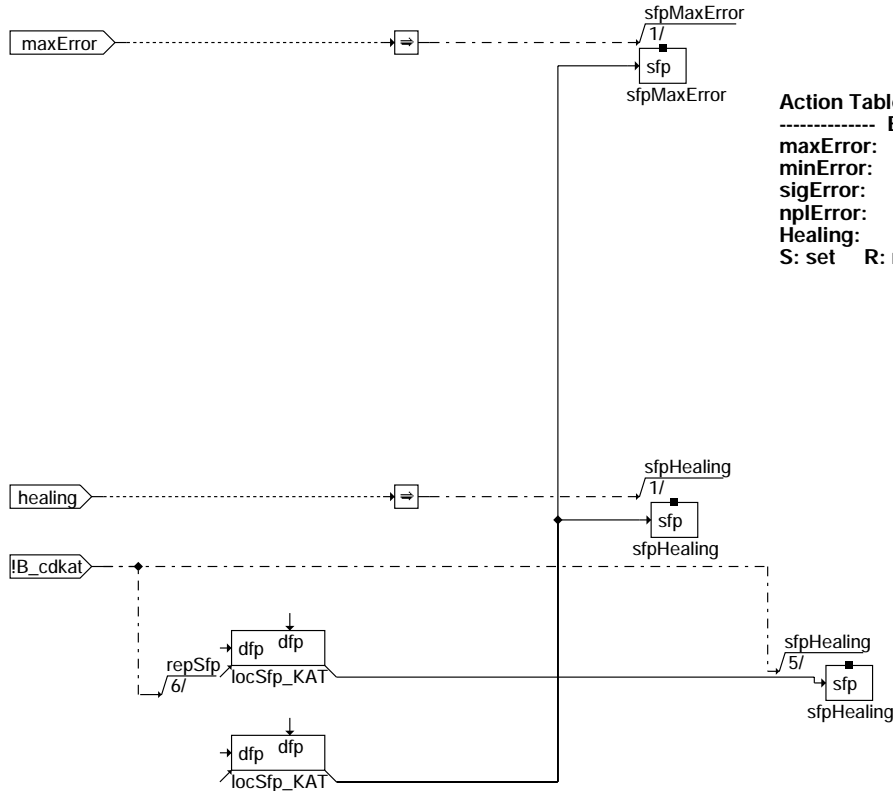


Origin of B\_cdkat: see %Prokon  
(CDKAT = 0: B\_cdkat := False  
CDKAT = 1: B\_cdkat := True)

dkat-dkateL

dkat-dkateL



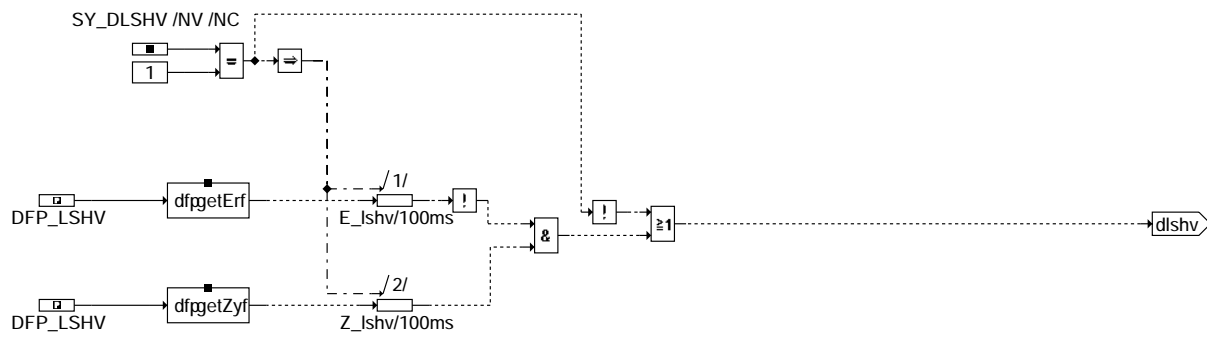


**Action Table for fault path \* in DFPM:**

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	S	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
npIError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

S: set R: reset

**dkat-kat-dfpm**

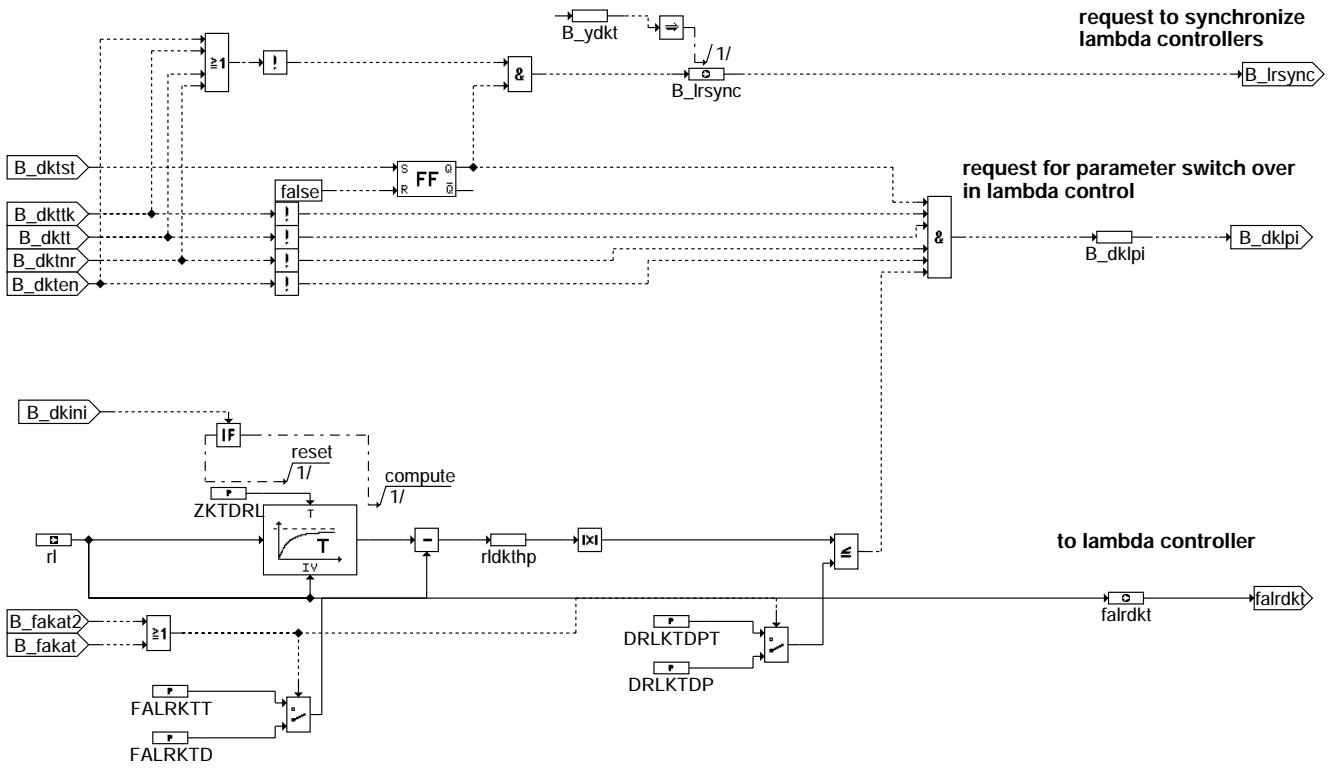


**dkat-dlshv**

dkat-kat-dfpm

dkat-dlshv

## DKATLRP



### Parameters for lambda control

#### dkat-dkatlrp

DKATLRP: Parameter zur Umschaltung der Lambdaregelungsamplitude

### ABK DKAT 58.140 Abbreviations

The following values are "describing values" i.e. they are no RAM cells.

B\_avkct(2)... condition initialize avkatf(2)  
B\_erdkt ... catalyst diagnosis error detected (bank1)  
B\_erdkt2... catalyst diagnosis error detected (bank2)

Parameter	Source-X	Source-Y	Type	Description
ADKATNF			FW	scaling factor for signal amplitude of the sensor resp. of the catalyst stress
AHKATMN			FW	threshold value catalyst good, AHKAT < AHKATMN
AHKATMX			FW	threshold value catalyst defect, AHKAT > AHKATMX
AHKATS			FW	threshold value for sum AHKAT,AHKAT2 (stereo)
AHKATSB			FW	threshold value for error of adding range (stereo)
AHKTMXT			FW	threshold value catalyst defect at tester's request
AHKTTSW			FW	setting value for timer in signal evaluation
APEKTDX			FW	max. number of tests with error result
AVKATFS			FW	setting value for AVKATF in case of powerfail
CDCKAT	BLOKNR		KL	code word CARB: catalyst conversion
CDCKAT2	BLOKNR		KL	code word CARB: catalyst conversion, cyl.row 2
CDKATLK			FW	code word for B_lrka active
CDKKAT			FW	code word customer: catalyst conversion
CDKKAT2			FW	Code word customer: Catalyst conversion (Bank 2)
CDTKAT			FW	code word tester: catalyst deteriorated [040]
CDTKAT2			FW	code word tester: catalyst conversion, cyl.row 2 [045]
CLAKAT			FW	Error class: catalyst
CLAKAT2			FW	Error class: catalyst bank 2
CWKATUM			FW	code word for switch-over in the catalyst diagnosis
DKATCW			FW	single run resp. initialization of the DKAT function
DMRKTD			FW	torque reserve for catalyst monitoring
DRLKTDPT			FW	Threshold for engine load change
DRLKTD			FW	Threshold for engine load change at tester's request
FALRKTD			FW	amplification factor for amplitude of lambda controller
FALRKTT			FW	amplification factor for amplitude of lambda controller at tester mode
HYKATA			FW	Absolute hysteresis, cat. monitoring
HYKATR			FW	Reactive hysteresis, cat. monitoring
KATBFML	ML		KL	filter time constant for signal attenuation in catalyst stress
KATBFML2	ML		KL	filter-time constant for signal attenuation in catalyst stress (assymmetrical)
KATBFMN			FW	threshold value for small catalyst stress
KATBFMNT			FW	threshold value for small catalyst stress at tester's request
KATBFN			FW	standardized mean value of the sensor amplitude



Parameter	Source-X	Source-Y	Type	Description
KATBFNM			FW	scaling factor multiplicative for catalyst stress
KATBFNP			FW	scaling factor additive for catalyst stress
KATBFSX			FW	maximum integrator value for stop condition
KATBFXM	ML		KL	max. catalyst load threshold for stop condition
KATBFXT			FW	max. catalyst load threshold for stop condition, tester mode
KATBSG			FW	catalyst storage value for catalyst stress
KATBSH			FW	offset for lambda control slightly in the rich area
KATBSHF			FW	amplification factor for difference of mean values of the O2/S
KATBSHG			FW	limitation factor of model lambda-offset due to sensor mean values
KFKABMT	ML	TKDKTE2	KF	Map for correction of calculated amplitude, dependent on ml and cat. temperature
LSAKTD	TPSVKMF2_W		KL	Impact of slow front sensor on cat. monitoring
NDKTSO			FW	upper engine speed limit for DKAT-active
NDKTSOT			FW	upper engine speed limit for function request
NDKTSU			FW	lower engine speed limit for DKAT-active
NDKTSUT			FW	lower engine speed limit for function request
NKTDX			FW	Maximum speed for DKAT calculation
RLDKTOT			FW	upper load limit for function request
RLDKTSO	NMOT		KL	upper load characteristic line for DKAT-active
RLDKTSU	NMOT		KL	lower load characteristic line for DKAT-active
RLDKTUT			FW	lower load limit for function request
SML05DKUB	ML		SV (REF)	base point distribution air mass
SNM05DKUB	NMOT		SV (REF)	base point distribution nmot
SY_DLSHV			SYS (REF)	Sys. constant condition %DLSHV (sensor exchange behind KAT) existent
SY_SLS			SYS (REF)	system constant for engines with secondary air pump
SY_STERHK			SYS (REF)	system parameter condition stereo downstream catalyst
SY_STERSY			SYS (REF)	System constant Condition stereo Lambda control symmetrical
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TDKATAKT			FW	threshold value cycle finished if active monitoring time > TDKATAKT
TDKATATT			FW	threshold value cycle finished for function request
TMAXKAT			FW	maximum catalyst temp. for active diagnosis
TMINKAT			FW	minimum catalyst temperature for monitoring
TMNKATT			FW	minimum catalyst temperature for monitoring during tester mode
TMSUKTD			FW	minimum engine start temp. for monitoring
TSFKAT			FW	fault active time: catalyst conversion rate
TSFKAT2			FW	fault active time: catalyst conversion rate, bank 2
TVKTDTK	TKDKTH2		KL	temperature dependant delay time for catalyst monitoring
TWDKATST			FW	waiting time after stop condition for filter and integrator
TWKTDLP			FW	delay time after parameter switch over in lambda control
ZDKATAD			FW	filter time constant of the differentiator for signal amplitude
ZDKATAF			FW	time constant "absolute value filter" for signal amplitude
ZDKATSH			FW	time constant low pass filter, mean sensor values
ZDKTBD			FW	time constant of the differentiator for RF-alternating component
ZDKTBF			FW	time constant for gas mixing procedure in front of catalyst
ZKTDRL			FW	time constant low pass filter, engine load
ZKTDTKM			FW	loss pass filter time constant for tkatm filtering

Variable	Source	Type	Description
AHKAT	DKAT	LOK	mean value of the amplitude sensor signal behind catalyst corrected by KB
AHKAT2	DKAT	LOK	mean value of the amplitude sensor signal behind catalyst corr. by KB (2.bank)
AHKATI	DKAT	LOK	mean value of the amplitude sensor signal behind catalyst corrected by KB,intern
AHKATI2	DKAT	LOK	mean value of the amplitude sensor signal behind catalyst corrected by KB,intern
AHKATN	DKAT	LOK	amplitude sensor signal behind catalyst standardized
AHKATN2	DKAT	LOK	amplitude sensor signal behind catalyst standardized
AHKTI2_W	DKAT	LOK	amplitude sensor signal behind catalyst corrected and integrated
AHKTK1_W	DKAT	LOK	amplitude sensor signal behind catalyst corrected and integrated
AHKTNK	DKAT	LOK	corrected sensor signal amplitude standardized
AHKTNK2	DKAT	LOK	corrected sensor signal amplitude standardized (stereo 2.bank)
AKATBN	DKAT	LOK	amplitude of the catalyst stress signal
AKATBN2	DKAT	LOK	amplitude of the catalyst stress signal (stereo 2.bank)
AKATBNK	DKAT	LOK	corrected amplitude of the catalyst stress signal
AKATBNK2	DKAT	LOK	corrected amplitude of the catalyst stress signal, bank2
APEDKT	DKAT	LOK	number of tests with error-result
APEDKT2	DKAT	LOK	number of tests with error-result (bank2)
AVKATF	DKAT	AUS	amplitude ratio laafh/laafv strained
AVKATF2	DKAT	AUS	amplitude ratio laafh/laafv strained bank2
BLOKNR		EIN	DAMOS source for block number
B_BEKAT	DKAT	AUS	condition cat monitoring request
B_BEKAT2	DKAT	AUS	condition cat monitoring request, bank2
B_BKKAT	DKAT	AUS	Condition backup value for catalyst
B_BKKAT2	DKAT	AUS	Condition backup value for catalyst, bank2
B_CDKAT	PROKON	EIN	function active per codeword CDKAT
B_CLKAT		EIN	condition clear fault path DKAT
B_CLKAT2		EIN	condition clear failure path DKAT (stereo)
B_DKINI	DKAT	LOK	condition for initialize DKAT function
B_DKINI2	DKAT	LOK	condition for initialize DKAT function (stereo 2.bank)
B_DKLP1	DKAT	LOK	internal request of param. switch over in lambda control
B_DKLP12	DKAT	LOK	internal request of param. switch over in lambda control, bank2
B_DKTAKT	DKAT	LOK	catalyst monitoring active
B_DKTAKT2	DKAT	LOK	catalyst monitoring active (bank2)
B_DKTEN	DKAT	LOK	DKAT no longer active for this trip
B_DKTEN2	DKAT	LOK	DKAT no longer active for this trip (bank2)



Variable	Source	Type	Description
B_DKTLF	DKAT	AUS	Request of parameter switch over in lambda control
B_DKTNR	DKAT	LOK	speed-/load range left
B_DKTNR2	DKAT	LOK	speed-/load range left, bank2
B_DKTPB2	DKAT	LOK	DKAT: testing finished, bank2
B_DKTSB	DKAT	LOK	bank-specific stop condition
B_DKTSB2	DKAT	LOK	bank-specific stop condition (stereo 2.bank)
B_DKTSP	DKAT	LOK	physical stop condition
B_DKTSP2	DKAT	LOK	physical stop condition (stereo 2.bank)
B_DKTST	DKAT	LOK	DKAT function is stopped (B_dktst=FALSE)
B_DKTST2	DKAT	LOK	DKAT function is stopped (B_dktst=FALSE, stereo 2.bank)
B_DKTT	DKAT	LOK	DKAT active time over
B_DKTT2	DKAT	LOK	DKAT active time over, bank2
B_DKTTK	DKAT	LOK	Catalyst monitoring stopped due to catalyst temperature
B_DKTTK2	DKAT	LOK	Catalyst monitoring stopped due to catalyst temperature
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DTES	GKRA	EIN	Condition for active diagnosis of canister purge system
B_EDKVS	DKVS	EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS	EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_EKATS	DKAT	LOK	added-up error for MODE 6
B_EKATS2	DKAT	LOK	added-up error for MODE 6 (stereo 2.bank)
B_ERDKT	DKAT	LOK	Internal fault at catalyst diagnosis
B_ERDKT2	DKAT	LOK	Internal fault at catalyst diagnosis (bank2)
B_FA		EIN	condition general function request
B_FAKAT		EIN	condition function request catalyst monitoring
B_FAKAT2		EIN	condition function request catalyst monitoring (stereo 2.Bank)
B_FRMAX	LR	EIN	lambda control sets bit when lambda controller reaches its limit FRMAX
B_FRMAX2	LR	EIN	lambda control sets bit when lambda control reaches it limit FRMAX, bank2
B_FRMIN	LR	EIN	lambda control sets bit when lambda controller reaches its limit FRMIN
B_FRMIN2	LR	EIN	lambda control sets bit when lambda control reaches its limit FRMIN, bank2
B_FTKAT	DKAT	AUS	Condition fault entry by tester for catalyst
B_FTKAT2	DKAT	AUS	Condition fault entry by tester for catalyst, bank2
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRKA	LRKA	EIN	condition for neutralization of catalyst oxygen storage
B_LRKA2	LRKA	EIN	condition for neutralization of catalyst oxygen storage, cylinder row 2
B_LRSYINH	LR	EIN	Condition fr_b1-/fr_b2-synchronization due to min/max limiter disabled
B_LRSYNC	DKAT	AUS	Condition fr_b1-/fr_b2-synchronization requested
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_MDKAT	DMDMIL	EIN	cat. damaging misfire rate exceeded (for deactivation of other functions)
B_MNKAT	DKAT	AUS	condition: min-error catalyst detected
B_MNKAT2	DKAT	AUS	Fault type min.: Catalysator 2
B_MXKAT	DKAT	AUS	condition upper plausibility threshold exceeded
B_MXKAT2	DKAT	AUS	condition upper plausibility threshold exceeded (stereo)
B_NPKAT	DKAT	AUS	condition for fault type "unplausible signal" detected (Catalyst)
B_NPKAT2	DKAT	AUS	condition for fault type "unplausible signal" detected (Catalyst)2
B_PWF		EIN	Condition for powerfail
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_SBBVK2	DLSV	EIN	condition oxygen sensor upstream cat. bank2 ready for operation
B_SIKAT	DKAT	AUS	fault type 'signal missing' for DKAT detected
B_SIKAT2	DKAT	AUS	fault type 'signal missing' for DKAT 2 detected
B_SLS	AK	EIN	Condition for active secondary air
B_SZKAT	DKAT	LOK	cycle time and error one bank run out
B_SZKAT2	DKAT	LOK	cycle time and error bank2 run out
B_TEHB	TEB	EIN	condition for canister purge system with high canister load
B_UJKG	ESUK	EIN	condition transient control activated
B_VEKAT	DKAT	AUS	error suspected in catalytic-converter diagnosis
B_VEKAT2	DKAT	AUS	error suspected in catalytic-converter diagnosis, bank 2
B_YDKT	DKAT	LOK	Exhaust system with Y configuration (two pre cats, one main cat)
B_ZKATB	DKAT	LOK	bank-specific cycle time for MODE 6
B_ZKATB2	DKAT	LOK	bank-specific cycle time for MODE 6 (stereo 2.bank)
B_ZKATS	DKAT	LOK	cycle time for one bank run out
B_ZKATS2	DKAT	LOK	cycle time for 2. bank run out
B_ZKATZ	DKAT	LOK	condition for added-up error in MODE 6
B_ZKATZ2	DKAT	LOK	condition for added-up error in MODE 6 (stereo 2.bank)
DFP_AGRE	DKAT	DOK	ECU int. fault path no.: EKR power stage
DFP_AGRF	DKAT	DOK	ECU int. fault path no.: partial pressure EGR
DFP_DK	DKAT	DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_HSH	DKAT	DOK	ECU int. fault path no.: lambda sensor heating downstream cat.
DFP_HSH2	DKAT	DOK	ECU int. fault path no.: lambda sensor heating downstream cat. bank2
DFP_HSV	DKAT	DOK	ECU int. fault path no.: lambda sensor heating upstream cat.
DFP_HSV2	DKAT	DOK	ECU int. fault path no.: lambda sensor heating upstream cat., bank2
DFP_KAT	DKAT	DOK	internal fault path number: catalyst monitoring
DFP_KAT2	DKAT	DOK	internal failure path number: catalyst monitoring, bank2
DFP_LASH	DKAT	DOK	ECU int. fault path no.: lambda sensor aging downstream Cat.
DFP_LASH2	DKAT	DOK	ECU int. fault path no.: lambda sensor aging downstream Cat. bank 2
DFP_LATP	DKAT	DOK	ECU int. fault path no.: diagnosis lambda sensor upstream cat
DFP_LATP2	DKAT	DOK	ECU int. fault path no.: diagnosis lambda sensor upstram cat bank2
DFP_LATV	DKAT	DOK	ECU int. fault path no.: diagnosis lambda sensor upstream cat
DFP_LATV2	DKAT	DOK	ECU int. fault path no.: diagnosis lambda sensor upstream cat bank2
DFP_LM	DKAT	DOK	ECU-internal fault path no.: main-load sensor
DFP_LSH	DKAT	DOK	ECU int. fault path no.: lambda sensor downstream cat.



Variable	Source	Type	Description
DFP_LSH2	DKAT	DOK	ECU int. fault path no.: lambda sensor downstream cat. bank2
DFP_LSHV	DKAT	DOK	ECU int. fault path no.: lambda sensor exchange downstream Cat.
DFP_LSV	DKAT	DOK	ECU int. fault path no.: electrical diagnosis for lambda sensor upstream cat.
DFP_LSV2	DKAT	DOK	ECU int. fault path no.: electr. diagnos. for lambda sensor upstream cat. bank 2
DFP_MD	DKAT	DOK	ECU int. fault path no. misfire, multiple
DFP_SLPE	DKAT	DOK	Internal fault path number: secondary air pump power stage
DFP_SLVE	DKAT	DOK	Internal fault path number: secondary air valve power stage
DFP_TES	DKAT	DOK	Internal error path number evap system monitoring, pcv Struck open
DFP_TEVE	DKAT	DOK	Internal fault path number: canister purge valve power stage
DKATAKT2_W	DKAT	LOK	active monitoring time for DKAT (stereo 2.bank)
DKATAKT_W	DKAT	LOK	active monitoring time for DKAT
DMRDKT_W	DKAT	AUS	torque reserve for catalyst monitoring
E_AGRE		EIN	error flag: EGR power stage monitoring
E_AGRF		EIN	error flag: EGR flow monitoring
E_DK	DDVE	EIN	Error flag: throttle position sensor
E_HSH	DHLSHK	EIN	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK	EIN	error flag: lambda sensor heating downstream cat on the right
E_HSV	DHLSVK	EIN	error flag: lambda sensor heating upstream cat
E_HSV2	DHLSVK	EIN	error flag: lambda sensor heating upstream cat on the right
E_KAT	DKAT	AUS	error flag: catalyst conversion
E_KAT2	DKAT	AUS	error flag: catalyst conversion (cylinder row 2)
E_LASH	DLSAHK	EIN	error flag: lambda sensor aging downstream cat
E_LASH2	DLSAHK	EIN	error flag: lambda sensor aging downstream cat (cylinder row 2)
E_LATP	DLSA	EIN	error flag: lambda sensor aging tp
E_LATP2	DLSA	EIN	error flag: lambda sensor aging tp (cylinder row 2)
E_LATV	DLSA	EIN	error flag: lambda sensor aging tv
E_LATV2	DLSA	EIN	error flag: lambda sensor aging tv (cylinder row 2)
E_LM	EGFE	EIN	Error flag: main load sensor
E_LSH	DLSH	EIN	error flag: lambda sensor downstream cat
E_LSH2	DLSH	EIN	Errorflag: Lambda-Sensor downstream bank2
E_LSHV		EIN	error flag: lambda sensor exchange downstream cat
E_LSV	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_LSV2	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_MD	DMDMIL	EIN	Error flag: misfire, multiple
E_SLPE		EIN	error flag: secondary air pump (power stage)
E_SLVE		EIN	error flag: secondary air valve (power stage)
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
FALRDKT	DKAT	AUS	Request form cat monitoring: modify lambda controller amplitude
FR2_W	LR	EIN	Lambda controller output (word)
FR_W	LR	EIN	Lambda controller output (word)
KAKBMT	DKAT	LOK	Correction value for the modelled amplitude of the rear sensor
KAKBMT2	DKAT	LOK	Correction value for the modelled amplitude of the rear sensor, bank2
KATBF	DKAT	LOK	signal after memory standardized comparable to ushk
KATBF2	DKAT	LOK	signal downstream of accumulator, standardized, comp. with ushk2 (stereo, bank 2)
KATBF12_W	DKAT	LOK	amount of oxygen upstream of accumulator (catalyzer model, stereo, bank 2)
KATBFL_W	DKAT	LOK	amount of oxygen upstream of accumulator (catalyzer model)
KATBFS	DKAT	LOK	signal downstream of accumulator (catalyzer model)
KATBFS2	DKAT	LOK	signal downstream of accumulator (catalyzer model, stereo, bank 2)
KATBFTP	DKAT	LOK	signal downstream of accumulator, standardized, low-pass filtered
KATBFTP2	DKAT	LOK	signal downstream of accumulator, standardized, low-pass filtered (bank 2)
KATBSHD2_W	DKAT	LOK	signal for rich-shift of the catalyst model (bank2)
KATBSHD_W	DKAT	LOK	signal for rich-shift of the catalyst model
KBDKT2_W	DKAT	LOK	catalyst load signal, bank2
KBDKT_W	DKAT	LOK	catalyst load signal
LSADKT	DKAT	LOK	Correction value (slow front sensor) of cat. monitoring result
ML	SWADAP	EIN	air mass flow
MSABG2_W	BGMSABG	EIN	exhaust gas mass flow filtered (Word), bank 2
MSABG_W	BGMSABG	EIN	exhaust gas mass flow filtered (Word), bank 1
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RLDKTHP	DKAT	LOK	High pass filteres engine load signal
RLDKTHP2	DKAT	LOK	High pass filteres engine load signal, bank2
SFPKAT	DKAT	AUS	Status fault path: catalyst monitoring
SFPKAT2	DKAT	AUS	Status fault path: catalyst monitoring bank 2
TC6KATA	DKAT	AUS	Number of output codes SCAN-Tool mode6 from catalyst diagnosis
TC6KATC	DKAT	AUS	output code SCAN-tool mode 6 from catalyst diagnosis
TC6KATC2	DKAT	AUS	output code SCAN-tool mode 6 from catalyst diagnosis, bank 2
TC6KATS	DKAT	AUS	output threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATS2	DKAT	AUS	output threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATW	DKAT	AUS	output test threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATW2	DKAT	AUS	output test threshold SCAN-tool mode 6 from catalyst diagnosis, bank 2
TIKATM	ATM	EIN	exhaust gas temperature in catalyst (modelled)
TIKATM2	ATM	EIN	exhaust gas temperature in catalyst (modelled) bank2
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TKDKTE	DKAT	LOK	input temperature for catalyst monitoring
TKDKTE2	DKAT	LOK	input temperature for catalyst monitoring, bank2
TKDKTH	DKAT	LOK	highpass filtered catalyst temperature after sample&hold
TKDKTH2	DKAT	LOK	highpass filtered catalyst temperature after sample&hold
TKDKTHP	DKAT	LOK	high pass filtered catalyst temperature
TKDKTHP2	DKAT	LOK	high pass filtered catalyst temperature



Variable	Source	Type	Description
TMST	GGTFM	EIN	engine temperature at start
TPSVKMF2_W	DLSA	EIN	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (word)
TPSVKMF_W	DLSA	EIN	filtered cycle duration of sensor signal upstream cat. (word)
TVDKTTK	DKAT	LOK	temperature dependent delay time
TVDKTTK2	DKAT	LOK	temperature dependent delay time
URDDKTP	DKAT	LOK	difference of sensor mean values, low pass filtered
URDDKTP2	DKAT	LOK	difference of sensor mean values, low pass filtered, bank2
USHDKTP	DKAT	LOK	output voltage oxygen sensor downstream catalyst, low pass filtered
USHDKTP2	DKAT	LOK	output voltage oxygen sensor downstream catalyst, low pass filtered
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
Z_KAT	DKAT	AUS	cycle flag of catalyst conversion
Z_KAT2	DKAT	AUS	cycle flag: catalyst conversion (2nd bank)
Z_LATP	DLSA	EIN	cycle flag of lambda sensor aging tp
Z_LATP2	DLSA	EIN	cycle flag of lambda sensor aging tp (cylinder row 2)
Z_LSHV		EIN	cycle flag of lambda sensor exchange downstream cat

### FW DKAT 58.140 Fixed Values

Parameter	Value	Description
ADKATNF		scaling factor for signal amplitude of the sensor resp. of the catalyst stress
AHKATMN		threshold value catalyst good, AHKAT < AHKATMN
AHKATMX		threshold value catalyst defect, AHKAT > AHKATMX
AHKATS		threshold value for sum AHKAT,AHKAT2 (stereo)
AHKATSB		threshold value for error of adding range (stereo)
AHKATMX2		threshold value catalyst defect at tester's request
AHKTTSW		setting value for timer in signal evaluation
APEKTDX		max. number of tests with error result
AVKATFS		setting value for AVKATF in case of powerfail
CDKATLK		code word for B.Irka active
CDKKAT		code word customer: catalyst conversion
CDKKAT2		Code word customer: Catalyst conversion (Bank 2)
CDTKAT		code word tester: catalyst deteriorated [040]
CDTKAT2		code word tester: catalyst conversion, cyl.row 2 [045]
CLAKAT		Error class: catalyst
CLAKAT2		Error class: catalyst bank 2
CWKATUM		code word for switch-over in the catalyst diagnosis
DKATCW		single run resp. initialization of the DKAT function
DMRKT		torque reserve for catalyst monitoring
DRLKTD		Threshold for engine load change
DRLKTDPT		Threshold for engine load change at tester's request
FALRKTD		amplification factor for amplitude of lambda controller
FALRKTT		amplification factor for amplitude of lambda controller at tester mode
HYKATA		Absolute hysteresis, cat. monitoring
HYKATR		Reactive hysteresis, cat. monitoring
KATBFMN		threshold value for small catalyst stress
KATBFMNT		threshold value for small catalyst stress at tester's request
KATBFN		standardized mean value of the sensor amplitude
KATBFNM		scaling factor multiplicative for catalyst stress
KATBFNP		scaling factor additive for catalyst stress
KATBFSX		maximum integrator value for stop condition
KATBFXT		max. catalyst load threshold for stop condition, tester mode
KATBSG		catalyst storage value for catalyst stress
KATBSH		offset for lambda control slightly in the rich area
KATBSHF		amplification factor for difference of mean values of the O2/S
KATBSHG		limitation factor of model lambda-offset due to sensor mean values
NDKTSO		upper engine speed limit for DKAT-active
NDKTSOT		upper engine speed limit for function request
NDKTSU		lower engine speed limit for DKAT-active
NDKTSUT		lower engine speed limit for function request
NKTDX		Maximum speed for DKAT calculation
RLDKTOT		upper load limit for function request
RLDKTUT		lower load limit for function request
TDKATAKT		threshold value cycle finished if active monitoring time > TDKATAKT
TDKATATT		threshold value cycle finished for function request
TMAXKAT		maximum catalyst temp. for active diagnosis
TMINKAT		minimum catalyst temperature for monitoring
TMNKATT		minimum catalyst temperature for monitoring during tester mode
TMSUKTD		minimum engine start temp. for monitoring
TSFKAT		fault active time: catalyst conversion rate
TSFKAT2		fault active time: catalyst conversion rate, bank 2
TWDKATST		waiting time after stop condition for filter and integrator
TWKTDLP		delay time after parameter switch over in lambda control
ZDKATAD		filter time constant of the differentiator for signal amplitude
ZDKATAF		time constant "absolute value filter" for signal amplitude
ZDKATSH		time constant low pass filter, mean sensor values
ZDKTBD		time constant of the differentiator for RF-alternating component
ZDKTBF		time constant for gas mixing procedure in front of catalyst
ZKTDRL		time constant low pass filter, engine load
ZKTDTKM		loss pass filter time constant for tkatm filtering

**FB DKAT 58.140 Detailed description of function**

## Introduction :

The catalyst has the characteristics of storing oxygen. The oxygen stored during the lean phase is either completely or partially used during the rich phase. Due to aging or due to environmental influences the storage capability of the catalyst is reduced. In case of this aging the HC conversion is also reduced. According to OBDII requirements the HC emission in the FTP test may not exceed a given limit. The task of the catalyst monitoring function is to make a statement from the oxygen storage capability of the catalyst about the HC conversion in the FTP-test. By means of this procedure the oxygen storage capability is determined from the amplitude of the lambda sensor behind the catalyst. Since during non-steady state drive the storage capacity of the catalyst is at times taken up completely the function shall be protected against wrong conclusions by means of adequate measures.

## The catalyst conversion monitoring:

The amplitude of the lambda sensor behind the catalyst is strongly dependent on the alternating stress of the oxygen (deficiency / excess) in the catalyst. This catalyst stress may vary in different load ranges. So as to consider the working point influences a correcting function apart from the various stop criteria is introduced. The task of this function is, dependent on the manipulated variable of the lambda controller (fr-signal), to form an expectancy signal for the amplitude of the lambda sensor. The difference between the expectancy signal and the lambda sensor amplitude is integrated and standardized to the time. The standardized signal is a dimension for the aging of the catalyst. The monitoring is carried out in a single load-engine speed range. The structure of bank one and two is identical. Due to this only one bank was described. The differing signals were designated with index 2 for the second bank. The following blocks DKATAW2, DKATSTB2, DKATSTP2, DKATST2, AHKATB2, AHKTS2, AKATB2 are the same as those of bank 1 except for the index 2. So as to increase the overview these block diagrams were therefore omitted.

The catalyst conversion monitoring consists of the following blocks:

## Partial function block AKATB:

The task of this partial function is, dependent on the manipulated variable of the lambda controller and of the air mass throughput, to calculate a catalyst stress signal. For this the change of the fr-signal from the neutral position (phys. 1.0) is filtered with a high pass (formed from the low-pass filter and subtraction). This filtering is necessary to be independent of the position of the fr-signal.

In case of Y-configurations (two pre catalysts and one common main catalyst) the catalyst load is calculated by the sum of the catalyst loads of the two individual pre catalysts. The high-pass filtered signal is multiplied by the air mass throughput ml, which was converted to g/s. Thereafter it is filtered with a low pass. The low-pass filter is used for the gas mixing procedure. The output of the low-pass filter is added to the offset KATBSH and standardized to the catalyst storage value. This signal (katbfi\_w) is used for application purposes and for the formation of the stop criteria. The offset KATBSH is dependent on the control threshold of the pilot control and KATBSG is dependent on the catalyst volume of the borderline catalyst.

The catalyst was designed as integrator with limitation. The limitation was standardized to +-1. After the katbfi\_w-signal was integrated it is filtered through an air mass throughput-dependent low pass and standardized to the lambda sensor amplitude by means of a multiplying and an adding factor. The standardized signal katbf has a similar course to ushk. The output of the integrator is called katbfs and it is used for the formation of the physical stop criteria and for application purposes.

The time constant of the high-pass filter ZDKTBD should be chosen such that only the direct component of the fr-signal is filtered. The time constant of the gas mixing filter ZDKTBF lies between 0.05..0.2 sec. By this time constant the threshold values of the stop conditions are influenced.

The air mass-dependent time constant of the low-pass filter is realized via the characteristic line KATBFML (KATBFML2, bank2). In case of very air masses this filter generally has a larger time constant. For the given base points the time constants shall be adjusted so that the standardized katbf-signal shows the best possible match with the lambda sensor amplitude for the the designed borderline catalyst.

All filters and the integrator are reset to zero by B\_dkini=TRUE.

## Partial function block AHKATS :

By means of this function the alternating components of the ushk-signal are calculated by a high-pass filter (formed from low-pass filter and subtraction). Via the sum and the subsequent filtering the rectified mean value of the alternating components is obtained. The low-pass filter is stopped by the bit B\_dktst = FALSE. The output of the low-pass filter is multiplied by the factor ADKATNF so that on very old catalysts (washcoat only) ahkatn becomes = 1. The standardized signal ahkatn then complies to the avkat-signal from the filter procedure carried out so far.

Both filters are set to ZERO by the bit B\_dkini=TRUE.

The mean value of the oxygen sensors after catalyst is taken into account. This is performed by creating "katbshd" from the difference of the values of the rear sensor and the modelled rear sensor signal. This "katbshd" impacts the catalyst model.

## Partial function block AHKATB :

By means of this function the alternating components of the katbf-signal are calculated by a high-pass filter (formed from low-pass filter and subtraction). Via the sum and the subsequent filtering the rectified mean value of the alternating components is obtained. The low-pass filter is stopped by the bit B\_dktst = FALSE. The output of the low-pass filter is multiplied by the factor ADKATNF. The standardized signal akatbn is used as expectancy signal (set point).

Both filters are set to ZERO by the bit B\_dkini=TRUE.



Partial function block DKATAW :  
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First of all, the modelled amplitude akatbn is compensated with the correction factor kakbmt, in order to minimize the influence of air mass and corresponding catalyst temperature.

From the two signals ahkatn and akatbn a correcting signal ahktnk is formed for the evaluation of the catalyst conversion.

For this the difference between the ahkatn-signal and the akatbn-signal is formed. The difference is corrected by means of a straight line with a gradient of one. The straight line has the point of intersection KATBFN with the y-axis. The correcting signal ahktnk is integrated and thereafter divided by the time. The result (ahkat-signal) takes up a value between ZERO and one.

The integrator and the timer are definedly set during the initialization (B.dkini=TRUE). The setting values (avkatf\*AHKTTSW and AHKTTSW)

are necessary so that in the beginning no division by ZERO or no high value occurs. The integrator and the timer are stopped if

- B.dktst is equal to FALSE.
- akatbn is smaller than KATBFMN.
- the integrator or the timer have reached the limit.
- during the first seconds (2 x ZDKATAF) after monitoring start (B.dktst) in order allow the low pass filters of ahkatn and akatbn to warm up

There is the possibility, to feed the ahkat-integrator either with ahkatn-akatbn+KATBFN or directly with ahkat.

The latter offers the advantage to improve the signal to noise ratio in case of a fresh catalyst and low catalyst load.

The swiching mechanism is performed with CWKATUM=1. The hysteresis thresholds HYKATA and HYKATR respectivley can be tuned to define the switching condition. This condition is fulfilled if:

CWKATUM=1 AND ahkatn<HYKATA AND akatbn > (ahkatn+HYKATR) AND KATBFN > (akatbn+HYKATR).

The output of the timer (dkatakt\_w) supplies the active monitoring time. The ahktki\_w-signal supplies the actual integration value. These two signals are needed for application purposes.

The value ahkati can be adjusted dependent on the age of the lambda sensor (lsadkt).





Partial function block DKATST:

-----  
Stop criteria :

The catalyst conversion monitoring is not always active. The conditions leading to an interruption of the monitoring may either be derived physically or they are caused by the errors of other functions in the motronic. Due to this reason the two stop types are separated from each other.

a) physical stop criteria (partial function DKATSTP)

- The catalyst monitoring is only active within one load-engine speed range. The engine speed range lies between a lower (NDKTSU) and an upper (NDKTSO) threshold. The load range is limited by two engine speed-dependent characteristic lines (RLDKATSO, RLDKATSU). The engine speed base points are identical on both characteristic lines.
- During low temperature (start temperatur) the HC conversion decreases and the amplitudes of the lambda sensor behind the catalyst increase. Therefore a monitoring during this temperatur is excluded. The catalyst temperature tkatm is reformed in the function ATM. The catalyst diagnosis is only active if the temperature tkatm is larger than TMINKAT.
- During high temperature (tkatm >= TMAXKAT) the diagnosis will be stopped too, in order to prevent a "false pass" diagnosis.
- Moreover, a delay time tvdtktk can be applicated. It depends from the temperature gradient of tkatm, at the time when tkatm enters the temperature window, that is formed from TMINKAT and TMAXKAT respectively.
- During tester mode the lower temperature threshld TMNKATT must be exceeded.

- The katbfs- resp. katbfi\_w-signals gained from the partial function AKATB are used for the formation of the physical stop criteria. Cut-off limits for the katbfs-signal (KATBFSX) and for the katbfi\_w-signal (KATBFXM) are fixed. The catalyst conversion monitoring is stopped if the katbfi- resp. the katbfs-signal at the same time exceed resp. fall short of the limits (KATBFXM (KATBFXT at tester's request, KATBFSX). By these limiting values resp. by chosing the load-engine speed range it is possible to influence the active monitoring time in the FTP-test.

Stop criteria if a tester requests a function:

If a tester requests a function (B\_fakat = TRUE) a special load-engine speed range is defined. Thus it is ensured that the request can only be triggered for the intended working point. The engine speed nmot can vary between the limits (NDKTSUT, NDKTSOT) and the load rl can vary between the limits (RLDKTUT, RLDKTOT). Out of these ranges the function is stopped.

b) non-physical stop criteria (partial function DKATSTB)

The monitoring of the catalyst conversion can only take place during undisturbed functioning of the lambda controller. At the same time the sensors in front of and behind the catalyst must be fully available. This includes the results of the heating diagnosis and of the monitoring of the aging. The condition B\_lr indicates the normal operating of the lambda controller especially no fuel cut-off and readiness of the front sensor. A high charging of the activated carbon filter can disturb the monitoring and is therefore considered as a ban. This also applies for quick load changes which require a considerable correction in the transient control (B\_ukg). Furthermore misfires, AGR-errors, TES-errors as well as general errors in the load sensing are used as exclusion criteria.

Test modes:

- Permanent testing (DKATCW=0, APEKTDX=255, for application purpose only)  
The function will be initialized (B\_dikini), as soon as the diagnosis has finished on both banks (see chapter DKATINI). The function will be stopped for this trip (B\_dkten=TRUE), as soon as fault counter apedtk exceeds APEKTDX. The fault counter will be increased at the event of a fault at bank1 and bank2 respectively. In case of o.k.-testresult the diagnosis will be repeated for ever, in case of a fault it will be repeated 255 times.
- One healing test (DKATCW=1, APEKTDX=2, for series application)  
In case of an detected fault the diagnosis will be stopped when the fault counter exceeds the threshold "2". I.e. max. one healing test is possible. If in the first test no fault is detected (Z\_kat,-2=TRUE, E\_kat,-2=FALSE), the diagnosis will be stopped as well (B\_dkten=TRUE).
- Single test (DKATCW=2, APEKTDX > 0).  
The diagnosis will be stopped after the first run-through (B\_szkat=TRUE and hence B\_dkten=TRUE).

From the two stop types the bit B\_dktst is generated by connecting the OR function. After the stop condition has ended the waiting time TWDKATST is still waited for until the filters resp. the integrators are again enabled.

Partial function block DKATEL :

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For the setting of the error and cycle flags the following considerations were laid down:

- 1.) An individual error exists that means in one bank after the active monitoring time (TDKATAKT) has run out ahkat is larger than the maximum limit (AHKATMX). In this case E\_kat and Z\_kat are immediately set to TRUE (individual error has high priority).
- 2.) An added-up error exists that means that after the active monitoring time has run out the sum of the ahkat-signals of the two banks exceed the preselected border AHKATS. In this case the catalyst which shows a larger ahkat-signal is detected as defective. For this purpose a lower limit (AHKATMN) is defined which may not be undershot. Furthermore the active monitoring time of the two banks must have run out and in none of the banks no individual error may exist. By forming the flag (B\_zkats) three conditions are fixed. Firstly that in one bank the time has run out, secondly that no individual errors have occurred and thirdly that the ahkat-signal of the concerned bank does not lie below AHKATMN.
- 3.) An error of the adding range exists that means after the active monitoring time has run out an added-up error exists if the ahkat-signal is not larger than AHKATSB. The meaning of this being that in case of an added-up error both catalysts will be detected as being defective if they do not differ largely in the state of their age.

Z\_kat is set to FALSE by B\_dkini = TRUE. The cycle flag is not set until the monitoring end of the lambda sensor period is reported by the setting of the cycle flag Z\_latp=TRUE. By setting B\_fakat = TRUE the border for the active monitoring time is changed from TDKATAKT to TDKATATT. The E\_kat(2) and the Z\_kat(2) are set to FALSE in case of B\_pwf =TRUE resp. B\_clkat=TRUE. For the European version "CDKAT=0" E\_kat(2) is set to FALSE, Z\_kat(2) is set to TRUE and thus the function is stopped. In case of E\_kat(2) = TRUE B\_mxkat(2) = TRUE is set. B\_mxkat(2) is used in the error memory management.



Partial function block DKATINI:  
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The catalyst conversion monitoring is initialized in case of the following conditions:

- a) If the bit B\_ini = TRUE
- b) If the bits B\_szkat resp. B\_szkat2 = TRUE were set
- c) If the fault code storage is cleared
- d) If the diagnosis is started via tester request (B\_fakat)

The initialization means that all filters are set to ZERO, the integrators are either set to ZERO or to the setting values, the timer is set to the value AHKTTSW and Z\_kat is set to False.

After a single run of the monitoring function (cycle bit was set) it is possible to stop the catalyst conversion via the code word DKATCW bit no. ONE = TRUE.

Due to a historical reason ahkat is stored in a battery-backed RAM-cell with the edge of the Z\_kat-signal for the function %LC under the name avkatf. The avkatf-signal is set to the value AVKATFS in case of powerfail = TRUE.

Subfunction block DKATLRP:  
-----

In order to amplify the downstream sensor signal, it can be useful to enlarge the lambda perturbations. The parameter switch over for this performance is requested by B\_dktlp, falrdkt is the wanted value for amplification factor of the amplitude of the lambda perturbation.

B\_dktlp is set when DKAT is active (dkatakt\_w > AHKTTSW) and is cleared when the speed/load-range is left (B\_dktnr) or the DKAT-time is elapsed (B\_dktt) or the load oscillations are too rough.

## APP DKAT 58.140 Application hint

Application process:  
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The application of DKAT can be started usefully only if the application of the lambda controller and of the transient enrichment/lean-out has been completed and the FTP-results of the vehicle lie close to the target value. Only in this case it is possible to select a borderline catalyst. During application always a "mid-range" lambda sensor should be used to avoid the influences of sensor characteristics on FTP-results and on DKAT.

The condition B\_dktst indicates whether the function is actually active at the moment (B\_dktst = TRUE) or whether it is blocked. The application is largely carried out off-line. For this an evaluation software is available. Although the application must be carried out for the entire operating range, in this case an attempt is made to give corresponding suggestions for the determination of the individual application values for each individual block.

The results of the catalyst diagnosis can be improved by activating the lambda control after catalyst (rear control, trim control).

In case of "Y" exhaust configurations the RAM cell tikatm has to be applied in the middle of the main catalyst.

- Application of AKATB-block :  
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Application values

ZDKTBD	filter time constant for differentiator	[0,5...1,0...1,5] sec
ZDKTBF	filter time constant for low pass	[0,05...0,15...0,2] sec
KATBSH	offset for lambda control threshold	[0,0...0,47...0,80,0] mg/sec
KATBSG	memory value	[2,0...55,0...160] g
KATBFNM	scaling factor multiplicative for KB	[0,0...0,30...1,0] Volt
KATBFNP	scaling factor additive for KB	[0,0...0,40...1,0] Volt
KATBFML	filter time constant for sensor signal attenuation	characteristic line over ml, bank1
KATBFML2	filter time constant for sensor signal attenuation	characteristic line over ml, bank2

Characteristic line KATBFML (KATBFML2)

ml/(kg/h)	12	25	50	80	130
time constant/sec	[0,1..2,0..4,0]	[0,1..1,0..2,0]	[0,01..0,15..1,0]	[0,01..0,14..0,9]	[0,01..0,08,..0,3]

The values indicated in the middle are to be understood as reference values.

Determination of the two scaling factors KATBFNP and KATBFNM by the conformal mapping:

With these two factors the output signal of the low-pass filter for the sensor signal attenuation of +-1 is mapped onto the sensor signal threshold. The mapping is implemented by a straight line (y = a \* X + b).

Example:

If the sensor signal has the values 0.7 volt during rich phase and 0.1 volt during lean phase then the factors are to be determined by the following equation.

$$0.7 = \text{KATBFNM} * 1 + \text{KATBFNP}$$

$$0.1 = \text{KATBFNM} * (-1) + \text{KATBFNP}$$

The conclusion from this is KATBFNM = 0.3 volt and KATBFNP = 0.4 volt

Determination of the air mass throughput-dependent time constant KATBFML (KATBFML2) :

The time constant generally drops with increasing air mass throughput. For differing air mass the ushk-signal is compared with the katbf-signal. If the katbf-signal is attenuated compared to ushk the time constant is decreased. The time constant may not rise during increasing air mass. Whether the characteristic line was adjusted correctly can easily be read by comparing the katbfs-signal with the ushk-signal. Because if katbfs takes a similar course to ushk but katbf does not then the characteristic line was adjusted incorrectly. The precondition for a comparison between the ushk- and the katbf-signal is good conformance



of the two signals ahkatn and akatbn.

Determination of the time constants ZDKTBD and ZDKTBF :

The time constant ZDKTBD should be chosen in such a way that only the direct component of the fr-signal is filtered. Here it is possible to determine the period of the fr-signal during idling and to calculate the time constant as follows.

$$ZDKTBD = [1,5...2,0] * Tp/6 \text{ sec (Tp is the period during idling)}$$

The time constant ZDKTBF should be chosen in such a way that the area filtered of (fr-1.0)\*ml approximately equals the area  $\lambda * ml$ .  $\lambda$  may either be measured by a LSU-sensor or it may be determined by linearization of the LSH-sensor. If this time constant is chosen too large then the katbfi\_w-signal is very attenuated and the katbfs-signal has no ushk-similar course. Since katbfi\_w is used for the physical stop condition the attenuation has a direct influence on the selection of the two application values KATBFIO, KATBFIU. (See application instruction of DKATSTP)

Determination of the two application values KATBSH and KATBSG :

A conformance of the two signals ahkatn and akatbn can mainly be obtained by the correct selection of the KATBSG-values. Both signals are shown during the entire measurement. If akatbn is smaller than ahkatn then the value of KATBSG is too large. Should no conformance be achieved by reduction of the KATBSG then at first ZDKTBF should be checked whether it was not chosen too large and then the characteristic line KATBFML (KATBFML2) should be changed. Here katbfs shall be similar to ushk.

If the two signals ahkatn and akatbn chiefly correspond the signals ahkkti\_w and ahkat shall be monitored during the entire measurement range. For this at first the constant KATBFN must be set to ZERO so that it has no influence on the ahktnk-signal during integration.

If the fluctuations of the ahkkti\_w-signal are smaller than 5 to 10 % and if ahkat fluctuates around zero then KATBSH and KATBSG are adjusted correctly. Should ahkat be positive then KATBSH is too large. If the fluctuations are greater than 10 % then the application of the block should be repeated.

Application of AHKATB and AHKATS :

Application values

ZDKATAD	time constant differentiated signal amplitude	[0,3...0,8...1,0] Sec
ZDKATAF	time constant "absolute value filter" signal amplitude	[2,0...2,5...3,0] Sec
ADKATNF	scaling factor for signal amplitude	[2,0...4,0...8,0] 1/Volt

The values indicated in the middle are reference values

The task of these two blocks is to disconnect the alternating components and to form the rectified mean value of these alternating components.

The ADKATNF factor is introduced due to the comparison of ahkat with avkat from the filter procedure. For this the rectified mean value of the avkat-signal is compared to the rectified mean value of the akatbn-signal after the application of the AKATB-block. The scaling factor results from:

$$ADKATNF = \frac{\text{mean value of the avkat-signal}}{\text{mean value of the akatbn-signal}} \quad [1/\text{volt}]$$

ADKATNF can also be determined with a washcoat only catalyst such that ahkatn becomes = 1 ( ADKATNF\*ahkatn = 1 ). Should no washcoat only catalyst be present it is possible to take into consideration the sensor voltage in front of the catalyst as output signal.

When selecting the time constant attention should be paid that the output signal is not too attenuated and that the input signal is not filtered too quickly. In principal the reference values should be used.

Compensation of mean value of the rear sensor:

ZDKATSH	Time constant difference mean values	[1...3 ...10] Sec
KATBSHF	weighing factor mean value difference	[1...12...30]
KATBSHG	limitation ahkatn-impact	[0.05...0,2...0,5]

KATBSHF to be chosen so low that no oscillation of %DKAT occurs.

Application of the DKATSTP block:

Application values

KATBFSX	limit catalyst stress signal	[0,85...0,9...1,0] 1/sec
KATBFXM	limit gradient of the KB	[3,0...6,0...9,0]
KATBFXT	limit of the KB at tester's request	[3,0...6,0...9,0]
TMINKAT	lower limit for temperature	[350...350...450] °C
TMNKATT	lower limit for temperature during tester mode	[350...350...450] °C
TMAXKAT	upper limit for temperature	[450...550...650] °C
TMSUKTD	lower limit for engine start temp.	[-20...-15...-10] °C
NDKTSU	lower limit engine speed range	[640...720...1000] rpm
NDKTSO	upper limit engine speed range	[1500...2540...4000] rpm
NDKTSUT	lower engine speed function request	[640...740...1000] rpm
NDKTSOT	upper engine speed function request	[1500...2500...4000] rpm
RLDKTUT	lower load function request	[18...20...22] %
RLDKTOT	upper load function request	[27...30...53] %



RLDKTSO upper limit for rl-characteristic line over nmot [20.....70] %  
RLDKTSU lower limit for rl-characteristic line over nmot [10.....30] %

nmot / rpm	640	1200	1600	2000	2500
RLDKTSO / %	27	27	42	53	47
RLDKTSU / %	22	20	20	18	22

TVKTDTK	tkatm gradient dependent delay time	tkdkth [°C]	0	50	100	400
		TVKTDTK [s]	0	10	50	200
ZKTDTKM	low pass filter time constant for tkatm		[10.....50.....100] s			

The values indicated in the middle are reference values. The characteristic lines must be adjusted. The above-mentioned characteristic line values may be used as reference values.

TMUKTD ensures that no monitoring happens in case of extreme low ambient temp. (hazard of snow that might cool down the cat)

TMINKAT shall guarantee the definite operating readiness of the borderline catalyst.

TMAXKAT ensures that the catalyst is not monitored at high temperatures.

ZKTDTKM is the low pass filter time constant for tkatm.  
ZKTDTKM and TVKTDTK should be applied in that way that a significant delay time tvdkttk occurs only if tkatm shows a high slope just before entering the TMINKAT / TMAXKAT window.  
If tkatm only slightly exceeds TMAXKAT it is not necessary to delay the catalyst monitoring via tvdkttk.

By means of KATBFXM (KATBFXT at tester's request), KATBFSX an evaluation of the lambda sensor amplitude is refrained from during steady-state operation as well as during non-steady state operation with high catalyst stress. Thus the absolute value filters from the partial function blocks AHKATS, AHKATB and the integrator from the partial function block DKATAW are kept on the old value.

By these factors it is possible to influence the active monitoring time in the FTP test. If they are set to the indicated minimum limits and if the active time is smaller than 90 sec in the FTP test then they must be increased very carefully. In the FTP test a monitoring time in CT-phase of 150 sec is sufficient.

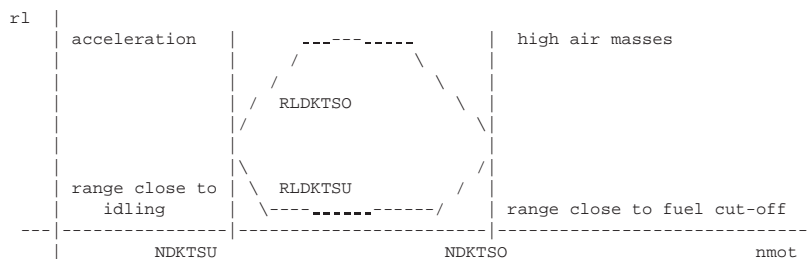
The evaluation time may be influenced by the evaluation range. In this case a compromise between load- engine speed range and the stopping with deactivation factors has to be found. The factors are, however, mainly intended for the stopping during non-steady-state drives or for high catalyst stress.

Application of the evaluation range:

The catalyst conversion monitoring works within one load-engine speed range only. The range is limited by two characteristic lines (rl-characteristic lines) and by two limits (engine speed limits). The range should be surrounded by NDKTSU, NDKTSO, RLDKTSO, RLDKTSU. The largest range is adjusted as follows.

- a) Application of RLDKTSO :  
The characteristic line shall be adjusted for high load such that during small engine speed ranges high loads are excluded. In the FTP test in high hills the accelerations are excluded. Very large air masses (approx. 150 kg/h) at higher engine speeds are not to occur in the evaluation range. Thus the main points of the RLDKTSO characteristic line are fixed.
- b) Application of RLDKTSU  
The characteristic line is adjusted for low loads. During low engine speeds small air masses (approx. 12 kg/h) shall not occur in the evaluation range. During higher engine speeds ranges close to the fuel cut-off are to be excluded. Thus the main points of the RLDKTSU characteristic line are fixed.
- c) Application of the NDKTSU and the NDKTSO values  
NDKTSU can be set equal to the idle speed. NDKTSO can be limited to the medium engine speed range.

The excluded area should be made as large as possible. In the middle of the area ahkatn shall be approx. 50 % of the maximum value.



Application of the DKATSTB block :

Application values

CDKATLK	Codeword stop DKAT while B_lrka	0 ... diagnosis conducted during B_lrka
		> 0 ... diagnosis topped with B_lrka



DKATCW	Codeword testing mode	0 ... permanent test (-->APEKTDX=255), for application phase only 1 ... one healing test (-->APEKTDX=2) 2 ... single test (-->APEKTDX > 0)
APEKTDX	Max. number of test with an error-result (see DKATCW)	

Application of the DKATAW block:

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A p p l i c a t i o n   v a l u e s

AHKTTSW	timer setting value	1,0 Sec
KATBFMN	lower threshold for KB-amplitude	[0,1...0,2...0,3]
KATBFN	standardized correction for signal amplitude	[0,1...0,5...1,0]
HYKATA	absolute hysteresis value	[0....0,1...0.2]
HYKATR	relative hysteresis value	[0.....0,1...0.2]
CWKATUM	codeword for switching	[0.....0....1]
LSAKTD	Adjustment line to compensate sensor age	[0,5...1,0...1,0]
KFKABMT	Correction map of the modelled amplitude	[0.....1.....2]

After the ahkatn-signal and the akatbn-signal have been adjusted so that the ahkkti\_w-fluctuations are smaller than 10 % and ahkat is approximately zero KATBFN shall be adjusted to the mean value of the ahkatn-signal. This correction works like a straight line with a gradient of one. It intersects with the y-axis at KATBFN. The KATBFN summand enables a comparison between ahkat and avkat.

In case of very small amplitudes it is impossible to differentiate between the borderline catalyst and a catalyst which is to be detected as "good". Due to this reason the integrator and the timer are stopped in case of such amplitudes. This lower limit should be 20 % of the KB-amplitude at the maximum otherwise no DKAT is possible while driving in small load-engine speed ranges.

There is the possibility, to feed the ahkat-integrator either with ahkatn-akatbn+KATBFN or directly with ahkat. The latter offers the advantage to improve the signal to noise ratio in case of a fresh catalyst and low catalyst load. The switching mechanism is performed with CWKATUM=1. The hysteresis thresholds HYKATA and HYKATR respectively can be tuned to define the switching condition. This condition is fulfilled if:  
CWKATUM=1 AND ahkatn>HYKATA AND akatbn > (ahkatn+HYKATR) AND KATBFN > (akatbn+HYKATR).

KFKABMT has to be tuned with support of the application tool DKAT\_Sx.

LSAKTD: First conduct DKAT with a good front sensor. Then do it with an aged front sensor and adjust LSAKTD in such way that ahkat obtains the former value.

Application of the DKATEL block:

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A p p l i c a t i o n   v a l u e s

AHKATMX	threshold value catalyst defect	[0,1...0,5...1,0]
AHKATMN	threshold value catalyst good	[0,1...0,3...1,0]
AHKATS	added-up threshold value (stereo 1. and 2.bank)	[0,2...1,1...2,0]
AHKATSB	adding range threshold value (stereo)	[0,2...1,1...2,0]
TDKATAKT	threshold for active monitoring time	[30....100...400] sec
TDKATATT	time threshold function request	[10....30.....50] sec

The values indicated in the middle are reference values.

The threshold for the active monitoring time should be chosen as large as possible in the FTP test so that the standardized integration (ahkat-signal) can stabilize. Due to the quantization the time should, however, not exceed 400 sec.

The AHKATS-value should be at least double that of AHKATMN, AHKATSB must be larger than AHKATMN.

Application of AVKATFS :

AVKATFS	AVKATF setting value	[0,1...0,5...1,0]
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AVKATFS is adjusted for a bad catalyst.

TEXT/ANF

Application of speed threshold NKTDX

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Above the speed of NKTDX rpm the diagnosis calculation will be stopped due to ECU computation time saving.

NKTDX	rpm-threshold for calculation inhibit	[3000...4000...5000] rpm
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Application of the DKATLRP block :

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A p p l i c a t i o n   v a l u e s

DRLKTDTP	Threshold load-transients	[1...5...20 %]
ZKTDRL	Time constant rl-low pass	[0,5...2...4] s
FALRKTD	Ampl. factor of lambda controller amplitude	[1...1...3]

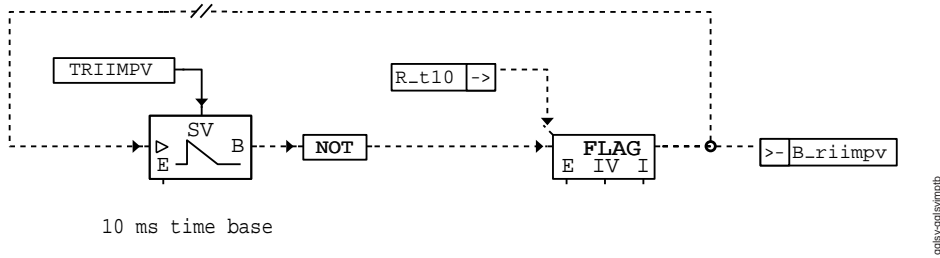
Default-Application: DLRKTDTP = -2% (switch off the feature to impact the lambda controller amplitude, because many other monitoring functions are disturbed).

Recommendation: Switch off this feature of influencing the lambda controller amplitude.



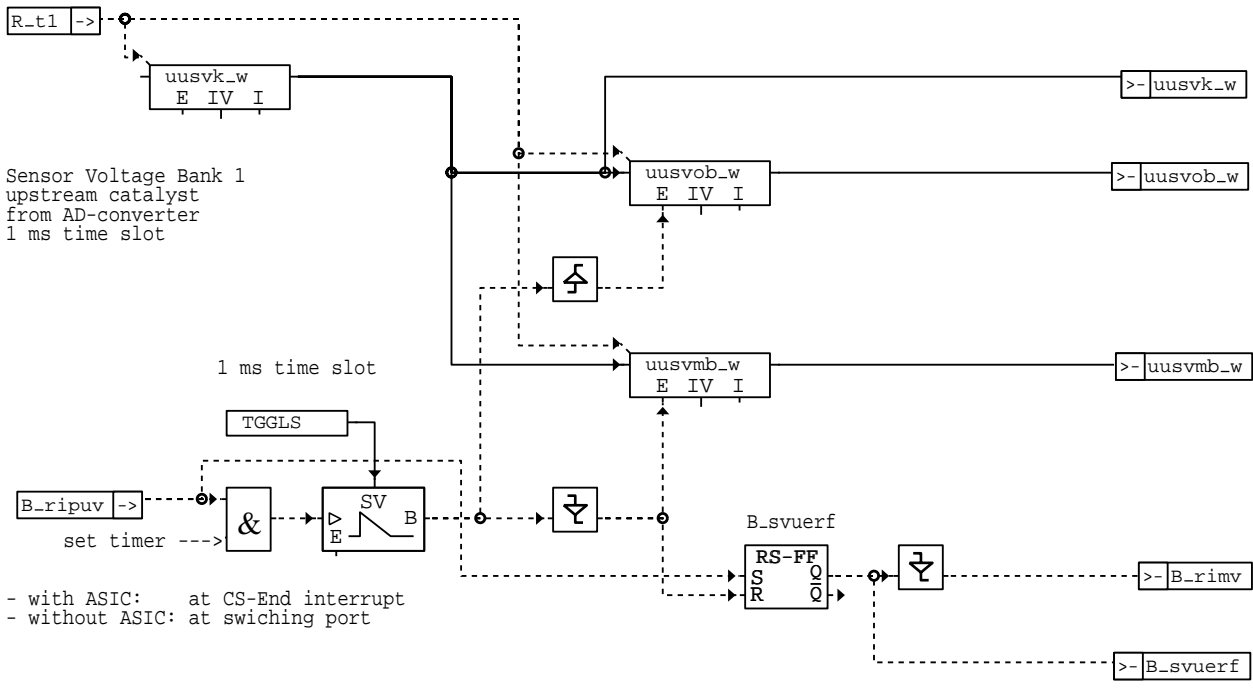


GGLSVIMPTP: Generating pumping time intervals for bank1 und bank2



gglsv-gglsvimpb

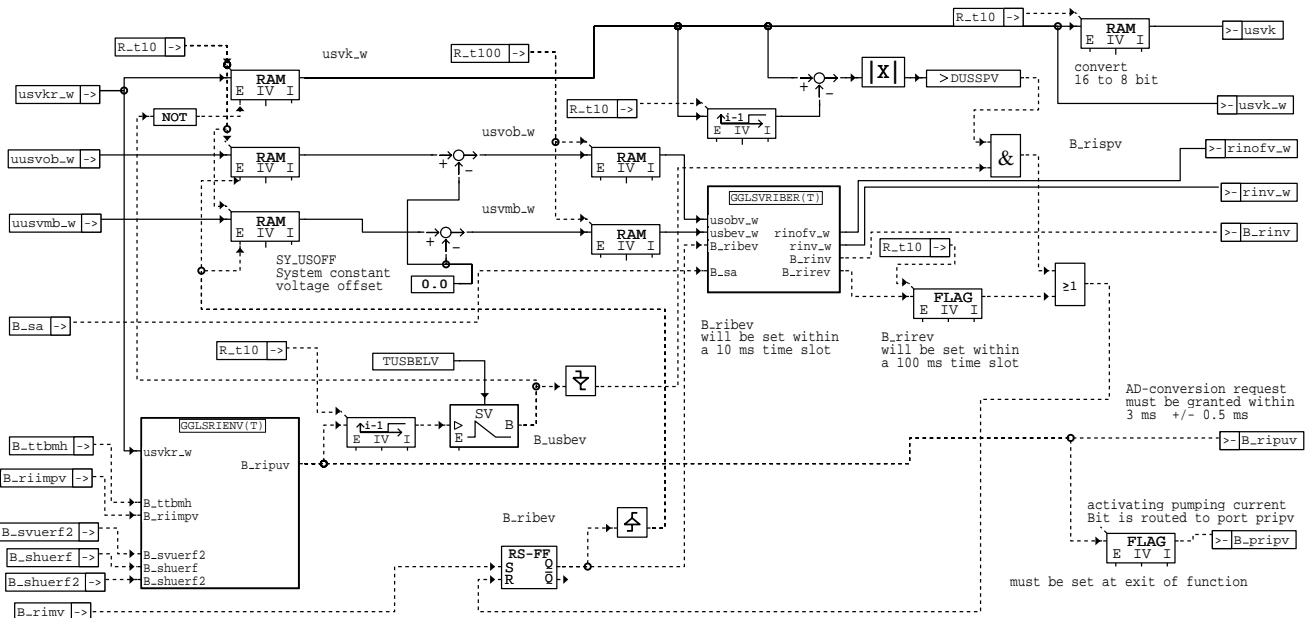
GGLSERFV: Measuring the unloaded and the loaded sensor voltage into 1 ms-time frame, bank1



gglsv-gglservv

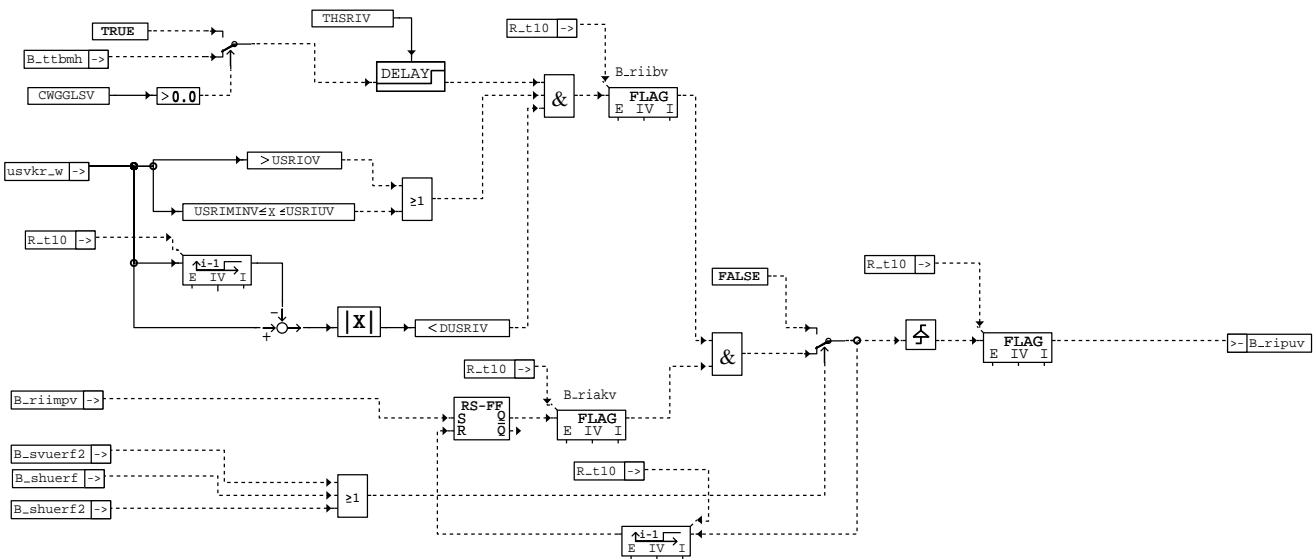


GGLSVFV: Transfer of the measured values unloaded and loaded after pumping into 100 ms-time frame, bank 1



### gglsv-gglsvf

GGLSRIENV: Enabling of Ri-measurement, bank 1:

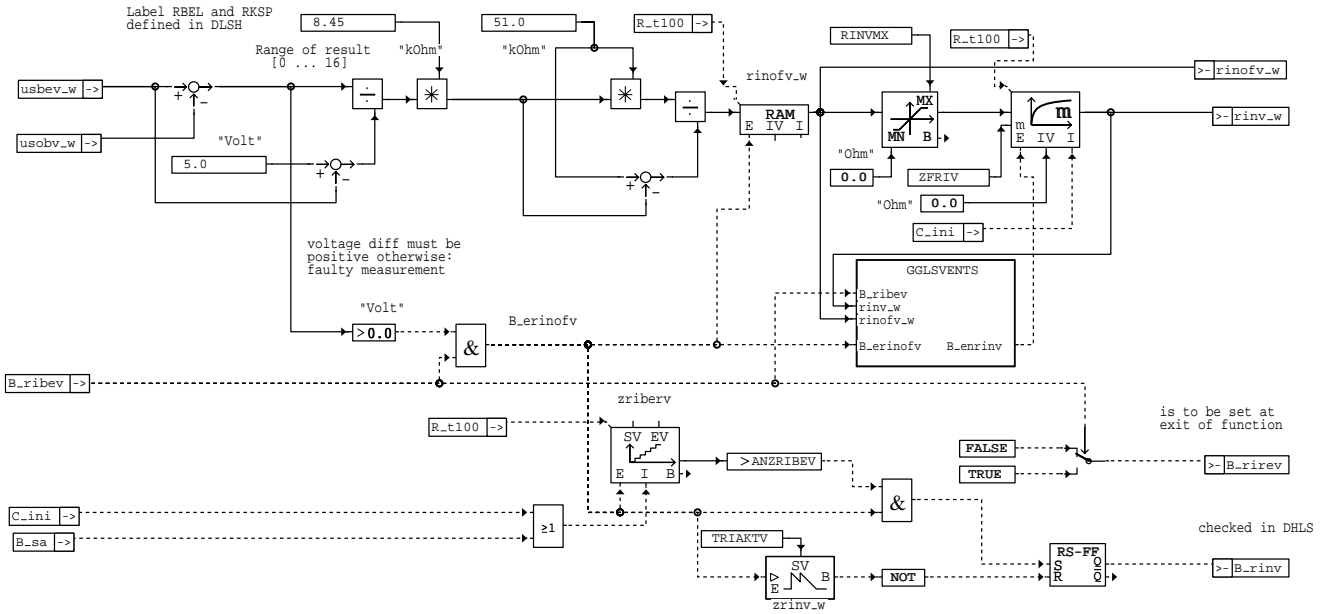


### gglsv-gglsvrienv



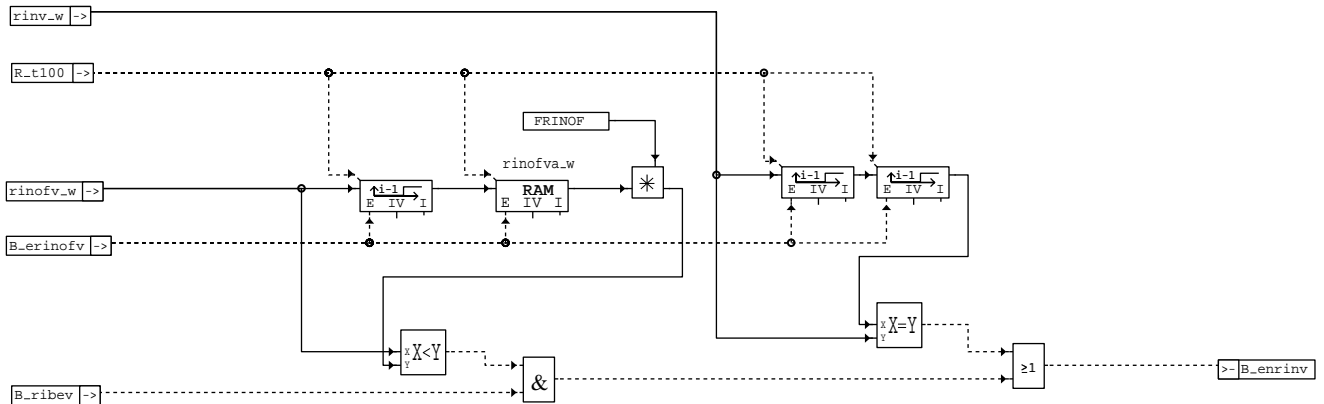


GGLSVRIBER: Ri-calculation and statistical evaluation, bank 1



gglsv-gglsvrber

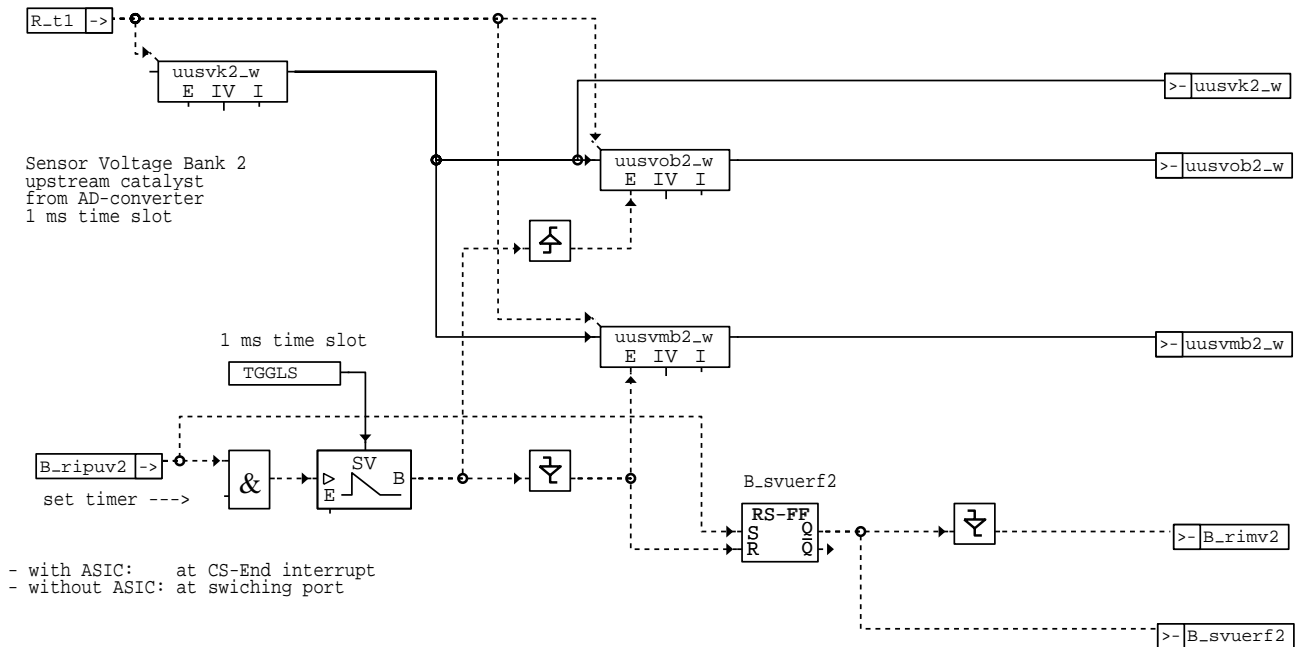
GGLSEVENTS: Additional interference suppression of Ri-measurement and formation of enable for the Ri-filter, bank1



gglsv-gglsevents

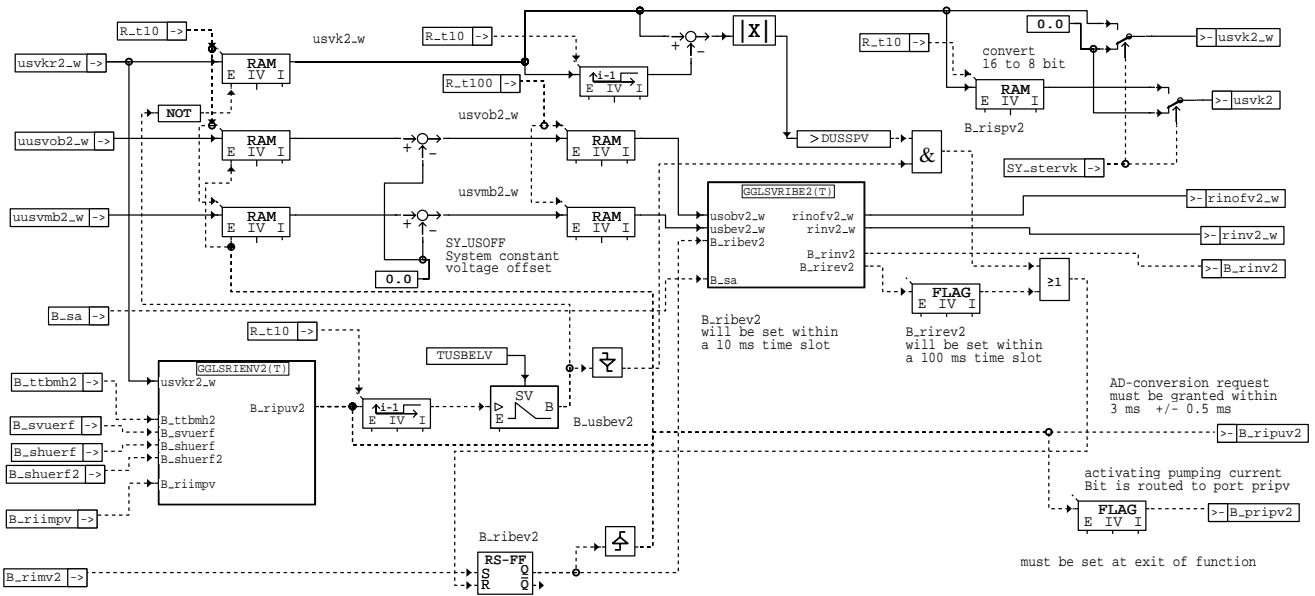


GGLSERFV2 : Measuring the unloaded and the loaded sensor voltage into 1 ms-time frame, bank2



### gglsv-gglserfv2

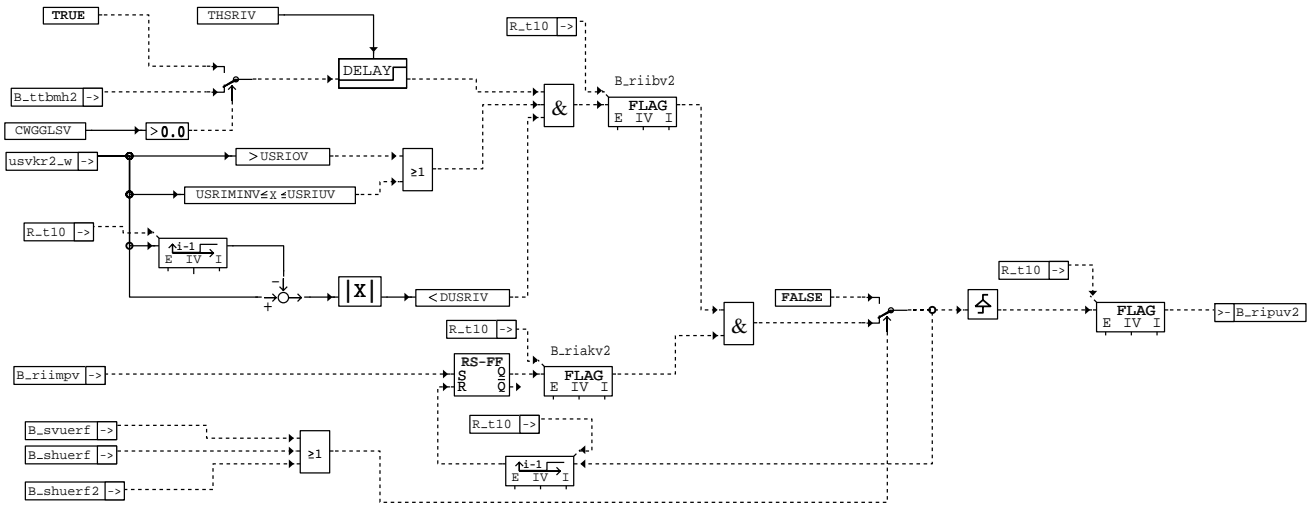
GGLSFV2 : Transfer of the measured values unloaded and loaded after pumping into 100 ms-time frame, bank 2



### gglsv-gglsvf2

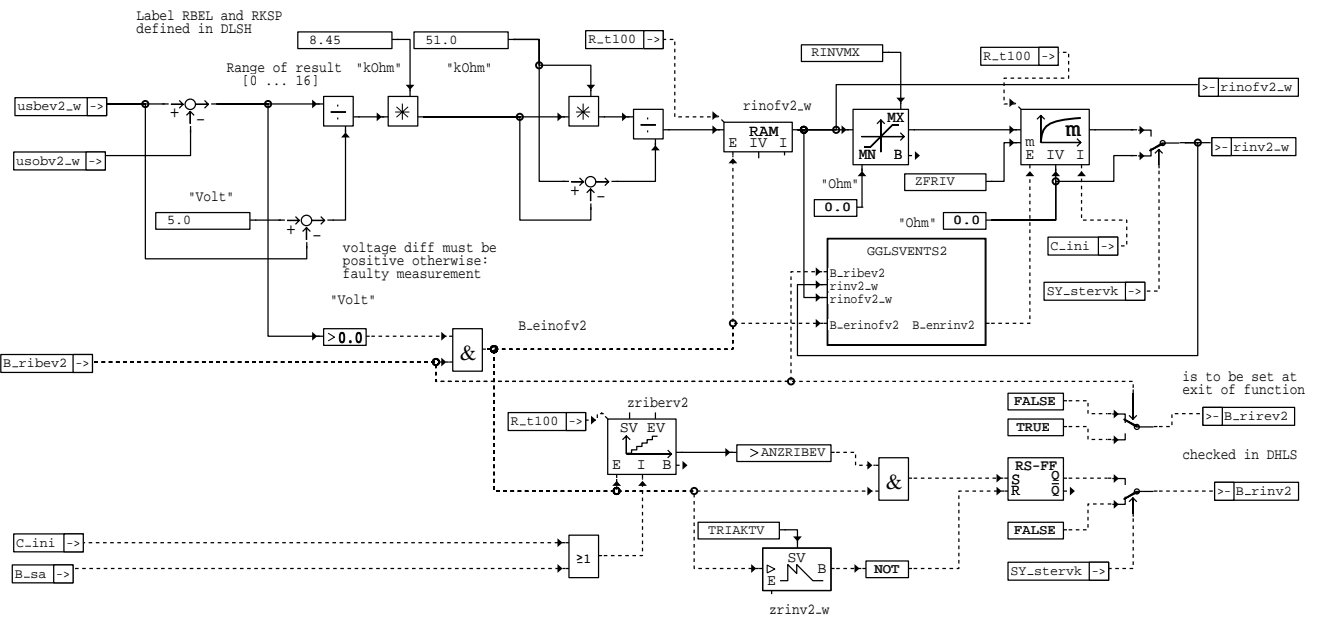


### GGLSRIENV2: Enabling of Ri-measurement, bank 2



### gglsv-gglstrienv2

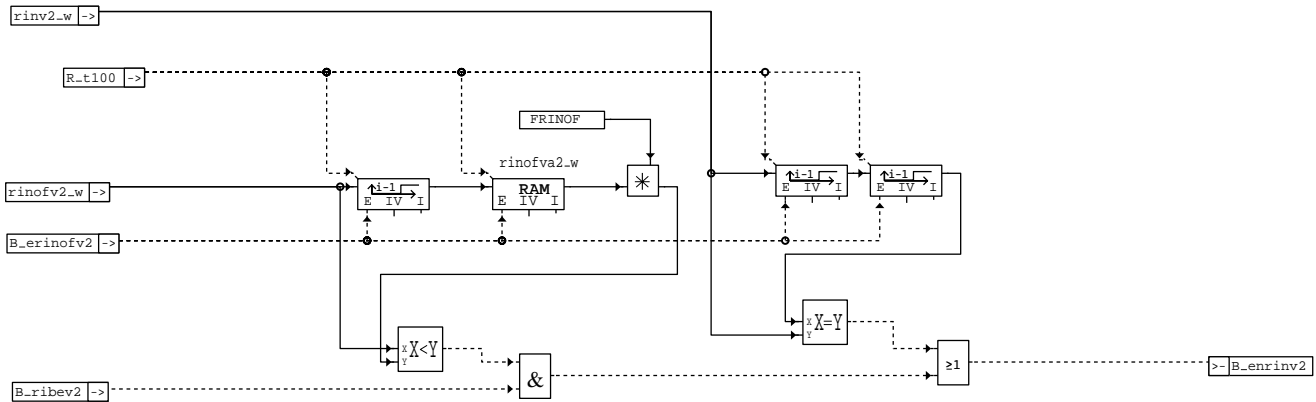
### GGLSVRIBE2: Ri-calculation and statistical evaluation, bank 2



### gglsv-gglsvribe2



GGLSVENTS2: Additional interference suppression of Ri-measurement and formation of enable for the Ri-filter, bank 2



gglsv-gglsvents2

### ABK GGLSV 2.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ANZRIBEV			FW	Amount of Ri calculation pre cat
CWGGLSV			FW	Code word for Ri-measurement for O2sensor pre cat (not fully heated)
DUSRIV			FW	Delta sensor voltage pre cat between new and old value for Ri measurement
DUSSPV			FW	Delta sensor volt.front cat between new and old val. for sensor jump knowledge
FRINOF			FW	Factor for validation of old Ri-value without filter
RINVMX			FW	Internal resistor Ri of nernst sensor limited to maximal value
TGGLS			FW	Time needed for ADC after interrupt in the function calculator (Asic)
THSRIV			FW	Ready condition, time delay,of Ri measurement after sensor heating on pre cat
TRIAKTV			FW	Time for Ri calculation actual pre cat
TRIIMPV			FW	Time for pump impulse for both banks pre cat
TUSBELV			FW	Time for holding of O2 sensor voltage after Impuls charge
USRIMINV			FW	Minimum voltage threshold for Ri-mesurement of the sensor upstream cat
USRIOV			FW	Upper voltage threshold for Ri-measurement of the sensor upstream cat
USRIUV			FW	Lower voltage threshold for Ri-measurement of the sensor upstream cat
ZFRIV			FW	Reduction factor for internal resistor Ri-Nernst filter pre cat

Variable	Source	Type	Description
B_ENRINV	GGLSV	LOK	Condition enable for Ri-Nernst wit filter pre cat
B_ENRINV2	GGLSV	LOK	Condition enable for Ri-Nernst wit filter pre cat bank 2
B_ERINOFV	GGLSV	LOK	Condition enable for Ri-Nernst without filter pre cat
B_ERINOFV2	GGLSV	LOK	Condition enable for Ri-Nernst without filter pre cat bank 2
B_LSV	PROKON	EIN	Cond. lambda sensor inst. upstr. of the cat., 1. sensor downst. of outlet(Bank1)
B_LSV2	PROKON	EIN	Cond. lambda sensor inst. upstr. of the cat., 1. sensor downst. of outlet(Bank2)
B_PRIPV	GGLSV	AUS	Condition switch port for pump impuls upstream catalyst
B_PRIPV2	GGLSV	AUS	Condition switch port for pump impuls upstream catalyst bank2
B_RIAKV	GGLSV	LOK	Condition for pumping current updated upstream catalyst
B_RIAKV2	GGLSV	LOK	Condition for pumping current updated upstream catalyst, bank 2
B_RIBEV	GGLSV	LOK	Condition calculate internal resistance Ri for sensor upstream cat
B_RIBEV2	GGLSV	LOK	Condition calculate internal resistance Ri for sensor upstream cat, bank 2
B_RIBV	GGLSV	LOK	Cond. sensor volt. in the perm. range for pump. current upstream cat
B_RIBV2	GGLSV	LOK	Cond. sensor volt. in the perm. range for pump. current upstream cat, bank2
B_RIIMPV	GGLSV	LOK	Condition impuls for pumping current upstream catalyst
B_RIMV	GGLSV	LOK	Cond. (adc-trigger) for measuring of loaded sensor voltage upstream cat
B_RIMV2	GGLSV	LOK	Cond. (adc-trigger) for measuring of loaded sensor voltage upstream cat, bank2
B_RINV	GGLSV	AUS	Condition: Internal resistance Ri of O2 sensor activ,pre cat
B_RINV2	GGLSV	AUS	Condition: Internal resistance Ri of O2 sensor activ,pre cat bank 2
B_RIPUV	GGLSV	LOK	Condition pumping current for sensor upstream catalyst
B_RIPUV2	GGLSV	LOK	Condition pumping current for sensor upstream catalyst bank2
B_RIREV	GGLSV	LOK	Condition result for internal resistance Ri for sensor upstream cat
B_RIREV2	GGLSV	LOK	Condition result for internal resistance Ri for sensor upstream cat, bank2
B_SA	MDRED	EIN	Condition fuel cut-off
B_SHUERF		EIN	Condition sensor voltage post cat measured
B_SHUERF2		EIN	Condition sensor voltage post cat measured bank 2
B_SVUERF	GGLSV	LOK	Condition sensor voltage pre cat measured
B_SVUERF2	GGLSV	LOK	Condition sensor voltage pre cat measured bank 2
B_TTBMH		EIN	condition theoretical lambda sensor operation readiness with heating
B_TTBMH2		EIN	condition theoretical lambda sensor operation readiness with heating bank2
B_USBEV	GGLSV	LOK	Condition for time counter for deactivation of the sensor load upstream cat
B_USBEV2	GGLSV	LOK	Condition for time counter for deactivation of the sensor load upstream cat bank2
C_JNI	SWADAP	EIN	ECU-condition for intialisation
RINOFV2_W	GGLSV	AUS	Internal resistor (word) Ri Nernst without filter, pre cat, bank 2
RINOFVA2_W	GGLSV	LOK	Internal resistor (word) Ri Nernst (old value) without filter, pre cat bank2
RINOFVA_W	GGLSV	LOK	Internal resistor (word) Ri Nernst (old value) without filter, pre cat
RINOFV_W	GGLSV	AUS	Internal resistor (word) Ri Nernst without filter, pre cat
RINV2_W	GGLSV	AUS	Actual value of internal resistance of lambda sensor 2, pre ca
RINV_W	GGLSV	AUS	Actual value of internal resistance of lambda sensor,pre cat (word)



Variable	Source	Type	Description
R_T1		EIN	Time schedule 1 ms
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
SY_STETLR	PROKON	EIN	System constant condition continuous Lambda control present
USBEV2_W	GGLSV	LOK	Voltage (word) lambda sensor loaded with resistance upstream cat, bank 2
USBEV_W	GGLSV	LOK	Voltage (word) lambda sensor loaded with resistance upstream cat
USOBV2_W	GGLSV	LOK	Voltage (word) lambda sensor without load upstream catalyst bank 2
USOBV_W	GGLSV	LOK	Voltage (word) lambda sensor without load upstream catalyst
USVK	GGLSV	AUS	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	AUS	output voltage oxygen sensor upstream catalyst 2
USVK2_W	GGLSV	AUS	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVKR2_W	GGLSV	LOK	Voltage (word) O2-sensor in raw value, pre cat , bank 2
USVKR_W	GGLSV	LOK	Voltage (word) O2-sensor in raw value, pre cat
USVK_W	GGLSV	AUS	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst
USVMB2_W	GGLSV	LOK	Voltage (word, 10 ms time slot) sensor with resistor loaded, upstream cat, bank2
USVMB_W	GGLSV	LOK	Voltage (word, 10 ms-time slot) O2-sensor with resistor loaded , upstream cat
USVOB2_W	GGLSV	LOK	Voltage (word, 10 ms time slot) sensor, unloaded, upstream cat, bank 2
USVOB_W	GGLSV	LOK	Voltage (word 10 ms-time slot) sensor, unloaded, upstream cat
UUSVK2_W	GGLSV	LOK	ADC voltage for lambda sensor upstream of catalyzer 2 (Word)
UUSVK_W	GGLSV	LOK	ADC voltage for lambda sensor upstream of catalyzer (Word)
UUSVMB2_W	GGLSV	LOK	Voltage (word, 1 ms-time slot) sensor with resistor loaded, upstream cat bank2
UUSVMB_W	GGLSV	LOK	Voltage (word, 1 ms-time slot) O2-sensor with resistor loaded , upstream cat
UUSVOB2_W	GGLSV	LOK	ADC voltage (word, 1 ms-time slot) O2-sensor unloaded upstream cat bank2
UUSVOB_W	GGLSV	LOK	ADC voltage (word, 1 ms-time slot) O2-sensor unloaded upstream cat
ZRIBERV	GGLSV	LOK	Ri calculation counter after engine start pre cat
ZRIBERV2	GGLSV	LOK	Ri calculation counter after engine start pre cat, bank 2
ZRINV2_W	GGLSV	LOK	Time counter for preparation of the actual condition Ri-Nernst pre cat bank 2
ZRINV_W	GGLSV	LOK	Time counter for preparation of the actual condition Ri-Nernst pre cat

### FW GGLSV 2.30 Fixed Values

Parameter	Value	Description
ANZRIBEV		Amount of Ri calculation pre cat
CWGGGLSV		Code word for Ri-measurement for O2sensor pre cat (not fully heated)
DUSRIV		Delta sensor voltage pre cat between new and old value for Ri measurement
DUSSPV		Delta sensor volt.front cat between new and old val. for sensor jump knowledge
FRINOF		Factor for validation of old Ri-value without filter
RINVMX		Internal resistor Ri of nernst sensor limited to maximal value
TGGLS		Time needed for ADC after interrupt in the function calculator (Asic)
THSRIV		Ready condition, time delay,of Ri measurement after sensor heating on pre cat
TRIAKTV		Time for Ri calculation actual pre cat
TRIIMPV		Time for pump impulse for both banks pre cat
TUSBELV		Time for holding of O2 sensor voltage after Impuls charge
USRIMINV		Minimum voltage threshold for Ri-measurement of the sensor upstream cat
USRIOV		Upper voltage threshold for Ri-measurement of the sensor upstream cat
USRIUV		Lower voltage threshold for Ri-measurement of the sensor upstream cat
ZFRIV		Reduction factor for internal resistor Ri-Nernst filter pre cat



## FB GGLSV 2.30 Detailed description of function

### 1. Introduction:

The sensor function GGLSV serves for the acquisition and the quantization of the sensor voltage upstream catalyst as well as for the generating of a pump current while at the same time the internal resistance  $R_i$  of the Nernst sensor is determined.

In this sensor function the sensor voltage is periodically pulsed by means of a pump current (0.5 mA for 10 ms) so that the sensors LSH and LSF4 are completely compatible. Thus no sensor diagnosis need to be changed. The sensors LSH and LSF4 have an air reference and would not need a pump current. However, if a pulsed pump current is used on these sensors then the internal resistance  $R_i$  can be determined. By the internal resistance an indirect check is performed in the heater diagnosis DHL5 on whether the sensor heater is o.k. In case of defect sensor heating or strongly reduced heating performance at low exhaust gas temperatures the internal resistance increases markedly.

### 2. Enable sensor function by configuration bit (GGLSV):

The sensor function can be enabled by the code word CWKONLS, provided the corresponding bits for the sensor installed upstream of the catalyst have been set. Bank1 can be enabled by means of bit 0 and with  $B_{_lsv} = 1$  and Bank1 enabled by bit 4 with  $B_{_lsv2} = 1$  (sum = 17).

If the universal sensor LSU is installed upstream of the catalyst, then the above condition must also be set by this code word as recognition for the sensor installed upstream of catalyst. SY\_STETLR must be set so that this sensor function will not be active for the Nernst sensor.

### 3. Generation of pump impulse (current impulse) GGLSRIENV:

An instable multi-vibrator with the output  $B_{_riimpv}$  serves to generate a pump impulse. The multi-vibrator supplies an impulse with the duration of 10 ms after an adjustable timer TRIIMPV has passed. This impulse  $B_{_riimpv}$  sets the flip-flop  $B_{_riakv}$ , i.e. the pumping current is updated. One timer only is used for both banks.

A pumping current with the condition  $B_{_ripuv} = 1$  can be performed if the sensor voltage lies within the permitted permissible voltage ranges ( $B_{_riibv} = 1$ ) and if the condition  $B_{_ttbmh} = 1$  from %DLSV was continuously active for a time longer than THSRIV. The condition  $B_{_ttbmh}$  from %DLSV can be disabled by the codeword CWGGLSV in order that  $R_i$  can be measured for application purpose even before end of dewpoint (refer to Application Note).

A permitted voltage range for permissible pumping current exists if the sensor voltage  $usvkr\_w$

"- is greater than USRIOV in the rich range"

"- lies between USRIMINV and USRIUV in the lean range"

"- the gradient of the sensor voltage (difference between new value and old value (i-1) in the 10 ms grid) is less than the threshold value DUSRIV

After the pumping current was enabled  $B_{_ripuv} = 1$  the flip-flop  $B_{_riakv}$  is reset in the next 10 ms grid (i-1) so that the period for pumping current is exactly 10 ms.

To maintain a correct current balance for the sensor LSF8, a timer TRIIMPV ( $B_{_riimpv} = 1$ , i.e. pump impulse is necessary) has passed and if at the same time sensor voltages occur in the not permitted voltage range ( $USRIV < usvkr\_w < USRIOV$ ) the triggering of the pump impulse is at first forbidden and stored as information in the flip-flop  $B_{_riakv}$ . Only once the non permitted voltage range is left immediately afterwards  $B_{_ripuv} = 1$  is set in the permitted voltage range and by doing so the pump impulse is triggered.

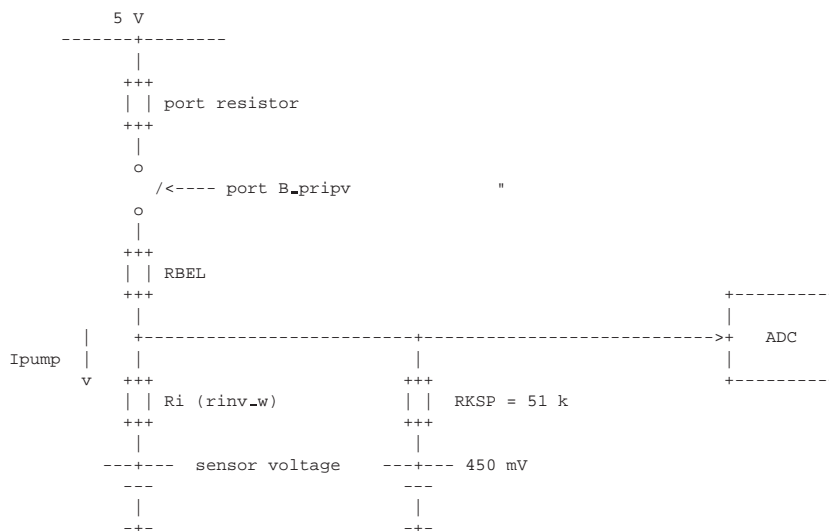
There must be a definite relationship between unloaded and loaded sensor voltage for a sensor in the 10 ms grid. This requirement is met by only one sensor being allowed to be pumped in the 10 ms grid.

$B_{_ripuv}$  cannot be used to pump current if the sensor voltage at bank2 upstream of catalyst, or the voltages downstream of catalyst are momentarily being detected by  $B_{_svuerf2}$ , or  $B_{_shuerf}$  and  $B_{_shuerf2}$  respectively.

Via  $B_{_ripuv}$  a port is switched with the bit  $B_{_pripv} = 1$  so that a pump current of 0,5 mA can flow for 10 ms from the 5V voltage supply and through a fixed defined resistor RBEL.

### Hardware:

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#### 4. Transfer of the sensor voltage measured values (unloaded and loaded) into the 100 ms grid for the Ri-calculation

For the calculation of the internal resistance Ri of the sensor it is important that the unloaded and the loaded sensor voltages are read within a time grid of 10 ms. This can be achieved if prior to the on-load impulse the unloaded sensor voltage usvk\_w is read via the ADC and if during the on-load impulse (10 ms) after approx. 3 ms the loaded sensor voltage usvb\_w is read via the ADC.

After the pump impulse was triggered B\_ripuv = 1 the sensor voltage ushkr\_w is held at the old value via a timer TUSBELH during the following 10 ms grid (i-1) so that the increased loaded sensor voltage cannot have an effect.

##### 4.1 Measuring the loaded and unloaded sensor voltage in the 1 ms time frame (GGLSERFV):

The ADC value of the sensor voltage is sampled in the 1 ms-time frame and is stored as the word usvk\_w in the RAM. If a permissible pump impulse B\_ripuv follows, then the unloaded voltage usvob\_w is stored by setting the timer TGGLS with a positive edge. After elapse of the time TGGLS, the loaded sensor voltage usvob\_w is stored is then retained in the 1 ms time frame with the negative edge. Setting the pump impulse B\_ripuv will also set the Flip-Flop B\_svuerf in the 1 ms frame, i.e. for the sensor upstream of the catalyst at bank1, the requirement is set that only the the sensor voltage will be measured here. TGGLS is reset following elapse of the timer by the negative edge of this detection Flip-Flop B\_svuerf. It must be ensured that the order of the bank calculation is observed (first bank1 and then bank2).

##### 4.2 Transfer of loaded and unloaded sensor voltage from the 1 ms time frame in 10 ms and 100 ms time frames (GGLSFV):

The condition B\_rimv is set by resetting the Flip-Flop B\_svuerf with the negative edge. The Flip-Flop B\_ribev is set by B\_rimv for transfer to the 10 ms and 100 ms time frames. The unloaded sensor voltage usvob\_w and the loaded sensor voltage usvmb\_w are transferred into a RAM in the 10 ms time frame with the positive edge of this Flip-Flop. The increase from sensor grounding, SY\_USOFF, that is specific to the control unit, is subtracted from the unloaded sensor voltage usvob\_w or loaded sensor voltage usvmb\_w and then receives the unloaded sensor voltage usvob\_w and the loaded sensor voltage usvmb\_w in the 10 ms time. These are then transferred in the 100 ms time frame to the RAM, usobv\_w and usbev\_w respectively. The increase in the sensor grounding, SY\_USOFF, that is specific to the control unit is then also subtracted in the 1 ms-time frame from the ADC voltage and stored in the 10 ms-time frame as the raw value in the RAM usvkr\_w (word). This 16 bit sensor voltage usvkr\_w is converted to the 8 bit format (usvk) for additional use in sensor diagnostics and lamda control.

##### Ri-calculation (rinofv\_w)

The internal resistance Ri' of the sensor is calculated from:

$$Ri' = \frac{usbev\_w - usobv\_w}{5V - usbev\_w} * RBEL$$

Corrected by the counter-resistance RKSP in the hardware Ri becomes:

$$Ri = \frac{Ri' * RKSP}{RKSP - Ri'}$$

This Ri value is given in the 100 ms-time frame by setting the Flip-Flop B\_ribev = 1 and is limited to RINVMX. The following measures are performed in order to prevent the loaded sensor voltage from being used in a jump of the sensor voltage during the 10 ms-impulse:

- a) If, primarily the rich tolean jump, the difference between the loaded sensor voltage usbev\_w and the unloaded sensor voltage usobv\_w is less than zero, then the B\_erinofv is not set and Ri is not comuted.
- b) If, primarily during the leasn to rich jump, it is determined following elapse of the timer that the magnitude from the difference of the sensor voltage from the new-old value in the 10 ms time frame is grater than DUSSEV and hence Ri is not calculated.

Thereafter rinofv\_w is filtered through an event filter with the attenuation factor ZFRIV so that the filtered internal resistance rinh\_w of the sensor is obtained. -----> Event filter :  $y[k] = y[k-1] + ZFRIV(x[k] + y[k-1])$

After the calculation of the internal resistance a flag is set in the 10 ms grid via B\_rireh = 1 (Ri-calculation terminated) and the flip-flop B\_ribev is reset.

##### 4.3 Additional interference suppression of Ri measurements and formation of enable for the Ri filter (GGLSEVENTS):

In the new unfiltered new value of Ri (rinofv\_w) is greater by a factor FRINOF than the old Ri value rioffv\_w, then B\_enrinv is not set and hence the calculated value is transferred to the filter. In order than an increase in the internal resistance Ri is possible during sensor cooling (new Ri value is greater than the old value vby the factor FRINOF), the transfer of rinofv\_w to the filter is enabled by B\_enrinv = 1 after measuring 2 Ri values.

The Ri-calculations B\_ribev are added-up by means of a counter zriberv. If the number of Ri-calculations is greater than ANZRIBEV then a flip-flop B\_rinv is set, which indicates to the heater diagnosis the state that the calculation of the internal resistance is active and up to date. ANZRIBEV = 3/ZFRIV is chosen.

As soon as the counter starts a retriggerable timer zrinv\_w is triggered, whose timer time is chosen at TRIAKTV = 4\*TRIMPV. Once the timer has passed zrinv\_w = 0 the flip-flop B\_rinv is reset (resistance value rinv\_w is not updated). If within the period TRIAKTV again current Ri-calculations are performed (B\_ribev =1), then this timer zrinv\_w is continuously started again so that the condition B\_rinv is currently active.



Course of the ADC-sequence:



## APP GGLSV 2.30 Application hint

SY\_USOFF

The fixed value voltage difference between sensor ground and electronic ground can adjustable with a system constant SY\_USOFF and it must be adjusted ECU-specific by the software.

Example: If the voltage between sensor ground and electronic ground is 0.268V the SY\_USOFF must be adjusted to 0.268V.

Corresponding to the hardware design SY\_USOFF becomes 0V; 0,268V or 0,714V.

Typical application values:

THSRIV = 10 s  
TUSBELV = 30 ms  
TRIIMPV = 2 s  
TRIAKTHV = 4\*TRIMPV = 8 s  
ZFRIV = 0.3  
ANZRIBEV = 3/ZFRIV = 10  
RBEL = 8.45 KOhm  
RKSP = 51 KOhm  
RINVMX = 100 KOhm  
USRIOV = 550 mV  
USRIUV = 250 mV  
USRIMINV = 60 mV  
DUSRIV = 25 mV  
UBDLS > 11 V  
TGGLS = 3 ms  
FRINOF = 1.5

CWGGLSV = 0 -----> Code word = 0 : Ri is only calculated after end of dewpoint for full heating power (series)  
= 1 : Ri can be measured as high-resistance for application purposes during phase of dewpoint

CWKONLS : -----> Code word in % PROKON : Sensors present upstream of the catalyst ---> Bank1: B\_lsv by Bit 0 = 1  
Bank2: B\_lsv2 by Bit 4 = 16  
(gives 17 as the sum)

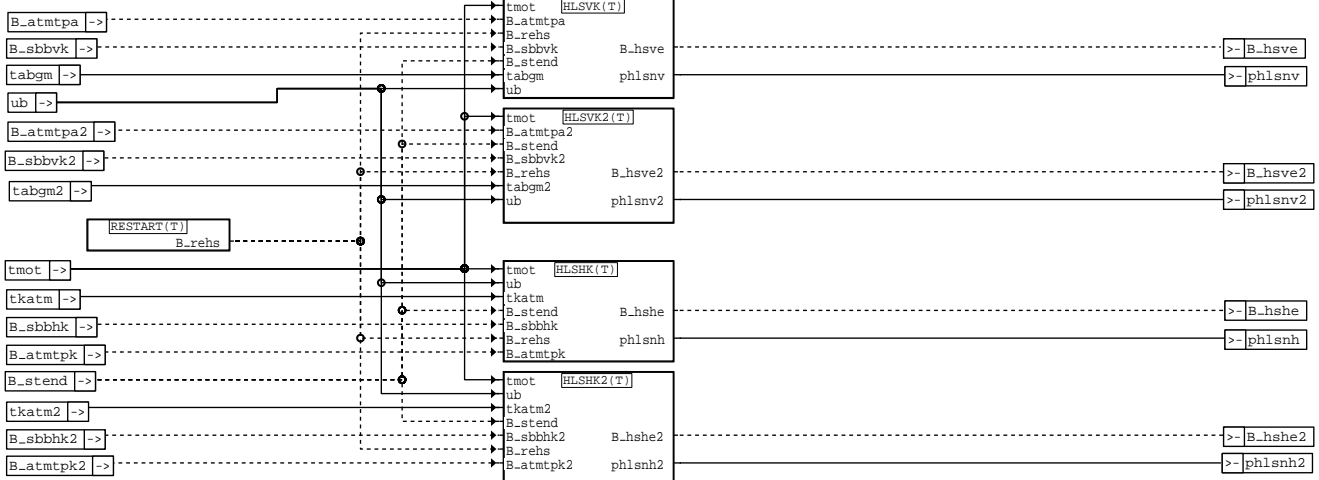
Sensors present downstream of the catalyst --> Bank1: B\_lsh by bit 1 = 2  
Bank2: B\_lsh2 by bit 5 = 32  
(gives 34 as the sum)

For all 4 installed sensors: CWKONLS = 51

## HLS 16.40 Lambda sensor heater

### FDEF HLS 16.40 Function definition

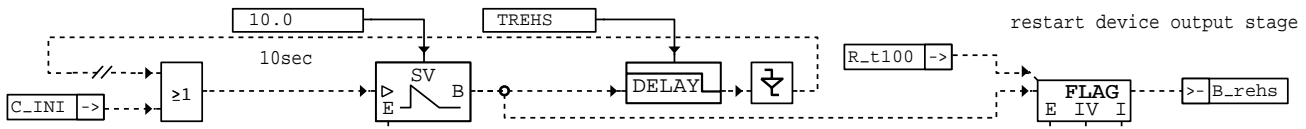
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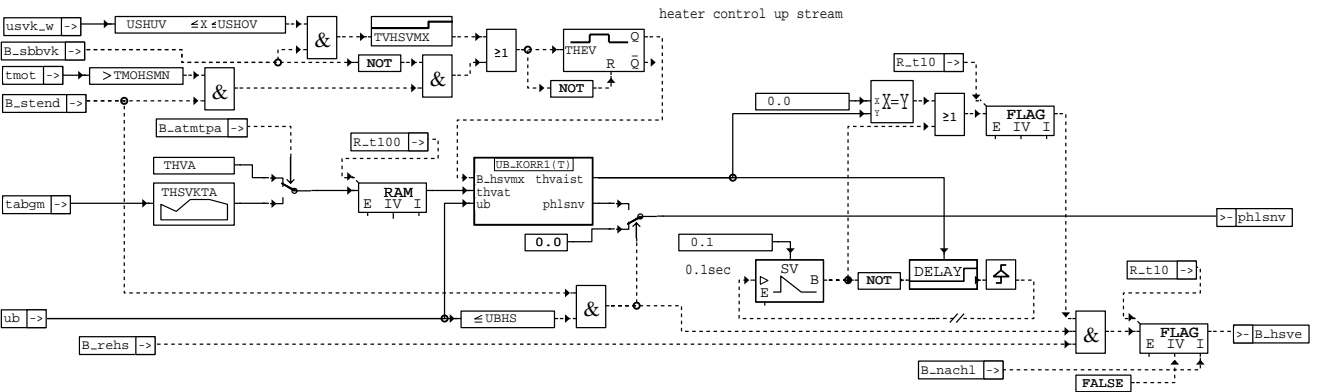
hls-hls

hls-hls

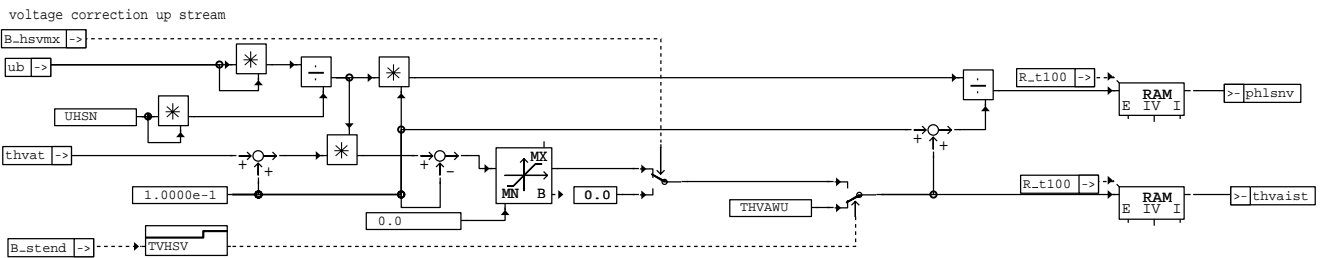




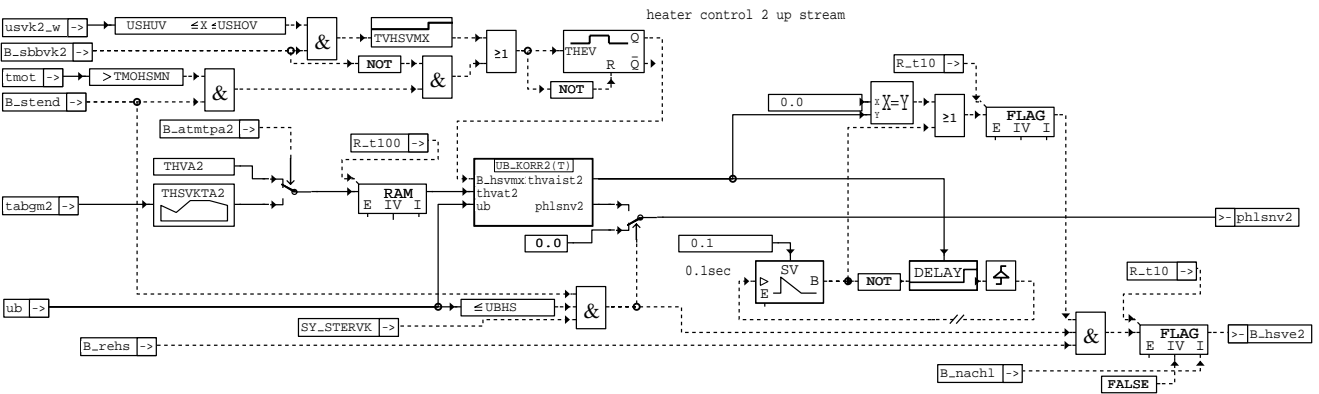
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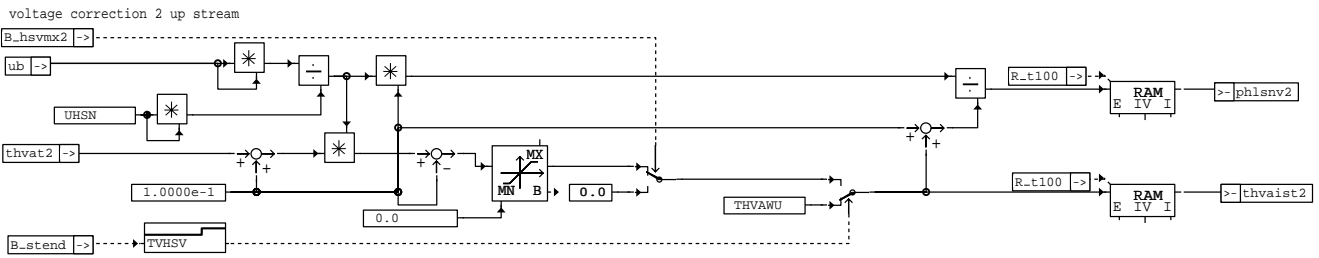
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**hls-ub-korr1**

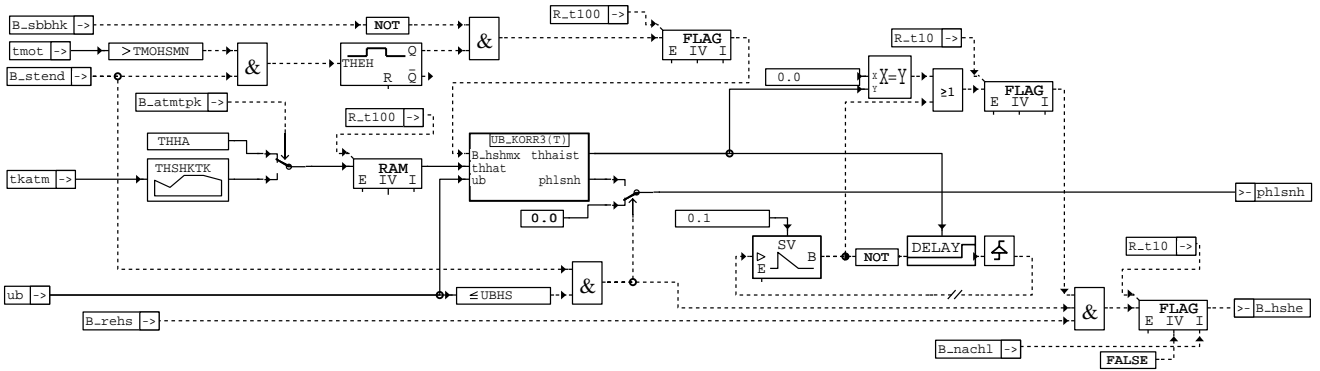


**hls-hlsvk2**



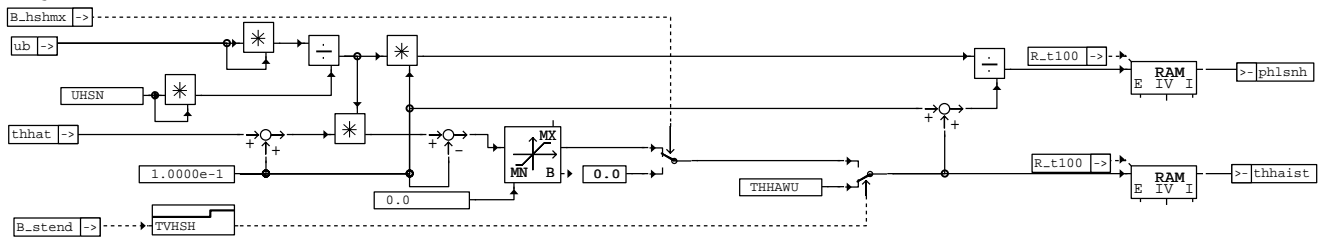
**hls-ub-korr2**

heater control down stream



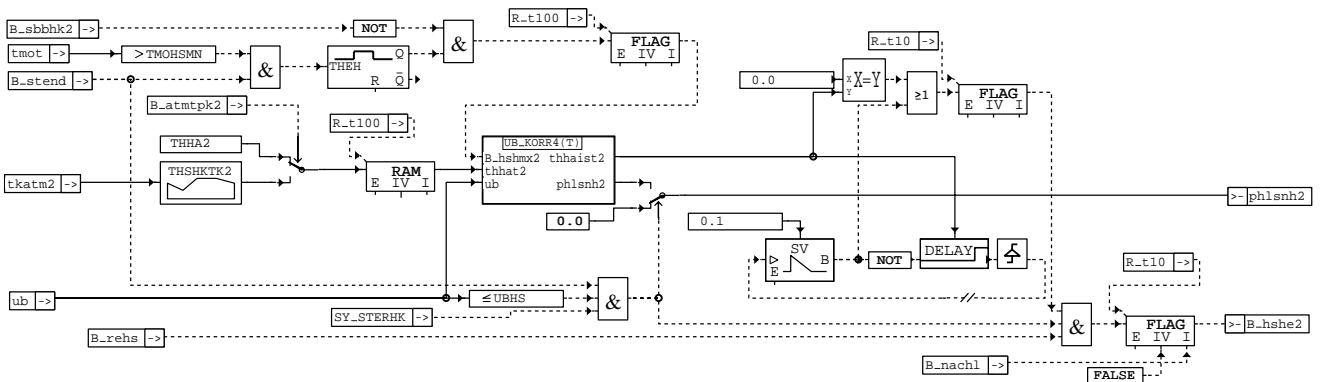
hls-hshk

voltage correction down stream



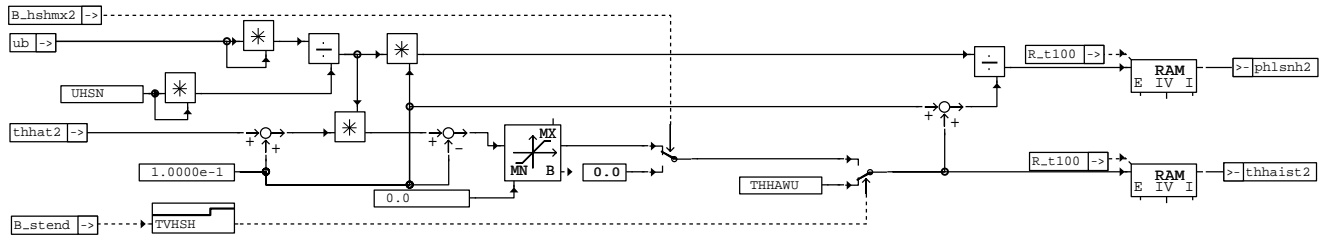
hls-ub-korr3

heater control 2 down stream



hls-hshk2

voltage correction 2 down stream



hls-ub-korr4

ABK HLS 16.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
THEH			FW	Time for maximal lambda sensor heating post cat after engine start
THEV			FW	Time for maximal lambda sensor heating after start , pre cat
THHA			FW	off time to reduce heater power of oxygen sensor downstream cat at 13Volt
THHA2			FW	off time to reduce heater power of oxygen sensor2 downstream cat at 13Volt
THHAWU			FW	Switch OFF time during power reduction of sensor heating post cat
THSHKTK	TKATM		KL	Line for switch off time of lambda sensor heating post cat dep. on temp
THSHKTK2	TKATM2		KL	ine for switch off time of lambda sensor heating 2 post cat dep. on temp



Parameter	Source-X	Source-Y	Type	Description
THSVKTA	TABGM		KL	Line of switching off time for lambda sensor heating depending on exh.gas temp
THSVKTA2	TABGM2		KL	Line of switching off time for lambda sensor heating depending on exh.gas temp 2
THVA			FW	off time to reduce heater power of oxygen sensor upstream cat at 13 Volt
THVA2			FW	off time to reduce heater power of oxygen sensor2 upstream cat at 13 Volt
THVAWU			FW	Switch OFF time during power reduction of sensor heating pre cat
TMOHSMN			FW	Minimum engine temperature for lambda sensor heating
TREHS			FW	time for restart sensor heating
TVHSH			FW	delay time for sensor heater downstream cut
TVHSHV			FW	delay time for sensor heater upstream cut
TVHSHVMX			FW	delay time for maximum sensor heater upstream cut
UBHS			FW	battery voltage threshold for switching off oxygen sensor heater
UHSN			FW	Nominal battery voltage for lambda sensor heating
USHOV			FW	Upper O2-sensor voltage threshold for maximal sensor heating pre catalyst
USHUV			FW	Lower O2sensor voltage threshold for maximal sensor heating pre catalyst

Variable	Source	Type	Description
B_ATMTPA	ATM	EIN	condition temperature upstream catalyst exceeds dew-point
B_ATMTPA2	ATM	EIN	condition temperature upstream catalyst exceeds dew-point2
B_ATMTPK	ATM	EIN	condition temperature downstream catalyst exceeds dew-point
B_ATMTPK2	ATM	EIN	condition temperature downstream catalyst exceeds dew-point2
B_HSHE	HLS	AUS	condition for lambda sensor heating-switch downstream cat on
B_HSHE2	HLS	AUS	condition for lambda sensor2 heating-switch downstream cat on
B_HSHMX	HLS	LOK	Condition maximal power of lambda sensor heating post cat
B_HSHMX2	HLS	LOK	Condition maximal power of lambda sensor heating 2 post cat
B_HSVE	HLS	AUS	condition for lambda sensor heating-switch upstream cat on
B_HSVE2	HLS	AUS	condition for lambda sensor2 heating-switch upstream cat on
B_HSVMX	HLS	LOK	Condition maximal power of lambda sensor heating pre cat
B_HSVMX2	HLS	LOK	Condition maximal power of lambda sensor heating 2 pre cat
B_NACHL	MOTAUS	EIN	ECU control for ECU switch off delay
B_REHS	HLS	LOK	Restart Lambda sensor heating
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_SBBVK	DLSV	EIN	condition for lambda sensor upstream cat ready for operation
B_SBBVK2	DLSV	EIN	condition oxygen sensor upstream cat. bank2 ready for operation
B_STEND	BBSTT	EIN	condition end of start
C_JNI	SWADAP	EIN	ECU-condition for intialisation
PHLSNH	HLS	AUS	Standardized heating power of the Lambda sensor downstream of the catalyzer
PHLSNH2	HLS	AUS	Standardized heating power of the Lambda sensor 2 downstream of the catalyzer
PHLSNV	HLS	AUS	normalized heating power of lambda sensor upstream of catalyst
PHLSNV2	HLS	AUS	normalized heating power of lambda sensor 2 upstream of catalyst
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
THHAIST	HLS	LOK	"Off"-duration for sensor heating downstream catalyst
THHAIST2	HLS	LOK	"Off"-duration for sensor heating2 downstream catalyst
THHAT	HLS	LOK	Uncorrected switch off time for lambda sensor heating post cat
THHAT2	HLS	LOK	Uncorrected switch off time for lambda sensor heating 2 post cat
THVAIST	HLS	LOK	"Off"-duration for sensor heating upstream catalyst
THVAIST2	HLS	LOK	"Off"-duration for sensor heating2 upstream catalyst
THVAT	HLS	LOK	Uncorrected switch off time for lambda sensor heating pre cat
THVAT2	HLS	LOK	Uncorrected switch off time for lambda sensor heating 2 pre cat
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TMOT	SWADAP	EIN	Engine temperature
UB	SWADAP	EIN	battery voltage
USVK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst

### FW HLS 16.40 Fixed Values

Parameter	Value	Description
THEH		Time for maximal lambda sensor heating post cat after engine start
THEV		Time for maximal lambda sensor heating after start , pre cat
THHA		off time to reduce heater power of oxygen sensor downstream cat at 13Volt
THHA2		off time to reduce heater power of oxygen sensor2 downstream cat at 13Volt
THHAWU		Switch OFF time during power reduction of sensor heating post cat
THVA		off time to reduce heater power of oxygen sensor upstream cat at 13 Volt
THVA2		off time to reduce heater power of oxygen sensor2 upstream cat at 13 Volt
THVAWU		Switch OFF time during power reduction of sensor heating pre cat
TMOHSMN		Minimum engine temperature for lambda sensor heating
TREHS		time for restart sensor heating
TVHSH		delay time for sensor heater downstream cut
TVHSHV		delay time for sensor heater upstream cut
TVHSHVMX		delay time for maximum sensor heater upstream cut
UBHS		battery voltage threshold for switching off oxygen sensor heater
UHSN		Nominal battery voltage for lambda sensor heating



Parameter	Value	Description
USHOV		Upper O2-sensor voltage threshold for maximal sensor heating pre catalyst
USHUV		Lower O2-sensor voltage threshold for maximal sensor heating pre catalyst

### FB HLS 16.40 Detailed description of function

This heater control is suitable also for power stages without current measuring shunt. The heating of the Lambda sensor is controlled such that independent of the ambient conditions (condensate, exhaust gas temperature, battery voltage) the Lambda sensor is not damaged. The heater power stage is short-circuit-proof and switches off automatically in case of too high current. Via a port, B\_hsv triggers the heater power stage, that means B\_hsv=1 ==> sensor is heated. The port must be inverted for integrated power stages CJ920. It must be operated within 10ms after B\_hsv. The output signal phlsnv represents the standardized heating performance of the sensor heating. With nominal voltage (UHSN = 13 Volt) the output shows the value 1,0 if the heating is not reduced. If the battery voltage is greater than UHSN then the sensor heating is clocked such that phlsnv = 1.

Function of the heater control after start:

1. Ceramic protection (avoiding ceramic stress)  
During the time TVHSV after end of start the heating performance is reduced (dependent on THVAWU) so as to limit the temperature gradient of the sensor ceramic.
2. maximum heating  
Maximum heating (phlsnv > 1) is performed during the time THEV, in order to reach the sensor operating readiness as quickly as possible.  
If the operating readiness stops again due to too little heating performance, maximum heating is again performed during THEV. If the sensor voltage is within the limits of the threshold USHUV / USHOV, the sensor heating will be switched on to Maximum when the delay time TVHSVMX is exceeded.  
If maximum heating is not allowed (downstream catalyst) then the time THEH must be set to the value zero.
3. Ceramic protection (avoiding thermal shock)  
After the time THEV has elapsed or in case of sensor ready for operating the heating performance is reduced dependent on THVA until dew point end is reached. In addition the heating performance is corrected dependent on the battery voltage (ceramic protection during condensate phase).
4. Temperature control  
After end of dew point the heating performance can be controlled dependent on the exhaust gas temperature (characteristic line THSVKTA) so that the ceramic temperature is e.g. 750°C.
5. Power stage protection  
With high battery voltage (booster start) the heating must be switched off (threshold UBHS).
6. Power stage diagnosis  
For the diagnosis of the power stage the heating is switched off periodically every 10s for TREHS. A power stage switched off due to short-circuit or overloading is activated again by this (block restart).

### APP HLS 16.40 Application hint

1. Determination of THVA/2, THHA/2	Set point ceramic temperature: upstr. cat 300 to 350°C, downstr. cat 200 to 250°C
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During the condensate phase the ceramic temperature of the sensors must be limited. For this, the necessary mean heater voltage is determined. The heater voltage is measured at an exhaust pipe wall temperature of 60°C. Above 60°C condensate no longer occurs. So as to reach 300 to 350°C on the ceramic, e.g. a heater voltage UHM of 7.5V is necessary on the LSH25-PL (vehicle-specific). With Te = 100ms the following times result for THVA from the below-mentioned formula.

LSH25P	LSH25PL	LSH25PL	LSF4.7	LSF4.7	
u.cat	u.cat	d.cat	u.cat	d.cat	
0.16s	0.20s	0.58s	0.24s	0.62s	

\*\*\*\*\* Permitted ceramic temperature of the measuring sensor with condensate 350°C, after end of dew point approx. 650°C.\*\*\*\*\*

Determination of the mean heater voltage UHM:

- a) Mount a measuring sensor instead of the Lambda sensor for the ceramic temperature ( from K3-LS/ESV ).  
The measuring sensor should be of the same type (heating performance, protection pipe) as the sensor to be substituted.
- b) Supply the sensor heating via an external constant-voltage source and adjust the voltage UHM such that the desired ceramic temperature (see above) is reached.
- c) Start the vehicle (tmot < 70°C), operate at idling and correct UHM such that the demanded temperature is reached.  
The value UHM is valid at an exhaust pipe wall temperature of 55 to 60°C.  
The measurement should be terminated before the exhaust pipe wall temperature at the location where the sensor is mounted exceeds 60°C.
- d) Calculate the off-time from UHM with the formula given below.



$$THVA = Te * \left( \frac{13V * 13V}{UHM * UHM} - 1 \right)$$

UHM = mean heater voltage for the demanded ceramic temperature  
Te = on-time (0.10s)

Checking of the ceramic temperature:

The exhaust gas temperature model must already have been adjusted. Especially the values in %ATM for end of dew point must be adjusted correctly. In case of too early end of dew point (B.atmtpa=1) cracking of the ceramic may result!

- a1) Connect measuring sensor to the vehicle wiring harness.
- b1) Start vehicle (tmot < 70°C, exhaust pipe wall temperature < 50°C), operate at idling, record the ceramic temperature and the exhaust pipe wall temperature (VS100, thermoscanner).  
(attach the measuring position of pipe wall temperature just in front of the location where the sensor is mounted to the exhaust pipe by a conduit clip)
- c1) In case of deviations of the ceramic temperature from the set point (moment: pipe wall exceeds 60°C) THVA must be corrected. Ceramic temperature too high ==> increase THVA resp. THHA!  
Should the bit end of dew point already have been set prior to this moment, then the %ATM application must be checked.
- d1) After each correction of the off-time the course of the temperature must be checked again in case of a new start.

Hint: The control behaviour of the Lambda control is not good with the temperature-measuring sensor, i.e. the control readiness (B.sbbvk = 1) can be reset during the condensate phase. The control is OK with a normal sensor.

2. UBHS:  $UBHS = 15.5V$

With very high battery voltage (booster start) and extremely cold sensor it is possible that the power stage switches off due to too high heating performance at it. By means of the threshold UBHS the possible heating performance is limited and a switch-off is avoided. The value of UBHS should be around 15 to 16V.

3. TVHSV, TVHSH:  $Time\ to\ reduce\ heating\ after\ start.$

LSH25PL	LSF4.7	
0s	4s	

4. THVAWU THHAWU

LSH25P	LSH25PL	LSH25PL	LSF4.7	LSF4.7	
u.Kat	u.Kat	d.Kat	u.Kat	d.Kat	
THVAWU 0s	0s	-	0.03s	-	
THHAWU -	-	0s	-	0.10s	

In order to avoid ceramic stress the heating is clocked after the start during the time TVHSV/H on the LSF4.7.

5. THEV, THEH:

LSH25	LSH25	LSF4.7	LSF4.7	
u.Kat	d.Kat	u.Kat	d.Kat	
THEV 50s	-	20s	-	
THEH -	0s	-	0s	

Advantage: Maximum heating is again performed if the operating readiness is reset during the condensate phase. To protect the sensor for overheating, it is recommended to limit the time for operating readiness. The maximum value must not be higher than 2 times the normal operating readiness because of overheating protection if the sensor signal cable is defect.

6. USHUV, USHOV:  $USHOV = 0,63V$   $USHUV = 0,37V$

If the sensor voltage is within the limits of the threshold USHUV / USHOV, the sensor heating will be switched on to Maximum when the delay time TVHVMX is exceeded to avoid the reset of the sensor operating readiness condition.

7. TVHVMX = 1s

The delay time for the maximal sensor heating should be higher than the time of the half of one period of the lambda regulation in idle condition.  
(Normal swinging of the sensor voltage thru the threshold USHOV / USHUV should not switch on the heating additionally) .



8. TREHS = 0,1s  
-----

9. THSVKTA/2, THSHKTK/2  
-----

The heating performance of the sensor can be adjusted by this characteristic lines such that a constant ceramic temperature is achieved independent of the exh. gas temp.

The values THSVKTA/TK are dependent on the sensor type. The resistance rinh\_w should be measured with a reference sensor type "PM" at exhaust gas temperature of 650°C. THSHKT should be calibrated that rinh\_w is kept at a constant value. For the sensor upstream catalyst a reduction of the heating performance via THSVKTA in the of 650°C to 800°C is not necessary.

The LSF4.7 is operated at 100°C tabgm with only about 80% heating performance (lesser ceramic stress after end of dew point).

	100°C	200°C	650°C	700°C	750°C	800°C	850°C	900°C
tabgm, tkatm	100°C	200°C	650°C	700°C	750°C	800°C	850°C	900°C
LSH25P vK	0	0	0	0	0	0.10	1,3	2.55s
LSH25PL hK	0	0	0	0.01	0.03	0.16	1,3	2.55s
LSF4.7D2 vK	0.03	0	0	0	0	0	0.8	2.00s
LSF4.7D2 hK	0.03	0	0	0.01	0.02	0.03	0.8	2.00s

10. TMOHSMN  
-----

+-----+  
| TMOHSMN = -10°C |  
+-----+

If the engine temperature is less than the threshold TMOHSMN only a reduced sensor heating is performed.

11. UHSN  
-----

+-----+  
| UHSN = 13.0V |  
+-----+

If the battery voltage is greater than UHSN the heater voltage is clocked, i.e. the heating performance remains constant.

## DLSA 44.20 Lambda sensor aging monitoring

### FDEF DLSA 44.20 Function definition

Function definition of the Lambda sensor aging monitoring

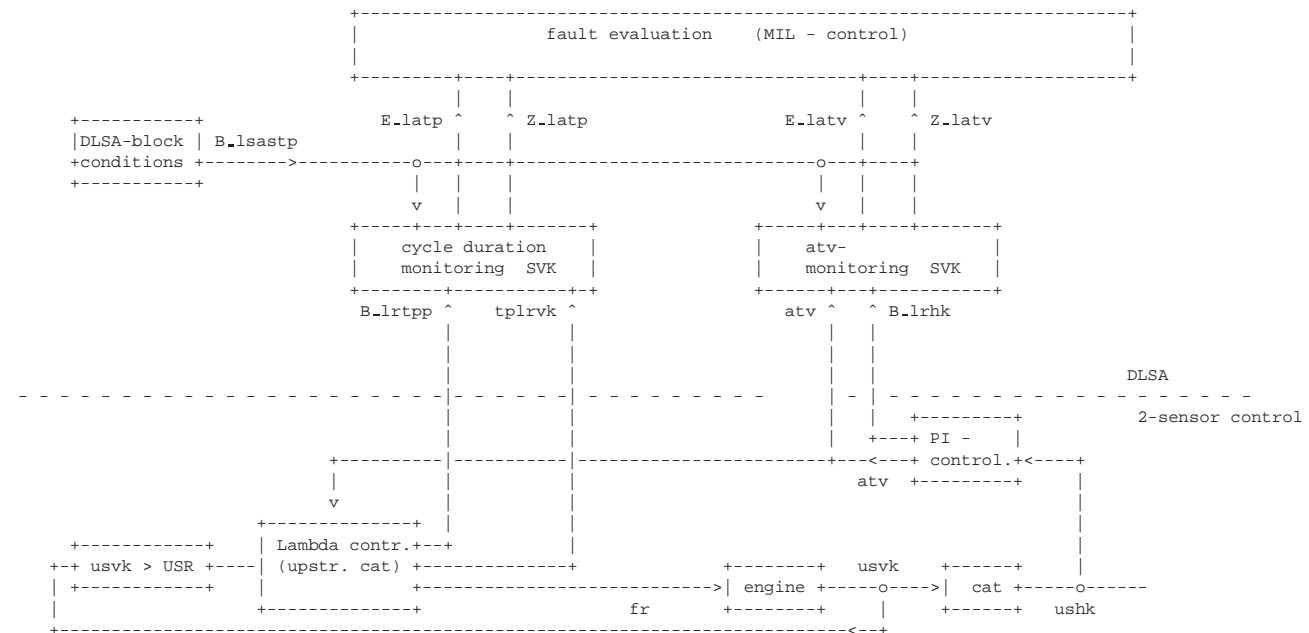
The diagnosis of Lambda sensor aging DLSA serves for detection of upstream lambda sensors, which inadmissibly exceed the emission limits because of aging effects.

For detection of a shifted upstream sensor characteristic the correction factor atv of the superimposed I-controller is used.

This I-controller ensures (for the two-sensor-control) that by means of the controller delay time TV a lawful emission behaviour is obtained, even in case of a sensor characteristic shift.

For detection of an upstream sensor, which is too slow, cycle duration monitoring of the sensor signal is applied.

Overview: "Two Sensor Control and Lambda Sensor Aging Monitoring Upstream Catalyst"



Abbreviations in the block diagram, as far as they are not defined in %DLSA:

atv = regulated variable of the integrator for the reference controller; B\_lr = condition flag for the lambda closed loop control  
B\_lrhk = condition flag for the downstream lambda control; F\_sgnlr = flag, for usvk RICH or LEAN  
fr = control factor; ushk = voltage of downstream sensor; usvk = voltage of upstream sensor; USR = control threshold



In block diagrams fault type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the fault path xyz back into the central diagnosis management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external fault paths which occur as inputs, access methods are available which read these informations directly from the fault path status managed in the DFPM.

For each fault path "wxyz" of this diagnosis function the following values are defined:

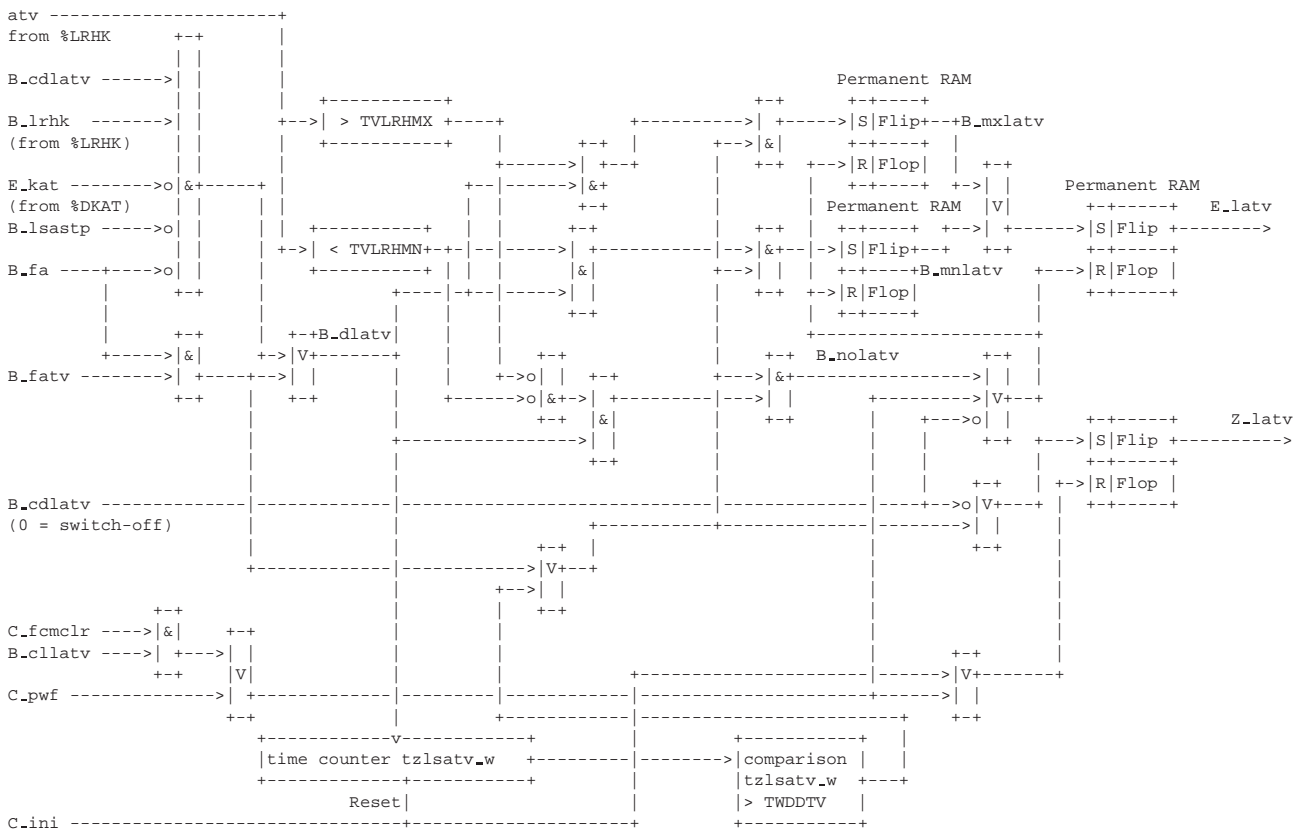
Status fault path wxyz:	sfpwxyz
Error flag wxyz:	E_wxyz
Cycle flag wxyz:	Z_wxyz
Fault type wxyz:	TYP_wxyz: (B_mxwxyz, B_mnwxyz)
Clear fault path:	B_clwxyz
Default value active:	B_bkwxyz (optional)
Fault path code wxyz:	CDTwxxyz
Fault class wxyz:	CLAwxyz
Fault intensity wxyz:	TSFwxyz
CARB CODE wxyz:	CDCwxyz
Table of ambient cond. wxyz:	FFTwxxyz

In this FDEF the following fault paths wxyz are treated:

Fault path name	used abbreviation (substitutes "wxyz")
Lambda sensor upstream CAT cycle duration monitoring bank 1	latp
Lambda sensor upstream CAT cycle duration monitoring bank 2	latp2
Lambda sensor upstream CAT atv monitoring bank 1	latv
Lambda sensor upstream CAT atv monitoring bank 2	latv2

DLSA-SVK atv monitoring (bank1)

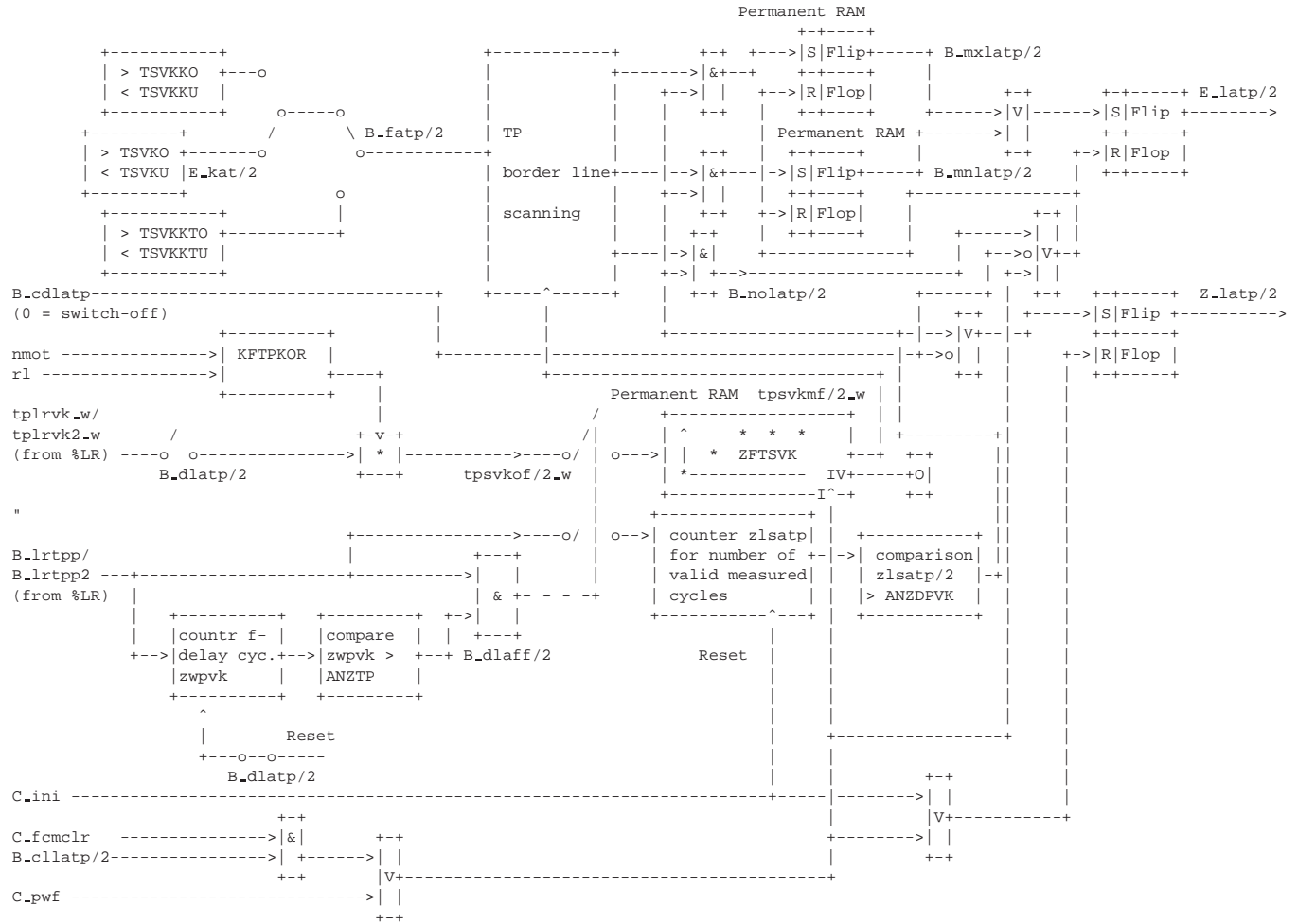
(Bank1)



DLSA-SVK atv monitoring (bank2)



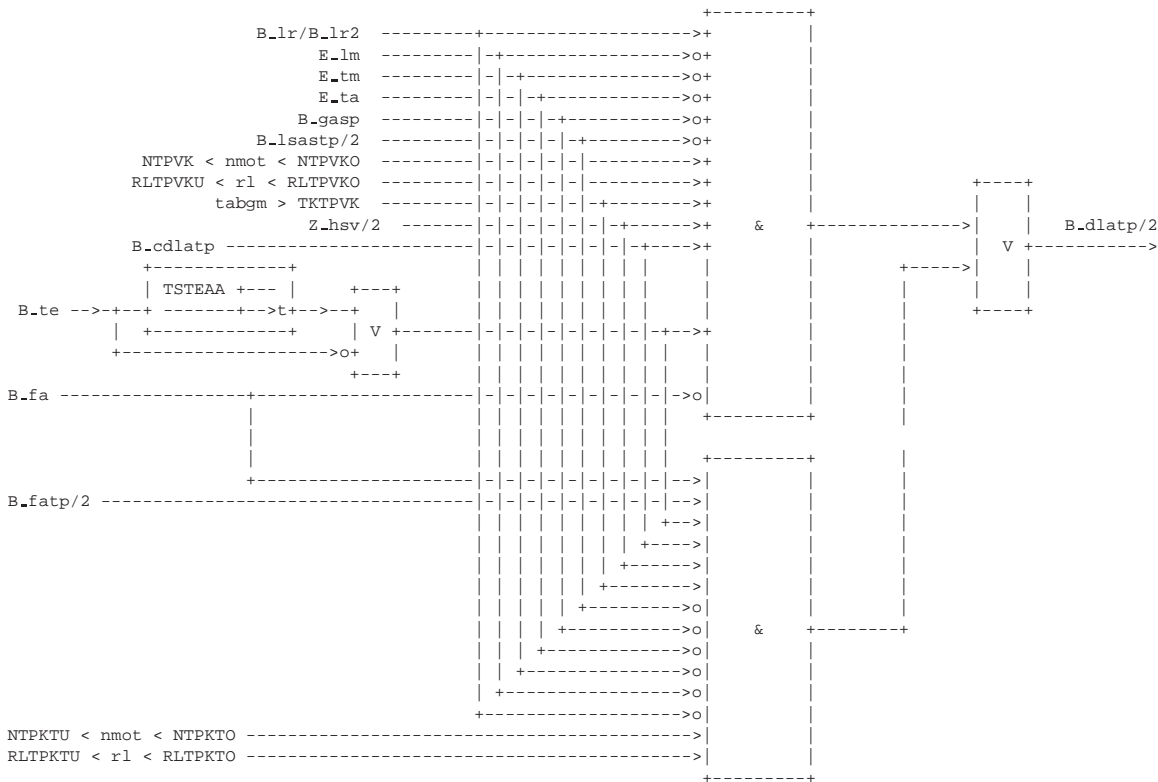




The filters `tpsvkmf_w` and `tpsvkmf2_w` are event-controlled.

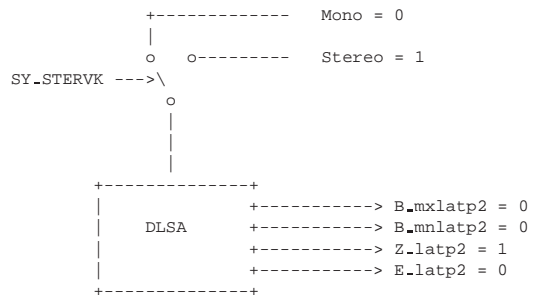
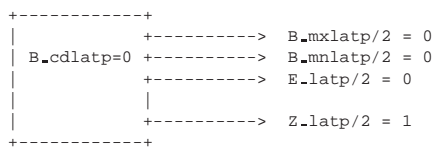


Release function for cycle duration monitoring with short trip



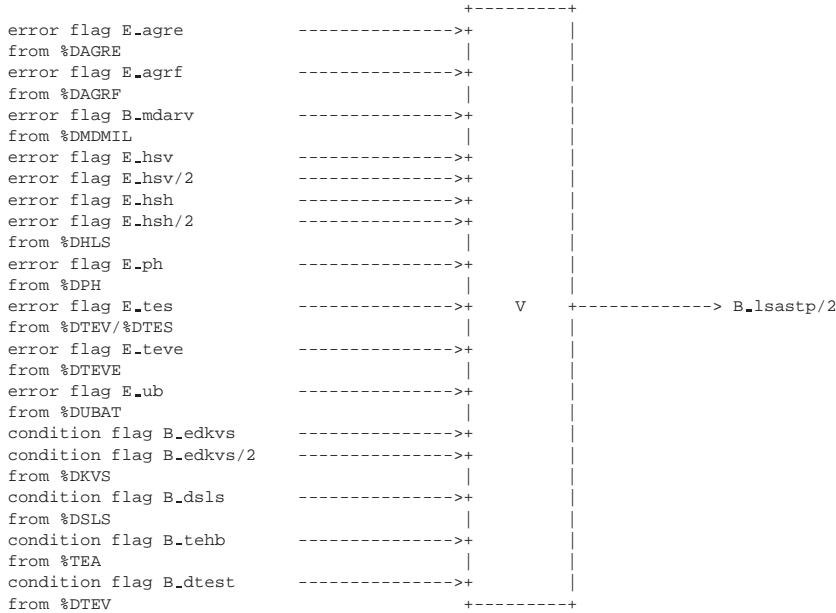
For B\_cdlatp = 0 (switch-off):

For Mono with bit switch-over SY\_STERVK = 0:





Release function for DLSA



### ABK DLSA 44.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ANZDPVK			FW	number of perodes for ready flag of Usvk period monitoring
ANZERTV			FW	amount of error measurements for ATV
ANZTP			FW	number of unconsidered cycles for cycle duration monitoring
CDCLATP	BLOKNR		KL	code word CARB: lambda sensor aging tp
CDCLATP2	BLOKNR		KL	code word CARB: lambda sensor aging tp, cyl. row 2
CDCLATV	BLOKNR		KL	code word CARB: lambda sensor aging tv
CDCLATV2	BLOKNR		KL	code word CARB: lambda sensor aging tv, cyl.row 2
CDLATP			FW	code word oxygen sensor aging diagnosis (TP) in OBDII mode (inv.: in Europe mode)
CDLATV			FW	code word lambda sensor monitoring (Tv) in OBDII mode (invers: Europe mode)
CDTLATP			FW	code word tester: lambda sensor aging tp [015]
CDTLATP2			FW	code word tester: lambda sensor aging tp, cyl.row 2 [021]
CDTLATV			FW	code word tester: lambda sensor aging tv [016]
CDTLATV2			FW	code word tester: lambda sensor aging tv, cyl.row 2 [022]
CIDATV			FW	component ID for ATV single test
CIDATV2			FW	component ID for ATV single test bank2
CIDTP			FW	component ID for period TP single test
CIDTP2			FW	component ID for period TP single test bank2
CLALATP			FW	fault class: O2 sensor aging upstream cat TP
CLALATP2			FW	fault class: O2 sensor aging upstream cat TP bank 2
CLALATV			FW	fault class: O2 sensor aging upstream cat Tv
CLALATV2			FW	fault class: O2 sensor aging upstream cat Tv bank 2
CWDLSA			FW	Code word for single test of O2 sensor aging pre cat for application
FFTLATP	BLOKNR		KL	Table ambient conditions Lambda sensor aging Tp upstream catalyst
FFTLATP2	BLOKNR		KL	Table ambient conditions Lambda sensor aging Tp upstream catalyst bank2
FFTLATV	BLOKNR		KL	Table ambient conditions Lambda sensor aging Tv upstream catalyst
FFTLATV2	BLOKNR		KL	Table ambient conditions Lambda sensor aging Tv upstream catalyst bank2
KFTPKOR	NMOT	RL	KF	correction map for the measured cycle duration TP (tpsvkof)
NTPKTO			FW	upper speed threshold for cycle duration monitoring, short test
NTPKTU			FW	lower speed threshold for cycle duration monitoring, short test
NTPVKO			FW	upper speed threshold for cycle duration monitoring upstream catalyst
NTPVKU			FW	lower speed threshold for cycle duration monitoring upstream catalyst
RLTPKTO			FW	upper load threshold for cycle duration monitoring, short test
RLTPKTU			FW	lower load threshold for cycle duration monitoring, short test
RLTPVKO			FW	upper load threshold for cycle duration monitoring upstream catalyst
RLTPVKU			FW	lower load threshold for cycle duration monitoring upstream catalyst
TKTPVK			FW	exhaust gas temperature (from ATM) for TP monitoring lambda sensor before KAT
TSFLATP			FW	fault active time: lamda sensor ageing time period
TSFLATP2			FW	fault active time: lambda sensor ageing time period, bank 2
TSFLATV			FW	fault active time: lambda sensor aging TV
TSFLATV2			FW	fault active time: lambda sensor ageing TV, bank 2
TSTAAA			FW	inhibit time after condition B_te (canister purge active)
TSVKKO			FW	upper limit of cycle duration of lambda sensor upstream cat at cat fault
TSVKKTO			FW	upper limit for cycle duration of oxygen sensor upstream, short test
TSVKKTU			FW	lower limit for cycle duration of oxygen sensor upstream, short test
TSVKKU			FW	lower limit of cycle duration of lambda sensor upstream cat at cat fault
TSVKO			FW	upper limit for cycle duration of lambda sensor upstream cat
TSVKU			FW	lower limit for cycle duration of lambda sensor upstream cat



Parameter	Source-X	Source-Y	Type	Description
TVLRHMN			FW	lower limit for tv-correction
TVLRHMN2			FW	lower limit for tv-correction unequal parameter bank2
TVLRHMX			FW	upper limit for tv-correction
TVLRHMX2			FW	upper limit for tv-correction unequal parameter bank2
TWDDTV			FW	delay time for readiness flag delta-TV diagnosis
ZFTSVK			FW	time constant for filter cycle duration of sensor upstream catalyst
Variable	Source		Type	Description
ATV	LRHK		EIN	current integrator value of lambda control downstream cat
ATV2	LRHK		EIN	current integrator value of lambda control downstream cat 2
B_CDLATP	PROKON		EIN	function active per codeword CDLATP
B_CDLATV	PROKON		EIN	function active per codeword CDLATV
B_CLLATP			EIN	Clear fault path in DLSA.
B_CLLATP2			EIN	Clear fault path in DLSA. Bank2
B_CLLATV			EIN	Clear fault path in DLSA.
B_CLLATV2			EIN	Clear fault path in DLSA. Bank2
B_DISTP	DLSA		AUS	condition disable period diagnosis and make available measured values for Mode 6
B_DISTP2	DLSA		AUS	cond. disable period diagnosis and make available measured val. for Mode 6 bank2
B_DISTV	DLSA		LOK	condition disable atv diagnosis
B_DISTV2	DLSA		LOK	condition disable atv diagnosis bank2
B_DLAFF	DLSA		LOK	Number of valid Tp measurements reached since B_dlatp=1
B_DLAFF2	DLSA		LOK	Number of valid Tp measurements reached since B_dlatp2=1 bank2
B_DLATP	DLSA		AUS	condition for active diagnosis: lambda sensor aging TP
B_DLATP2	DLSA		AUS	condition for active diagnosis: lambda sensor aging TP (cylinder row 2)
B_DLATV	DLSA		AUS	condition for active diagnosis of lambda sensor aging TV
B_DLATV2	DLSA		AUS	condition for active diagnosis of lambda sensor aging TV (cylinder row 2)
B_DSLS			EIN	condition for active diagnosis of secondary air system
B_DTEST	DTEV		EIN	condition for start of TEV opening
B_EDKVS	DKVS		EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS		EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_ENWS	DNWS		EIN	condition error camshaft control
B_FA			EIN	condition general function request
B_FATP			EIN	condition diagnosis oxygen sensor aging TP function request
B_FATP2			EIN	condition diagnosis oxygen sensor aging TP function request bank2
B_FATV			EIN	condition diagnosis oxygen sensor aging TV function request
B_FATV2			EIN	condition diagnosis oxygen sensor aging TV function request bank2
B_GASP	LRAEB		EIN	condition for basic mixture adaptation disabled
B_GASP2			EIN	condition for basic mixture adaptation disabled, bank2
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRHK	LRHK		EIN	condition for lambda closed loop control downstream cat
B_LRHK2	LRHK		EIN	condition for lambda closed loop control downstream cat (bank 2)
B_LRTPP	LR		EIN	Periodic time valid, static cond. for %LR (amplitude/periodic time) = TRUE
B_LRTPP2	LR		EIN	static condition for lambda controller (amplitude/periodic time) bank2
B_LSASTP	DLSA		LOK	flag for general disabling conditions for DLSA
B_LSASTP2	DLSA		LOK	flag for general disabling conditions for DLSA bank2
B_M6ATV	DLSA		LOK	Schwellen und Codewort an MOD6 übertragen
B_M6ATV2	DLSA		LOK	Schwellen und Codewort an MOD6 übertragen Bank2
B_MAXLATV	DLSA		LOK	Condition for fault type "maximum value" for ATV-test upstr. cat detected 'dyn.'
B_MAXLATV2	DLSA		LOK	Cond. for fault type "max. value" for ATV-test upstr. cat detected 'dyn.' bank2
B_MDARV	DMDMIL		EIN	critical misfire rate detected
B_MINLATV	DLSA		LOK	Condition for fault type "minimum value" for ATV-test upstream cat'dyn.'detected
B_MINLATV2	DLSA		LOK	Cond. for fault type "minimum value" for ATV-test upstr. cat'dyn.'detect. Bank2
B_MNLATP	DLSA		AUS	Condition for fault type "minimum value" of cycle duration upstream cat detected
B_MNLATP2	DLSA		AUS	Condition for fault type "min. value" of cycle duration upstr. cat detec. bank2
B_MNLATV	DLSA		AUS	Condition for fault type "minimum value" for ATV-test upstream cat detected
B_MNLATV2	DLSA		AUS	Condition for fault type "minimum value" for ATV-test upstr. cat detected bank2
B_MXLATP	DLSA		AUS	Condition for fault type "maximum value" for cycle duration upstr. cat detected
B_MXLATP2	DLSA		AUS	Condition for fault type "max.value" for cycle duration upstr. cat detec. bank2
B_MXLATV	DLSA		AUS	Condition for fault type "maximum value" for ATV-test upstream cat detected
B_MXLATV2	DLSA		AUS	Condition for fault type "maximum value" for ATV-test upstr. cat detected bank2
B_NOLATP	DLSA		LOK	Condition diagnosis cycle duration finished with o.k. report
B_NOLATP2	DLSA		LOK	Condition diagnosis cycle duration finished with o.k. report bank2
B_NOLATV	DLSA		LOK	Condition diagnosis atv-test finished with o.k. report
B_NOLATV2	DLSA		LOK	Condition diagnosis atv-test finished with o.k. report bank2
B_TE	TEBEB		EIN	Condition canister purge active
B_TEBB	TEB		EIN	condition for canister purge system with high canister load
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
E_AGRE			EIN	error flag: EGR power stage monitoring
E_AGRF			EIN	error flag: EGR flow monitoring
E_HSH	DHLSHK		EIN	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK		EIN	error flag: lambda sensor heating downstream cat on the right
E_HSV	DHLSVK		EIN	error flag: lambda sensor heating upstream cat
E_HSV2	DHLSVK		EIN	error flag: lambda sensor heating upstream cat on the right
E_KAT	DKAT		EIN	error flag: catalyst conversion
E_KAT2	DKAT		EIN	error flag: catalyst conversion (cylinder row 2)
E_LATP	DLSA		AUS	error flag: lambda sensor aging tp
E_LATP2	DLSA		AUS	error flag: lambda sensor aging tp (cylinder row 2)
E_LATV	DLSA		AUS	error flag: lambda sensor aging tv
E_LATV2	DLSA		AUS	error flag: lambda sensor aging tv (cylinder row 2)



Variable	Source	Type	Description
E_LM	EGFE	EIN	Error flag: main load sensor
E_PH	DPH	EIN	error flag: phase sensor
E_TA	GGTFA	EIN	error flag: TANS
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
E_UB	GGUB	EIN	error flag: power supply voltage UB
M6CATV	DLSA	AUS	Mode 6-Memory: Comp. ID for check Lambda sensor aging TV
M6CATV2	DLSA	AUS	Mode 6-Memory: Comp. ID for check Lambda sensor aging TV on bank 2
M6CTP	DLSA	AUS	Mode 6-Memory: Comp. ID for check Lambda sensor aging TP
M6CTP2	DLSA	AUS	Mode 6-Memory: Comp. ID for check Lambda sensor aging TP on bank 2
M6SATV	DLSA	AUS	Mode 6-Memory: Threshold value with Lambda sensor aging TV
M6SATV2	DLSA	AUS	Mode 6-Memory: Threshold value with Lambda sensor aging TV on bank 2
M6STP2_W	DLSA	AUS	Mode 6-Memory: Threshold value with Lambda sensor aging TP on bank 2
M6STP_W	DLSA	AUS	Mode 6-Memory: Threshold value with Lambda sensor aging TP
M6WATV	DLSA	AUS	Mode 6-Memory: Measured value Lambda sensor aging TV
M6WATV2	DLSA	AUS	Mode 6-Memory: Measured value Lambda sensor aging TV on bank 2
M6WTP2_W	DLSA	AUS	Mode 6-Mem.: Measured value Lambda sensor aging TP on bank 2
M6WTP_W	DLSA	AUS	Mode 6-Mem.: Measured value Lambda sensor aging TP
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SFPLATP	DLSA	AUS	status fault path:
SFPLATP2	DLSA	AUS	status fault path:
SFPLATV	DLSA	AUS	status fault path:
SFPLATV2	DLSA	AUS	status fault path:
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyzt
SY_STERSY	PROKON	EIN	system constant condition stereo lambda control symmetrical
SY_STERSVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TFRN2_W	LR	EIN	time duration lambda controller negativ slope, bank 2
TFRN_W	LR	EIN	time duration lambda controller negativ slope
TFRP2_W		EIN	time duration lambda controller positiv slope, bank 2
TFRP_W		EIN	time duration lambda controller positiv slope
TPLRVK2_W	LR	EIN	cycle duration of sensor upstream cat, calculated by %LR, bank 2
TPLRVK_W	LR	EIN	cycle duration of sensor upstream cat, calculated by %LR
TPOTV2_W	DLSA	LOK	cycle duration of sensor upstream cat, without tv-value bank2
TPOTV_W	DLSA	LOK	cycle duration of sensor upstream cat, without tv-value
TPSVKMF2_W	DLSA	AUS	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (word)
TPSVKMF_W	DLSA	AUS	filtered cycle duration of sensor signal upstream cat. (word)
TPSVKOF2_W	DLSA	LOK	measured cycle duration of sensor upstream cat, without filter, cylinder row 2
TPSVKOF_W	DLSA	LOK	measured cycle duration of sensor upstream cat, without filter
TYP_LATP	DLSA	LOK	Fault type: lambda sensor aging Tp upstream
TYP_LATP2	DLSA	LOK	Fault type: lambda sensor aging Tp upstream bank2
TYP_LATV	DLSA	LOK	Fault type: lambda sensor aging Tv upstream
TYP_LATV2	DLSA	LOK	Fault type: lambda sensor aging Tv upstream bank2
TZLSATV	DLSA	LOK	present time counter value for ready flag of atv-monitoring
TZLSATV2	DLSA	LOK	present time counter value for ready flag of atv-monitoring, cylinder bank 2
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyzt
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyzt 2
USRHK	LRHK	EIN	momentary control threshold for downstream lambda control
USRHK2	LRHK	EIN	momentary control threshold for downstream lambda control, bank2
ZERLATV	DLSA	LOK	counter for error of the atv measurement
ZERLATV2	DLSA	LOK	counter for error of the atv measurement bank2
ZLSATP	DLSA	LOK	present cycle counter for ready flag of cycle duration monitoring
ZLSATP2	DLSA	LOK	present cycle counter for ready flag of cycle duration monitoring, cylinder row2
ZWPVK	DLSA	LOK	waiting cycle counter for cycle duration monitoring
Z_HSH	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat
Z_HSH2	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat, cylinder row 2
Z_HSV	DHLSVK	EIN	cycle flag of lambda sensor heating upstream cat
Z_HSV2	DHLSVK	EIN	cycle flag of lambda sensor heating upstream cat, cylinder row 2
Z_LATP	DLSA	AUS	cycle flag of lambda sensor aging tp
Z_LATP2	DLSA	AUS	cycle flag of lambda sensor aging tp (cylinder row 2)
Z_LATV	DLSA	AUS	cycle flag of lambda sensor aging tv
Z_LATV2	DLSA	AUS	cycle flag of lambda sensor aging tv (cylinder row 2)
Parameter	Value	Description	
ANZDPVK		number of perodes for ready flag of Usvk period monitoring	
ANZERTV		amount of error measurements for ATV	
ANZTP		number of unconsidered cycles for cycle duration monitoring	
CDLATP		code word oxgen sensor aging diagnosis (TP) in OBDII mode (inv.: in Europe mode)	
CDLATV		code word lambda sensor monitoring (Tv) in OBDII mode (invers: Europe mode)	
CDTLATP		code word tester: lambda sensor aging tp [015]	
CDTLATP2		code word tester: lambda sensor aging tp, cyl.row 2 [021]	
CDTLATV		code word tester: lambda sensor aging tv [016]	
CDTLATV2		code word tester: lambda sensor aging tv, cyl.row 2 [022]	
CIDATV		component ID for ATV single test	
CIDATV2		component ID for ATV single test bank2	
CIDTP		component ID for period TP single test	
CIDTP2		component ID for period TP single test bank2	
CLALATP		fault class: O2 sensor aging upstream cat TP	



Parameter	Value	Description
CLALATP2		fault class: O2 sensor aging upstream cat TP bank 2
CLALATV		fault class: O2 sensor aging upstream cat Tv
CLALATV2		fault class: O2 sensor aging upstream cat Tv bank 2
CWDLSA		Code word for single test of O2 sensor aging pre cat for application
NTPKTO		upper speed threshold for cycle duration monitoring, short test
NTPKTU		lower speed threshold for cycle duration monitoring, short test
NTPVKO		upper speed threshold for cycle duration monitoring upstream catalyst
NTPVKU		lower speed threshold for cycle duration monitoring upstream catalyst
RLTPKTO		upper load threshold for cycle duration monitoring, short test
RLTPKTU		lower load threshold for cycle duration monitoring, short test
RLTPVKO		upper load threshold for cycle duration monitoring upstream catalyst
RLTPVKU		lower load threshold for cycle duration monitoring upstream catalyst
TKTPVK		exhaust gas temperature (from ATM) for TP monitoring lambda sensor before KAT
TSFLATP		fault active time: lamda sensor ageing time period
TSFLATP2		fault active time: lambda sensor ageing time period, bank 2
TSFLATV		fault active time: lambda sensor aging TV
TSFLATV2		fault active time: lambda sensor ageing TV, bank 2
TSTEEA		inhibit time after condition B.te (canister purge active)
TSVKKO		upper limit of cycle duration of lambda sensor upstream cat at cat fault
TSVKKTO		upper limit for cycle duration of oxygen sensor upstream, short test
TSVKKTU		lower limit for cycle duration of oxygen sensor upstream, short test
TSVKKU		lower limit of cycle duration of lambda sensor upstream cat at cat fault
TSVKO		upper limit for cycle duration of lambda sensor upstream cat
TSVKU		lower limit for cycle duration of lambda sensor upstream cat
TVLRHMN		lower limit for tv-correction
TVLRHMN2		lower limit for tv-correction unequal parameter bank2
TVLRHMX		upper limit for tv-correction
TVLRHMX2		upper limit for tv-correction unequal parameter bank2
TWDDTV		delay time for readiness flag delta-TV diagnosis
ZFTSVK		time constant for filter cycle duration of sensor upstream catalyst

## FB DLSA 44.20 Detailed description of function

### 1. DLSA TV monitoring of the upstream Lambda sensor

The definition of the function "Monitoring of Lambda sensor aging" is based on a cascade control with a Lambda sensor installed upstream and downstream of the catalyst. In order to create a rich-shift of the mixture, the present Lambda controller is operating with a dp-portion. Now, a two-level controller with I-portion and "P"-portion has been introduced, where the rich shift is caused by the delay time tvlr. The delay time tvlr is constructed by the map KFRTV (constants) and the corrective value tvlrh. The tvlrh value may be positive or negative.

A two-level controller with the control difference from voltage of downstream sensor and a load point dependent voltage set point creates the corrective value tvlrh by means of an integrator (atv: adaptation TV) and the weighting map KFFTV. The corrective value tvlrh increases or decreases the corresponding TV map value, dependent on the changed sensor characteristics, which result in the course of the sensor life.

The atv-diagnosis is only activated, if the fault flag of DKAT (catalyst diagnosis) has not been set, i.e., the catalyst is working properly. This check is required due to the fact that an aged or defective catalyst can cause a TV-shift. A Lambda sensor which may only cause a marginal TV-shift, can therefore be detected as defective. However, a defective upstream lambda sensor blocks the DKAT, i.e., a defective catalyst could not be detected without this check. Therefore, in case a catalyst is detected as defective, only the dynamic properties of the upstream lambda sensor are monitored. Furthermore the general DLSA turn-on condition (F.lsastp) has to be fulfilled and the downstream lambda control (B.lrhk) must be active.

The evaluation routine includes the comparison of the atv value with the upper and lower threshold for the DLSA (TVLRHMX, TVLRHMN). By B.stersy = 0 a switch-over is performed for bank2 to not equal parameter TVLRHMN2 and TVLRHMX2.

If the regulated variable atv is below TVLRHMN (falling short of the minimum) or above TVLRHMX (exceeding the maximum), then the sensor error flag E.latv is set, due to a poor upstream lambda sensor. In case the atv-value is between TVLRHMN and TVLRHMX (no error), then the sensor error flag E.latv will not be set.

The ready-flag Z.latv for the atv-diagnosis of DLSA is only set, if the momentary time count (tzlsatv) is equal to or exceeds the reference time TWDDTV.

#### Quicktest:

If a scan tool is connected, (B.fa = 1), the atv monitoring of the DLSA is disabled until the command for the atv-quicktest (B.fatv = 1) is received. Since the LRHK control value is relatively slow, no real test for characteristically shifted front sensor is performed. During the atv quicktest the cycle flag Z.latv is set immediately, the actual atv value compared with the border thresholds (TVLRHMN, TVLRHMX) and the result transmitted via E.latv.

### 2. DLSA cycle duration monitoring of the upstream Lambda sensor

Cycle duration monitoring of the upstream sensor is required due to the fact that the dynamic properties may deteriorate, the mean sensor voltage, however, remains constant. This dynamic shift of the lambda sensor characteristic may result in exceeding the emission limits.

The cycle duration is determined in the lambda control %LR. In the process the P-portion and the tv-time from the catalyst deoxidization are automatically excluded from the calculation.

An incorrectly measured cycle duration (B.lrtpp = FALSE) is not taken over into the filter for the formation of the TP-mean value. The measurement of the cycle duration only takes place in an adjustable engine speed, load range. If the engine speed, load window is entered for the monitoring of the cycle duration, also a definable number of valid measured cycles (ANZTP) can be disabled. Together with the steady-state condition of the %LR this possibility is necessary to make the DLSA cycle duration monitoring immune against interferences. In order to be able to increase the detection range and thus to increase the number of detected



cycles, the cycle duration is weighted by the factor KFTPKOR. By this factor the operating point dependent influence of dead time and response time of the sensor on the cycle duration is described. The corrective map KFTPKOR is the same map as the weighting map KFFTV in %LRHK and it must therefore not be adjusted again.

In order to avoid excessively long cycle durations (caused by Lambda deviations) during the transient stage of mixture adaptation, and canister purge adaptation, the condition flag B\_te is monitored. Disturbances which can be caused by canister purging at the beginning of a purge control phase are eliminated by means of the blocking time TSTEAA.

The delay counter zwpvk is only reset, when the condition flag B\_dlatp releases the cycle duration monitoring.

Tpsvkmf is initialized with 0 in the event of powerfail or when clearing the fault memory. Thereafter tpsvkmf=tpsvkof is set at the first valid measurement of the cycle duration. Otherwise tpsvkmf is initialized with the last value stored in the RAM.

The mean value of the cycle duration of upstream lambda sensor is compared with an upper and lower limit. It has been proven efficient to operate with two pairs of fault thresholds (TSVKO, TSVKU and TSVKKATO, TSVKKATU). If the catalyst monitoring has detected a fault, then the cycle duration of the upstream sensor signal is compared with more stringent fault thresholds. By evaluating the amplitude ratio (usvk/ushk), a slower upstream sensor may erroneously result in considering a properly working (border line) catalyst as insufficient (concerning emissions). This comparison takes place in an operating point, where the differences in cycle durations between "good" and "slow" lambda sensors are at a maximum. Depending on the momentary cycle duration of the sensor signal, within the predetermined duration limits or outside, the MIL is/is not activated by the fault evaluation algorithm by means of the cycle duration monitoring of the upstream sensor.

If a defective lambda sensor has been detected, based on the above procedure, then "Fault dynamic sensor characteristic" (slow sensor) must be reported to the diagnosis routine via the flag E\_latp.

The ready flag Z\_latp for cycle duration monitoring is set after ANZDPVK measured cycles, which are valid. The cycle counter zlsatp is reset during cranking.

#### Quicktest:

If a scan tool is connected, (B\_fa = 1), the cycle duration monitoring of the DLSA is disabled until the command for the quicktest of cycle duration (B\_fatp = 1) is received. This quicktest is performed in its own engine operating area (zero load, increased RPM). The cycle duration in this area is compared with the quicktest specific thresholds (TSVKKTO, TSVKKTU).

#### 4. General DLSA turn-on conditions

For the DLSA, the following cross-connections with other OBD II diagnosis functions are relevant:

Function:	Processed by means of:
DAGRE Diagnosis EGR power stage	B_lsastp
DAGRF Diagnosis EGR	B_lsastp
DASE Diagnosis misfire detection (emission relevant)	B_lsastp
DEV Diagnosis injectors	LRVK and LRHK
DHFM Diagnosis load sensing	E_lm directly
DHLS Diagnosis sensor heating	B_lsastp
DKAT Diagnosis catalyst conversion	E_kat directly
DKVS Diagnosis fuel supply system	B_lsastp
DLSH Diagnosis downstream lambda sensor	LRHK
DLSV Diagnosis upstream lambda sensor	LRVK and LRHK
DPH Diagnosis phase sensor	B_lsastp
DSL S Diagnosis secondary air system	B_dsls
DTEV/DTES Diagnosis canister purge valve	B_lsastp
DTEVE Diagnosis canister purge valve (driver stage)	B_lsastp
DUBAT Diagnosis UBAT	B_lsastp

During active DLSA, the DSL S (diagnosis of secondary air system) must not be turned on. This is considered by the condition flag B\_dsls. The Lambda closed-loop control is active, when the diagnosis of the secondary air system is performed. However, the cycle duration of the sensor signal and the correction factor of the downstream lambda control are inadmissibly influenced by the operation of the secondary air pump. Therefore, this interaction between DLSA and DSL S must be interrupted by means of the flag B\_dsls.

If the DTEV (diagnosis of canister purge valve) is active, then the cycle duration monitoring shows a wrong result based on the air-fuel mixture from active carbon filter and canister purge valve. In order to prevent this effect, the flag B\_dtest from the DTEV is checked in the release function for the DLSA.

If B\_dtest is set, then the DLSA is blocked. This occurs, when the canister purge valve is opened for DTEV.

## 5. Stereo version

For stereo exhaust system the three DLSA diagnosis functions must be performed twice, for each exhaust pipe the lambda sensor upstream and downstream catalyst is to be monitored. The general turn-on conditions SY\_STERVK/SY\_STERHK = 1 (stereo) are to be executed.

Scanned error flags of stereo-OBD II functions are to be scanned, combined by an OR function, by the DLSA turn-on conditions.

## 6. Measures to be taken in case of clearing of the fault memory or in the event of powerfail

If the fault memory is cleared or in the event of powerfail, the following conditions for the DLSA are given:

- a.) The filter for the cycle duration monitoring is initialized, i.e. the starting value for tpsvkmf is again the first valid measurement of the cycle duration value.
- b.) The cycle time counter tzlsatv is reset.
- c.) The counter for delay cycles zwpvk is reset.
- d.) The cycle counter zlsatp is reset.

## APP DLSA 44.20 Application hint

### Application hints

DLSA - European version (selected via EURO bits)

For the European version, the DLSA-atv-monitoring, the DLSA cycle duration monitoring, and the DLSA oscillation check can be turned off. The partial functions are then not longer processed.

atv-monitoring can be switched off via the bit B\_cdlatv:

(B\_cdlatv=0) --> atv-monitoring blocked, E\_latv/2 = 0, Z\_latv/2 = 1, B\_dsvkd/2 = 0  
(B\_cdlatv=1) --> atv-monitoring active

Cycle duration monitoring can be switched off via the bit B\_cdlatp:

(B\_cdlatp=0) --> Cycle duration monitoring blocked, E\_latp/2 = 0, Z\_latp/2 = 1  
(B\_cdlatp=1) --> Cycle duration monitoring active

Function-orientated selection of the diagnosis labels in the VS100:

Fault memory relevant values of the diagnosis function xyz are assigned to the function DFPM\_xyz in the function-orientated selection.

Requirements for DLSA calibration:

The two sensor Lambda control and the transient control must have been completely calibrated:

Parameters to be calibrated:

The classification between properly working and defective upstream lambda sensors is carried out by means of the DLSA fault limits TVLRHMx, TVLRHMn, TSVKO, TSVKU, TSVKKATO and TSVKKATU.

It is very unlikely that the lower fault limits for cycle duration monitoring (TSVKU, TSVKKATU) ever will be used for sensor evaluation, since upstream sensors with faster response time do not have a negative impact on emissions. However, the lower limits could be possibly used for detection of "chemical noise".

The constant ZFTSVK determines the filter time constant of the upstream sensor cycle duration monitoring. The lower ZFTSVK, the less the influence of the next input value on the filter output.

With ANZTP, the number of valid measured periods at entrance into the defined n-, t1-window can be calibrated, which are neglected. In order to carry over as many as possible valid periods into the filter, ANZTP should reflect a low value.

NTPVKU, NTPVKO, TLTPVKU and TLTPVKO determine the n-, t1-window, in which the cycle duration monitoring is performed.

TWDDTV is the time threshold, at which the ready flag for atv-monitoring is set.

ANZDPVK contains the minimum number of measured usvk-periods of the cycle duration monitoring, before the ready flag can be set for this diagnosis section.

Disturbances, which may occur during the transition stage between mixture adaptation and purge control adaptation, are suppressed by means of the blocking time TSTEAA. Cycle duration monitoring will be only released if the condition flag B\_te is still set after the blocking time TSTEAA or the mixture adaptation is active. By this, excessively long cycle durations at the beginning of a canister purge phase can be suppressed.



Calibration values:

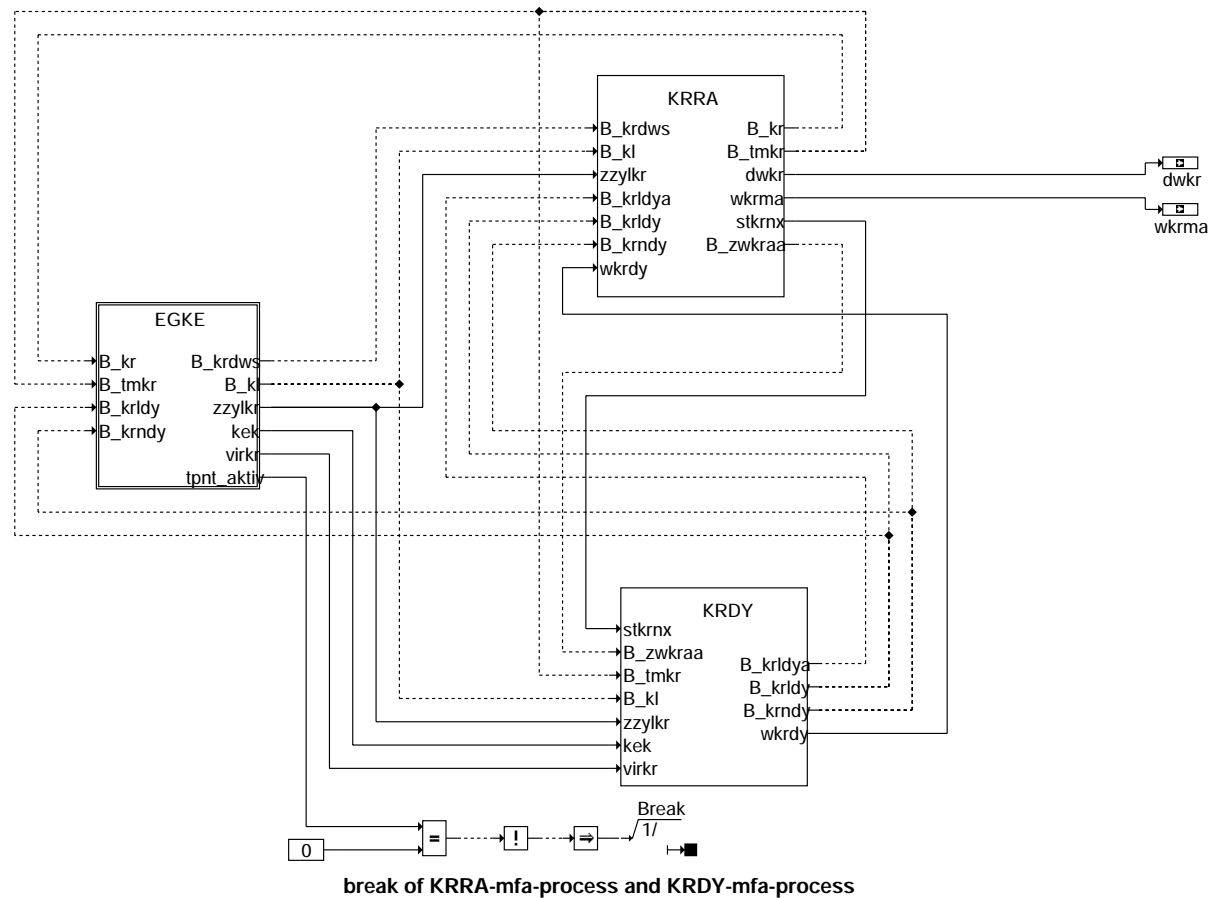
ANZDPVK	20
ANZTP	1
NTPVKO	2400 rpm
NTPVKU	1800 rpm
NTPKTO	1800 rpm short trip
NTPKTU	1000 rpm short trip
RLTPVKO	70 % upper load in the large hill in the FTP 75
RLTPVKU	40 % lower load in the large hill in the FTP 75
RLTPKTO	40 % short trip
RLTPKTU	20 % short trip
TSTEAA	10 s
TVLRHMX	+ 800 ms
TVLRHMN	- 800 ms
ZFTSVK	0.1
TWDDTV	200 s
TSVKO	3 ... 5 s dependent on catalyst volume
TSVKU	0.2 s
TSVKKTO	3 ... 5 s dependent on catalyst volume
TSVKKTU	0.2 s
TSVKKO	2 ... 4 s dependent on catalyst volume
TSVKKU	0.2 s

## EGKE 1.10 Input variables for knocking detection

### FDEF EGKE 1.10 Function definition

KUE: overview knock control

=====

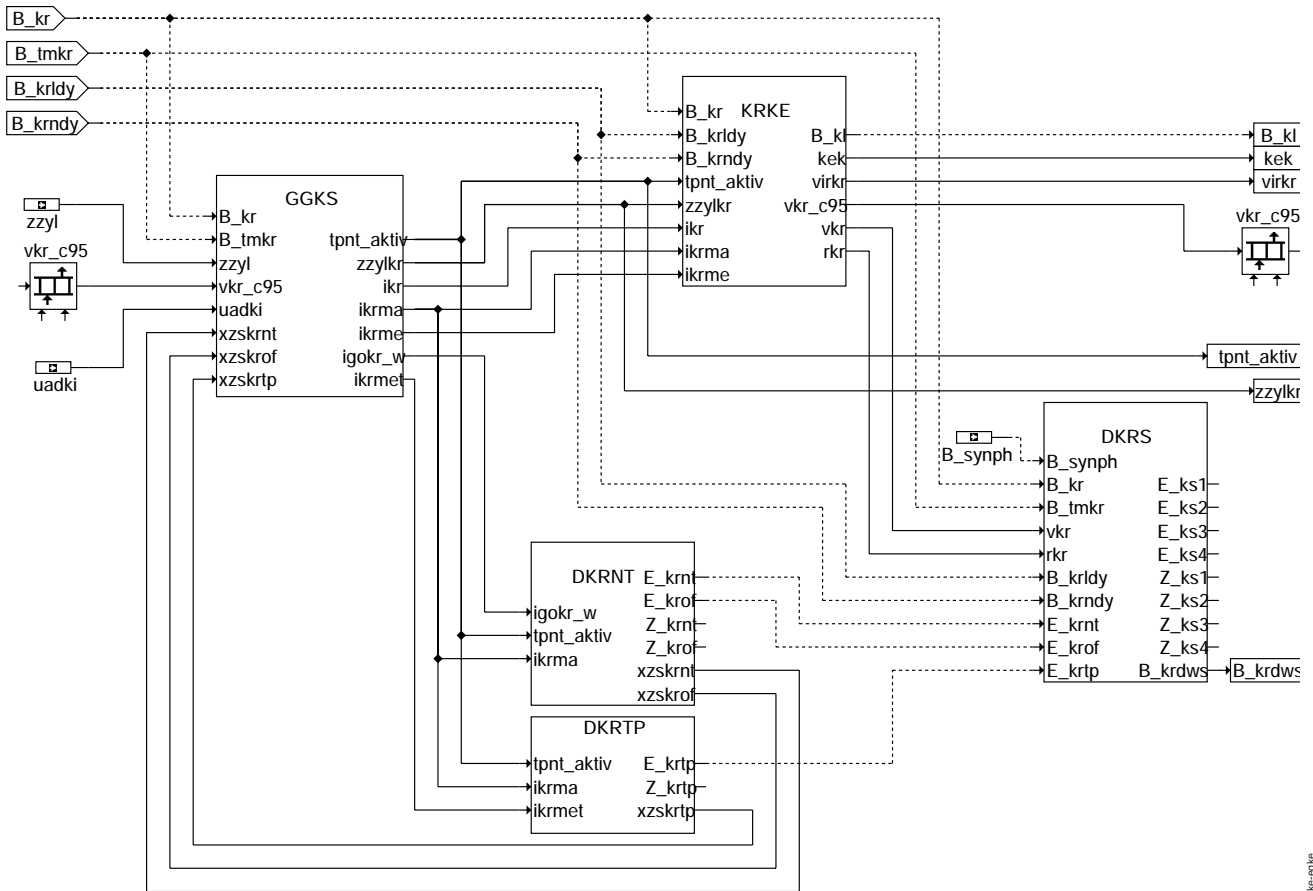


egke-main

egke-main

EGKE: input variables

=====



egke-egke

### ABK EGKE 1.10 Abbreviations

Variable	Source	Type	Description
B_KL	EGKE	AUS	condition for knocking
B_KR	KRRA	EIN	condition for knock control active
B_KRDWS	EGKE	AUS	condition knock control safety ignition retarding
B_KRLDY	KRDY	EIN	Condition load dynamics for knock detection active
B_KRLDYA	EGKE	LOK	Condition load dynamics retard and dynamics adaptation active
B_KRNDY	KRDY	EIN	condition speed dynamics for knock detection active
B_SYNPH	GGDPP	EIN	condition synchronization phase
B_TMKR	KRRA	EIN	Condition temperature (tmot) for knock control achieved
B_ZWKRAA	EGKE	LOK	condition ignition angle of the KC is given
DWKR	EGKE	AUS	cylinder-specific ignition-timing retardation
E_KRNT	EGKE	LOK	error flag: knock control zero test
E_KROF	EGKE	LOK	Errorflag: knock control offset
E_KRTP	EGKE	LOK	error flag: knock control test pulse
E_KS1	EGKE	LOK	error flag: knock sensor 1
E_KS2	EGKE	LOK	error flag: knock sensor 2
E_KS3	EGKE	LOK	error flag: knock sensor 3
E_KS4	EGKE	LOK	error flag: knock sensor 4
IGOKR_W	EGKE	LOK	integrator gradient for offset correction knock control (word)
IKR	EGKE	LOK	integrator value with offset correction
IKRMA	EGKE	LOK	integrator value at start of measurement window, knock control
IKRME	EGKE	LOK	integrator value at end of measurement window, knock control
IKRMET	EGKE	LOK	integrator value at end of measurement window, knock control test pulse
KEK	EGKE	AUS	knock detection threshold corrected
RKR	EGKE	LOK	reference level knock control
STKRNX	EGKE	LOK	speed range adaption map KC
TPNT_AKTIV	EGKE	AUS	activation of kc-functions
UADKI		EIN	current integrator value
VIRKR	EGKE	AUS	Ratio: integrator / reference level knock control
VKR	EGKE	LOK	amplification stage knock control
VKR_C95	EGKE	LOK	amplification stage for input amplification stage of knock-IC
WKRDY	EGKE	LOK	ignition retard during dyn-function of knock control
WKRMA	EGKE	AUS	Average value of ignition retarding by KC, generally (limpe home with safety)
XZSKRNT	EGKE	LOK	safety counter for knock control zero test
XZSKROF	EGKE	LOK	safety counter for knock control offset



Variable	Source	Type	Description
XZSKRTP	EGKE	LOK	Timer knock control error flag E_krtp
ZZYL	GGDPG	EIN	SW-cylinder counter
ZZYLKR	EGKE	AUS	cylinder counter KC
Z_KRNT	EGKE	LOK	cycle flag: knock control zero test
Z_KROF	EGKE	LOK	cycle flag: knock control offset
Z_KRTP	EGKE	LOK	cycle flag: knock control test pulse
Z_KS1	EGKE	LOK	cycle flag: knock sensor 1
Z_KS2	EGKE	LOK	cycle flag: knock sensor 2
Z_KS3	EGKE	LOK	cycle flag: knock sensor 3
Z_KS4	EGKE	LOK	cycle flag: knock sensor 4

### FW EGKE 1.10 Fixed Values

Parameter	Value	Description
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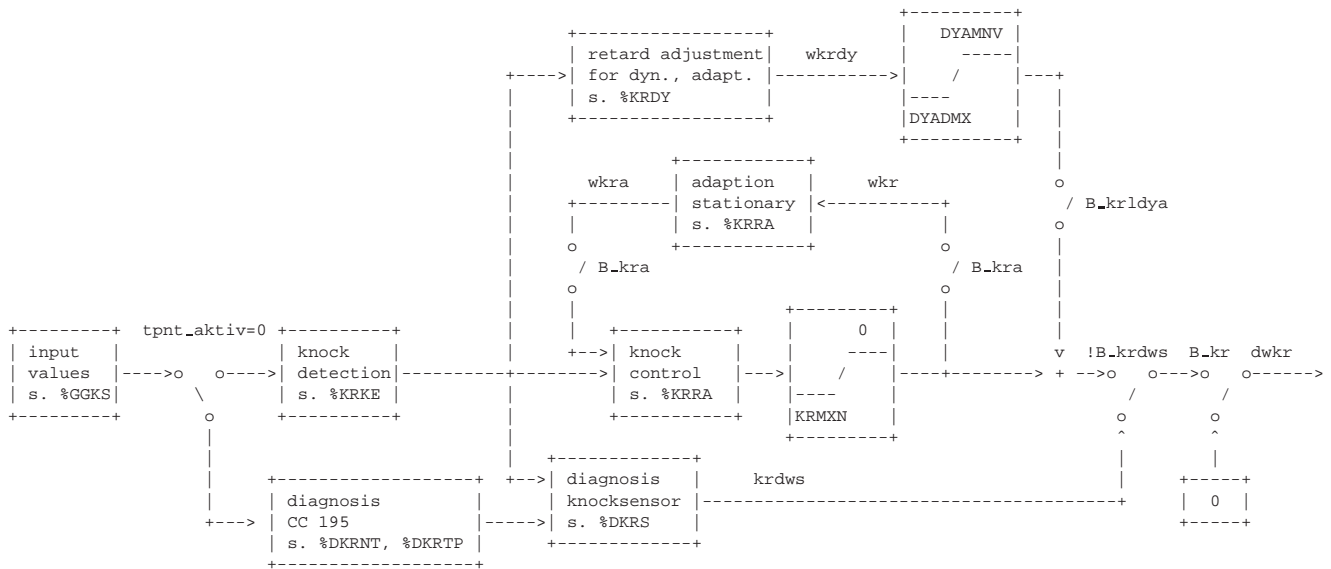
### FB EGKE 1.10 Detailed description of function

EGKE: input variables  
=====

The function group EGKE describes the co-operation of the following functions:

GGKS	control of IC CC195 and signal processing of A/D-converted knock integral uadki	s. %GGKS 2.*
KRKE	knock detection by using the signal processed by GGKS	s. %KRKE 10.*
DKRNT	diagnosis of IC CC195 - test with no signal ("zero") and integrator reset value	s. %DKRNT 4.*
DKRTP	diagnosis of IC CC195 - test with puls	s. %DKRTP 6.*
DKRS	diagnosis of knock sensors and signal path sensor - CC195	s. %DKRS 9.*

KUE: knock control overview  
=====



KUE describes the co-operation of EGKE with KRRA and KRDY:

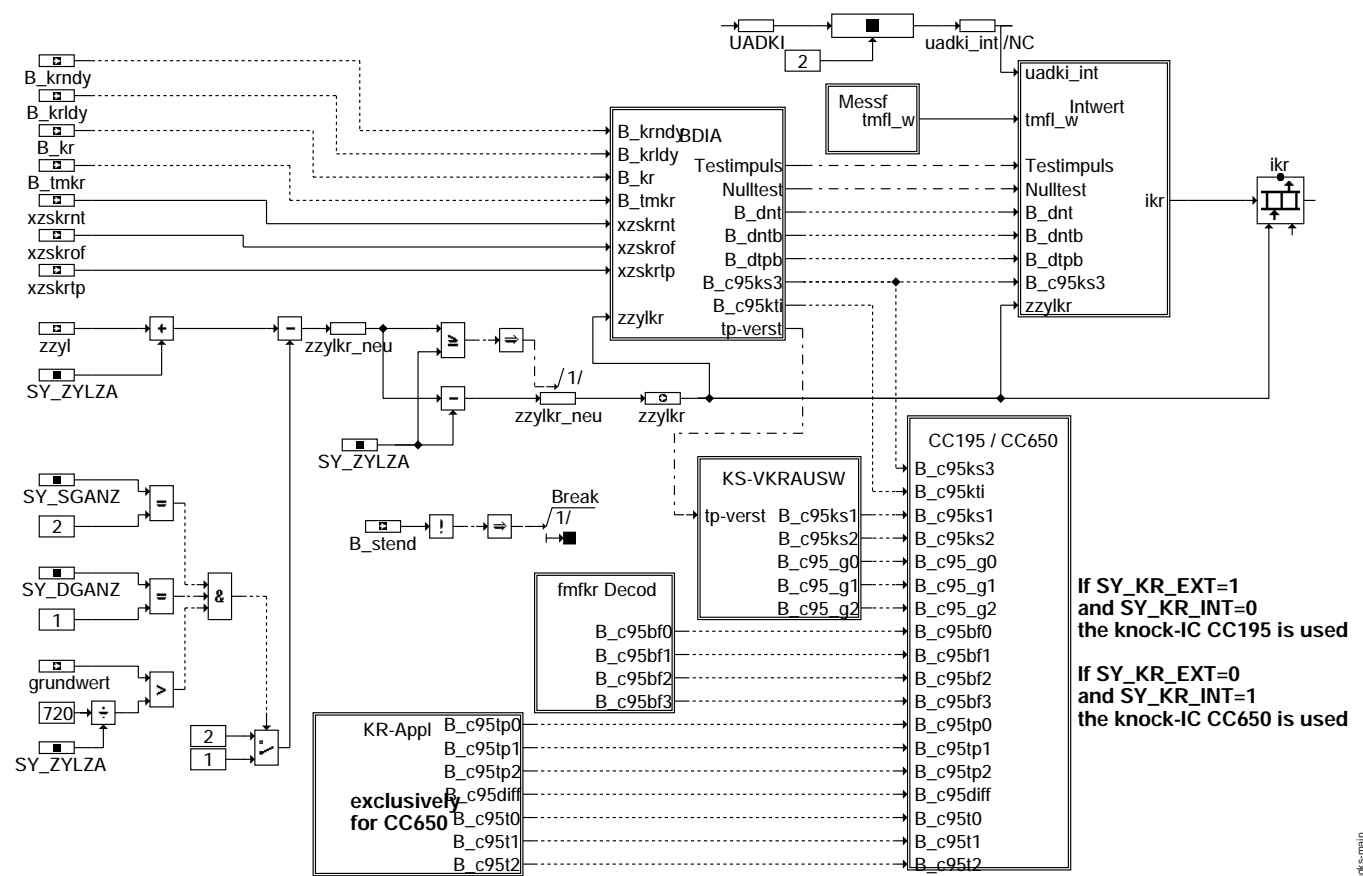
KRRA	control and stationary adaptation of ignition timing retard	s. %KRRA 10.*
KRDY	detection of load and speed dynamics, adaptation of dynamics ignition timing retard	s. %KRDY 10.*

## GGKS 4.50 Sensor signal for knocking detection

### FDEF GGKS 4.50 Function definition

#### GGKS: Sensor signal knock detection

#### reduction of knock integral from 10 to 8-bit



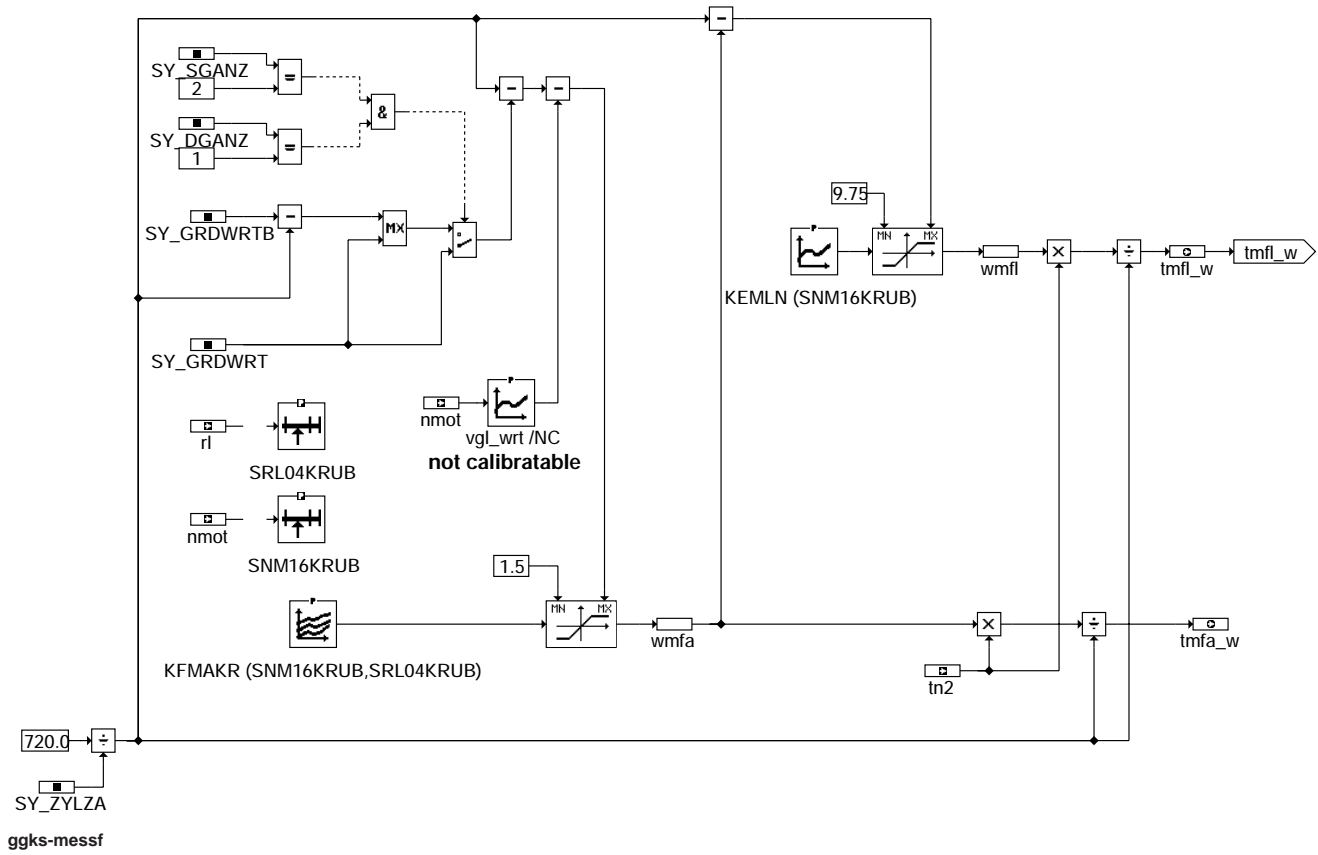
If SY\_KR\_EXT=1  
and SY\_KR\_INT=0  
the knock-IC CC195 is used

If SY\_KR\_EXT=0  
and SY\_KR\_INT=1  
the knock-IC CC650 is used

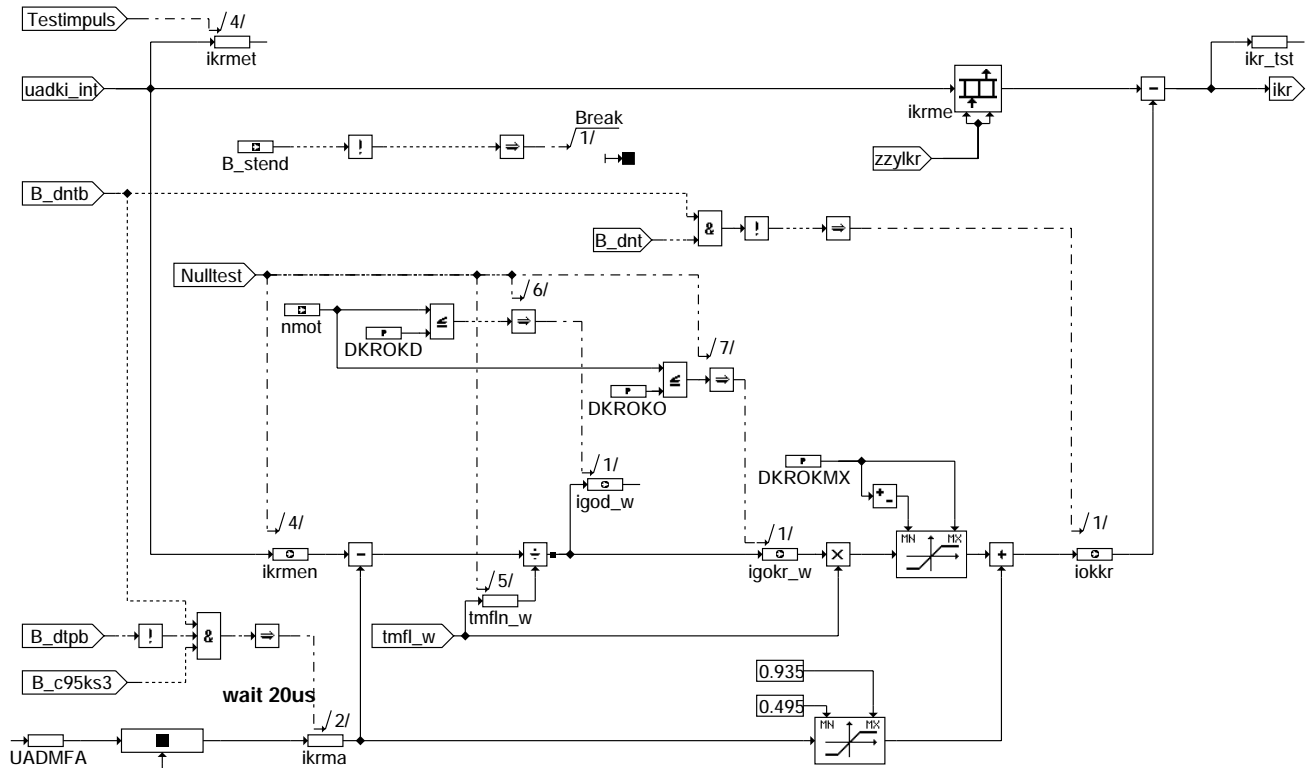
ggks-main

ggks-main

## MESSF: Calculation of beginning and duration of measuring window



### Intwert: Calculation of the offset corrected integrator value

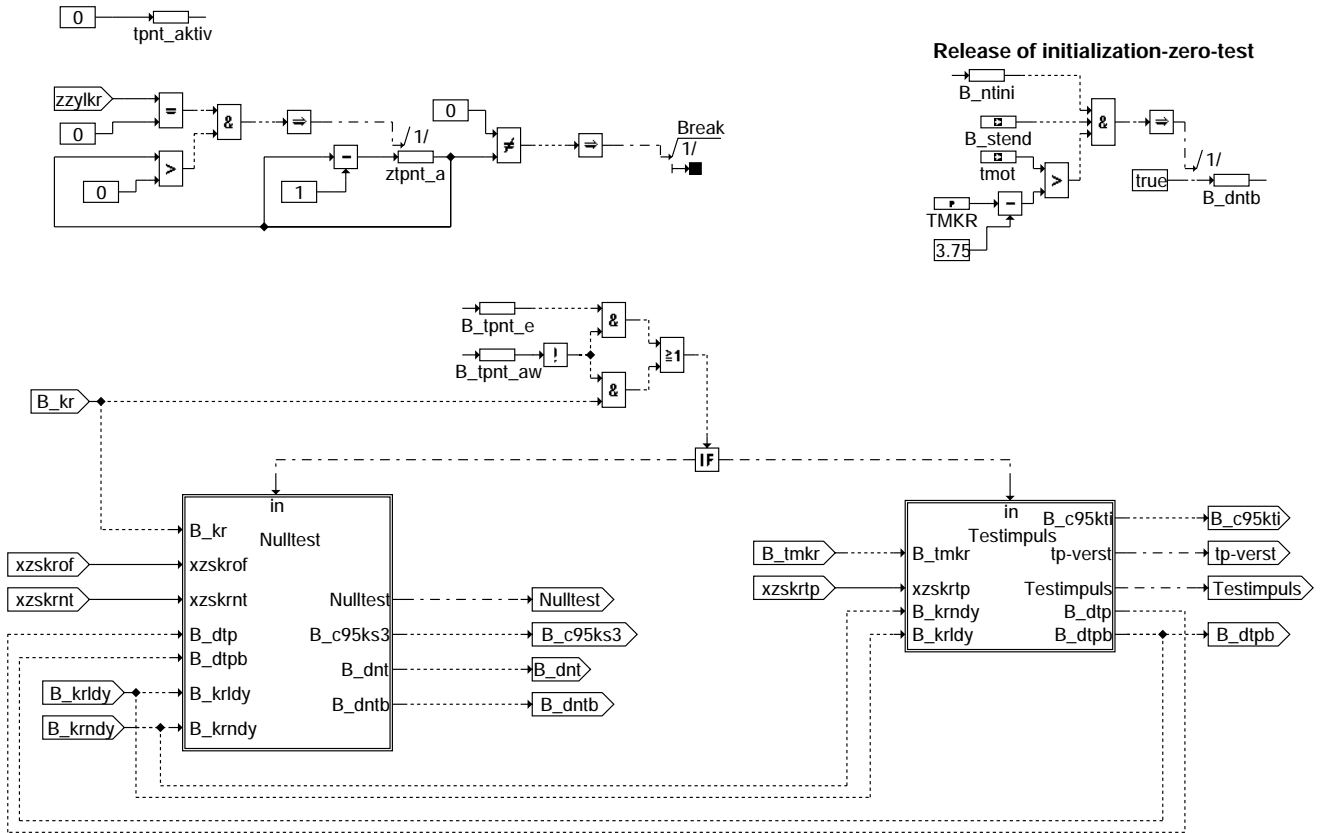


reduction of integrator start value from 10 to 8-bit

ggks-intwert

ggks-intwert

## BDIA: Release of Diagnosis



ggks-bdia

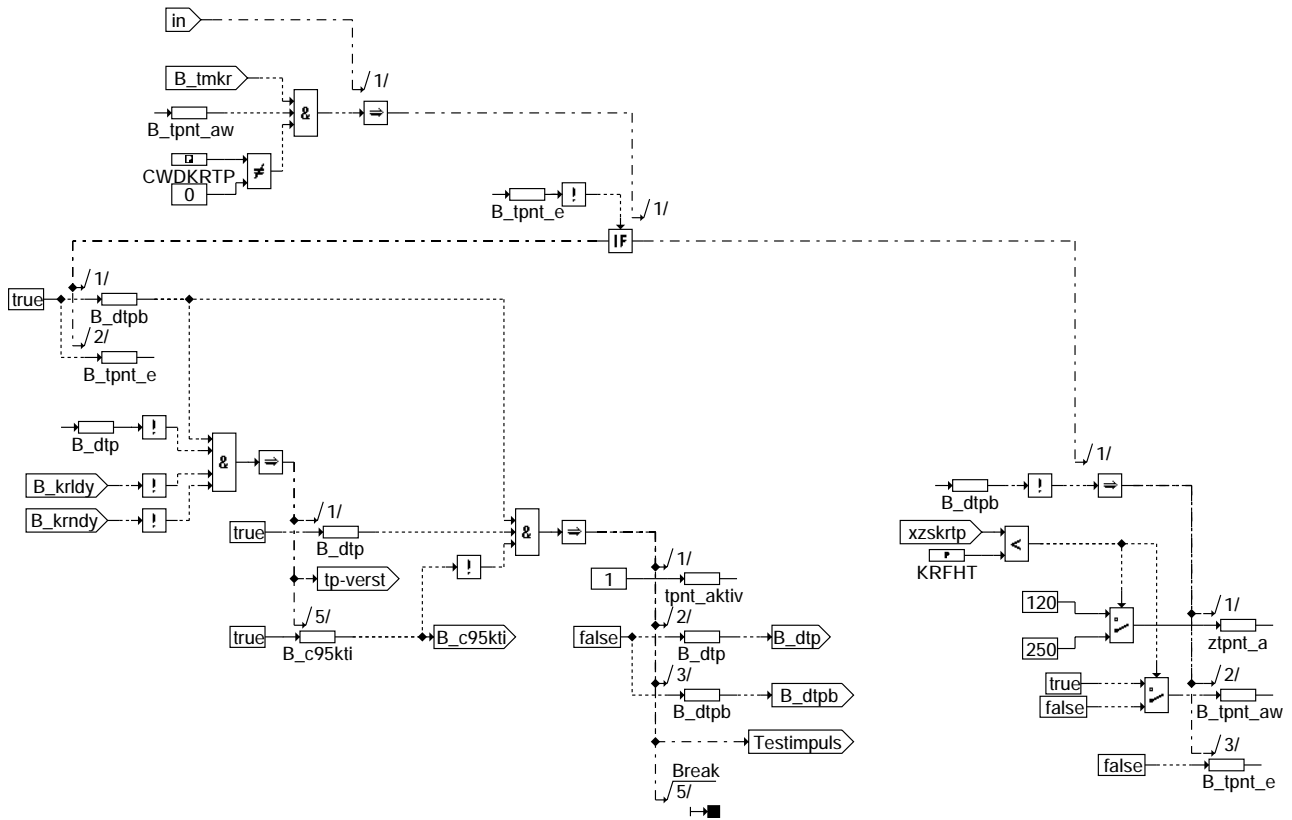
ggks-bdia







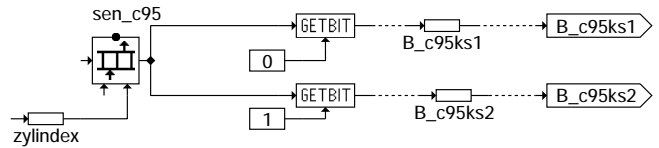
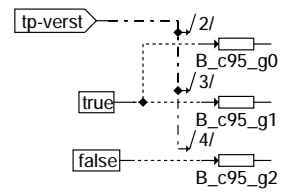
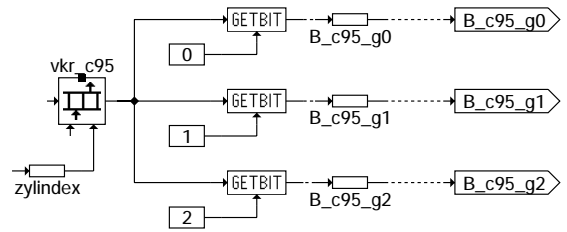
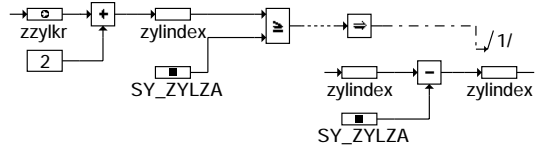
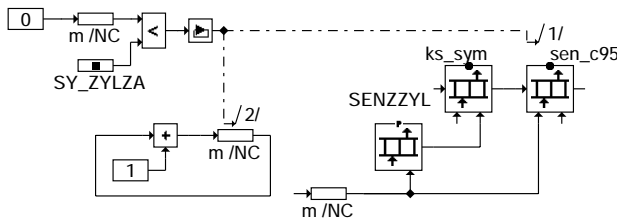
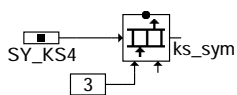
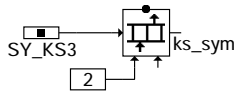
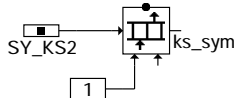
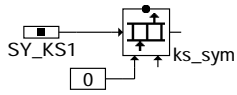
## Testimpuls: Enable Testimpuls



ggks-testimpuls

ggks-testimpuls

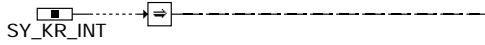
## KS + vkr Auswahl: Choice of the actual knock sensor and amplification level



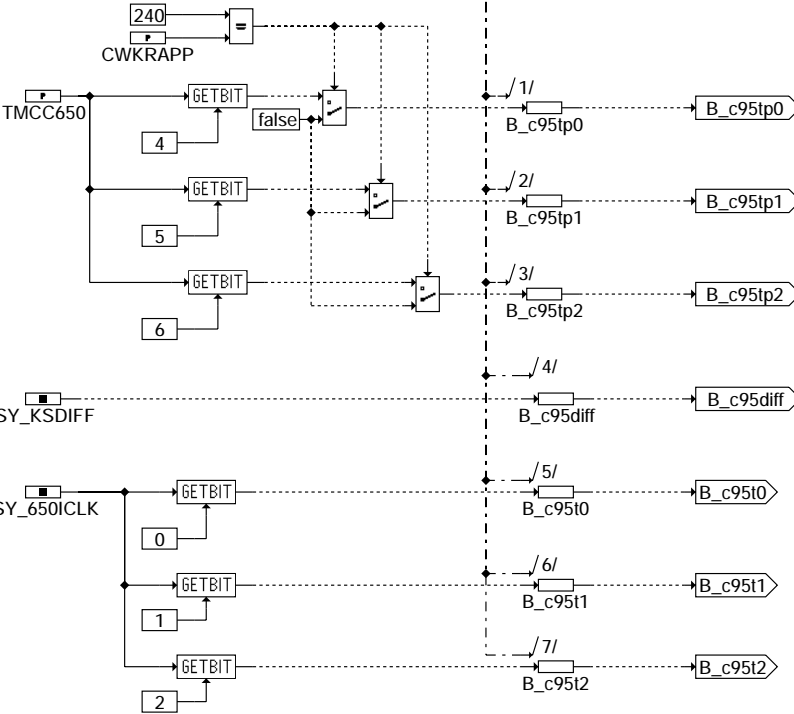
ggks-ks-vkrausw

ggks-ks-vkrausw

## KR-Applikation: test mode



**Attention: exclusivley for CC650**  
**May only be used with an KC-application ECU**



- Test mode CC195 integrated in CC650**  
**TMCC650 KTI/ADT at PIN 61 of CC650**
- 0 KTI-input (asymmetrical sensor mode)
  - 16 internal frequency CC195
  - 32 KTI-input (symmetrical sensor mode)
  - 48 testpulse output
  - 64 filter output
  - 80 rectifier output
  - 96 amplifier output
  - 112 muxer output

different values for TMCC650, like specified in the table, may have major impact on the integrator value uadki.

### SY\_650ICLK | ext. Taktfrequenz

0	8 MHz
1	18 MHz
2	4 MHz
3	10 MHz
4	16 MHz
5	12 MHz
6	14 MHz
7	1 MHz

ggks-kr-appl

## ABK GGKS 4.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWDKRTP			FW (REF)	code word: kc-diagnosis testpulse
CWKRAPP			FW	code word for calibration of kc
DKROKD			FW	upper rpm-limit for zero test diagnosis (knock control)
DKROKMX			FW	maximum offset-compensation value
DKROKO			FW	upper rpm-limit for determination of offset-compensation-value
FMFKRB0			FW	filter mean frequency area 0
FMFKRB1			FW	filter mean frequency area 1
FMFKRB2			FW	filter mean frequency area 2
FMFKRB3			FW	filter mean frequency area 3
KEMLN	NMOT		KL	length of the sampling window for knock control
KFMAKR	NMOT	RL	KF	map for starting measuring window knock control
KRANH			FW (REF)	n hysteresis for adaptation maps
KRFHT			FW	error frequency, test pulse
NKRFM1			FW	revolution threshold for filter mean frequency area 1
NKRFM2			FW	revolution threshold for filter mesn frequency area 2
NKRFM3			FW	revolution threshold for filter mean frequency area 3
SENZZYL			KWB	knock sensor for sw-cylinder counter 0-7
SNM16KRUB	NMOT		SV (REF)	datapoint distribution engine speed, 16 datapoints
SRL04KRUB	RL		SV (REF)	datapoint distribution relative charge, 4 datapoints
SY_650ICLK			SYS (REF)	system constant: external clock frequency of CC650
SY_DGANZ			SYS (REF)	system constant number rotational-speed sensor
SY_GRDWRT			SYS (REF)	System constant basic value, space between SW reference mark to OT in ° KW
SY_GRDWRTB			SYS (REF)	system constant basic value 2.ECU, space between SW reference mark to OT in °KW
SY_KR_INT			SYS (REF)	system constant: CC650 present
SY_KS1			SYS (REF)	system constant: input of the CC195 onto which knock sensor 1 is connected
SY_KS2			SYS (REF)	system constant: input of the CC195 onto which knock sensor 2 is connected
SY_KS3			SYS (REF)	system constant: input of the CC195 onto which knock sensor 3 is connected
SY_KS4			SYS (REF)	system constant: input of the CC195 onto which knock sensor 4 is connected
SY_KSDIFF			SYS (REF)	system constant: connection type of knock sensor(s)
SY_SGANZ			SYS (REF)	system constant number engine control unit
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TMCC650			FW	kc test mode on pin ADT of CC650
TMKR			FW	engine-temperature threshold to enable knock control



Variable	Source	Type	Description
B_C95BF0	GGKS	LOK	signal for control of CC195's filter frequency (pin BF0)
B_C95BF1	GGKS	LOK	signal for control of CC195's filter frequency (pin BF1)
B_C95BF2	GGKS	LOK	signal for control of CC195's filter frequency (pin BF2)
B_C95BF3	GGKS	LOK	signal for control of CC195's filter frequency (pin BF3)
B_C95DIFF	GGKS	LOK	signal for control CC650: connection type of knock sensor(s)
B_C95KS1	GGKS	LOK	signal for control of knock sensor signal's path (pin KSA1)
B_C95KS2	GGKS	LOK	signal for control of knock-sensor signal's path (pin KSA2)
B_C95KS3	GGKS	LOK	signal for control of the zero test of the CC195
B_C95KT1	GGKS	LOK	signal for control of the testimpulse of the CC195
B_C95T0	GGKS	LOK	signal for control CC650: external clock frequency
B_C95T1	GGKS	LOK	signal for control CC650: external clock frequency
B_C95T2	GGKS	LOK	signal for control CC650: external clock frequency
B_C95TP0	GGKS	LOK	signal for control of the testmode of CC195/CC650
B_C95TP1	GGKS	LOK	signal for control of the testmode of CC195/CC650
B_C95TP2	GGKS	LOK	signal for control of the testmode of CC195/CC650
B_C95_G0	GGKS	LOK	signal for control of CC195's amplifier stage (pin G0)
B_C95_G1	GGKS	LOK	signal for control of CC195's amplifier stage (pin G1)
B_C95_G2	GGKS	LOK	signal for control of CC195's amplifier stage (pin G2)
B_DNT	GGKS	LOK	condition for active diagnosis: knock control zero test
B_DNTB	GGKS	LOK	condition : ready for knock control zero test (execution: next measure window)
B_DTP	GGKS	LOK	condition : knock control test pulse active
B_DTPB	GGKS	LOK	condition: ready for knock control test pulse(execution: next measurement window)
B_FMFKRC	GGKS	AUS	filter center frequency of CC195/CC650 changed
B_KR	KRRA	EIN	condition for knock control active
B_KRLDY	KRDY	EIN	Condition load dynamics for knock detection active
B_KRNDY	KRDY	EIN	condition speed dynamics for knock detection active
B_NTINI	GGKS	LOK	kc: condition initialization zero test
B_STEND	BBSTT	EIN	condition end of start
B_TMKR	KRRA	EIN	Condition temperature (tmot) for knock control achieved
B_TPNT_AW	GGKS	LOK	KC: selection zerotest or testimpulse
B_TPNT_E	GGKS	LOK	KC: zero test/ testimpulse enable
FMFKRAKT	GGKS	LOK	filter center frequency of kc bandpass
FMFKRAKTOL	GGKS	LOK	filter center frequency of kc bandpass, old value
FMFW	GGKS	LOK	bit coded filter frequency of kc bandpass
GRUNDWERT		EIN	space between SW reference mark to TDC in °KW
IGOD_W	GGKS	AUS	integrator gradient for zero test diagnosis knock control
IGOKR_W	GGKS	AUS	integrator gradient for offset correction knock control (word)
IKR	GGKS	AUS	integrator value with offset correction
IKRMA	GGKS	LOK	integrator value at start of measurement window, knock control
IKRME	GGKS	LOK	integrator value at end of measurement window, knock control
IKRMEN	GGKS	AUS	integrator value at end of measurement window, knock control zero test
IKRMET	GGKS	LOK	integrator value at end of measurement window, knock control test pulse
IKR_TST	GGKS	LOK	integrator value with offset correction updated with cyl.counter
IOKKR	GGKS	AUS	correction of integrator's offset, knock control
KRFTPAKT	KRKE	EIN	actual low pass characteristic
KS_SYM	GGKS	AUS	Input of the knock evaluation IC
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SEN_C95	GGKS	AUS	knock sensor input at knock evaluation IC
TMFA_W	GGKS	AUS	beginning of measurement window knock control
TMFLN_W	GGKS	LOK	duration of measurement window knock control zero test
TMFL_W	GGKS	AUS	duration of measurement window
TMOT	SWADAP	EIN	Engine temperature
TN2		EIN	Segment time per ignition
TPNT_AKTIV	GGKS	LOK	activation of kc-functions
UADKI	GGKS	LOK	current integrator value
UADMFA	GGKS	LOK	integrator value at start of measurement window
VKR_C95	KRKE	EIN	amplification stage for input amplification stage of knock-IC
WMFA	GGKS	LOK	beginning of measurement window in degree crank angle
WMFL	GGKS	LOK	duration of measurement window in degree crank angle
XZSKRNT	DKRNT	EIN	safety counter for knock control zero test
XZSKROF	DKRNT	EIN	safety counter for knock control offset
XZSKRTP	DKRTP	EIN	Timer knock control error flag E_krtp
ZKRFMU	GGKS	LOK	Counter knock control filter mean frequency change
ZTPNT_A	GGKS	LOK	kc: counter for release of zero test or test pulse
ZYLINDEX	GGKS	LOK	cylinder counter for knock-IC control
ZZYL	GGDPG	EIN	SW-cylinder counter
ZZYLKR	GGKS	AUS	cylinder counter KC

## FW GGKS 4.50 Fixed Values

Parameter	Value	Description
CWKRAPP		code word for calibration of kc
DKROKD		upper rpm-limit for zero test diagnosis (knock control)
DKROKMX		maximum offset-compensation value
DKROKO		upper rpm-limit for determination of offset-compensation-value
FMFKRB0		filter mean frequency area 0
FMFKRB1		filter mean frequency area 1
FMFKRB2		filter mean frequency area 2
FMFKRB3		filter mean frequency area 3
KRFHT		error frequency, test pulse



Parameter	Value	Description
NKRFM1		revolution threshold for filter mean frequency area 1
NKRFM2		revolution threshold for filter mesn frequency area 2
NKRFM3		revolution threshold for filter mean frequency area 3
TMCC650		kc test mode on pin ADT of CC650
TMKR		engine-temperature threshold to enable knock control

### FB GGKS 4.50 Detailed description of function

A knock sensor (piezo-ceramic acceleration sensor) records the combustion noises and converts these into electrical signals. In the evaluation circuit in the ECU which mainly consists of the Bosch IC CC195 or of the CC650, this KS signal consecutively passes through the components multiplexer, control amplifier, active band pass, rectifier and integrator.

The control of the CC195 and of the CC650 (connection of the multiplexer as well as of the cylinder-individual input amplification, starting and stopping of the integrator, selecting the filter center frequency on some ECUs) as well as the signal conditioning in the ECU is realized by the function GGKS.

The signal conditioning in the ECU takes place by an offset correction of the final integrator values.

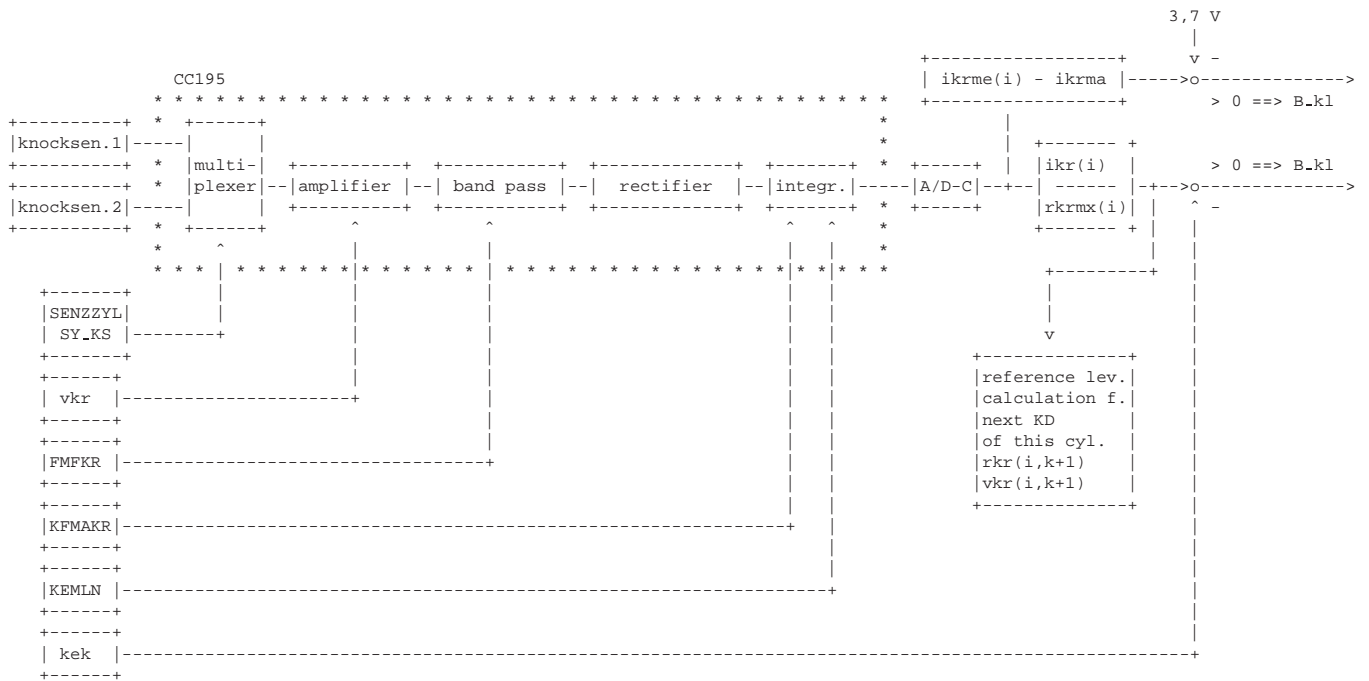
The processing of the signals is identical in the two IC's, since the CC650 is an ASIC into which the CC195 is completely integrated. The only difference existing with regard to the knock control lies in the triggering of the CC195 proportion on the CC650. While the triggering of the CC195 is performed via the hardware, i.e. micro controller ports, it is performed via registers, i. e. a parallel bus, on the CC650.

This calls for a knock control application modus for the CC650 which is controlled by the software.

With the CC195 the corresponding adjustments are made via the KC box.

When the CC195 is mentioned in the following FDEF both chips are ment. Differences will be mentioned explicitly.

The designation of the control signals is identical in both chips.

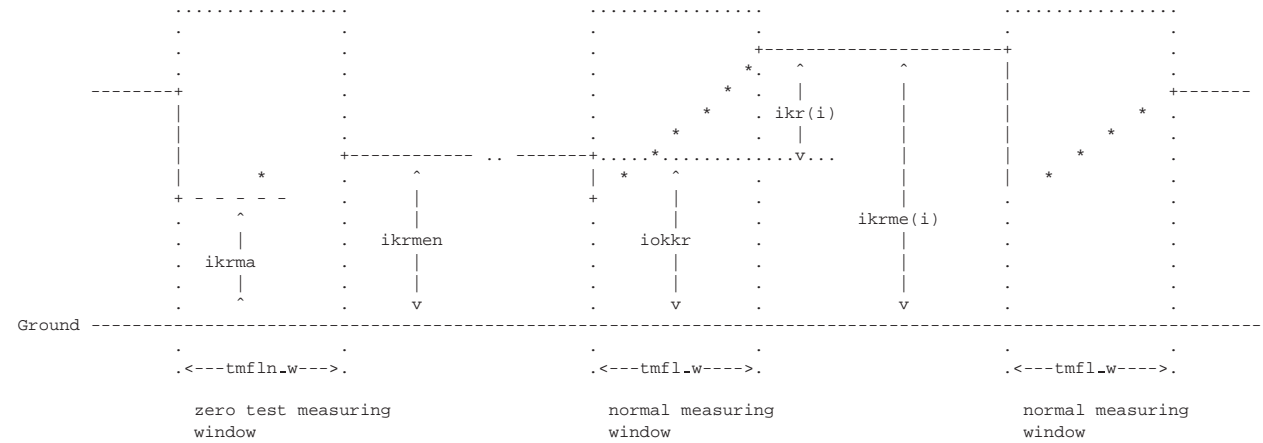




Hint: The cylinder-individual values (ikr, ikrme ) are indicated in the following description by a control variable (i) - like in the ECU-code - for example ikr(i). The corresponding RAM-cell which is illustrated in the ASCET-picture and which can be read via VS100 is marked by \_i , for example ikr\_i.  
The variable i travels from 0 up to SY\_ZYLZA-1.

The knock detection and thus the calculation of rkr(i), vkr(i), kek and B\_kl is described in %KRKE.

Determination of the measuring values (Intwert)



During each combustion the processor reads the CC195 integrator value via the A/D converter and calculates the offset corrected integrator value ikr(i) relevant to the knock decision:

$$ikr(i) = ikrme(i) - iokkr, \text{ with}$$

$$iokkr = ikrma + (igokr_w * tmfl_w), \text{ in which case } ikrma \text{ is limited to } 715 \text{ mV } \pm 220 \text{ mV} \text{ (220 mV = limit value for}$$

$$\text{diagnosis reset value) and } |igokr_w * tmfl_w| \text{ to DKROKMX}$$

$$igokr_w = igod_w = (ikrmen - ikrma) / tmfln_w, \text{ } ikrma \text{ is not limited}$$

For the calculation of the current offset correction value iokkr the values for the integrator gradient igokr\_w and for the integrator reset value ikrma as well as the current measuring window length tmfl\_w which were determined in the preceding zero test are used. The product of current measuring window length tmfl\_w and integrator gradient igokr\_w is limited to the maximum value DKROKMX, so that for the determination of the offset with short measuring windows the conversion error to long measuring windows, due to rough incrementation, remains small.

In the zero test ikrma and igokr are determined for the offset compensation and igod\_w for checking the CC195. In the test pulse ikrmet is determined for the checking of the CC195. Thereafter the corresponding diagnosis function is called up and the values are checked for plausibility.

Due to the ADC resolution (approx. 20 mV) and the small integrator offset values in case of small measuring window lengths the determination of the integrator gradient igokr\_w for the offset correction in case of small measuring window lengths may not be performed. This can be achieved by using an upper engine speed threshold DKROKO. When this threshold is exceeded the integrator gradient igokr\_w is frozen.

Hints for the application of this engine speed threshold, see below and in %DKRNT.

For the diagnosis of the integrator gradient igod\_w is used, not igokr\_w. igod\_w is also calculated above the engine speed threshold DKROKO. Therefore the diagnosis can be enabled in an extended engine speed range as it is possible while using igokr\_w. That means, if nmot <= DKROKO then igokr\_w = igod\_w. The calculation of igod\_w will be stopped if nmot > DKROKD. In this case the value for igod\_w is freed.

DKROKD must be greater than DKROKO.



#### Generating the measuring window (Messf)

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The beginning of the measuring window with regard to DTC is determined by the tooth flank signal (resolution 3°). In order to realize the resolution demanded for tmfa (beginning of measuring window with regard to DTC in s) resp. tmfl\_w (measuring window length in s) timers which are on the uC are used. During the measuring window the knock sensor signal is integrated in the CC195.

#### Triggering of zero test and test pulse (BDIA, BDIA\DIAPR)

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Normally the zero test and the test pulse are triggered alternately approx. every 255 working cycles (that means zero test, after 255 working cycles test pulse, after a further 255 again zero test and so on).

The zero test is only performed if the knock control is active ( i.e. B\_kr = 1 ) and if the secondary conditions Ztpnt\_a=0 and B\_tpnt\_aw=0 are fulfilled. In case Ztpnt\_a=0 and B\_tpnt\_aw=0 and !B.kr are set, the state is frozen and a zero test is performed during the next transition from !B.kr to B.kr.

The test pulse is performed if the temperature threshold for the KC is exceeded (i.e. B\_tmkr = 1) and if the conditions Ztpnt\_a=0 and B\_tpnt\_aw=1 are fulfilled.

Zero test and test pulse are only triggered if no dynamic response ( !B.krldy and !B.krndy ) exists. A request for zero test or for test pulse which takes place during active dynamic response, is only considered after the end of the dynamic response.

In case of suspected error of a diagnosis, i.e. the error counter of the corresponding diagnosis does not have the value KRFHT, the zero test and test pulse are no longer performed alternately. Instead the test which generated the suspected error is carried out at approx. every 120 working cycles until the error is definitely detected or healed. Thereafter a change back to the standard state is performed. This applies analogous for the healing.

(As far as further marginal conditions for the execution of the diagnosis are concerned see %DKRNT and %DKRTP).

With sufficient time before the beginning of the diagnosis measuring window the following points must be observed:

- for the zero test the signal sources (KS) must be deactivated (e.g. by B\_dntb, waiting time until the beginning of the measuring window at least 250 us)
  - for the test pulse the test pulse needs to be switched on and the medium amplification stage 2^3 must be adjusted on the CC195 (e.g. by B\_dtpb)
- (The change-over of the amplification stage for the test pulse cannot be measured with VS100.)

The amplification during zero test must be equal to the current amplification of the current measuring window. (Theoretically also larger amplifications are possible and sensible so as to increase the reliability of detecting a stuck multiplex switch. However, these can cause additional problems if a disturbance noise from the printed board in the CC195 exists ==> falsely a stuck multiplex switch is then detected).

The test pulse and the diagnosis DKRTP can be switched off by the label CWDKRTP (CWDKRTP = 0 switched off, CWDKRTP > 0 switched on). If the test pulse is switched off also the test pulse activation of the CC195 is no longer performed. In this case the zero test is performed every 255 working cycles.

Due to the diagnosis DKRNT being switched off only the evaluation is suppressed. The zero test, i.e. the determination of ikrma and igokr\_w, is still performed because the values are needed for the offset correction. (Labels for the switching off of the zero test diagnosis:

The activation or deactivation of the diagnosis is only allowed to take place during the ECU reset, so as to ensure that the functions are performed correctly.

Hint: The diagnosis may only be switched off for application purposes and not for the mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. (That means CWDKRNT, CWDKROF and CWDKRTP must be set to a value > 0.)

In order to obtain reasonable starting values for the offset correction, the values for ikrma and igokr are determined once after the start, if tmot > TMKR - (5 increments) and B.kr=0. These values are not diagnosed.

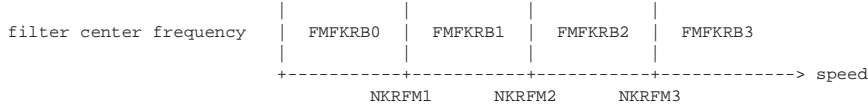






### Filter center frequency (fmfkr Decod)

The filter center frequency depends on the engine speed. There are four speed areas. The filter center frequency is adjusted by means of the constants FMFKRB0-3. The desired filter center frequency has to be entered in kHz. The areas are limited via the constants NKRFM1-3.



To avoid a jitter, a hysteresis (KRANH, hysteresis of the kc-adaptation map) is used. (Application hints for KRANH see %KRRA) According to the desired filter center frequency the corresponding pins of the CC195 are triggered. If a change of the filter center frequency has occurred, B\_fmfkr is set true for KRFTPAKT + 1 working cycles. The bit is used in %KRKE.

### KC application mode only for the CC650 (Cannot be used for the CC195)

The CC650 must be switched to a KC application mode via the code word CWKRAPP for the KC application with the KID. This is necessary, because the amplification stage is controlled via internal registers. By means of the switch-over the contents of the register is transferred to ports on the outside and it can thus be used for the KID. In this mode also the ADT signal is led to the exterior by a port. By the fixed value TMCC650 it is possible to select which internal signal is to be transferred to the output ADT.

TMCC650	ADT output
0	KTI input ( asymmetrical mode )
16	internal pulse of the CC195 proportion
32	KTI input ( symmetrical mode )
48	test pulse output
64	filter output
80	rectifier output
96	amplifier output
112	multiplexer output

CWKRAPP = 0 : Normal operating and series production setting  
CWKRAPP = F0h = 240 : KC application mode

Hint: The KC application mode may only be used in connection with a KC control unit, since the amplification stage is transferred to ports which are used for other purposes during normal operating. In the KC control unit these lines are then separated. The ADT-output may only be used for special investigations. For the kc-application (for example with KID) TMCC650 must be set to zero (TMCC650=0).  
The labels CWKRAPP and TMCC650 have no function in connection with the CC195.

The CC650 is set to asymmetrical or symmetrical mode by means of a system constant. The tabular above for the ADT-output is valid for both the asymmetrical and the symmetrical mode with one exception. The exception is TMCC650 = 0. If the IC is switched to the symmetrical mode via the system constant, the CC650 is in the symmetrical mode at TMCC650=0 too.

The application mode is not necessary for the CC195, since the signals for the KID measurement can be taken directly from the chip.

### Setting of the knock sensor evaluation IC

The software modul contains the triggering of the CC195 as well as the triggering of the CC650. The selection is performed by means of system constants. So that a correct selection is performed the following settings are necessary:

CC195: SY\_KR\_INT = 0  
SY\_KR\_EXT = 1  
  
CC650: SY\_KR\_INT = 1  
SY\_KR\_EXT = 0

### APP GGKS 4.50 Application hint

The values B\_mf, B\_ntinires, B\_dnta and B\_dtpa are dependent on the representation and they do not exist in the software. The bits B\_c95\* as well as tptn\_aktiv cannot be measured correctly by VS100, since some of them are updated twice during a synchro program run.

#### Asymmetric/symmetric sensor operation

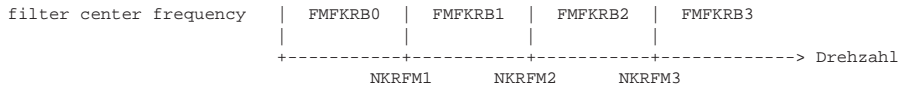
Sensors can be connected to the CC195 asymmetrically as well as symmetrically. If the test inputs TP0, TP1 and TP2 are connected to VSS the CC195 operates (compatible to the CC192) in the asymmetrical mode. If TP1 = high and TP2 = TP0 = low is connected then the CC195 operates in the symmetrical mode. The input multiplexer can only change-over up to two knock sensors.

The CC650 must be switched to the KC application mode for KID measurements. In this mode also the diagnosis test pulse should be switched off.

Hint: The KC application mode may only be used in connection with a KC control unit, since the amplification stage is transferred to ports which are used for other purposes during normal operating. In the KC control unit these lines are then separated. The ADT-output may only be used for special investigations. For the kc-application (for example with KID) TMCC650 must be set to zero (TMCC650=0).  
The labels CWKRAPP and TMCC650 have no function in connection with the CC195.

The fixed value block SENZZYL(i) for knock sensor assignment must be adjusted according to the description in the text.

The filter center frequency is adjusted by means of the constant FMFKRB0-3. The desired filter center frequency has to be entered in kHz. The areas are limited via the constants NKRFM1-3. (Application hints for KRANH see %KRRA)



It may occur that not all pins of the CC195 for the filter center frequency adjustment are connected to the uC in the HW. In this case not all frequencies which can be adjusted in the software can be adjusted in the CC195. This must be settled with the HW development.

Due to the ADC resolution (approx. 20 mV) and the small integrator offset values with small measuring window length, the determination of the integrator gradient `igokr_w` for the offset correction with small measuring window lengths may not be performed. This is achieved by using an upper engine speed threshold `DKROKO`. When this threshold is exceeded the integrator gradient `igokr_w` is frozen.

The engine speed threshold `DKROKO` must be adjusted according to the following recommendations:

- The measuring window for the calculation of the gradient `igokr_w` must be larger than 2 ms.
- The threshold should not fall below 5000 rpm.
- Only if it is not possible to fulfill the two requirements just mentioned, the threshold may be selected such that the measuring window becomes smaller. It may, however, not become smaller than 1,5 ms.

In this case the following is recommended:

If the measuring window length at 5000 rpm lies between 1,5 ms and 2,0 ms, then the threshold `DKROKO` should be set to 5000 rpm. If the measuring window length at 5000 rpm is less than 1,5 ms the threshold `DKROKO` should be set such that the measuring window length is 1,5 ms.

`DKROKD` must be greater than `DKROKO`.

Further hints see `%DKRNT`.

The diagnosis `DKRTP` can be switched off by means of the label `CWDKRTF` (`CWDKRTF` = 0 switched off, `CWDKRTF` > 0 switched on). If the diagnosis is switched off, also the test pulse triggering of the CC195 is no longer performed. In this case the zero test is performed every 255 working cycles.

Due to the diagnosis `DKRNT` being switched off only the evaluation is suppressed. The zero test, i.e. the determination of `ikrma` and `igokr`, is still performed because the values are needed for the offset correction. (Labels for the switching off of the zero test diagnosis: `CWDKRNT` and `CWDKROF`)

The activation or deactivation of the diagnosis is only allowed to take place during the ECU reset, so as to ensure that the functions are performed correctly.

Hint: The diagnosis may only be switched off for application purposes and not for the mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. (That means `CWDKRNT`, `CWDKROF` and `CWDKRTF` must be set to a value > 0.)

During the application of the characteristic map for the beginning of the measuring window and for the measuring window length it must be observed that at each operating point the sum of the values for beginning of measuring window and for measuring window length is smaller than the segment length. (That means `wmfa` + `wmfl` <  $720^\circ / SY\_ZYLZA$ ).  $0^\circ KW$  may not be entered into `KFMAKR` and `KEMLN`.

Hint: The beginning of the measuring window must lie in between TDC and the following SW reference mark. A safety distance between the begin of the measuring window and SW reference mark has to be kept. This limitation of the beginning of the measuring windows is realized via SW.

The maximum beginning of the measuring window is limited to  $((720^\circ KW / SY\_ZYLZA) - SY\_GRDWRT - \text{safety distance})$ . The safety distance depends on the speed.

	nmot < 2000	2000 < nmot < 4000	4000 < nmot < 5000	5000 < nmot < 6000	6000 < nmot
safety distance begin of measuring window to SW reference mark °KW	3,75	5,25	6,75	7,5	9

The characteristic map `KFMAKR` is not limited. The values from `KFMAKR` are limited in the SW to the value described above. The current, limited value of the beginning of the measuring window is `wmfa`.

For further application hints regarding the beginning of the measuring window and the measuring window length see `%KRKE`.

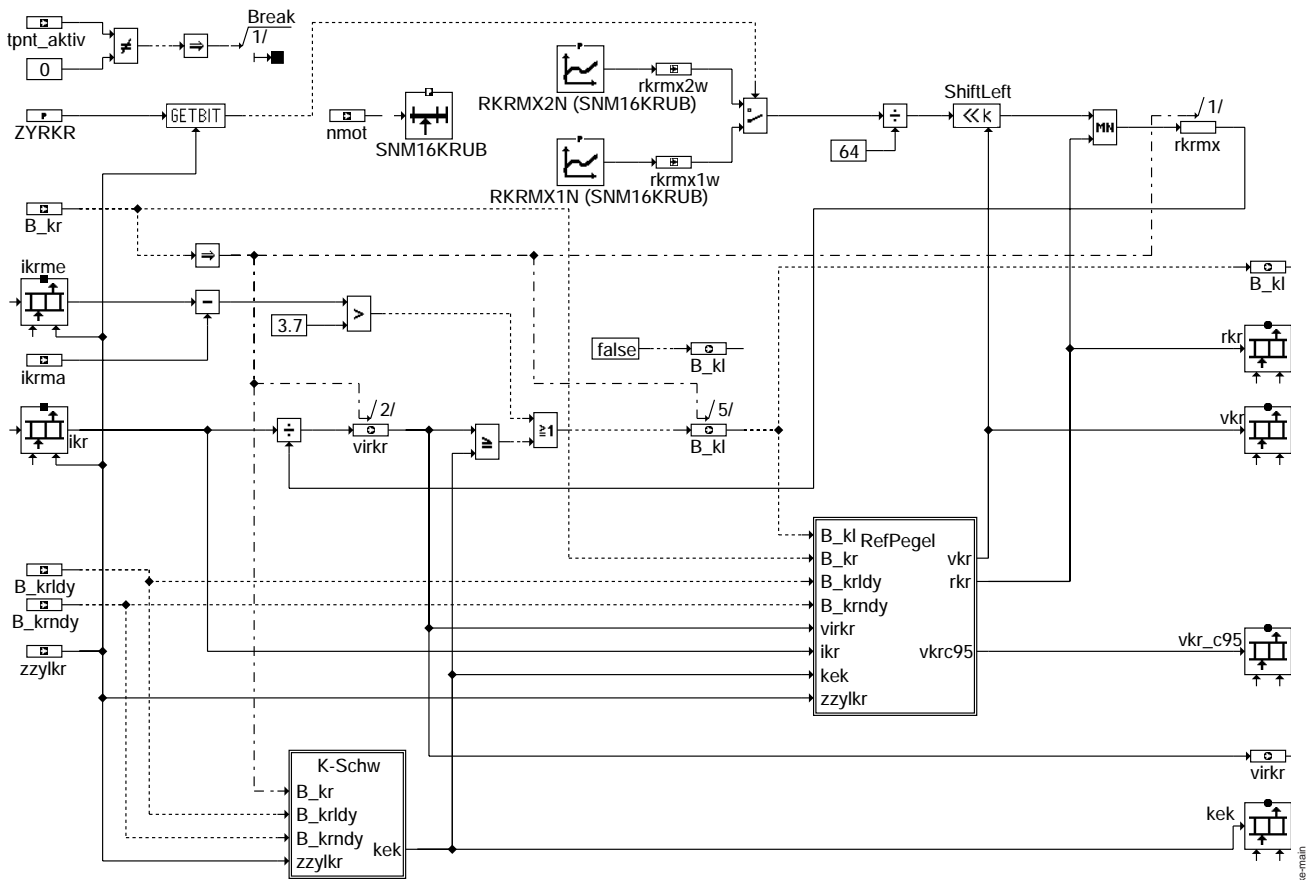
The following guidance values are recommended:

- `CWDKROF` = 1
- `CWDKRNT` = 1
- `CWDKRTF` = 1
- `CWKRAPP` = 0
- `DKROKMX` = 400 mV
- `DKROKO` approx. 5000 rpm ( for measuring window > 2 ms )
- `DKROKD` > `DKROKO`
- `TMCC650` = 0

## KRKE 14.30 Knocking detection

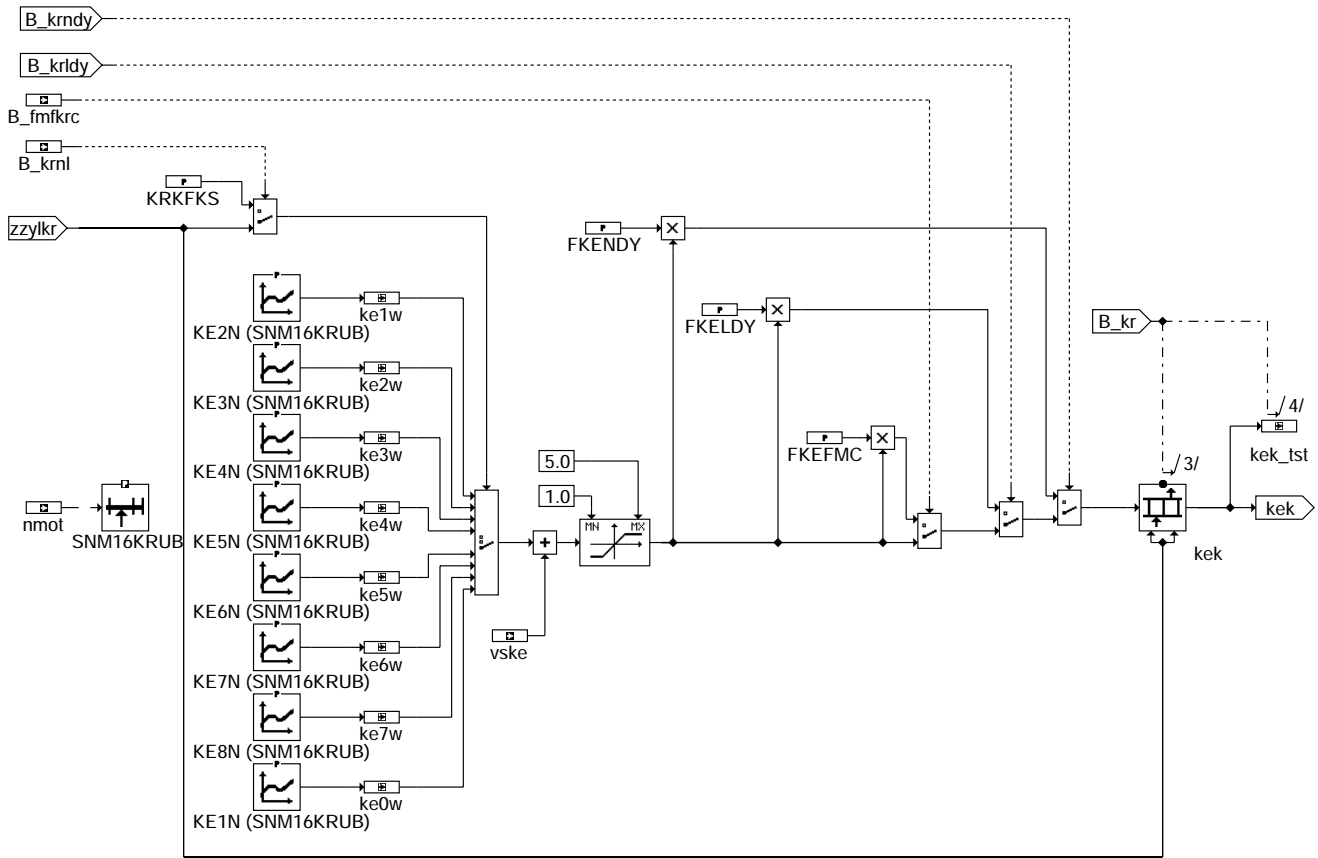
### FDEF KRKE 14.30 Function definition

KRKE: knock detection



krke-main

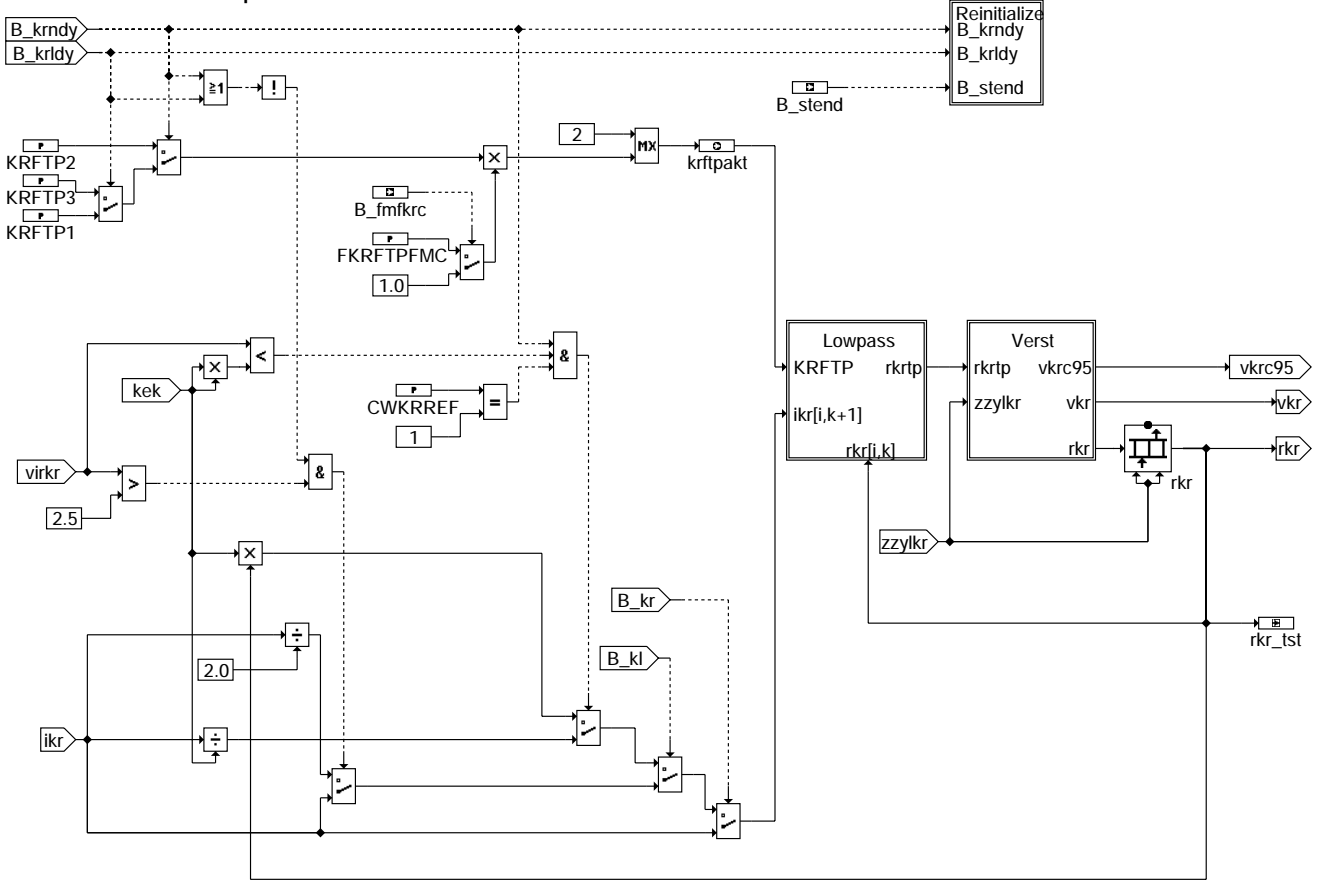
### K-SCHW: determination of corrected knock detection threshold



krke-k-schw

krke-k-schw

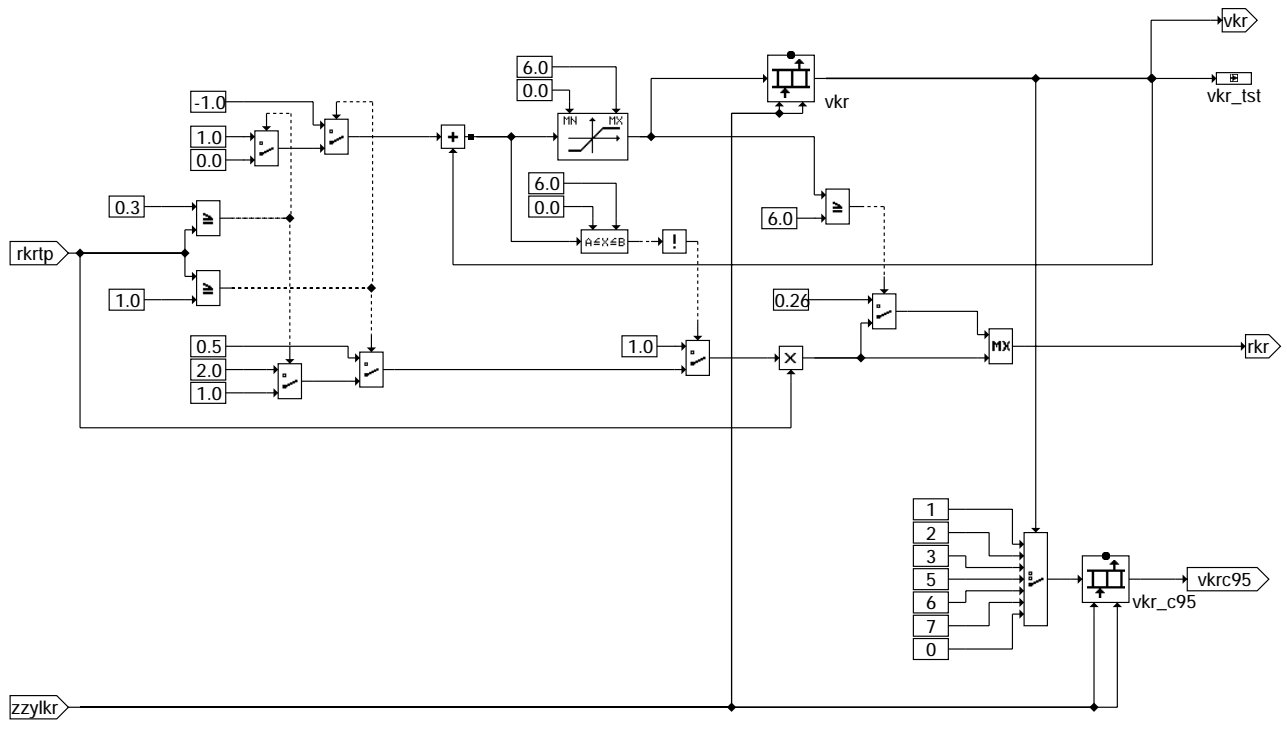
### REFPEGEL: follow-up of reference value



krke-refpegel

### krke-refpegel

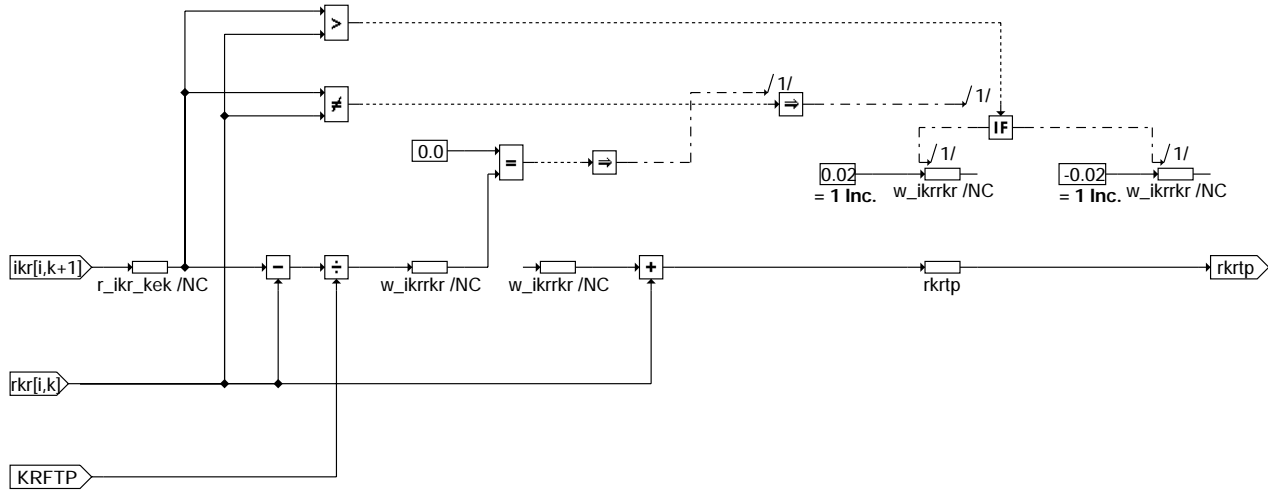
### VERST: change-over amplification stage



krke-verst

### krke-verst

### LOWPASS: calculation of reference value

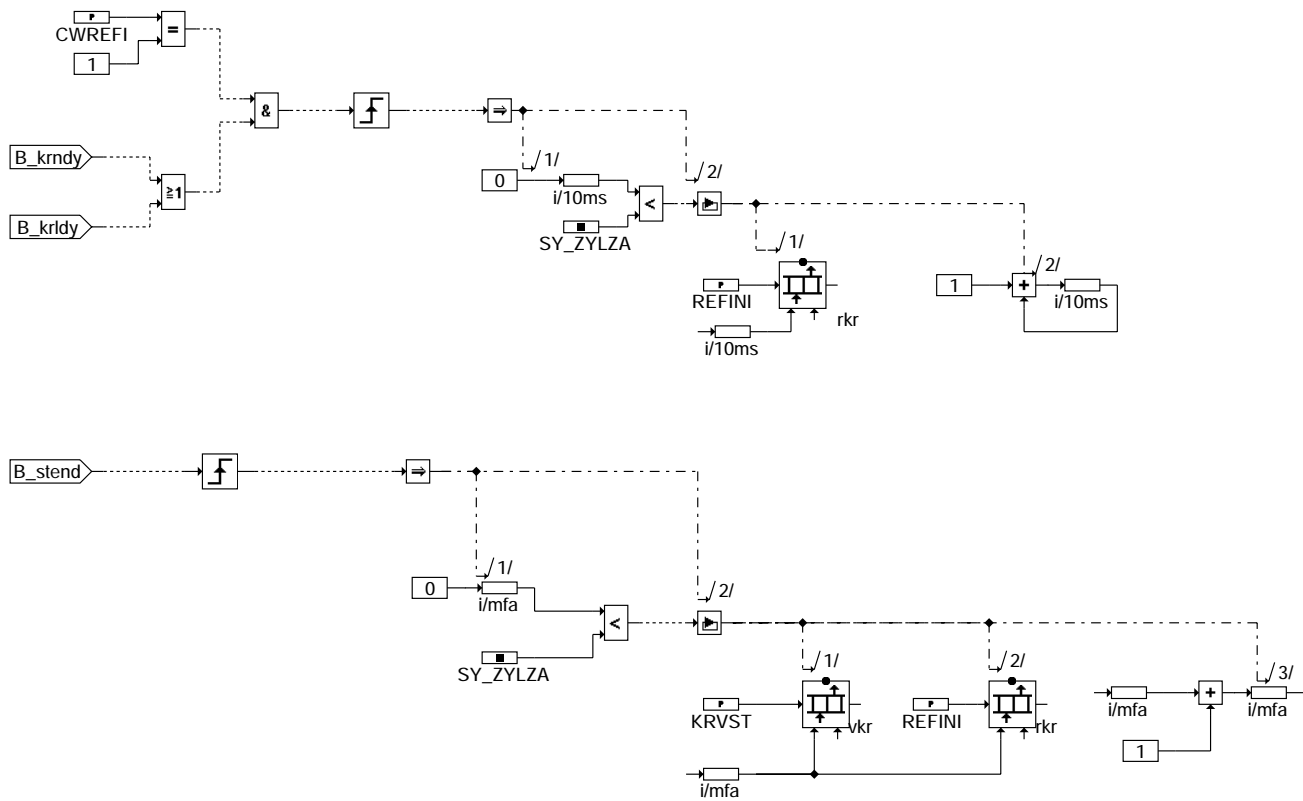


$$rkr[i,k+1] = rkrtp = rkr[i,k] + (ikr[i,k+1] - rkr[i,k]) / KRFTP$$

**k:** combustion cycle  
**i:** cylinder counter

### krke-lowpass

#### REINITIALIZE: reinitialize of vkr and rkr

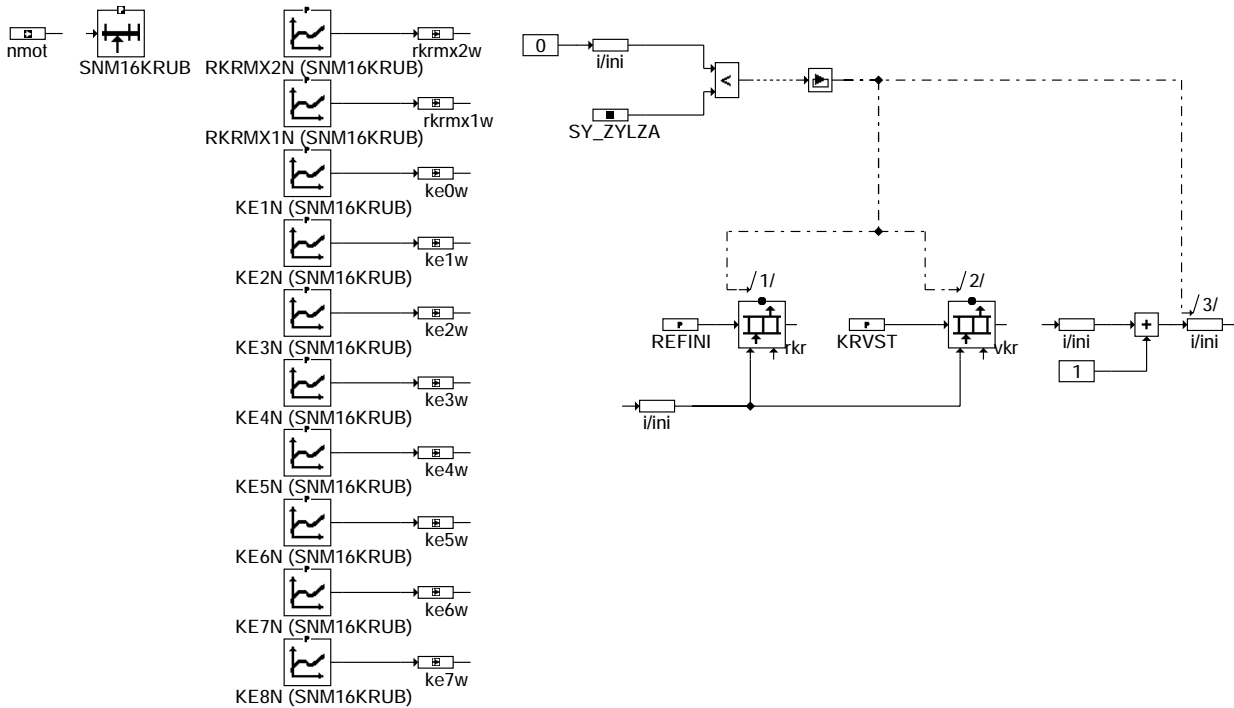


### krke-reinitiali

krke-lowpass

krke-reinitiali

### INITIALIZE: initialization



### krke-initialize

### ABK KRKE 14.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWKRREF			FW	code word: characteristic of rkr follow-up at speed dynamics
CWREFI			FW	code word: reinitialize of rkr with REFINI at dynamics conditions
FKEFMC			FW	correction factor for knock detection thresh. in case of change of filter frequ.
FKELDY			FW	correction factor for knock detection threshold during load dynamics
FKENDY			FW	correction factor for knock detection threshold with engine-speed dynamics
FKRFTPFC			FW	correction factor of low pass characteristic at switch of filter mean frequency
KE1N	NMOT		KL	knock detection threshold at cylindertimer 1
KE2N	NMOT		KL	knock detection threshold at cylindertimer 2
KE3N	NMOT		KL	knock detection threshold at cylindertimer 3
KE4N	NMOT		KL	knock detection threshold at cylindertimer 4
KE5N	NMOT		KL	knock detection threshold at cylindertimer 5
KE6N	NMOT		KL	knock detection threshold at cylindertimer 6
KE7N	NMOT		KL	knock detection threshold at cylindertimer 7
KE8N	NMOT		KL	knock detection threshold at cylindertimer 8
KRFTP1			FW	low pass characteristic normal
KRFTP2			FW	low pass characteristic at engine speed dynamics
KRFTP3			FW	low pass characteristic at load dynamic
KRKFKS			FW	selected knock detection threshold, if missing cylinder one detection
KRVST			FW	gain after cranking
KSZA			FW	number of knock sensor
REFINI			FW	initial value for reference level if knock control enabled
RKRMX1N	NMOT		KL	Maximum of reference level for knock detection threshold cylinder group 1
RKRMX2N	NMOT		KL	maximum of reference level for knock detection threshold cylinder group 2
SNM16KRUB	NMOT		SV (REF)	datapoint distribution engine speed, 16 datapoints
SY_ZYLZA			SYS (REF)	system constant number of cylinders
ZYRKR			FW	cylinder selective reference level limitation

Variable	Source	Type	Description
B_FMFKRC	GGKS	EIN	filter center frequency of CC195/CC650 changed
B_KL	KRKE	AUS	condition for knocking
B_KR	KRRA	EIN	condition for knock control active
B_KRLDY	KRDY	EIN	Condition load dynamics for knock detection active
B_KRNDY	KRDY	EIN	condition speed dynamics for knock detection active
B_KRNL	KRRA	EIN	emergency operation of knock detection for emergency operation of phase sensor
B_STEND	BBSTT	EIN	condition end of start
IKR	GGKS	EIN	integrator value with offset correction
IKRMA		EIN	integrator value at start of measurement window, knock control
IKRME		EIN	integrator value at end of measurement window, knock control
KE0W	KRKE	LOK	instantaneous value of characteristic KE0N
KE1W	KRKE	LOK	instantaneous value of characteristic KE1N
KE2W	KRKE	LOK	instantaneous value of characteristic KE2N

krke-initialize



Variable	Source	Type	Description
KE3W	KRKE	LOK	instantaneous value of characteristic KE3N
KE4W	KRKE	LOK	instantaneous value of characteristic KE4N
KE5W	KRKE	LOK	instantaneous value of characteristic KE5N
KE6W	KRKE	LOK	instantaneous value of characteristic KE6N
KE7W	KRKE	LOK	instantaneous value of characteristic KE7N
KEK	KRKE	AUS	knock detection threshold corrected
KEK_TST	KRKE	AUS	knock detection threshold corrected updated with cyl.counter
KRFTPAKT	KRKE	AUS	actual low pass characteristic
NMOT	SWADAP	EIN	engine speed
RKR	KRKE	AUS	reference level knock control
RKRMX	KRKE	LOK	reference level limited upwards
RKRMX1W	KRKE	LOK	instantaneous value of characteristic RKRMX1N
RKRMX2W	KRKE	LOK	instantaneous value of characteristic RKRMX2N
RKRTP	KRKE	LOK	reference level behind low pass knock control
RKR_TST	KRKE	AUS	reference level knock control updated with cyl.counter
TPNT_AKTIV	EGKE	EIN	activation of kc-functions
VIRKR	KRKE	AUS	Ratio: integrator / reference level knock control
VKR	KRKE	AUS	amplification stage knock control
VKR_C95	KRKE	AUS	amplification stage for input amplification stage of knock-IC
VKR_TST	KRKE	AUS	amplification stage knock control updated with cyl.counter
VSKE	VS_VERST	EIN	adjustable offset for knock detection threshold via VS20
ZZYLKR	GGKS	EIN	cylinder counter KC

### FW KRKE 14.30 Fixed Values

Parameter	Value	Description
CWKRREF		code word: characteristic of rkr follow-up at speed dynamics
CWREFI		code word: reinitialize of rkr with REFINI at dynamics conditions
FKEFMC		correction factor for knock detection thresh. in case of change of filter frequ.
FKELDY		correction factor for knock detection threshold during load dynamics
FKENDY		correction factor for knock detection threshold with engine-speed dynamics
FKRFTPFC		correction factor of low pass characteristic at switch of filter mean frequency
KRFTP1		low pass characteristic normal
KRFTP2		low pass characteristic at engine speed dynamics
KRFTP3		low pass characteristic at load dynamic
KRKFKS		selected knock detection threshold, if missing cylinder one detection
KRVST		gain after cranking
KSZA		number of knock sensor
REFINI		initial value for reference level if knock control enabled
ZYRKR		cylinder selective reference level limitation

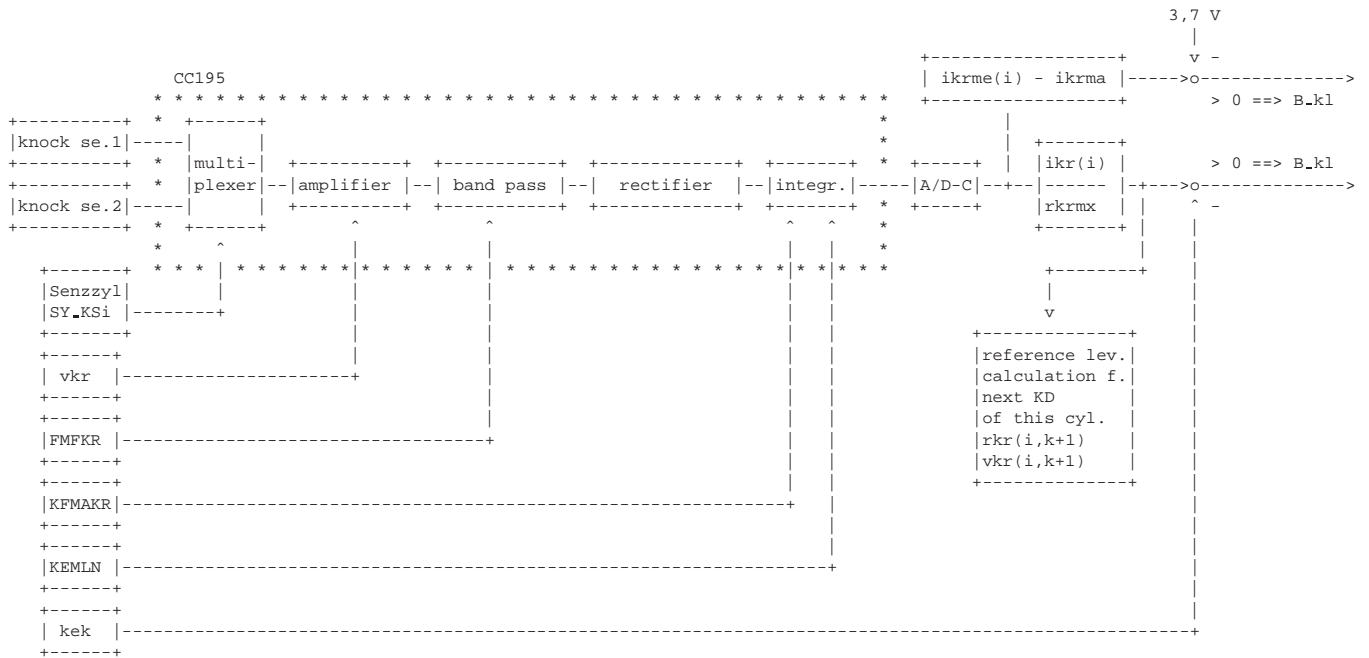
Hint: The cylinder-individual values (ikr, ikrme, rkr, kek, vkr) are indicated in the following description by a control variable (i) - like in the ECU-code - for example rkr(i). The corresponding RAM-cell which is illustrated in the ASCET-picture and which can be read via VS100 is marked by `_i`, for example rkr\_i.  
The KC cylinder counter zzylkr serves as control variable. The following applies to it:

`zzylkr = 0 ... SY_ZYLZA -1 ECU-code`





**FB KRKE 14.30 Detailed description of function**



**Knock detection (KRKE)**  
=====

For the knock detection the oscillations characteristic of knocking are transformed into electrical signals by one or more knock sensors and passed on to the Electronic Control Unit. The evaluation circuit in the ECU mainly consists of a BOSCH-IC, the CC195, which processes the sensor signals, i.e. amplifies, filters, rectifies and integrates them within a measuring window. In the process the uC cylinder-individually controls the amplification stages in the CC195 and starts and stops the integration in the CC195. The integrator values are read into the uC via the A/D-converter. As can be taken from %GGKS an offset correction of the integrator values takes place in the micro-computer. Knocking is detected if the following conditions are met:

$$B\_kl: \quad ikr(i) / rkrmx \geq kek(i) \quad \text{or} \quad ikrme(i) - ikrma \geq 3,7 \text{ V}$$

$$\text{with } rkrmx = \min ( rkr(i), rkrmx1/2w * 2^{(vkr(i)-6)} )$$

during which the cylinder-individual reference level rkr(i) is limited to the maximum value rkrmx1/2w \* 2^(vkr(i)-6). (The standardized reference level from the characteristic lines RKRMX1/2N is calculated to a cylinder-individual absolute limit value with the aid of the cylinder-individual amplification stage.) Thus a knock detection is still made possible even in case of an unusually strong increase in engine noise (for example due to a beginning engine trouble)

The cylinders are assigned to the characteristic lines RKRMX1N and RKRMX2N by the label ZYRKR (grouping into "loud" and "quiet" cylinders)

Switch logic: bit = 0 => RKRMX1N  
bit = 1 => RKRMX2N

Examples:





amplification stage CC195 = vkr(i)	6	5	4	3	2	1	0
input amplification factor 2^vkr	64	32	16	8	4	2	1
amplification factor incl. filter factor 2^vkr *2	128	64	32	16	8	4	2

----->  
increase of basic engine noise  
idle                    nominal  
speed                    engine speed

## APP KRKE 14.30 Application hint

For the application the following typical values are suggested:  
=====

- FKELDY = approx. 1,1
- FKENDY = approx. 1,1
- FKEFMC = approx. 1,1
- PKRFTPFMC = 0,5 ... 1
- KEiN = cylinder-specific and dependent on the detection quality, standard is 2 - 3, see following description
- KRFTP1 = 16
- KRFTP2 = 4
- KRFTP3 = 4
- KRVST = input amplification stage = 4
- REFINI = 980 mV (just below the upper change-over threshold)
- RKRMX1/2N = maximum value during the application (limitation is not effective), exact explanation see below
- ZYRKR = see RKRMX1/2N
- KRKFKS = should take the value of the kc-cylinder counter by which the most sensitive knock detection threshold is chosen  
e.g. KE3N is the most sensitive knock detection threshold and is read into ke\_2 when zzylkr=2, consequently KRKFKS has to take the value 2 in this case
- vske = while applying knock detection thresholds with connected VS2x the value of vske has to be taken into consideration as after the end of communication between VS2x and ECU (disconnection) vske is set to zero (see %VS\_VERST)

The following sequence is useful:

1. Determine and check the knock sensor assignment as described in %GGKS (measuring window, phase and multiplexed knock sensor signal to be observed by oscilloscope, test of varying knock sensor assignments)
2. Determine the beginning and the length of the measuring window (MF) for the entire engine speed range (oscilloscope). For each base point the MF must be stipulated during full load and partial load. Experience has shown that only in case of large differences in ignition angle between full load and partial load an earlier beginning of the measuring window is necessary during partial load.  
The sum of MF-beginning and MF-length (in deg. crankshaft (° KW)) must be smaller than the segment length (720° KW / amount of cylinders, s.a. %GGKS).  
Both values must each be chosen different from 0. (for further details see %GGKS)  
Generally the MF-lengths and positions must be adjusted in such a way that the main emphasis of the knock occurrence, represented by the knock sensor raw signal from the original mounting place, lies within the MF. Corresponding to the MF-characteristic line base points at first the best compromise for one engine speed regarding the MF-beginning should be found. Here medium and a little heavier knocking during full load and during partial load have to be considered. The beginning of the knocking should each time lie within the MF. Thereafter the MF-length is chosen such that in case of medium knocking the knock occurrence lies within the MF and in case of a little heavier knocking the dying-out oscillations of the knock occurrence are cut off. The adjustment of the MF must be especially optimal for light and medium knocking.  
Heavy knocking as a rule always fills out the entire MF and therefore it is no problem to detect it.  
This procedure now is to be repeated for the remaining engine speed base points.  
It is also important that the knocking for the selection of the MF is generated with basic ignition angles ready to go into production (so no advance adjustment using vszwr res. zwappl should be carried out). Therefore it is absolutely necessary to operate the engine with fuel of the lowest planned octane number.  
  
If the engine has disturbing noises then this should be taken into consideration when selecting the MF as follows:
  - continuous disturbing noises may lie in the MF (here too it would, however, be better if they would lie outside the MF)
  - pulsating disturbing noises must lie outside the MF
 In any case the customer needs to be informed about existing disturbing noises.
3. Adjustment of the filter center frequency (VS100, knock intensity detector: KID)  
The filter center frequency must be chosen such that for all operating points the best possible detection is obtained. In this case the behaviour during high load and high engine speed is decisive for the selection of the frequency. The frequency which guarantees the best detection in this range must be selected.
4. Taking over of the above data listing
5. Fixing the knock detection thresholds KE1N , KE2N ... (VS100, KID)  
Now it is useful to decide on the knock detection (KD) thresholds for the individual cylinders. Especially recommendable in this case is the use of combustion chamber pressure sensors in order to be able to measure the pressure amplitudes in the combustion chamber during the knock occurrence. Should the engine not have bore holes for the pressure sensor in the cylinder head then also spark plugs with integrated pressure sensor can be used. If no exact details were given by the customer then the KD thresholds for the individual cylinders are to be fixed in such a way that knock occurrences whose amplitude exceed the following thresholds are detected 100 %.



n <= 1 800 rpm press.amplitude +- 0,5 - 1 bar Here not the engine durability is decisive but the audibility threshold in the vehicle. In connection with knock control the knocking which is audible in the engine test bench

n = 3 000 rpm press.amplitude +- 2 - 2,5 bar room or during open bonnet must also be detected. The knocking occurring during active knock control, however, may not be audible later on in the interior of the vehicle.

n = 4 000 rpm press.amplitude +- 3 - 3,5 bar

n = 5 000 rpm press.amplitude +- 5,0 bar Now the engine durability is decisive. In case of this high engine speed

n = 6 000 rpm press.amplitude +- 5,5 bar the engine noise is so loud that the knocking is no longer audible.

Attention!!! For characteristic lines with 16 engine speed base points only every 2. engine speed base point is to be adjusted (delta 800 RPM).

Thereafter the misdetection thresholds (retarding at control limit) for each cylinder and for each engine speed are to be determined by reducing the above-determined KD thresholds. Up to 5000 rpm these misdetection thresholds should be for at least 0,5 below the above-determined KD thresholds. Above this engine speed the distance to misdetection may be a little smaller.

These measurements also have to be performed with REGULAR UNLEADED fuel. Standard are knock detection thresholds of 2 - 3. The value 3,3 may under no circumstances be exceeded during steady-state operation. The determined knock thresholds must then be confirmed at an early stage by the customer in an engine endurance test.

6. Fixing of the maximum permitted reference level for the knock detection RKRMX1/2N (VS100)  
So that also in case of very loud background noise of the engine or of a cylinder a knock detection keeps on being possible the reference level rkr(i) is limited to the maximum with RKRMX1/2N only for the calculation of the knock condition B\_kl (see picture in FDEF).

For the characteristic lines RKRMX1N and RKRMX2N the following concept is recommended:

- equip the engine with normal noise behaviour with max-KS (upper limit of the tolerance range)
- by means of the RAM-contents of rkr(i) and vkr(i) on the engine speed base points of the characteristic lines RKRMX1/2N the standardized reference levels rkrn(i) are to be determined with the formula  $rkr(i) * 64 / (2^{vkr(i)})$  cylinder-specific for all cylinders or they are to be measured directly (s.a. %DKRS).
- divide cylinders into loud and quiet groups, e. g. 4-cyl. and 1 KS ==> cyl. 2+3 loud a. cyl. 1+4 quiet

in case of 2-cyl./KS a grouping is usually not necessary

Via a corresponding bit pattern in the label ZYRKR the reference level is limited cylinder-specifically to RKRMX1N or RKRMX2N just as in the KS assignment.

bit = 0 => RKRMX1N  
bit = 1 => RKRMX2N (see function description earlier on)

- Approx. the following values are to be stored in RKRMX1N and RKRMX2N:

# if n = 2 000 rpm	approx.	1,5 * mean value of rkrn(i) for the loud resp. quiet cylinder groups
# if n = 4 000 "	approx.	1,3 * " " " " " " " " " " " " " " " "
# if n = 6 000 "	approx.	1,2 * " " " " " " " " " " " " " " " "

The plausibility of the applied data should be proved at several engines in order to prevent misdetections of knocking.

Especially RKRMX1/2N must be adjusted in such a way that also when using min-KS a definite detection of heavy knocking is possible that means  $ikr(\text{heavy knocking}) > rkrmx * kek$ . In order to cover the characteristic line RKRMX1/2N it should be checked with min-KS whether the knock detection for heavy knocking is still at all possible with the above-determined knock thresholds ( $rkrmx * kek$ ) if rkr is becoming higher by louder engine. So as to simulate this case the knock detection threshold KEiN must be increased since the reference levels cannot be influenced. Thus rkr can (e.g. if light knocking occurs since it is no longer detected as such) be limited by rkrmx1/2w which makes it possible to check whether following heavy knocking is definitely being detected.

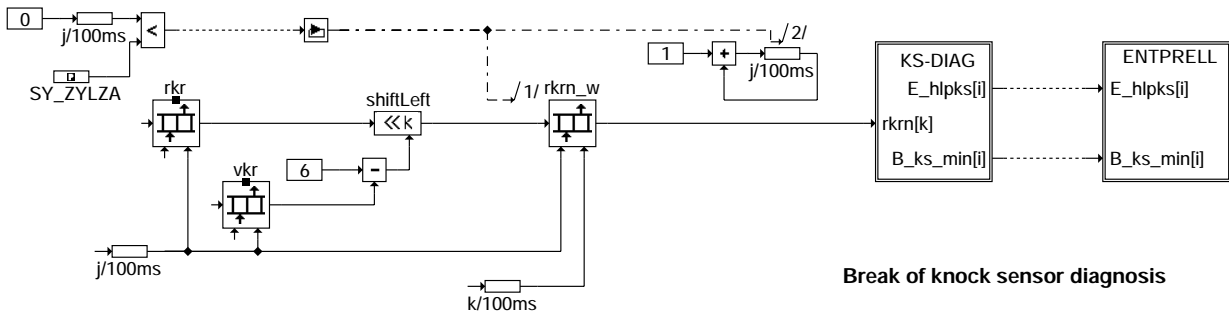
For the knock detection the following grades are now obtained:

- normal engine noise:  $rkr(i) < RKRMX1/2N * (2^{vkr(i)}) / 64$  ==> knock detection with  $rkrmx = rkr(i)$
- loud engine:  $RKRMX1/2N * (2^{vkr(i)}) / 64 < rkr(i) < UDKSNO * (2^{vkr(i)}) / 64$  ==> knock detection with  $rkrmx = RKRMX1/2N * (2^{vkr(i)}) / 64$ , since rkr(i) too large
- very loud engine:  $rkr(i) > UDKSNO$  (see %DKRS) ==> B\_krdws = safety retarding

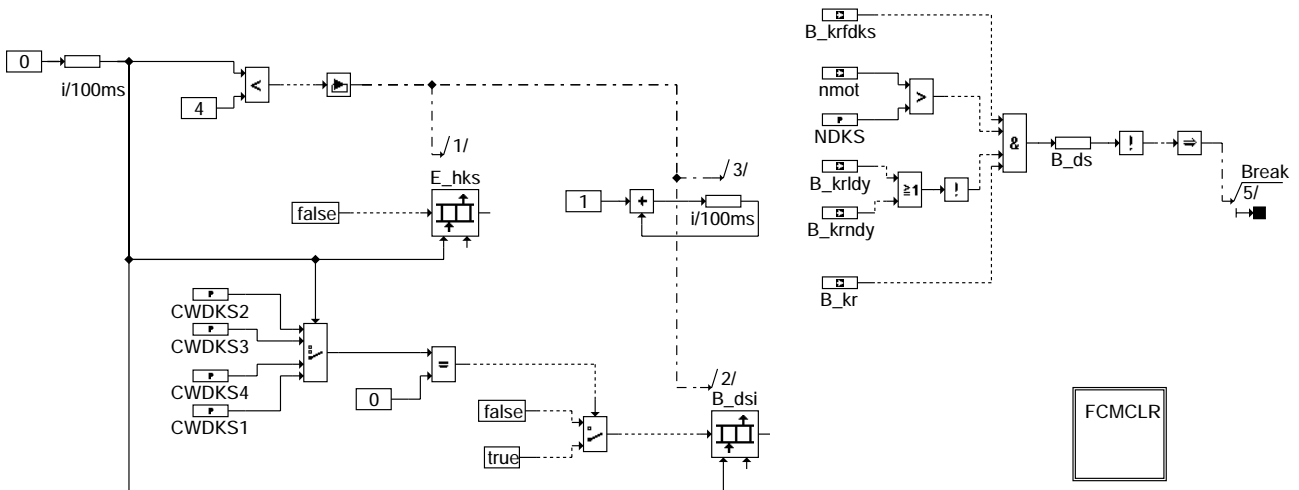
## DKRS 29.80 Diagnosis; knock sensor

### FDEF DKRS 29.80 Function definition

#### DKRS: Overview knock sensor diagnosis

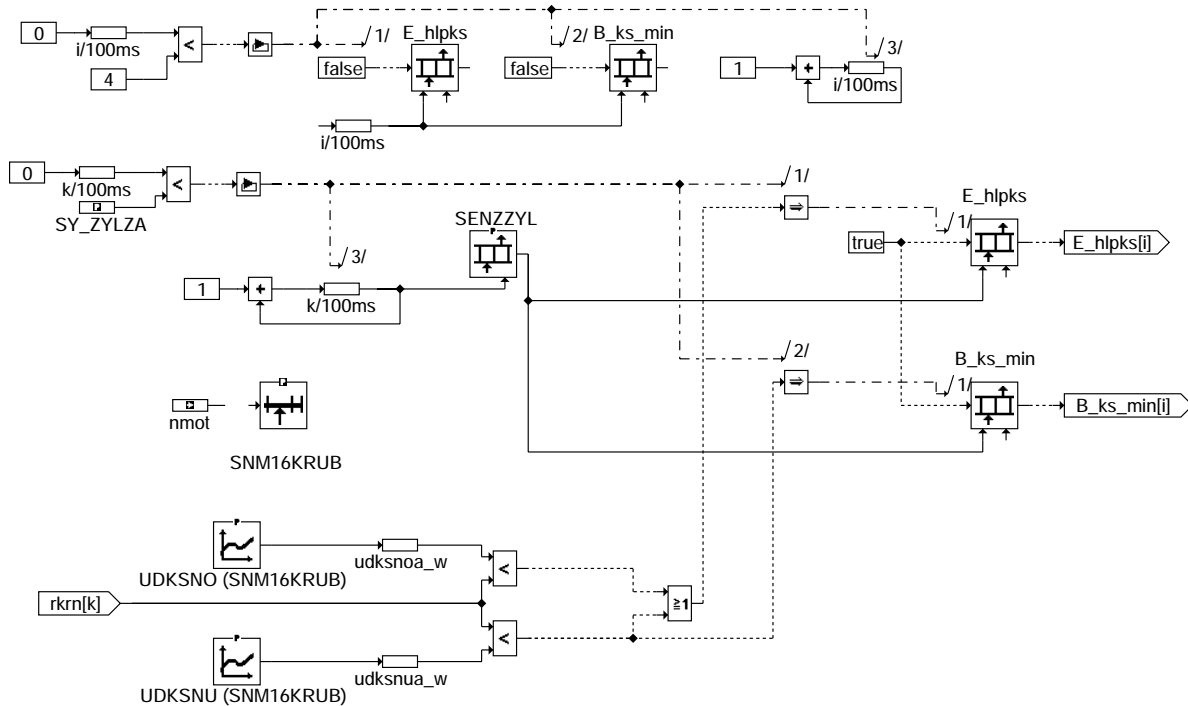


#### Break of knock sensor diagnosis



dkrs-main

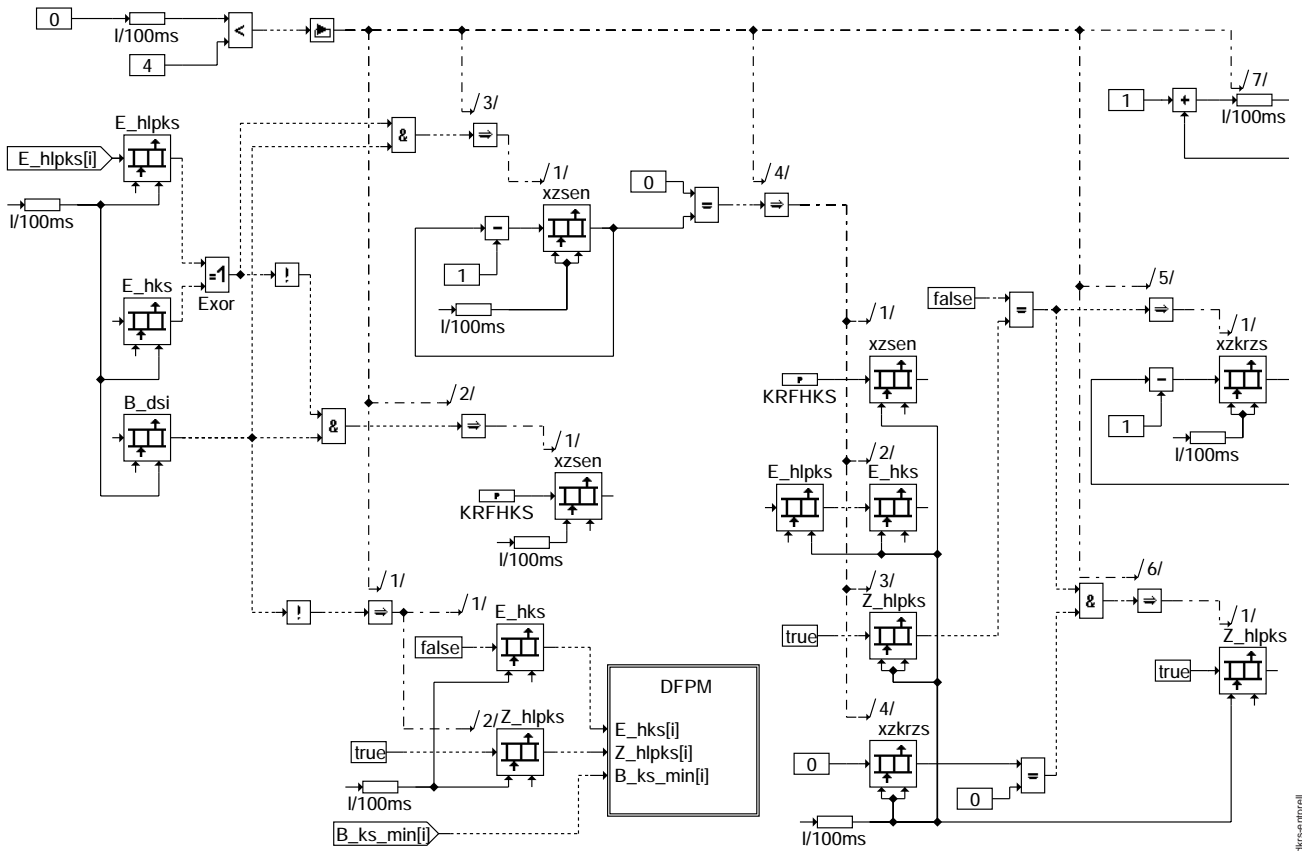
#### KS-DIAG: knock sensor diagnosis



dkrs-ks-diag



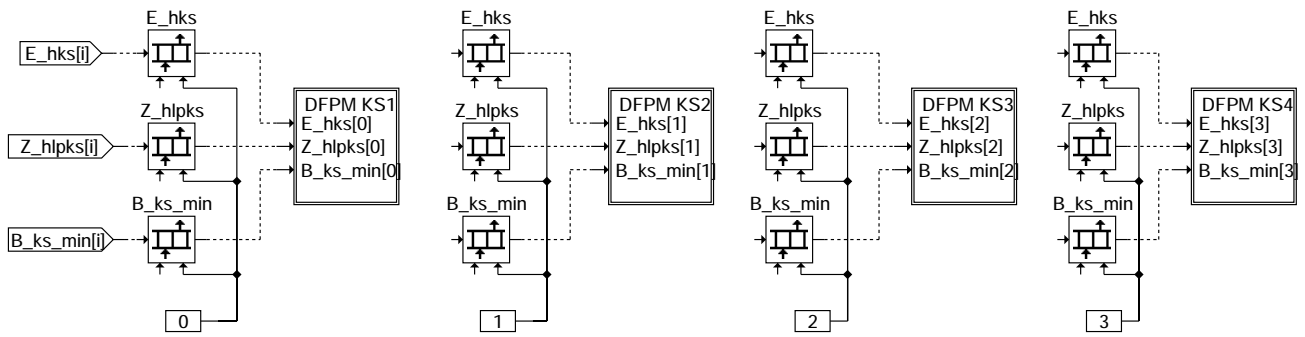
### ENTPRELL: debounce of fault memory entry



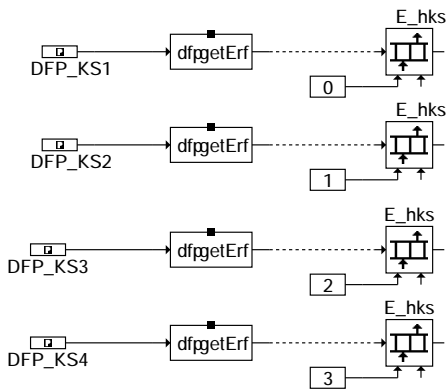
dkrs-entprell

dkrs-entprell

**DFPM: Interface: fault memory <==> knock sensor diagnosis**



**read DFPM**

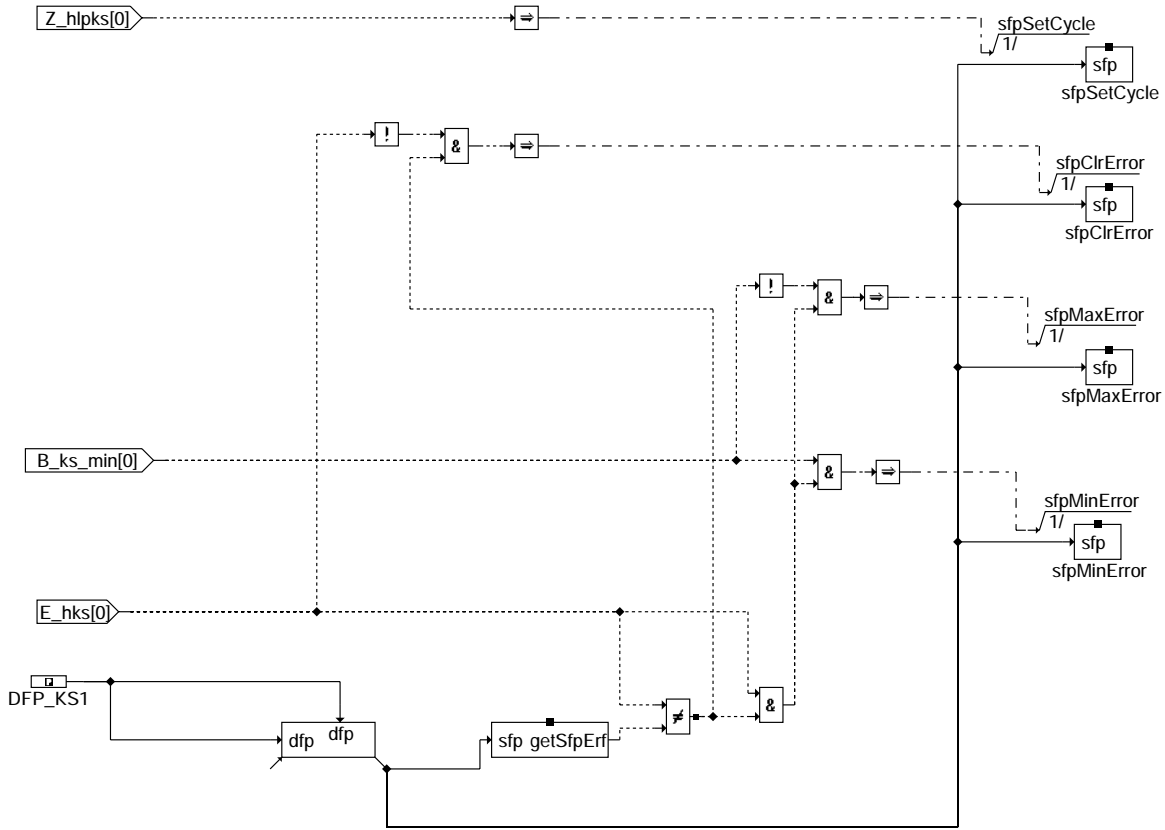


dkrs-dfpm

dkrs-dfpm

In this FEDF the interface to the DFPM is only represented for knock sensor one, the other knock sensors are treated analogously.

**DFPM KS1: Interface for knock sensor 1**

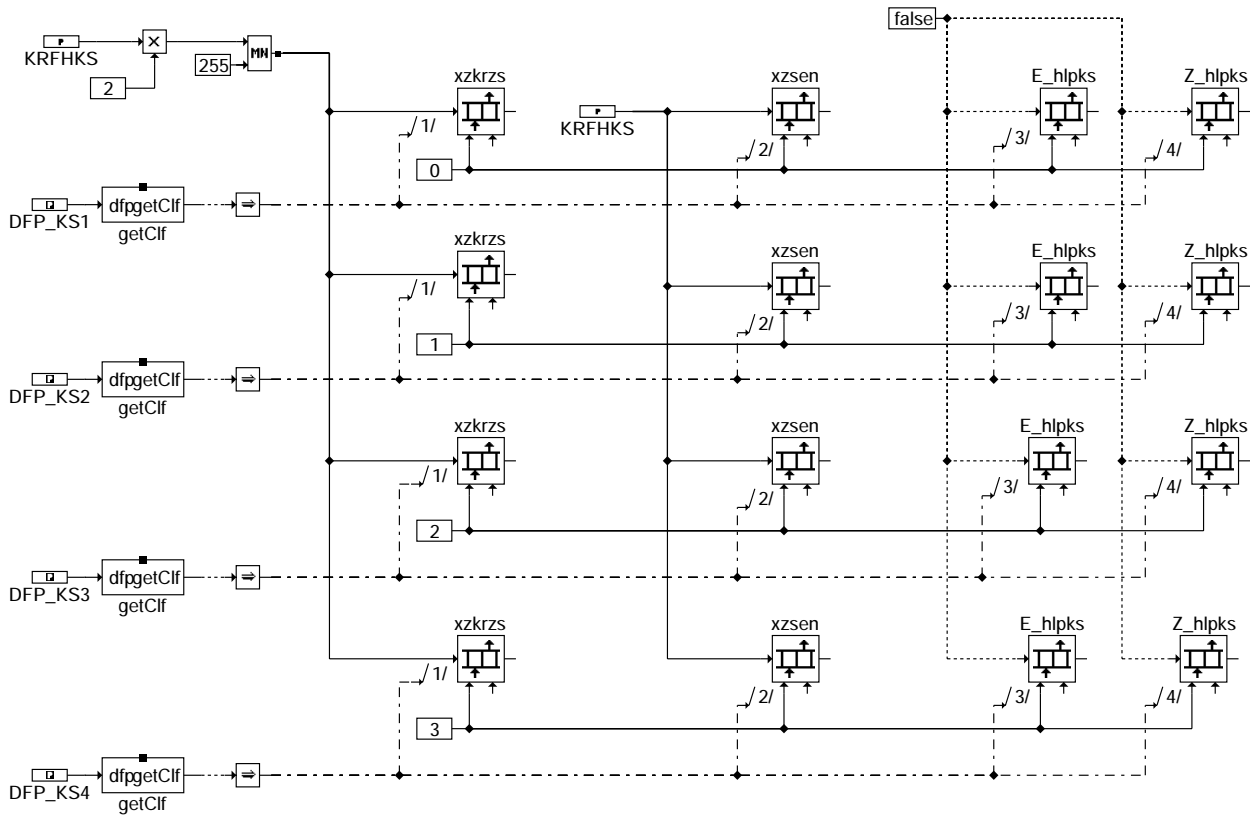


dkrs-dfpm-ks1

dkrs-dfpm-ks1



## FCMCLR: clear fault memory



### dkrs-fcmclr

In block diagrams error type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word `sfpxyz` of the error path `xyz` back into the central diagnosis management DFPM. The bits `E_xyz`, `Z_xyz`, `B_mxyz` etc. are contents of this status word. For error and cycle flags of external error paths which occur as inputs access methods are available which read these informations directly from the error path status managed in the DFPM.

For each error path the following values are defined:

status error path ks*:	<code>sfpks*</code>
error flag ks*:	<code>E_ks*</code>
cycle flag ks*:	<code>Z_ks*</code>
error type ks*:	<code>TYPks*</code>
	<code>B_mxks*</code>
	<code>B_mnks*</code>
delete error path:	<code>B_clks*</code>
error path code ks*:	<code>CDTks*</code>
error class ks*:	<code>CLAKs*</code>
error intensity ks*:	<code>TSFks*</code>
CARB code ks*:	<code>CDCKs*</code>
table of the environmental cond. ks*:	<code>FFTks*</code>

\* is a wildcard and stands here for the number of the knock sensor.

In this function definition (FDEF) the following error paths are treated:

```
knock sensor 1 ks1
knock sensor 2 ks2
knock sensor 3 ks3
knock sensor 4 ks4
```

Substitute measures if `E_ks(KS)`:

- Instead of the current cylinder-specific retardings the safety retarding is given out with `KRDWS` in the range "knock control active"
- KC adaptation not active (the adjusted values remain stored)
- knock detection algorithm remains active for the error healing
- In the range 'knock control not active' no retarding is performed



## ABK DKRS 29.80 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCKS1	BLOKNR		KL	code word CARB: knock sensor 1
CDCKS2	BLOKNR		KL	code word CARB: knock sensor 2
CDCKS3	BLOKNR		KL	code word CARB: knock sensor 3
CDCKS4	BLOKNR		KL	code word CARB: knock sensor 4
CDKKS1			FW	code word customer: knock sensor 1
CDKKS2			FW	code word customer: knock sensor 2
CDKKS3			FW	Code word customer: knock sensor 3
CDKKS4			FW	Code word customer: knock sensor 4
CDTKS1			FW	code word tester: knock sensor 1
CDTKS2			FW	code word tester: knock sensor 2
CDTKS3			FW	code word tester: knock sensor 3
CDTKS4			FW	code word tester: knock sensor 4
CLAKS1			FW	fault class: knock sensor 1
CLAKS2			FW	fault class: knock sensor 2
CLAKS3			FW	fault class: knock sensor 3
CLAKS4			FW	fault class: knock sensor 4
CWDKS1			FW	code word: knock sensor diagnosis, sensor 1
CWDKS2			FW	code word: knock sensor diagnosis sensor 2
CWDKS3			FW	code word: knock sensor diagnosis, sensor 3
CWDKS4			FW	code word: knock sensor diagnosis, sensor 4
FFTKS1	BLOKNR		KL	freeze frame table: knock sensor 1
FFTKS2	BLOKNR		KL	freeze frame table: knock sensor 2
FFTKS3	BLOKNR		KL	freeze frame table: knock sensor 3
FFTKS4	BLOKNR		KL	freeze frame table: knock sensor 4
KRFHKS			FW	fault frequency - knock sensors
NDKS			FW	engine-speed threshold for diagnosis knock sensors
SENZZYL			KWB (REF)	knock sensor for sw-cylinder counter 0-7
SNM16KRUB	NMOT		SV (REF)	datapoint distribution engine speed, 16 datapoints
SY_ZYLZA			SYS	system constant number of cylinders
TSFKS1			FW	fault active time: knock sensor 1
TSFKS2			FW	fault active time: knock sensor 2
TSFKS3			FW	fault active time: knock sensor 3
TSFKS4			FW	fault active time: knock sensor 4
UDKSNO	NMOT		KL	upper reference voltage threshold for diagnosis knock sensors
UDKSNU	NMOT		KL	lower reference voltage threshold for diagnosis knock sensors

Variable	Source	Type	Description
B_BKKS1	DKRS	AUS	condition: knock sensor 1 active
B_BKKS2	DKRS	AUS	condition: knock sensor 2 active
B_BKKS3	DKRS	AUS	condition: knock sensor 3 active
B_BKKS4	DKRS	AUS	condition: knock sensor 4 active
B_CLKS1		EIN	condition clear fault path knock sensor 1
B_CLKS2		EIN	condition clear fault path knock sensor 2
B_CLKS3		EIN	condition clear fault path knock sensor 3
B_CLKS4		EIN	condition clear fault path knock sensor 4
B_DS	DKRS	LOK	kc: sensor diagnosis active
B_DSI	DKRS	LOK	condition for active diagnosis: knock sensor i test
B_KR	KRRA	EIN	condition for knock control active
B_KRFDKS	KRRA	EIN	condition permission for knock sensor diagnosis
B_KRLDY	KRDY	EIN	Condition load dynamics for knock detection active
B_KRNDY	KRDY	EIN	condition speed dynamics for knock detection active
B_KS_MIN_I	DKRS	LOK	Condition: min error knock sensor i
B_MNKS1	DKRS	AUS	condition: min-error knock sensor 1
B_MNKS2	DKRS	AUS	condition: min-error knock sensor 2
B_MNKS3	DKRS	AUS	condition: min-error knock sensor 3
B_MNKS4	DKRS	AUS	condition: min-error knock sensor 4
B_MXKS1	DKRS	AUS	condition: max-error knock sensor 1
B_MXKS2	DKRS	AUS	condition: max-error knock sensor 2
B_MXKS3	DKRS	AUS	condition: max-error knock sensor 3
B_MXKS4	DKRS	AUS	condition: max-error knock sensor 4
B_NPKS1	DKRS	AUS	not plausible error: knock sensor 1
B_NPKS2	DKRS	AUS	not plausible error: knock sensor 2
B_NPKS3	DKRS	AUS	not plausible error: knock sensor 3
B_NPKS4	DKRS	AUS	not plausible error: knock sensor 4
B_PWF		EIN	Condition for powerfail
B_SIKS1	DKRS	AUS	error type: knock sensor 1
B_SIKS2	DKRS	AUS	error type: knock sensor 2
B_SIKS3	DKRS	AUS	error type: knock sensor 3
B_SIKS4	DKRS	AUS	error type: knock sensor 4
E_HKS_I	DKRS	LOK	auxiliary error flag: knock sensor i
E_HLPKS_I	DKRS	LOK	auxiliary error flag: knock sensor i
E_KS1	DKRS	AUS	error flag: knock sensor 1
E_KS2	DKRS	AUS	error flag: knock sensor 2
E_KS3	DKRS	AUS	error flag: knock sensor 3
E_KS4	DKRS	AUS	error flag: knock sensor 4
NMOT	SWADAP	EIN	engine speed
RKR	KRKE	EIN	reference level knock control
RKR_NW	DKRS	LOK	reference pegel nominaized for knock regulation
SFPKS1	DKRS	AUS	status fault path: knock sensor 1
SFPKS2	DKRS	AUS	status fault path: knock sensor 2
SFPKS3	DKRS	AUS	status fault path: knock sensor 3



Variable	Source	Type	Description
SFPKS4	DKRS	AUS	status fault path: knock sensor 4
UDKSNOA_W	DKRS	LOK	knock sensor diagnosis: actual value upper threshold (UDKSNO)
UDKSNUA_W	DKRS	LOK	knock sensor diagnosis: actual value lower threshold (UDKSNU)
VKR	KRKE	EIN	amplification stage knock control
XZKRZS(I)	DKRS	LOK	counter knock sensor cycle flag; individual relationship sensor-counter s.FDEF
XZSEN(I)	DKRS	LOK	safety counter knock sensor; individual relationship sensor - counter s. FDEF
Z_HLPKS_J	DKRS	LOK	auxiliary cycle flag: knock sensor i
Z_KS1	DKRS	AUS	cycle flag: knock sensor 1
Z_KS2	DKRS	AUS	cycle flag: knock sensor 2
Z_KS3	DKRS	AUS	cycle flag: knock sensor 3
Z_KS4	DKRS	AUS	cycle flag: knock sensor 4

### FW DKRS 29.80 Fixed Values

Parameter	Value	Description
CDKKS1		code word customer: knock sensor 1
CDKKS2		code word customer: knock sensor 2
CDKKS3		Code word customer: knock sensor 3
CDKKS4		Code word customer: knock sensor 4
CDTKS1		code word tester: knock sensor 1
CDTKS2		code word tester: knock sensor 2
CDTKS3		code word tester: knock sensor 3
CDTKS4		code word tester: knock sensor 4
CLAKS1		fault class: knock sensor 1
CLAKS2		fault class: knock sensor 2
CLAKS3		fault class: knock sensor 3
CLAKS4		fault class: knock sensor 4
CWDKS1		code word: knock sensor diagnosis, sensor 1
CWDKS2		code word: knock sensor diagnosis sensor 2
CWDKS3		code word: knock sensor diagnosis, sensor 3
CWDKS4		code word: knock sensor diagnosis, sensor 4
KRFHKS		fault frequency - knock sensors
NDKS		engine-speed threshold for diagnosis knock sensors
TSFKS1		fault active time: knock sensor 1
TSFKS2		fault active time: knock sensor 2
TSFKS3		fault active time: knock sensor 3
TSFKS4		fault active time: knock sensor 4



### FB DKRS 29.80 Detailed description of function

By means of the diagnosis knock sensor drop off a disconnection of the wiring to the knock sensor ( e.g. not plugged sensor ) as well as a short circuit to U\_Batt or ground can be detected. Furthermore it can point to a defect engine if an error is detected ( e.g. increased noise level due to expanded piston groove ).

The decisive signal for these tests is the normalized reference level rkrn(i) obtained from the reference level rkr and the amplification stages vkr of each cylinder. The calculation of the normalized reference level rkrn(i) for the test UDKSNO > rkrn > UDKSNU is performed according to:

$$rkrn(i) = ( 1 / ( 2^{vkr(i)} ) ) * rkr(i) * 2^6$$

The assignment of the knock sensors to the normalized reference levels is performed via SENZZYL which is described in %GGKS. In this case the normalized reference level rkrn\_0 belongs to SENZZYL0, i.e. rkrn\_0 belongs to the error path of the knock sensor entered into SENZZYL0.

The diagnosis is activated in case of:

- knock control activ (B.kr) and
- no dynamics conditions (!B.krndy and !B.krldy) and
- nmot above threshold NDKS and
- no IC-error (!E.krnt, !E.krtp and !E.krof)
- B.krfdks (see %KRRA 18.40 or higher)

If the current reference level - in case of KC active (B.kr) and engine speeds greater than NDKS and no phase sensor error ( B.synph ) and not detected dynamic response ( ! B.krndy and ! B.krldy ) - undershoots resp. exceeds the reference level thresholds UDKSNU resp. UDKSNO which are stored in the engine speed-dependent characteristic lines for KRFHKS successive tests ( i.e. an error which lies in between and is not detected means reset of the error counter ) then a knock sensor drop off E.ks(KS) is detected and the above-described substitution measures are taken.

The error check is performed once per 100 ms grid for the normalized reference levels of all cylinders, i.e. each knock sensor path is checked several times in the process. An error is detected if a normalized reference level of the knock sensor path lies outside the limits during the check. No error is only detected if all normalized reference levels of the knock sensor path lie within the limits. To avoid a unnecessary activation of the KC safety measures after a ECU-reset, B.krdws cannot be set in the first 3 seconds after c.inisyn.

The safety measures are lifted again if the current reference level lies again within the range defined by the reference voltage thresholds UDKSNO and UDKSNU for KRFHKS successive checks ( i.e. an error check which lies in between means reset of the counter ). So that no jumps in the ignition angle ( torque ) occur during the error healing the transition from safety retarding back to normal operating is performed not until the first 'knock control-not-active-phase' after determined error healing.

The cycle flags Z\_ks(KS) are set after an each time (2\*KRFHKS)-times diagnosis check ( counter xzkrzs(KS-1) ) or if an error is definitely dedected or healed. Thus it is ensured that e.g. after the repair in a workshop the error diagnosis is at least run through with the debouncing frequency KRFHKS in order to reliably determine the error clearance. During the initialization with C.ini the cycle flags Z\_ks(KS) as well as the counters xzkrzs(KS-1) are reset.

The sensor diagnosis can be switched off for each knock sensor individually by setting CWDKS(KS) = 0. ( The corresponding cycle flags are then set to 1 and the error flags to 0 ). The activation or deactivation may only take place during the ECU reset so as to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means all CWDKS(i) must be set to a value > 0 ).

The calculation of the normalized reference level and the evaluation of the path for the change-over to safety retarding are not switched off by the switches.

**APP DKRS 29.80 Application hint**

The characteristic lines UDKSNU and UDKSNO must be adjusted such that there is a sufficient safety margin to normal operating and that a unplugged knock sensor is detected just as a short circuit to ground or U\_Batt. The application of the characteristic lines UDKSNU and UDKSNO must be performed with max.- and min.-sensors. Thereby a safety margin of at least factor 2 is to be kept to.

In order to ensure that the application engine with its noise behaviour lies within the tolerance of the mass production the normalized reference levels should be checked every 500 rpm on all engines available during the application and on at least one pilot vehicle.

These measurements are performed with mass production knock sensors. The measured normalized reference levels must lie within the limits determined with min.- and max.-sensors ( safety margin of at least factor 2 to the characteristic lines UDKSNU and UDKSNO ).

Should no sufficient safety margin be guaranteed in some parts of the range ( an intact, connected knock sensor may under no circumstances lead to the error lamp being switched on ) then it has to be done without the possibility of diagnosis in these partial ranges ( fix threshold in such a way that the diagnosis does not react ).  
The customer must be informed about these partial ranges.

When load or engine speed dynamic response is triggered the normalized reference levels can possibly exceed the characteristic line UDKSNO for a short time. For this reason the diagnosis is not performed in case of detected dynamic response ( B\_krldy oder B\_krndy ).

Nevertheless a check of the debouncing period is recommendable in this case because the refence levels have not yet again stabilized after the end of the dynamic response.

With low engine speeds there may be ranges in which an error detection is not possible. Therefore an engine speed threshold NDKS was introduced below which the diagnosis is blocked. The threshold must be adjusted such that errors which were detected during higher engine speeds are not falsely healed again in the lower range.

The amount available knock sensors must be set in the fixed value KSZA. The amount available knock sensors must be set in the fixed value KSZA. If the guiding cylinder function is active and the system has only one knock sensor, KSZA has to be two. If phase sensor emergency operating mode with double ignition is possible in the project and the system has only one knock sensor, KSZA has to be two.

The initialization of the reference level with REFINI during the starting phase or during the transition from KC not active to KC active can possibly lead to a wrong error detection or error healing.

When fixing the initialization values for the amplification and for the reference level attention must be paid that the normalized reference level has stabilized prior to the end of the debouncing time ( error frequency counter ), that means the debouncing period must be large enough so that wrong error detections or healings are ruled out.

The sensor diagnosis can be switched off for each knock sensor individually by setting CWDKS(KS) = 0. ( The corresponding cycle flags are then set to 1 and the error flags to 0 ). The activation or deactivation may only take place during the ECU reset so as to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means all CWDKS(i) must be set to a value > 0 ).

The values E\_hks\* contained in the ASCET pictures are only aid values for the representation and they cannot be measured.

The following guidance values are recommended:

KRFHKS > 20 ( KRFHKS = 0 is inadmissible )  
NDKS > 2000 rpm  
CWDKS1 = 1  
CWDKS2 = 1  
CWDKS3 = 1  
CWDKS4 = 1

Needed measured values:

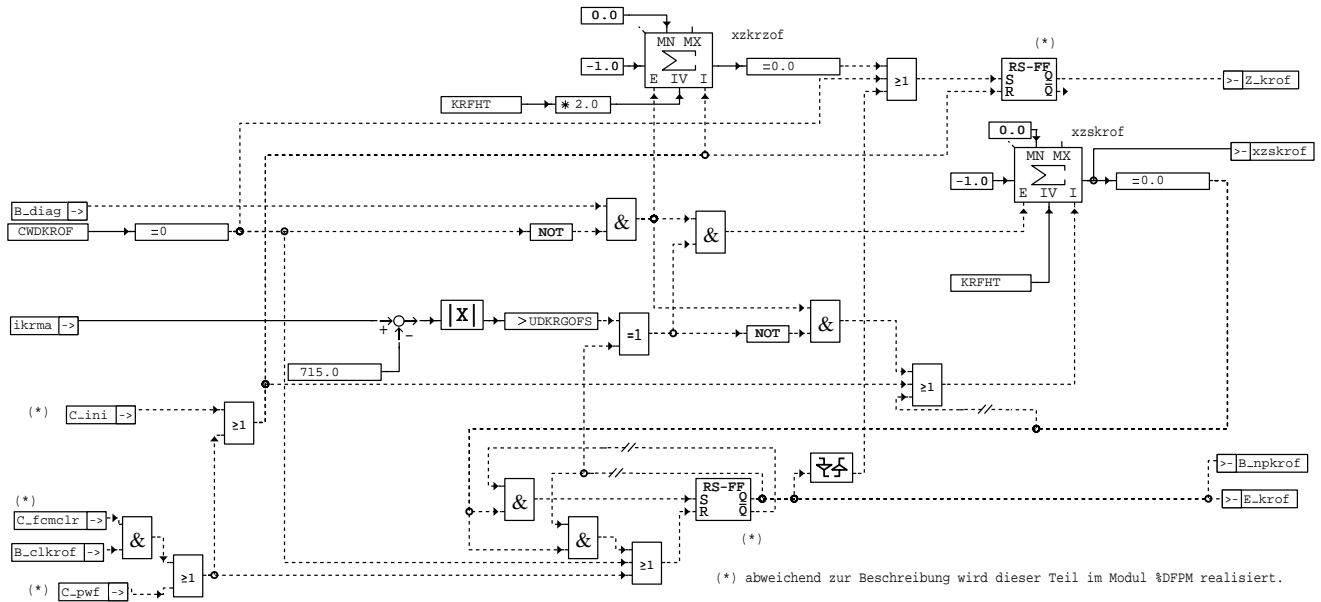
- E\_ks1 - x
- Z\_ks - x
- B\_krdws
- nmot
- rkrn\_w0 - x
- xzkrzs0 - x
- xzsen0 - x

**DKRNT 11.10 Diagnosis; Knock-control, zero-test (OBDII)****FDEF DKRNT 11.10 Function definition**

Missing picture

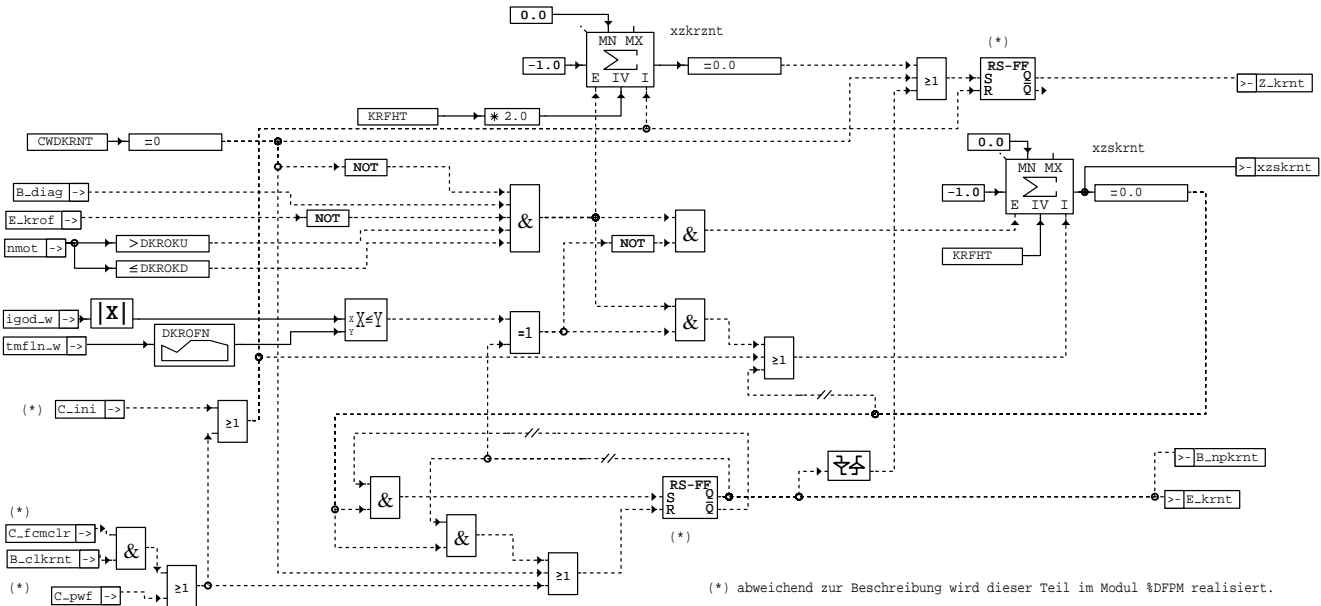
dkrnt-dkrnt

dkrnt-dkrnt



dkrrt-resetwnt

**dkrrt-resetwnt**



dkrrt-nulltest

**dkrrt-nulltest**



In block diagrams error type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the error path xyz back into the central diagnosis management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external error paths which occur as inputs access methods are available which read these informations directly from the error path status managed in the DFPM.

For each error path the following values are defined:

```

status error path krof:      sfpkrof
error flag krof:           E_krof
cycle flag krof:           Z_krof
error type krof:           TYPkrof
                           B_npkrof
delete error path:         B_clkrof
error path code krof:      CDTkrof
error class krof:          CLAkrof
error intensity krof:      TSFkrof
CARB code krof:           CDCkrof
table of environmental cond. krof: FFTkrof
    
```

```

status error path krnt:     sfpkrnt
error flag krnt:           E_krnt
cycle flag krnt:           Z_krnt
error type krnt:           TYPk(i)
                           B_npkrnt
delete error path:         B_clkrnt
error path code krnt:      CDTkrnt
error class krnt:          CLAKrnt
error intensity krnt:      TSFKrnt
CARB code krnt:           CDCkrnt
table of environmental cond. krnt: FFTkrnt
    
```

In this function definition (FDEF) the following error paths are treated:

```

integrator reset value (offset)   krof
integrator gradient (zero test)   krnt
    
```

Substitute measures :

- Instead of the current cylinder-specific retardings the safety retarding is given out with KRDWS in the range "knock control active"
- KC adaptation not active (the adjusted values remain stored)
- knock detection algorithm remains active for the error healing
- In the range 'knock control not active' no safety retarding is performed

## ABK DKRNT 11.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCKRNT	BLOKNR		KL	code word CARB: knock control zero test pulse
CDCKROF	BLOKNR		KL	code word CARB: knock control offset
CDTKRNT			FW	code word tester: knock control zero test pulse [220]
CDTKROF			FW	code word tester: knock control offset
CLAKRNT			FW	fault class: knock control zero test
CLAKROF			FW	fault class: knock control offset
CWDKRNT			FW	code word: kc-diagnosis integrator gradient
CWDKROF			FW	code word: kc-diagnosis reset value
DKROFN	TMFLN_W		KL	limit of integrator rise for zero test
DKROKD			FW	upper rpm-limit for zero test diagnosis (knock control)
DKROKU			FW	lower rpm-limit for determination of offset-compensation-value
FFTKRNT	BLOKNR		KL	freeze frame table: knock control zero test
FFTKROF	BLOKNR		KL	freeze frame table: knock control offset
KRFHT			FW	error frequency, test pulse
TSFKRNT			FW	fault active time: knock control zero test
TSFKROF			FW	fault active time: knockcontrol offset
UDKRGOF5			FW	voltage threshold for DIA/KR basic offset amplifier

Variable	Source	Type	Description
B.CLKRNT		EIN	condition clear fault path kc-diagnosis integrator gradient
B.CLKROF		EIN	condition clear fault path kc-diagnosis reset value
B.NPKRNT	DKRNT	AUS	condition plausibility error of kc-diagnosis intgrator gradient
B.NPKROF	DKRNT	AUS	condition plausibility error of kc-diagnosis reset value
C.FCMCLR		EIN	system state: reset fault memory
C.JNI	SWADAP	EIN	ECU-condition for intialisation
C.PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E.KRNT	DKRNT	AUS	error flag: knock control zero test
E.KROF	DKRNT	AUS	Errorflag: knock control offset
IGOD_W	GGKS	EIN	integrator gradient for zero test diagnosis knock control
IKRMA		EIN	integrator value at start of measurement window, knock control
NMOT	SWADAP	EIN	engine speed
SFPKRNT	DKRNT	AUS	status fault path: knock control zero test
SFPKROF	DKRNT	AUS	status fault path: knock control offset
TMFLN_W		EIN	duration of measurement window knock control zero test
TPNT_AKTIV	EGKE	EIN	activation of kc-functions
XZKRZNT	DKRNT	LOK	counter for knock control cycle flag Z_krnt
XZKRZOF	DKRNT	LOK	counter for knock control cycle flag Z_krof
XZSKRNT	DKRNT	AUS	safety counter for knock control zero test
XZSKROF	DKRNT	AUS	safety counter for knock control offset



Variable	Source	Type	Description
Z_KRNT	DKRNT	AUS	cycle flag: knock control zero test
Z_KROF	DKRNT	AUS	cycle flag: knock control offset

### FW DKRNT 11.10 Fixed Values

Parameter	Value	Description
CDTKRNT		code word tester: knock control zero test pulse [220]
CDTKROF		code word tester: knock control offset
CLAKRNT		fault class: knock control zero test
CLAKROF		fault class: knock control offset
CWDKRNT		code word: kc-diagnosis integrator gradient
CWDKROF		code word: kc-diagnosis reset value
DKROKD		upper rpm-limit for zero test diagnosis (knock control)
DKROKU		lower rpm-limit for determination of offset-compensation-value
KRFHT		error frequency, test pulse
TSFKRNT		fault active time: knock control zero test
TSFKROF		fault active time: knockcontrol offset
UDKRGOF5		voltage threshold for DIA/KR basic offset amplifier

### FB DKRNT 11.10 Detailed description of function

The zero test serves for the determination of the integrator offset and for the checking of the KC-evaluation-IC CC195 with regard to

- keeping to the valid limits for the starting value of the integrator ( integrator reset value )
- keeping to the admissible integrator offsets
- the function of the multiplexer regarding 'open switch'

During the zero test all multiplexer switches are brought into the position 'open' ( deactivate signal sources ). The amplitude of the integrator is watched in a measuring window. Then the plausibility of the reset value and the integrator offset is checked. If the integration result lies within the limits of the permitted offset then the determined value is used for the offset compensation. If the integration result is markedly larger than the permitted offset then it can be assumed that the switch of the multiplexer is stuck in the position 'closed'.

1) Reset values ==> Checking of the integrator value at the beginning of the measuring window ( picture RESETWNT ):

The plausibility of the integrator voltage  $ikrma$  at the beginning of the measuring window and with deactivated signal sources is checked. In this case the following must apply:  $| ikrma - 715 \text{ mV} | < UDKRGOF5$ .

The counters  $xzskrof$ ,  $xzkrzof$  and the flags  $E\_krof$  and  $Z\_krof$  are part of this diagnosis ( error path offset ).

2) Zero test ==> Checking of the integrator gradient  $igod\_w$  ( picture NULLTEST ):

The integrator gradient ( integrator value at end of measuring window minus integrator at beginning of measuring window with open multiplexer switch divided by the current measuring window length ) is checked for plausibility. The following must apply:  $| igod\_w | < DKROFN(tmfln\_w)$ .

DKROFN is a characteristic line over the zero test measuring window length. While using the characteristic line the diagnosis is active in a great speed range.

The value  $igod\_w$  determined in %GGKS may not be used for the diagnosis of stuck MUX-switches if the measuring window lengths are  $> 5 \text{ ms}$  since in this case a definite distinction between permitted integrator offset and stuck MUX-switch is not possible ( in case of 10 ms measuring window lengths the permitted integrator offset is 300 mV and it thus lies within the normal integral range between 300 and 1000 mV ==> double safety results in a max. measuring window lengths of 5 ms ). This is achieved by the threshold DKROKU. When the lower engine speed threshold DKROKU is undershot the integrator gradient  $igod\_w$  is determined but no diagnosis with regard to DKROFN(tmfln\_w) ( stuck MUX-switch ) is performed.

The diagnosis can be switched off with an upper engine speed threshold. In this case the diagnosis is not performed. This is achieved by the upper engine speed threshold DKROKD. The diagnosis of the integrator gradient is frozen above the engine speed threshold.

Application hints see below

The counters  $xzskrnt$ ,  $xzkrznt$  and the flags  $E\_krnt$  and  $Z\_krnt$  are part of this diagnosis ( error path zero test ).

3) Conditions for the execution of the zero test ( s %GGKS ):

The diagnosis zero test (DKRNT) and test pulse (DKRTP) are normally triggered alternately approx. every 255 working cycles ( i.e. DKRNT, after 255 working cycles DKRTP, after further 255 again DKRNT etc. )

The zero test is performed if the knock control is active ( i.e.  $B\_kr=1$  ). In case the KC is not active while the zero test is to be performed the state is frozen and a zero test is performed at the next transition from  $!B\_kr$  to  $B\_kr$ .

In case of suspected error of a diagnosis, i.e. the error counter of the corresponding diagnosis does not have the value KRFHT, zero test and test pulse are no longer performed alternately. Instead the diagnosis which generated the suspected error is carried out at approx. 120 working cycles until the error is definitely detected or healed. Thereafter a change back to the normal state is performed. This applies analogous for the healing.

In order to obtain reasonable starting values for the offset correction the values for  $ikrma$  and  $igokr$  are determined but not diagnosed if  $tmot > TMKR-5^\circ\text{C}$  and if the KC is not yet active.

4) Amplification during zero test

The amplification during zero test must be equal to the current amplification of the current measuring window. (Theoretically also larger amplifications are possible and sensible in order to increase the reliability of detecting a stuck multiplex switch. However, these can cause additional problems if a disturbance noise from the printed board in the CC195 exists ==> falsely a stuck





multiplex switch is then detected). For the adjustment of the amplification see %GGKS resp. %KRKE.

#### 5) Error healing and error management

If the respective checks result in inadmissible values then the corresponding error counter xzskrxx is decremented. An error entry into the error memory ( E\_krof resp. E\_krnt ) and a reset of the respective error counter to KRFHT are performed for the detected error after KRFHT-times consecutive error checks ( i.e. an error which lies in between and is not detected means reset of the respective error counter )

After KRFHT-times consecutive healing checks ( i.e. an error check which lies in between means reset of the counter ) error healing and a reset of the error counter to KRFHT are performed.

So that no jumps in the ignition angle ( torque ) occur during the error healing the transition from safety retarding back to normal operating is performed only in the first "KC-not-active-phase" after error healing was determined ( s. %DKRS ).

The cycle flags Z\_krof and Z\_krnt are set after (2\*KRFHT)-times diagnosis checks ( counters xzkrzof and xzkrznt ) or if an error is definitely detected or healed. Thus it is ensured that, e.g. after the repair in a workshop, the error diagnosis must be at least run through with the debouncing frequency KRFHT in order to reliably determine the error clearance ( Z\_krtp = 1 & E\_krtp = 0 ).

During the initialization with C.ini the cycle flags Z\_krof and Z\_krnt as well as the cycle and error flags are reset.

The diagnosis of the integrator gradient can be switched off by CWDKRNT=0 and the diagnosis of the starting value can be switched off by CWDKROF=0. (The corresponding cycle flags are then set to 1 and the error flags are set to 0).

Through deactivation of the diagnosis only the evaluation is suppressed. The zero test is still performed since the values are needed for the offset correction.

The activation or deactivation may only take place during the ECU reset in order to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means CWDKRNT and CWDKROF must be set to a value > 0.)



## APP DKRNT 11.10 Application hint

The limit value for the tolerance of the reset value is 100 mV according to the specification of the CC195 for the reset value. The limit value for the integrator gradient - according to the specification of the CC195 - is dependent on the internal pulse frequency of the CC195.

Frequency	100 kHz	110 kHz	120 kHz	130 kHz	140 kHz	150 kHz
Limit value f. integrator gradient acc. to specification of the CC195	+/- 30 mV/ms	+/- 36 mV/ms	+/- 42 mV/ms	+/- 48 mV/ms	+/- 54 mV/ms	+/- 60 mV/ms

(specification values as at September 1996)

However, when using these limits it has shown that disturbance noises from the printed board in the CC195 or disturbances of the supply voltage of the CC195 can easily lead to a diagnosis misdetection. Due to this reason it may be necessary to broaden these limits. This must be checked in each individual case. For this measurements need to be performed. Generally it should obviously be ensured that no disturbance noises occur into the CC195! ( Layout updating! )

The diagnosis threshold UDKRGOPS = 220 mV is recommended for the reset value.

The following is recommended for the integrator gradient threshold DKROFN (internal pulse Frequency of CC195: 100 kHz)

measuring window length	tmfln_w > 3 ms	3 ms > tmfln_w > 2 ms	2 ms > tmfln_w > 1,5 ms	1,5 ms > tmfln_w > 1 ms
DKROFN	40 mV/ms	45 mV/ms	50 mV/ms	60 mV/ms

DKROKU must set to a value, so that the zero test measuring window length is < 5 ms (description s. 2)).

The diagnosis can be switched off via the upper engine speed threshold DKROKD, so that in case of short measuring window lengths the diagnosis-threshold DKROFN is not too great. DKROKD has to be greater than DKROKO (s.%GGKS).

The protection of the ECU-dependent value is absolutely necessary.

In case a broadening of the recommended values is necessary it should be discussed with the function application or with the function development first.

The error frequency of the functions DKRNT and DKRTP ( master functions ) is identical. Both use the label KRFHT.

The diagnosis of the integrator gradient can be switched off by CWDKRNT=0 and the diagnosis of the starting value can be switched off by CWDKROF=0. (The corresponding cycle flags are then set to 1 and the error flags are set to 0).

Through deactivation of the diagnosis only the evaluation is suppressed. The zero test is still performed since the values are needed for the offset correction.

The activation or deactivation may only take place during the ECU reset in order to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means CWDKRNT and CWDKROF must be set to a value > 0.)

The values tpnt.aktiv and B\_diag cannot be measured with VS100.

The following guidance values are recommended:

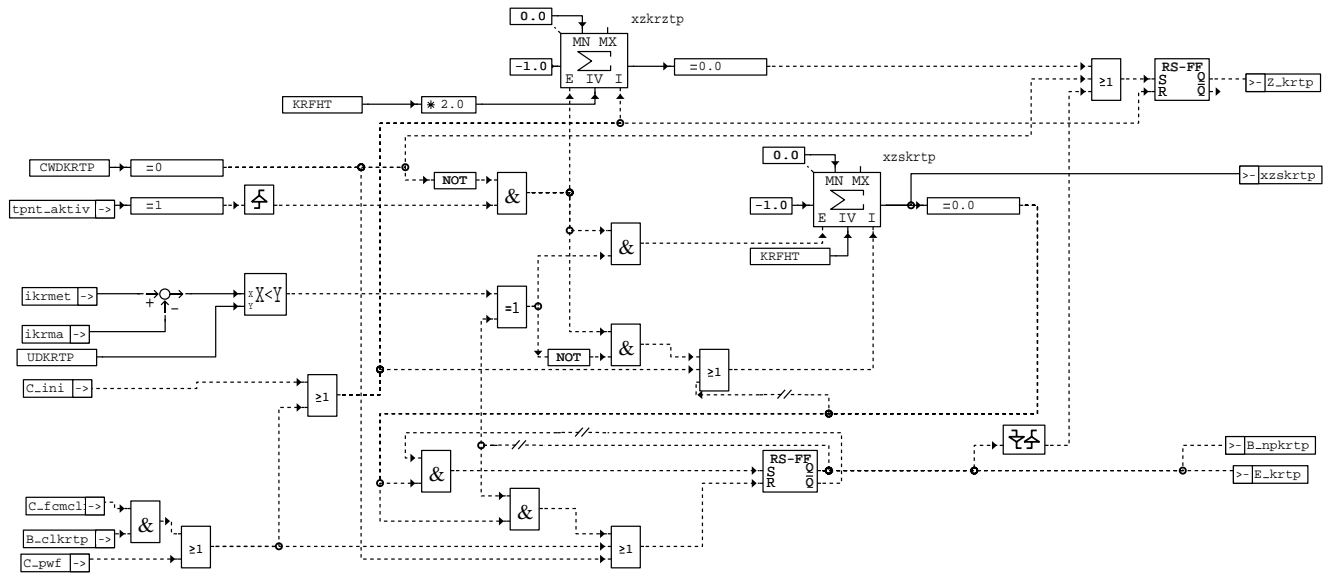
KRFHT > 2 ( KRFHT = 0 inadmissible )  
UDKRGOPS = 220 mV  
DKROKU ca. 2000 rpm ( measuring window > 5 ms )  
CWDKRNT = 1  
CWDKROF = 1

Needed measured values:

- B\_dnt
- B\_kr
- E\_krnt
- E\_krof
- igod\_w
- ikrma
- nmot
- zzkrznt
- zzkrzof
- zzskrnt
- zzskrof
- Z\_krnt
- Z\_krof

## DKRTP 11.10 Diagnosis of knock control, test pulse for OBDII

### FDEF DKRTP 11.10 Function definition



#### dkrtp-dkrtp

In block diagrams error type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpkxyz of the error path xyz back into the central diagnosis management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external error paths which occur as inputs access methods are available which read these informations directly from the error path status managed in the DFPM.

For each error path the following values are defined:

status error path krtp:	sfpkrtp
error flag krtp:	E_krtp
cycle flag krtp:	Z_krtp
error type krtp:	TYPkrtp
	B_npkrtp
delete error path:	B_clkrtp
error path code krtp:	CDTkrtp
error class krtp:	CLAKrtp
error intensity krtp:	TSPkrtp
CARB code krtp:	CDCKrtp
table of the environmental cond. krtp:	FFTKrtp

In this function definition (FDEF) the following error paths are treated:

test pulse krtp

Substitute measures in case of E\_krtp:

- Instead of the current cylinder-specific retardings the safety retarding is given out with KR DWS in the range "knock control active"
- KC adaptation not active (the adjusted values remain stored)
- knock detection algorithm remains active for the error healing
- In the range 'knock control not active' no retarding is performed

#### ABK DKRTP 11.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCK RTP	BLOKNR		KL	code word CARB: knock control test pulse
CDTK RTP			FW	code word tester: knock control test pulse
CLAK RTP			FW	fault class: knock control test pulse
CWDK RTP			FW	code word: kc-diagnosis testpulse
FFTK RTP	BLOKNR		KL	freeze frame table: knock control test pulse
KRFHT			FW	error frequency, test pulse
TSPK RTP			FW	fault active time: knock control test pulse
UDK RTP			FW	integr.volt.thresh. f.diagn. knock eval.circ. test pulse

Variable	Source	Type	Description
B_CLK RTP		EIN	condition clear fault path kc-diagnosis test pulse
B_NPK RTP	DKRTP	AUS	condition plausibility error fo kc-diagnosis test pulse
C_FCM CLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for initialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_K RTP	DKRTP	AUS	error flag: knock control test pulse
IKRMA		EIN	integrator value at start of measurement window, knock control
IKR MET		EIN	integrator value at end of measurement window, knock control test pulse



Variable	Source	Type	Description
SFPKRTP	DKRTP	AUS	status fault path: knock control test pulse
TPNT_AKTIV	EGKE	EIN	activation of kc-functions
XZKRZTP	DKRTP	LOK	Timer knock control cycle flag Z_krtp
XZSKRTP	DKRTP	AUS	Timer knock control error flag E_krtp
Z_KRTP	DKRTP	AUS	cycle flag: knock control test pulse

### FW DKRTP 11.10 Fixed Values

Parameter	Value	Description
CDTKRTP		code word tester: knock control test pulse
CLAKRTP		fault class: knock control test pulse
CWDKRTP		code word: kc-diagnosis testpulse
KRFHT		error frequency, test pulse
TSFKRTP		fault active time: knock control test pulse
UDKRTP		integr.volt.thresh. f.diagn. knock eval.circ. test pulse

### FB DKRTP 11.10 Detailed description of function

The test pulse serves for the checking of the knock evaluation circuit CC195. By the test pulse an error localization (knock sensor - evaluation circuit) is made possible.

If the raw integral value (  $ikrmet - ikrma$  ), i.e. without offset compensation ( s. GGKS ) undershoots the value UDKRTP then the error counter xzskrtp is decremented. After KRFHT-times, consecutive error checks ( i.e. an error which lies in between and was not detected means reset of the error counter ) an error entry into the error memory (  $E\_krtp = 1$  ) and a reset of the error counter to KRFHT is performed. In the following tests a checking of whether the error state was healed is carried out. After KRFHT-times consecutive checks of the healing ( i.e. an error which lies in between and is detected means reset of the counter ) the error healing (  $E\_krtp = 0$  ) and a reset of the error counter to KRFHT is performed.

The diagnosis zero test (DKRNT) and test pulse (DKRTP) are normally triggered alternately approx. every 255 working cycles (i.e. DKRNT, after 255 working cycles DKRTP, after further 255 again DKRNT etc.)  
The test pulse is performed if the temperature threshold for the KC was exceeded (i.e.  $B\_tmkr=1$  fulfilled).

In case of suspected error, i.e. the error counter of a diagnosis does not have the value KRFHT, the diagnosis are no longer performed alternately. Instead the diagnosis which generated the suspected error is carried out at approx. 120 working cycles until the error is definitely detected or healed. Thereafter a change back to the normal state is performed. This applies analogous for the healing ( s. %GGKS )

The test pulse must be performed at a random distribution so that all knock sensor paths are checked in a statistically uniform distribution. By omitting a combustion evaluation the test pulse is carried out in a normal measuring window.  
The amplification of the knock evaluation circuit is set to  $2^3$  ( medium amplification ). Thus it is ensured that also in case of short measuring windows the integrator is fully activated. The frequency of the test pulse is adjusted to the filter center frequency of the band pass.

So that no jumps in the ignition angle ( torque ) occur during the error healing the transition from safety retarding back to normal operating is performed only in the first "KC-not-active-phase" after error healing was determined ( see %DKRS ).

The cycle flag Z\_krtp is set after (  $2 \cdot KRFHT$  )-times diagnosis checks ( counter xzkrztp ) or if an error is definitely dedected or healed. Thus it is ensured that e.g. after the repair in a workshop the error diagnosis must be at least run through with the debouncing frequency KRFHT in order to reliably determine the error clearance (  $Z\_krtp = 1$  &  $E\_krtp = 0$  ).  
During the initialization with C.ini the cycle flag Z\_krtp and the counter xzkrztp are reset.

The diagnosis can be switched off by CWDKRTP=0. (The cycle flag is set to 1 and the error flag is set to 0).  
Through deactivation of the diagnosis the evaluation and the triggering of the CC195 are suppressed ( s. %GGKS ). The activation or deactivation may only take place during the ECU reset so as to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means CWDKRTP must be set to a value  $> 0$ .)

## APP DKRTP 11.10 Application hint

The error frequency of the functions DKRNT and DKRTP ( master functions ) is identical. Both use the label KRFHT.

The diagnosis can be switched off by CWDKRTP=0. (The cycle flag is set to 1 and the error flag is set to 0).  
Through deactivation of the diagnosis the evaluation and the triggering of the CC195 are suppressed ( s. %GGKS). The activation or deactivation may only take place during the ECU reset so as to ensure that the function is correctly performed.

Hint: This diagnosis may only be switched off for application purposes and not for mass production since otherwise IC-errors cannot be detected which may lead to knock damages on the engine. ( That means CWDKRTP must be set to a value > 0.)

The value tpnt\_aktiv cannot be measured with VS100.

The following guidance values are recommended:

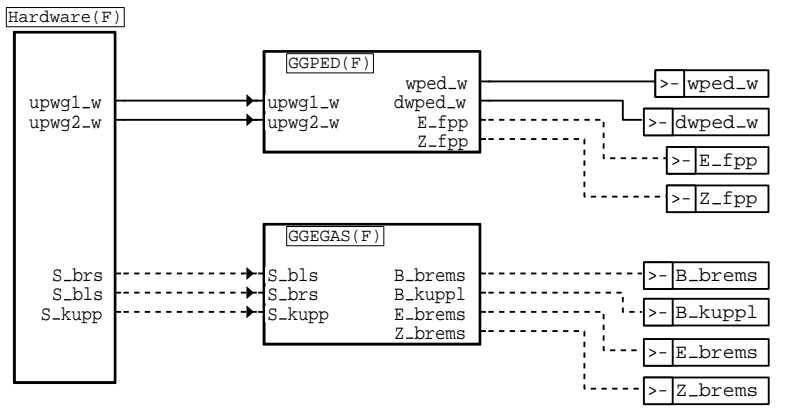
UDKRTP = 3,7 V  
KRFHT > 2 ( KRFHT = 0 inadmissible )  
CWDKRTP = 1

Needed measured values:

- ikrma
- ikrmet
- xzkrztp
- xzskrtp
- B\_dtp
- E\_krtp
- Z\_krtp

## EGEG 1.0 Input variable E-GAS

### FDEF EGEG 1.0 Function definition



egeg-egeg

### ABK EGEG 1.0 Abbreviations

Variable	Source	Type	Description
B_BREMS	EGEG	AUS	condition: brake operated
B_KUPPL	EGEG	AUS	EGAS Condition clutch is disengaged
DWPED_W	EGEG	AUS	gradient of the standardized accelerator pedal angle
E_BREMS	EGEG	AUS	error flag: brake pedal signal
E_FPP	EGEG	AUS	Error flag drive pedal potentiometer
S_BLS		EIN	brake light switch (true=activated pedal)
S_BRS		EIN	Switch for brake
S_KUPPL		EIN	Clutch switch
UPWG1_W		EIN	Voltage PWG potentiometer 1 (word)
UPWG2_W		EIN	Voltage PWG potentiometer 2 (word)
WPED_W	EGEG	AUS	normed angle acceleration pedal
Z_BREMS	EGEG	AUS	cycle flag: brake pedal signal
Z_FPP	EGEG	AUS	Cycle flag drive pedal potentiometer

### FW EGEG 1.0 Fixed Values

Parameter	Value	Description
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### FB EGEG 1.0 Detailed description of function

The overview shows the functions

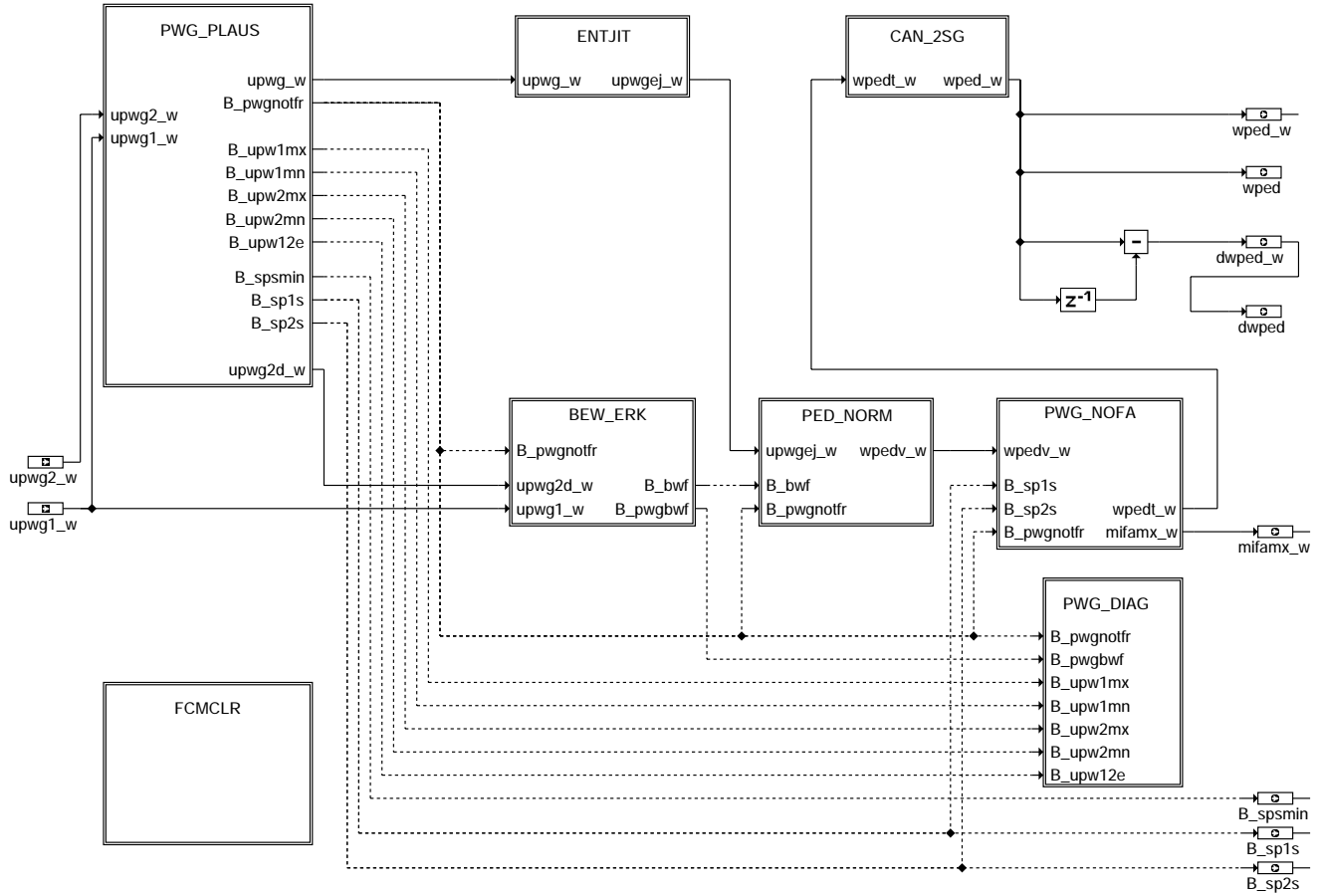
- GGPED: Evaluation of accelerator pedal sensors with plausibility check,
- GGEGAS: Evaluation of brake switches and clutch switch.



APP EGEG 1.0 Application hint

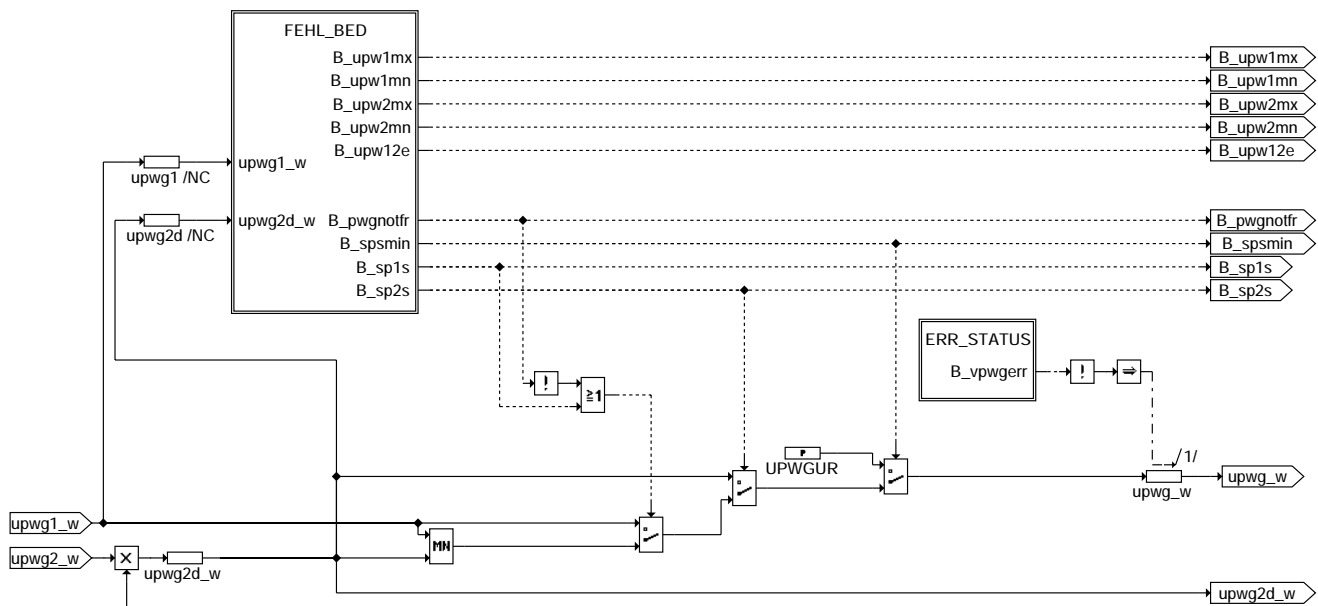
## GGPED 8.30 Sensor variable for accelerator pedal

### FDEF GGPED 8.30 Function definition



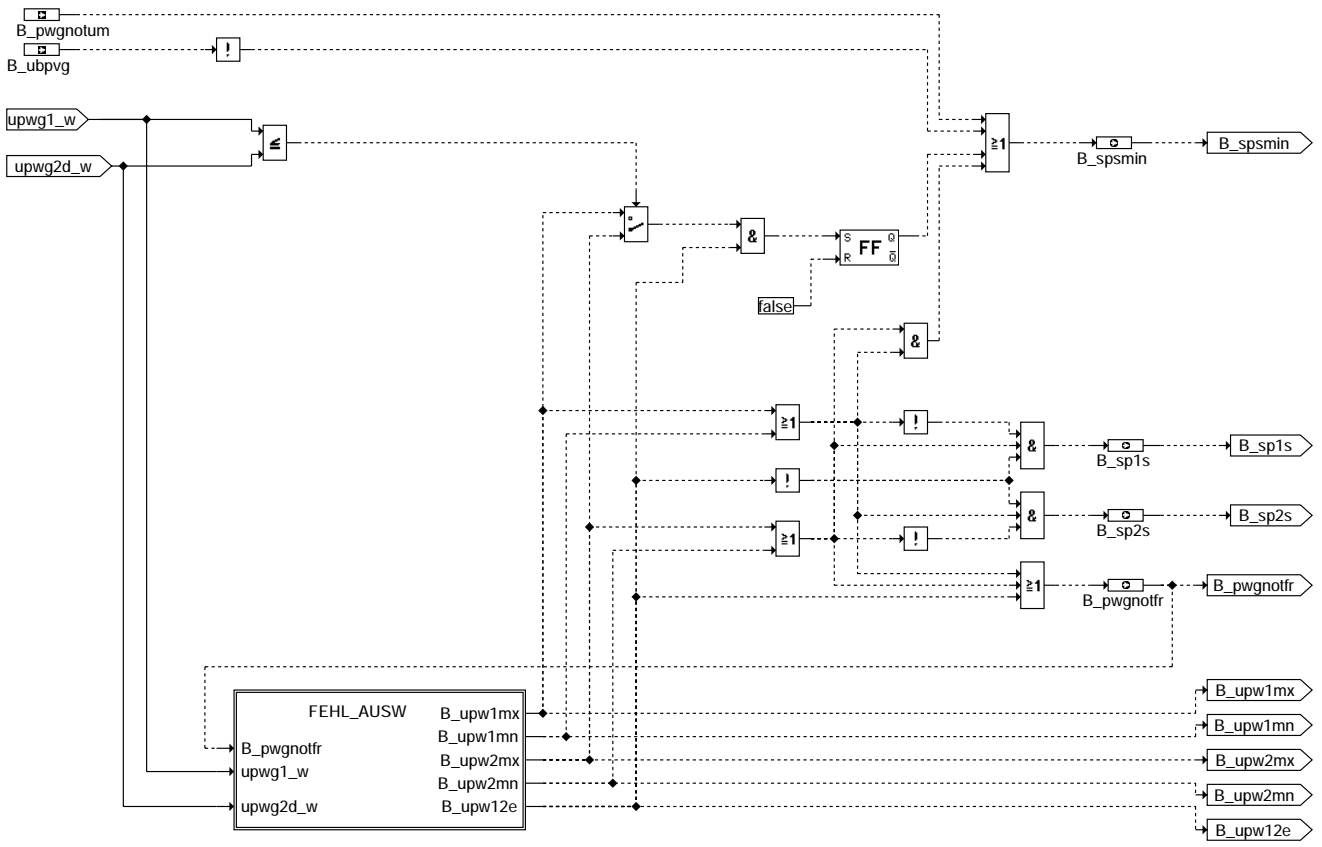
ggped-main

### PWG\_Plaus: Plausibilitätsprüfung der beiden PWG-Poti-Spannungen



ggped-pwg-plaus

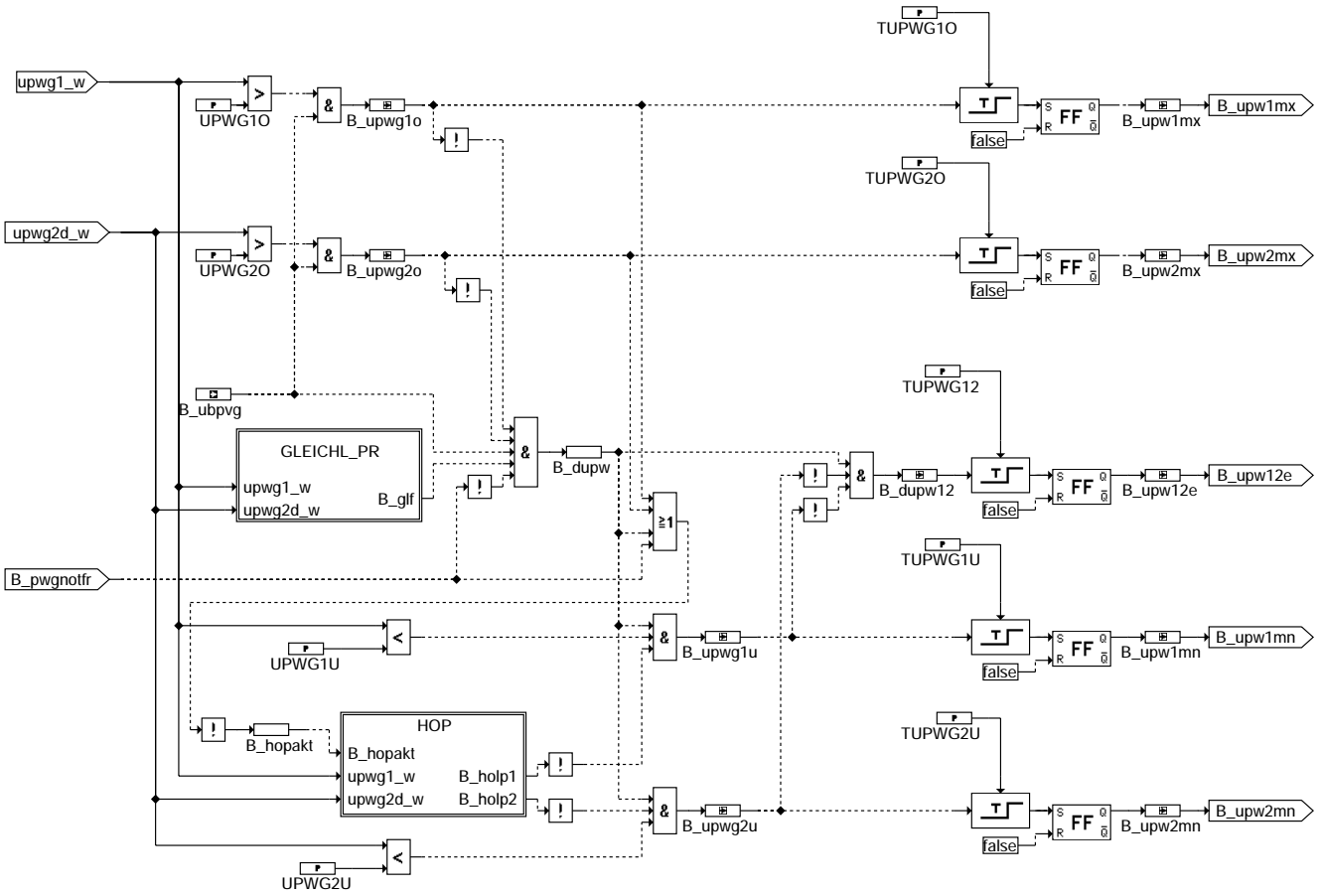
## FEHL\_BED: Generieren der Fehlerbedingungen



ggped-fehl-bed

ggped-fehl-bed

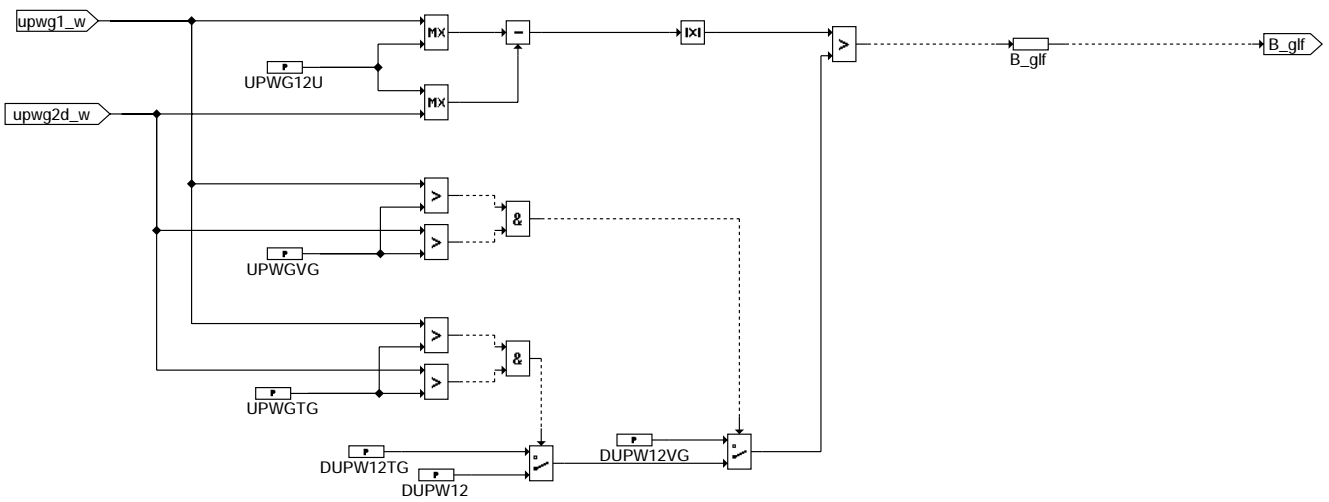
### Fehl\_Ausw: Fehlerauswertung



ggped-fehl-ausw

### ggped-fehl-ausw

#### GLEICHL\_PR: Gleichlaufprüfung

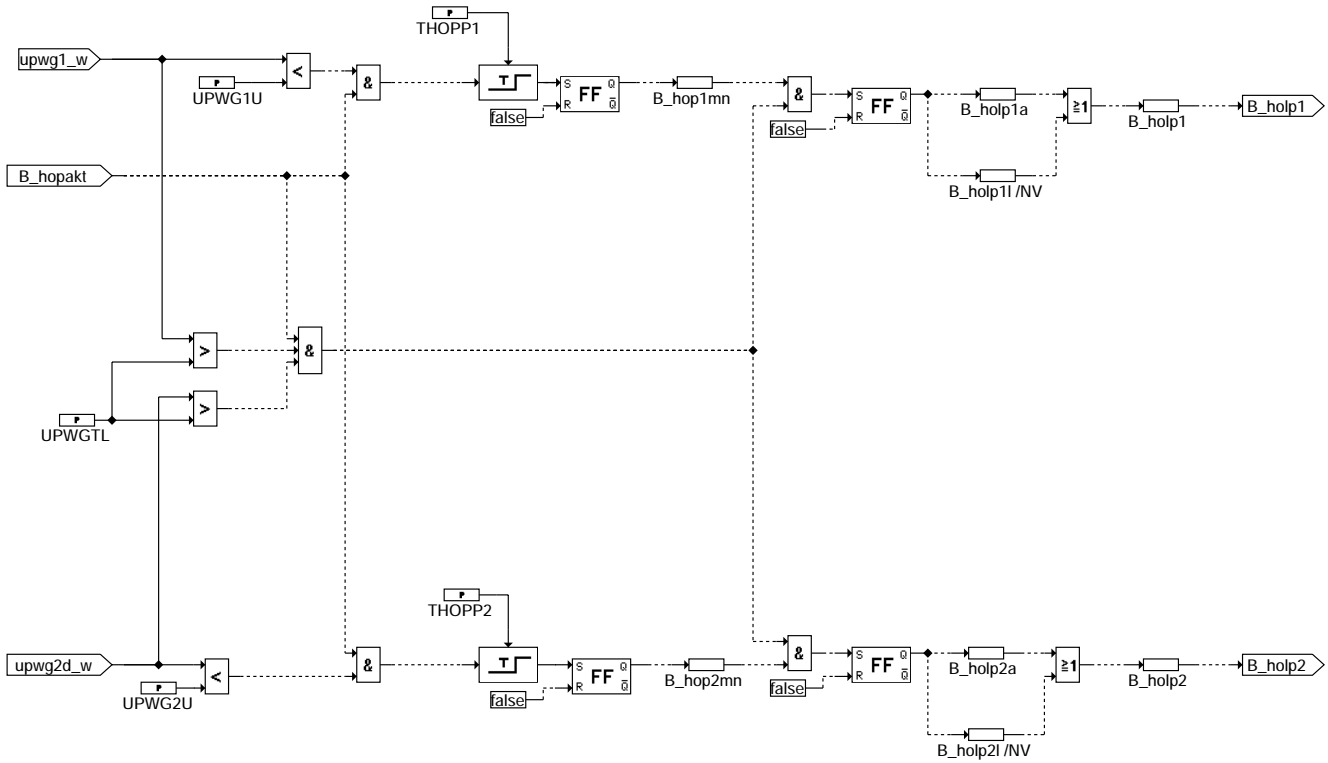


ggped-gleich-pr

### ggped-gleich-pr



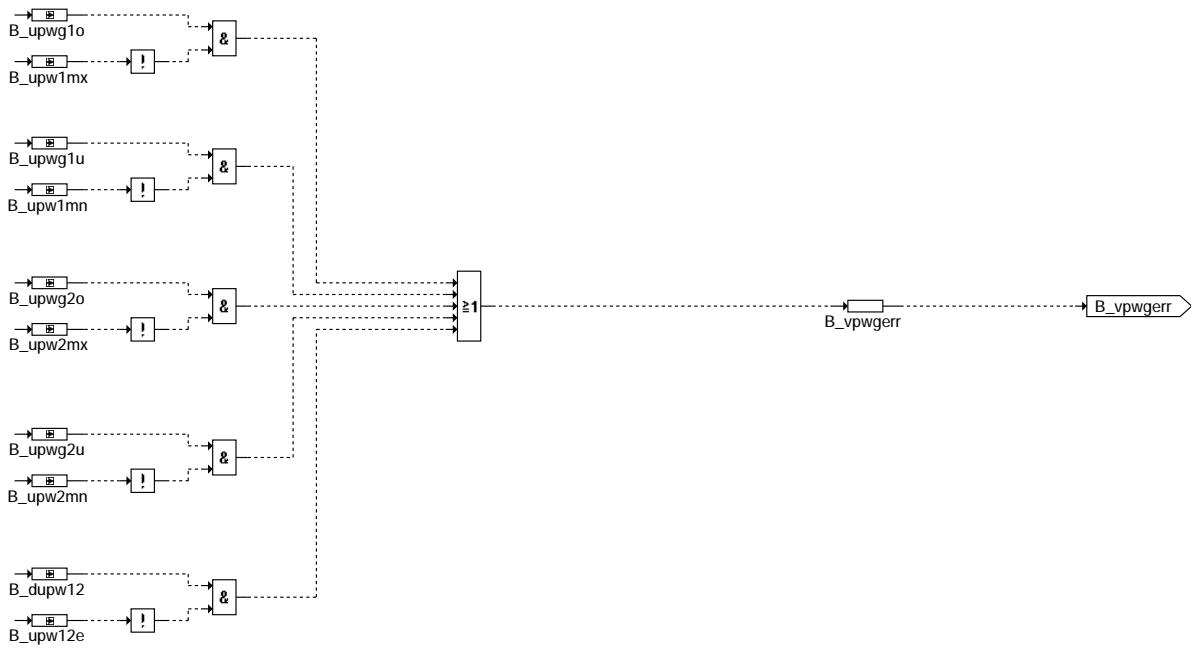
### HOP: Hochomigkeitsprüfung im Leerlauf



ggped-hop

### ggped-hop

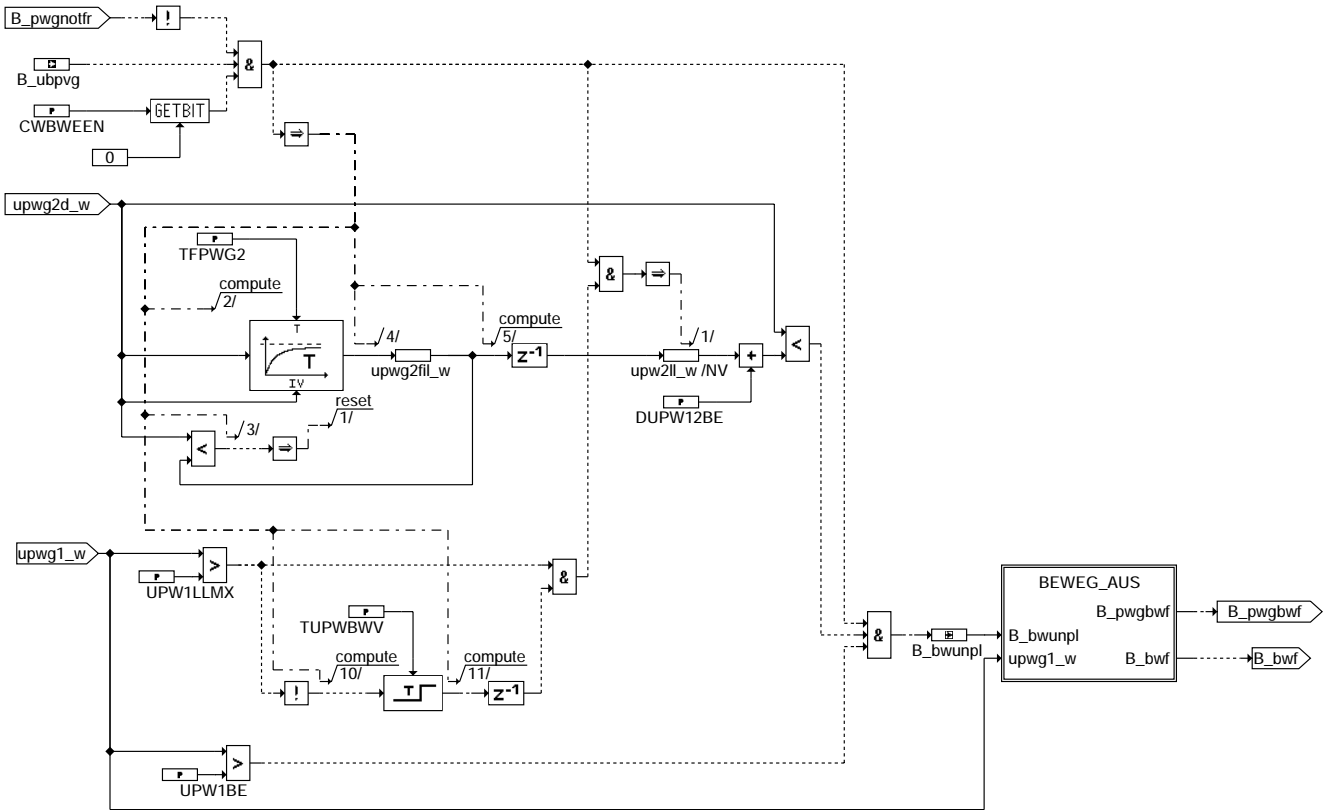
### ERR\_STATUS: Fehlerstatus bzgl. Verdacht auf PWG-Fehler



ggped-err-status

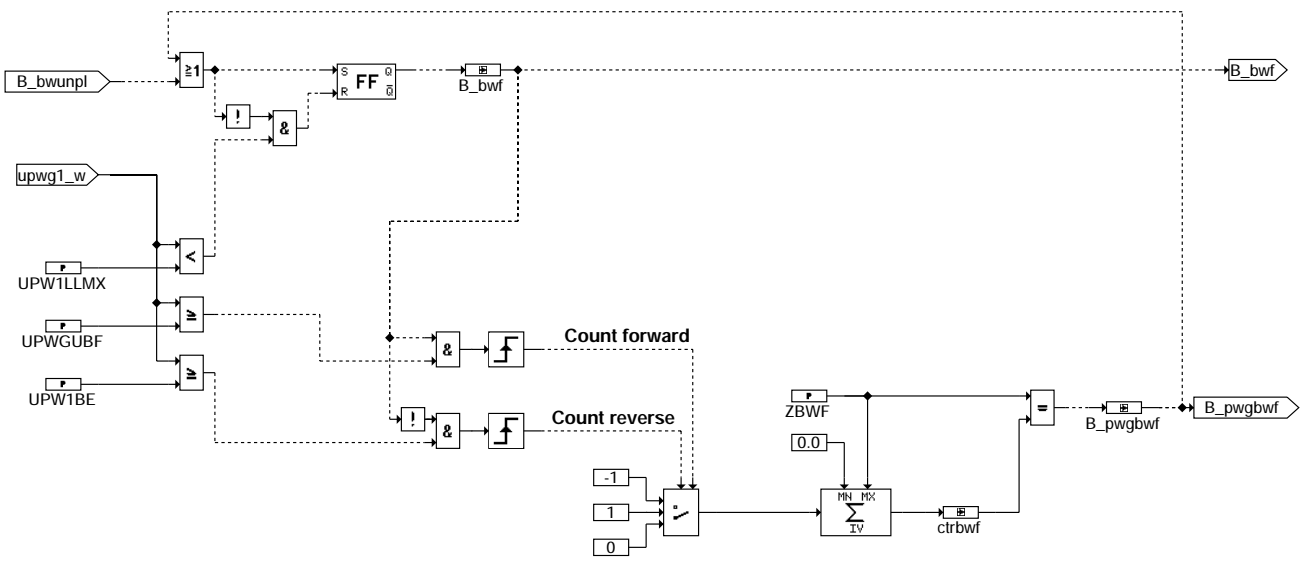
### ggped-err-status

## BEW\_ERK: Bewegungserkennung



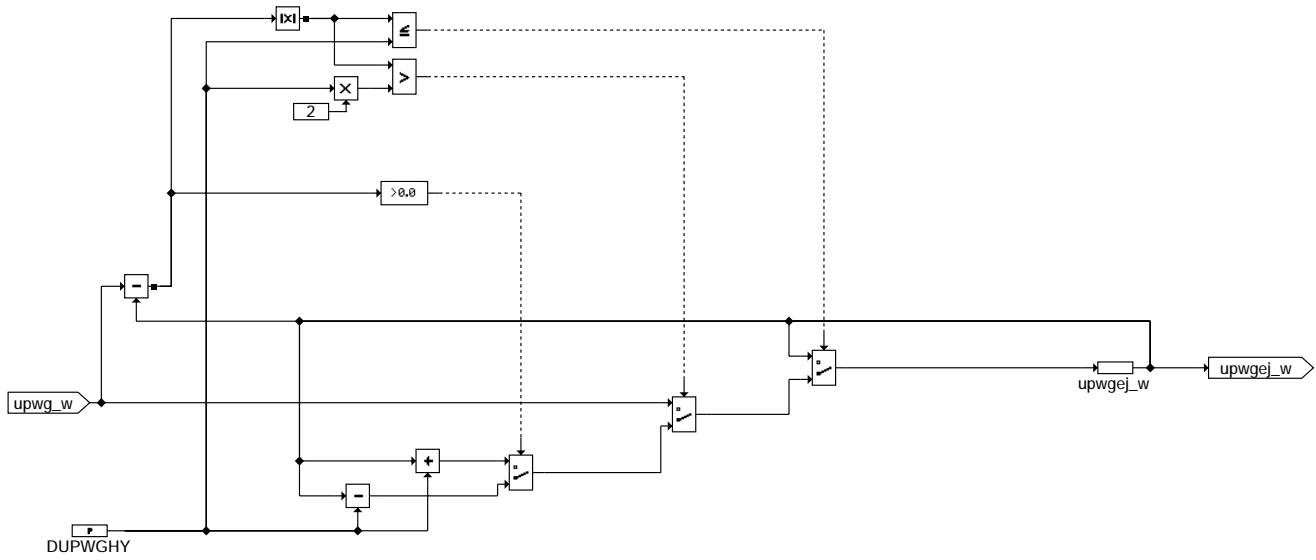
ggped-bew-erk

## BEWEG\_AUS: Auswertung der Bewegungserkennung



ggped-beweg-aus

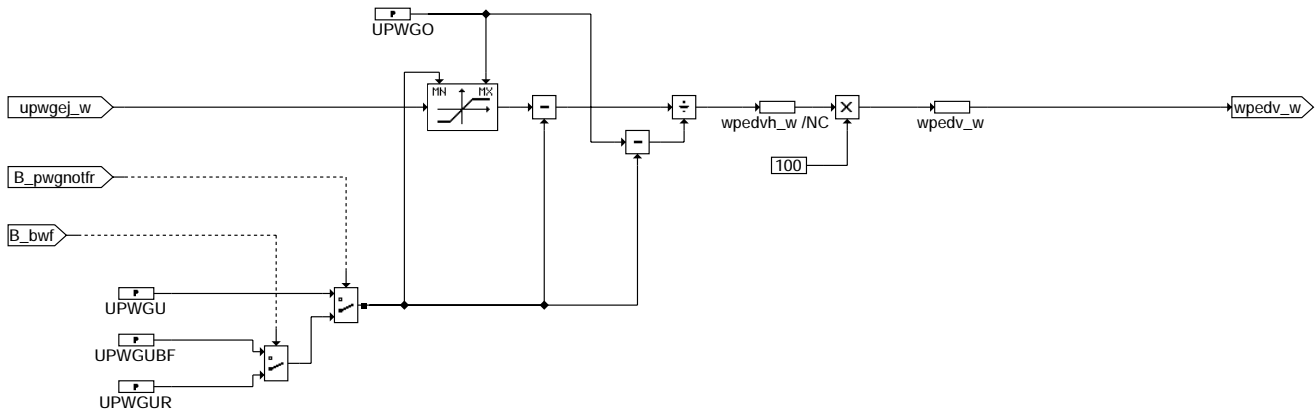
### ENTJIT: Entjitterung der PWG-Poti\_Spannung



ggped-entjit

ggped-entjit

### PED\_NORM: Umrechnung Potispannung in Pedalwert

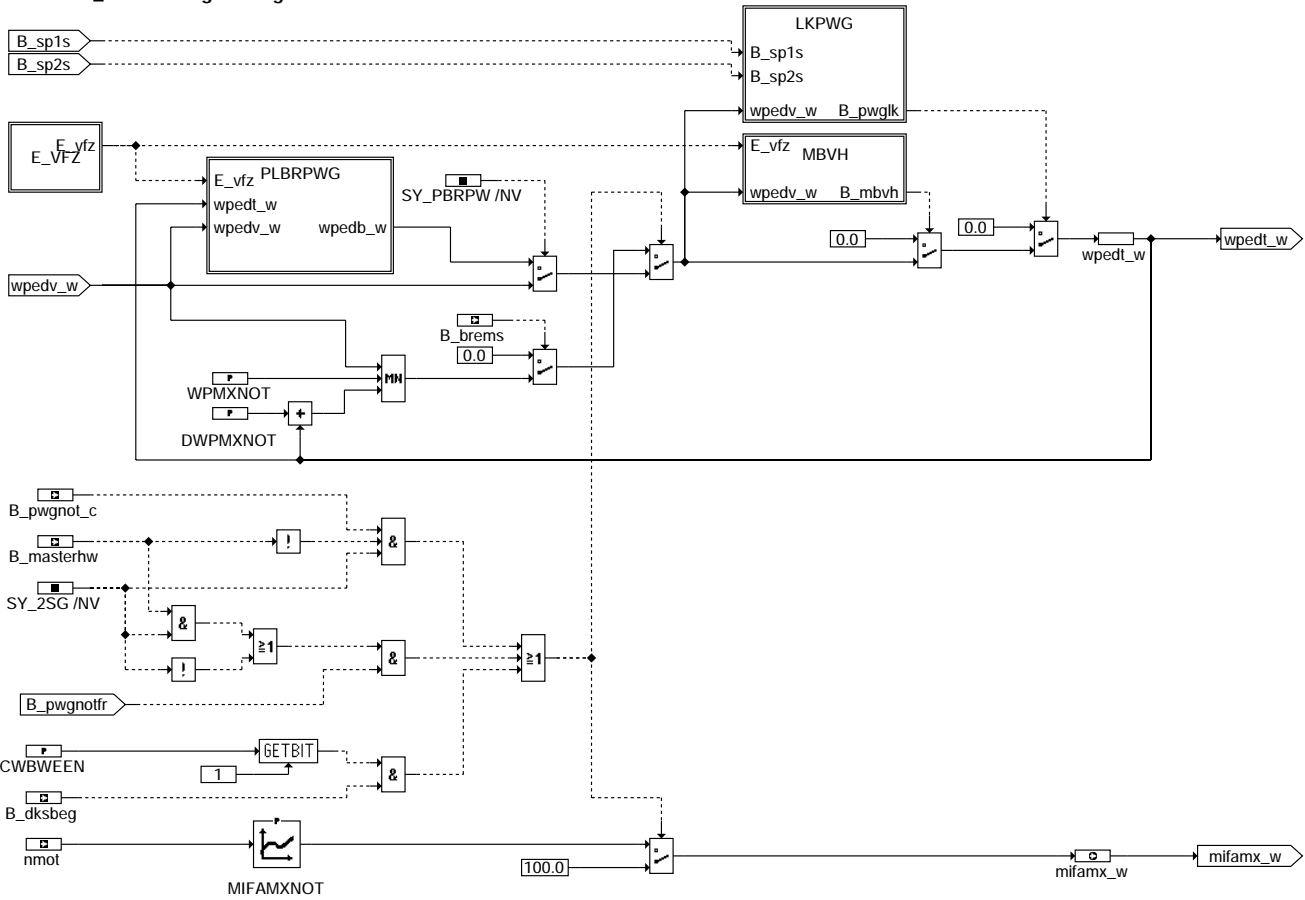


ggped-ped-norm

ggped-ped-norm



### PWG\_NOTFA: Begrenzung des Pedalwerts im PWG-Ersatzbetrieb

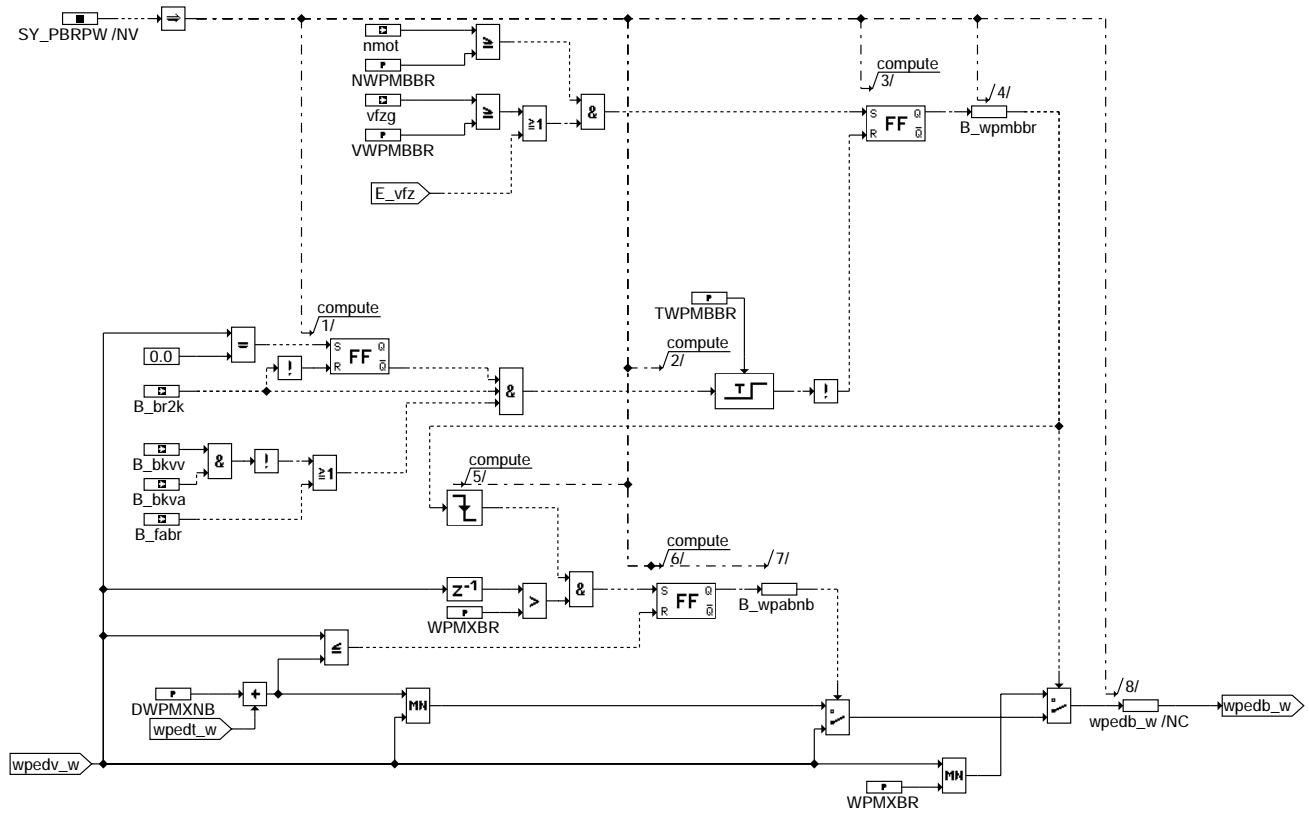


ggped-pwg-nofa

ggped-pwg-nofa

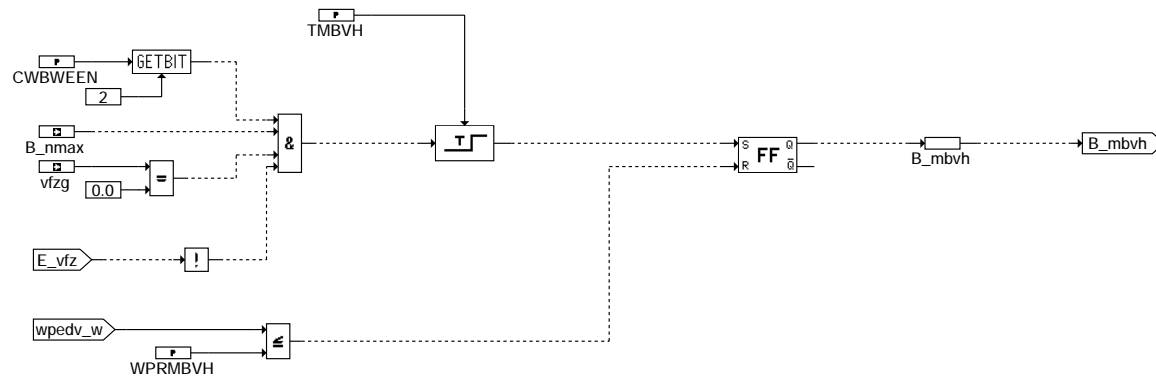


### PLBRPWG: Plausibilitätsprüfung Bremse/PWG



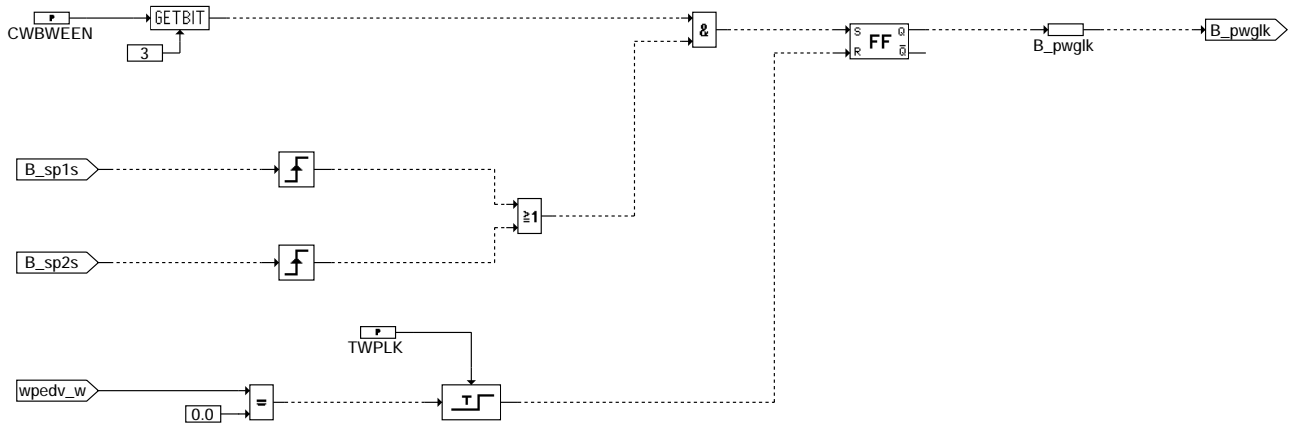
ggped-plbrpwg

### MBVH: Mißbrauchsverhinderung

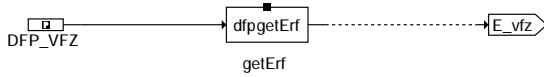


ggped-mbvh

### LKPWG: Lebenderkennung des PWG nach erkanntem Fehler

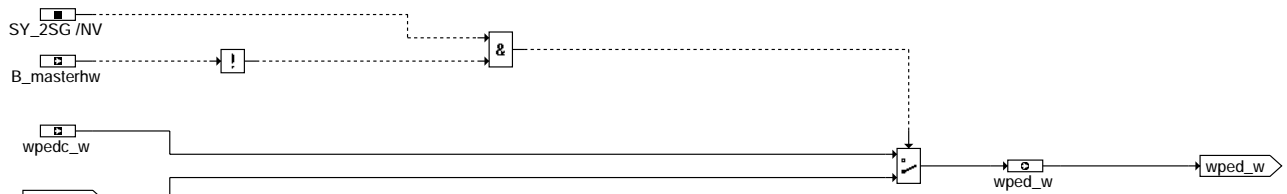


### ggped-lkpwg



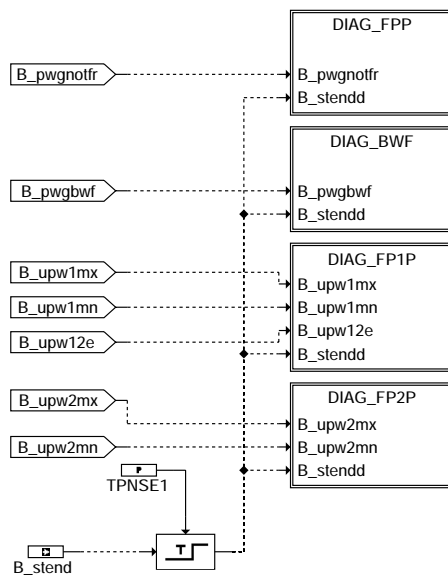
### ggped-e-vfz

### CAN\_2SG: Pedalwertübertragung über CAN mit Plausibilisierung für System mit 2 ME-Steuergeräten



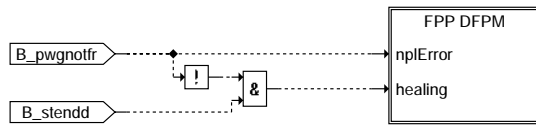
### ggped-can-2sg

### PWG\_DIAG: Diagnose für PWG



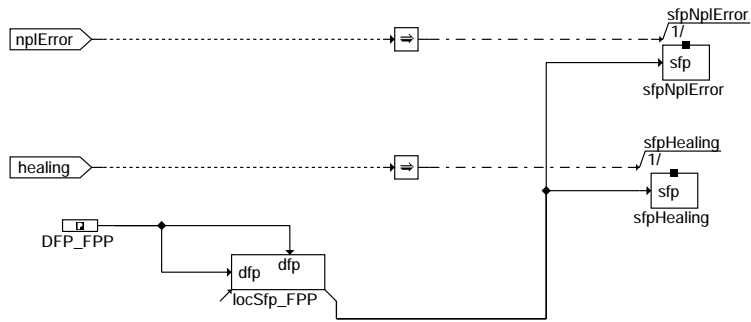
### ggped-pwg-diag

## DIAG\_FFP: Diagnose für PWG



ggped-diag-fpp

### FPP\_DFPM



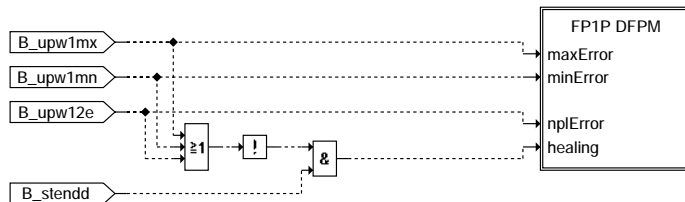
#### Action Table for fault path \* in DFPM:

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	S	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
nplError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

S: set R: reset

ggped-fpp-dfpm

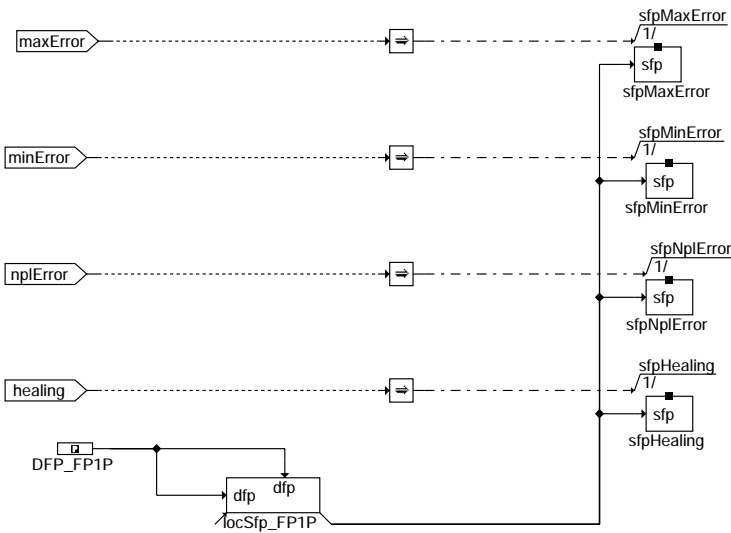
## DIAG\_FP1P: Diagnose für PWG-Poti 1



ggped-diag-fp1p



### FP1P\_DFPM



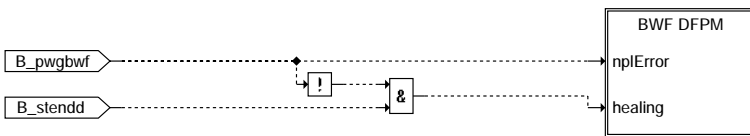
**Action Table for fault path \* in DFPM:**

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	R	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
nplError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

S: set R: reset

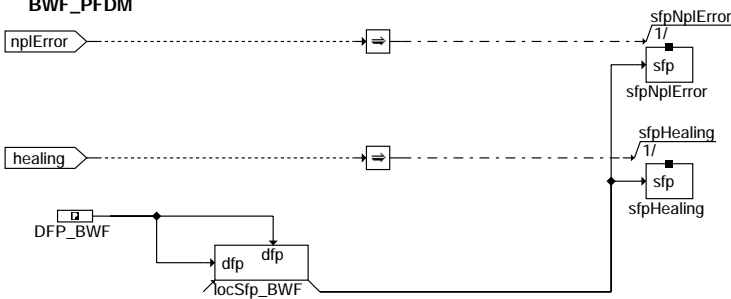
### ggped-fp1p-dfpm

#### DIAG\_BWF: Diagnose PWG-Bewegungserkennung



### ggped-diag-bwf

### BWF\_PFD



**Action Table for fault path \* in DFPM:**

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	S	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
nplError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

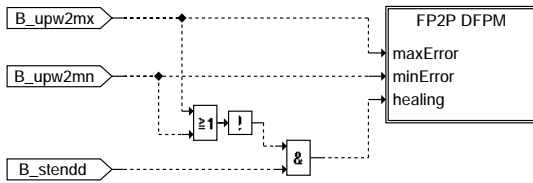
S: set R: reset

### ggped-bwf-dfpm



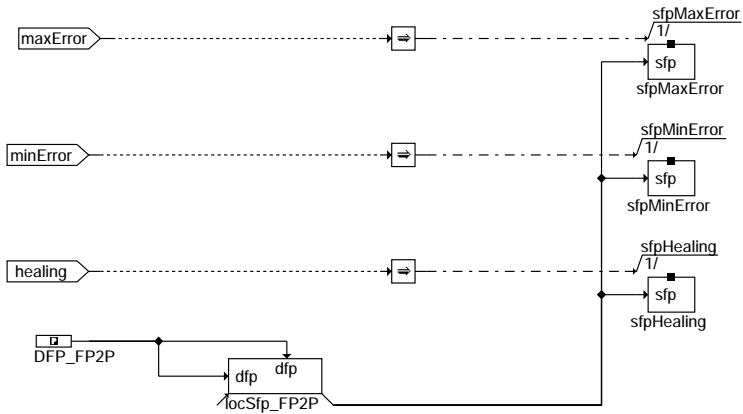


## DIAG\_FP2P: Diagnose für PWG-Poti 2



ggped-diag-fp2p

### FP2P\_DFPM



#### Action Table for fault path \* in DFPM:

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	S	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
nplError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

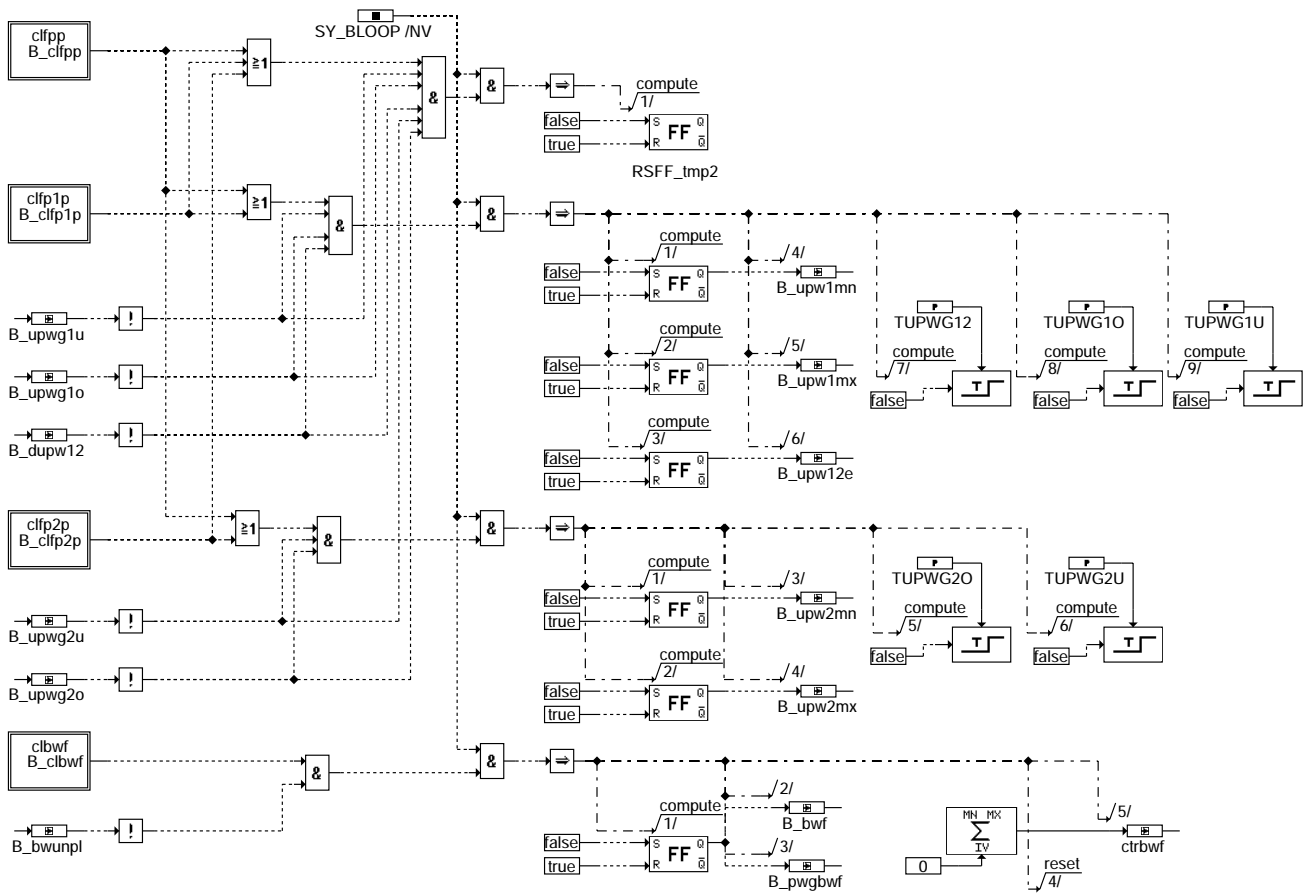
S: set R: reset

ggped-fp2p-dfpm

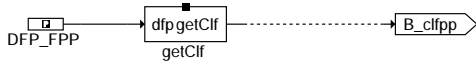
ggped-diag-fp2p

ggped-fp2p-dfpm

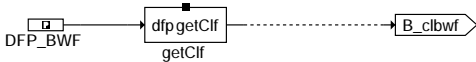
## FCMCLR



### ggped-fcmclr



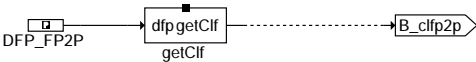
### ggped-clfp



### ggped-clbwf



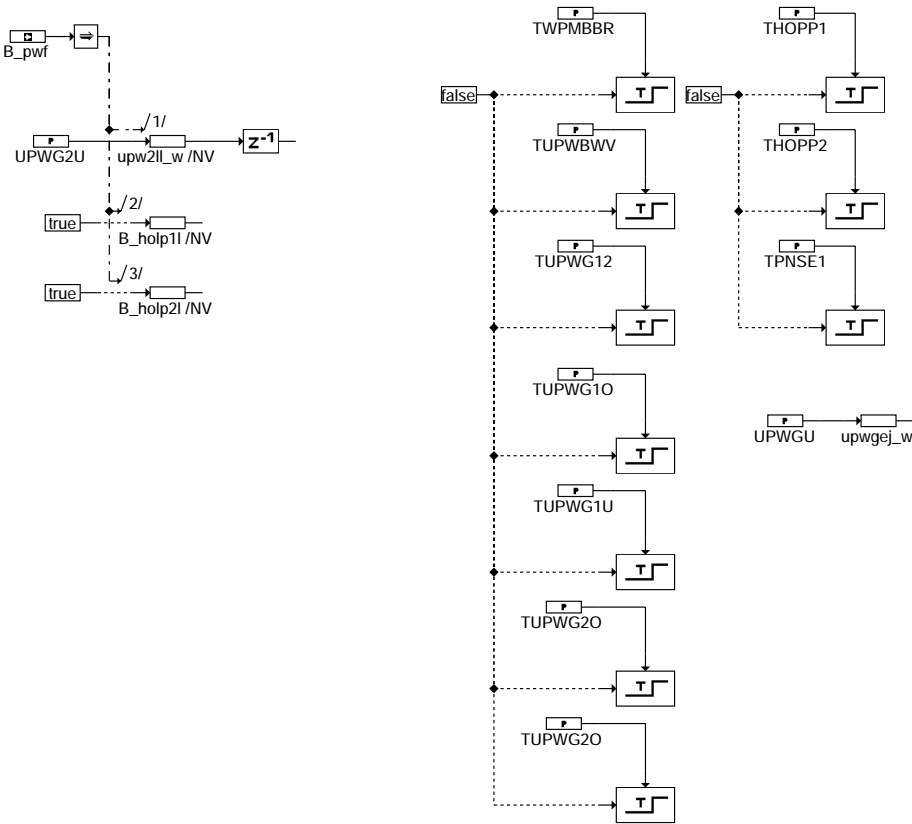
### ggped-clfp1p



### ggped-clfp2p



**Ini**



**ggped-initialize**

**ABK GGPED 8.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWBWEEN			FW	Code word for deactivation of movement detection
DUPW12			FW	Permissible voltage deviation between PWG potentiometer 1 and 2
DUPW12BE			FW	Necessary voltage path of poti 2 for the movement detection
DUPW12TG			FW	Permitted voltage deviation between PWG poti 1 and 2 during part. throttle range
DUPW12VG			FW	Permissible volt. deviation between PWG potentiometer 1 and 2 in full gas range
DUPWGHY			FW	Voltage hysteresis for dejittering the PWG voltage
DWPMXNB			FW	Max. permissible pedal value increase per computation step after operating brake
DWPMXNOT			FW	Max. permissible increase in pedal travel per calc. step in PWG standby mode
MIFAMXNOT	NMOT		KL	maximum indicated engine torque at limp home
NWPMBBR			FW	minimum speed for limiting pedal travel for operated brake
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_BLOOP			SYS (REF)	sys. con. resetting of irreversible EGAS fault possible during clearing of FCM
SY_PBRPW			SYS (REF)	system constant plausibility check brake/PWG
TFPWG2			FW	Filter time for filtering potentiometer 2 during movement detection
THOPP1			FW	Fault time for high resistance test potentiometer 1
THOPP2			FW	Fault time for high resistance test potentiometer 2
TMBVH			FW	Delay time for activation of misuse prevention
TPNSE1			FW	Test time after start end for PWG diagnostic routine
TUPWBWV			FW	Time delay for storing a new potentiometer-2 value
TUPWG12			FW	Fault time during comparison of PWG potentiometer 1 and 2
TUPWG10			FW	Fault time for upper violation of range by PWG potentiometer 1
TUPWG1U			FW	Fault time for lower violation of range by PWG potentiometer 1
TUPWG20			FW	Fault time for upper violation of range by PWG potentiometer 2
TUPWG2U			FW	Fault time for lower violation of range by PWG potentiometer 2
TWPLK			FW	debouncing time for withdrawal of the idle input at life detection
TWPMBBR			FW	Delay time for limiting pedal travel for operated brake
UPW1BE			FW	Voltage PWG potentiometer 1 for executing movement detection
UPW1LLMX			FW	Maximum voltage of potentiometer 1 at no-throttle point
UPWG12U			FW	Lower limit for PWG potentiometer volt. before comparison potentiometer 1 and 2
UPWG10			FW	Upper barrier for PWG potentiometer-1 voltage
UPWG1U			FW	Lower barrier for PWG potentiometer-1 voltage
UPWG20			FW	Upper barrier for PWG potentiometer-2 voltage
UPWG2U			FW	Lower barrier for PWG potentiometer-2 voltage
UPWGO			FW	Upper PWG voltage value for re-scaling to pedal value
UPWGTG			FW	PWG voltage threshold for partial throttle range
UPWGTL			FW	Partial load threshold of the PWG voltage in high resistance testing



Parameter	Source-X	Source-Y	Type	Description
UPWGU			FW	Lower PWG voltage value for re-scaling to standard value
UPWGUBF			FW	Lower voltage value for the re-scaling for detected movement fault
UPWGUR			FW	Reduced lower PWG voltage value for re-scaling to pedal value
UPWGVG			FW	PWG voltage threshold for full-throttle range
VWPMBBR			FW	minimum speed for limiting pedal travel for operated brake
WPMXBR			FW	Maximum permissible pedal value for actuated brake (prior to detection of wped=0)
WPMXNOT			FW	Max. permissible pedal travel in PWG limp-home
WPRMBVH			FW	pedal angle for deactivation of misuse protection
ZBWF			FW	Counter status for movement-detection fault entry

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B.BEBWF	GGPED	AUS	Condition function request for motion control of pedal
B.BEFP1P	GGPED	AUS	Condition function request for error poti1 of pedal
B.BEFP2P	GGPED	AUS	Condition function request for error poti2 of pedal
B.BEFP	GGPED	AUS	Condition function request for error of pedal
B.BKBWF	GGPED	AUS	Flag for default value: pedal moving detection
B.BKFP1P	GGPED	AUS	Condition: Pedal 1.potentiometer active
B.BKFP2P	GGPED	AUS	Condition: Pedal 2.potentiometer active
B.BKFP	GGPED	AUS	Condition: drive pedal potentiometer active
B.BKVA		EIN	condition BKV triggered
B.BKV		EIN	condition BKV installed (for evaluating brakes)
B.BR2K	GGEGAS	EIN	Condition brakes actuated 2-channel detection
B.BREMS	GGEGAS	EIN	condition: brake operated
B.BWF	GGPED	LOK	Condition: movement detection has detected fault
B.BWUNPL	GGPED	LOK	Condition non-plausibility during movement detection
B.CLBWF		EIN	Flag for clearance: pedal moving detection
B.CLFP1P		EIN	Flag for clearing measures: accelerator pedal potentiometer 1
B.CLFP2P		EIN	Flag for clearing measures: accelerator pedal potentiometer 2
B.CLFP		EIN	Delete condition fault path FPP (drive pedal potentiometer)
B.DKSBE	GGDVE	EIN	condition: limiting throttle-valve setpoint value
B.DUPW	GGPED	LOK	Condition deviation between potentiometer 1 and 2 too large
B.DUPW12	GGPED	LOK	Condition permissible deviation between PWG potentiometers 1 and 2 exceeded
B.FABR		EIN	condition driver brakes because of CAN message
B.FTBWF	GGPED	AUS	Condition fault entry by tester for motion control of pedal
B.FTFP1P	GGPED	AUS	Condition fault entry by tester for poti1 of pedal
B.FTFP2P	GGPED	AUS	Condition fault entry by tester for poti2 of pedal
B.FTFP	GGPED	AUS	Condition fault entry by tester for pedal
B.GLF	GGPED	LOK	Condition synchronization between potentiometers 1 and 2 violated
B.HOLP1	GGPED	LOK	Condition high resistance in idling at PWG potentiometer 1 detected
B.HOLP1A	GGPED	LOK	Cond. high resistance in idling at PWG potentiometer 1 in current drive cycle
B.HOLP1L	GGPED	LOK	Cond. high resistance in idling at PWG potentiometer 1 in previous drive cycle
B.HOLP2	GGPED	LOK	Condition high resistance in idling at PWG potentiometer 2 detected
B.HOLP2A	GGPED	LOK	Cond. high resistance in idling at PWG potentiometer 2 in current drive cycle
B.HOLP2L	GGPED	LOK	Cond. high resistance in idling at PWG potentiometer 2 in previous drive cycle
B.HOP1MN	GGPED	LOK	Condition lower violation of range at potentiometer 1 in high resistance testing
B.HOP2MN	GGPED	LOK	Condition lower violation of range at potentiometer 2 in high resistance testing
B.HOPAKT	GGPED	LOK	Condition high resistance testing active
B.MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)
B.MBVH	GGPED	LOK	condition abuse prevention
B.MNBWF	GGPED	AUS	Fault type min.: pedal moving detection
B.MNFP1P	GGPED	AUS	Fault type min.: accelerator pedal potentiometer 1
B.MNFP2P	GGPED	AUS	Fault type min.: Pedal 2. poti
B.MNFPP	GGPED	AUS	Fault type min.: drive pedal potentiometer
B.MXBWF	GGPED	AUS	Fault type max.: pedal moving detection
B.MXFP1P	GGPED	AUS	Fault type max.: Pedal 1. poti
B.MXFP2P	GGPED	AUS	Fault type max.: Pedal 2. poti
B.MXFPP	GGPED	AUS	Fault type max.: drive pedal potentiometer
B.NMAX	NMAXMD	EIN	1 = maximum engine speed exceeded
B.NPBWF	GGPED	AUS	Fault type not plausible: movement by pedal-travel sensor
B.NPFP1P	GGPED	AUS	Fault type not plausible: accelerator pedal potentiometer 1
B.NPFP2P	GGPED	AUS	Fault type unplaus.: Pedal 2. poti
B.NPFP	GGPED	AUS	Condition potentiometer signals from drive pedal not plausible
B.PWF		EIN	Condition for powerfail
B.PWGBWF	GGPED	LOK	Condition pedal-travel sensor movement fault
B.PWGLK	GGPED	LOK	condition life detection PWG
B.PWGNOTFR	GGPED	AUS	FR error reaction pedal-travel sensor limphome
B.PWGNOTUM	URADCC	EIN	= b.pwgnotLum function monitoring fault response PWG idling (= b.pwgnot_sr)
B.PWGNOT.C		EIN	condition: info PWG limp-home via CAN
B.SIBWF	GGPED	AUS	Fault type sig.: pedal moving detection
B.SIFP1P	GGPED	AUS	error type: Pedal 1.potentiometer
B.SIFP2P	GGPED	AUS	error type: Pedal 2.potentiometer
B.SIFPP	GGPED	AUS	error type: drive pedal potentiometer
B.SP1S	GGPED	AUS	message to SR: SP1S is command variable
B.SP2S	GGPED	AUS	SP2S is valid set value for PWG failure driving
B.SPSMIN	GGPED	AUS	message to SR: '1' = pedal-travel sensor limphome with SPSMIN
B.STEND	BBSTT	EIN	condition end of start
B.UBPVG	ADVE	EIN	condition: battery voltage sufficient for 5-V potentiometer supply
B.UPW12E	GGPED	LOK	Cond.: Fault during comparison of both standardized PWG potentiometer voltages
B.UPW1MN	GGPED	LOK	Condition: Voltage PWG potentiometer 1 below minimum value
B.UPW1MX	GGPED	LOK	Condition: Voltage PWG potentiometer 1 above maximum value



Variable	Source	Type	Description
B_JPW2MN	GGPED	LOK	Condition: Voltage PWG potentiometer 2 below minimum value
B_JPW2MX	GGPED	LOK	Condition: Voltage PWG potentiometer 2 above maximum value
B_JPWG1O	GGPED	LOK	Condition upper violation of range at PWG potentiometer 1
B_JPWG1U	GGPED	LOK	Condition lower violation of range at PWG potentiometer 1
B_JPWG2O	GGPED	LOK	Condition upper violation of range at PWG potentiometer 2
B_JPWG2U	GGPED	LOK	Condition lower violation of range at PWG potentiometer 2
B_VPWGERR	GGPED	LOK	Condition: suspicion on error at pedal-travel sensor
B_WPABNB	GGPED	LOK	condition limit chage in pedal-travel value after brake actuation
B_WPMBBR	GGPED	LOK	condition: max. limiting of pedal-sensor value for brake actuation
CTRBWF	GGPED	LOK	Fault counter movement detection
DFP_BWF	GGPED	DOK	ECU int. fault path no. pedal moving detection
DFP_FP1P	GGPED	DOK	ECU int. fault path no.: pedal 1. potentiometer
DFP_FP2P	GGPED	DOK	ECU int. fault path no.: pedal 2. potentiometer
DFP_FPP	GGPED	DOK	ECU int. fault path no.: pedal potentiometer
DFP_VFZ	GGPED	DOK	ECU int. fault path no.: vehicle speed signal
DWPED	GGPED	AUS	gradient of the standardized accelerator pedal angle
DWPED_W	GGPED	AUS	gradient of the standardized accelerator pedal angle
E_BWF	GGPED	AUS	Error flag: pedal moving detection
E_FP1P	GGPED	AUS	Error flag: accelerator pedal potentiometer 1
E_FP2P	GGPED	AUS	Error flag: accelerator pedal potentiometer 2
E_FPP	GGPED	AUS	Error flag drive pedal potentiometer
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
MIFAMX_W	GGPED	AUS	maximum indicated engine torque at limp home
NMOT	SWADAP	EIN	engine speed
SFPBWF	GGPED	AUS	Status word: pedal moving detection
SFPFP1P	GGPED	AUS	status fault path: pedal 1. potentiometer
SFPFP2P	GGPED	AUS	status fault path: pedal 2. potentiometer
SFPFPP	GGPED	AUS	status fault path: pedal potentiometer
UPW2LL_W	GGPED	LOK	Value for voltage from pedal-travel sensor potentiometer 2 before movement
UPWG1_W		EIN	Voltage PWG potentiometer 1 (word)
UPWG2D_W	GGPED	LOK	Doubled PWG potentiometer-2 voltage (word)
UPWG2FIL_W	GGPED	LOK	Filtered potentiometer 2 voltage
UPWG2_W		EIN	Voltage PWG potentiometer 2 (word)
UPWGEJ_W	GGPED	LOK	De-jittered PWG potentiometer voltage
UPWG_W	GGPED	LOK	Resulting PWG potentiometer voltage following plausibility check
VFZG	SWADAP	EIN	vehicle speed (km/h)
WPED	GGPED	AUS	Standardized accelerator pedal angle
WPEDC_W		EIN	pedal value for 2 ME ECU's (from CAN)
WPEDT_W	GGPED	LOK	Pedal value (temporary) for 2 ME ECU's
WPEDV_W	GGPED	LOK	Standardized drive pedal angle prior to allowance for limiting in standby drive
WPED_W	GGPED	AUS	normed angle acceleration pedal
Z_BWF	GGPED	AUS	Cycle flag: pedal moving detection
Z_FP1P	GGPED	AUS	Cycle flag: Pedal 1. poti
Z_FP2P	GGPED	AUS	Cycle flag: Pedal 2. poti
Z_FPP	GGPED	AUS	Cycle flag drive pedal potentiometer

## FW GGPED 8.30 Fixed Values

Parameter	Value	Description
CWBWEEN		Code word for deactivation of movement detection
DUPW12		Permissible voltage deviation between PWG potentiometer 1 and 2
DUPW12BE		Necessary voltage path of poti 2 for the movement detection
DUPW12TG		Permitted voltage deviation between PWG poti 1 and 2 during part. throttle range
DUPW12VG		Permissible volt. deviation between PWG potentiometer 1 and 2 in full gas range
DUPWGHY		Voltage hysteresis for dejittering the PWG voltage
DWPMXNB		Max. permissible pedal value increase per computation step after operating brake
DWPMXNOT		Max. permissible increase in pedal travel per calc. step in PWG standby mode
NWPMBBR		minimum speed for limiting pedal travel for operated brake
TFPWG2		Filter time for filtering potentiometer 2 during movement detection
THOPP1		Fault time for high resistance test potentiometer 1
THOPP2		Fault time for high resistance test potentiometer 2
TMBVH		Delay time for activation of misuse prevention
TPNSE1		Test time after start end for PWG diagnostic routine
TUPWBWV		Time delay for storing a new potentiometer-2 value
TUPWG12		Fault time during comparison of PWG potentiometer 1 and 2
TUPWG1O		Fault time for upper violation of range by PWG potentiometer 1
TUPWG1U		Fault time for lower violation of range by PWG potentiometer 1
TUPWG2O		Fault time for upper violation of range by PWG potentiometer 2
TUPWG2U		Fault time for lower violation of range by PWG potentiometer 2
TWPLK		debouncing time for withdrawal of the idle input at life detection
TWPMBBR		Delay time for limiting pedal travel for operated brake
UPW1BE		Voltage PWG potentiometer 1 for executing movement detection
UPW1LLMX		Maximum voltage of potentiometer 1 at no-throttle point
UPWG12U		Lower limit for PWG potentiometer volt. before comparison potentiometer 1 and 2
UPWG1O		Upper barrier for PWG potentiometer-1 voltage
UPWG1U		Lower barrier for PWG potentiometer-1 voltage
UPWG2O		Upper barrier for PWG potentiometer-2 voltage
UPWG2U		Lower barrier for PWG potentiometer-2 voltage
UPWGO		Upper PWG voltage value for re-scaling to pedal value
UPWGTG		PWG voltage threshold for partial throttle range
UPWGTL		Partial load threshold of the PWG voltage in high resistance testing



Parameter	Value	Description
UPWGU		Lower PWG voltage value for re-scaling to standard value
UPWGUBF		Lower voltage value for the re-scaling for detected movement fault
UPWGUR		Reduced lower PWG voltage value for re-scaling to pedal value
UPWGVG		PWG voltage threshold for full-throttle range
VWPMBBR		minimum speed for limiting pedal travel for operated brake
WPMXBR		Maximum permissible pedal value for actuated brake (prior to detection of wped=0)
WPMXNOT		Max. permissible pedal travel in PWG limp-home
WPRMBVH		pedal angle for deactivation of misuse protection
ZBWF		Counter status for movement-detection fault entry

## FB GGPED 8.30 Detailed description of function

The function calculates the standardized accelerator angle wped from the poti voltage of the pedal sensor (PWG). The PWG has two potentiometers, which are independently supplied with 5V from the control unit. Poti 2 possesses an additional resistor of the size of the track resistor, so that its characteristic displays only half the gradient as compared to that of poti 1. By various plausibility checks (voltage range, synchronization etc.) it is ensured that due to a single fault wped cannot take on higher values than correspond to the accelerator position. In addition to the component monitoring for the PWG realized here, further parts of the PWG monitoring are contained in the functions %UFSPSC (watchdog function for %GGPED) and %URADCC (watchdog function of the A/D-converter).

Apart from wped further variables are made available:

- o The pedal value gradient dwped,
- o if needed, several fault code memory entries (FP1P, FP2P, FPP, BWF) as well as
- o information on the PWG limp-home operation (B\_pwgnotfr, B\_spsmin, B\_spls, B\_sp2s) for the watchdog function.

The function is also suitable for use in a system with 2 ME control units (SY\_2SG = 1), in which the PWG evaluation and monitoring is performed entirely in the master ECU and in which the pedal value wped is transferred to the slave ECU via CAN.

PWG\_PLAUS  
=====

Dependent on the result of the plausibility check the resulting poti voltage upwg is selected, which is thereafter used for the calculation of the pedal value. During normal operation (B\_pwgnotfr = 0, B\_spsmin = 0) upwg1, the signal of poti 1, is used for the calculation of the pedal value. With undervoltage (B\_ubpv = 0), with a fault detection in the watchdog function (B\_pwgnotum = 1) and with a range violation of the remaining poti during PWG limp-home operation, upwg is set to the smallest possible lower standard limit UPWGUR (s. partial function PED\_NORM), which leads to wped = 0. In case of a range violation of poti 1, upwg is set to upwg2d, the signal of poti 2. Inversely, upwg is set to upwg1 in case of a range violation of poti 2. With a synchronization fault (B\_upw12e = 1) upwg equals the minimum of poti 1 and poti 2.

FEHL\_BED  
=====

From the individual fault conditions, which indicate upper or lower range violations for both potis and synchro faults, the conditions for the selection of the resulting poti voltage upwg are generated. B\_pwgnotfr is set if a range violation or a synchro fault is detected. B\_spsmin is set in case of undervoltage, with a fault detected in the watchdog function as well as in case of range violation of both potis and in case of a range violation of the used poti after a synchro fault. B\_spls is set if a range violation of poti 2 but no range violation of poti 1 is given. Analogous B\_sp2s is set, if a range violation of poti 1 but no range violation of poti 2 is given.

FEHL\_AUSW  
=====

The calculation of the fault conditions is only active if there is sufficient battery voltage to supply the potis (B\_ubpv = 1). All fault conditions are only set once the respective fault tolerance time has elapsed, then, however, they remain set for the entire current driving cycle. At first an upper range check is performed for upwg1 and upwg2d. If necessary B\_upw1mx or B\_upw2mx is set. If no fault arises during the upper range check the synchro check is performed during normal operation (see partial function GLEICHL\_PR). If in the process a fault is detected a lower range check of both potis takes place. If no non-plausibility resulted in the process or if in the current or the previous driving cycle a high-resistance during idle was detected, B\_upw12e is set. Otherwise the fault condition for the lower range violation (B\_upw1mn or B\_upw2mn) is set. If no upper range violation and no synchro fault is given the high-resistance check at idle is performed during normal operation (see partial function HOP). The concerned irreversible fault bits and the accompanying fault counters are cleared when the fault code memory is cleared. Clearing of a fault bit is only possible, if the fault that has triggered it, is actually not given any longer, i.e. the function no longer detects the fault. Resetting of the irreversible fault bits is only allowed, if SY\_BLOOP = 1 has been set.

GLEICHL\_PR  
=====

During the synchro check of the two potis the deviation of upwg1 and upwg2d is compared with the synchro tolerance. If the deviation is large, B\_glf is set. After the specification of the PWG very large transition resistance can occur in the idle range. For this reason, upwg1 and upwg2d are low-limited to UPWG12U prior to the calculation of the deviation. A transition resistance at idle thus does not lead to a synchro fault. Since possible transition resistance may have varying effects in



different ranges of the poti track the synchro tolerance is switched dependent on the range between DUPW12 (idle), DUPW12TG (partial throttle) and DUPW12VG (full throttle).

**ERR\_STATUS**  
=====

Updating of the determined pedal value is only performed, if no fault is suspected. That means, during fault debouncing always the last valid pedal value is maintained. Only once the fault check has been terminated with selection of the remaining sensor signal or when a fault is no longer suspected, is the pedal value updated again.

**HOP**  
===

The high-resistance check at idle serves to increase the availability when the signal lead of a poti is disconnected. With synchro fault and detected lower range violation of this poti it is possible to use - instead of the minimum of both potis, which would permanently lead to  $wped = 0$  - the other poti for the calculation of the pedal value, provided no high-resistance was detected in the current and in the previous driving cycle.

The high-resistance check is only performed during normal operation if neither an upper range violation nor a synchro fault is given. Should a poti in this state show a lower range violation for a certain time, this is stored (B\_hop1mn or B\_hop2mn). If both potis again exceed the threshold UPWGTL in the same driving cycle, high-resistance at idle is stored for the concerned poti (B\_hop1a or B\_hop2a). The two bits are stored in the non-volatile memory for the use in the next driving cycle.

**BEW\_ERK**  
=====

The movement detection ensures that a safety-relevant power increase of the engine will only take place if the two potis have moved away from their idle position. A slight drift of poti 1, which cannot be detected by the synchro check is thereby intercepted. The movement detection is only executed during normal operation with sufficient poti voltage supply and it can be deactivated via the code word CWBWEEN.

If poti 1 exits the idle range, after it was there for the time TUPWBWV beforehand, then the latest value of poti 2 is stored. The time condition is important so that in case of short-termed interference no erroneous storage will be performed. The signal of poti 2 is filtered at upward movement, so that in case of short-termed interference no too high value of poti 2 will be stored. If poti 1 exceeds the threshold UPW1BE, poti 2 must have moved by at least DUPW12BE as compared to the stored value upw211. Otherwise B\_bwunpl is set.

**BEWEG\_AUS**  
=====

If a non-plausibility was detected during the movement detection (B\_bwunpl = 1), the lower standard limit is switched to UPWGUBF in the partial function PED\_NORM by the setting of B\_bwf. UPWGUBF lies so high that when it is exceeded a synchro fault occurs. In case of a drifting poti 1,  $wped$  remains at zero until the synchro check responds. B\_bwf is reset when poti 1 undershoots the threshold UPW1LLMX.

If the accelerator is operated while B\_bwf is set, so that poti 1 exceeds the threshold UPWGUBF, the fault counter ctrbwf is incremented. ctrbwf is decremented, if B\_bwf was reset and thereafter by operating the accelerator poti 1 exceeds the threshold UPW1BE. B\_pwgbwf is set if the fault counter ctrbwf reaches the value ZBWF, and a fault code memory entry is performed (see partial function DIAG\_BWF). When the fault code memory is cleared (fault path BWF), B\_bwf is set to false and ctrbwf to zero. Clearing of a fault bit is only possible, if the fault that has triggered it, is actually not given any longer, i.e. the function no longer detects the fault.

**ENTJIT**  
=====

So as to avoid a jittering of the pedal value especially with aged PWG the resulting poti voltage upwg is smoothed as follows: If the new value does not deviate by more than DUPWGHY from the old value then the old value is maintained. If the deviation from the old value lies between DUPWGHY and  $2 * DUPWGHY$ , the new de-jittered value results by an increase resp. decrease of the old value by DUPWGHY. Only once a deviation of more than  $2 * DUPWGHY$  is given is the new value accepted without filtering.

**PED\_NORM**  
=====

For the conversion of the de-jittered poti voltage to a temporary pedal value the voltage range between lower and upper standard limit is linearly imaged to the range 0 to 100%. The upper standard limit is UPWGO. As lower standard limit UPWGUR, the maximum possible voltage value of poti 1 at idle, is used during normal operation. During PWG limp-home operation UPWGU is used, the maximum possible voltage value of poti 2 at idle. With detected movement fault during normal operation standardization is only



performed as of UPWGUBF, which lies higher by the value of the synchro tolerance than UPWGU resp. higher by twice the synchro tolerance than UPWGUR.

PWG\_NOTFA  
=====

During PWG and throttle sensor limp-home operation the pedal value is immediately set to zero when the brake is applied (B\_brems = 1) for safety reasons. When the brake is not applied the pedal value is high-limited to fixed value WPMXNOT. Furthermore a rate-of-change limitation is performed with the maximum permissible pedal-value increase DWPXNOT per calculation step (so within 10 ms). Alternatively it is possible to preset a maximum indicated torque via the characteristic MIFAMXNOT as function of the engine speed. This maximum indicated torque is used in %MDFAW to limit the indicated desired driver's torque.

Plausibility check brake / PWG:

When SY\_PBRPW = 1, additionally a plausibility check between brake and PWG is performed.

If, at normal operation, the brake is operated by the driver (not by FDR) for longer than TWPMBBR, then the pedal value is high-limited to WPMXBR, provided engine speed and speed exceed certain minimum values (NWPMBBR, VWPMBBR). Purpose of this functionality is to defuse a possible mechanical defect of the PWG. The limitation is removed, if wpedv goes back to zero and if it is thereby ensured that pedal idle can be detected. If the limitation is still active when the brake pedal is loosened, the pedal value is brought to the unlimited value wpedv by means of a rate-of-change limitation (DWPXNB).

B\_br2k is set, if both brake switches detect "brake operated" and if no fault has occurred during the plausibility check of the brake switch. In contrast to this, B\_brems is already set, if only one brake switch detects "brake operated" or if a fault was detected during the monitoring of the brake switch (cf. %GGEGAS). For the pedal value limitation at operated brake during normal operation B\_br2k is used and not B\_brems for availability reasons, so that vehicle is not stalled due to a defective brake switch.

Prevention of misuse:

When BIT2(CWBWEEN)=1 (Bit 2 of CWBWEEN set) additionally a misuse prevention is activated.

An automatic idle presetting takes place, if the NMAX-limitation is active for the time TMBVH when vfzg=0. Withdrawal of this automatic presetting is performed, if wped =< WPRMBVH is detected on driver's request.

Life detection:

When BIT3(CWBWEEN)=1 (Bit 3 of CWBWEEN set) additionally a life detection is activated.

After detected wire interruption at the PWG with selection of the remaining sensor signal (B\_sp1s, B\_sp2s), an automatic idle presetting is performed for as long as the remaining sensor value was within the idle range for the duration TWPLK. That means the default signal for the wped-formation must lead to wped=0 for at least the time TWPLK to terminate the automatic idle presetting. The limitation is only effective after active fault detection, i.e. the automatic idle presetting always assumes an edge detection at the fault bits B\_sp1s resp. B\_sp2s (refer to block PWGLK).

CAN\_2SG  
=====

On projects with two ME control units, the pedal value is adopted in the slave ECU from the CAN. The pedal value is otherwise calculated from the PWG poti signals as explained above.

PWG\_DIAG  
=====

The fault code memory entries FP1P (accelerator 1. poti), FP2P (accelerator 2. poti), BWF (movement detection) and FPP (accelerator poti) are generated in this partial function. The fault path FPP is redundant and can be dropped as soon as E\_fpp is no longer scanned in any other function. In case of a synchro fault, for which it cannot be decided which poti is defective (B\_upw12e = 1), E\_fplp is set.





## APP GGPED 8.30 Application hint

The parameters used in this function result from the tolerance calculation.  
UPWG12U is to be set less or equal to UPWGUR.

Coding via CWBWEEN  
=====

### Bit 0

0: Movement detection disabled  
1: Movement detection active

### Bit 1

0: No limitation of the pedal value at throttle sensor default operation  
1: Limitation of the pedal value at throttle sensor default operation (as at PWG default operation)

### Bit 2

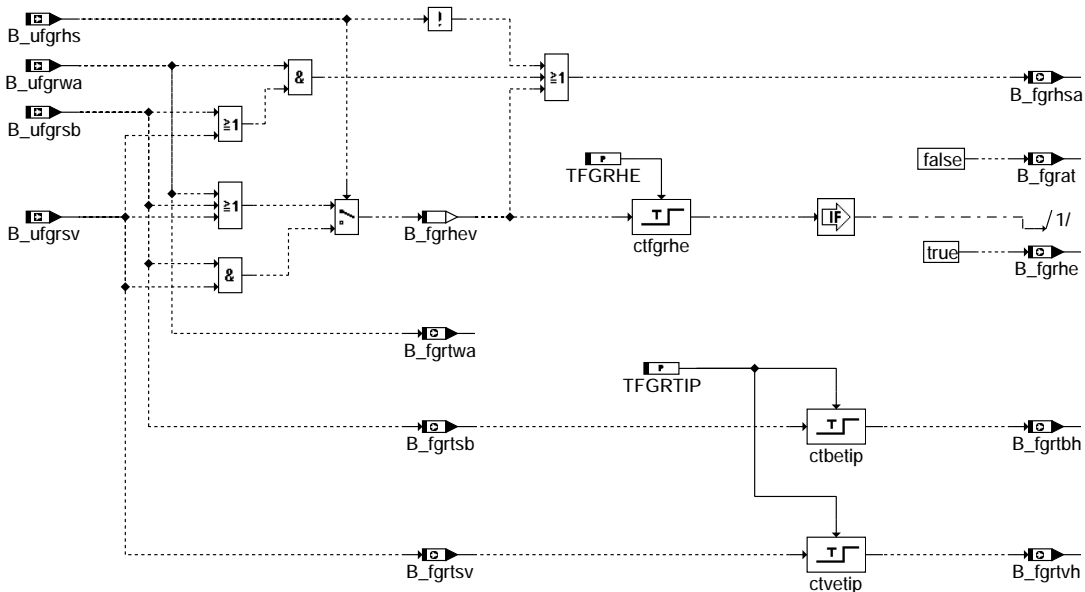
0: Misuse prevention disabled  
1: Misuse prevention active

### Bit 3

0: Life detection disabled  
1: Life detection active

## GGFGRH 11.10 Sensor Signals Cruise Control Lever

### FDEF GGFGRH 11.10 Function definition



ggfgrh-ggfgrh

### ABK GGFGRH 11.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TFGRHE			FW	Delay time for detecting FGR operating-lever fault
TFGRTIP			FW	Time to detect held FGR function key accelerate or decelerate
Variable	Source		Type	Description
B_FGRAT	GGFGRH		AUS	condition: tip-switch off CC lever control
B_FGRHE	GGFGRH		AUS	condition: CC-lever fault
B_FGRHEV	GGFGRH		LOK	Condition: Fault, FGR operating unit (temporary)
B_FGRHSA	GGFGRH		AUS	condition: CC main switch off
B_FGRTBH	GGFGRH		AUS	Condition: FGR switch acceleration held (no Tip)
B_FGRTSB	GGFGRH		AUS	Condition: FGR switch set/accelerate
B_FGRTSV	GGFGRH		AUS	Condition: FGR switch set/decelerate
B_FGRTVH	GGFGRH		AUS	Condition: FGR switch decelerate held (no Tip)
B_FGRTWA	GGFGRH		AUS	condition: Cruise control button RESUME
B_UFGRHS	UFFGRE		EIN	information cruise control level "main switch ON"
B_UFGRSB	UFFGRE		EIN	information cruise control level "set / accelerate"
B_UFGRSV	UFFGRE		EIN	information cruise control level "set / coast"
B_UFGRWA	UFFGRE		EIN	information cruise control level "resume"
CTBETIP	GGFGRH		LOK	Time counter for Tip detection FGR switch accelerate



Variable	Source	Type	Description
CTFGRHE	GGFGRH	LOK	Time counter to detect FGR operating-lever fault
CTVETIP	GGFGRH	LOK	Time counter for Tip detection FGR switch decelerate

### FW GGFGRH 11.10 Fixed Values

Parameter	Value	Description
TFGRHE		Delay time for detecting FGR operating-lever fault
TFGR TIP		Time to detect held FGR function key accelerate or decelerate

### FB GGFGRH 11.10 Detailed description of function

The purpose of the function is to process the signals from the vehicle-speed controller (FGR) that are read-in from function monitoring (Level 2) as hardware inputs. The operating lever has the following switches:

- o Main switch (indexed) (B\_ufgrhs)
- o Tip switch "Set/Accelerate" (B\_ufgrsb)
- o Tip switch "Set/Decelerate" (B\_ufgrsv)
- o Tip switch "Resumption" (B\_ufgrwa)

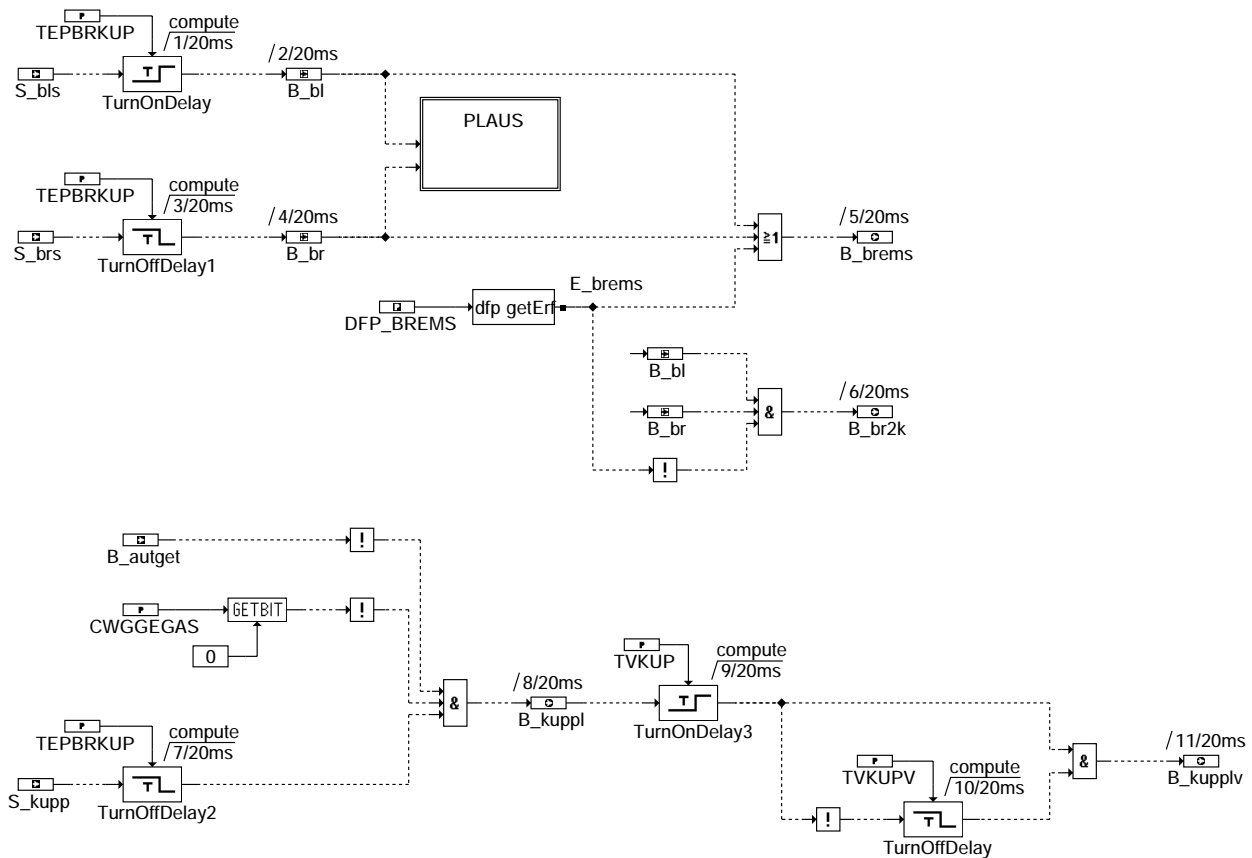
The three tip switches are designed to be in parallel with each other and in series with the main switch. When the main switch is turned off, there shall therefore be no signal at any of the three tip switches either. Because of the mechanical configuration of the switches, the tip switch "Set/Accelerate" may not be operate together with the tip switch "Set/Decelerate" when the main switch is activated. The operating-lever fault B\_fgrhe is set after elapse of the debounce time TFGRHE in the event of such implausible signals. The vehicle-speed controller is disabled by the main switch if the tip switch "Resumption" is operated at the same time as operating one of the tip switches "Set/Accelerate" or "Set/Decelerate".

The bits B\_fgrtbh and B\_fgrtvh indicate that the tip switch "Set/Accelerate" or "Set/Decelerate" has been operated for longer than approx. 0.5 s. This leads to a transition in the vehicle-speed controller function control to an acceleration or deceleration ramp, whereas operation for a time less than approx. 0.5 s causes only a one-time increase or decrease of the desired speed. B\_fgrtbh and B\_fgrtvh are calculated using the time TFGRTIP from B\_fgrrtsb and B\_fgrrtsv respectively.

### APP GGFGRH 11.10 Application hint

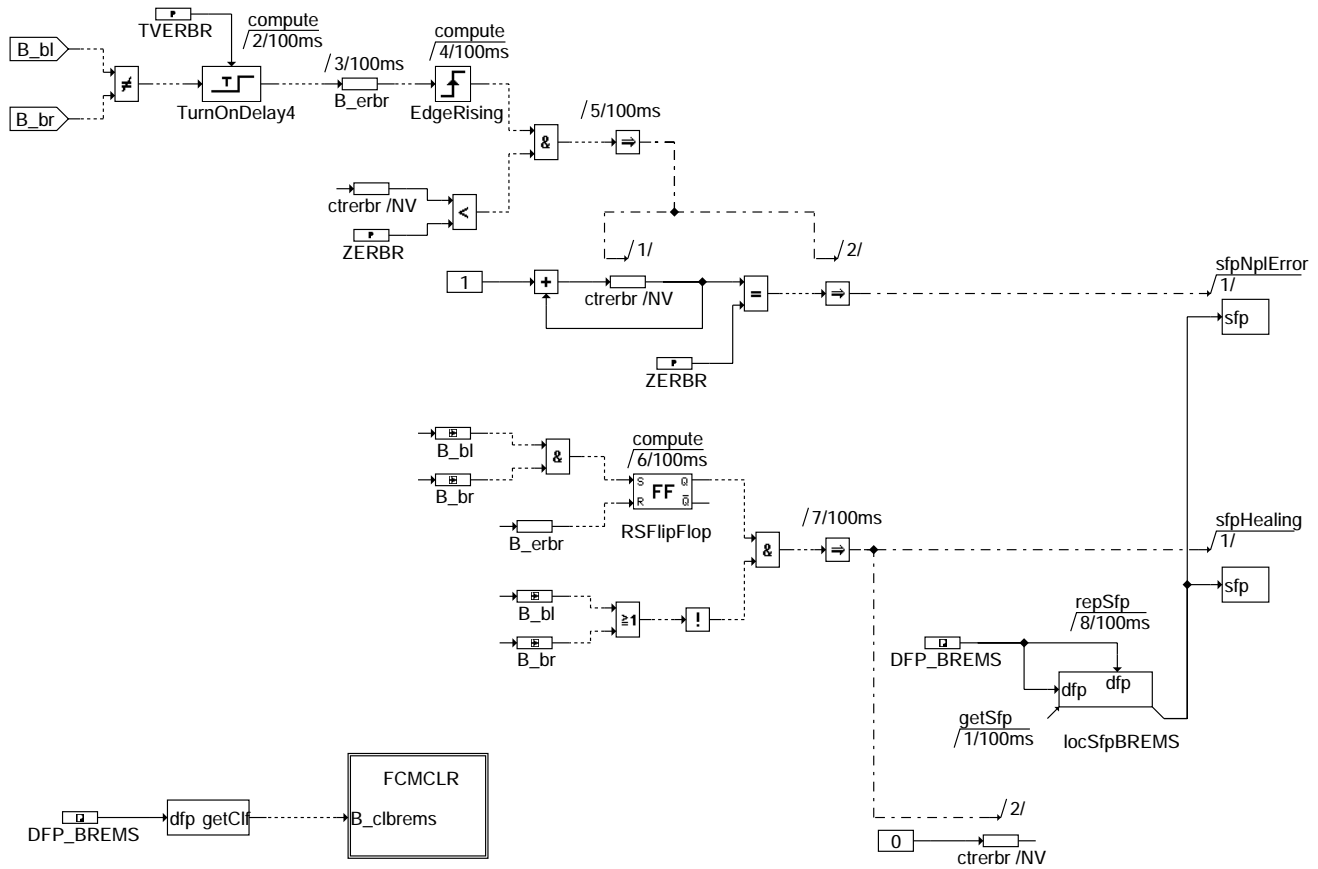
## GEGAS 9.30 Sensor variable for brake and clutch switches

### FDEF GEGAS 9.30 Function definition



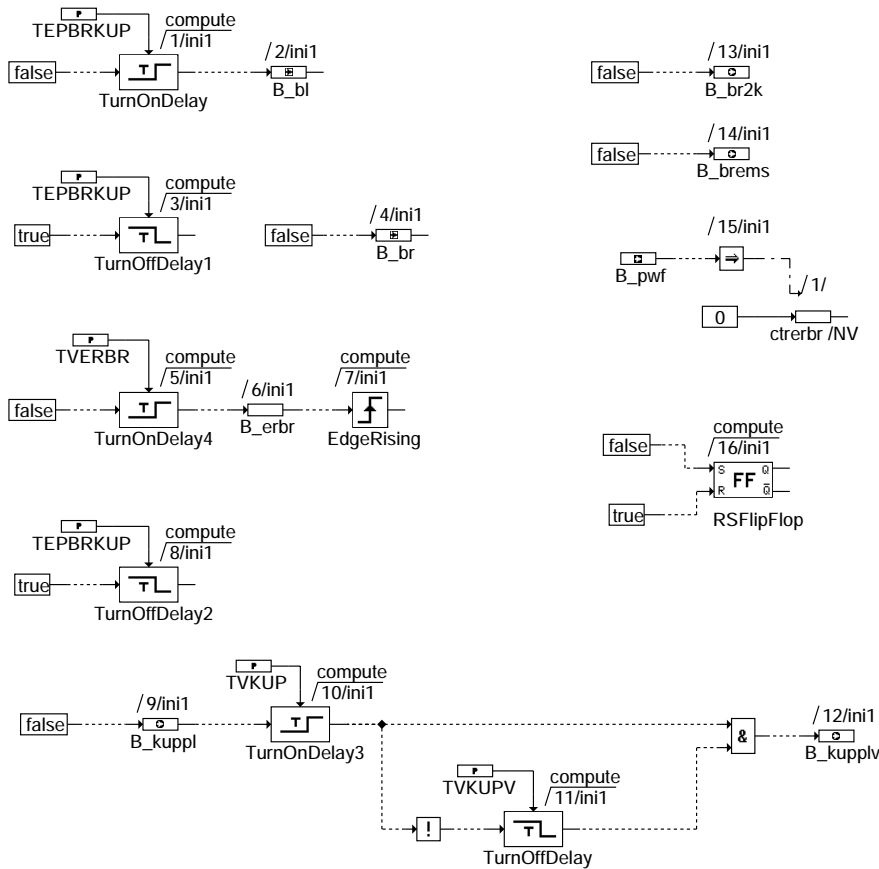
ggeg-as-main

ggeg-as-main



ggegass-plaus

ggegass-plaus



ggegass-init

### ABK GEGAS 9.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDKBREMS			FW	code word customer: Brake pedal sensor
CDTBREMS			FW	fault path code: brake pedal sensor
CLABREMS			FW	fault class: brake pedal sensor
CWGGEGAS			FW	code word for GGEGAS
TEPBRKUP			FW	debouncing time for brake and clutch switch
TSFBREMS			FW	fault active time: brake pedal sensor
TVERBR			FW	Delay time for brake-switch plausibility check
TVKUP			FW	Delay time for B_kupplv
TVKUPV			FW	delay time for resetting of B_kupplv
ZERBR			FW	Fault counter status for brake-switch implausibility

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B_AUTGET	PROKON	EIN	condition automatic gearbox
B_BKBREMS	GGEGAS	LOK	backup value active
B_BL	GGEGAS	LOK	Brake lights switch info: brakes operated
B_BR	GGEGAS	LOK	Brakes switch info: brakes operated
B_BR2K	GGEGAS	AUS	Condition brakes actuated 2-channel detection
B_BREMS	GGEGAS	AUS	condition: brake operated
B_CLBREMS		EIN	condition: clear fault-path BREMS (brake pedal signal)
B_ERBR	GGEGAS	LOK	Condition break switch signals differ
B_KUPPL	GGEGAS	AUS	EGAS Condition clutch is disengaged
B_KUPPLV	GGEGAS	AUS	Condition clutch delayed
B_MNBREMS	GGEGAS	LOK	fault type BREMS (brake):minimum value exceeded
B_MXBREMS	GGEGAS	LOK	fault type BREMS (Bremse): maximum value exceeded
B_NPBREMS	GGEGAS	LOK	fault type BREMS: test result not plausible
B_PWF		EIN	Condition for powerfail
B_SIBREMS	GGEGAS	LOK	fault type BREMS: signal inactiv
CTRERBR	GGEGAS	LOK	Error counter for break switch plausibility check
DFP_BREMS	GGEGAS	DOK	internal fault path number: brake pedal sensor
E_BREMS	GGEGAS	AUS	error flag: brake pedal signal
SFPBREMS	GGEGAS	AUS	status fault path BREMS: brake pedal signal
S_BLS		EIN	brake light switch (true=activated pedal)
S_BRS		EIN	Switch for brake



Variable	Source	Type	Description
S_KUPP		EIN	Clutch switch
Z_BREMS	GEGAS	AUS	cycle flag: brake pedal signal

### FW GEGAS 9.30 Fixed Values

Parameter	Value	Description
CDKBREMS		code word customer: Brake pedal sensor
CDTBREMS		fault path code: brake pedal sensor
CLABREMS		fault class: brake pedal sensor
CWGGEGAS		code word for GEGAS
TEPBRKUP		debouncing time for brake and clutch switch
TSEFBREMS		fault active time: brake pedal sensor
TVERBR		Delay time for brake-switch plausibility check
TVKUP		Delay time for B_kupplv
TVKUPV		delay time for resetting of B_kupplv
ZERBR		Fault counter status for brake-switch implausibility

### FB GEGAS 9.30 Detailed description of function

**- Connection:**

S\_BRS: Switch opens when break is operated. Switch is connected to terminal (KL) 15.  
S\_BLS: Switch closes when break is operated. Switch is connected to terminal (KL) 30.

The operating sequence is not defined

The input S\_kuppl does not exist on vehicles with automatic gearbox, the evaluation must then not be calculated.

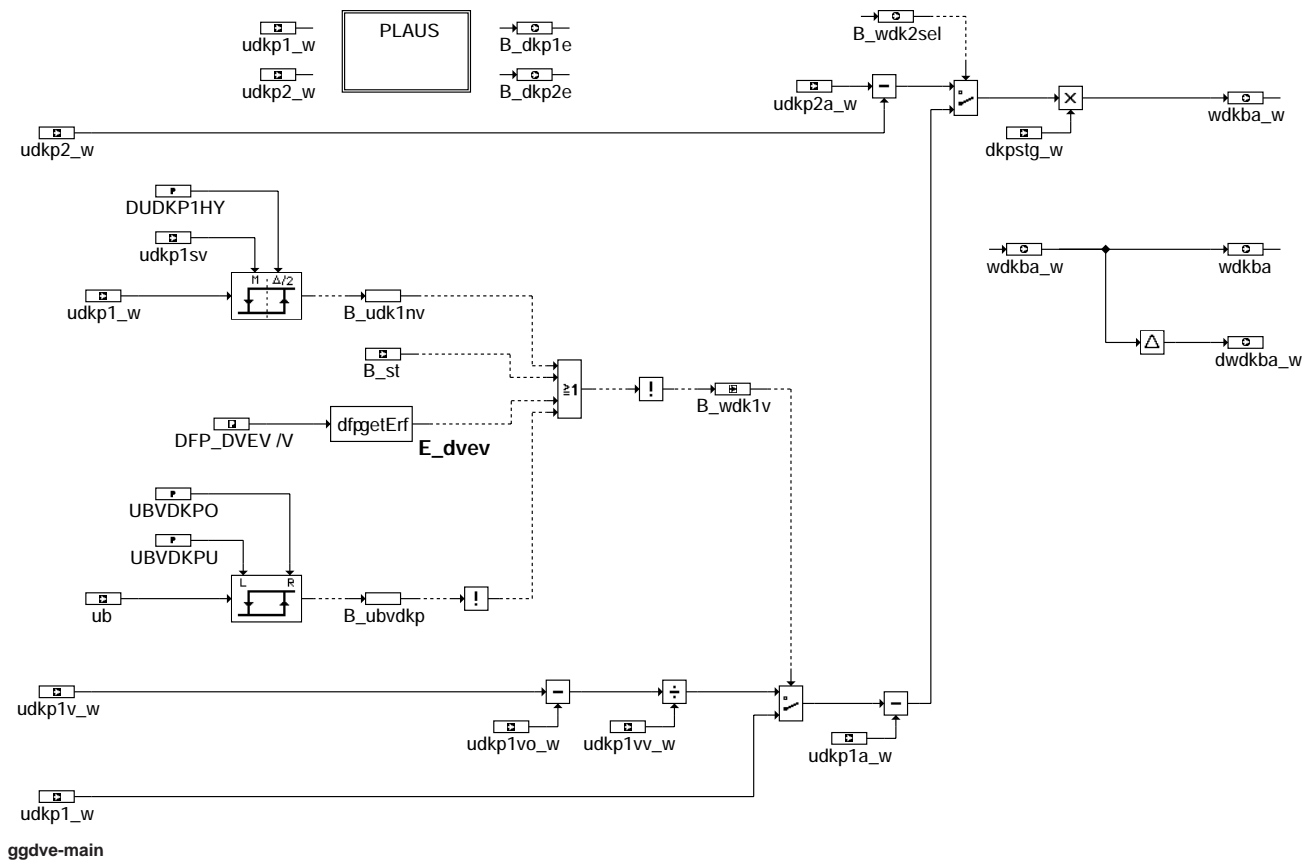
**- Diagnosis part:**

The two break informations B\_br and B\_bl may differ for the time TVERBR at the most.  
If this time is exceeded then the error counter is incremented. A break error is set as from the adjustable counter state ZERBR.  
The error counter is reset if breaking and non-breaking were successively definitely detected.

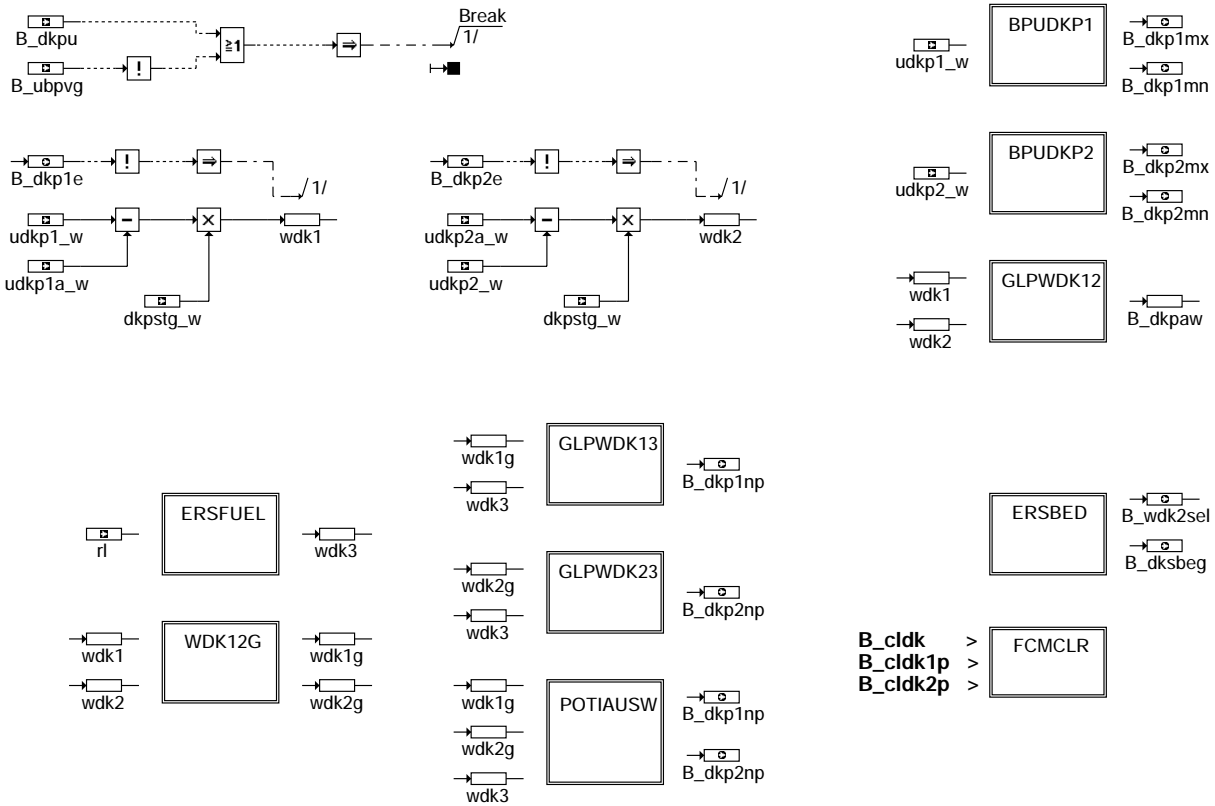
### APP GEGAS 9.30 Application hint

## GGDVE 2.40 Sensor variables for throttle-valve actuator

### FDEF GGDVE 2.40 Function definition

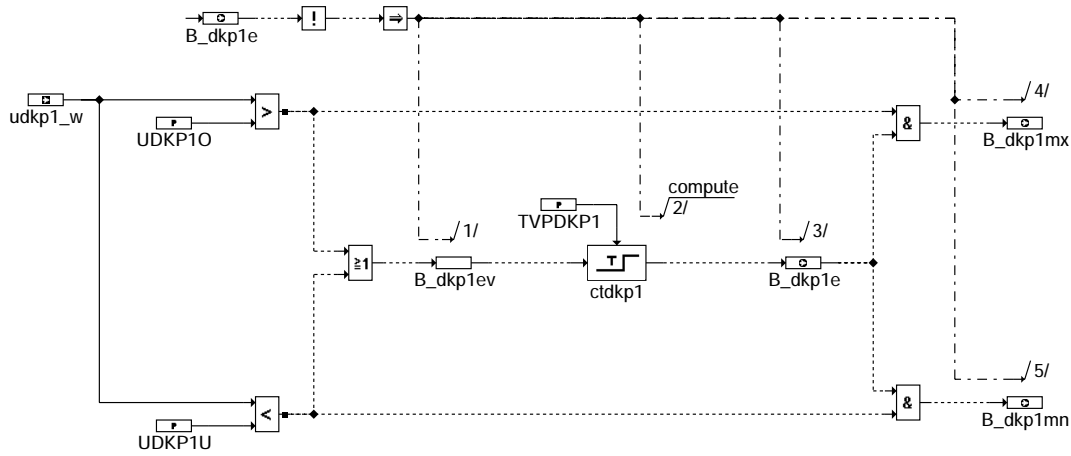


GGDVE: Calculation of the throttle angle



**ggdve-plaus**

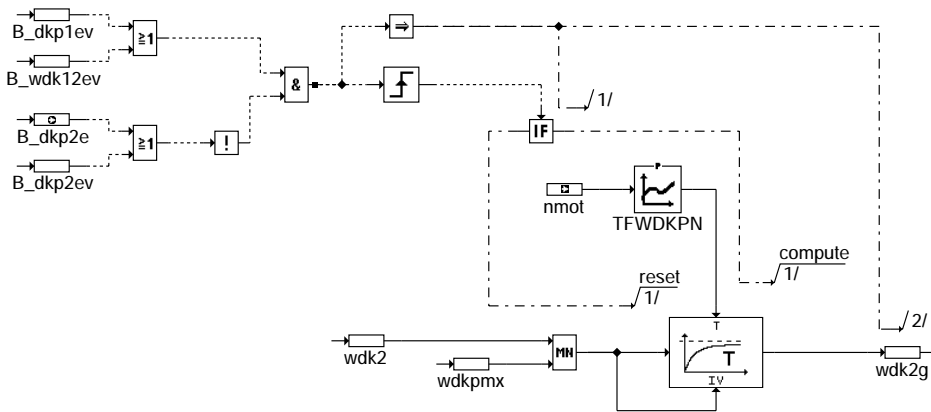
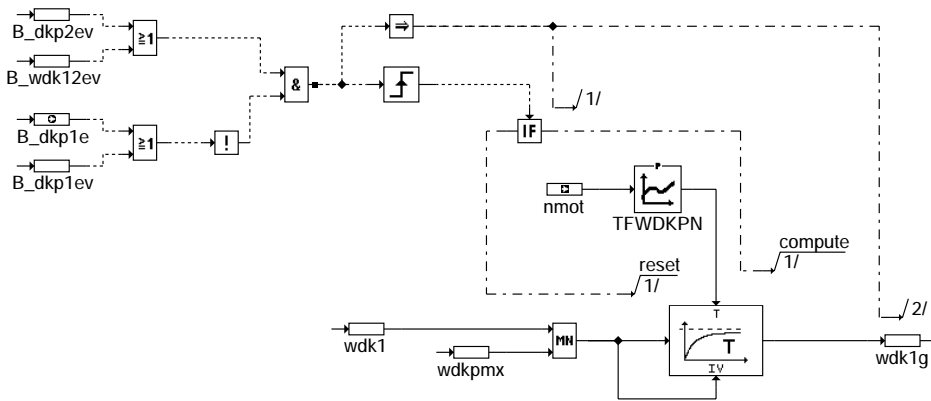
Partial function PLAUS: Overview of the plausibility checks



**ggdve-bpudkp1**

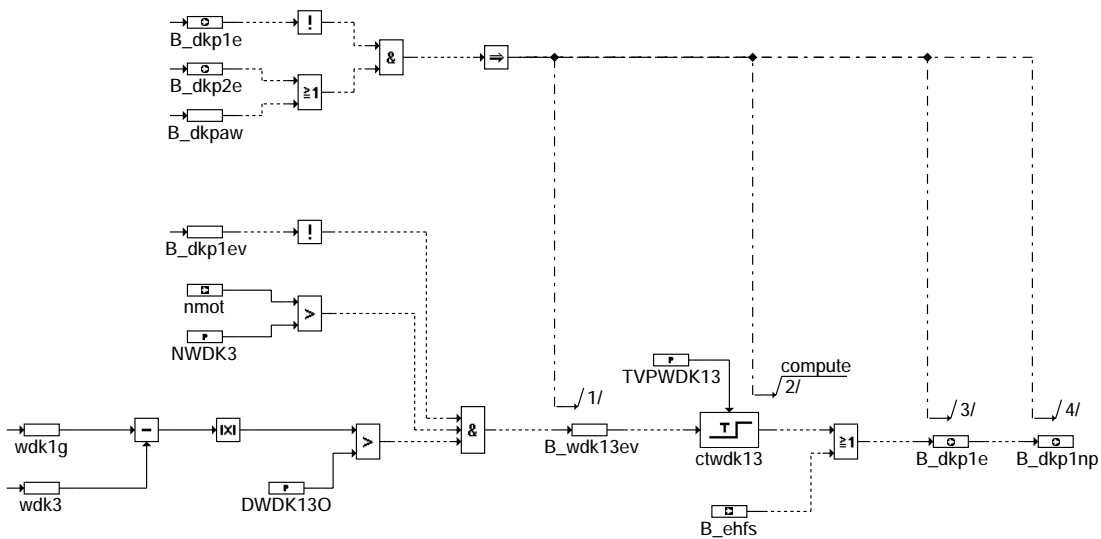


Partial function ERSFUEL: Calculation of the throttle-angle default value from the charge signal



### ggdve-wdk12g

Partial function WDK12G: Limitation and filtering of the throttle angles for comparison with default value from charge

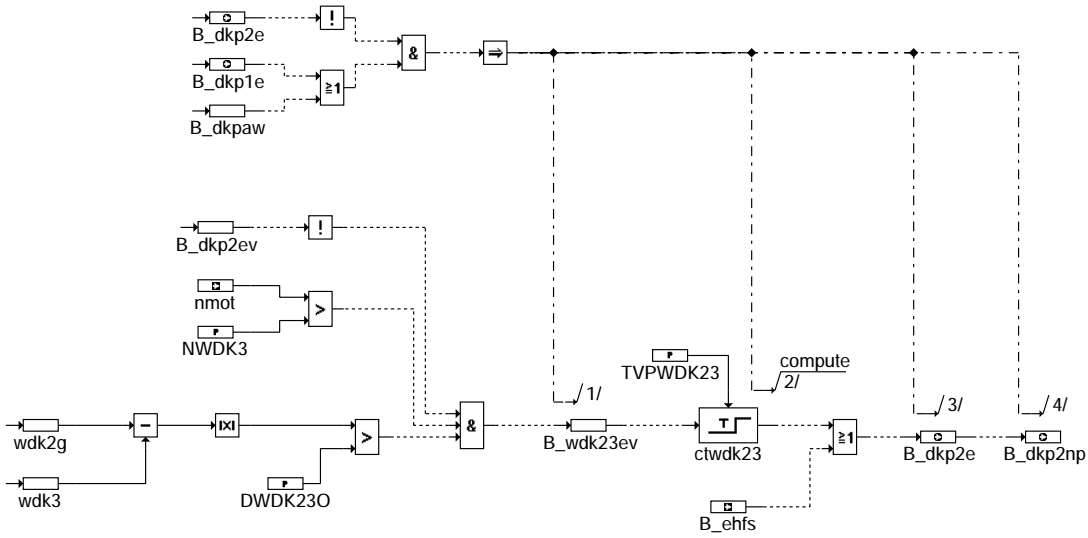


### ggdve-glpwdk13



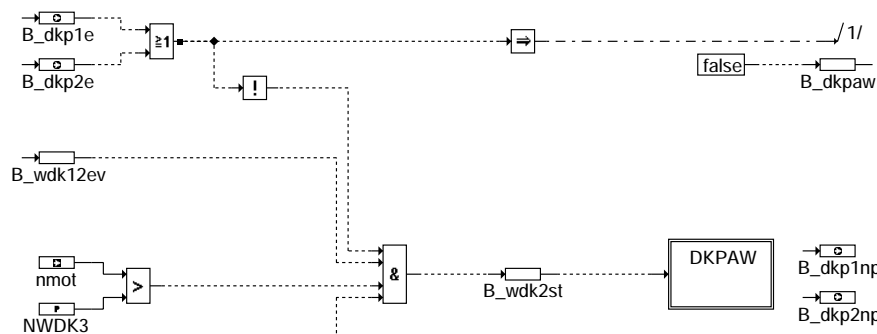


Partial function GLPWDK13: Synchronization check between throttle poti 1 and default value from charge



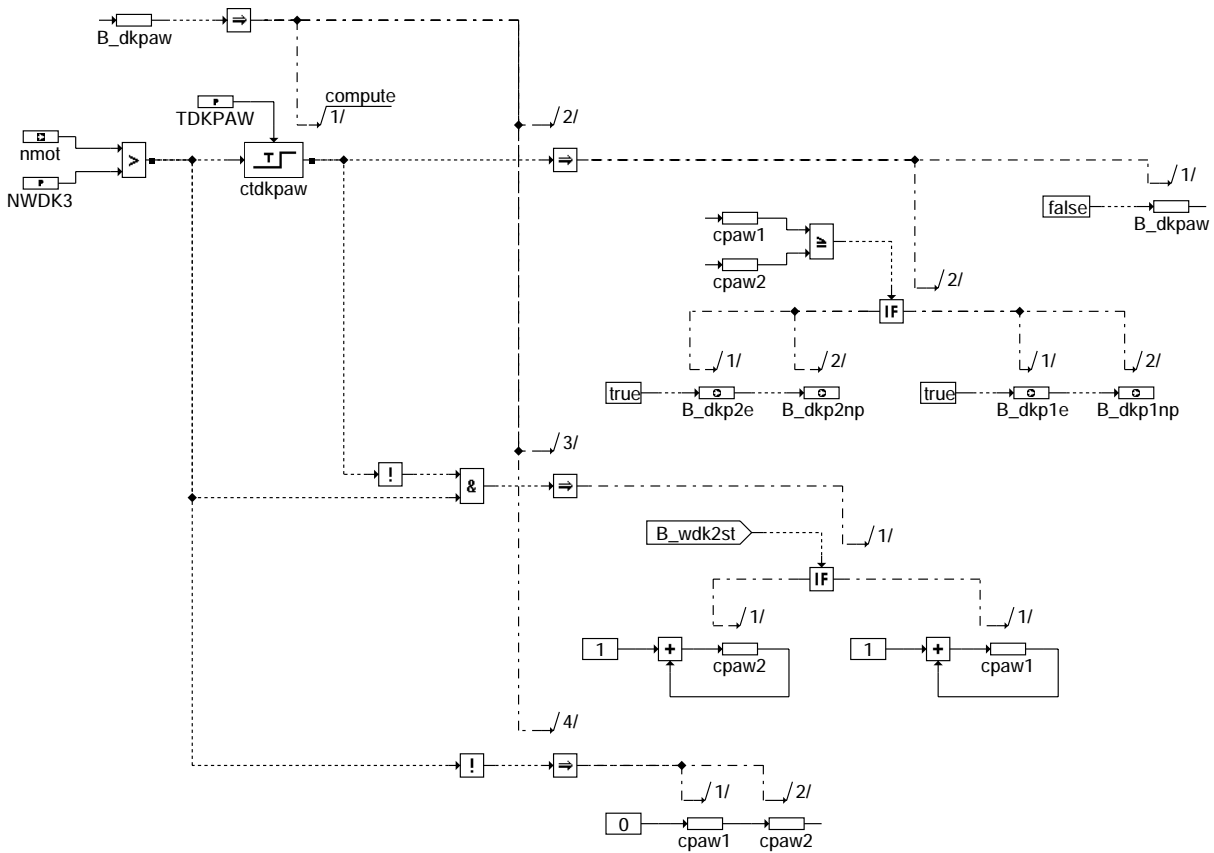
### ggdve-glpwdk23

Partial function GLPWDK23: Synchronization check between throttle poti 2 and default value from charge



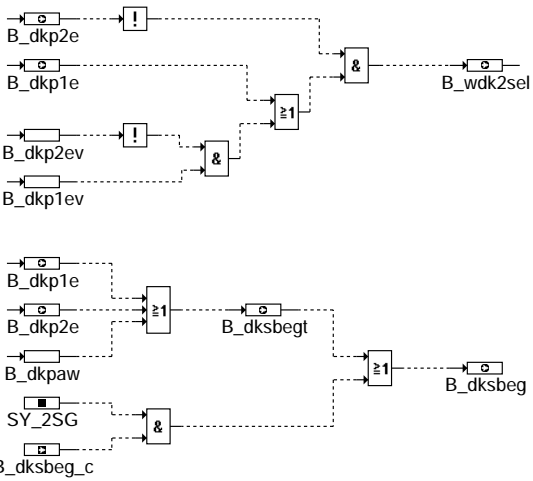
### ggdve-potiausw

Partial function POTIAUSW: Selection of the intact throttle poti for TP sensor default operation



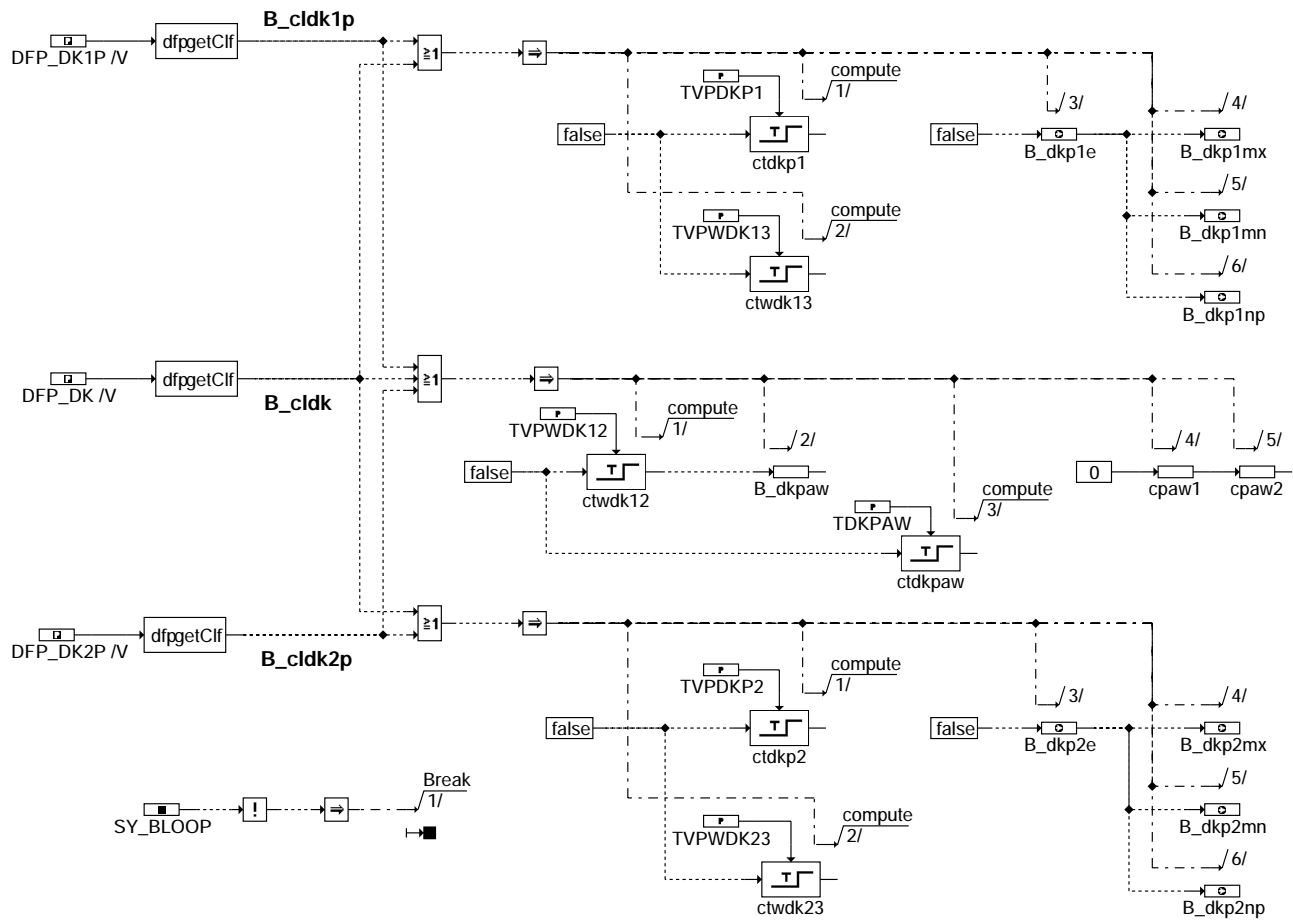
**ggdve-dkpaw**

Partial function DKPAW: Calculation and evaluation of the counters for throttle-poti selection



**ggdve-ersbed**

Partial function ERSBED: Calculation of the conditions for TP sensor default operation



**ggdve-fcmclr**

Partial function FCMCLR: Measures when clearing the fault code memory

**ABK GGDVE 2.40 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
DUDKP1HY			FW	offset of hysteresis for switching to amplified throttle poti 1 signal
DWDK12O			FW	max. permissible difference between throttle-valve angles from pot's 1 and 2
DWDK13O			FW	max. permissible difference between throttle-valve angles from pot's 1 and 3
DWDK23O			FW	max. permissible difference between throttle-valve angles from pot's 2 and 3
KFWDKPP	NMOT	RLV/PPL	KF	throttle blade position dependent on air charge signal
NDKPPU			FW	lower limit of engine speed for throttle poti plausibility check
NWDK3			FW	Minimum engine speed for calculation of throttle angle default value from charge
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_BLOOP			SYS (REF)	sys. con. resetting of irreversible EGAS fault possible during clearing of FCM
TDKPAW			FW	time for throttle-valve potentiometer selection
TFWDKPN	NMOT		KL	time constant for filtering DK angle before comp. with subs. value from charging
TVPDKP1			FW	delay time for recognition of implausible signal from throttle potentiometer 1
TVPDKP2			FW	delay time for recognition of implausible signal from throttle potentiometer 2
TVPWDK12			FW	Fault-tolerance time for checking synchronous operation of DK potentiometers
TVPWDK13			FW	fault-tol. time checking sync.-operation pot. 1 and subs. value from charging
TVPWDK23			FW	fault-tol. time checking sync. operation DK-pot. 2 and subs. value from charging
UBVDKPO			FW	batt. voltage threshold for using amplified signal from DK-potentiometer 1
UBVDKPU			FW	batt. voltage threshold for using non-amplified signal from DK-potentiometer 1
UDKP1O			FW	maximum permissible voltage from throttle potentiometer 1
UDKP1U			FW	minimum permissible voltage from throttle potentiometer 1
UDKP2O			FW	maximum permissible voltage from throttle potentiometer 2
UDKP2U			FW	minimum permissible voltage from throttle potentiometer 2
WDKPMXN	NMOT		KL	maximum throttle angle for plausibility check with charge signal
Variable	Source		Type	Description
B_CLDK			EIN	condition: clear error throttle potentiometer
B_CLDK1P			EIN	Flag for clearing measures: throttle valve (DK) potentiometer 1
B_CLDK2P			EIN	Flag for clearing measures: throttle valve (DK) potentiometer 2
B_DKP1E	GGDVE		AUS	condition: defect in throttle actuator potentiometer 1
B_DKP1EV	GGDVE		LOK	Condition temporary violation of range, DK potentiometer 1
B_DKP1MN	GGDVE		AUS	Condition lower-range violation DK potentiometer 1



Variable	Source	Type	Description
B_DKP1MX	GGDVE	AUS	Condition upper-range violation DK potentiometer 1
B_DKP1NP	GGDVE	AUS	Condition signal DK potentiometer 1 not plausible
B_DKP2E	GGDVE	AUS	condition: defect in throttle actuator potentiometer 2
B_DKP2EV	GGDVE	LOK	Condition temporary range violation throttle potentiometer 2
B_DKP2MN	GGDVE	AUS	Condition: lower-range violation DK potentiometer 2
B_DKP2MX	GGDVE	AUS	Condition: upper-range violation DK potentiometer 2
B_DKP2NP	GGDVE	AUS	Condition: signal DK potentiometer 2 not plausible
B_DKPAW	GGDVE	LOK	Condition DK-potentiometer selection for DK-sensor standby operation
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DKSBEG	GGDVE	AUS	condition: limiting throttle-valve setpoint value
B_DKSBEGT	GGDVE	AUS	condition: limiting DK setpoint value (for CAN for 2-ECU applications)
B_DKSBEG_C		EIN	condition: limiting DK setpoint value from other ECU by CAN
B_EDKS	GGDVE	AUS	Condition fault in throttle-valve sensor
B_EHFS	DHFM	EIN	Condition substitute value main charge sensor
B_ST	SWADAP	EIN	condition for start
B_UBPVG	ADVE	EIN	condition: battery voltage sufficient for 5-V potentiometer supply
B_JBVDKP	GGDVE	LOK	Condition battery voltage sufficient for amplification of DK potentiometer 1
B_JUDK1NV	GGDVE	LOK	Condition voltage of DK potentiometer 1 above the amplification range
B_WDK12EV	GGDVE	LOK	Condition temporary synchronization fault in throttle potentiometer
B_WDK13EV	GGDVE	LOK	Condition temporary non-plausibility between throttle poti 1 and default value f
B_WDK1V	GGDVE	LOK	Condition: amplified signal from potentiometer 1 used to calc. throttle angle
B_WDK23EV	GGDVE	LOK	Condition temporary non-plausibility between throttle poti 2 and default value f
B_WDK2SEL	GGDVE	AUS	Condition: DV-E position control is performed with actual-value-poti 2
B_WDK2ST	GGDVE	LOK	Condition throttle-angle calculation for position controller temporary from poti
CPAW1	GGDVE	LOK	Counter for potentiometer 1 for DK potentiometer selection
CPAW2	GGDVE	LOK	Counter for potentiometer 2 for DK potentiometer selection
DFP_DK	GGDVE	DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_DK1P	GGDVE	DOK	ECU int. fault path no.:
DFP_DK2P	GGDVE	DOK	ECU int. fault path no.:
DFP_DVEV	GGDVE	DOK	ECU int. fault path no.: DV-E fault in amplifier adjustment
DKPSTG_W	BGDVE	EIN	slope of throttle potentiometer (% DK / V)
DWDKBA_W	GGDVE	AUS	gradient of actual throttle blade position
E_DVEV	DDVE	EIN	Error flag: DV-E cause of failure: amplifier adjustment
FPVDKDS	BGPU	EIN	Factor pressure in front of throttle valve of pressure sensor
FTVDK	SWADAP	EIN	correction factor for temperature upstream of throttle valve
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RLVPPL	GGDVE	LOK	relative density-corrected air charge for calc. throttle-angle standby value
UB	SWADAP	EIN	battery voltage
UDKP1A_W	BGDVE	EIN	sensor voltage poti 1 of throttle actuator at (lower) mechanical stop (word)
UDKP1SV	BGDVE	EIN	Max. DK potentiometer-1 value for using amplified signal
UDKP1VO_W	BGDVE	EIN	voltage offset of DK potentiometer 1 amplification characteristic
UDKP1VV_W	BGDVE	EIN	amplification of throttle potentiometer 1
UDKP1V_W		EIN	amplified sensor voltage throttle potentiometer 1
UDKP1_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UDKP2A_W	BGDVE	EIN	sensor voltage throttle potentiometer 2 at (lower) mechanical stop
UDKP2_W		EIN	sensor voltage from throttle potentiometer 2 (word)
WDK1	GGDVE	LOK	Throttle angle from potentiometer 1
WDK1G	GGDVE	LOK	Throttle angle from pot. 1 limited & filtered for comparison with backup value
WDK2	GGDVE	LOK	Throttle angle from potentiometer 2
WDK2G	GGDVE	LOK	Throttle angle from pot. 2 limited & filtered for comparison with backup value
WDK3	GGDVE	LOK	throttle blade position dependent on air charge signal
WDKBA	GGDVE	AUS	throttle angle
WDKBA_W	GGDVE	AUS	throttle angle with respect to lower mechanical stop
WDKPMX	GGDVE	LOK	Maximum throttle angle for plausibility check with charge signal

### FW GGDVE 2.40 Fixed Values

Parameter	Value	Description
DUDKP1HY		offset of hysteresis for switching to amplified throttle poti 1 signal
DWDK12O		max. permissible difference between throttle-valve angles from pot's 1 and 2
DWDK13O		max. permissible difference between throttle-valve angles from pot's 1 and 3
DWDK23O		max. permissible difference between throttle-valve angles from pot's 2 and 3
NDKPPU		lower limit of engine speed for throttle poti plausibility check
NWDK3		Minimum engine speed for calculation of throttle angle default value from charge
TDKPAW		time for throttle-valve potentiometer selection
TVPDKP1		delay time for recognition of implausible signal from throttle potentiometer 1
TVPDKP2		delay time for recognition of implausible signal from throttle potentiometer 2
TVPWDK12		Fault-tolerance time for checking synchronous operation of DK potentiometers
TVPWDK13		fault-tol. time checking sync.-operation pot. 1 and subs. value from charging
TVPWDK23		fault-tol. time checking sync. operation DK-pot. 2 and subs. value from charging
UBVDKPO		batt. voltage threshold for using amplified signal from DK-potentiometer 1
UBVDKPU		batt. voltage threshold for using non-amplified signal from DK-potentiometer 1
UDKP1O		maximum permissible voltage from throttle potentiometer 1
UDKP1U		minimum permissible voltage from throttle potentiometer 1
UDKP2O		maximum permissible voltage from throttle potentiometer 2
UDKP2U		minimum permissible voltage from throttle potentiometer 2

**FB GGDVE 2.40 Detailed description of function**

The throttle angle is sensed by two potentiometers (poti 1 and poti 2), which are supplied together by the control unit with 5V. By a suitable connection poti 1 possesses a rising characteristic (i.e. larger poti voltage means larger throttle angle) and poti 2 possesses a falling characteristic (i.e. larger poti voltage means smaller throttle angle). One also refers to crossed characteristics. The different characteristics are necessary to possibly be able to detect a short-circuit of the poti signal lines. In case of a line interruption of one of the two signal lines the respective poti signal is taken to a value by the input resistance in the control unit, which signalizes a fully open throttle valve. So poti 1 is drawn towards 5V, poti 2 towards 0. The size of the input resistance resembles a compromise between insensitivity against transition resistance at the poti and the possibility to detect an interruption of the signal line.

So as to be able to adjust the demanded idle speed as exact as possible via the charge a higher resolution of the actual value is necessary in the region of smaller throttle angles. For this purpose the voltage signal of poti 1 is amplified by about factor 4 by means of an analog circuit in the control unit, which makes it possible to increase the resolution of 10 bit given by the A/D converter by 2 bit. When calculating the throttle angle from the amplified signal a resolution of about 0,025 degrees thus results, when using the non-amplified signal in the region of larger throttle angles the resolution will only be about 0,1 degrees. During normal operation always poti 1 servers for the calculation of the throttle angle and poti 2 for the monitoring of poti 1.

In order to prevent a non-desired power increase due to a too far open throttle valve or a stalling of the engine due to an erroneously too far closed throttle valve in case of a single fault, a plausibility check is performed on the two poti signals. During the range check the mechanically not accessible voltage ranges are used for the detection of short-circuits and line interruptions. The upper and lower range check is constantly active for the master poti (poti, from which the throttle angle is calculated, during normal operation poti 1). Signal falsifications by transition resistance are not permanently effective here, since they lead to a movement of the throttle valve due to the closed position control loop. With poti 2 the upper range check is continuously active during normal operation, whereas the lower range check only becomes active outside of the idle range due to possible signal falsifications by transition resistance. The engine speed serves as criterion for the detection of the idle range. With definitely detected faults at a poti the respective range check is no longer performed. If a fault is detected at a poti during the range check a transition into the TP sensor default operation is performed, in the process of which the remaining intact poti is monitored with the charge signal. If a range violation has occurred at both potis, SKA (safety fuel deactivation) is triggered due to the unknown throttle angle.

For the synchronization check each throttle angle is calculated from poti 1 and poti 2 by taking into consideration the learning values at the lower mechanical limit stop. The two calculated throttle angles must lie within a certain tolerance due to the mechanical coupling of both potis. Also the synchronization check is only active one-sided outside of the idle range at poti 2 due to possible signal falsifications by transition resistance. The synchronization check is only performed for as long as no fault is detected at one of the two potis. In case of a synchronization fault the defective poti is determined by comparison of the throttle angle calculated from the two poti signals with the charge signal. Thereafter TP sensor default operation with the intact poti is performed, monitored by the charge signal.

For the selection of the intact poti in case of a synchronization fault and for the monitoring at TP sensor default operation a default value is determined for the throttle angle from the charge signal, which is stored in a map. In the process the pressure and temperature influence is also taken into consideration besides the engine speed. Since a definite relation between charge and throttle angle during unthrottled operation is no longer given, respective limitation is performed. For the comparison with the thus determined default value the throttle angles calculated from the poti signals are not used directly. Instead the dynamic behavior of the intake manifold is approximated by filtering of the throttle angle calculated from the poti signals with an engine speed-dependent time constant. The necessary tolerances and fault tolerance times can be reduced in this way. Monitoring of the throttle angle by the charge signal is no longer possible with a fault of the main load sensor. In this case SKA is triggered as soon as a definite range or synchronization fault occurs at the throttle potis.

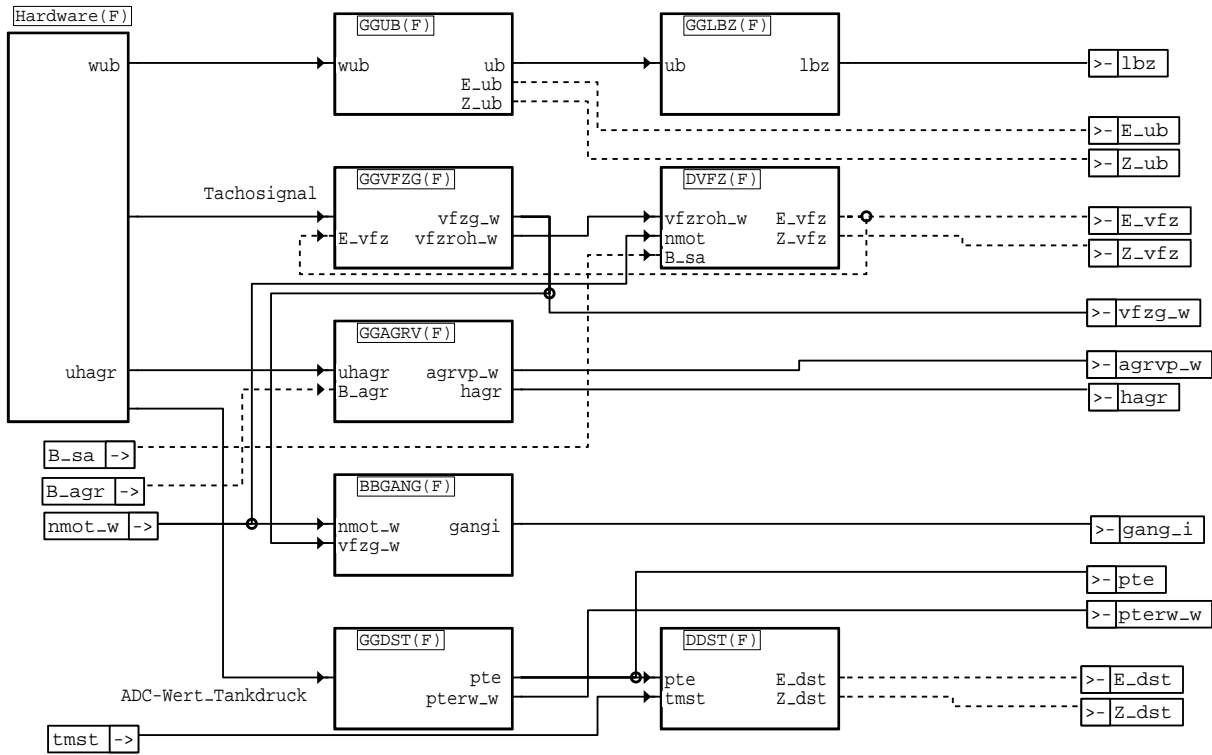
**Explanations:**

UMA:	Lower mechanical throttle limit stop (leakage air $\leq$ 4,8 kg/h)
UEA:	Lower electrical throttle limit stop (leakage air ca. 7,2 kg/h)
UDKPAOFF:	Standard setting 25,6 mV $\rightarrow$ 0,538 Grad DK
OEA:	Upper electrical throttle limit stop
OMA:	Upper mechanical throttle limit stop
UIP:	Voltage of actual-value poti % of 5 Volt
udkp1:	Voltage of actual-value poti in Volt
wdkba:	Actual throttle angle in % of the maximum opening, related to the UEA

## APP GGDVE 2.40 Application hint

## EGAG 2.0 General inputs

### FDEF EGAG 2.0 Function definition



### egag-egag

Responsible:

### ABK EGAG 2.0 Abbreviations

Variable	Source	Type	Description
AGRVP_W	EGAG	AUS	EGR- valve position, 16bit
B_AGR	EGAG	EIN	Condition AGR active
B_SA	MDRED	EIN	Condition fuel cut-off
DRUCK	EGAG	LOK	fed, unevaluated intake-manifold pressure
E_DST	EGAG	AUS	error flag: tank pressure sensor
E_UB	EGAG	AUS	error flag: power supply voltage UB
E_VFZ	EGAG	AUS	Error flag: vehicle speed signal
GANGI	EGAG	LOK	Engaged gear
GANG_J	EGAG	AUS	current gear
HAGR	EGAG	AUS	Stroke EGR valve
LBZ	EGAG	AUS	charge state of the battery
NMOT	EGAG	LOK	engine speed
NMOT_W	SWADAP	EIN	engine speed
PTE	EGAG	AUS	tank pressure (from ADC)
PTERW_W	EGAG	AUS	tank pressure rough value (16 bit)
TMST	GGTFM	EIN	engine temperature at start
UB	EGAG	LOK	battery voltage
UHAGR	EGAG	LOK	Voltage potentiometer EGR valve after ADC
VFZG_W	EGAG	AUS	Vehicle speed
VFZROH_W	EGAG	LOK	vehicle speed output value to scan tool
WUB	EGAG	LOK	battery voltage; scanned value of ADC
Z_DST	EGAG	AUS	cycle flag: pressure sensor gasoline tank
Z_UB	EGAG	AUS	cycle flag: power supply voltage UB
Z_VFZ	EGAG	AUS	cycle flag: vehicle speed signal

### FW EGAG 2.0 Fixed Values

Parameter	Value	Description
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## FB EGAG 2.0 Detailed description of function

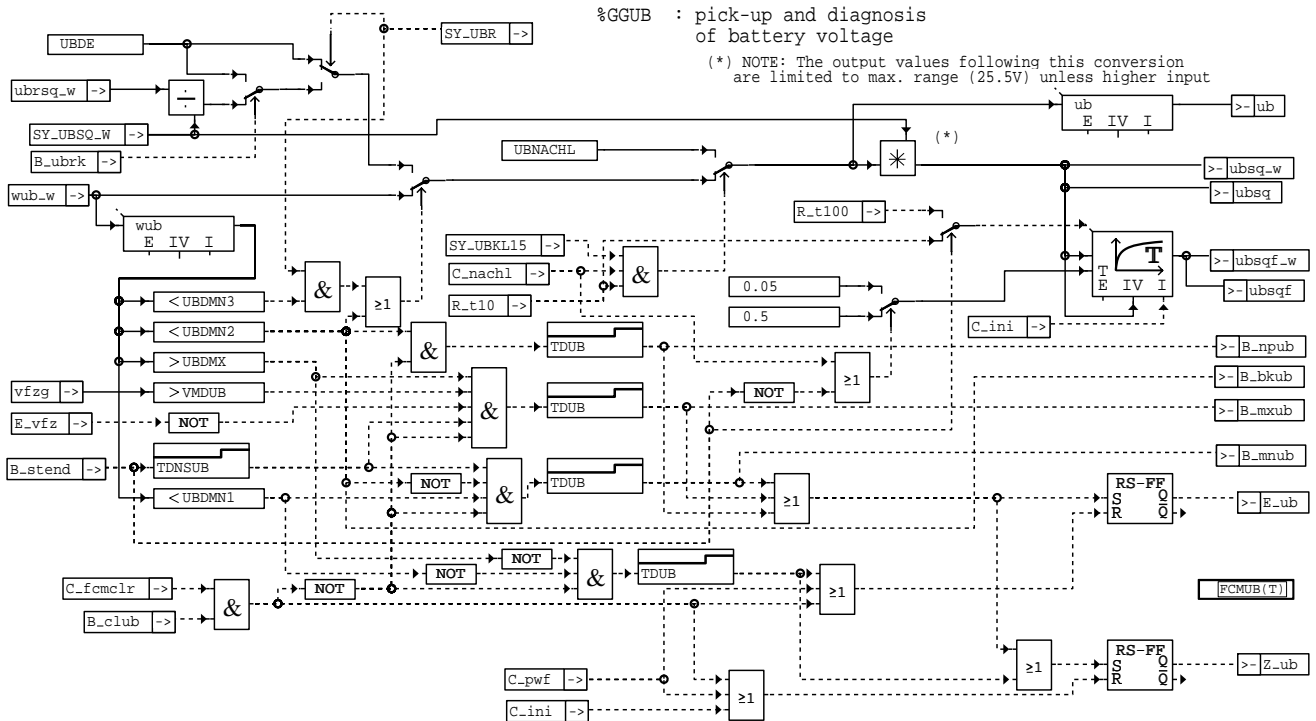
Description is missing !!!!

Responsible:

## APP EGAG 2.0 Application hint

## GGUB 11.30 Sensor variable for battery voltage incl. diagnosis

### FDEF GGUB 11.30 Function definition



### ggub-ggub

Fault memory management:

Status fault path UB: SFPUB  
Error flag UB: E\_ub  
Cycle flag UB: Z\_ub  
Fault type UB: B\_mxub  
B\_mnub  
B\_npub  
(B\_siub)

Reset fault path: C\_fmclr & B\_club  
Fault path UB: CDTUB  
Fault class UB: CLAUB  
Fault rate UB: TSFUB  
Carb Code UB: CDCUB  
Freeze frame table ub: FFTUB

### ABK GGUB 11.30 Abbreviations

### ABK GGUB 11.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCUB	BLOKNR		KL	code word CARB: battery voltage UB (onboard)
CDTUB			FW	code word tester: power supply voltage UB
CLAUB			FW	error class: battery voltage UB (onboard)
FFTUB	BLOKNR		KL	freeze frame table: battery voltage UB (onboard)
TDNSUB			FW	time period for battery after start
TDUB			FW	delay time of voltage diagnosis
TSFUB			FW	fault active time: battery voltage UB (onboard)
UBDE			FW	replace value for UBATT at damaged AD-channel
UBDMN1			FW	min. battery voltage (power supply)
UBDMN2			FW	min. battery voltage (ADC)
UBDMN3			FW	battery voltage, lower threshold to take over value for delayed power down



Parameter	Source-X	Source-Y	Type	Description
UBDMX			FW	max. battery voltage
UBNACHL			FW	UB-replace value during ECU afterrun
VMDUB			FW	Lower threshold of vehicle speed for battery voltage diagnosis
Variable	Source		Type	Description
BLOKNR			EIN	DAMOS source for block number
B_BKUB	GGUB		AUS	condition backup value for battery voltage (onboard)
B_CLUB			EIN	condition clear fault path battery voltage (onboard)
B_MNUB	GGUB		AUS	fault type: minimum value of battery voltage (onboard)
B_MXUB	GGUB		AUS	fault type: maximum value battery voltage (onboard) exceeded
B_NPUB	GGUB		AUS	Error type: signal of battery voltage not plausible
B_STEND	BBSTT		EIN	condition end of start
B_UBRK			EIN	condition main relay contact fault
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_NACHL			EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
E_JUB	GGUB		AUS	error flag: power supply voltage UB
E_VFZ	EGAG		EIN	Error flag: vehicle speed signal
R_T10			EIN	Time schedule 10 ms
R_T100			EIN	Time schedule 100 ms
SFPUB	GGUB		AUS	status fault path: battery voltage UB (onboard)
SY_UBKL15			EIN	system constant onboard battery voltage scanned from ignition key on input
SY_UBR	PROKON		EIN	system constant onboard battery voltage scanned from main relay input
SY_UBSQ_W			EIN	System constant conversion factor UB resolution to standard quantization ubsq
UB	GGUB		AUS	battery voltage
UBRSQ_W			EIN	battery voltage (word) via main relay, standard quantization
UBSQ	GGUB		AUS	battery voltage (on board), converted to standard quantization
UBSQF	GGUB		AUS	battery voltage (on board), converted to standard quantization and low pass filter
UBSQF_W	GGUB		AUS	battery voltage (on board), converted to standard quantization and low pass filter
UBSQ_W	GGUB		AUS	battery voltage (on board), converted to standard quantization
VFZG	SWADAP		EIN	vehicle speed (km/h)
WUB	GGUB		LOK	battery voltage; scanned value of ADC
WUB_W			EIN	battery voltage; scanned value of ADC (16Bit from 10Bit resolution)
Z_UB	GGUB		AUS	cycle flag: power supply voltage UB

### FW GGUB 11.30 Fixed Values

Parameter	Value	Description
CDTUB		code word tester: power supply voltage UB
CLAUB		error class: battery voltage UB (onboard)
TDNSUB		time period for battery after start
TDUB		delay time of voltage diagnosis
TSFUB		fault active time: battery voltage UB (onboard)
UBDE		replace value for UBATT at damaged AD-channel
UBDMN1		min. battery voltage (power supply)
UBDMN2		min. battery voltage (ADC)
UBDMN3		battery voltage, lower threshold to take over value for delayed power down
UBDMX		max. battery voltage
UBNACHL		UB-replace value during ECU afterrun
VMDUB		Lower threshold of vehicle speed for battery voltage diagnosis

### FB GGUB 11.30 Detailed description of function

If the signal is below the threshold UBDMN2, this points to a fault in the UB determination in the ECU (e.g. ADC), since, if  $U \leq 2.5$  V, the processor does not work. The use of a substitute value (UBDE) is only useful and intended of this type of fault.

On the other hand a max. value check is only effective after the delay TDNSUB and only with a rolling vehicle (and with faultless speed signal). This is intended to avoid a faulty diagnosis which could arise, for example in the case of start assistance with a 24 V battery. Conversely, if setting conditions for B\_maxflr will disappear, a B\_maxflr based error will be reset in case of falling below max. threshold only.

The check of the lower threshold UBDMN1 (fault in board voltage system) is also allowed only after the waiting period TDNSUB from the start end when the board voltage has recovered from the breakdown caused by the start procedure.

As soon as one of the threshold value scans ( $>UBDMX$  /  $<UBDMN1$  /  $<UBDMN2$ ) have been fulfilled, the respectiv bits (B\_maxflr / B\_minflr / B\_plaus) and the error and cycle flags after expiry of the debouncing time TDUB will be set simultaneously. A common debouncing period is provided for the fault detection in order to limit the expenditure of ram cells for the time monitoring. Conversely in I.O. case (B\_noflr) the debouncing period TDUB also has to expire before the fault flag is reset.

The cycle flag is either set parallel to the fault B\_minflr / E\_ub, as described above, or, in all other cases, especially when no fault is detected, at the latest when the recovery period TDNSUB expires after the start end.

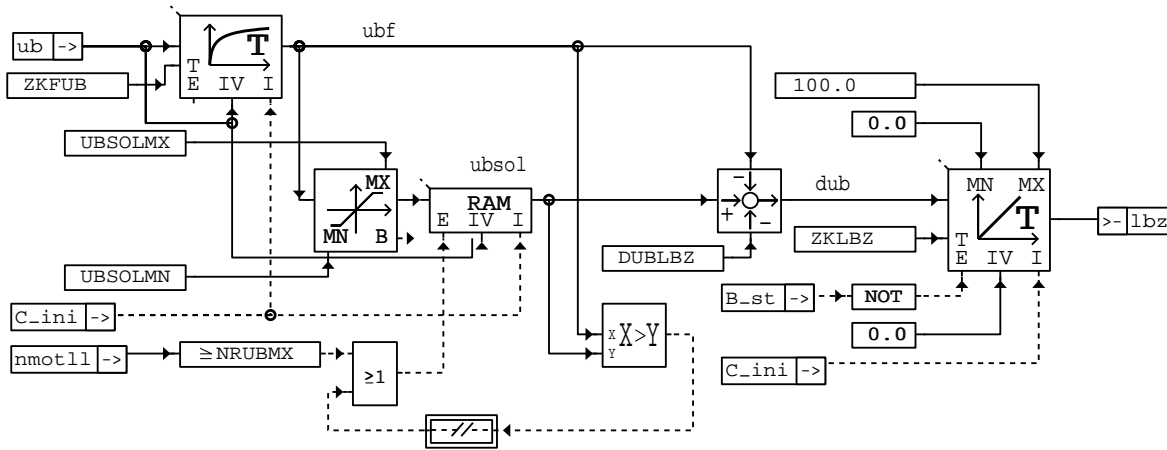


## APP GGUB 11.30 Application hint

Reference values: UBDMX 16 V; UBDMN1 10 V; UBDMN2 2,5 V; TDNSUB ca. 3 min  
TDUB ca. 200ms

## BGLBZ 4.1 Calculated charge deficit of the battery

### FDEF BGLBZ 4.1 Function definition



bglbz-bglbz

### ABK BGLBZ 4.1 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DUBLBZ			FW	Voltage offset for battery charge computation
NRUBMX			FW	maximal engine speed for battery voltage control
UBSOLMN			FW	Lower limit for Battery target voltage
UBSOLMX			FW	Upper limit for Battery target voltage
ZKFUB			FW	time constant for filtering the battery voltage
ZKLBZ			FW	time constant of the LBZ integrator
Variable	Source		Type	Description
B_ST	SWADAP		EIN	condition for start
C_JNI	SWADAP		EIN	ECU-condition for intialisation
DUB	BGLBZ		LOK	difference of battery voltage for voltage control
LBZ	BGLBZ		AUS	charge state of the battery
NMOTLL	BGNMOT		EIN	engine speed
UB	SWADAP		EIN	battery voltage
UBF	BGLBZ		LOK	filtered battery voltage for charge control
UBSOL	BGLBZ		LOK	target battery voltage

### FW BGLBZ 4.1 Fixed Values

Parameter	Value	Description
DUBLBZ		Voltage offset for battery charge computation
NRUBMX		maximal engine speed for battery voltage control
UBSOLMN		Lower limit for Battery target voltage
UBSOLMX		Upper limit for Battery target voltage
ZKFUB		time constant for filtering the battery voltage
ZKLBZ		time constant of the LBZ integrator

### FB BGLBZ 4.1 Detailed description of function

This function determines if the actual power of the generator is high enough to avoid a battery discharge. Therefore the difference dub between a target voltage ubsol and the filtered actual voltage ubf ist calculated. An offset of DUBLBZ (env. 0.5 Volt) is subtracted from dub due to tolerances. The value dub is integrated and represents a value lbz for the charge deficit of the battery. lbz could be used for example in the idle speed control to increase idle speed if the battery is no more charged by the too slowly rotating generator.

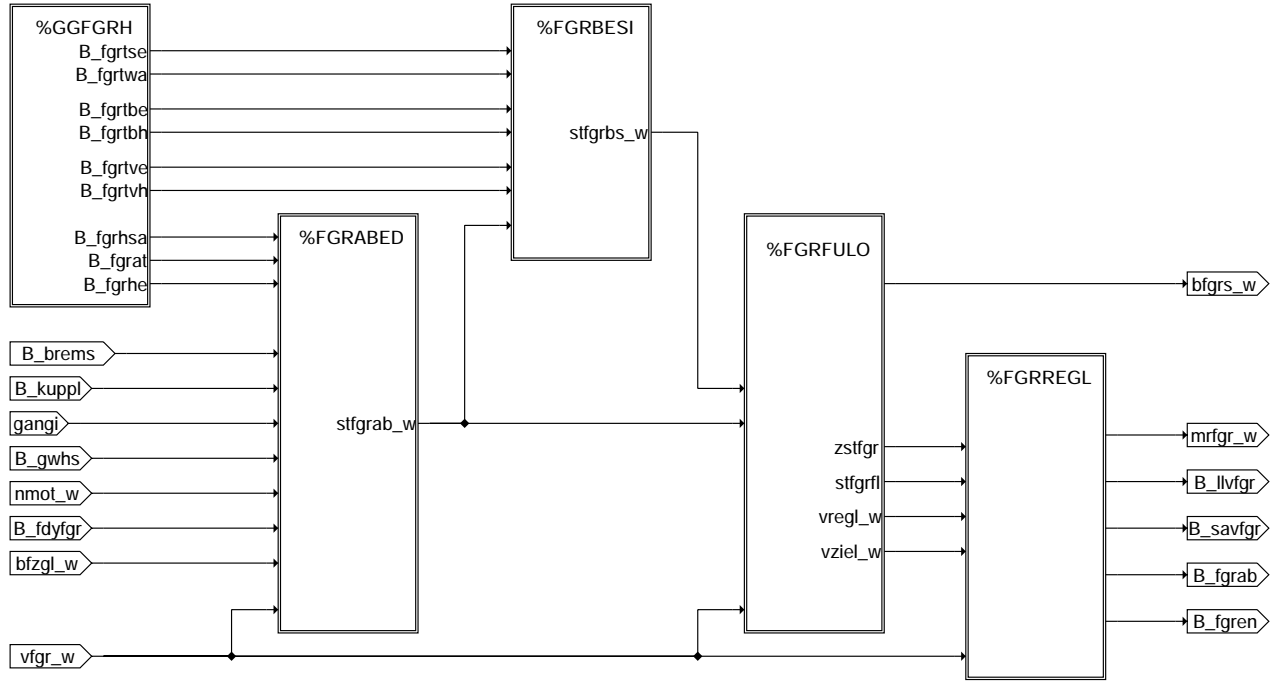
The target voltage ubsol is directly measured by the ECU when the actual engine speed guarantees the maximal power of the generator or when the actual voltage is higher than the target voltage. To be shure that there are no erroneus values stored into ubsol, this target voltage is limited between the limits UBSOLMN and UBSOLMX.

bglbz-bglbz

## APP BGLBZ 4.1 Application hint

## FGRUE 6.10 Overview of vehicle-speed controller

### FDEF FGRUE 6.10 Function definition



fgrue-fgrue

### ABK FGRUE 6.10 Abbreviations

Variable	Source	Type	Description
BFZGL_W	GGVFZG	EIN	Vehicle acceleration in longitudinal direction
B_BREMS	GGEGAS	EIN	condition: brake operated
B_FDYFGR		EIN	Condition: Intervention in driving dynamics function (as cut-off condition: for CC/ACC shut-off from the function)
B_FGRAB	FGRUE	AUS	condition: tip-switch off CC lever control
B_FGRAT	FGRUE	LOK	condition: cruise control is active (enable)
B_FGREN	FGRUE	AUS	condition: CC-lever fault
B_FGRHE	FGRUE	LOK	condition: CC main switch off
B_FGRHSA	FGRUE	LOK	condition: Cruise control button ACCELERATE
B_FGRTBE	FGRUE	LOK	Condition: FGR switch acceleration held (no Tip)
B_FGRTBH	FGRUE	LOK	condition: CC button (+ or -) set
B_FGRTSE	FGRUE	LOK	condition: Cruise control button DECELERATE
B_FGRTVE	FGRUE	LOK	Condition: FGR switch decelerate held (no Tip)
B_FGRTVH	FGRUE	LOK	condition: Cruise control button RESUME
B_FGRTWA	FGRUE	LOK	Condition gear change on manual transmission vehicle
B_GWHS	BBGANG	EIN	EGAS Condition clutch is disengaged
B_KUPPL	SWADAP	EIN	Condition: Idling disabled by FGR
B_LLVFGR	FGRUE	AUS	Condition: prohibited trailing throttle fuel cut-off by cruise control
B_SAVFGR	FGRUE	AUS	Engaged gear
GANGI	SWADAP	EIN	relative torque demand from cruise control
MRFGR_W	FGRUE	AUS	engine speed
NMOT_W	SWADAP	EIN	Status word, cut-out conditions, vehicle-speed controller
STFGRAB_W	FGRUE	LOK	Status word operating signals, vehicle-speed controller
STFGRBS_W	FGRUE	LOK	Status byte FGR function logic
STFGRFL	FGRUE	LOK	Status of vehicle-speed controller
VFGR_W	GGVFZG	EIN	cruise control vehicle speed
VREGL_W	FGRUE	LOK	desired speed for cruise control
VZIEL_W	FGRUE	LOK	target velocity cruise control
ZSTFGR	FGRUE	LOK	Status of vehicle-speed controller

### FW FGRUE 6.10 Fixed Values

Parameter	Value	Description
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## FB FGRUE 6.10 Detailed description of function

Functionality of the vehicle-speed controller

The task of the vehicle-speed controller (FGR) is to keep the speed of the vehicle constant irrespective of the road resistance without the accelerator pedal having to be operated to this end. Besides maintaining the current speed (Constant driving), reaching a previously stored target speed (Resumption), accelerating or decelerating as well as increasing or decreasing in small increments (Tip-up and Tip-down) and accepting the current vehicle speed as the desired speed (Set) are also possible.

Control of the vehicle-speed controller by the driver is by a special operating component, the switch for the functions of Set, Resumption, Accelerate and Decelerate. Depending on the version of the operating component, the switch can have more than one function (e.g. a function button for Set/Decelerate and a button for Resumption/Accelerate) because the function to be executed is given clearly from the status of the vehicle-speed controller and the duration of switch operation. The functions Tip-up and Tip-down are triggered by briefly operating the switch for acceleration or deceleration.

Besides the switches for the functions, the operating component also has an optional main switch and a switch for turning the vehicle-speed controller off. A previously stored target speed is lost when the main switch is turned off. Apart from by the operating component, the vehicle-speed controller can also be turned off by operating the brake or the clutch.

When the vehicle-speed controller is switched on, the driver can set a higher engine performance by operating the accelerator pedal so that the vehicle will accelerate (override). The vehicle-speed controller remains active in the background throughout this and resumes controlling the previously set desired speed when the accelerator pedal is released.

An alternative to the internal vehicle-speed controller can be a control by externally realized vehicle-to-vehicle ranging (ACC = Adaptive Cruise Control). This system communicates with the ME over CAN. The presence of an ACC ECU is indicated B\_acc being set. The internal vehicle-speed controller is then deactivated in this case.

The vehicle-speed controller functionality is only calculated in the master in a system where there are 2 ME ECU's. The output variables are transmitted to the slave via CAN.

### Program architecture

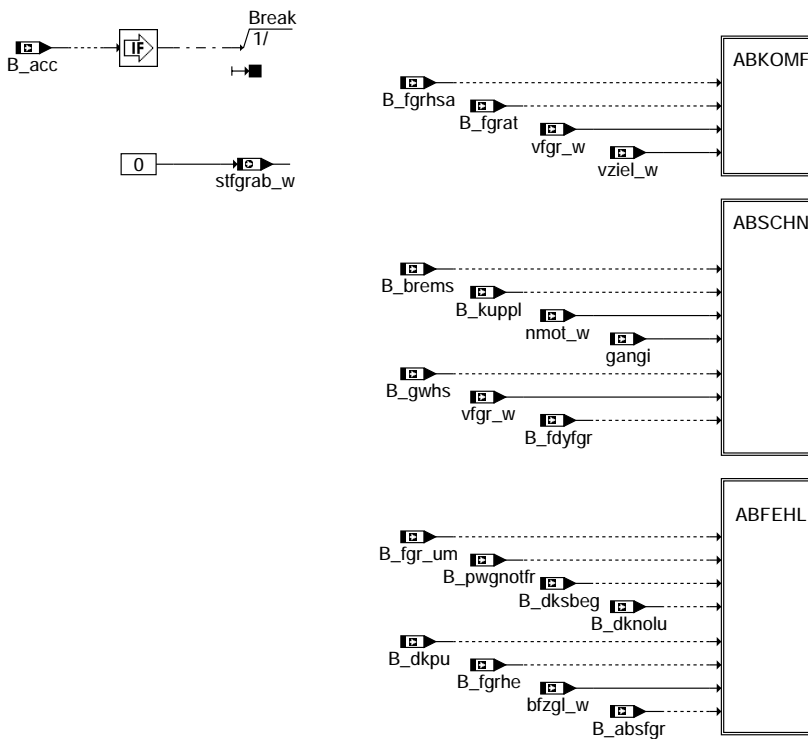
The functionality shown is realized by the functions given in the overview. These functions assume the following tasks:

- GGFGRH: Sensing the switch status of the vehicle-speed controller operating component (hardware signals or CAN message)
- FGRABED: Monitoring the enable and disable conditions for the vehicle-speed controller
- FGRBESI: Evaluating the vehicle-speed controller and calculating the status word "FGR operating signals"
- FGRFULO: Function logic and calculating the status of the vehicle-speed controller, target and desired speeds
- FGRREGL: Controller calculations, disabling idling and overrun fuel cutoff

## APP FGRUE 6.10 Application hint

## FGRABED 1.30 Shutdown conditions, vehicle-speed controller

### FDEF FGRABED 1.30 Function definition

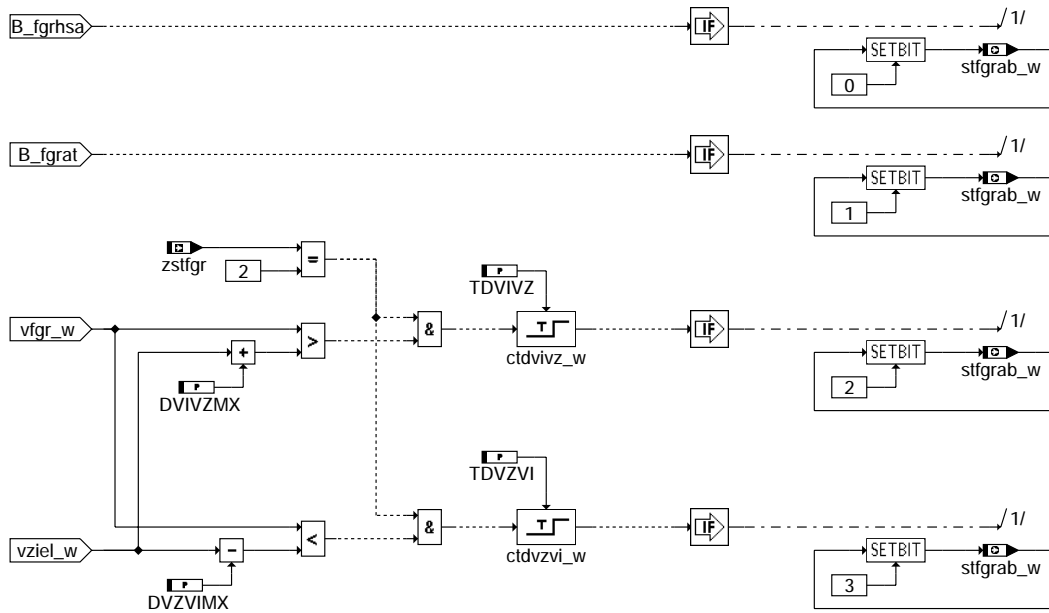


fgrabed-fgrabed

fgrabed-fgrabed

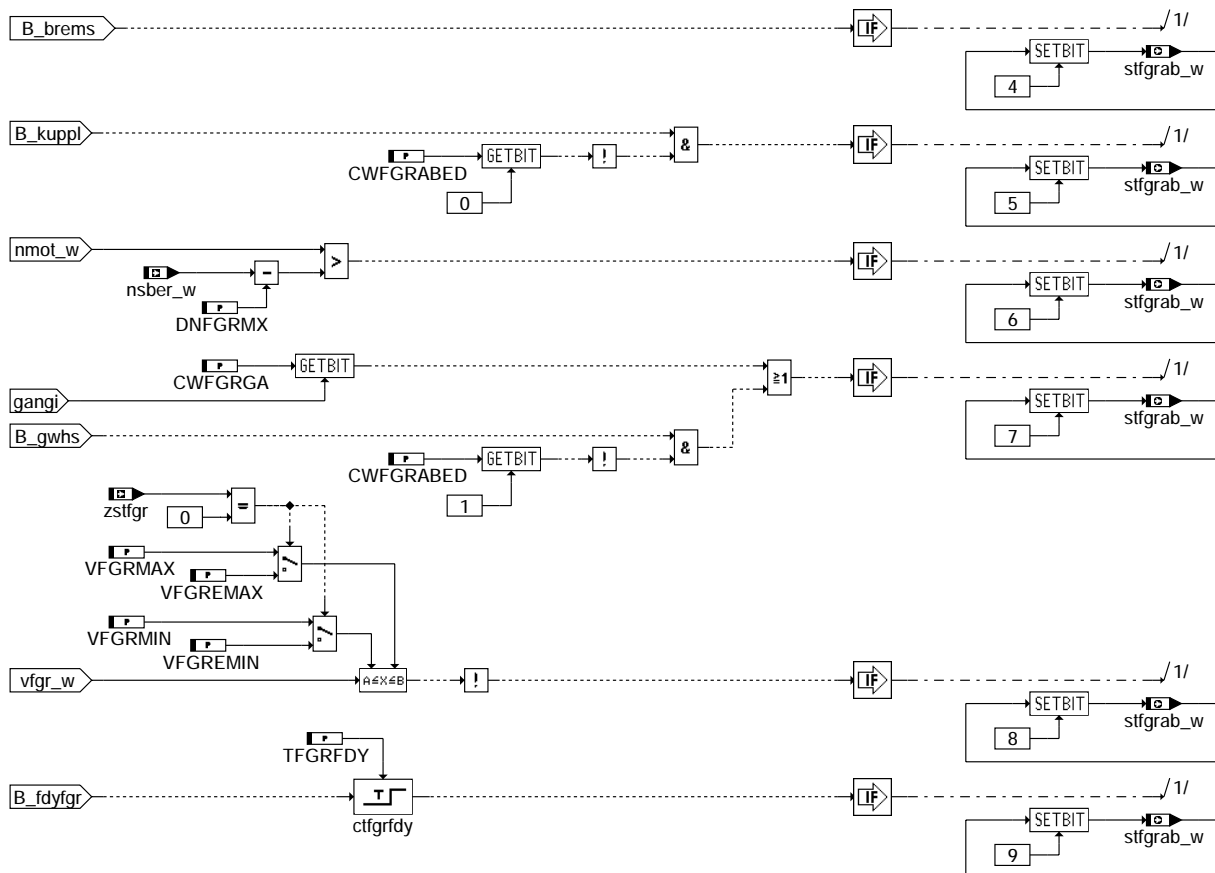


Sub-function ABKOMP: Conditions for comfortable shutdown



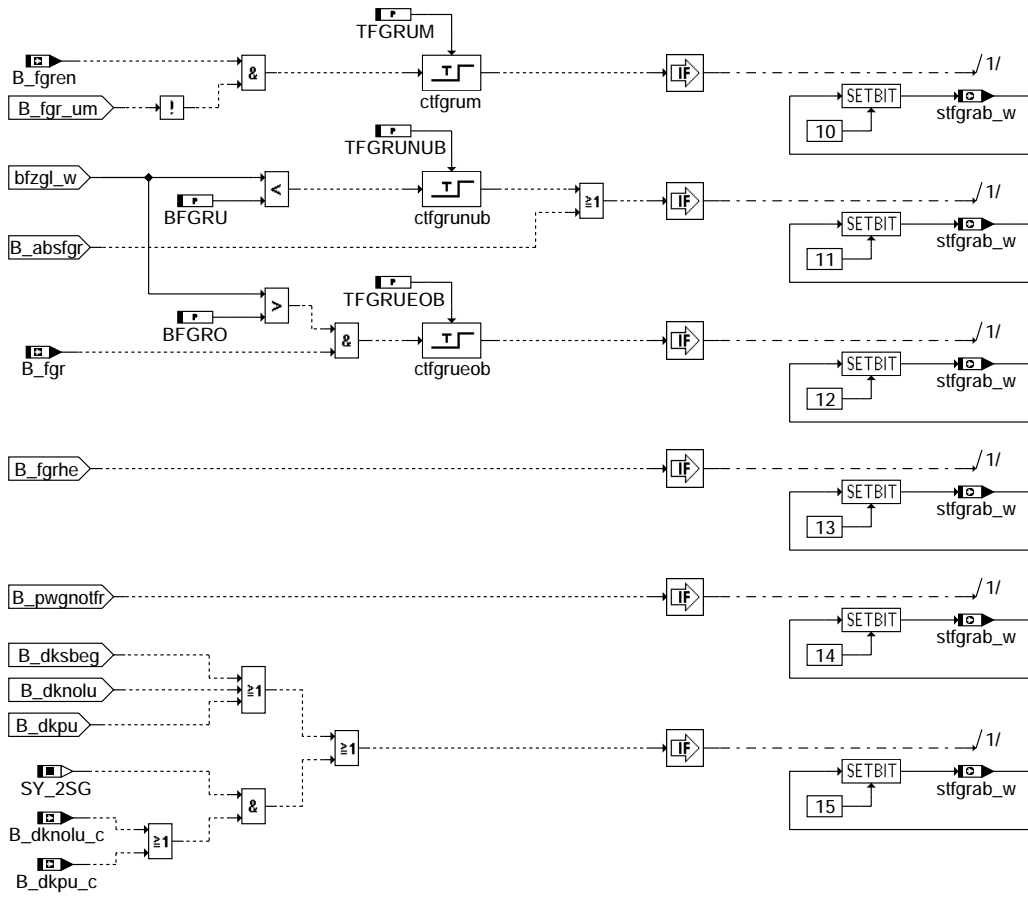
### fgrabed-abkomf

Sub-function ABSCHN: Conditions for quick shutdown



### fgrabed-abschn

Sub-function ABFEHL: Conditions for shutdown in case of a fault



fgrabed-abfehl

### ABK FGRABED 1.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
BFGRO			FW	upper limit for acceleration while cruise control is active
BFGRU			FW	lower limit for acceleration while cruise control is active
CWFGABED			FW	
CWFGGRA			FW	Code word for gear-dependent FGR disable
DNFGRMX			FW	Speed difference from maximum speed for FGR shutdown
DVIVZMX			FW	max. permitted deviation between actual speed and target speed in cruising mode
DVZVIMX			FW	max. permitted deviation between target speed and actual speed in cruising mode
SY_2SG			SYS (REF)	system constant 2 motronic systems
TDVIVZ			FW	tolerance time of high deviation between actual and target velocity
TDVZVI			FW	tolerance time of high deviation between target and actual velocity
TFGRFDY			FW	Tolerance time for interventions by driving dynamics functions during FGR operat
TFGRUEOB			FW	tolerance time for violation of upper acceleration threshold
TFGRUM			FW	Tolerance time for detection of FGR-mode in function monitoring
TFGRUNUB			FW	tolerance time for violation of lower acceleration threshold
VFGREMAX			FW	Maximum FGR switching-on rate
VFGRMIN			FW	Minimum FGR switching-on rate
VFGRMAX			FW	max. permitted velocity during active cruise control
VFGRMIN			FW	Minimum permissible speed during FGR-operation

Variable	Source	Type	Description
BFZGL_W	GGVFZG	EIN	Vehicle acceleration in longitudinal direction
B_ABSFGR		EIN	Condition: ABS braking (as cut-out condition: for FGR)
B_ACC		EIN	Condition: ACC-control unit exists
B_BREMS	GGEGAS	EIN	condition: brake operated
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKNOLU_C		EIN	CAN-Receive-Message: 2.SG has set DK at air limphomeposition
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DKPU_C		EIN	CAN: condition: safety fuel cut-off from 2. motronic
B_DKSBEG	GGDVE	EIN	condition: limiting throttle-valve setpoint value
B_FDVFGR		EIN	Condition: Intervention in driving dynamics function (as cut-out condition: for
B_FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control
B_FGRAT	GGFGRH	EIN	condition: tip-switch off CC lever control
B_FGREN	FGRUE	EIN	condition: cruise control is active (enable)
B_FGRHE	GGFGRH	EIN	condition: CC-lever fault



Variable	Source	Type	Description
B_FGRHSA	GGFGRH	EIN	condition: CC main switch off
B_FGR_UM	UFUE	EIN	CC/ACC torque intervention in function monitoring permitted
B_GWHS	BBGANG	EIN	Condition gear change on manual transmission vehicle
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_PWGNOTFR	GGPED	EIN	FR error reaction pedal-travel sensor limphome
CTDVIVZ_W	FGRABED	LOK	Time counter for exceeding the set speed by more than DVIVZMX
CTDVZVI_W	FGRABED	LOK	Time counter when falling below the set speed by more than DVZVIMX
CTFGRFDY	FGRABED	LOK	Time counter for FGR cut-out for intervention by driving dynamics functions
CTFGRUEOB	FGRABED	LOK	Time counter for exceeding the upper accelerations threshold
CTFGRUM	FGRABED	LOK	Time counter to detect FGR operation in function monitoring
CTFGRUNUB	FGRABED	LOK	Time counter when falling below the lower accelerations threshold
GANGI	SWADAP	EIN	Engaged gear
NMOT_W	SWADAP	EIN	engine speed
NSBER_W		EIN	Calculated requested engine speed of the NMAX controller
STFGRAB_W	FGRABED	AUS	Status word, cut-out conditions, vehicle-speed controller
VFGR_W	GGVFZG	EIN	cruise control vehicle speed
VZIEL_W	FGRFULO	EIN	target velocity cruise control
ZSTFGR	FGRFULO	EIN	Status of vehicle-speed controller

### FW FGRABED 1.30 Fixed Values

Parameter	Value	Description
BFGRO		upper limit for acceleration while cruise control is active
BFGRU		lower limit for acceleration while cruise control is active
CWFGRABED		
CWFGRGA		Code word for gear-dependent FGR disable
DNFGRMX		Speed difference from maximum speed for FGR shutdown
DVIVZMX		max. permitted deviation between actual speed and target speed in cruising mode
DVZVIMX		max. permitted deviation between target speed and actual speed in cruising mode
TDVIVZ		tolerance time of high deviation between actual and target velocity
TDVZVI		tolerance time of high deviation between target and actual velocity
TFGRFDY		Tolerance time for interventions by driving dynamics functions during FGR operation
TFGRUEOB		tolerance time for violation of upper acceleration threshold
TFGRUM		Tolerance time for detection of FGR-mode in function monitoring
TFGRUNUB		tolerance time for violation of lower acceleration threshold
VFGREMAX		Maximum FGR switching-on rate
VFGREMIN		Minimum FGR switching-on rate
VFGRMAX		max. permitted velocity during active cruise control
VFGRMIN		Minimum permissible speed during FGR-operation



## FB FGRABED 1.30 Detailed description of function

The function controls enable and shutdown of the vehicle-speed controller (FGR).

If at least one shutdown condition is fulfilled, then the vehicle-speed controller is deactivated or the controller cannot be activated. There are a number of shutdown conditions that trigger a comfortable shutdown when the vehicle-speed controller is active, whereby the controller output is controlled continuously over a ramp with an applicable running time. The controller output is set immediately to zero for all other shutdown conditions. Also, certain shutdown conditions trigger the stored target speed. This makes any subsequent resumption impossible.

The different shutdown conditions lead to specific bits being set in the status word "Vehicle-speed controller shutdown conditions", stfgrab\_w. The individual shutdown conditions and their assignment to the bits in stfgrab\_w are given in the following table:

bit	Reason for shutdown/No-enable of the FGR	Comfort-shutdown (ramp)	Cancel target speed
0	Main switch off	X	X
1	Tip-switch "off" actuated	X	
2	Actual speed exceeds the set speed during constant driving by more than DVIVZMX for longer than TDVIVZ	X	
3	Actual speed falls below the set speed during constant driving by more than DVZVIMX for longer than TDVZVI	X	
4	Brake pedal operated or fault in the brake-switch diagnosis		
5	Clutch operated		
6	Engine speed greater than maximum engine speed minus DNFGRMX		
7	FGR disabled in current gear selection by CWFGRGA or different gear detected during manual gear-shift		
8	Vehicle speed lower than VFGRMIN or higher than VFGRMAX, respectively lower than VFGREMAX or higher than VFGREMAX if cruise control is not active		
9	Intervention by a vehicle-dynamics function (e.g. ASR, MSR, ESP, EDS) for longer than TFGRFDY		
10	No vehicle-speed controller enable from function monitoring for longer than TFGRUM when FGR is active		
11	Vehicle acceleration less than BFGRU for longer than TFGRUNUB or ABS intervention		
12	Vehicle acceleration greater than BFGRO longer than TFGRUEOB as long as FGR is intervening (no overriding by the driver)		
13	Fault at the operating lever		X
14	Pedal-travel sensor limp-home operation		X
15	Throttle-valve actuator limp-home operation		X

The shutdown conditions are not checked in an ACC system (externally realized vehicle-speed controller with vehicle-to-vehicle ranging).

## APP FGRABED 1.30 Application hint

Conditions to be fulfilled:

VFGREMIN >= Max(VREGLMIN, VFGRMIN)  
VFGREMAX <= Min(VREGLMAX, VFGRMAX)

Configuration with CWFGRABED:

Bit 0 0: Disabling of cruise control if B\_kuppl is set  
1: No Disabling of cruise control if B\_kuppl is set  
  
Bit 1 0: Disabling of cruise control if B\_gwhs is set  
1: No Disabling of cruise control if B\_gwhs is set



## D2CTR 2.20 Diagnosis; system verification counter

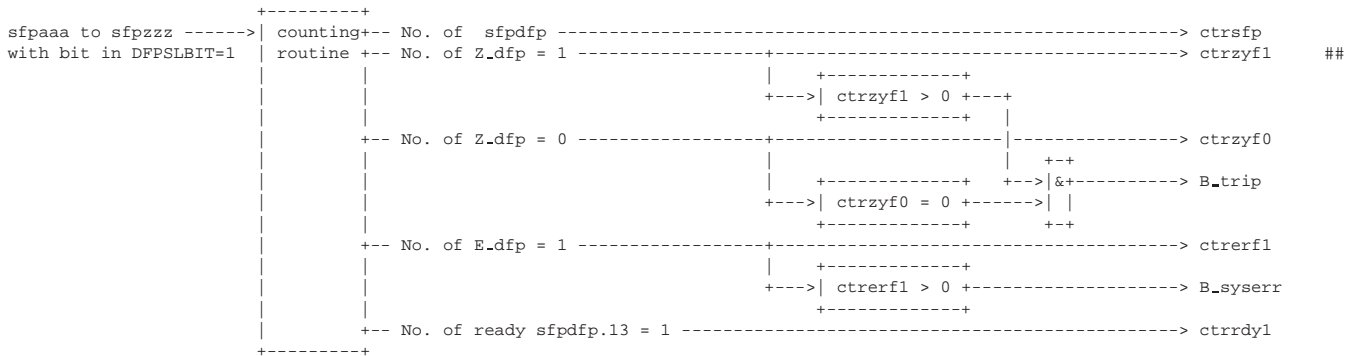
### FDEF D2CTR 2.20 Function definition

The fault code memory statuses `sfpdfp` are searched by means of the selection via the control bits from `DFPSLBIT` from `sfpaaa` to `sfpzzz` (always exclusively) for the following states: ##

1. Number of given `sfpdfp` is written into 'ctr`sfp`'.
2. Number of set cycle flags (`Z_dfp = 1`) is written into 'ctr`zyf1`'.
3. Number of not set cycle flags (`Z_dfp = 0`) is written into 'ctr`zyf0`'.
4. Number of set error flags (`E_dfp = 1`) is written into 'ctr`rerf1`'.
5. Number of set status-ready bits (`sfpdfp.13 = 1`) is written into 'ctr`rdyl`'.

Additionally, the bit `B_trip` is derived from the number of not checked (`Z_dfp = 0`) paths for `ctrzyf0 > 0`.  
From the number of stored fault (`E_dfp = 1`) paths for `ctrerf1 > 0`, the bit `B_syserr` is derived.

The counting routine needs to take place once during each initialization (`C_ini`) after initialization of the `sfpdfp`. Thereafter in the 200ms task or more frequently.



### ABK D2CTR 2.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DFPSLBIT			KWB	Section bits for indication of the activated error paths
Variable	Source		Type	Description
B_SYSERR	D2CTR		AUS	condition for detection of at least one fault ( <code>E_abc</code> ) within the system (coded)
B_TRIP	D2CTR		AUS	flag for fulfilled 'trip'
CTRERF1	D2CTR		AUS	Counter for amount of detected error in the system since <code>pwf</code> (filtered)
CTRRDY1	D2CTR		AUS	Counter of amount of checked error paths in the system since powerfail
CTRSFP	D2CTR		AUS	Counter for amount of error paths in the system
CTRZYF0	D2CTR		AUS	Counter of amount of not checked error paths in the system since engine start
CTRZYF1	D2CTR		AUS	Counter for amount of checked error paths in the system since engine start

### FW D2CTR 2.20 Fixed Values

Parameter	Value	Description
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### FB D2CTR 2.20 Detailed description of function

#### APP D2CTR 2.20 Application hint

Application of the selected fault paths as follows: ##

The amount of the `sfpdfp` to be activated or deactivated needs to be determined program-version dependent from `VS100`. ##

This amount is divided by 16. ##

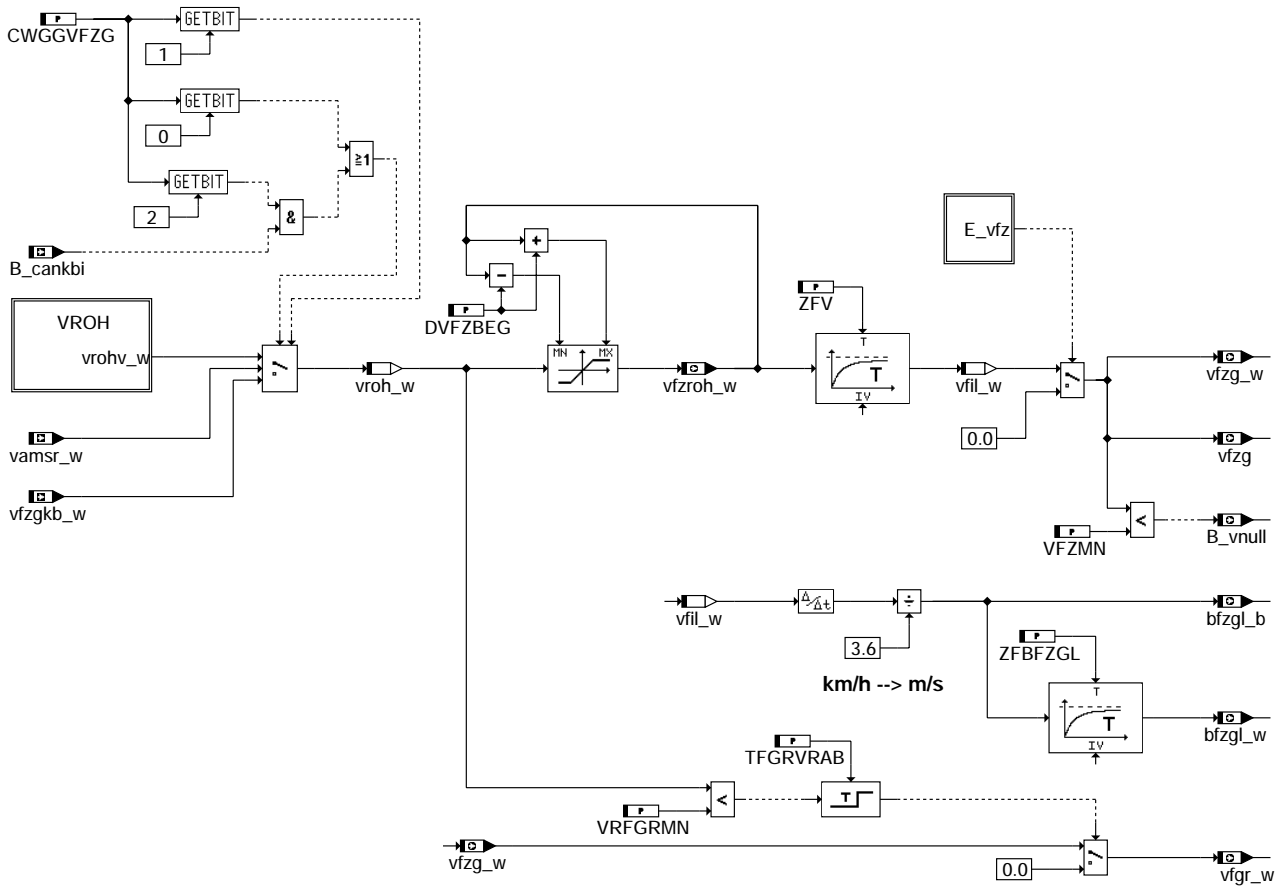
The integer from the division result declares the block to be changed, the division remainder declares the bit to be changed. ##

Example: Number of the `sfptm` is to be 87; -->  $87 / 16 = 5$  remainder 7, so bit 7 in the 5th block needs to be changed. ##



## GGVFZG 14.70 Input signal: vehicle speed

### FDEF GGVFZG 14.70 Function definition

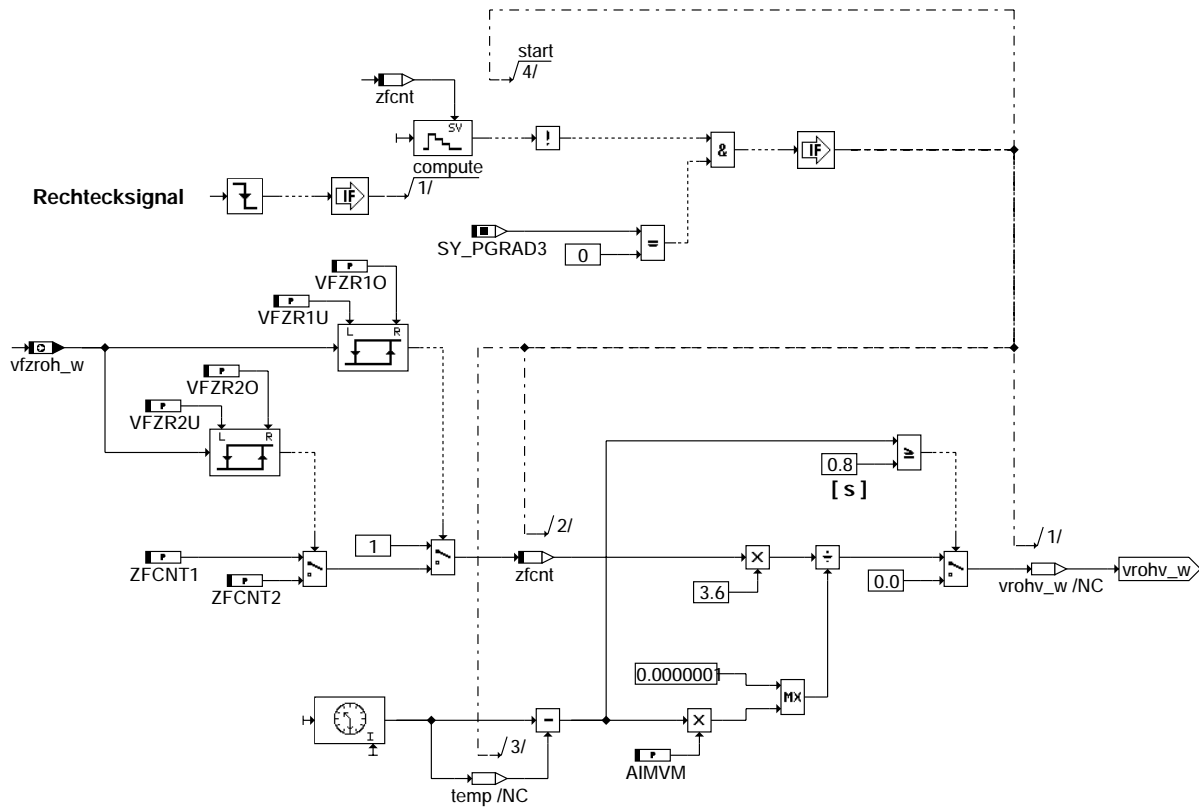


ggvfzg-ggvfzg

ggvfzg-ggvfzg



Sub-function VROH: Calculation of the raw speed



ggvfzg-vroh

### ABK GGVFZG 14.70 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
AIMVM			FW	number of speedpulses for calibration of vehicle speed signal
CWGGVFZG			FW	Code word for %GGVFZG
DVFBEG			FW	Delta speed for change limitation
SY_PGRAD3			SYS (REF)	system constant: kind of the 3. phase signal
TFGRVRAB			FW	FGR: Time speed shutdown by vroh = 0
VFZMN			FW	Detection of driving-standing
VFZR10			FW	Threshold vfzroh_w to switch over zfcnt from 1 to ZFCNT1
VFZR1U			FW	Threshold vfzroh_w to switch over zfcnt from ZFCNT1 to 1
VFZR20			FW	Threshold vfzroh_w to switch over zfcnt from ZFCNT1 to ZFCNT2
VFZR2U			FW	Threshold vfzroh_w to switch over zfcnt from ZFCNT2 to ZFCNT1
VRFGRMN			FW	Lower threshold vroh_w for FGR shutdown by vfzg_w = 0
ZFBFZGL			FW	Filter time constant for 16-bit acceleration signal
ZFCNT1			FW	Number of tooth flanks in the middle speed range
ZFCNT2			FW	Number of tooth flanks in the upper speed range
ZFV			FW	time constant for filter vehicle speed signal

Variable	Source	Type	Description
BFZGL_B	GGVFZG	AUS	Automobile acceleration in the longitudinal direction
BFZGL_W	GGVFZG	AUS	Vehicle acceleration in longitudinal direction
B_CANKBI		EIN	Condition: Combi message detected
B_VNULL	GGVFZG	AUS	condition vehicle at stillstand
DFP_VFZ	GGVFZG	DOK	ECU int. fault path no.: vehicle speed signal
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
VAMSR_W		EIN	Reference speed from ASR/MSR ECU
VFGR_W	GGVFZG	AUS	cruise control vehicle speed
VFIL_W	GGVFZG	LOK	Filtered speed (16-bit)
VFZG	GGVFZG	AUS	vehicle speed (km/h)
VFZGKB_W		EIN	Speed from combi message
VFZG_W	GGVFZG	AUS	Vehicle speed
VFZROH_W	GGVFZG	AUS	vehicle speed output value to scan tool
VROH_W	GGVFZG	LOK	Vehicle speed
ZFCNT	GGVFZG	LOK	Counter of tooth slopes for measurement of vehicle speed



## FW GGVFZG 14.70 Fixed Values

Parameter	Value	Description
AIMVM		number of speedpulses for calibration of vehicle speed signal
CWGGVFZG		Code word for %GGVFZG
DVFBEG		Delta speed for change limitation
TFGRVRAB		FGR: Time speed shutdown by vroh = 0
VFZMN		Detection of driving-standing
VFZR10		Threshold vfzroh_w to switch over zfcnt from 1 to ZFCNT1
VFZR1U		Threshold vfzroh_w to switch over zfcnt from ZFCNT1 to 1
VFZR20		Threshold vfzroh_w to switch over zfcnt from ZFCNT1 to ZFCNT2
VFZR2U		Threshold vfzroh_w to switch over zfcnt from ZFCNT2 to ZFCNT1
VRFRGMN		Lower threshold vroh_w for FGR shutdown by vfzg_w = 0
ZFBFZGL		Filter time constant for 16-bit acceleration signal
ZFCNT1		Number of tooth flanks in the middle speed range
ZFCNT2		Number of tooth flanks in the upper speed range
ZFV		time constant for filter vehicle speed signal

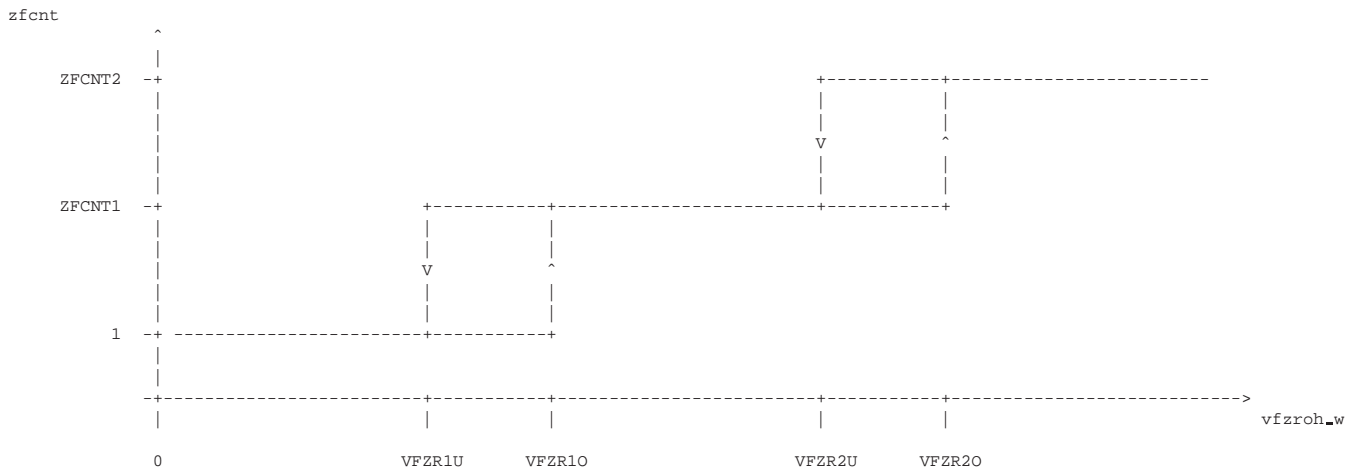
## FB GGVFZG 14.70 Detailed description of function

Purpose of the function is to make the vehicle speed available. This is needed for amongst others, vehicle speed control (FGR), speed limiting (VMAX) and for gear detection in the case of manual transmissions. The possibility is given depending on the configuration, to use the values supplied by the combined instrument or from CAN or to evaluate an interrupt-controlled rectangular-pulse signal. The raw speed obtained in this way is subsequently filtered by a change limitation and a low-pass filter.

Configuration is by means of the code word CWGGVFZG. If bit 0 in CWGGVFZG is set, then the speed from the CAN message Kombi 1 (vfzgb\_w) is used. The same applies when bit 2 in CWGGVFZG is set and B\_cankbi = 1 indicates that the CAN message has been received by the combined instrument. If vfzgb\_w is not used and if bit 1 in CWGGVFZG is set, then the speed from CAN message Bremse 1 (vamsr\_w) is used instead. The hardware signal is otherwise evaluated.

To do this, a time entry is generated interrupt-controlled in each case after a certain number of zfcnt from the negative flanks of the rectangular-pulse signal. The current raw speed is calculated in the 20-ms schedule after each new time entry from the difference between the last two time entries. The parameter AIMVM is also included in the calculations besides zfcnt, the number of pulses to which the measured time period refers. AIMVM describes the number of pulses per travel path, i.e. the number of pulses per wheel revolutions divided by the wheel circumference. The raw speed is set to zero if there has been no time entry made for longer than 0.8 s.

It is principally meaningful in order to eliminate inaccuracies due to tooth-pitch errors at the sensor wheel, to always evaluate a full sensor-wheel revolution, i.e. to set zfcnt to the number of pulses per sensor-wheel revolution. An update of the raw signal is then however so seldom at low speeds that an evaluation is made using zfcnt = 1. The computing task is too large at high speeds if a new time entry has to be made after each revolution by the sensor wheel. This is why zfcnt is set to a whole-number multiple of the number of pulses per sensor-wheel revolution. Switchover is made between the different values for zfcnt is made depending on the speed while employing a hysteresis:



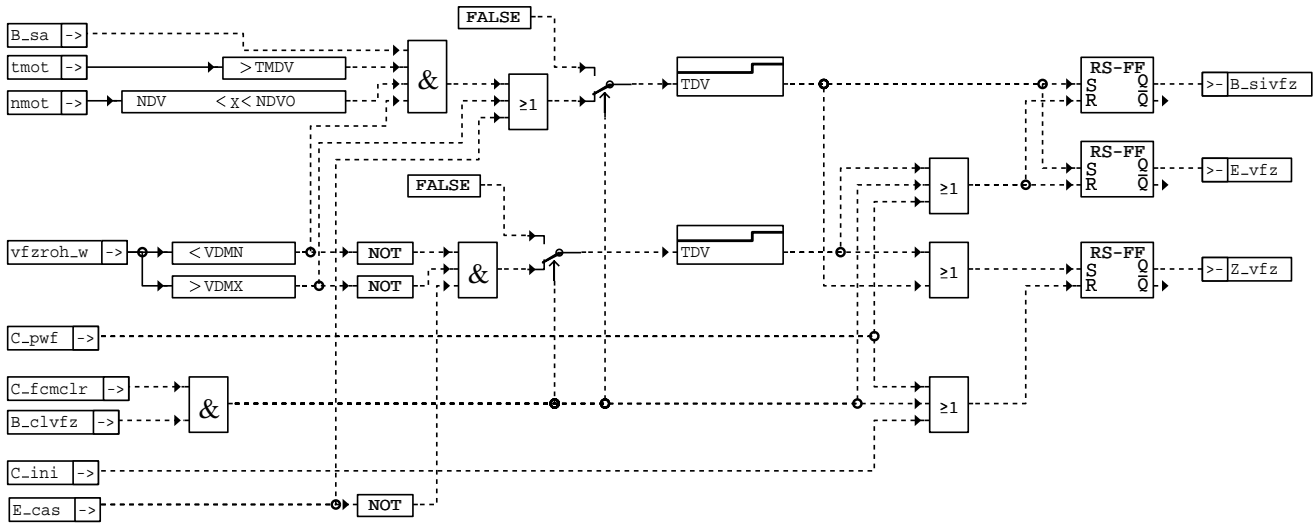
A separate speed signal, vfgr\_w, is made available for the vehicle-speed controller. If the raw signal, vroh\_w, falls below the threshold VRFRGMN for the time TFGRVRAB, then a drop in the signal is assumed and vfgr\_w is set to zero so that the vehicle-speed controller cuts out as soon as possible and there is no unwanted acceleration until the filter output has reached the minimum vehicle-speed controller speed.



## APP GGvFZG 14.70 Application hint

## DVfZ 19.10 Diagnosis; plausibility test vehicle speed

### FDEF DVfZ 19.10 Function definition



### dvfz-dvfz

### ABK DVfZ 19.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
NDV			FW	error detection vehicle speed signal / minimum threshold for engine speed
NDVO			FW	error detection vehicle speed signal, maximum threshold for engine speed
TDV			FW	error detection tachometer signal / time for interrogation
TMDV			FW	motor temperature threshold for release of vehicle speed diagnosis
VDMN			FW	vehicle speed threshold; fault detection vhehicle speed signal
VDMX			FW	vehicle speed threshold; fault detection vfz-signal

Variable	Source	Type	Description
B_CLVfZ		EIN	condition: delete error path VFZ (Vehicle speed)
B_SA	MDRED	EIN	Condition fuel cut-off
B_SIVfZ	DVfZ	AUS	Condition missing signal vehicle speed
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_CAS	DCAS	EIN	errorflag: CAN-interface, timeout ASC
E_VfZ	DVfZ	AUS	Error flag: vehicle speed signal
NMOT	SWADAP	EIN	engine speed
TMOT	SWADAP	EIN	Engine temperature
VFZROH_W	GGvFZG	EIN	vehicle speed output value to scan tool
Z_VfZ	DVfZ	AUS	cycle flag: vehicle speed signal

### FW DVfZ 19.10 Fixed Values

Parameter	Value	Description
NDV		error detection vehicle speed signal / minimum threshold for engine speed
NDVO		error detection vehicle speed signal, maximum threshold for engine speed
TDV		error detection tachometer signal / time for interrogation
TMDV		motor temperature threshold for release of vehicle speed diagnosis
VDMN		vehicle speed threshold; fault detection vhehicle speed signal
VDMX		vehicle speed threshold; fault detection vfz-signal

### FB DVfZ 19.10 Detailed description of function

The function shall enable the diagnosis of the V signal during a FTP75 test also on vehicles with automatic gearbox with "soft" converter. For this the SAS-flag is checked within an engine speed range: if it is fulfilled within the range for a certain amount of time the vehicle must be in motion and thus  $V > VDMN$  must be fulfilled, otherwise the error is stored.

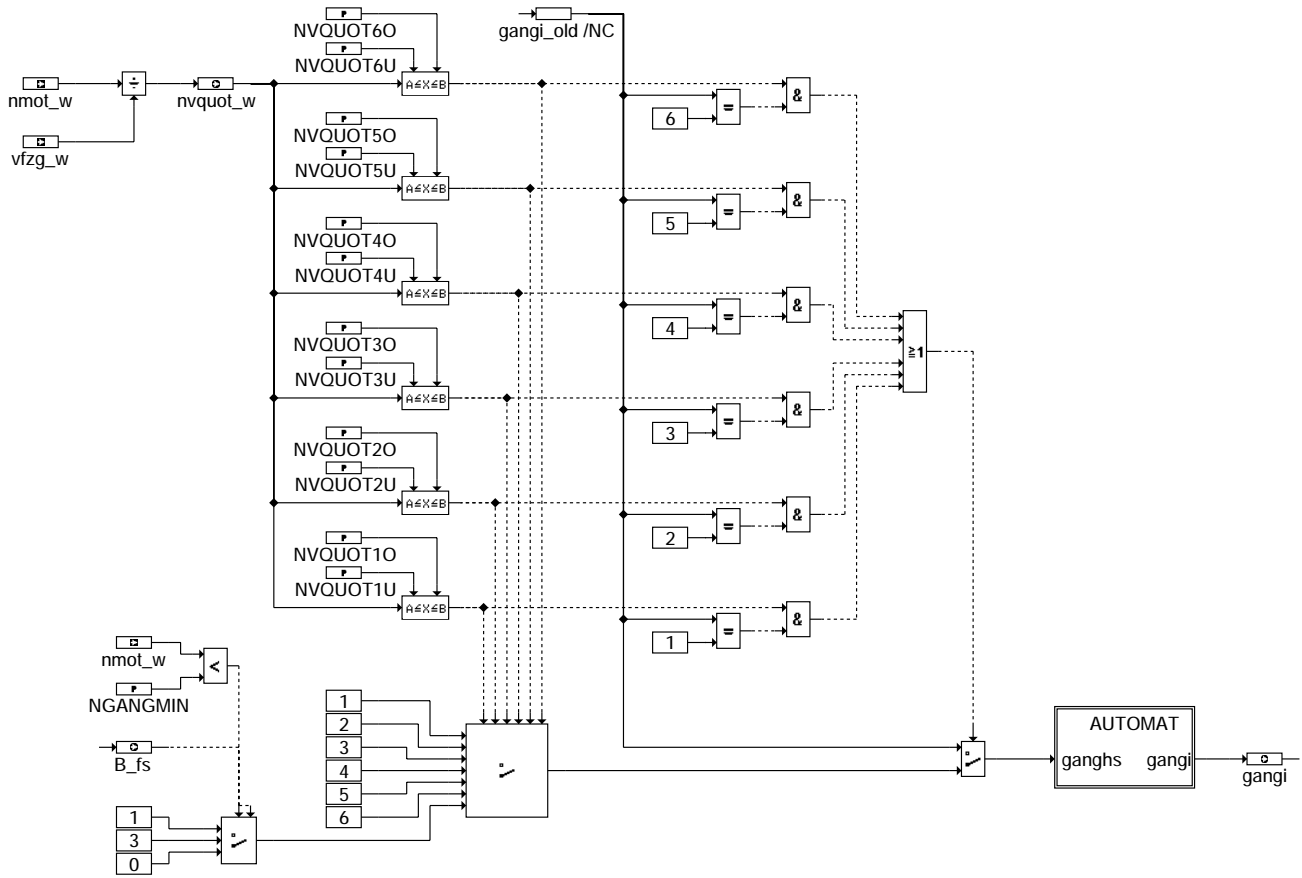
Devault measures: Block the demand adaptation of the LLR  
Block gear detection and thus compression control (see %KOS)  
LLR active, if B\_LL detected  
Deactivate the antijerking function

In case BBNMAX exists: switch-over speed limiter/enginge speed limiter.

## APP DVFZ 19.10 Application hint

## BBGANG 21.10 Detection of actual gear

### FDEF BBGANG 21.10 Function definition



bbgang-bbgang

### ABK BBGANG 21.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
IGESGA	GANGI		KL	Total transmission ratio
NGANGMIN			FW	minimum engine speed for gear detection
NVQUOT10			FW	gear detection n/v 1. gear high
NVQUOT1U			FW	gear detection n/v 1. gear low
NVQUOT20			FW	gear detection n/v 2. gear high
NVQUOT2U			FW	gear detection n/v 2. gear low
NVQUOT30			FW	gear detection n/v 3. gear high
NVQUOT3U			FW	gear detection n/v 3. gear low
NVQUOT40			FW	gear detection n/v 4. gear high
NVQUOT4U			FW	gear detection n/v 4. gear low
NVQUOT50			FW	gear detection n/v 5. gear high
NVQUOT5U			FW	gear detection n/v 5. gear low
NVQUOT60			FW	gear detection n/v 6. gear high
NVQUOT6U			FW	gear detection n/v 6. gear low

Variable	Source	Type	Description
B_AUTGET	PROKON	EIN	condition automatic gearbox
B_CVT	PROKON	EIN	Condition continuously variable transmission
B_FS	BBGANG	AUS	Condition driving state (automatic gear box)
B_GWHS	BBGANG	AUS	Condition gear change on manual transmission vehicle
B_SELESPEED		EIN	condition: car with selespeed
B_TIPPG		EIN	Condition Gear lifter in position "Tippgasse"
B_VNULL	GGVFZG	EIN	condition vehicle at stillstand
DFP_VFZ	BBGANG	DOK	ECU int. fault path no.: vehicle speed signal
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
GANGAUTI		EIN	current gear of automatic gearbox received by CAN
GANGI	BBGANG	AUS	Engaged gear
GANG_KUP	CAN	EIN	current gear received via CAN for F1 transmission
NMOT_W	SWADAP	EIN	engine speed
NVQUOT_W	BBGANG	AUS	quotient engine speed nmot / vehicle speed vfzg

bbgang-bbgang



Variable	Source	Type	Description
S_FFS	SWADAP	EIN	Drive position selected
UEFKTGET		EIN	Transfer function (Mrad/Mkurbelwelle) from transmission control
UEVGES	BBGANG	AUS	Transmission ratio total
VFZG.W	GGVFZG	EIN	Vehicle speed

### FW BBGANG 21.10 Fixed Values

Parameter	Value	Description
NGANGMIN		minimum engine speed for gear detection
NVQUOT1O		gear detection n/v 1. gear high
NVQUOT1U		gear detection n/v 1. gear low
NVQUOT2O		gear detection n/v 2. gear high
NVQUOT2U		gear detection n/v 2. gear low
NVQUOT3O		gear detection n/v 3. gear high
NVQUOT3U		gear detection n/v 3. gear low
NVQUOT4O		gear detection n/v 4. gear high
NVQUOT4U		gear detection n/v 4. gear low
NVQUOT5O		gear detection n/v 5. gear high
NVQUOT5U		gear detection n/v 5. gear low
NVQUOT6O		gear detection n/v 6. gear high
NVQUOT6U		gear detection n/v 6. gear low

### FB BBGANG 21.10 Detailed description of function

### APP BBGANG 21.10 Application hint

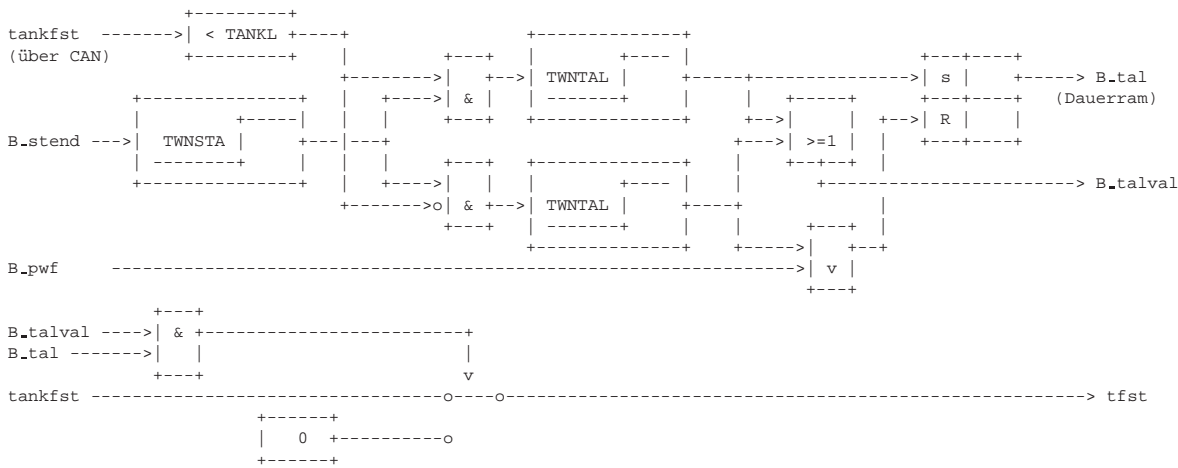
### GGFST 16.10 Sensor variable tank level

### FDEF GGFST 16.10 Function definition

```

+-----+
| Es gibt 2 Fahrzeugkonfigurationen: Signal tankfst über CAN oder fstl über Analogeingang |
| Mit dem Codewort CWGGFST kann die Funktion umgeschaltet werden:                   |
| CWGGFST = 0 --> CAN                                                                |
| CWGGFST = 1 --> Analogsignal                                                       |
+-----+
    
```

Für CWGGFST = 0:







## FB GGFST 16.10 Detailed description of function

Bei einem fast leeren Tank können z.B. Verbrennungsaussetzer durch die ungenügende Kraftstoffversorgung auftreten. Diese Funktion stellt eine Information über den Tankfüllstand für andere Funktionen zur Verfügung.

Je nach Karosserie steht ein Signal Tankfüllstand tankfst über CAN (Codewort CWGGFST = 0) oder ein analoges Signal fstl (codewort CWGGFST = 1) zur Verfügung. Das Analogsignal hat u.U. nur on/off Funktion.

Bei CAN: Unterschreitet tankfst den Schwellwert TANKL, so wird auf Tank leer erkannt.  
Bei Analogsignal: Unterschreitet fstl den Schwellwert FSTRES, so wird auf Tank leer erkannt.

Eine Erste Entprellung kann abhängig von der Zeit nach Motorstart gemacht werden (TWNSTA). Sie ist z.B. nötig, wenn die Reservelampe zu Testzwecken während der Initialisierung angesteuert wird.

Eine zweite Entprellung (TWN TAL) kann ein Toggeln von B\_tal bei stark schwappendem Tank und häufig ein und ausgehender Reservelampe verhindern. Die Entprellung gilt sowohl beim Setzen als auch beim Rücksetzen von B\_tal.

Einen Sonderfall deckt die Entprellzeit TVFSTA ab. Bei einigen Karosserien wird auf dem Analogsignal ein Blinken von 1 Hz übertragen, wenn das Armaturenbrett einen Fehler am Tankgeber erkennt. Mit TVFSTA = 2 s kann in diesem Fall das Signal "Tank leer" erzeugt werden.

Ein weiteres Bit "B\_talval" gibt an, ob B\_tal sicher validiert ist. Es wird erst dann gesetzt, wenn beide Entprellungen durchlaufen sind, also das Flip-Flop sicher gesetzt oder rückgesetzt werden soll.

## APP GGFST 16.10 Application hint

Applikationsvorschlag:

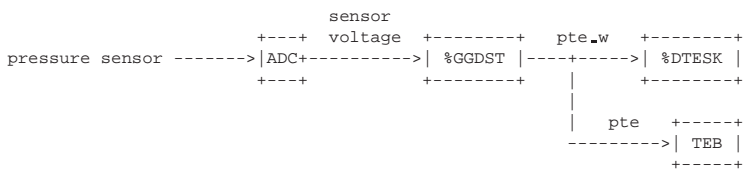
```

TWN TAL:      60 sec
TWN STA:      30 sec
TVF STA:      2 sec (sofern Signal im Fehlerfall mit 1 Hz blinkt)
    
```

## GGDST 3.10 pickup tank pressure sensor

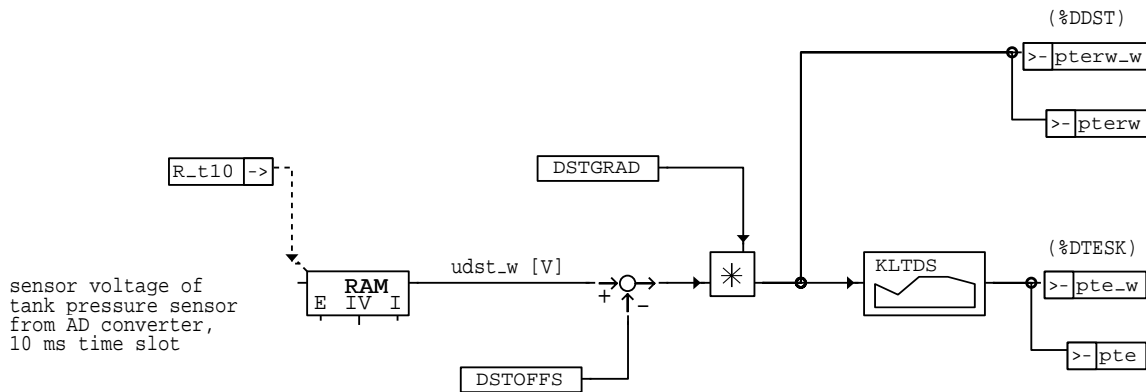
### FDEF GGDST 3.10 Function definition

Overview program environment:



brief description:

The analog signal of a tank pressure sensor is converted via an ADC (scanned in 10 ms time schedule) into an 10 Bit RAM-Cell. The voltage of the pressure sensor udst is converted by an offset DSTOFFS and and gradient DSTGRAD into the tank pressure rough signal pterw\_w (16 Bit) and pterw (8 Bit). The (programmable) characteristic line KLTDS converts the signal into the pressure sensor signal of the DS-T2 (pte, pte\_w).



ggdst-ggdst

ggdst-ggdst





## ABK GGDST 3.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DSTGRAD			FW	gradient for conversion voltage -> pressure of tank pressure sensor
DSTOFFS			FW	offset for conversion voltage -> pressure of tank pressure sensor
KLTD5	PTERW_W		KL	Conversion line for tank pressure sensor DS-T2

Variable	Source	Type	Description
PTE	GGDST	AUS	tank pressure (from ADC)
PTERW	GGDST	AUS	tank pressure rough value (8 bit)
PTERW_W	GGDST	AUS	tank pressure rough value (16 bit)
PTE_W	GGDST	AUS	tank pressure (16 Bit)
R.T10		EIN	Time schedule 10 ms

## FW GGDST 3.10 Fixed Values

Parameter	Value	Description
DSTGRAD		gradient for conversion voltage -> pressure of tank pressure sensor
DSTOFFS		offset for conversion voltage -> pressure of tank pressure sensor

## FB GGDST 3.10 Detailed description of function

### APP GGDST 3.10 Application hint

APPLICATION of the function

The Bosch DS-T2 has got the following physical range: -30.0 hPa...+31.3 hPa (voltage range: 0...5 V). This leads to the conversion formula:

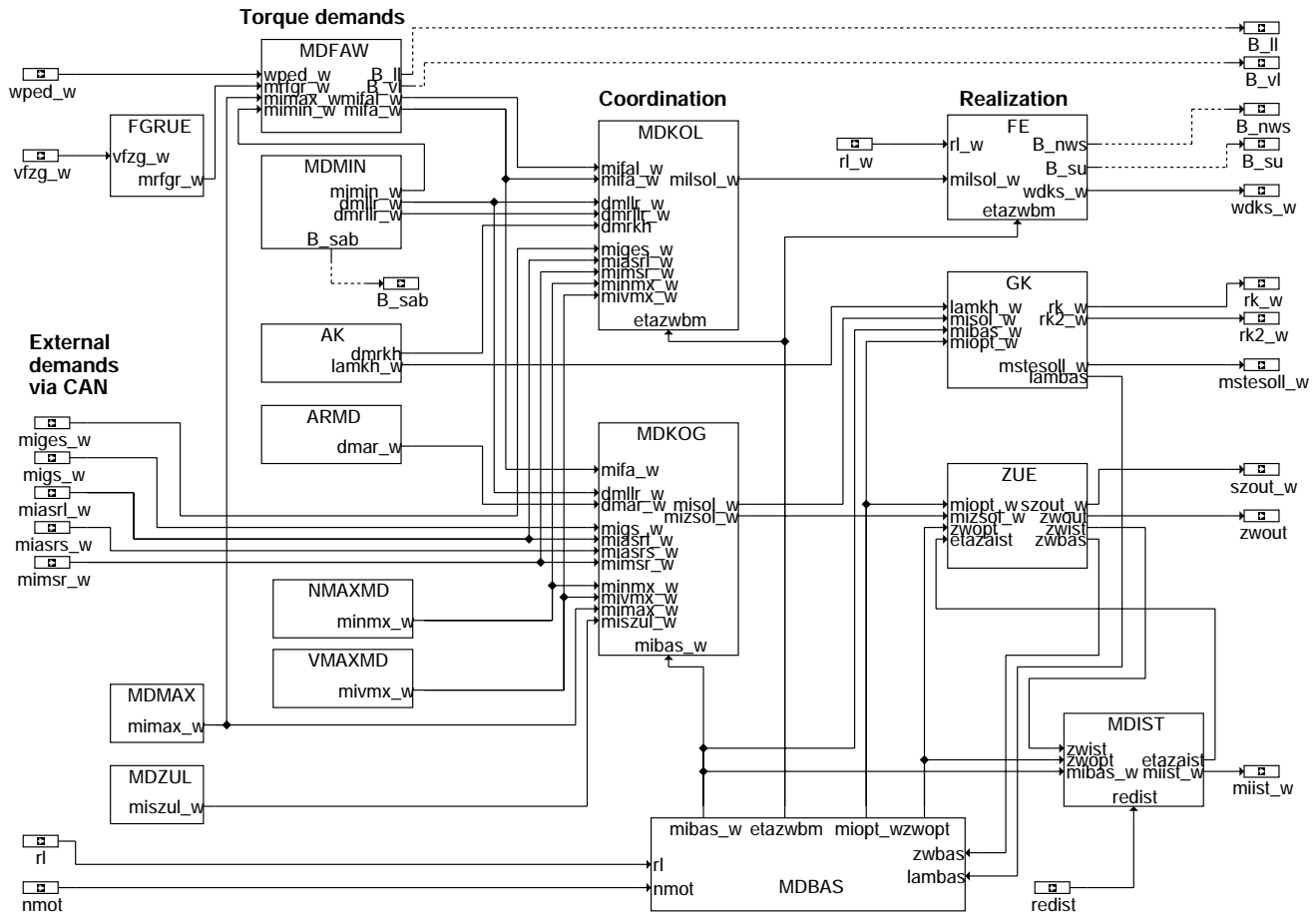
$$U(V) = 2/25 * p(hPa) + 5/2$$

That means for

- DSTGRAD := 25/2
- DSTOFFS := 5/2

## MSF 4.42 Engine control functions

### FDEF MSF 4.42 Function definition



msf-msf

### ABK MSF 4.42 Abbreviations

Variable	Source	Type	Description
B_LL	MSF	AUS	Condition idle
B_NWS	MSF	AUS	Condition camshaft control
B_SAB	MSF	AUS	Condition fuel cut-off requested
B_SU	MSF	AUS	condition intake manifold switch-over
B_VL	MSF	AUS	Condition for wide open throttle
DMAR_W	MSF	AUS	delta torque anti-jerk
DMLLR_W	LLRRM	EIN	desired torque change from the idle speed control (PD-part)
DMRKH	MSF	AUS	torque reserve for catalyzer heating
DMRLLR_W	LLRRM	EIN	torque reserve for idle speed control
ETAZAIST	MSF	AUS	actual cylinder masking effectiveness
ETAZWBM	MDBAS	EIN	mean ignition angle effectiveness of basic ignition angle
LAMBAS	MSF	AUS	basic Lambda
LAMKH_W	MSF	AUS	Lambda engine nominal at catalyst heating (word)
MIASRL_W	SWADAP	EIN	desired indicated torque from ASR for slow intervention
MIASRS_W	SWADAP	EIN	desired indicated torque from ASR for quick intervention
MIBAS_W	MDBAS	EIN	indicated basic torque
MIFAL_W	MSF	AUS	Indicated driver's wish torque for torque coordination cylinder filling
MIFA_W	MSF	AUS	desired indicated engine torque
MIGES_W	SWADAP	EIN	desired indicated torque for transmission protection
MIGS_W	SWADAP	EIN	desired indicated torque form GS for quick intervention
MIIST_W	MSF	AUS	indicated real engine torque
MILSOL_W	MDKOL	EIN	driver torque request for charge
MIMAX_W	MDMAX	EIN	maximum attainable indicated torque
MIMIN_W	MDMIN	EIN	Minimal engine torque
MIMSR_W	SWADAP	EIN	desired indicated torque from MSR
MINMX_W	NMAXMD	EIN	indicated nominal torque for NMAX limiting
MIOPT_W	MDBAS	EIN	optimum indicated torque
MISOL_W	MSF	AUS	indicated resultant nominal torque
MISZUL_W	MDZUL	EIN	maximum permissible indicated torque
MIVMX_W	VMAXMD	EIN	indicated nominal torque for VMAX control
MIZSOL_W	MSF	AUS	indicated resultant nominal torque for ignition angle intervention
MRFGR_W	MSF	AUS	relative torque demand from cruise control



Variable	Source	Type	Description
MSTESOLL_W	MSF	AUS	desired purge mass flow
NMOT	SWADAP	EIN	engine speed
REDIST	BGEVAB	EIN	real cylinder cut-off step
RK2_W	MSF	AUS	relative fuel mass Bank2
RK_W	MSF	AUS	relative fuel mass
RL	SWADAP	EIN	relative air charge
RL_W	EGFE	EIN	relative air charge (Word)
SZOUT_W	MSF	AUS	dwel time
VFZG_W	GGVFZG	EIN	Vehicle speed
WDKS_W	MSF	AUS	desired throttle angle w.r.t. to lower mechanical stop
WPED_W	SWADAP	EIN	normed angle acceleration pedal
ZWBAS	ZUE	EIN	basic ignition angle
ZWIST	ZUE	EIN	real ignition angle
ZWOPT	MSF	AUS	optimal ignition angle
ZWOUT	MSF	AUS	Ignition angle output value

### FW MSF 4.42 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB MSF 4.42 Detailed description of function

The structure of the functions based on the torque comprise a series of function which place requirements on the engine torque: Driver request (MDFAW), minimum torque for start and idling control (MDMIN), exhaust gas/catalyst functions (AK), driving comfort functions such as anti-jerk (ARMD), external requirements from ASR, MSR, transmission control communicated via CAN and limiting functions for engine speed and velocity (NMAXMD, VMAXMD).

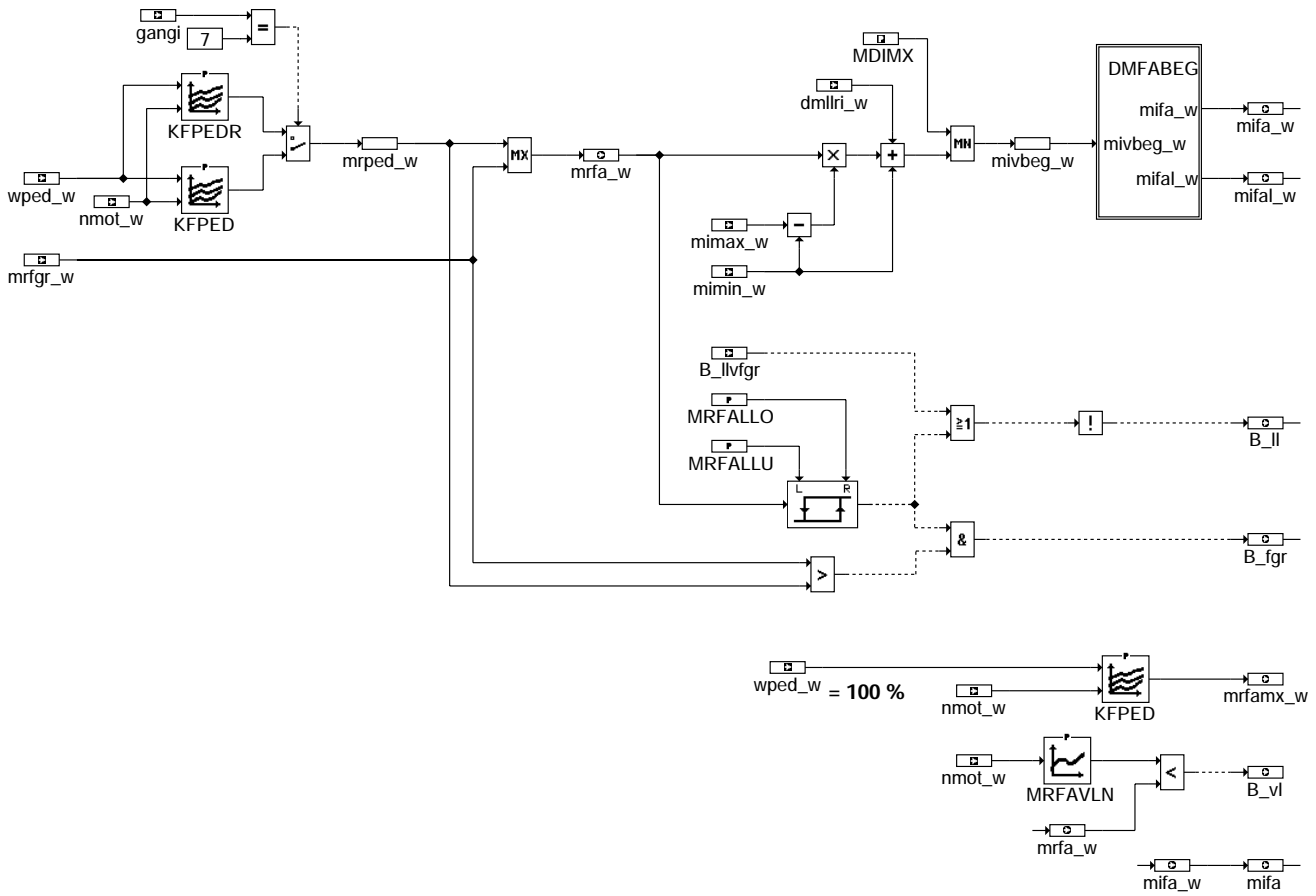
The coordination of these requirements is performed in the functions MDKOL for the air path and in MDKOG as the overall coordination. The selected nominal torques are implemented in the groups FE (filling interventions), GK (mixture control) and ZUE (ignition) in the correcting variables throttle position, injection time and injection angle.

The function MDBAS provides the primary quantities for the torque model, such as optimum torque, optimum ignition angle etc. MDIST calculates the actual internal torque set.

APP MSF 4.42 Application hint

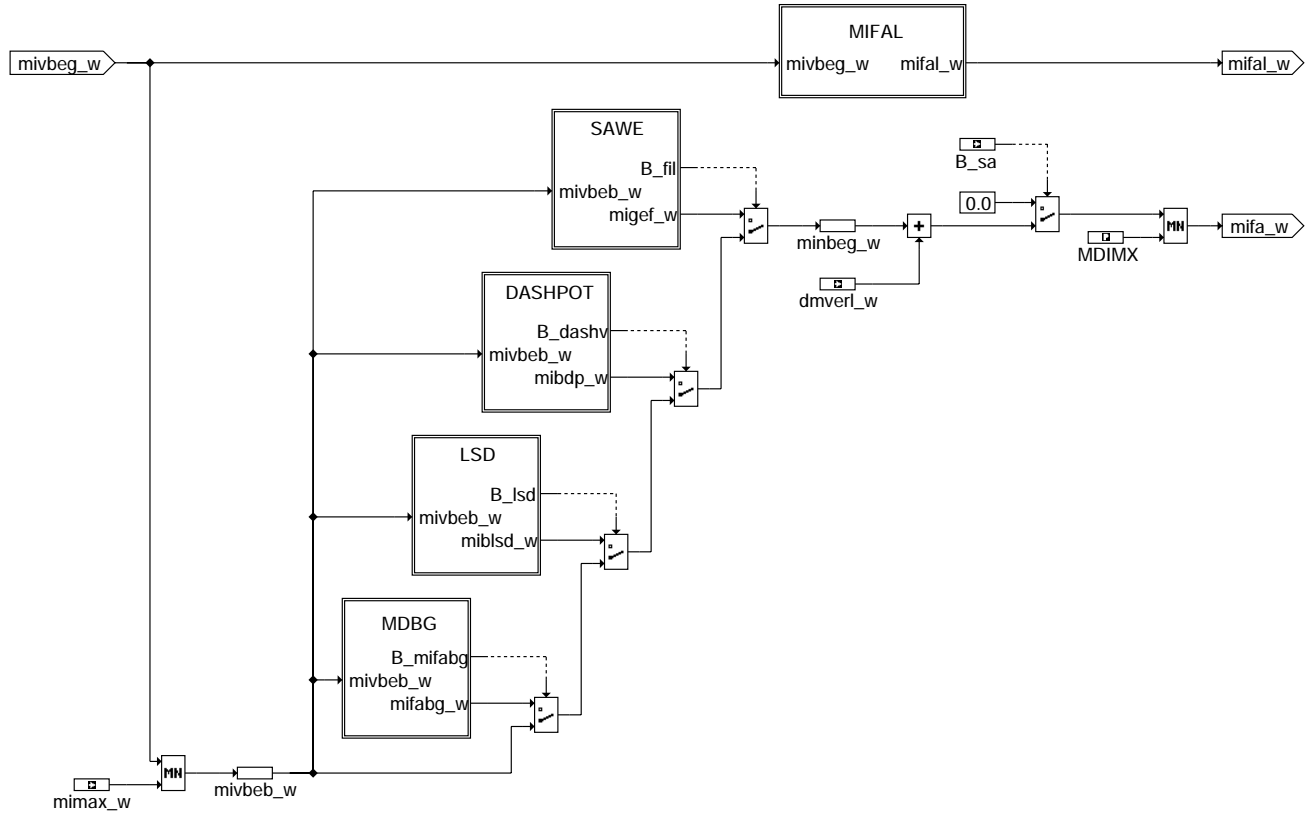
## MDFAW 12.120 Calculation of vehicle-operator demand

### FDEF MDFAW 12.120 Function definition



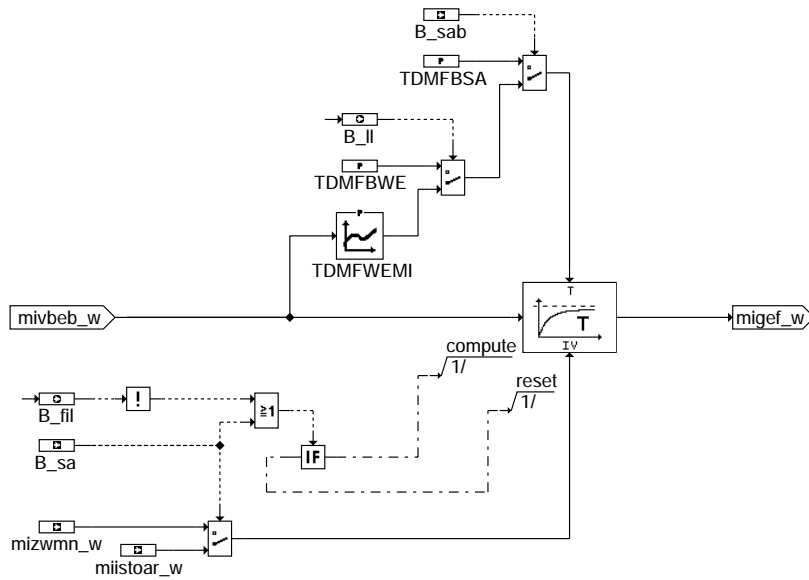
mdfaw-mdfaw

mdfaw-mdfaw



### mdfaw-dmfabeg

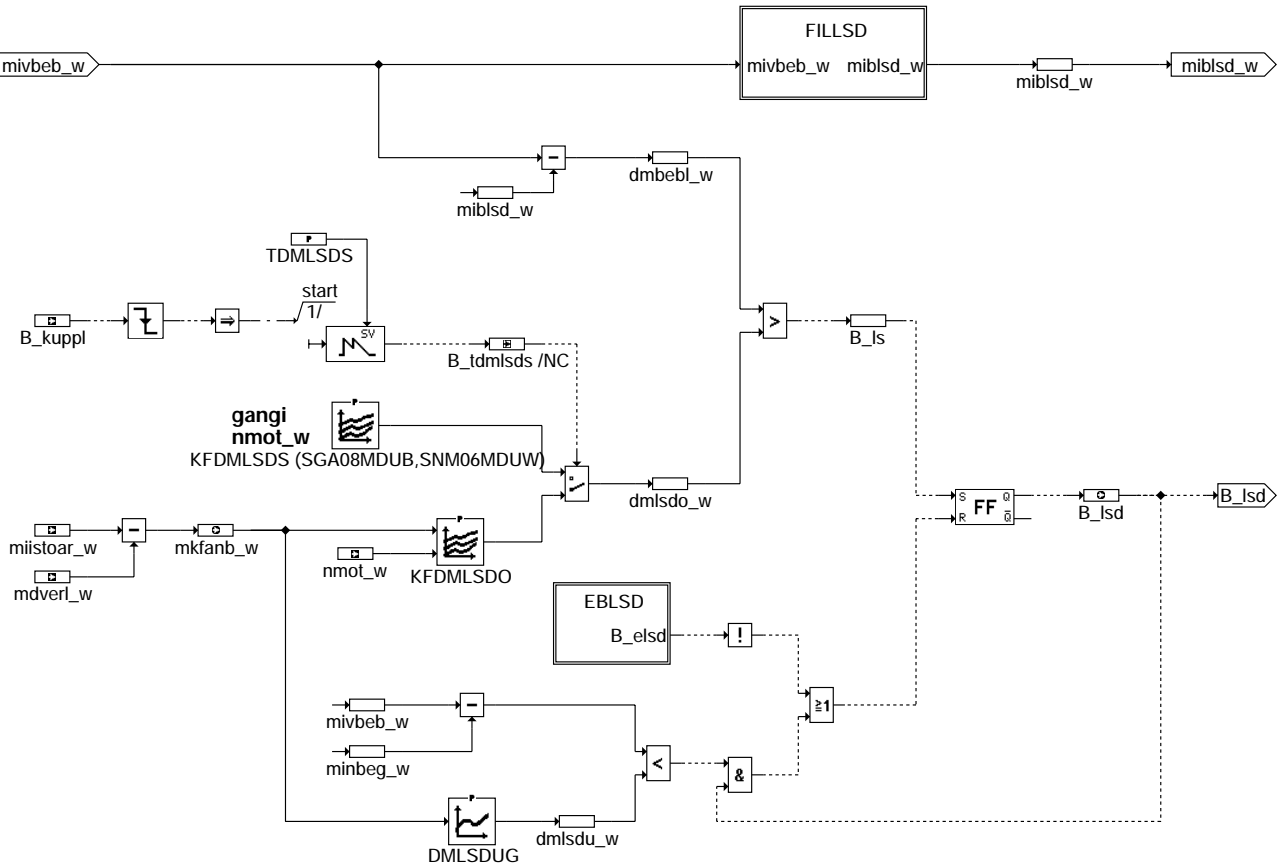
Subfunction DMFABEG: Slope limitation of the torque requested by the driver



### mdfaw-filsawe

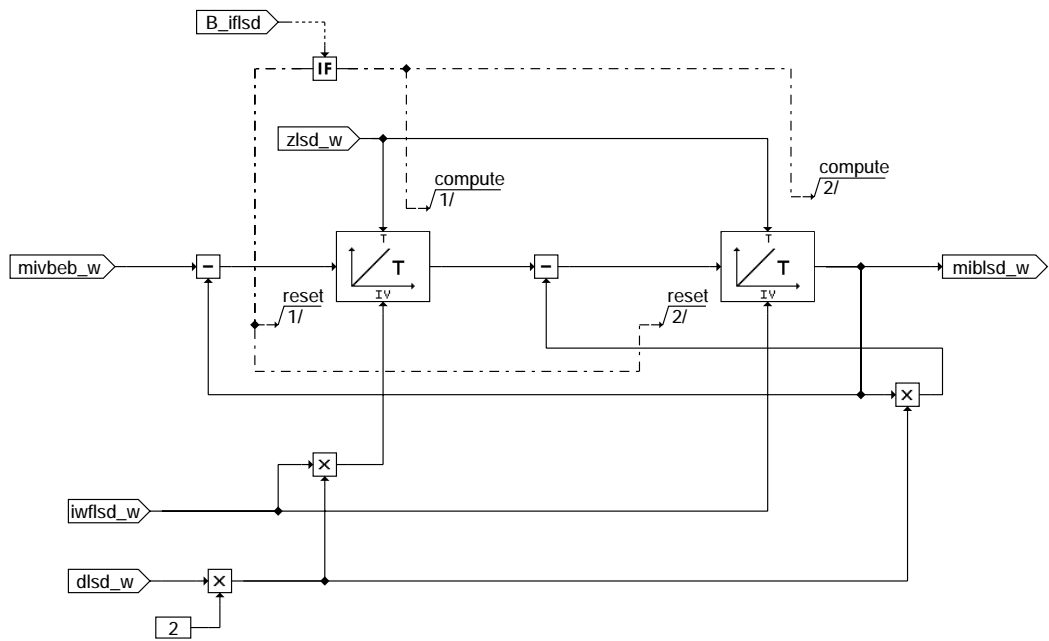


Subfunction DASHPOT: Slope limitation in case of transition from part/full load to coasting



**mdfaw-lsd**

Subfunction LSD: Slope limitation in case of transition from coasting to part/full load



**mdfaw-pt2fil**

Subfunction PT2FIL: PT2 filter for positive slope limitation



## ABK MDFAW 12.120 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWDMFAB			FW	code word software switch for slope limitation
DMDPUG	MKFANB_W		KL	delta torque threshold end of dashpot
DMIFLSD			FW	delta torque for initialization of filter load-shock damping
DMLSUDG	MKFANB_W		KL	Delta torque for finishing positive slope limitation
DMRFAWE			FW	Threshold of the mrafa-gradient for deactivation PT1-filter at fuel cut in
DRLMINDP			FW	Offset to r1min for deactivation of dashpot
FZDASHTM	TMOT		KL	factor for time constant dashpot
KFDLSD	GANGI	NMOT_W	KF	Damping of PT2 filter in positive torque slope limitation
KFDMDPO	MKFANB_W	GANGI	KF	Delta torque for starting negative slope limitation
KFDMLSDO	MKFANB_W	NMOT_W	KF	Delta torque for starting positive slope limitation
KFDMLSOS	GANGI	NMOT_W	KF	delta torque for triggering of load-shock damping after shifting procedure
KFMIFABG	MKFA_W	NMOT_W	KF	delta torque for gradient limitation
KFMIFALS	GANGI	MIFA_W	KF	Indicated driver's request torque for charge path at load-shock damping
KFMILSD	MIVBEB_W	NMOT_W	KF	Initial value for positive torque slope limitation
KFPED	WPED_W	NMOT_W	KF	accelerator pedal characteristic
KFPEDR	WPED_W	NMOT_W	KF	Pedal characteristic for reverse gear (only automatic transmission)
KFZDASH	GANGI	NMOT_W	KF	Time constant for negative torque slope limitation
KFZDASH2	GANGI	NMOT_W	KF	time constant PT1-filter dashpot at low clutch torque
KFZLSD	GANGI	NMOT_W	KF	Time constant for positive torque slope limitation
MDIMX			FW (REF)	maximum limit indicated engine torque
MIFABGMX			FW	maximum value mifa_w for limitation of torque change
MKFADPN	NMOT_W		KL	clutch torque for switch-over dashpot-filter time
MKFADPN1	NMOT_W		KL	clutch torque for switch-over dashpot-fil. time when AC comp. has been enabled
MKMIFABG			FW	clutch torque to activate the torque change limitation
MRFALLO			FW	Upper threshold of relative torque for idle detection
MRFALLU			FW	Lower threshold of relative torque for idle detection
MRFVLN	NMOT_W		KL	Full load detection threshold of the relative driver request
NGFSAWE			FW	Threshold engine speed gradient for disabling filter for transition fuel cut-off
TDMFBSA			FW	Time constant PT1 filter for transition to fuel cut-off
TDMFBWE			FW	Time constant of PT1 filter for transition from fuel cut-off
TDMFWEMI	MIVBEB_W		KL	filter-time constant at hard fuel cut-in
TDMLSOS			FW	time after clutch was applied with changed LSD triggering
TVFSAWE			FW	Time delay until resetting of B_fil
VDASH			FW	Minimum speed for dashpot
VLSD			FW	Minimum speed for load-shock damping

Variable	Source	Type	Description
B_ASR	MDKOG	EIN	condition for ASR active
B_DASH	MDFAW	AUS	condition: limitation of negative torque gradient active
B_DASHV	MDFAW	LOK	condition dashpot delayed
B_DP	MDFAW	LOK	Condition: Start of negative torque slope limitation
B_EDP	MDFAW	LOK	Condition: activation of negative torque slope limitation possible
B_ELSO	MDFAW	LOK	Condition activation of positive torque slope limitation possible
B_FGR	MDFAW	AUS	condition: driver's set engine torque determined by cruise control
B_FIL	MDFAW	AUS	condition: low pass filter for transition to or from fuel cut-off active
B_GWHS	BBGANG	EIN	Condition gear change on manual transmission vehicle
B_JFLSD	MDFAW	LOK	Condition : Initialisation of Antijerking filter
B_KO		EIN	condition AC compressor authorised
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_KUPPLV	GGEGAS	EIN	Condition clutch delayed
B_LL	MDFAW	AUS	Condition idle
B_LLVFGR	FGRUE	EIN	Condition: Idling disabled by FGR
B_LS	MDFAW	LOK	Condition: Start of positive torque slope limitation
B_LSD	MDFAW	AUS	condition: limitation of positive torque gradient active
B_MGBGAKT	MDFAW	LOK	condition torque-gradient limitation active
B_MGBGET		EIN	Condition torque gradient limitation active
B_MIFABG	MDFAW	LOK	condition limitation of mifa
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_SA	MDRED	EIN	Condition fuel cut-off
B_SAB	MSF	EIN	Condition fuel cut-off requested
B_SABFG	BBSAWE	EIN	condition fuel cut-off enable or release
B_STEND	BBSTT	EIN	condition end of start
B_VL	MDFAW	AUS	Condition for wide open throttle
B_VNULL	GGVFZG	EIN	condition vehicle at stillstand
DLSD_W	MDFAW	LOK	Damping of PT2 filter in positive torque slope limitation
DMBEBL_W	MDFAW	LOK	delta torque for triggering of load-shock damping
DMDPO_W	MDFAW	LOK	delta torque start of dashpot
DMDPU_W	MDFAW	LOK	delta torque end of dashpot
DMGBEG_W	MDFAW	LOK	delta torque for gradient limitation
DMLLRI_W	LLRRM	EIN	desired torque change from the idle speed control (I-)
DMLSDO_W	MDFAW	LOK	Delta torque for starting positive torque slope limitation
DMLSDU_W	MDFAW	LOK	Delta torque for finishing positive torque slope limitation
DMVERL_W	MDVER	EIN	Resistant torque after DT1-filter
FZDASH	MDFAW	LOK	factor for time constant dashpot
GANGI	SWADAP	EIN	Engaged gear
IWFLSD_W	MDFAW	LOK	Initial value for filter in positive torque slope limitation
MDGRAD_W		EIN	torque-gradient limitation by transmission
MDVERL_W	MDVER	EIN	Resistant torque of the engine
MIBDP_W	MDFAW	LOK	desired indicated engine torque dashpot
MIBLSD_W	MDFAW	LOK	Limited indicated torque of positive slope limitation
MIFA	MDFAW	AUS	desired indicated engine torque





Variable	Source	Type	Description
MIFABG_W	MDFAW	LOK	gradient-limited desired driver's torque
MIFAL_W	MDFAW	AUS	Indicated driver's wish torque for torque coordination cylinder filling
MIFA_W	MDFAW	AUS	desired indicated engine torque
MIGEF_W	MDFAW	LOK	Filtered indicated torque for transition to or from fuel cut-off
MIISTOAR_W	MDAUTG	EIN	Actual torque without anti-jerk component
MIMAX_W	MDMAX	EIN	maximum attainable indicated torque
MIMIN_W	MDMIN	EIN	Minimal engine torque
MINBEG_W	MDFAW	LOK	Indicated torque requested by driver after slope limitation
MIVBEB_W	MDFAW	LOK	Indicated torque before slope limitation, limited to mimax_w
MIVBEG_W	MDFAW	LOK	Indicated torque requested by driver before slope limitation
MIZWMN_W	MDRED	EIN	indicated engine torque at the latest spark angle
MKFANB_W	MDFAW	AUS	Clutch torque calculated from limited driver's request
MKFA_W	MDFAW	LOK	desired driver's torque (clutch) after change limitation
MRFAMX_W	MDFAW	AUS	Relative torque request by driver maximum value
MRFA_W	MDFAW	AUS	relative driver request torque from cruise control and pedal, =0 in limp-home
MRFRG_W	MSF	EIN	relative torque demand from cruise control
MRPED_W	MDFAW	LOK	Relative torque request by accelerator pedal
NGFIL_W	SWADAP	EIN	filtered engine-speed gradient
NMOT_W	SWADAP	EIN	engine speed
RLMINDP_W	MDFAW	LOK	minimum relative charge for dashpot deactivation
RLMIN_W	MDFUE	EIN	minimum permissible rl
RL_W	EGFE	EIN	relative air charge (Word)
TMOT	SWADAP	EIN	Engine temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)
WPED_W	SWADAP	EIN	normed angle acceleration pedal
ZDASH_W	MDFAW	LOK	time constant for dashpot
ZLSD_W	MDFAW	LOK	Time constant of filter in positive torque slope limitation

### FW MDFAW 12.120 Fixed Values

Parameter	Value	Description
CWDMFAB		code word software switch for slope limitation
DMIFLSD		delta torque for initialization of filter load-shock damping
DMRFAWE		Threshold of the mra-gradient for deactivation PT1-filter at fuel cut in
DRLMINDP		Offset to rlmin for deactivation of dashpot
MIFABGMX		maximum value mifa_w for limitation of torque change
MKMIFABG		clutch torque to activate the torque change limitation
MRFALLO		Upper threshold of relative torque for idle detection
MRFALLU		Lower threshold of relative torque for idle detection
NGFSAWE		Threshold engine speed gradient for disabling filter for transition fuel cut-off
TDMFBSA		Time constant PT1 filter for transition to fuel cut-off
TDMFBWE		Time constant of PT1 filter for transition from fuel cut-off
TDMLSDS		time after clutch was applied with changed LSD triggering
TVFSAWE		Time delay until resetting of B_fil
VDASH		Minimum speed for dashpot
VLSD		Minimum speed for load-shock damping

### FB MDFAW 12.120 Detailed description of function

The function calculates the indicated torque requested by the driver dependent on accelerator pedal position and state of cruise control. The torque coordination air flow and the torque coordination injection/ignition get separate torque requests (mifal\_w and mifa\_w). Additional important inputs are the minimal necessary indicated torque (depending on engine friction and additional consumers like e.g. the A/C-compressor) and the maximal possible indicated torque (depending on engine speed, boost control and ambient air density).

The pedal characteristic is stored in the map KFPED. From accelerator pedal position and engine speed, a factor (relative torque request) in the range of 0 to 2 is generated (mrped\_w). 0 is corresponding to the request of the minimal indicated torque, while 1 is corresponding to the request of the maximal indicated torque. Values between 0 and 1 lead to a linear interpolation. The setting signal of the cruise control is also a relative torque request (mrfrg\_w) that becomes important if it is higher than mrped\_w. In this case, B\_fgr is set.

The condition idle (B\_ll) is set if the relative torque request falls below of a threshold (close to 0). For this calculation, a hysteresis is used. The condition full load (B\_vl) is set if the relative torque request is higher than the engine speed depending threshold MRFVLN.

The task of subfunction DMFABEG is the limitation of torque gradient in order to avoid the jerking caused by transitions between coasting and part/full load with high torque gradient. The limitation takes effect only for the area where the gearbox output torque changes its sign. The limitation is especially necessary for vehicles with manual transmission. The function is only active if several conditions are fulfilled. It can be deactivated by a software switch (CWDMFAB). The low pass serves to avoid discontinuous steps of engine torque at transition to or from fuel cut-off.

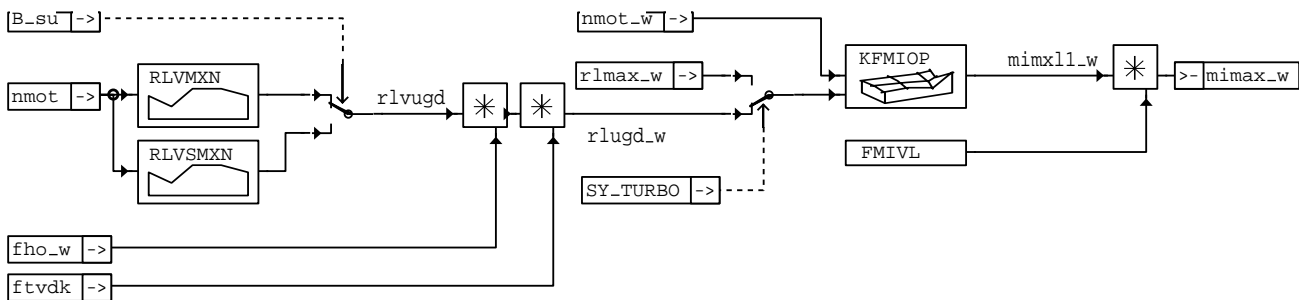
The I-quota of idle speed control and the differential engine torque loss (DT1 filter) are added after the slope limitation in order to avoid steps of the clutch torque when consumers like the A/C-compressor are switched on or off.

### APP MDFAW 12.120 Application hint

- MRFALLO and MRFALLU have to be set close to 0 and with little distance to each other.
- IGEGANG contains at first the transmission ratio for each gear. These values can be slightly changed for a fine application.
- TDMFABEG has to be some seconds (slow filter).
- CWDMFAB serves to switch on or off the slope limitation (bit 0 for positive slope limitation active, bit 1 for negative slope limitation active)
- The slope of the characteristic curves for constant engine speed in KFDMDP must not be higher 1.
- The slope of the characteristic curves for constant engine speed in KFDMLSD must not be less -1.

### MDMAX 1.30 Calculation maximum torque

#### FDEF MDMAX 1.30 Function definition



mdmax-mdmax

#### ABK MDMAX 1.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FMIVL			FW	factor correction maximum torque full load
KFMIOp	NMOT_W	RL_W_KGE	KF	map optimum engine torque
RLVMXN	NMOT		KL	maximum volumetric flow with open throttle valve
RLVSXN	NMOT		KL	maximum volumetric flow with open throttle valve and SU
Variable	Source		Type	Description
B_SU	SU		EIN	condition intake manifold switch-over
FHO_W	BGPU		EIN	correction factor: altitude
FTVDK	SWADAP		EIN	correction factor for temperature upstream of throttle valve
MIMAX_W	MDMAX		AUS	maximum attainable indicated torque
MIMXL1_W	MDMAX		LOK	maximum optimal torque at lambda = 1
NMOT	SWADAP		EIN	engine speed
NMOT_W	SWADAP		EIN	engine speed
RLMAX_W			EIN	maximum attainable charge with turbo
RLUGD_W	MDMAX		LOK	charge under unthrottled condition
RLVUGD	MDMAX		LOK	uncorrected charge in unthrottled condition
SY_TURBO	PROKON		EIN	system constant for turbocharged engine

#### FW MDMAX 1.30 Fixed Values

Parameter	Value	Description
FMIVL		factor correction maximum torque full load

#### FB MDMAX 1.30 Detailed description of function

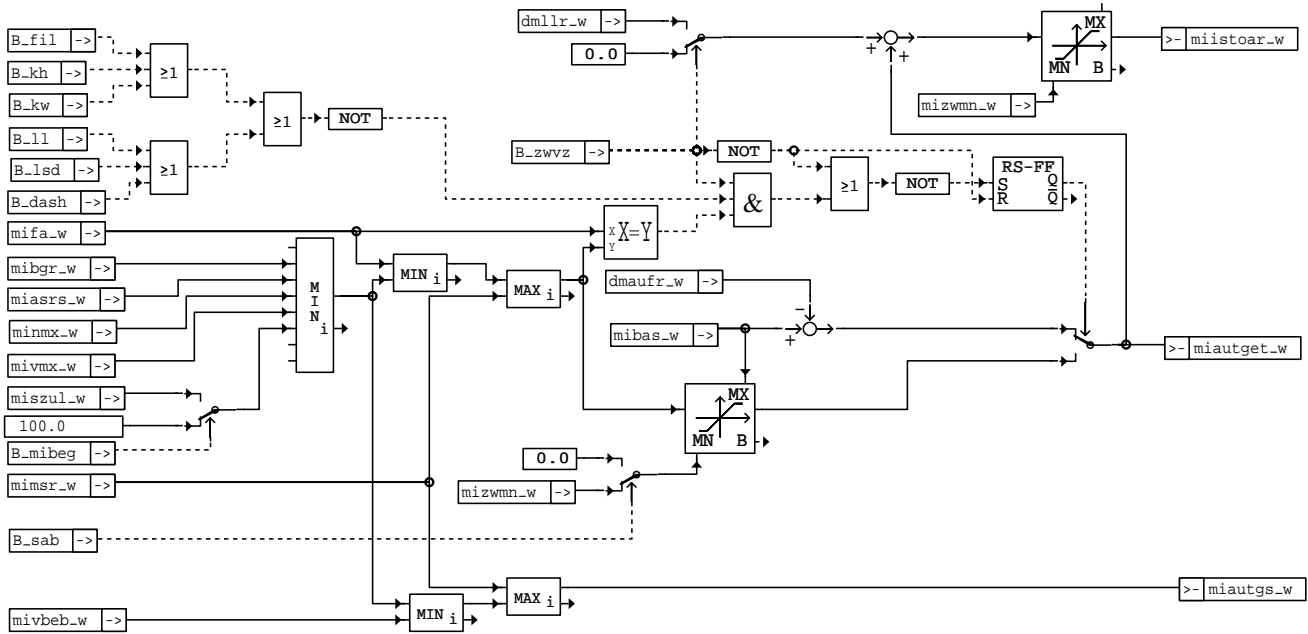
The maximum volumetric charge rlvugd at unthrottled engine operation is taken from the characteristic RLVMXN resp. from the characteristic RLVSXN dependent on the position of the manifold switch-over. Thereafter the conversion into the charge rlvugd\_w is performed by altitude- and temperature-correction. For configurations with turbo charger (SY\_TURBO=1), the maximum charge r\_lmax\_w is predefined directly. The maximum charge now is input variable for the map KFMIOp, in which the optimum torque is stored over speed and charge. The thus obtained torque mimxl1\_w is corrected by the factor FMIVL, which indicates the torque increase at full load and the maximum torque mimax\_w is obtained.

#### APP MDMAX 1.30 Application hint

Determination of the characteristics RLVMXN resp. RLVSXN: Measurement of rl at speed base points and open throttle valve. Conversion into corresponding rlv by division by the factors ftvd\_k and fho\_w (load sensing must already have been adjusted), entry into the respective characteristic. Application hint for the map KFMIOp cf. %MDBAS.

## MDAUTG 2.60 Calculation of torque actual value for gear control

### FDEF MDAUTG 2.60 Function definition



### mdautg-mdautg

For tuning of the transmission a computed engine torque is calculated, for which the influence of the transmission intervention was not taken into account. A "desired torque" as well as an "actual torque" is calculated for the transmission control in this function.

### ABK MDAUTG 2.60 Abbreviations

Variable	Source	Type	Description
B_DASH	MDFAW	EIN	condition: limitation of negative torque gradient active
B_FIL	MDFAW	EIN	condition: low pass filter for transition to or from fuel cut-off active
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_KW	BBKHZ	EIN	Condition catalyst warming
B_LL	MSF	EIN	Condition idle
B_LSD	MDFAW	EIN	condition: limitation of positive torque gradient active
B_MIBEG	MDKOG	EIN	condition torque limit active
B_SAB	MSF	EIN	Condition fuel cut-off requested
B_ZWVZ	MDKOG	EIN	condition for ignition angle intervention of torque interface
DMAUFR_W		EIN	delta torque rise
DMLLR_W	LLRRM	EIN	desired torque change from the idle speed control (PD-part)
MIASRS_W	SWADAP	EIN	desired indicated torque from ASR for quick intervention
MIAUTGET_W	MDAUTG	AUS	Engine torque without torque intervention
MIAUTGS_W	MDAUTG	AUS	Target engine torque without transmission intervention
MIBAS_W	MDBAS	EIN	indicated basic torque
MIBGR_W	MDBGGR	EIN	Indicated desired torque for gear-dependent limiting of the clutch torque
MIFA_W	MSF	EIN	desired indicated engine torque
MIISTOAR_W	MDAUTG	AUS	Actual torque without anti-jerk component
MIMSR_W	SWADAP	EIN	desired indicated torque from MSR
MINMX_W	NMAXMD	EIN	indicated nominal torque for NMAX limiting
MISZUL_W	MDZUL	EIN	maximum permissible indicated torque
MIVBEB_W		EIN	Indicated torque before slope limitation, limited to mimax_w
MIVMX_W	VMAXMD	EIN	indicated nominal torque for VMAX control
MIZWMN_W	MDRED	EIN	indicated engine torque at the latest spark angle

### FW MDAUTG 2.60 Fixed Values

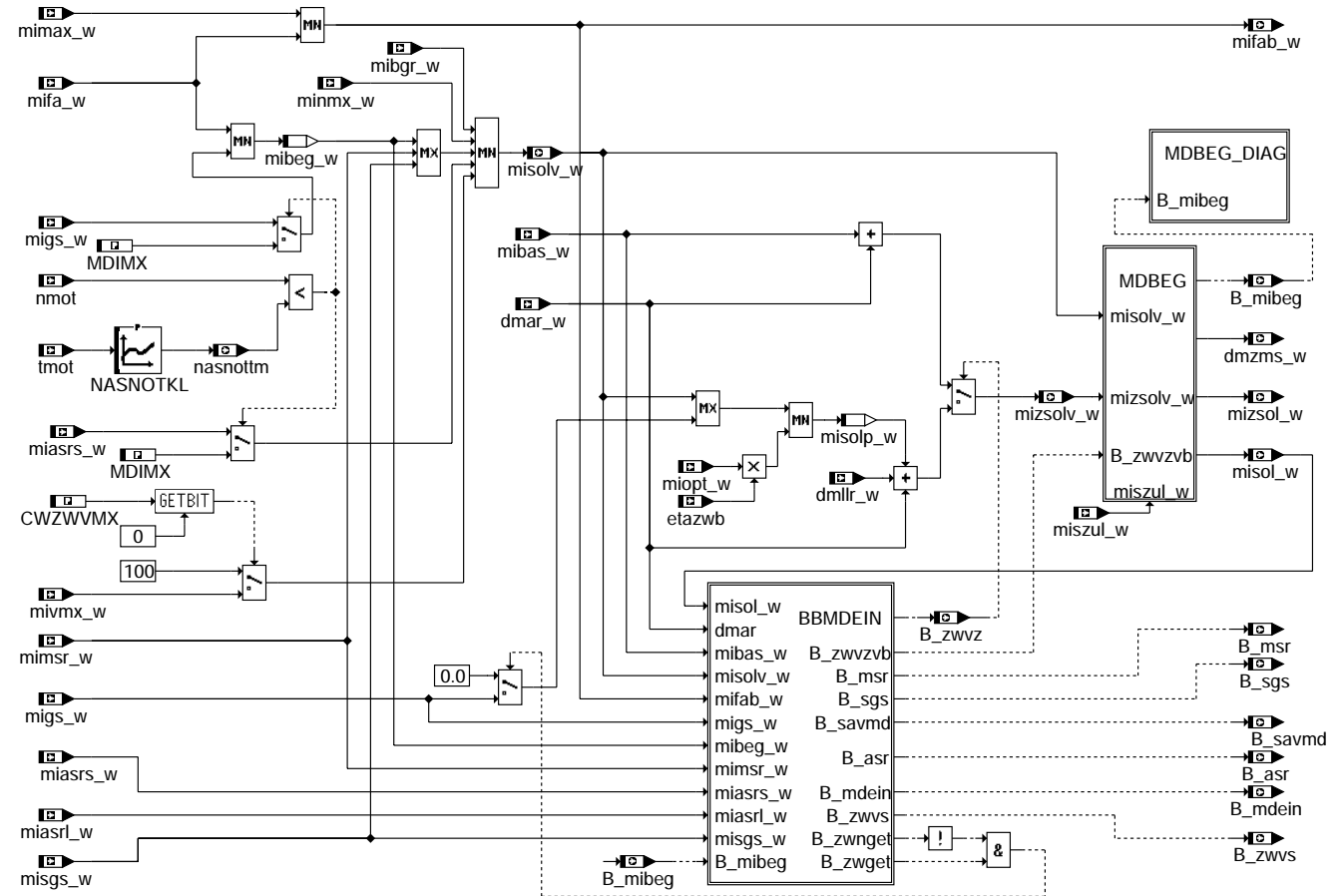
Parameter	Value	Description
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## FB MDAUTG 2.60 Detailed description of function

### APP MDAUTG 2.60 Application hint

## MDKOG 1.190 Coordination torque intervention

### FDEF MDKOG 1.190 Function definition

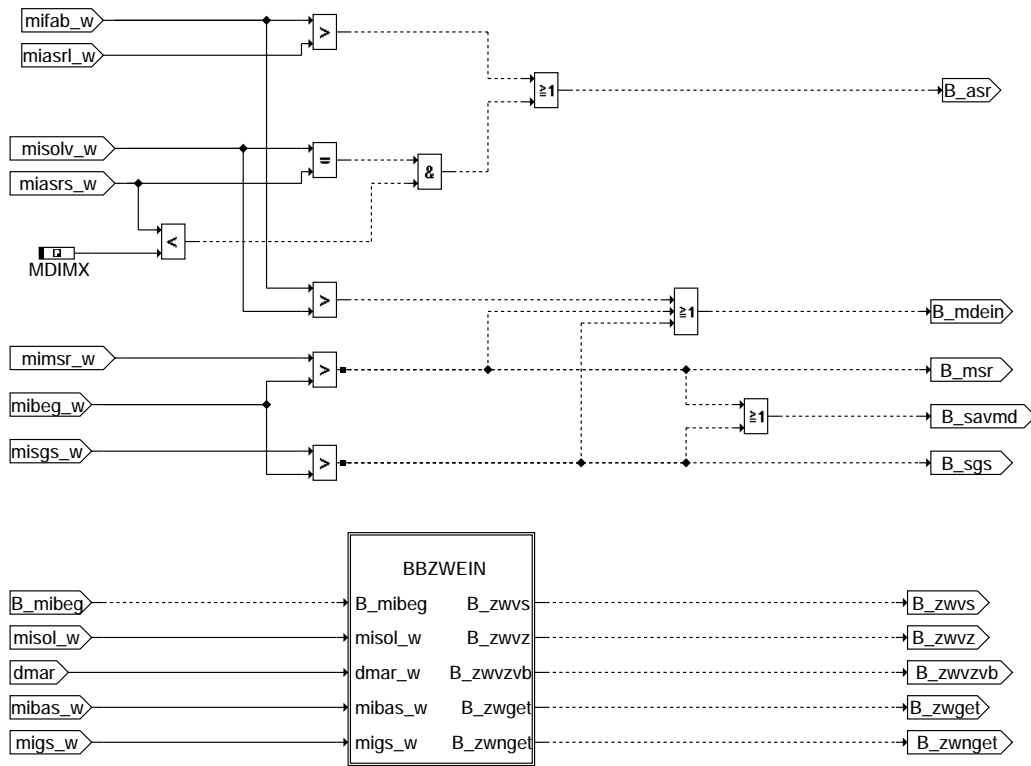


mdkog-main

mdkog-main

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Subfunction BBMDEIN: Conditions torque intervention active

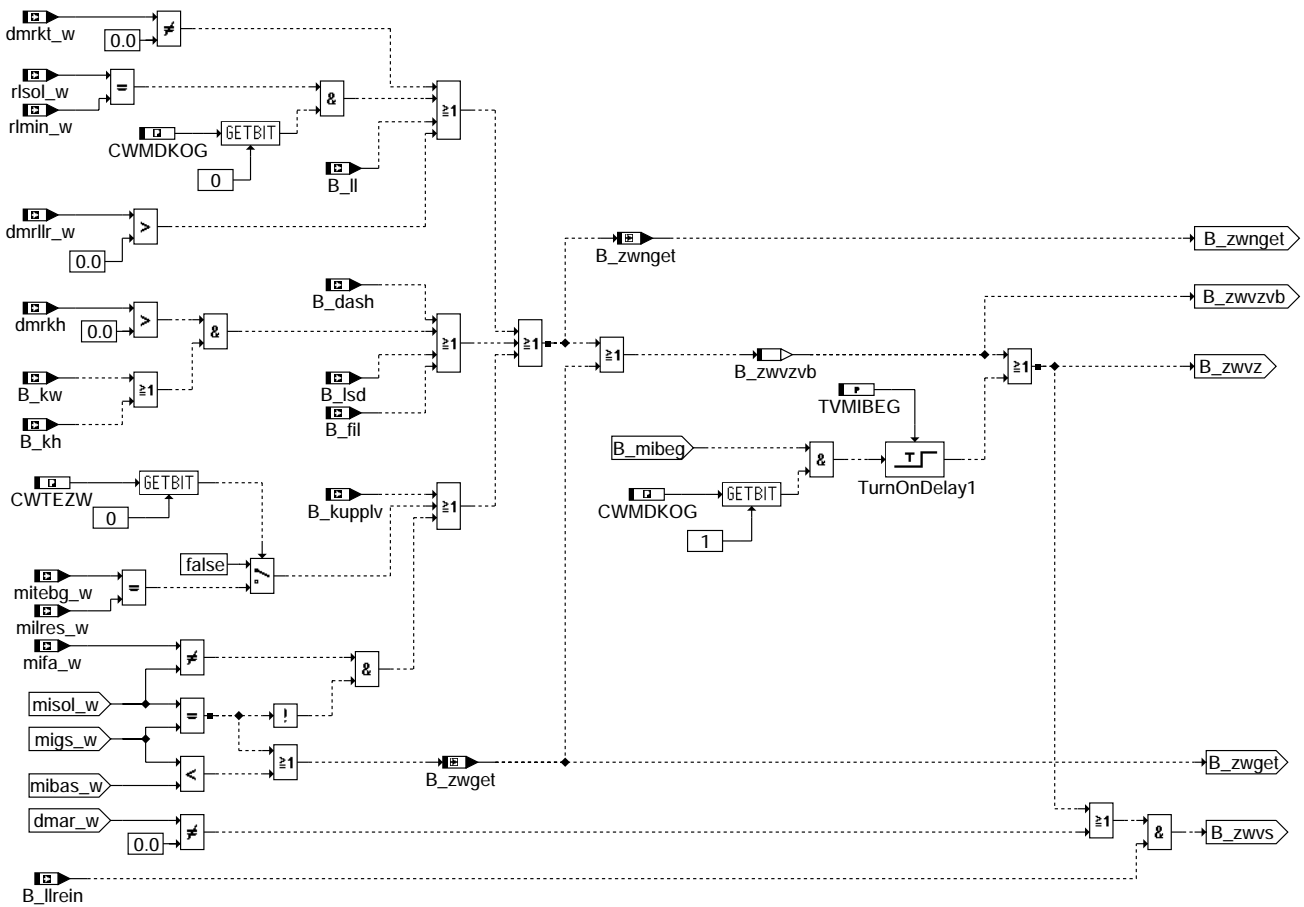


mdkog-bbmdein

mdkog-bbmdein



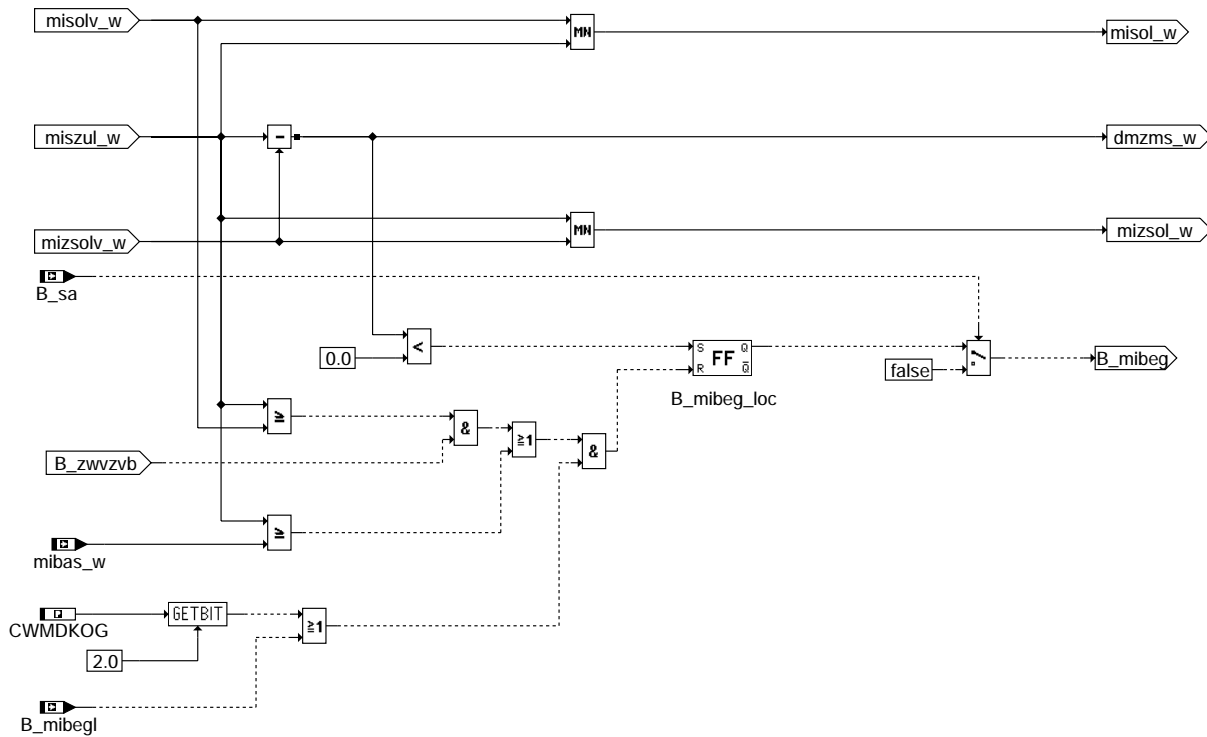
Subfunction BBZWEIN: Conditions for ignition angle intervention active



mdkog-bbzwein

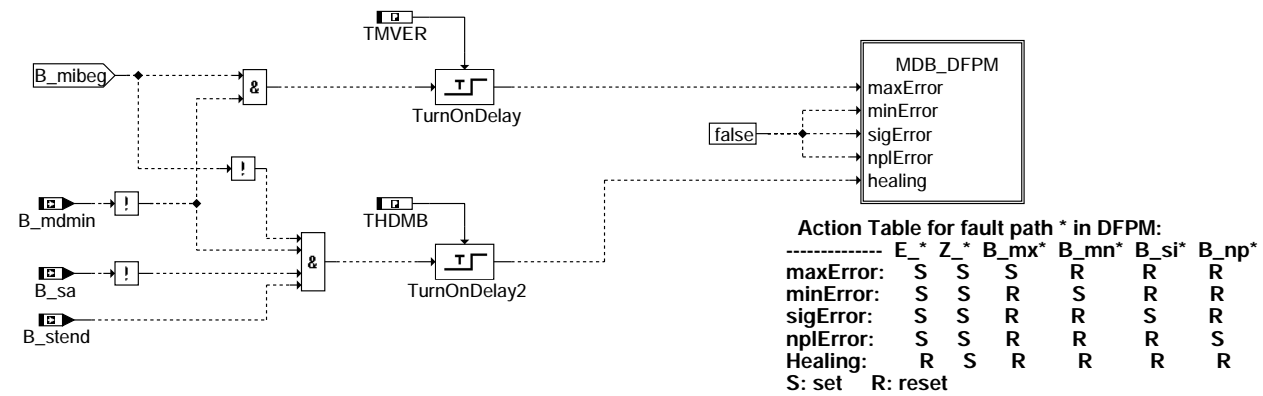
mdkog-bbzwein

Subfunction MDBEG: Limitation of indicated torque



mdkog-mdbeg

Subfunction MDBEG\_DIAG: Connection of torque limitation with diagnosis



Reset of the Error- and Cyclebits in %DFPM  
During "Clear fault code memory" (fcmclr):  
IF B\_clmdb = True then  
Reset TurnOnDelay



mdkog-mdbeg-diag



## ABK MDKOG 1.190 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCMDB	BLOKNR		KL	Code word CARB: Target torque limiter
CDKMDB			FW	code word customer: Target torque limiter
CDTMDB			FW	code word tester: Target torque limiter
CLAMDB			FW	error class: Target torque limiter
CWMDKOG			FW (REF)	code word MDKOG: ignition timing adjusted to retard for limiting vacuum
CWTEZW			FW (REF)	code word: ignition angle intervention at test of canister-purge valve
CWZWVMX			FW (REF)	code word: ignition-timing intervention for VMAX limiting
FFTMDB	BLOKNR		KL	freeze frame table: Target torque limiter
MDIMX			FW (REF)	maximum limit indicated engine torque
NASNOTKL	TMOT		KL	characteristic line rotational speed against engine stall
THDMB			FW (REF)	dwelt time, healing for fault path for permanent torque limitation
TMVER			FW (REF)	Debounce time: ETC torque limitation is activ for a longer time
TSFMDB			FW	fault active time: Target torque limiter
TVMIBEG			FW	debounce time for activation of ignition intervention during torque limitation
Variable	Source		Type	Description
BLOKNR			EIN	DAMOS source for block number
B_ASR	MDKOG		AUS	condition for ASR active
B_BEMDB	MDKOG		AUS	condition MDB request
B_BKMDB	MDKOG		AUS	Condition: ETC-torque limitation is active
B_CLMDB			EIN	Flag for clearance: ETC torque limitation is activ
B_DASH	MDFAW		EIN	condition: limitation of negative torque gradient active
B_FIL	MDFAW		EIN	condition: low pass filter for transition to or from fuel cut-off active
B_FTMDB	MDKOG		AUS	Condition fault entry by tester for MDB
B_KH	BBKHZ		EIN	condition catalyst heating activated
B_KUPPLV	GGEGAS		EIN	Condition clutch delayed
B_KW	BBKHZ		EIN	Condition catalyst warming
B_LL	MSF		EIN	Condition idle
B_LLEIN	LLRMD		EIN	Condition idle speed control is active
B_LSD	MDFAW		EIN	condition: limitation of positive torque gradient active
B_MDEIN	MDKOG		AUS	Condition actions on the torque are active
B_MDMIN	SWADAP		EIN	Condition minimal possible indicated torque reached
B_MIBEG	MDKOG		AUS	condition torque limit active
B_MIBEGL	MDKOL		EIN	condition torque limitation charge path active
B_MNMDB	MDKOG		AUS	Fault type min.: ETC torque limitation is active
B_MSR	MDKOG		AUS	Condition MSR
B_MXMDB	MDKOG		AUS	Fault type max.: ETC torque limitation is activ for a longer time
B_NPMDB	MDKOG		AUS	not plausible error: ETC torque limitation is activ
B_SA	MDRED		EIN	Condition fuel cut-off
B_SAVMD	MDKOG		AUS	flag: fuel cut-off prohibition because of torque request
B_SGS	MDKOG		AUS	torque intervention for engine speed synchr. during gear shift
B_SIMDB	MDKOG		AUS	error type: ETC torque limitation is active
B_STEND	BBSTT		EIN	condition end of start
B_ZWGET	MDKOG		LOK	ignition angle intervention by gearbox
B_ZWNGET	MDKOG		LOK	ignition angle intervention not by gearbox
B_ZWVS	MDKOG		AUS	condition for fast external ignition angle intervention of torque interface
B_ZWVZ	MDKOG		AUS	condition for ignition angle intervention of torque interface
B_ZWVZVB	MDKOG		LOK	condition for ignition angle intervention of torque interface before limitation
DFP_MDB	MDKOG		DOK	ECU int. fault path no.: ETC torque limitation is active
DMAR_W	MSF		EIN	delta torque anti-jerk
DMLLR_W	LLRRM		EIN	desired torque change from the idle speed control (PD-part)
DMRKH	KHMD		EIN	torque reserve for catalyzer heating
DMRKT_W	MDTRIP		EIN	Torque reserve during quicktest
DMRLLR_W	LLRMR		EIN	torque reserve for idle speed control
DMZMS_W	MDKOG		AUS	difference between internal nominal engine torque and permissible nominal torque
ETAZWB	MDBAS		EIN	ignition angle effectiveness of basic ignition angle
E_MDB	MDKOG		AUS	error flag: ETC torque limitation is active
MIASRL_W	SWADAP		EIN	desired indicated torque from ASR for slow intervention
MIASRS_W	SWADAP		EIN	desired indicated torque from ASR for quick intervention
MIBAS_W	MDBAS		EIN	indicated basic torque
MIBEG_W	MDKOG		LOK	limit torque
MIBGR_W	MDBGRG		EIN	Indicated desired torque for gear-dependent limiting of the clutch torque
MIFAB_W	MDKOG		AUS	limited desired indicated engine torque
MIFA_W	MSF		EIN	desired indicated engine torque
MIGS_W	SWADAP		EIN	desired indicated torque form GS for quick intervention
MILRES_W	MDKOL		EIN	torque request for air path including all torque reserves
MIMAX_W	MDMAX		EIN	maximum attainable indicated torque
MIMSR_W	SWADAP		EIN	desired indicated torque from MSR
MINMX_W	NMAXMD		EIN	indicated nominal torque for NMAX limiting
MIOPT_W	MDBAS		EIN	optimum indicated torque
MISGS_W	CAN		EIN	desired internal torque for engine speed synchronization during gear shift
MISOLP_W	MDKOG		LOK	indicated nominal torque before limitation, local variable
MISOLV_W	MDKOG		AUS	indicated resultant nominal torque before torque limitation
MISOL_W	MDKOG		AUS	indicated resultant nominal torque
MISZUL_W	MDZUL		EIN	maximum permissible indicated torque
MITEBG_W	TEB		EIN	torque value for minimum charge canister purge
MIVMX_W	VMAXMD		EIN	indicated nominal torque for VMAX control
MIZSOLV_W	MDKOG		AUS	ind. torque for an ignition timing intervention before torque limiting
MIZSOL_W	MDKOG		AUS	indicated resultant nominal torque for ignition angle intervention
NASNOTTM	MDKOG		AUS	Speed threshold due to stalling protection as a function of tmot
NMOT	SWADAP		EIN	engine speed





Variable	Source	Type	Description
RLMIN_W	MDFUE	EIN	minimum permissible rl
RLSOL_W	MDFUE	EIN	desired relative air charge
SFPMDB	MDKOG	AUS	status fault path: ETC torque limitation is active
TMOT	SWADAP	EIN	Engine temperature
Z_JMDB	MDKOG	AUS	Cycle flag: ETC torque limitation is active

### FW MDKOG 1.190 Fixed Values

Parameter	Value	Description
CDKMDB		code word customer: Target torque limiter
CDTMDB		code word tester: Target torque limiter
CLAMDB		error class: Target torque limiter
TSFMDB		fault active time: Target torque limiter
TVMIBEG		debounce time for activation of ignition intervention during torque limitation

### FB MDKOG 1.190 Detailed description of function

Coordination of requested engine torque

The calculated nominal engine torque `misol_w` induced by the torque coordination is used for calculation of the suppression stage and/or for adjusting the ignition angle. The indicated torques requested from outside sources `miasrs_w` (from ASR, i.e. traction slip control) and `migs_w` (from GS, i.e. gear shift) as well as the internal torque requests (e.g. driver torque, n-max or v-max) are converted either by a minimum or a maximum selection into an indicated nominal engine torque `misolv_w`. The maximum selection is performed before the minimum selection due to safety reasons. Thus a torque demand resulting from the maximum selection can be limited by the minimum selection.

Should the engine speed drop to below `NASNOTTM` for a torque reduction by ASR or GS, then `miext=MDIMX` is selected immediately such that both interventions are prohibited. `NASNOTKL` is a function of the engine temperature `tmot`.

The indicated nominal torque for the ignition intervention depends on the activation condition `B_zwvz` (see `BBMDEIN`):

- If the ignition intervention is enabled `mizsolv_w` is calculated as follows:  
The nominal torque `misolv_w` is limited above by the product of opt. internal torque (incl. Lambda efficiency) and ignition angle efficiency (`miopt_w*etazwb`). Then the torque requests from the idling control `dmlr_w` (P and D components only) and from the anti-jerk function `dmar_w` are added.
- If no ignition intervention is necessary, the basic torque `mibas_w` is used as nominal torque. It only depends on the efficiencies of ignition and mixture. Interventions of the anti-jerk function are also taken into account.

Hint:

An increase of the torque demand can be performed via the interface `misgs_w` for synchronization of the engine speed due to an intervention of transmission. An establishing of priorities for drag control (MSR), traction slip control (ASR) with `misgs_w` is not performed in `%MDKOG`. If priorities are desired, these have to be defined `muß` in the function where the desired torque `misgs_w` is generated (`misgs_w` has to be decreased linear to the desired torque demand).



Subfunction BBMDEIN: Conditions torque intervention active

The condition B\_msr is set in addition to this for MSR intervention, such that trailing throttle cut off is not allowed (see %MDRED). For ASR intervention (traction-slip control), the condition B.asr is set so that a cylinder suppression is possible (see %MDRED). While an increasing torque demand for engine speed synchronization while transmission intervention is active the condition B\_sgs is true. Thus overrun fuel cut off is forbidden (cf. %MDRED). If the conditions B\_msr or B\_sgs are set, the overrun fuel cut off is forbidden due to an increased torque demand (B.savmd = true). The condition B\_mdein serves to disable the misfire detection (see %DASE) as well as to enable the anti-jerk function and idling control (for B\_mdein=0).

For the release of torque adjustment through ignition angle intervention the activation conditions B\_zwvz and B\_zwvs are responsible.

- B\_zwvz is set, if on the level of time schedule the requirement of an intervention is detected. This is the case in all operating conditions that require a torque reserve. These are idling, catalyst heating, short trip and the driveability functions dashpot, load shift damping and filtering before trailing throttle fuel cutoff. With disengaged clutch intervention is also enabled in order to prevent the engine from racing. All external interventions are detected through comparison of mifa\_w and misol\_w.
- B\_zwvs is set, if there is either an intervention on time level or there is a torque request from the anti-jerk function. In this case the nominal value is not switched to misol\_w, but in the function %MDZW (torque intervention through ignition) the intervention is activated.

Subfunction BBZWEIN: Conditions for ignition angle intervention active

see subfunction BBMDEIN

Subfunction MDBEG: Limitation of indicated torque

Both torques misolv\_w and mizolv\_w are limited to the maximum permissible indicated torque miszul\_w (from %MDZUL). By this it shall be achieved that the monitoring in the level 2 is only active if the (possibly limited) nominal torque is incorrectly converted into an actual torque. The dating of KFMIZU is matched to the permitted torques in level 2. Undesirable response by the torque surveillance can thus be prevented by this in the application phase in particular. It can be detected by recording B\_mibeg whether a limitation of the nominal torques has been performed.

Subfunction MDBEG\_DIAG: Connection of torque limitation with diagnosis

The function MDBEG\_DIAG is part of the ETC monitoring concept (level 1).

The desired torque is limited to a maximum torque miszul\_w in MDBEG. If the limitation is active the bit B\_mibeg is set.

The level 1 limitation B\_mibeg should only be active for a short time, e.g. when the engine is cold and the drivers request is in idle position. If the limitation B\_mibeg is active for a longer time (for example 10 min), there may be a fault in the system and a diagnosis entry is made.

## APP MDKOG 1.190 Application hint

Typical value:

MDIMX = 99.6%

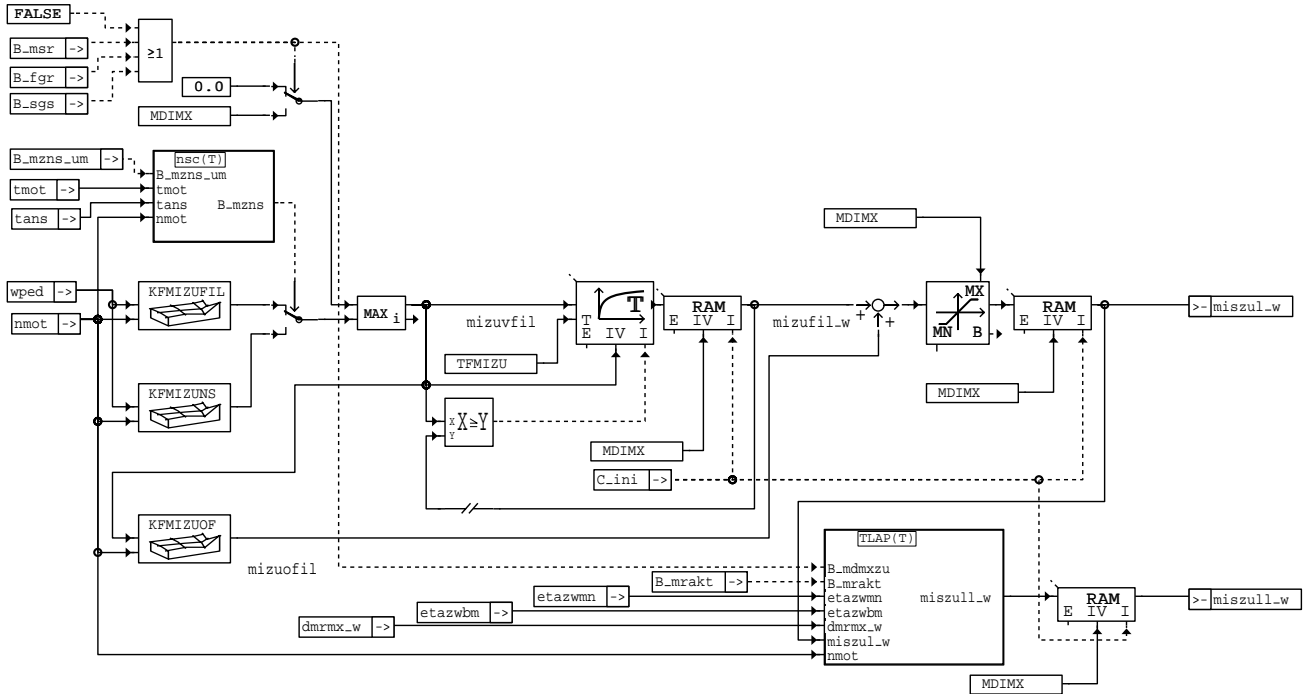
CWMDKOG = 6

NASNOTKL	tmot	-30	0	30	60
NASNOT		1500	900	600	600

The speed threshold NASNOTTM may not be greater than 2550 rpm.

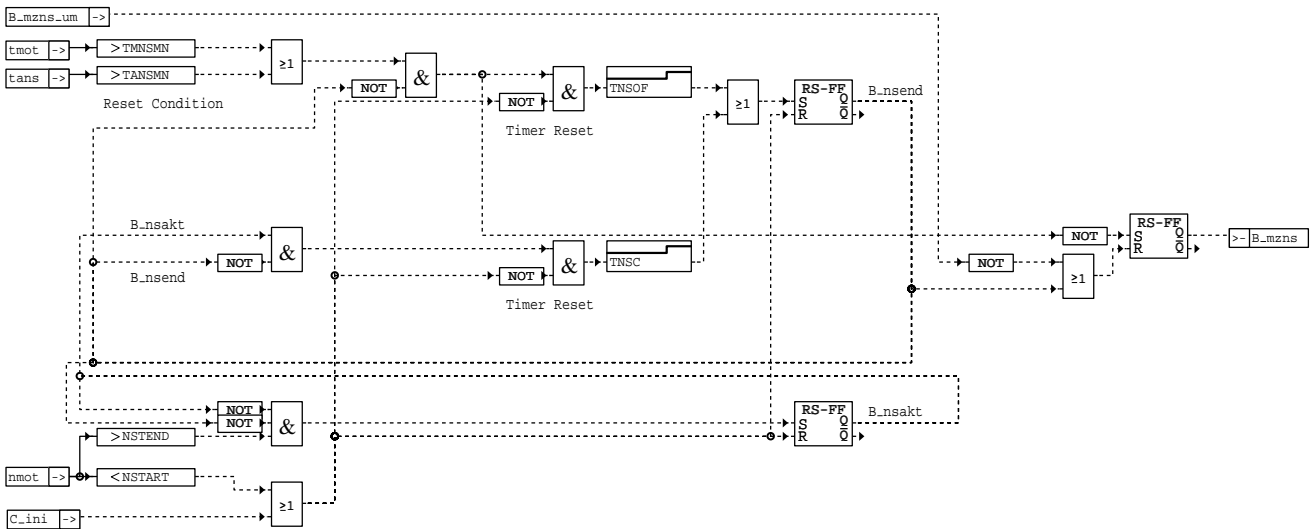
## MDZUL 4.21 Calculation of maximum permitted set torque

### FDEF MDZUL 4.21 Function definition



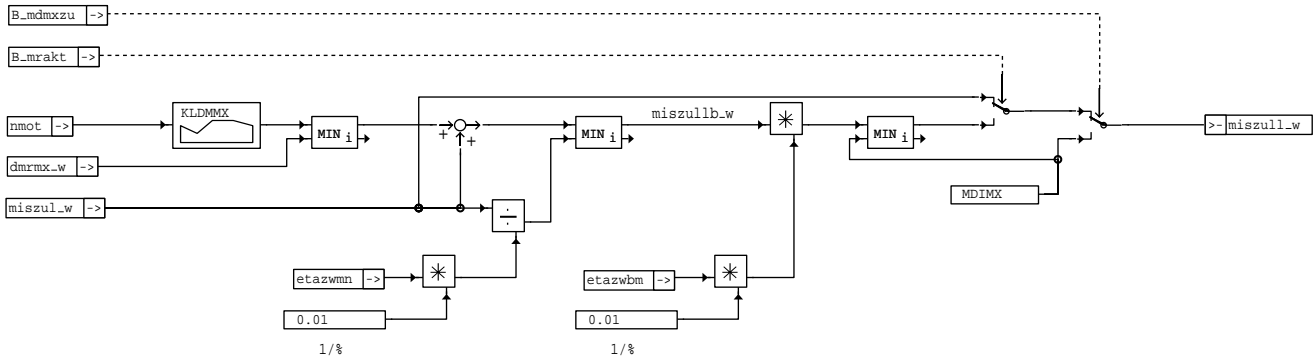
mdzul-mdzul

### mdzul-mdzul



mdzul-nsc

### mdzul-nsc



mdzul-tlap

**mdzul-tlap**

**ABK MDZUL 4.21 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
KFMIZUFIL	WPED	NMOT	KF	Maximum permitted indicated set torque for torque limitation before Filter
KFMIZUNS	WPED	NMOT	KF	Authorized torque for post-start torque increase
KFMIZUOF	MIZUVFIL	NMOT	KF	Maximum permitted indicated set torque for torque limitation
KLDMMX	NMOT		KL	Maximum delta torque for air path
MDIMX			FW	maximum limit indicated engine torque
NSTART			FW	engine speed limit for low engine speed exit (for post-start torque increase)
NSTEND			FW	engine speed limit for start end (for post-start torque increase)
TANSMN			FW	intake air temperature limit (for post-start torque increase)
TFMIZU			FW	Time constant of low pass filter for permitted set torque
TMNSMN			FW	engine temperature limit (for post-start torque increase)
TNSC			FW	post-start monitoring time
TNSOF			FW	debounce time for turning off the post-start torque increase

Variable	Source	Type	Description
B_FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control
B_MDMXZU	MDZUL	LOK	Condition maximum torque permitted
B_MRAKT	MDKOL	EIN	condition: torque reserve active
B_MSR	MDKOG	EIN	Condition MSR
B_MZNS	MDZUL	LOK	Post-start torque increase is active
B_MZNS_UM	UFNSC	EIN	afterstart torque increase of ETC-monitoring is active
B_NSACT	MDZUL	LOK	post-start is active (for post-start torque increase)
B_NSEND	MDZUL	LOK	post-start monitoring time is over (for post-start torque increase)
B_SGS	MDKOG	EIN	condition: torque intervention for engine speed synchr. during gear shift
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DMRMX_W	MDKOL	EIN	delta torque for charge by torque reserve
ETAZWBM	MDBAS	EIN	mean ignition angle effectiveness of basic ignition angle
ETAZWMN	ZWMIN	EIN	minimum ignition angle effectiveness
MISZULLB_W	MDZUL	DOK	maximum permissible internal torque for charge path (limited)
MISZULL_W	MDZUL	AUS	maximum permissible internal torque for charge path
MISZUL_W	MDZUL	AUS	maximum permissible indicated torque
MIZUFIL_W	MDZUL	LOK	Indicated torque after filtering allowed
MIZUOFIL	MDZUL	LOK	Indicated torque without filtering
MIZUVFIL	MDZUL	LOK	Indicated torque before filtering
NMOT	SWADAP	EIN	engine speed
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
WPED	GGPED	EIN	Standardized accelerator pedal angle

**FW MDZUL 4.21 Fixed Values**

Parameter	Value	Description
MDIMX		maximum limit indicated engine torque
NSTART		engine speed limit for low engine speed exit (for post-start torque increase)
NSTEND		engine speed limit for start end (for post-start torque increase)
TANSMN		intake air temperature limit (for post-start torque increase)
TFMIZU		Time constant of low pass filter for permitted set torque
TMNSMN		engine temperature limit (for post-start torque increase)
TNSC		post-start monitoring time
TNSOF		debounce time for turning off the post-start torque increase



### FB MDZUL 4.21 Detailed description of function

This function calculates a maximum indicated torque `miszul_w` for the ignition path and a maximum indicated torque `miszull_w` for the air path of the torque coordination. These torques are used in the functions `%mdkol` and `%mdkog` of the torque coordination to limit the desired torque. Limiting the desired torque shall prevent an unjustified triggering of level 2 of the monitoring concept. In level 2 of the monitoring concept (overview section `ufue`) a roughly calculated actual torque is compared with a maximum permitted actual torque. A desired torque from the torque coordination, which is calculated too large would lead to a too large actual torque with a response of the actual torque monitoring in level 2.

The calculation of the maximum permitted desired torque `miszul_w` in the function `%mdzul` can be described in detail as follows:

The maximum torque request of the pedal, which is permitted at a certain engine speed is stored in two maps (`KFMIZUOF = f(nmot, mizuvfil)`, `KFMIZUFIL = f(nmot, wped)`). In the process also an offset is taken into consideration, which comes from other torque-increasing functions, which will not be discussed in detail here (e.g. idle control). The sum of the two maps (referred to as sum map of level 1 in the following) results in the permitted desired torque. In order to avoid an unjustified limiting of the desired torque (which is e.g. increased due to the dashpot function) in case of quick setpoint changes (due to negative pedal angle gradient) the value obtained from map `KFMIZUFIL` is filtered in a low pass. This filter, however, is only active in case of a negative gradient of the value obtained from the map.

An after-start extension is performed in level 2 of the torque monitoring in dependency on the engine temperature and on the intake air temperature. The condition for the after-start extension is calculated there in the function `%UFNSC`. The actual after-start extension is performed in the function `%UFMZUL`. Level 1 may only perform an after-start extension (subfunction `NSC`) if an after-start extension is also performed in level 2. This must be ensured by the entering of data.

### APP MDZUL 4.21 Application hint

Starting point for the entering of data into the two maps is the permitted torque in dependency on pedal angle and engine speed. This maximum permitted torque (sum map of level 1) results among other from the idle demand and from the pedal map.

A complete deactivation of the function can be performed by the map `KFMIZUOF` (`KFMIZUOF = 99,6%` for all base points).

A deactivation of the after-start extension can take place by entering data into the map `KFMIZUNS`.

In the process the same data are entered into the map `KFMIZUNS` as into the map `KFMIZUFIL`. The value `-48 C` must be entered for the temperature thresholds `TNNSMN` and `TANSMN`.

A deactivation of the function `%mdzul` with active torque monitoring can lead to a response of the torque monitoring (`%ufmzul`) in level 2 with the fault reaction safety fuel switch-off.

The counts of `TNSOF` and `TNSC` can be looked at in `VS100` under `tnsofCtr` and `tnscCtr`.

While the offset was so far stored dependent on engine speed and pedal setpoint (`KFMIZU`) it is now stored dependent on permitted torque and engine speed (`KFMIZUOF`). The entered data can be changed as follows:

For a fixed engine speed and a fixed pedal setpoint an offset torque is obtained from the map `KFMIZU`.

This offset is now entered into the map `KFMDZOF` for the corresponding engine speed base point and the torque base point, which results from the map `KFMIUFIL` (with same engine speed and same pedal angle).

`KFMIZUOF:`

-----

The map `KFMIZUOF` is adjusted in the function `%ufmzul` following the map `KFMDZOF_UM`.

`KFMIZUFIL:`

-----

The map `KFMIZUFIL` is adjusted in the function `%ufmzul` following the map `KFMPEL_UM`.

The most important part of this map lies at an accelerator position of 0 and at an engine speed above 1000 rpm.

`TFMIZU:`

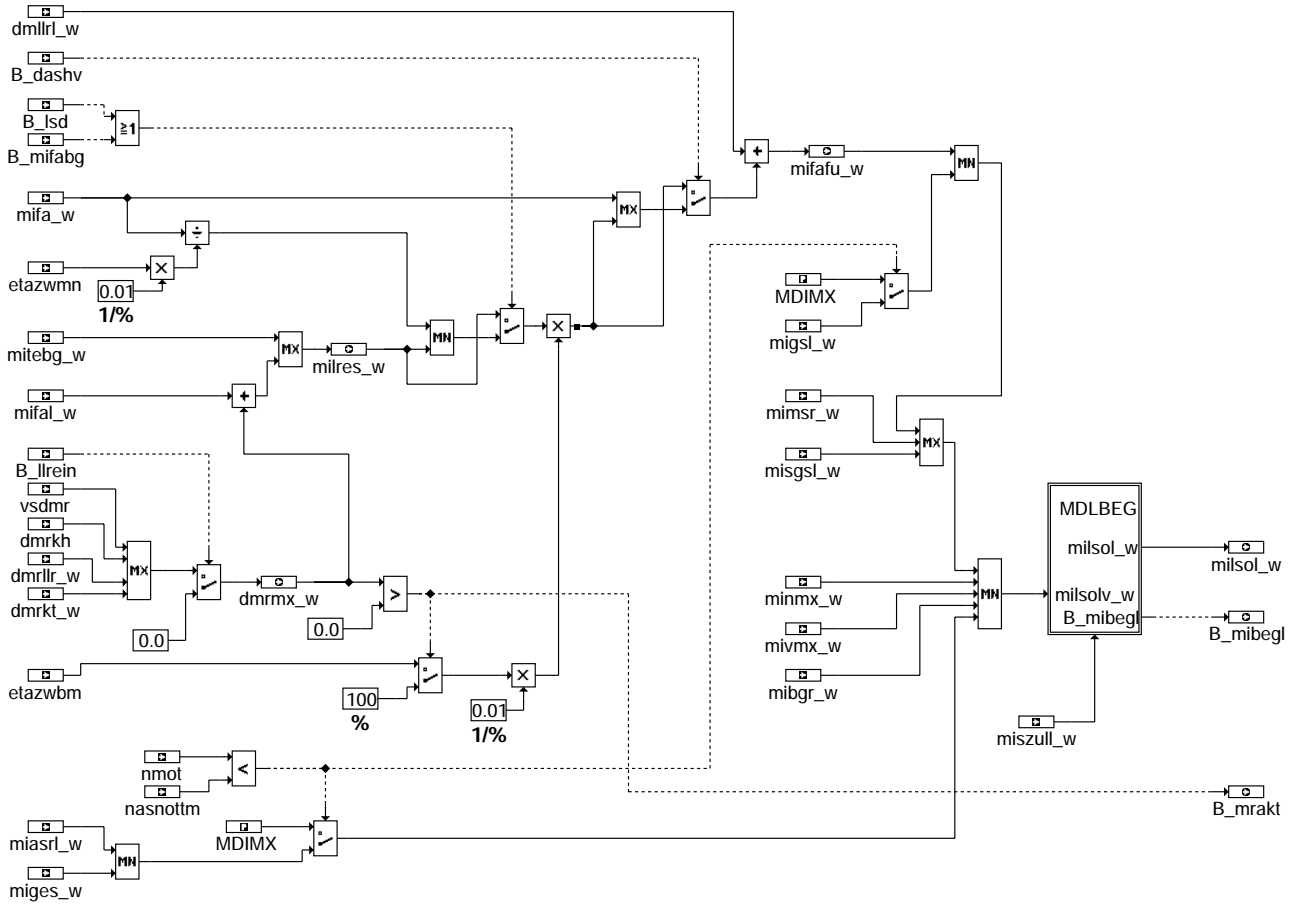
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This filter shall take into consideration torque-increasing functions, e.g. dashpot.

The filter time constant of this filter lies between 100 ms and 2 seconds (slow filter). It is to be tuned to the filter in the torque monitoring (section `ufmzf`). A filter time constant of 0,3s has so far proved to be worthwhile.

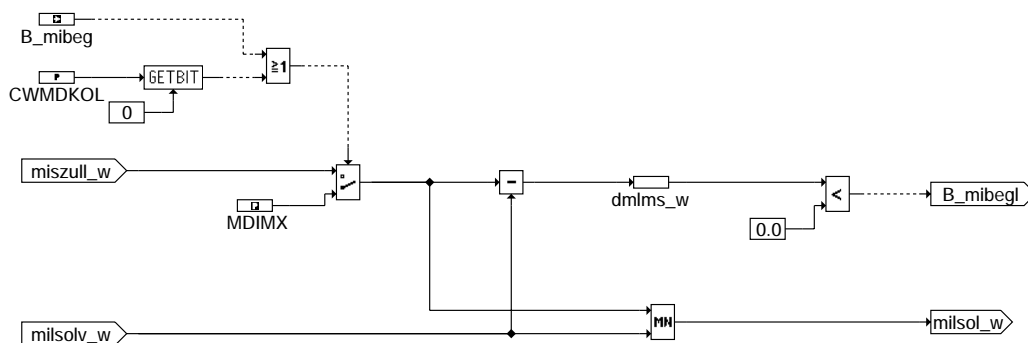
## MDKOL 10.110 Coordination torque intervention air path

### FDEF MDKOL 10.110 Function definition



#### mdkol-main

Subfunction MDLBEG: Limitation of desired torque for charge path



#### mdkol-mdlbeg

### ABK MDKOL 10.110 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWMDKOL			FW	codeword MDKOL: torque limitation
MDIMX			FW (REF)	maximum limit indicated engine torque
Variable	Source		Type	Description
B_DASHV			EIN	condition dashpot delayed
B_LLREIN	LLRMD		EIN	Condition idle speed control is active
B_LSD	MDFAW		EIN	condition: limitation of positive torque gradient active
B_MIBEG	MDKOG		EIN	condition torque limit active
B_MIBEGL	MDKOL		AUS	condition torque limitation charge path active
B_MIFABG			EIN	condition limitation of mifa



Variable	Source	Type	Description
B_MRAKT	MDKOL	AUS	condition: torque reserve active
DMLLR_LW	LLRRM	EIN	desired torque change from the idle speed control (part on the air path)
DM_LMS_W	MDKOL	LOK	difference between desired torque and permissible torque for charge path
DMRKH	KHMD	EIN	torque reserve for catalyzer heating
DMRKT_W	MDTRIP	EIN	Torque reserve during quickestest
DMRLLR_W	LLRMR	EIN	torque reserve for idle speed control
DMRMX_W	MDKOL	AUS	delta torque for charge by torque reserve
ETAZWBM	MDBAS	EIN	mean ignition angle effectiveness of basic ignition angle
ETAZWMN	ZWMIN	EIN	minimum ignition angle effectiveness
MIASRL_W	SWADAP	EIN	desired indicated torque from ASR for slow intervention
MIBGR_W	MDBGRG	EIN	Indicated desired torque for gear-dependent limiting of the clutch torque
MIFAFU_W	MDKOL	AUS	driver torque request for charge
MIFAL_W	MSF	EIN	Indicated driver's wish torque for torque coordination cylinder filling
MIFA_W	MSF	EIN	desired indicated engine torque
MIGES_W	SWADAP	EIN	desired indicated torque for transmission protection
MIGSL_W	CAN	EIN	desired internal torque for charge limitation during GS.
MILRES_W	MDKOL	AUS	torque request for air path including all torque reserves
MILSOL_W	MDKOL	AUS	driver torque request for charge
MIMSR_W	SWADAP	EIN	desired indicated torque from MSR
MINMX_W	NMAXMD	EIN	indicated nominal torque for NMAX limiting
MISGSL_W	CAN	EIN	desired internal torque (air path) for engine speed synchr. during gear shift
MISZULL_W	MDZUL	EIN	maximum permissible internal torque for charge path
MITEBG_W	TEB	EIN	torque value for minimum charge canister purge
MIVMX_W	VMAXMD	EIN	indicated nominal torque for VMAX control
NASNOTTM	MDKOG	EIN	Speed threshold due to stalling protection as a function of tmot
NMOT	SWADAP	EIN	engine speed
VSDMR	VS_VERST	EIN	adjustable torque reserve via VSxy

### FW MDKOL 10.110 Fixed Values

Parameter	Value	Description
CWMDKOL		codeword MDKOL: torque limitation

### FB MDKOL 10.110 Detailed description of function

#### 1. Calculation of increased air request milres, mechanism of torque reserve

The maximum torque reserve from catalyst heating, idle speed control and short trip is added to the driver air request mifal. Further increase for application purpose is possible via VSxy by the interface vsdmr. Another minimum air request is given by mitebg of the tank ventilation. The resulting air request with all torque reserves is milres. This increase of the charge torque automatically retards the ignition angle, since the driver request mifa can only be adjusted by retarding the ignition under an increased charge. The torque reserve always applies to the optimum ignition angle and not to the basic ignition angle, in order to allow non-ambiguous adjustment of the operating point.

#### 2. Calculation of resulting driver air request mifafu concerning torque reserve and limits of efficiency

The increased driver torque milres is limited to the torque that provides the minimum permissible ignition angle efficiency etazwmn. This limitation is not performed with active torque gradient limitation (B\_lsd) in order to control mifal independently (no influence of mifa for further calculations in MDKOL). The value is then multiplied by the basic efficiency in order to arrive at the same reference point as the rest of the coordination torques. If the torque reserve is greater than the required torque mifa because of the basic effectiveness, then the former is selected (taking the maximum between the driver request and the driver load request with torque reserve). Result is the drivers torque request for the engine load mifafu.

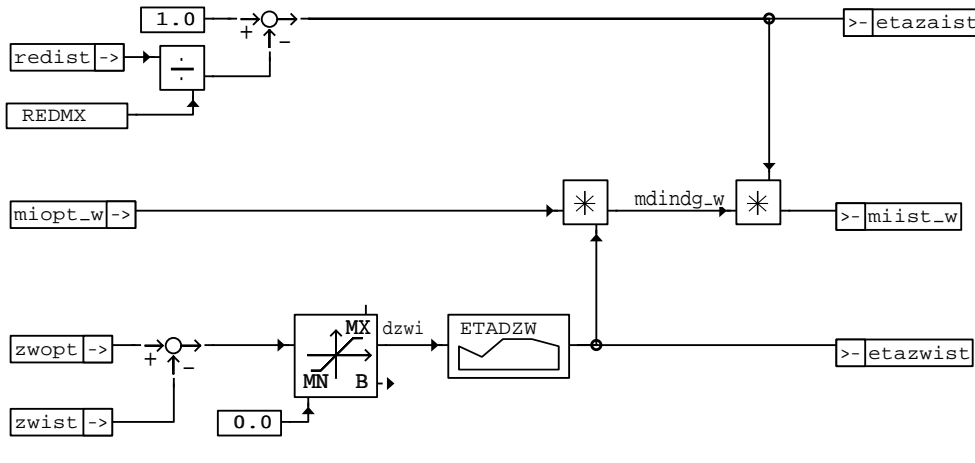
#### 3. Actual torque coordination

Maximum selection with torque request mimsr from MSR, then minimum selection with the torque of the rpm limiter minmx, the torque of the speed limiter mivmx, the torque from ASR and the torque request in case of transmission protection. The last two torques are only considered in case of exceeding a low engine speed to prevent engine stalling.

In case of limiting the torque by the safty concept (Level 1), the torque ist limited to miszul.w.

## MDIST 10.2 Engine torque calculation

### FDEF MDIST 10.2 Function definition



mdist-mdist

### ABK MDIST 10.2 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ETADZW	DZWI		KL	ignition efficiency depending on delta ignition angle
REDMX			FW	maximal step number for disabled injectors (f.e. =2*number of cylinder)
Variable	Source		Type	Description
DZWI	MDIST		LOK	difference ignition angle (between zwopt and zwout)
ETAZAIST	MDIST		AUS	actual cylinder masking effectiveness
ETAZWIST	MDIST		AUS	actual ignition angle effectiveness
MDINDG_W	MDIST		LOK	indicated torque in the case of all cylinders firing
MIIST_W	MDIST		AUS	indicated real engine torque
MIOPT_W	MDBAS		EIN	optimum indicated torque
REDIST	BGEVAB		EIN	real cylinder cut-off step
ZWIST	ZUE		EIN	real ignition angle
ZWOPT	MSF		EIN	optimal ignition angle

### FW MDIST 10.2 Fixed Values

Parameter	Value	Description
REDMX		maximal step number for disabled injectors (f.e. =2*number of cylinder)

### FB MDIST 10.2 Detailed description of function

This function supplies an indicated actual torque for all operating states of the engine. From the difference dzwi between the optimum ignition angle zwopt and the actual ignition angle zwist the actual ignition-angle efficiency etazwist results over the ignition-angle efficiency characteristic ETADZW. The indicated engine torque miopt\_w, at given Lambda and optimum ignition angle, is multiplied by the actual ignition-angle efficiency etazwist. The indicated actual engine torque miist\_w is the indicated engine torque mdindg\_w, which is reduced share-wise by the cut-out cylinders.

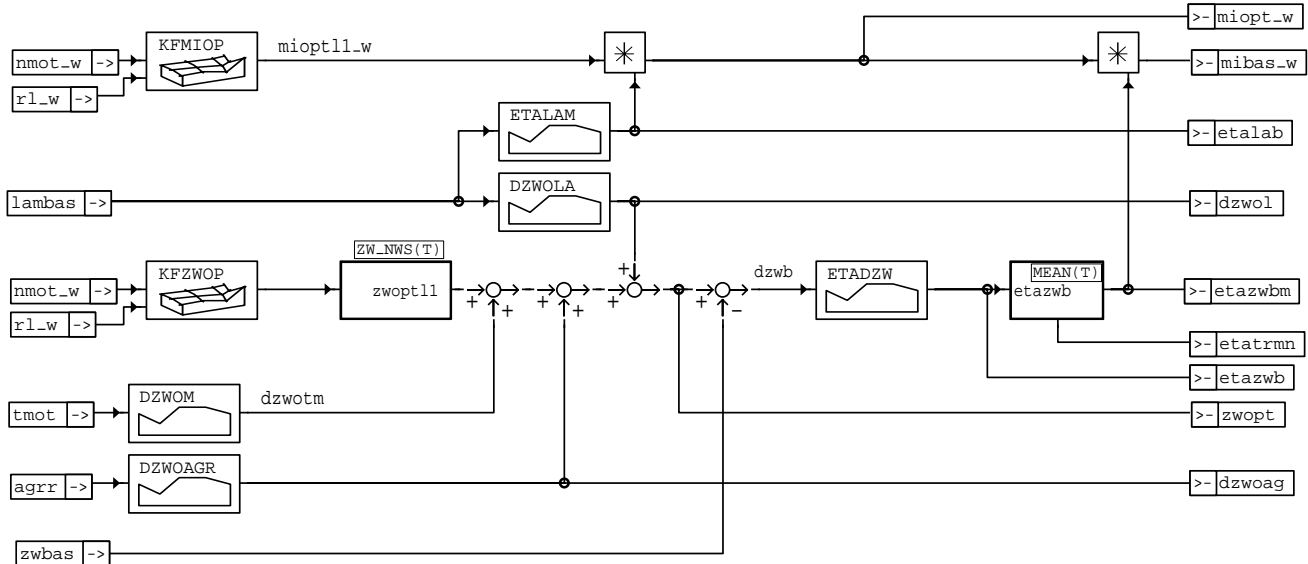
### APP MDIST 10.2 Application hint

Due to the multiple use of the parameter ETADZW in the functional extent, the working point indication in application aids is of no use for this table. The working point must be determined by a separate indication of the input dzwi.



## MDBAS 4.30 Basic calculation for torque interface

### FDEF MDBAS 4.30 Function definition



mdbas-mdbas

### ABK MDBAS 4.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DZWNWSUE	WNWUE		KL	Delta ignition angle dependent on the camshaft overlap
DZWOAGR	AGRR		KL	AGR-rate-dependent offset of optimum ignition angle
DZWOLA	LAMBAS		KL	Lambda dependency of optimum ignition angle referred to Lambda 1
DZWOM	TMOT		KL	temperature-dependent offset of optimum ignition angle
ETADZW	DZWB		KL	ignition efficiency depending on delta ignition angle
ETALAM	LAMBAS		KL	Lambda effectiveness
KFMiop	NMOT_W	RL_W	KF	map optimum engine torque
KFZWOP	NMOT_W	RL_W	KF	optimum ignition angle
KFZWOP2	NMOT_W	RL_W	KF	Optimum ignition angle, variant 2
Variable	Source		Type	Description
AGRR	SWADAP		EIN	exhaust gas recirculation rate
DZWOAG	MDBAS		AUS	exhaust recirculation rate-dependent correction of optimum ignition angle
DZWOL	MDBAS		AUS	Lambda-dependent correction of optimum ignition angle
DZWOTM	MDBAS		LOK	temperature-dependent correction of optimum ignition angle
ETALAB	MDBAS		AUS	Lambda effectiveness without intervention w.r.t. to optimum torque at Lambda=1
ETATRMN	MDBAS		AUS	minimum value in effectiveness drum
ETAZWB	MDBAS		AUS	ignition angle effectiveness of basic ignition angle
ETAZWBM	MDBAS		AUS	mean ignition angle effectiveness of basic ignition angle
FNWUE	NWS		EIN	Weighting factor camshaft overlap
LAMBAS	SWADAP		EIN	basic Lambda
MIBAS_W	MDBAS		AUS	indicated basic torque
MIOPTL1_W	MDBAS		LOK	optimal torque at lambda = 1
MIOPT_W	MDBAS		AUS	optimum indicated torque
NMOT_W	SWADAP		EIN	engine speed
RL_W	EGFE		EIN	relative air charge (Word)
R_SYN	GGDPG		EIN	Synchro schedule
SY_NWS	PROKON		EIN	system constant camshaft control: none, 2 point or continuous
TMOT	SWADAP		EIN	Engine temperature
WNWUE	NWS		EIN	camshaft overlap angle of inlet and outlet valve opening
ZWBAS	ZUE		EIN	basic ignition angle
ZWOPT	MDBAS		AUS	optimal ignition angle
ZWOPTL1	MDBAS		LOK	optimal ignition angle at lambda=1

### FW MDBAS 4.30 Fixed Values

Parameter	Value	Description
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## FB MDBAS 4.30 Detailed description of function

Calculation of the optimum torque  $m_{optll}$  at  $\Lambda=1$  with the aid of the map KFMIOP. Correction of this torque by the  $\Lambda$  influence via multiplication by the  $\Lambda$  effectiveness  $e_{\Lambda}$ . The  $\Lambda$  effectiveness is calculated from the curve ETALAM. Multiplication by the ignition angle effectiveness gives the basic torque  $m_{bas}$ . This corresponds to the indexed torque that stabilises if combustion occurs with the basic  $\Lambda$   $m_{bas}$  and the basic ignition angle  $\alpha_{bas}$ . Calculation of the optimum ignition angle via the map KFZWP for  $\Lambda=1$ . Additive corrections depending on  $\Lambda$ , the exhaust recirculation rate  $agrr$  and the engine temperature, are included. The ignition angle  $\alpha_{wpt}$  thus obtained now forms the basis for calculation of the ignition angle effectiveness. The basic ignition angle effectiveness is calculated with the curve ETADZW, and the input variable is formed from the difference between  $\alpha_{wpt}$  and  $\alpha_{bas}$ . The basic effectiveness values are then averaged over all cylinders to produce the basic effectiveness  $e_{\Lambda}$ .

## APP MDBAS 4.30 Application hint

Exhaust recirculation inactive for all measurements!

The following measurements must be performed:

### 1. $\Lambda=1$ operation:

Ignition angle loops on engine test stand at  $\Lambda=1$  at the following points with warm engine:

$n=500,750,1000,1250,1500,2000,2500,3000,3500,4000,4500,5000,5500,6000,6500$  (if possible) rpm

$r_l=10,20,30,40,50,60,70,80,90,100$  %

The ignition angle loops start at the angle at which the maximum torque is obtained (if not driveable at the knock limit).

Ignition is now retarded in steps of 4.5 degrees CA until the latest possible ignition angle is reached.

The following data should be recorded for each measuring point:  $n_{mot}$ ,  $r_l$ ,  $\Lambda$ , clutch torque, ignition angle.

### 2. $\Lambda$ dependency

Ignition angle loops over  $\Lambda$  at measuring points:

$n = 1000, 2000, 3000$  rpm

$r_l = 30, 50, 70$  %

$\Lambda = .8, .85, .9, .95, 1, 1.05, 1.1, 1.15, 1.2$

Measurements as above

### 3. Friction torque

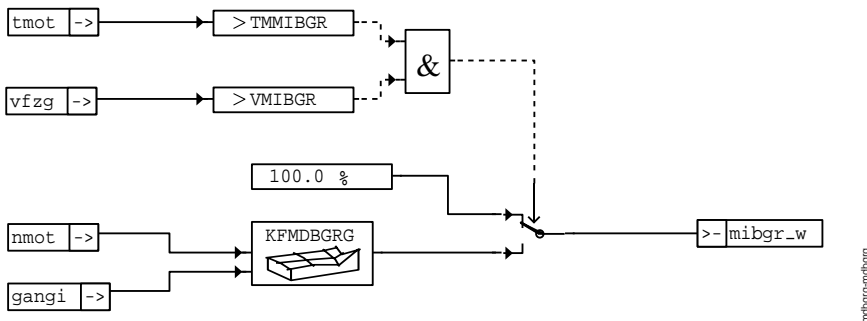
The friction torque must be present for all measurements under 1. Measurement on test stand, engine off but warm.

### 4. Evaluation

Measurement results evaluated by K3/ESY4-Hes or -Zg.

## MDBGRG 4.40 torque limitation minimum

### FDEF MDBGRG 4.40 Function definition



### mdbgrg-mdbgrg

Für die Typisierung der Fahrzeuge muß eventuell das Moment in den unteren Gängen in Abhängigkeit vom Gang und von der Drehzahl begrenzt werden.

### ABK MDBGRG 4.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFMDBGRG	NMOT	GANGI	KF	map with the value of the torque limitation
TMMIBGR			FW	$t_{mot}$ threshold for enabling of torque limitation
VMIBGR			FW	$v$ -threshold for enabling of torque limitation
Variable	Source		Type	Description
GANGI	SWADAP		EIN	Engaged gear
MIBGR_W	MDBGRG		AUS	Indicated desired torque for gear-dependent limiting of the clutch torque
NMOT	SWADAP		EIN	engine speed
TMOT	SWADAP		EIN	Engine temperature
VFZG	SWADAP		EIN	vehicle speed (km/h)

## FW MDBGRG 4.40 Fixed Values

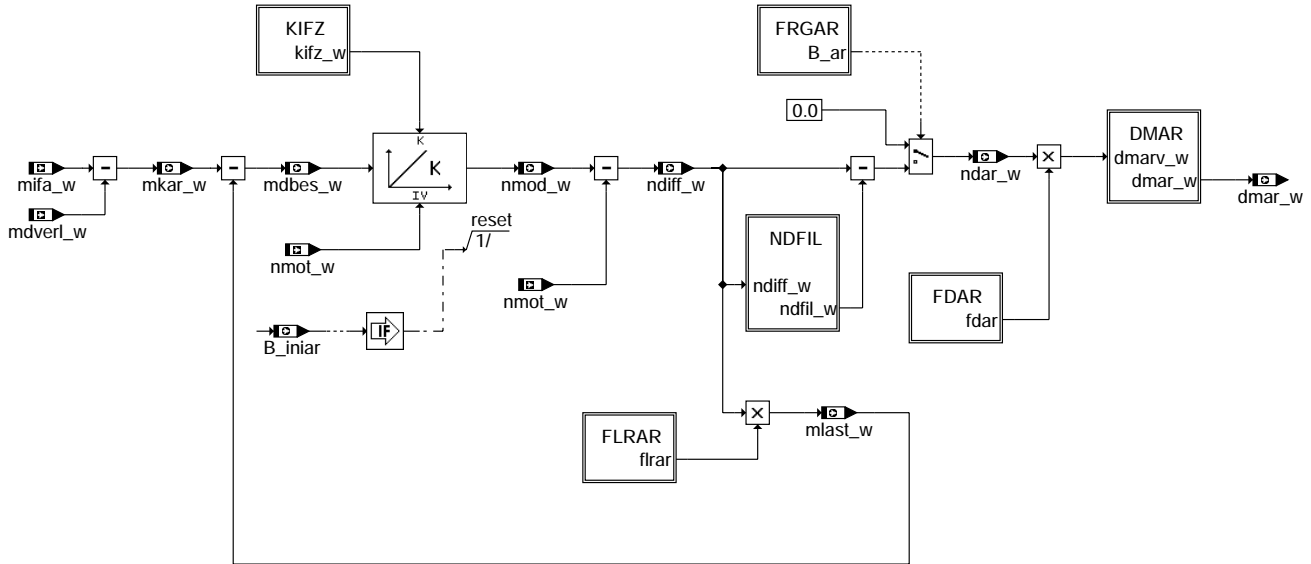
Parameter	Value	Description
TMMIBGR		tmot threshold for enabling of torque limitation
VMIBGR		v-threshold for enabling of torque limitation

## FB MDBGRG 4.40 Detailed description of function

### APP MDBGRG 4.40 Application hint

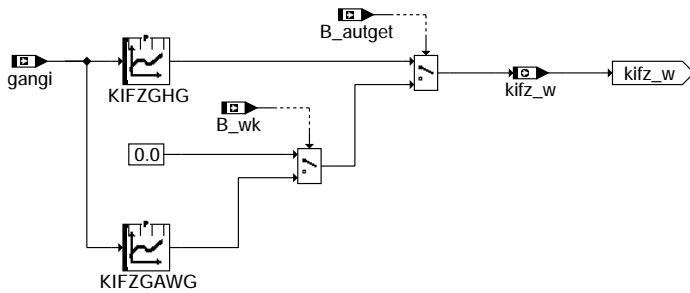
## ARMD 14.10 Torque based anti jerk function

### FDEF ARMD 14.10 Function definition



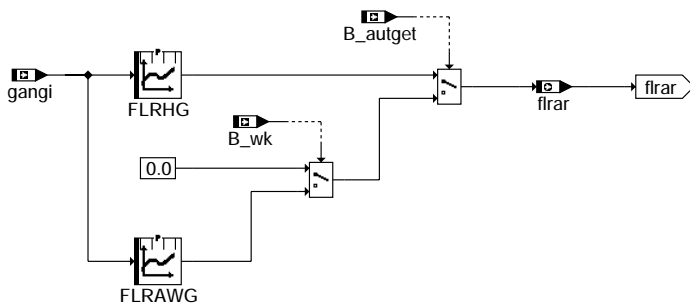
#### armd-main

Subfunction KIFZ:



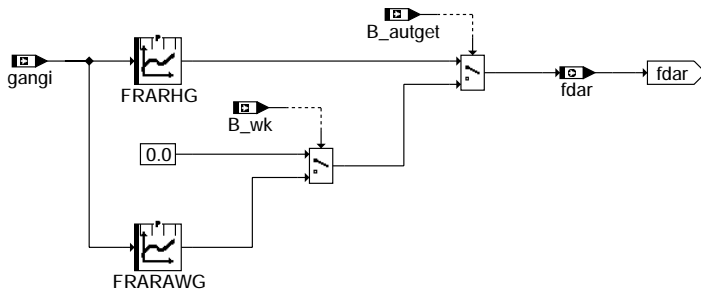
#### armd-kifz

Subfunction FLRAR:



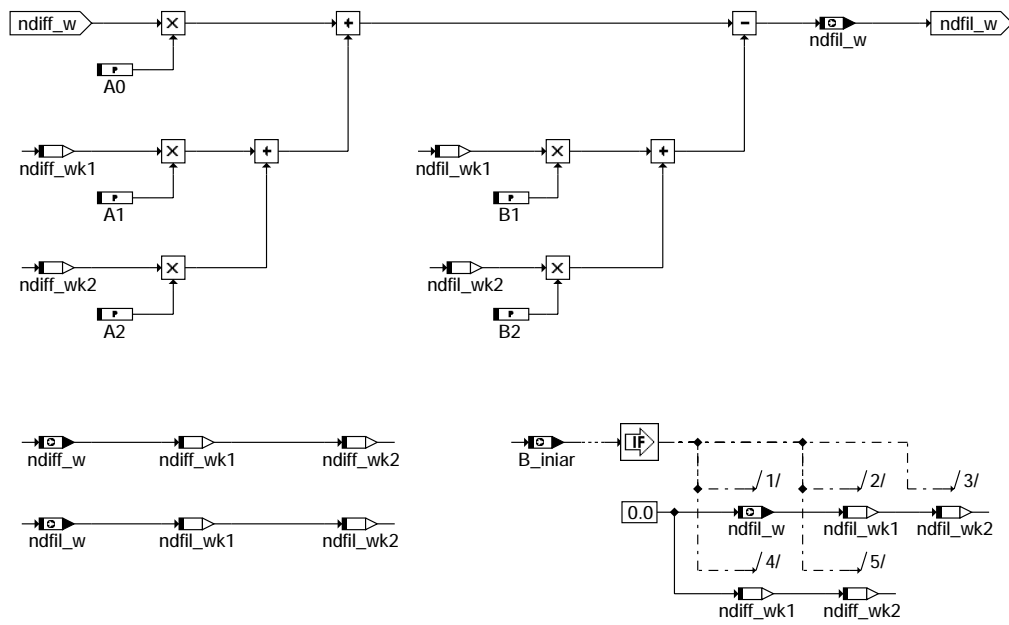
#### armd-flrar

### Subfunction FDAR:



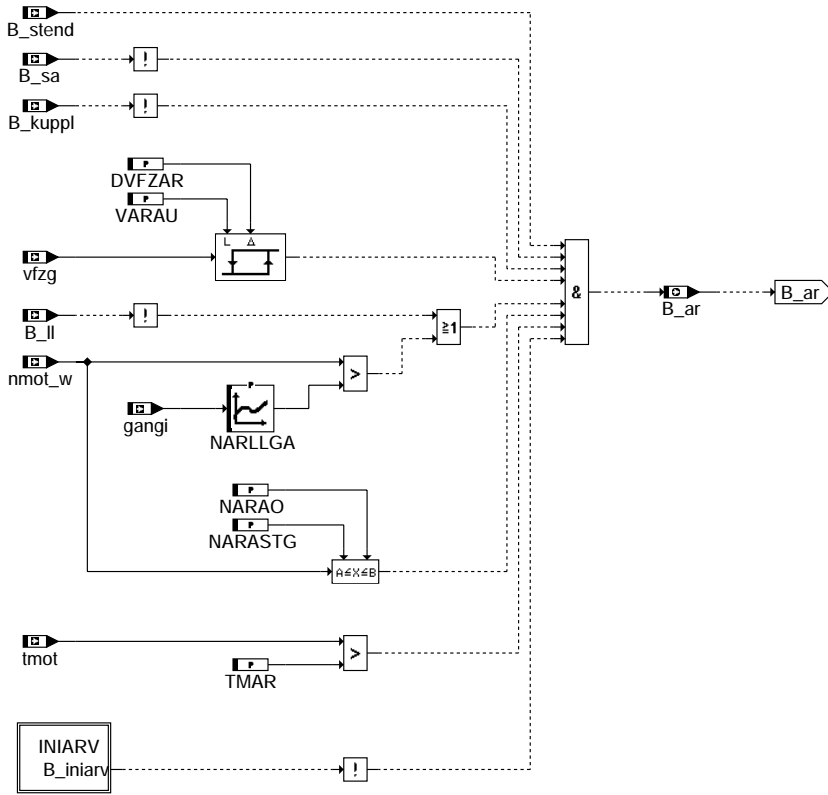
### armd-fdar

#### Subfunction NDFIL:



### armd-ndfil

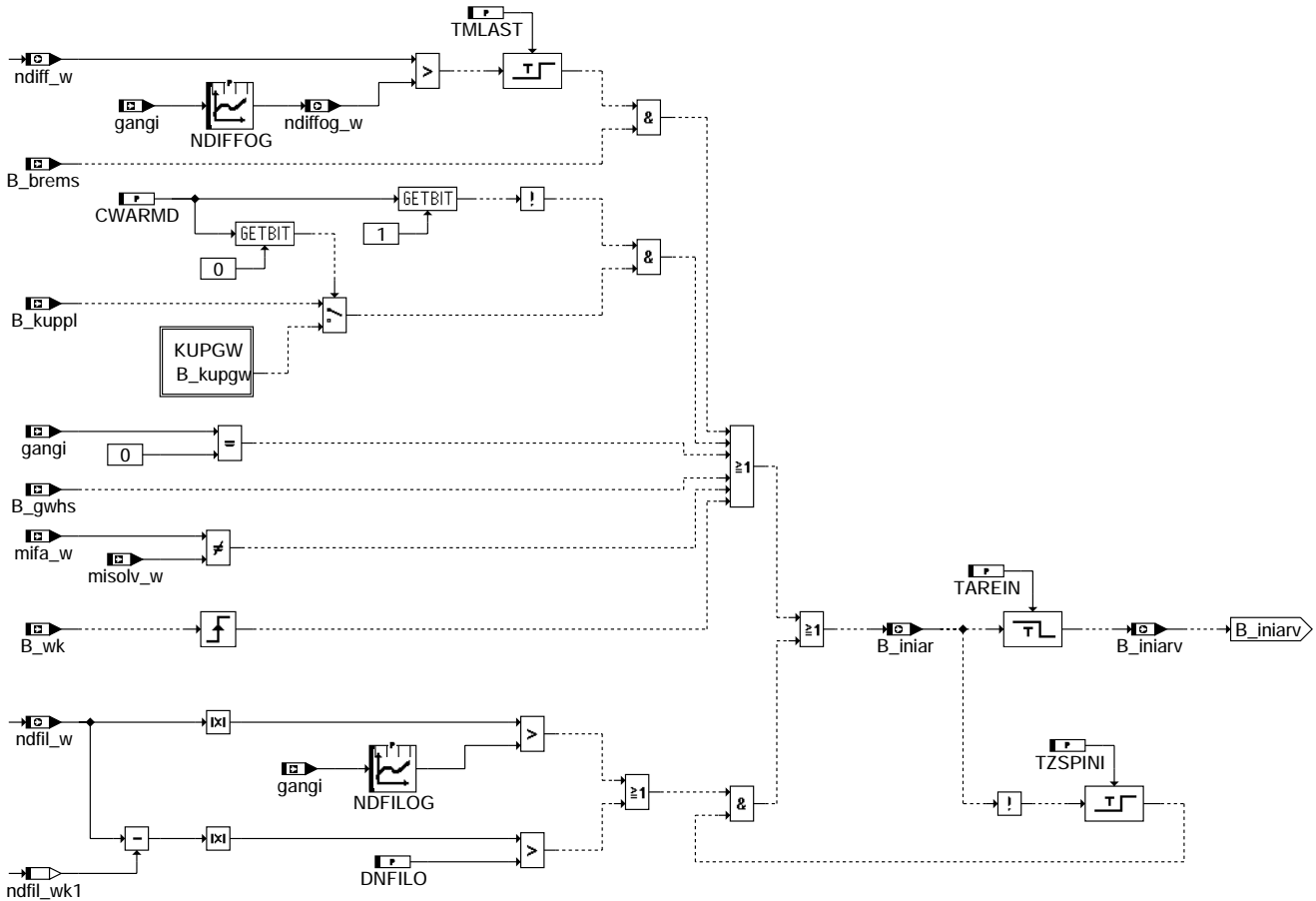
Subfunction FRGAR:



armd-frgar

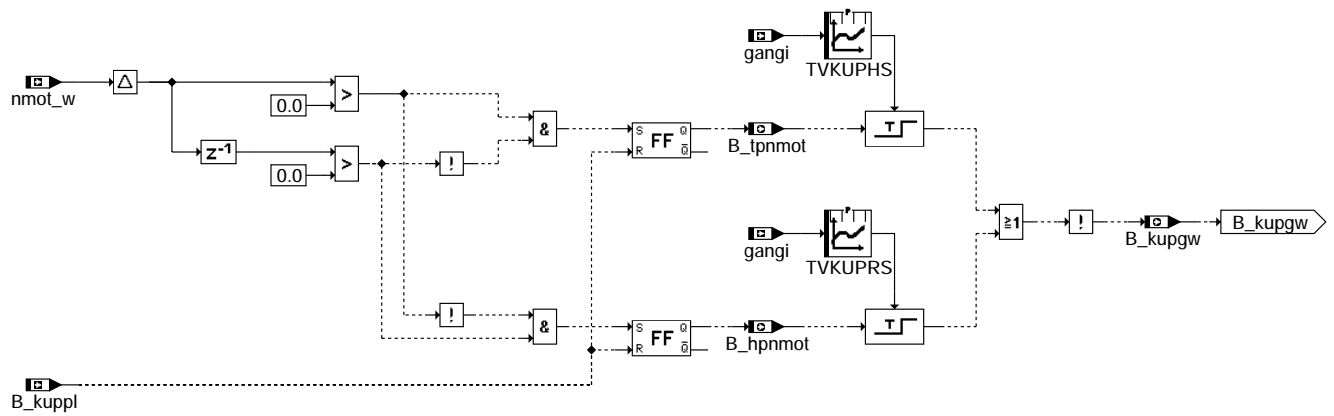
armd-frgar

Subfunction INIARV:



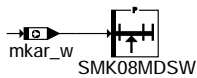
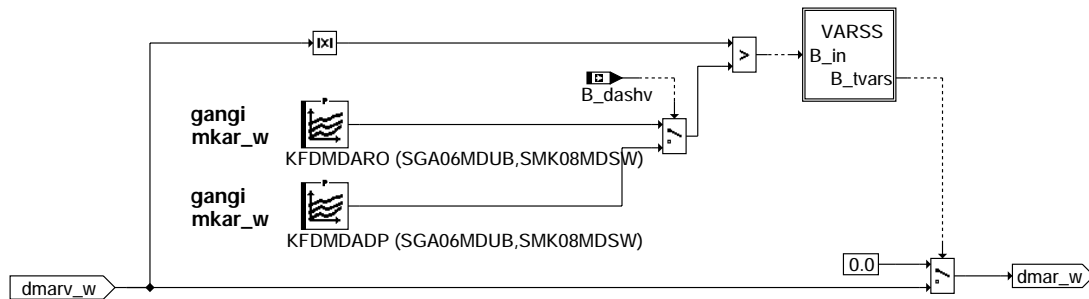
armd-iniarv

Subfunction KUPGW:



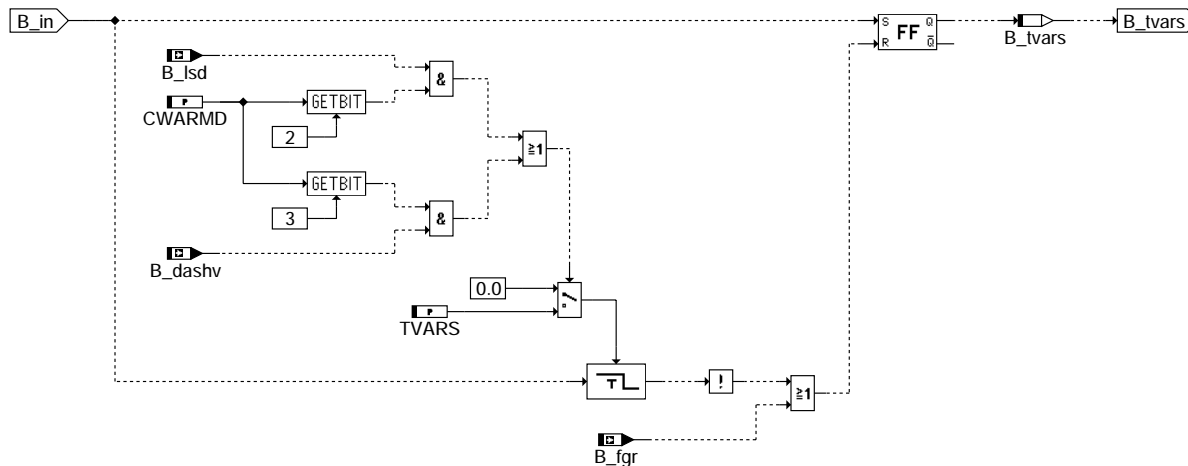
armd-kupgw

Subfunction DMAR:



armd-dmar

Subfunction VARSS:



armd-varss

Parameter	Source-X	Source-Y	Type	Description
A0			FW	transmission coefficient
A1			FW	transmission coefficient
A2			FW	transmission coefficient
B1			FW	transmission coefficient
B2			FW	transmission coefficient
CWARMD			FW	Code word anti jerk function
DNFILO			FW	upper threshold of filter output gradient ndfil
DVFZAR			FW	Hysteresis for vehicle speed limit during AR (Anti jerk)
FLRAWG	GANGI		KL	amplification of load controller
FLRHG	GANGI		KL	amplification of load controller
FRARAWG	GANGI		KL	amplification factor
FRARHG	GANGI		KL	amplification factor
KFDMDADP	GANGI	MKAR_W	KF	upper threshold for torque-intervention during dashpot
KFDMDARO	GANGI	MKAR_W	KF	Upper threshold for torque intervention
KIFZGAWG	GANGI		KL	amplification of vehicle model integrator at AT
KIFZGHG	GANGI		KL	amplification of vehicle model integrator at AT
NARAO			FW	upper engine speed threshold for anti-jerk function active
NARASTG			FW	RPM threshold in higher gear for AR active
NARLLGA	GANGI		KL	speed threshold for AR at idle
NDFILOG	GANGI		KL	Threshold for filter output ndfil
NDIFFOG	GANGI		KL	Threshold engine speed difference for initialization of AR during braking
SMK08MDSW	MKAR_W		SV	Antisurge torque dependent basic point (number =8)
TAREIN			FW	lockup time for anti-jerk function
TMAR			FW	Lower TMOT threshold for AR release
TMLAST			FW	blocking time until the initialization of the AR is triggered at deceleration
TVARS			FW	delay time until antisurge is inactive again
TVKUPHS	GANGI		FW	delay time for clutch switch during shifting in higher gear
TVKUPRS	GANGI		KL	delay time for clutch switch during shifting in lower gear



Parameter	Source-X	Source-Y	Type	Description
TZSPINI			FW	Resting time for filter initialisation
VARAU			FW	vehicle speed for anti-jerk active
Variable	Source		Type	Description
B_AR	ARMD		AUS	condition anti-jerk active
B_AUTGET	PROKON		EIN	condition automatic gearbox
B_BREMS	GGEGAS		EIN	condition: brake operated
B_DASHV			EIN	condition dashpot delayed
B_FGR	MDFAW		EIN	condition: driver's set engine torque determined by cruise control
B_GWHS	BBGANG		EIN	Condition gear change on manual transmission vehicle
B_HPNMOT	ARMD		AUS	condition high-point speed oscillation
B_JNIAR	ARMD		AUS	condition initialization of anti-jerk function
B_JNIARV	ARMD		AUS	condition initialization of the filter function is delayed
B_KUPGW	ARMD		AUS	condition clutch applied until shifting of gear is detected
B_KUPPL	SWADAP		EIN	EGAS Condition clutch is disengaged
B_LL	MSF		EIN	Condition idle
B_LSD	MDFAW		EIN	condition: limitation of positive torque gradient active
B_SA	MDRED		EIN	Condition fuel cut-off
B_STEND	BBSTT		EIN	condition end of start
B_TPNMOT	ARMD		AUS	condition low-point speed oscillation
B_TVARS	ARMD		LOK	condition anti-jerking function dynamically active
B_WK			EIN	condition: converter lockup clutch closed
DMAR_W	ARMD		AUS	delta torque anti-jerk
FDAR	ARMD		AUS	amplification factor for anti-jerk intervention
FLRAR	ARMD		AUS	amplification factor for modelling of external load
GANGI	SWADAP		EIN	Engaged gear
KIFZ_W	ARMD		AUS	amplification of vehicle model
MDBES_W	ARMD		AUS	Acceleration torque
MDVERL_W	MDVER		EIN	Resistant torque of the engine
MIFA_W	MSF		EIN	desired indicated engine torque
MISOLV_W	MDKOG		EIN	indicated resultant nominal torque before torque limitation
MKAR_W	ARMD		AUS	calculated clutch torque for anti-jerk function
MLAST_W	ARMD		AUS	Estimated load moment
NDAR_W	ARMD		AUS	Difference RPM for torque control
NDFIL_W	ARMD		AUS	filtered engine speed difference
NDIFFOG_W	ARMD		AUS	Threshold engine speed difference for reset of AR during braking
NDIFF_W	ARMD		AUS	engine speed difference for ISC amplification
NMOD_W	ARMD		AUS	engine speed from model
NMOT_W	SWADAP		EIN	engine speed
TMOT	SWADAP		EIN	Engine temperature
VFZG	SWADAP		EIN	vehicle speed (km/h)

### FW ARMD 14.10 Fixed Values

Parameter	Value	Description
A0		transmission coefficient
A1		transmission coefficient
A2		transmission coefficient
B1		transmission coefficient
B2		transmission coefficient
CWARMD		Code word anti jerk function
DNFILO		upper threshold of filter output gradient ndfil
DVFZAR		Hysteresis for vehicle speed limit during AR (Anti jerk)
NARAO		upper engine speed threshold for anti-jerk function active
NARASTG		RPM threshold in higher gear for AR active
TAREIN		lockup time for anti-jerk function
TMAR		Lower TMOT threshold for AR release
TMLAST		blocking time until the initialization of the AR is triggered at deceleration
TVARS		delay time until antisurge is inactive again
TZSPINI		Resting time for filter initialisation
VARAU		vehicle speed for anti-jerk active





## FB ARMD 14.10 Detailed description of function

### Function purpose

The anti-jerk function detects oscillations of the power train and smoothens them using phase correct torque interventions. The torque intervention is converted into ignition angle offset by the torque interface.

### Desired phase position of the torque intervention

In order to smoothen the power train oscillation efficiently, the torque intervention should be counterwise to the engine speed oscillations. Therby the same effect is achieved, as if the attenuation coefficient of the drive shaft is increased.

### Operation pattern of anti-jerk function

Basic idea: A reference speed without oscillation and corresponding to the desire of the driver is evaluated. The difference between desired and actual engine speed isolates the oscillation. A delta torque is conterset to this oscillation. Realization: A simple vehicle model consisting of an integrator with the constant kifz\_w. Input of this integrator is the difference between the calculated coupling torque mkar\_w and the load torque mlast\_w; output is the model engine speed nmod\_w. The engine speed difference ndiff\_w between model engine speed nmod\_w and engine speed nmot\_w serves now as basis for the torque intervention as well as for the calculation of the load torque. The load torque is evaluated proportional to the engine speed difference, the factor flrar is taken from the corresponding char. line. The engine speed difference ndiff\_w contains besides the oscillation part another offset. This offset is filtered in 50 ms scan rate through a discrete low pass of 2nd order. (Coefficients of the nominator polynomial are denoted A0, A1 and A2, of the denominator polynomial 1, B1 and B2. The filtered offset ndfil\_w is subtracted from the differential engine speed and gives the engine speed oscillation ndar\_w. Proportionally to this engine speed and using the factor fdar, a delta torque as torque intervention is calculated. If this intervention lays between the limits KFDMDARU and KFDMDARO it is set to zero.

### Activation conditions

The model is always active, just the intervention can be switched off.

## APP ARMD 14.10 Application hint

### Conditions for calibration of anti-jerk

The basic calibration of the vehicle must have been done. This includes the compensation for transition (ÜK) and all functions for the torque interface.

#### 1. Evaluation of the integer constant kifz\_w and flrar

##### Coarse application:

Drive on the road (flat surface, no hills) with constant speed in respective gear with deactivated anti-jerk function (fdar=0). Then execute a change in load and register the calculated coupling torque mkar\_w and the speed nmot\_w.

Evaluation of integrator constant as follows: at a load step the torque jump is approximately delta M (in %) and the speed approximately rises with constant gradient gradn (in RPM/s). kifz\_w is then calculated from gradn/(delta M). A typical value for 2nd gear is 4.6\*100/MDNORM [RPM/(s\*%)].

##### Fine application:

Driving on flat surface. Setting of the product kifz\_w\*flrar on a fixed value (recommendation: 15). Realization of load jumps with registration of mkar\_w, mlast\_w, nmot\_w, ndiff\_w. Variation of the couple kifz\_w, flrar (with constant product!) until ndiff\_w stays approximately constant at load jump.

In principle the following is valid for the amplification factor flrar: high factors cause a reduction of the offset ndfil\_w, but also a big phase advance of ndiff\_w.

#### 2. Evaluation of filter parameters

Low pass in 50 ms scan rate: transmission function has the form  $G(z) = Z(z)/N(z)$  with

$$Z(z) = A0 + A1*z^{(-1)} + A2*z^{(-2)} \quad N(z) = 1 + B1*z^{(-1)} + B2*z^{(-2)}$$

Selection of one of the low pass below, according to the appearing jerk frequency:

TP No.	limit freq.	A0	A1	A2	B1	B2
1	0.67 Hz	.0095	.0191	.0095	-1.7056	.7437
2	0.8 Hz	.0134	.0267	.0134	-1.6475	.7009
3	1.0 Hz	.0201	.0402	.0201	-1.561	.6414

Recommended is low pass No. 3. The attenuation of the jerk frequency is determined by the distance between jerk frequency and filter cut-off frequency. The bigger the filter cut-off frequency, the smaller the time the filter needs to stabilize. Attenuation: any modification of a single coefficient of G(z) is not allowed!

#### 3. Evaluation of fdar

Recommendation is fdar = .67\*100/MDNORM (%/RPM. Increase of attenuation by enlargement of fdar, reduction of fdar decreases the attenuation.

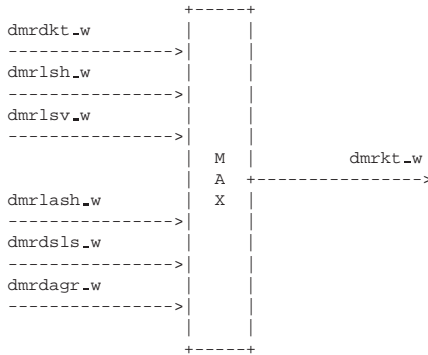
#### 4. Thresholds KFDMDARO and KFDMDARU

In case the delta torque for the intervention is within these thresholds, it is set to zero. This avoids undesired instabilities

of the ignition angle. Typical values: KFDMDARU=-5\*100/MDNORM [%], KFDMDARO= 5\*100/MDNORM [%].

## MDTRIP 1.20 Calculation of torque reserve for short trip

### FDEF MDTRIP 1.20 Function definition



### ABK MDTRIP 1.20 Abbreviations

Variable	Source	Type	Description
DMRDAGR_W		EIN	Torque reserve for EGR- diagnosis
DMRDKT_W	DKAT	EIN	torque reserve for catalyst monitoring
DMRDSLS_W	KHMD	EIN	Torque reserve for SAI- diagnosis
DMRKT_W	MDTRIP	AUS	Torque reserve during quicktest
DMRLASH_W	DLSAHK	EIN	torque reserve for lambda sensor ageing diagnosis downstream cat
DMRLSH_W	DLSH	EIN	torque reserve for lambda sensor diagnosis downstream cat
DMRLSV_W		EIN	torque reserve for lambda sensor diagnosis upstream Kat

### FW MDTRIP 1.20 Fixed Values

Parameter	Value	Description

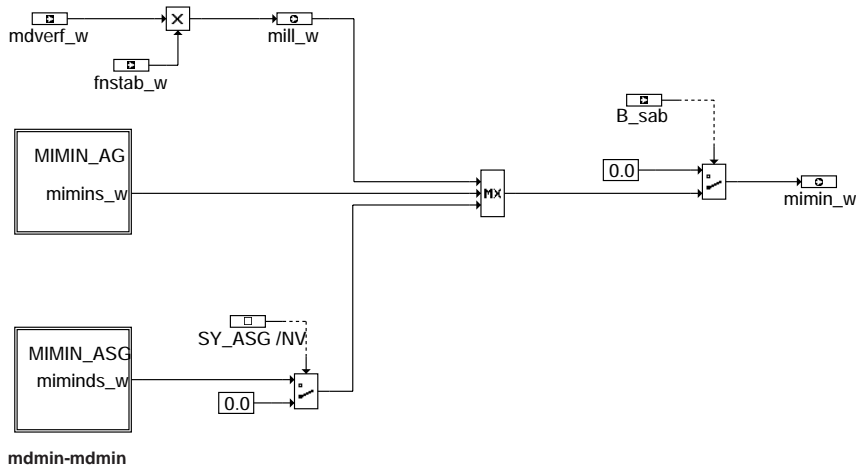
### FB MDTRIP 1.20 Detailed description of function

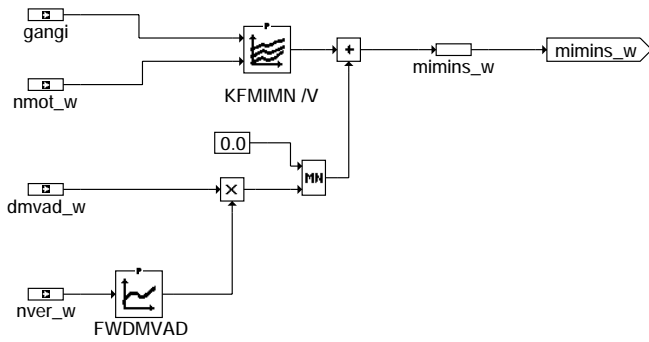
The torque reserve dmrkt\_w will be done by maximum choice of each short-trip reserves.

### APP MDTRIP 1.20 Application hint

## MDMIN 10.30 Minimum engine torque coordination

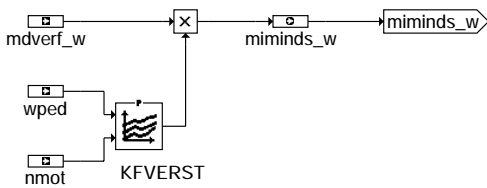
### FDEF MDMIN 10.30 Function definition





### Kompensation der Momentendifferenz im Schubetrieb bei Automatikgetriebe

mdmin-mimin-ag



### Kompensation der Verlustmomente bei ASG

mdmin-mimin-asg

#### ABK MDMIN 10.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FWD MVAD	NVER_W		KL	factor for the weighting of dmvad_w in %MDMIN
KFMIMN	GANGI	NMOT_W	KF	minimum drag torque
KFVERST	WPED	NMOT	KF	weighting map for increasing control of friction torque
SY_ASG			SYS	automatic standard transmission

Variable	Source	Type	Description
B_SAB	MSF	EIN	Condition fuel cut-off requested
DMVAD_W	MDVERAD	EIN	Delta resistant torque from resistant torque adaptation
FNSTAB_W	MDNSTAB	EIN	Factor for speed stabilization
GANGI	SWADAP	EIN	Engaged gear
MDVERF_W	MDVER	EIN	Filtered charge torque
MILL_W	MDMIN	AUS	Indicated engine torque at idle
MIMINDS_W	MDMIN	AUS	weighted torque loss in case of AST
MIMINI_W	MDMIN	AUS	text of Mr. Herrmann
MIMINS_W	MDMIN	LOK	minimum drag torque
MIMIN_W	MDMIN	AUS	Minimal engine torque
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
NVER_W		EIN	Quotient of engine speed
WPED	GGPED	EIN	Standardized accelerator pedal angle

#### FW MDMIN 10.30 Fixed Values

Parameter	Value	Description
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## FB MDMIN 10.30 Detailed description of function

During fuel cut-off readiness the torque to be indicated at the minimum 0 is outputted. Otherwise the torque to be indicated at the minimum is taken from a maximum selection. To achieve a self-stabilization, the sum from  $mdverl_w$  and  $mdwan_w$  is weighted with the quotient  $nstat/nmot_w$ . After the initialization the sum is weighted with 1 until the actual speed  $nmot_w$  has reached the desired speed  $nstat$  (MDNSTAB).

MIMIN\_AG:

On certain automatic transmission types a noise develops, if the direction of the torque flow changes and if the absolute value of the fuel cut-off torque is greater than that of the indicated torque. The map KFMIMN serves to limit the indicated torque to an upper value in such cases. It is thereby possible to suppress the disturbing transmission noises. The values may not be greater than the minim torque loss ( $dmvad=0$ ,  $mds(nstat)$ ,  $mdsm=0$ ,  $mdko=0$ ,  $mdgen(nstat)$ ,  $mdsl=0$ ,  $mdslp=0$ ,  $mdns=0$ ) at no  $nmot$ . In case of an easily moving transmission, a negative  $dmvad$  results. KFMIMN would in this case lie above  $mimin$  and thereby contribute to an acceleration. Therefore  $dmvad$  is subtracted from KFMIMN in this case. The weighting factor FWDVMAD is to have the value 1 for all  $nver_w > 1$ . FWDVMAD is to travel toward 0 for smaller  $nver$ . If there are no problems with "noisy automatic transmissions", then FWDVMAD and KFMIMN should equal 0.

MIMIN\_ASG:

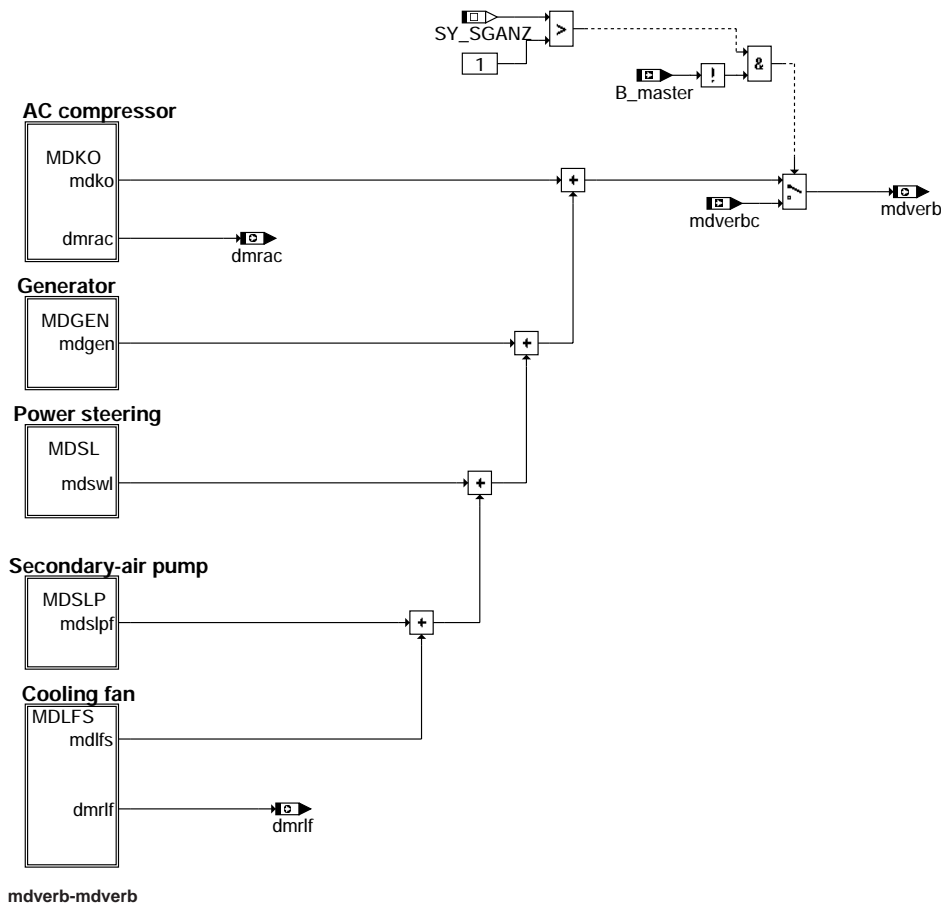
By the factor  $fnstab_w$ , the friction torque ( $mimini_w$ ) is not compensated when  $nmot$  is above  $nstat$ . The friction torque compensation with  $mdverf_w$ , however, is necessary when the desired wheel torque is preset. Therefore a switch is performed with the factor  $\{0, \leq 1.0\}$  from KFVERST ( $f(wpel_w, nmot_w)$ ) between the conventional calculation  $mimini_w$  and the friction torque compensation  $mdverf_w$ . In the range of fuel cut-off monitoring and at idle a switch to  $mimini_w$  is performed by entering the value 0 into KFVERST. With the value KFVERST=1,  $mimin$  is set to  $mdverf_w$ .

## APP MDMIN 10.30 Application hint

Data entry into the maps KFMIMN and KFVERST is safety-relevant. A maximum engine speed of 1500 may not be exceeded, as long as the end of idle range is not detected by both potentiometers. Attention, therefore, need to be paid that that by too large values in the maps KFMIMN and KFVERST no engine torque will result that leads to the speed threshold being exceeded.

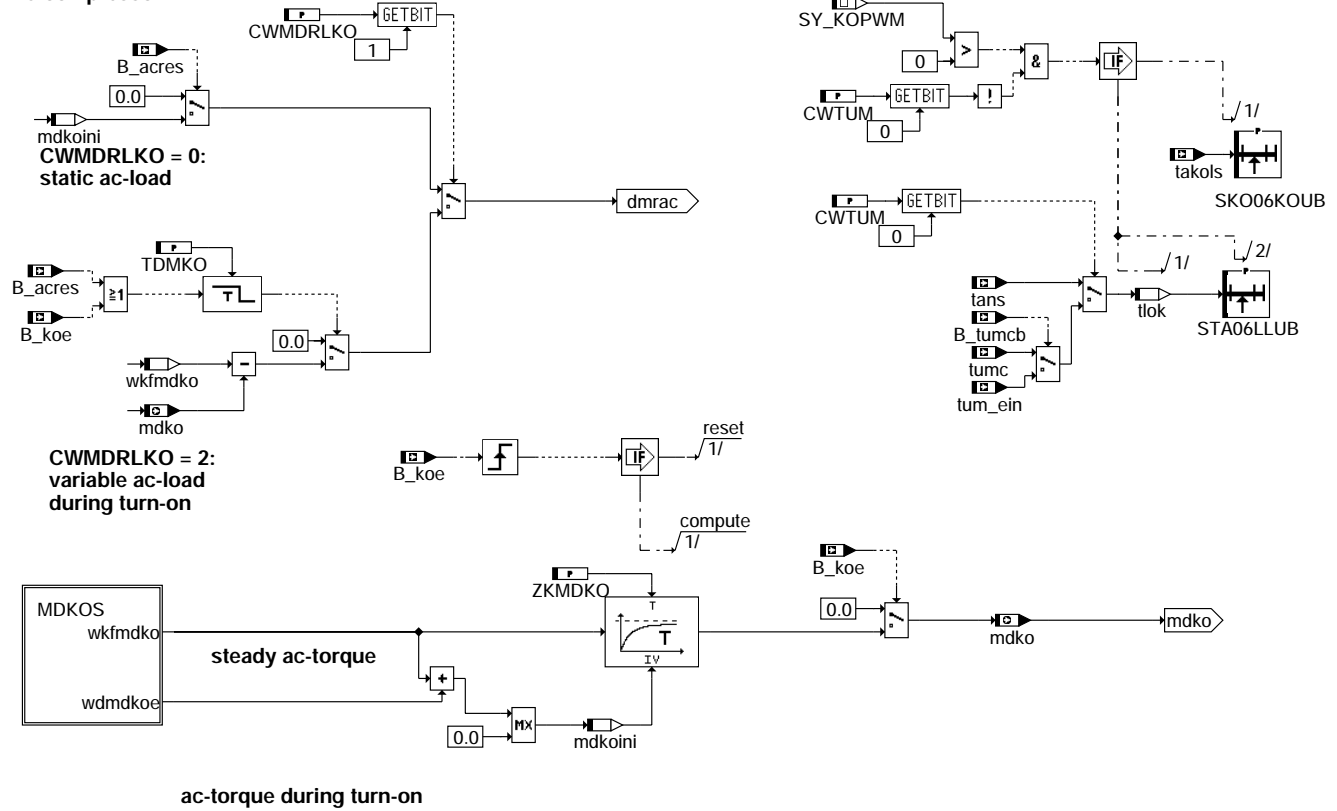
## MDVERB 12.170 Torque demand by auxiliary systems (e.g. air conditioner, misc. consumers)

### FDEF MDVERB 12.170 Function definition



determination of accessory torque demands

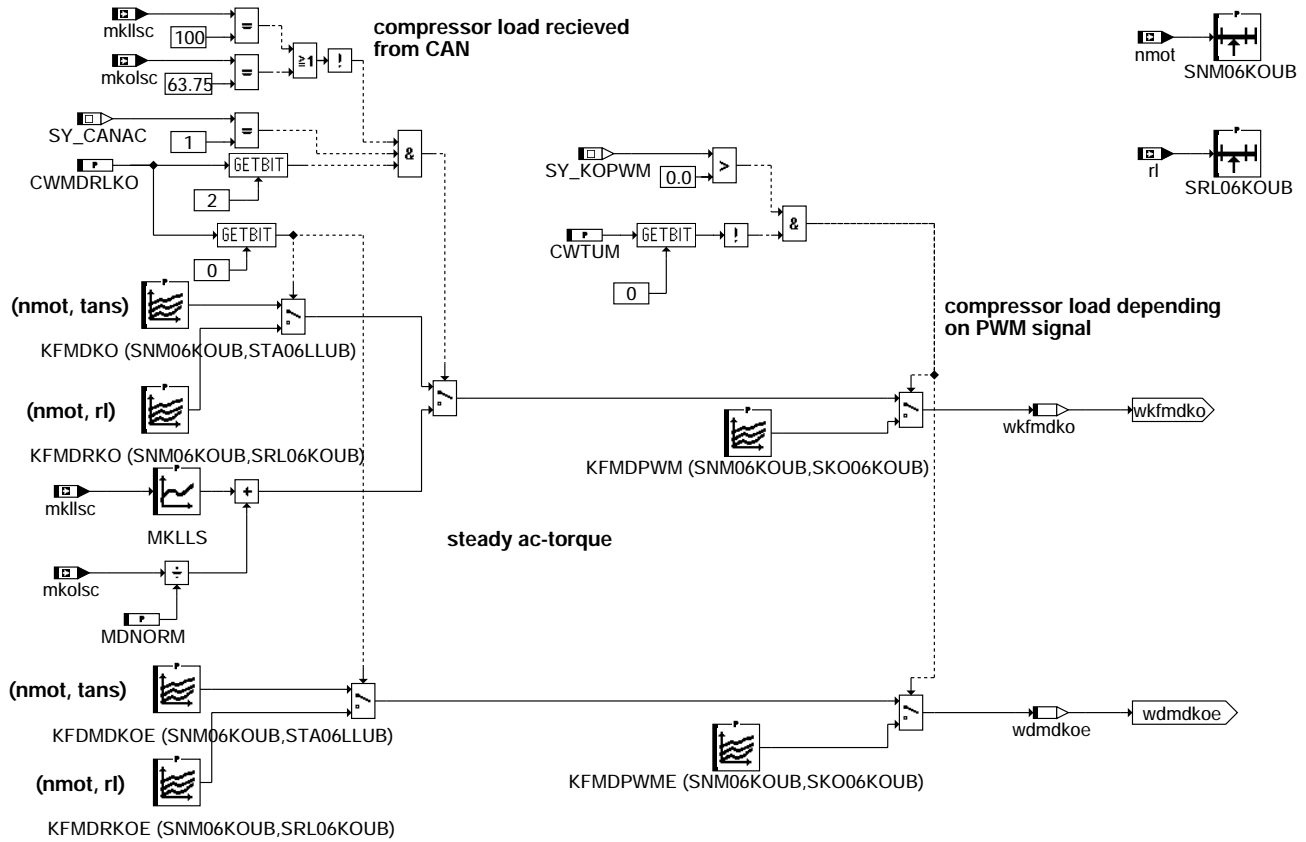
### AC compressor



mdverb-mdko

mdverb-mdko

AC-compressor torque demand

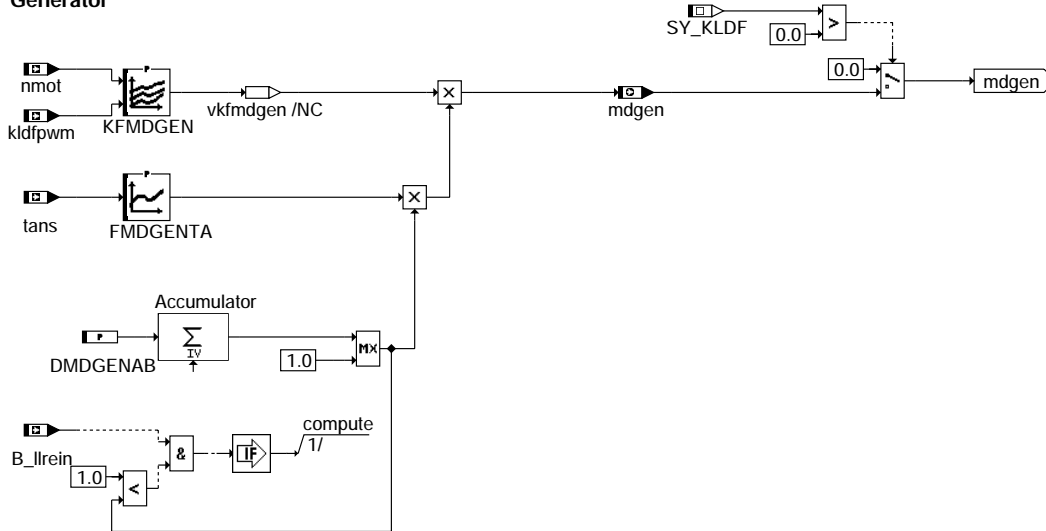


ac-torque during turn-on

mdverb-mdkos

AC-compressor torque demand: steady state and initial value

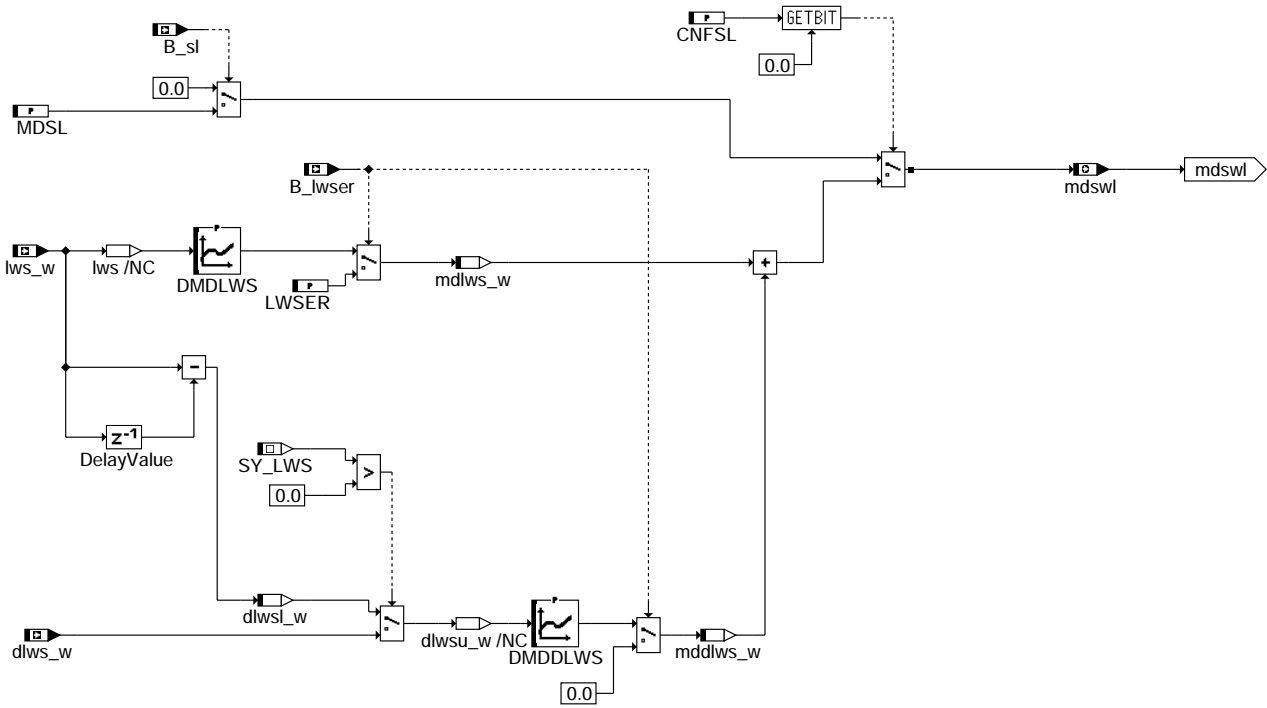
Generator



mdverb-mdgen

alternator torque demand

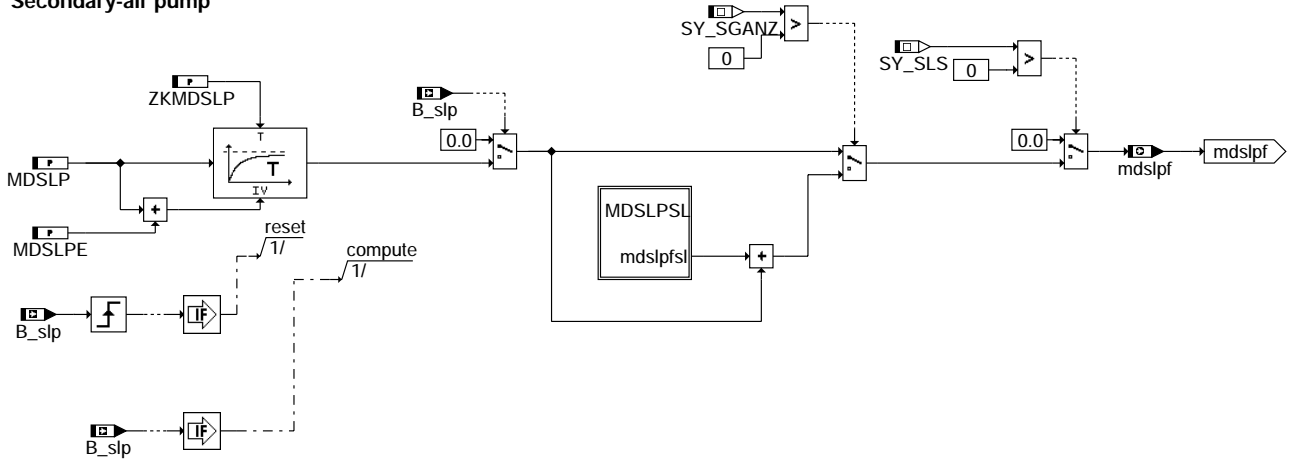
## Power steering



mdverb-mdsl

torque demand of hydraulic power steering pump

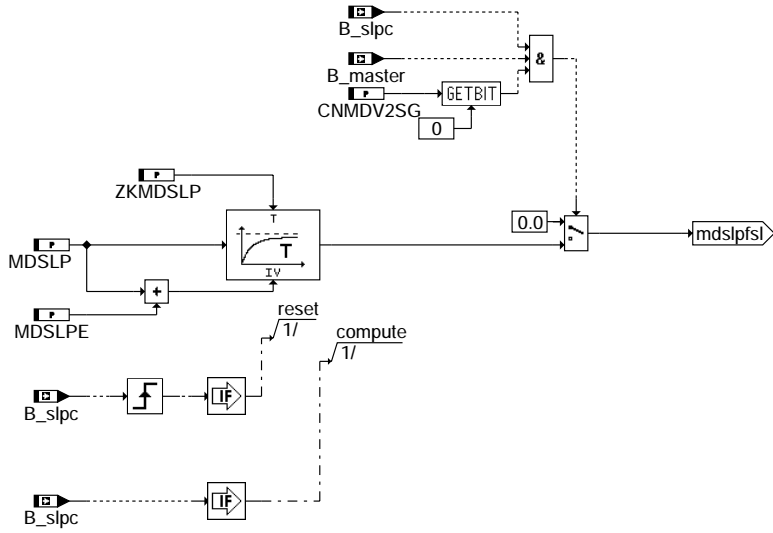
## Secondary-air pump



mdverb-mdslp

torque demand of secondary air pump

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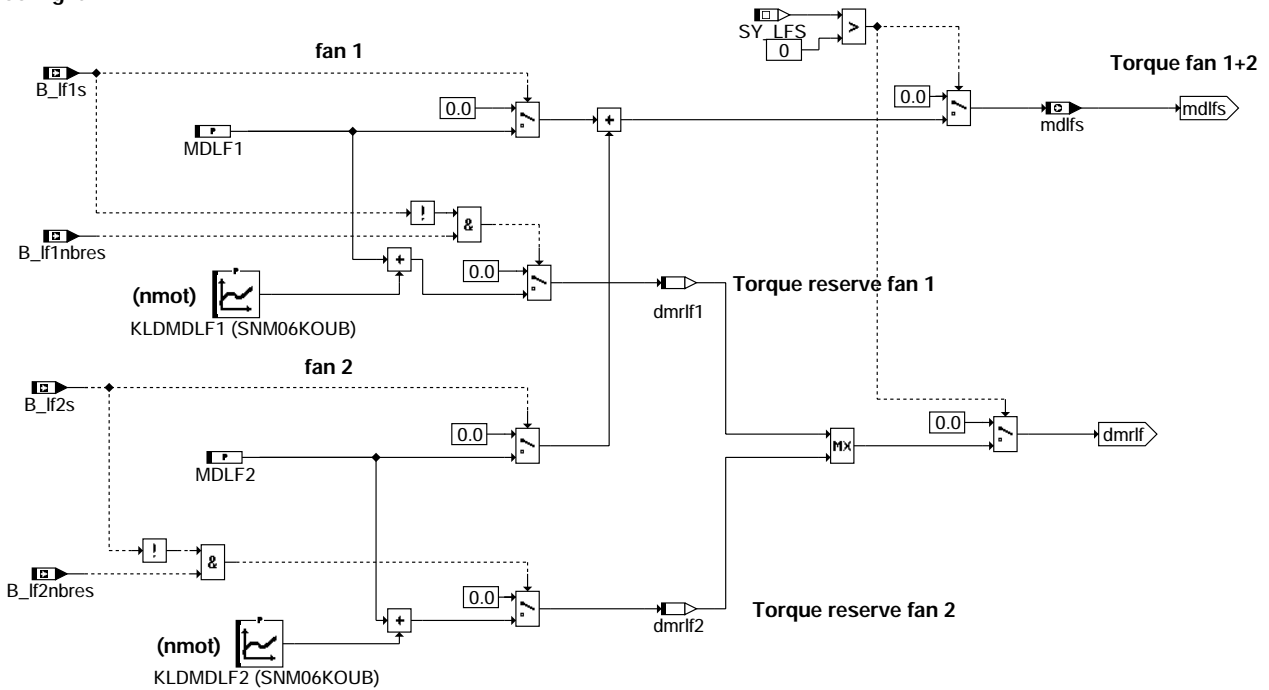


**mdverb-mdslpsl**

torque demand of secondary air pump for slave (multi-ECU system)

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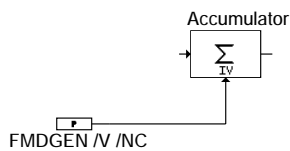
**Cooling fan**



**mdverb-mdlfs**

torque demand of fan

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**mdverb-init**

initialization

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## ABK MDVERB 12.170 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CNFSL			FW	Codeword to allow for the steering angle
CNMDV2SG			FW	code word torque request of the accessories for 2-ME-concept
CWMDRLKO			FW	codeword: torque loss ac-compressor dependend of rl, nmot
CWTUM			FW	configuration: ambient temperature for ac-compressor
DMDLWS	DLWSU_W		KL	Torque for power steering function of the
DMDGENAB			FW	decrement of temperature factor generator torque
DMDLWS	LWS		KL	Torque for power steering
FMDGENTA	TANS		KL	factor: generator torque due to temperature
KFDMDKOE	NMOT	TLOK	KF	Starting value torque filter when air-conditioner compressor is activated
KFMDGEN	NMOT	KLDFPWM	KF	Torque intake generator
KFMDKO	NMOT	TLOK	KF	map for torque needed for air condition
KFMDPWM	NMOT	TAKOLS	KF	steady state load of ac-compressor for PWM-signal of its load
KFMDPWME	NMOT	TAKOLS	KF	initial load of ac-compressor for PWM-signal of its load
KFMDRKO	NMOT	RL	KF	look-up-table: torque loss dependend of rl, nmot
KFMDRKOE	NMOT	RL	KF	look-up-table: torque loss dyn. part dependend of rl, nmot
KLDMDLF1	NMOT		KL	Characteristic curve reserve torque fan
KLDMDLF2	NMOT		KL	Characteristic curve reserve torque fan 2
LWSER			FW	Torque for power steering without angle sensor
MDLF1			FW	stationary torque for cooling fan 1
MDLF2			FW	stationary torque for cooling fan 2
MDNORM			FW	maximum limit indicate engine torque
MDSL			FW	Torque request of the power steering
MDSLPE			FW	Torque to compensate the secondary air pump (stat.)
MKLLS	MKLLSC		KL	Torque to compensate the secondary air pump (switching on)
SKO06KOUB	TAKOLS		SV	torque needed for air condition fan
SNM06KOUB	NMOT		SV	Distribution PWM-signal: load of ac-compressor
SRL06KOUB	RL		SV	distribution for ac-compressor torque function
STA06LLUB	TLOK		SV	6 air charge set points for A/C-compressor torque loss
SY_CANAC			SYS	temperature: ambient air, PWM -signal of AC/compressor
SY_KLDF			SYS	systemconstant: AC-compressor signal from CAN
SY_KOPWM			SYS	system constant for generator DF-signale
SY_LFS			SYS	PWM-compressor-signal enabled
SY_LWS			SYS	System constant Fan Control configuration
SY_SGANZ			SYS	system constant steering angle via CAN
SY_SLS			SYS	system constant number engine control unit
TDMKO			FW	system constant for engines with secondary air pump
ZKMDKO			FW	debounce time after torque reserve: ac-clutch
ZKMDSLPE			FW	time constant A/C compressor-load decreasing
			FW	Time constant to decrease the switching-on torque of the sec. air pump
Variable	Source		Type	Description
B_ACRES	SWADAP		EIN	Condition for increasing the torque reserve by AC-stand-by
B_KOE	KOS		EIN	Condition for AC-compressor ON
B_LF1NBRES	LFS		EIN	Condition for torque reserve for engine cooling fan step 1 normal operation on
B_LF1S	LFS		EIN	fan 1 on condition
B_LF2NBRES	LFS		EIN	Condition for torque-reserve build at engine-fan stage 2, normal operation on
B_LF2S	LFS		EIN	fan 2 on condition
B_LLRIN	LLRMD		EIN	Condition idle speed control is active
B_LWSER			EIN	Error in the path of the steering angle
B_MASTER			EIN	Condition MASTER-ECU
B_SL			EIN	Condition power steering
B_SLP	AK		EIN	condition for secondary air pump
B_SLPC			EIN	condition for secondary air pump via CAN (2-ME-concept)
B_TUMCB			EIN	Condition: Fault in CAN ambient-temperature information
DLWSL_W	MDVERB		LOK	
DLWS_W			EIN	
DMRAC	MDVERB		AUS	Torque reserve for AC-compressor
DMRLF	MDVERB		AUS	Torque reserve for cooling fan
DMRLF1	MDVERB		LOK	Torque reserve, fan level 1
DMRLF2	MDVERB		LOK	Reserve torque, fan level 2
KLDFPWM			EIN	generator signale as PWM-signale filtrated
LWS_W			EIN	Steering angle
MDDLWS_W	MDVERB		LOK	Torque depending on the steering angle gradient
MDGEN	MDVERB		AUS	Torque consumption generator
MDKO	MDVERB		AUS	torque needed for air condition
MDKOINI	MDVERB		LOK	compressor torque for turn-on
MDLFS	MDVERB		AUS	Torque needed by the engine cooling fan
MDLWS_W	MDVERB		LOK	Torque depending on the steering angle
MDSLPE	MDVERB		AUS	Torque needed by the secondary air pump
MDSWL	MDVERB		AUS	torque loss: power steering
MDVERB	MDVERB		AUS	Torque request of the accessories
MDVERBC			EIN	Torque request of the accessoires via CAN (2-ME-Concept)
MKLLSC			EIN	Compressor-fan signal from CAN message Clima 1
MKOLSC			EIN	Compressor load signal from CAN message Clima 1
NMOT	SWADAP		EIN	engine speed
RL	SWADAP		EIN	relative air charge
TAKOLS			EIN	air-condition information as PWM
TANS	SWADAP		EIN	Intake air temperature
TLOK	MDVERB		LOK	ambient temp. for ac-compressor load
TUMC			EIN	Ambient temperature from CAN combi
TUM_EIN			EIN	ambient temperature for soak time calculation





## ABK MDVER 5.90 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CNFMDVER			FW	Codeword to configure the function MDVER
DMDNSM	TMOT		KL	Torque offset for after cranking compensation
DMVERLMN			FW	Minimum torque-loss threshold
KFMDS	NMOT_W	RL_W	KF	map for engine drag torque
KFMDSZAS	NMOT_W	RL_W	KF	map for engine drag torque during cyclinder cut off
MDSH	FHO		KL	Part of the resistant torque depending on altitude
MDSM	TMOT		KL	temperatuer share of engine friction torque
MDSMZAS	TMOT		KL	temperatuer share of engine friction torque during cylinder cut off
SNM16OPUW	NMOT_W		SV	16 speed set points for ?
SRL11OPUW	RL_W		SV	set point distribution relative charge
SY_ZAS			SYS	system constant cylinder deactivation ZAS included
ZFMDVERL			FW	Time constant for filtering the resistant torque
ZMDNSM	TMOT		KL	time constant for decay of torque offset after cranking

Variable	Source	Type	Description
B_DMVERLIN	MDVER	LOK	Condition dmverl = 0
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_SA	MDRED	EIN	Condition fuel cut-off
B_ZASAKT		EIN	Cylinder cut-out active
DMVAD_W	MDVERAD	EIN	Delta resistant torque from resistant torque adaptation
DMVERL_W	MDVER	AUS	Resistant torque after DT1-filter
FHO	BGPU	EIN	Correction factor altitude
KFMDSZAS_W	MDVER	LOK	map for engine drag torque duringcylinder cut off
KFMDS_W	MDVER	LOK	map for engine drag torque
MDNS_W	MDVER	AUS	torque after start
MDSMZAS_W	MDVER	LOK	Drag torque temperature component during cylinder cut off
MDSM_W	MDVER	LOK	Drag torque temperature component
MDS_W	MDVER	LOK	engine drag torque
MDVERB	MDVERB	EIN	Torque request of the accessories
MDVERF_W	MDVER	AUS	Filtered charge torque
MDVERL_W	MDVER	AUS	Resistant torque of the engine
MDVERV_W	MDVER	LOK	Unfiltered torque loss
MDWAN_W	MDWAN	EIN	Torque request of the torque converter
NMOTLL	BGNMOT	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
NSOL	LLRNS	EIN	idle reference speed
RL_W	EGFE	EIN	relative air charge (Word)
TMOT	SWADAP	EIN	Engine temperature

## FW MDVER 5.90 Fixed Values

Parameter	Value	Description
CNFMDVER		Codeword to configure the function MDVER
DMVERLMN		Minimum torque-loss threshold
ZFMDVERL		Time constant for filtering the resistant torque

## FB MDVER 5.90 Detailed description of function

The calculated engine-torque loss, `mdverl_w`, is made up of the engine drag torque `mds`, the adapted delta drag torque, `dmvad_w`, and the torque demand from the auxiliary equipment, `mdverb`.

The engine drag torque, `mds`, is made up of the drag torque, `KFMDS`, dependent on the engine speed, `nmot`, and the relative load, `r`, the engine-temperature dependent corrective torque, `MDSM`, and the altitude-dependent component, `MDSH`.

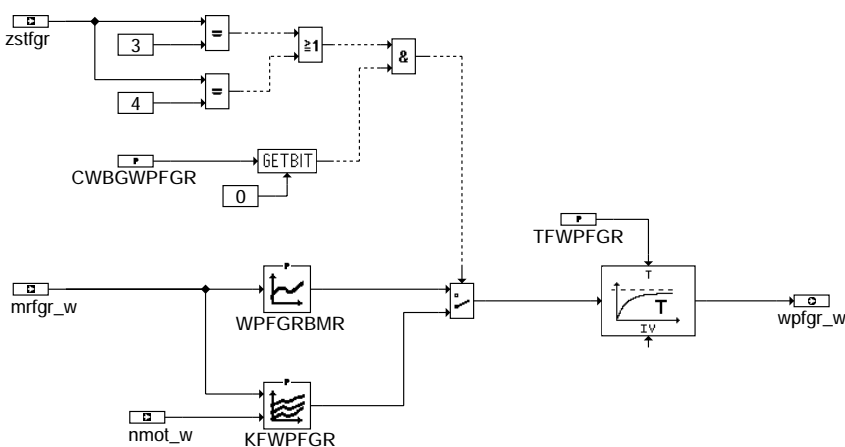
In order to meet the higher torque demand from the engine during the post-start phase, an additional torque, `DMDNSM`, is included in the calculations as of the end of the start-up phase (`B_llrein = 1`) as a function of the engine's temperature. This additional torque is gradually decreased down to zero again over a filter using the temperature-dependent time constant `ZMDNSM`. Besides allowing for `mdverl_w`, the necessary change in the torque loss, `dmverl_w`, needed to calculated the vehicle-operator demand also takes the change in the converter torque, `mdwan_w`, into account. The change is calculated and passed over a highpass filter.

## APP MDVER 5.90 Application hint

- Adaptation of KFMD5:** KFMD5 constitutes the drag torque of the engine and is determined during non-firing operation of the engine torque at drag test bench. The engine must be warm to do this (min. 80 °C for the oil temperature). The torque is determined for various speed and load points. This is needed to drag the non-firing engine. This map has already been established during basic engine parameterization at the engine test bench.
- Adaptation of MDSM:** MDSM contains the temperature influence from the engine drag torque (internal friction). The temperature influence is particularly high for the changed oil viscosity and hence by this, to find the thereby associated change in the friction torque of the engines. The influence of the temperature is determined in the climatic chamber. The set speed is kept constant throughout warming-up from lowest possible start-up temperature until the engine is warm. The necessary target torque is then determined over the temperature. The value for the warm engine must correspond to KFMD5 for the given operating point of the engine and MDSM forms the difference between mimin and mds for lower temperatures. It is however important to carry out these measurements at differing set speeds, engine and oil qualities (new, used oil, viscosity range). The temperature datapoints of MDSM are run through dynamically, i.e. the engine has already been running for some time and passes through the various temperature datapoints as the engine temperature rises. As this has a very large influence on the oil viscosity, an adjustment is needed immediately after the start-up phase for the temperature compensation.
- Adaptation of MDSH:** The adaptation of the altitude component is executed with the neutral values of 0 % as part of the basic adaptation. These values then apply for the altitude of the location of the adaptation (e.g. Schwieberdingen is 350 m above sea level). The drag torque decreases as the altitude increases. This is because the resistance falls by the change in the gas (pressure difference between manifold and exhaust sides become less). The drag torque will increase for a falling altitude (compare with the altitude for the basic adaptation). The adaptation is made by transferring the different of the I-component of the idle-speed control (comparison between altitude for the basic application and the current altitude for the same load on the engine).
- Adaptation of DMDNSM:** DMDNSM serve as a correction between the friction torque for a stationary and a dynamic oil viscosity. The stationary oil viscosity is given when the oil is held in a rigid state at a constant temperature over a longer period of time. The oil molecules have increased in length here and hence the viscosity of the oil becomes higher. It is only after the oil has been thoroughly mixed through again by mechanical pumping within the lubrication circuit that it has the viscosity that matches MDSM. This is then the viscosity referred to as the dynamic oil viscosity.
- Adaptation of ZMDNSM:** This time constant is for gradual decrease of the correction DMDNSM. The interventions by the controller are observed during the post-start phase for several cold and warm start-up's in order to adapt this time constant. The controller will reach a neutral values after a longer period of time. The controller must however apply this correction for such time until this is the case, whereby this correction is not yet part of the characteristic curve DMDNSM. This correction for the controller should no longer occur once adaptation of MDSM and ZMDNSM has finished.
- Adaptation of ZFMDVERL:** No sudden changes in mimin\_w are permitted. This is to prevent sudden changes in the accelerator-pedal characteristics. It is established using the filter ZFMDVERL how quickly the change in the lower limit for the driver torque can take place.

## BGWPFGR 2.10 Calculation variable, back-calculated pedal value for FGR

### DDEF BGWPFGR 2.10 Function definition



bgwpfgr-main

bgwpfgr-main



## ABK BGWPFGR 2.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWBGWPFGR			FW	Code word for %BGWPFGR
KFWPFGR	MRFGR_W	NMOT_W	KF	Inverse pedal characteristic for cruise mode
TFWPFGR			FW	Time constant of the filter for calculation of wpfgr_w
WPFGRBMR	MRFGR_W		KL	Back-calculated pedal value during acceleration with FGR

Variable	Source	Type	Description
MRFGR_W	MSF	EIN	relative torque demand from cruise control
NMOT_W	SWADAP	EIN	engine speed
WPFGR_W	BGWPFGR	AUS	Recalculated accelerator pedal position in cruise mode
ZSTFGR	FGRFULO	EIN	Status of vehicle-speed controller

## FW BGWPFGR 2.10 Fixed Values

Parameter	Value	Description
CWBGWPFGR		Code word for %BGWPFGR
TFWPFGR		Time constant of the filter for calculation of wpfgr_w

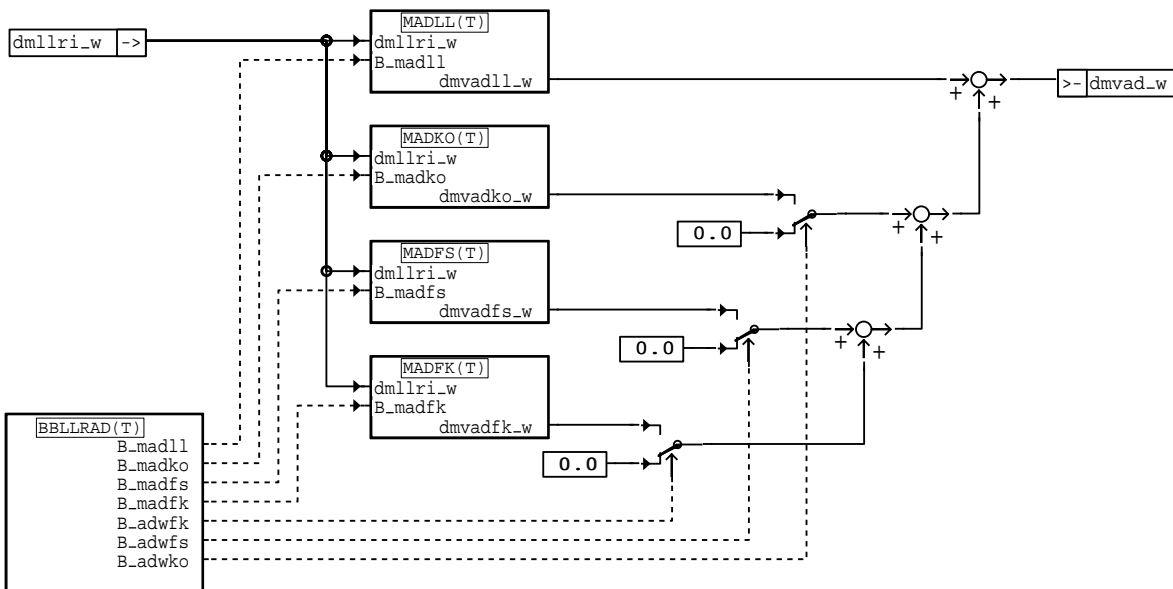
## FB BGWPFGR 2.10 Detailed description of function

A value for the pedal travel is calculated back from the relative torque demand of the vehicle-speed controller so as to be able to provide transmission control during operation of the vehicle-speed controller (FGR) as well with a parameter equivalent to the pedal-travel value for triggering gear shifting. This usually happens from an inverted pedal map. When appropriately coded, a separate characteristic curve is then used instead of this for accelerations by the vehicle-speed controller.

## APP BGWPFGR 2.10 Application hint

## MDVERAD 1.50 Adaptation of torque loss

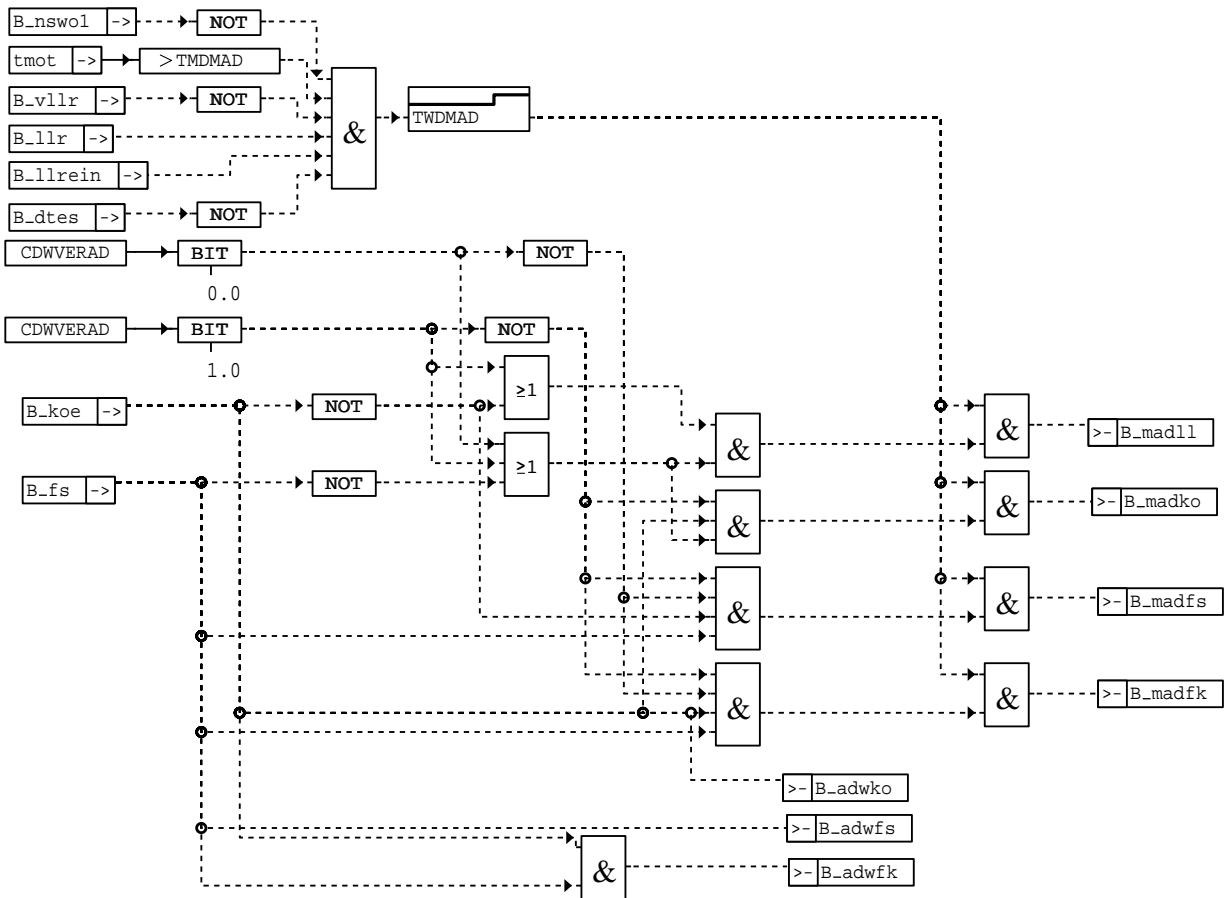
### FDEF MDVERAD 1.50 Function definition



### mdverad-mdverad

Overview of the demand adaptation: The demand adaptation is divided into 4 ranges:  
 -----  
 MADLL : Operation without air-conditioning compressor and without engaged drive driving position  
 MADKO : Operation with air-conditioning compressor and without engaged driving position  
 MADFS : Operation without air-conditioning compressor and with engaged driving position  
 MADFK : Operation with air-conditioning compressor and with engaged driving position

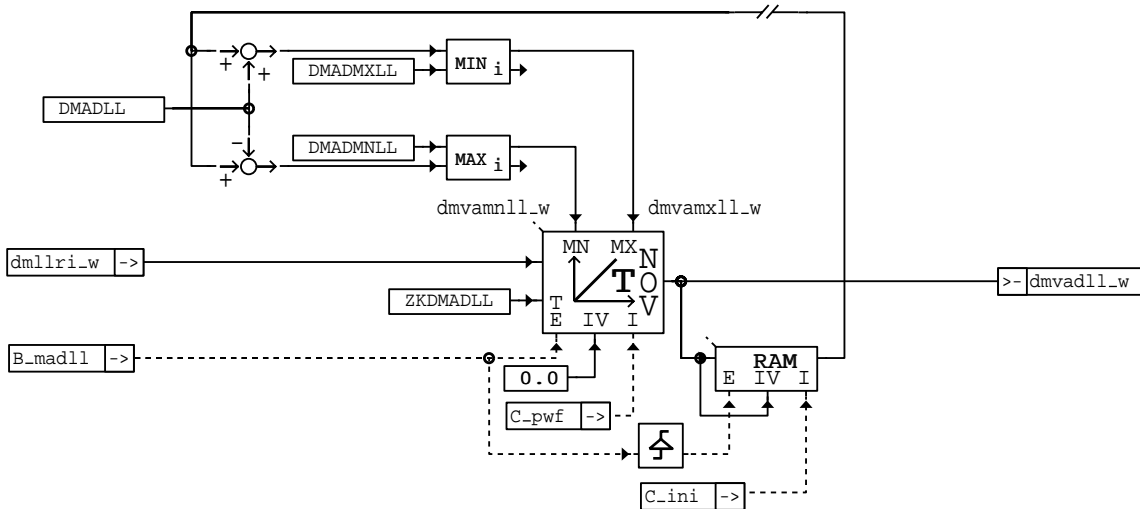
The choice of the current range is made in the BBLLRAD



mdverad-bllrad

**mdverad-bllrad**

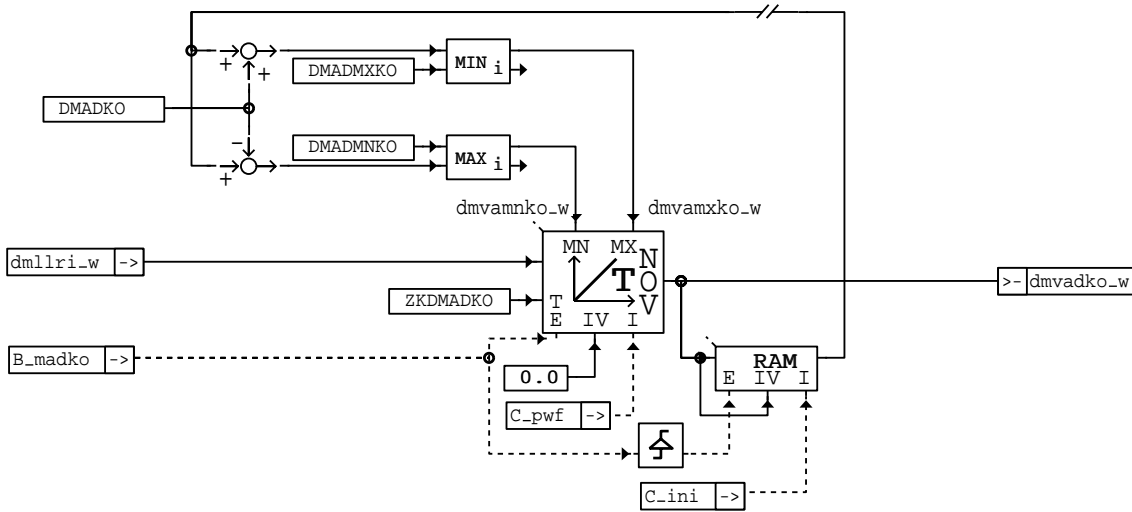
BLLRAD: Determination of the operating range and enabling of the adaptation in these ranges



mdverad-madll

**mdverad-madll**

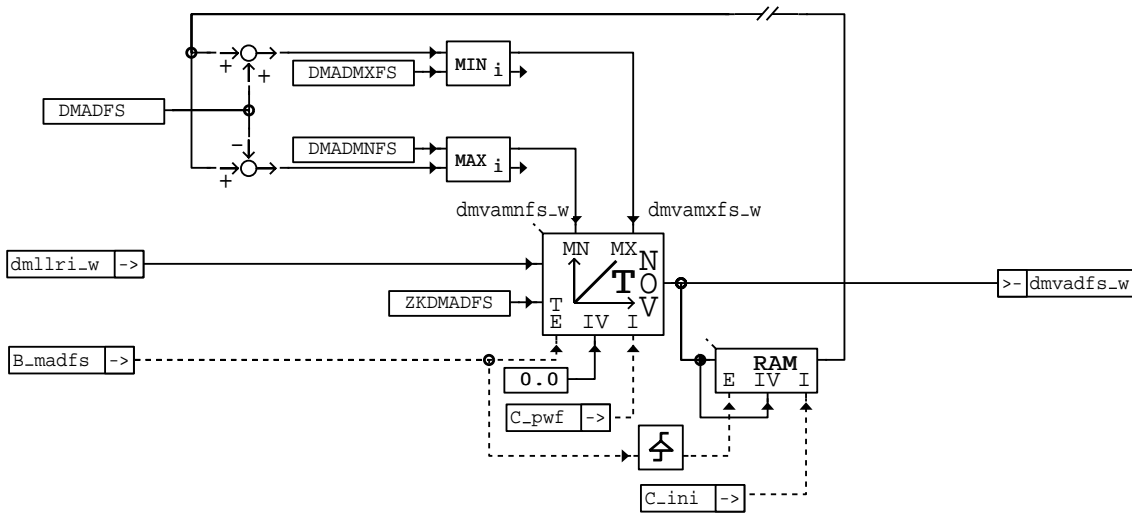
DMADLL :Adaptation for operation without air-conditioning system and without engaged driving position



mdverad-madko

**mdverad-madko**

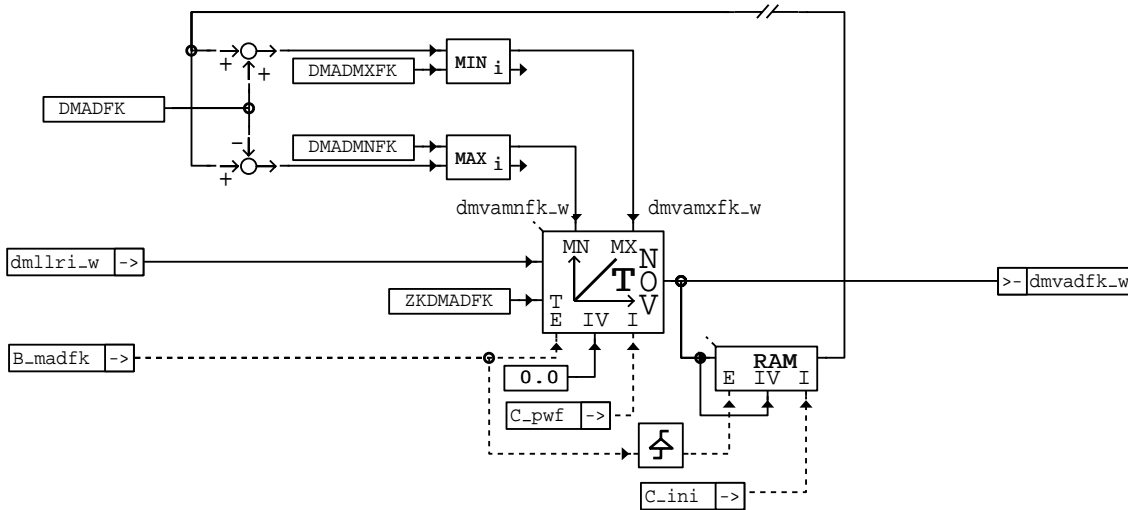
DMADKO :Adaptation for operation with air-conditioning system and without engaged driving position



mdverad-madfs

**mdverad-madfs**

DMADFS :Adaptation for operation without air-conditioning system and with engaged driving position



mdverad-madfk

**mdverad-madfk**

DMADFK :Adaptation for operation with air-conditioning system and with engaged driving position

**ABK MDVERAD 1.50 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CDWVERAD			FW	Codewort
DMADFK			FW	maximum adaptable change of resistant torque during one idle cycle AT-drvie + AC
DMADFS			FW	maximum adaptable change of resistant torque during one idle cycle AT in drive
DMADKO			FW	maximum adaptable change of resistant torque during one idle cycle compressor on
DMADLL			FW	maximum adaptable change of resistant torque during one idle cycle loadless
DMADMNFK			FW	lower limit for torque adaptation At in drive + AC compressor on
DMADMNFS			FW	lower limit for torque adaptation At in drive
DMADMNKO			FW	lower limit for torque adaptation AC compressor on
DMADMNLL			FW	lower limit for torque adaptation loadless
DMADMXFK			FW	upper limit for torque adaptation AT in drive + AC compressor on
DMADMXFS			FW	upper limit for torque adaptation AT in drive
DMADMXKO			FW	upper limit for torque adaptation AC compressor on
DMADMXLL			FW	upper limit for torque adaptation loadless
TMDMAD			FW	Engine temperature threshold to enable adaptation of resistant torque
TWDMAD			FW	Waiting time to enable adaptation of resistant torque
ZKDMADFK			FW	time constant for torque adaptation AT in drive and AC compressor on
ZKDMADFS			FW	time constant for torque adaptation AT in drive
ZKDMADKO			FW	time constant for torque adaptation AC compressor on
ZKDMADLL			FW	time constant for torque adaptation loadless

Variable	Source	Type	Description
B_ADWFK	MDVERAD	LOK	condition to use adaptation value for AT in drive and AC compressor on
B_ADWFS	MDVERAD	LOK	condition to use adaptation value for AT in drive
B_ADWKO	MDVERAD	LOK	condition to use adaptation value for AC compressor on
B_DTES	GKRA	EIN	Condition for active diagnosis of canister purge system
B_FS	BBGANG	EIN	Condition driving state (automatic gear box)
B_KOE	KOS	EIN	Condition for AC-compressor ON
B_LLR	LLRBB	EIN	condition idle speed control
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_MADFK	MDVERAD	LOK	condition for torque adaptation AT in drive and AC compressor on
B_MADFS	MDVERAD	LOK	condition for torque adaptation AT in drive
B_MADKO	MDVERAD	LOK	condition for torque adaptation AC-compressor on
B_MADLL	MDVERAD	LOK	condition for torque adaptation loadless
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_VLLR	LLRBB	EIN	Condition vehicle is moving with engaged gear
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DMLLR1_W	LLRRM	EIN	desired torque change from the idle speed control (I-)
DMVADF_K_W	MDVERAD	LOK	Delta resistant torque from resistant torque adaptation(B_fs=1 & B_ko=1)
DMVADF_S_W	MDVERAD	LOK	Delta resistant torque from resistant torque adaptation(B_fs=1)
DMVADKO_W	MDVERAD	LOK	Delta resistant torque from resistant torque adaptation(B_ko=1)
DMVADLL_W	MDVERAD	LOK	Delta resistant torque from resistant torque adaptation(B_ll=1)
DMVAD_W	MDVERAD	AUS	Delta resistant torque from resistant torque adaptation
DMVAMNFK_W	MDVERAD	DOK	Lower limit of resistant torque adaptation (B_fs=1 & B_ko=1)
DMVAMNFS_W	MDVERAD	DOK	Lower limit of resistant torque adaptation (B_fs=1)
DMVAMNKO_W	MDVERAD	DOK	Lower limit of resistant torque adaptation (B_ko=1)
DMVAMNLL_W	MDVERAD	DOK	Lower limit of resistant torque adaptation (B_ll=1)
DMVAMXFK_W	MDVERAD	DOK	Upper limit of resistant torque adaptation (B_fs=1 & B_ko=1)
DMVAMXFS_W	MDVERAD	DOK	Upper limit of resistant torque adaptation (B_fs=1)





Variable	Source	Type	Description
DMVAMXKO_W	MDVERAD	DOK	Upper limit of resistant torque adaptation (B <sub>ko</sub> =1)
DMVAMXLL_W	MDVERAD	DOK	Upper limit of resistant torque adaptation (B <sub>ll</sub> =1)
TMOT	SWADAP	EIN	Engine temperature

### FW MDVERAD 1.50 Fixed Values

Parameter	Value	Description
CDWVERAD		Codewort
DMADFK		maximum adaptable change of resistant torque during one idle cycle AT+drive + AC
DMADFS		maximum adaptable change of resistant torque during one idle cycle AT in drive
DMADKO		maximum adaptable change of resistant torque during one idle cycle compressor on
DMADLL		maximum adaptable change of resistant torque during one idle cycle loadless
DMADMNFK		lower limit for torque adaptation At in drive + AC compressor on
DMADMNFS		lower limit for torque adaptation At in drive
DMADMNKO		lower limit for torque adaptation AC compressor on
DMADMNLL		lower limit for torque adaptation loadless
DMADMXFK		upper limit for torque adaptation AT in drive + AC compressor on
DMADMXFS		upper limit for torque adaptation AT in drive
DMADMXKO		upper limit for torque adaptation AC compressor on
DMADMXLL		upper limit for torque adaptation loadless
TMDMAD		Engine temperature threshold to enable adaptation of resistant torque
TWDMAD		Waiting time to enable adaptation of resistant torque
ZKDMADFK		time constant for torque adaptation AT in drive and AC compressor on
ZKDMADFS		time constant for torque adaptation AT in drive
ZKDMADKO		time constant for torque adaptation AC compressor on
ZKDMADLL		time constant for torque adaptation loadless

### FB MDVERAD 1.50 Detailed description of function

The demand adaptation learns the different friction loss of the system engine+auxiliary aggregates. Included as auxiliary aggregates for the adaptation are only the compressor for the air-conditioning system and the converter for the automatic transmission. Since the engine is sometimes run without the air-conditioning compressor turned on, or with driving positions of the automatic transmission not engaged, the adaptation must take the different load states into account.

The adaptation MADLL is performed when idling without the air-conditioning compressor and without an engaged driving position (only for AT). In dmvadll\_w, the change in the load torque of the engine alone is learned (basic change in the engine torque corresponds to a change in the internal friction of the engine by, e.g. wear or differences in viscosity).

The basic load change is retained when the air-conditioning compressor is switched on, new changes in the load are primarily attributable to the air-conditioning compressor. A further factor dmvadko\_w is thus adapted to the basic load change dmvadll\_w by addition.

This adaptation is as a rule more rapid than the basic load adaptation because the compressor load changes much quicker for regulated compressors (depending on the quality of the check-back signal from the compressor for the load) than the basic load of the engine (given by the mechanical friction and the viscosity).

A similar process takes place when the driving position (automatic transmission) is engaged, as for switching on the compressor.

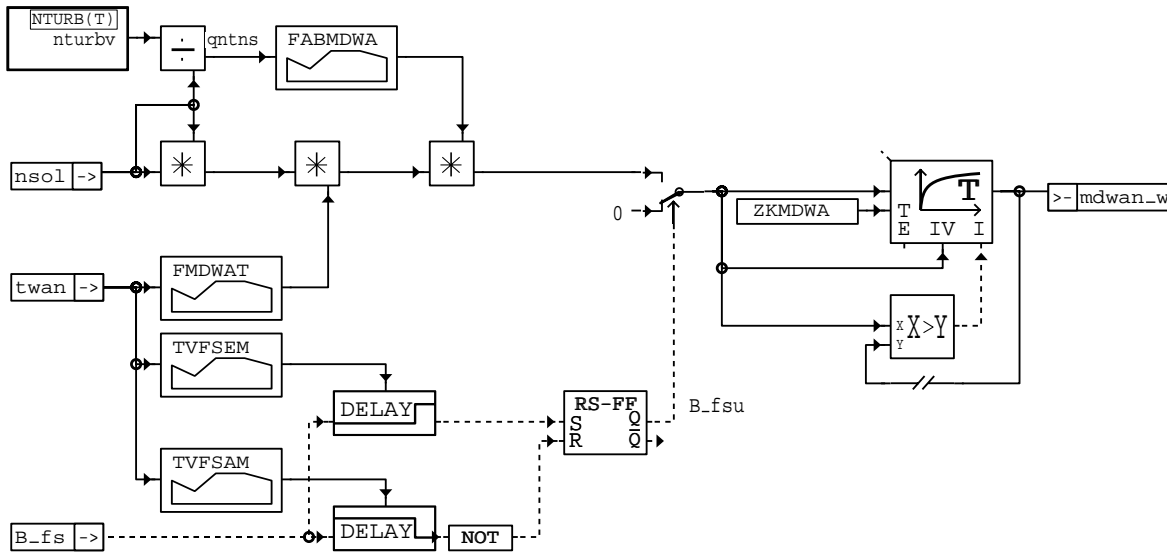
In the event that the compressor and driving position take place as loads at the same time, then the adaptation only sees the sum of changes in load from the compressor and driving position. Hence in this case, the factors already learned for the den air-conditioning compressor and the driving position alone are included in the calculation. A new factor dmvadfk\_w is adapted however.

As soon as one of the loads (air-conditioning compressor or driving position) is turned off again, the inclusion of dmvadk\_w in the calculation and the corresponding factor dmvadko\_w or dmvadfs\_w are learned again and included in the computation.

## APP MDVERAD 1.50 Application hint

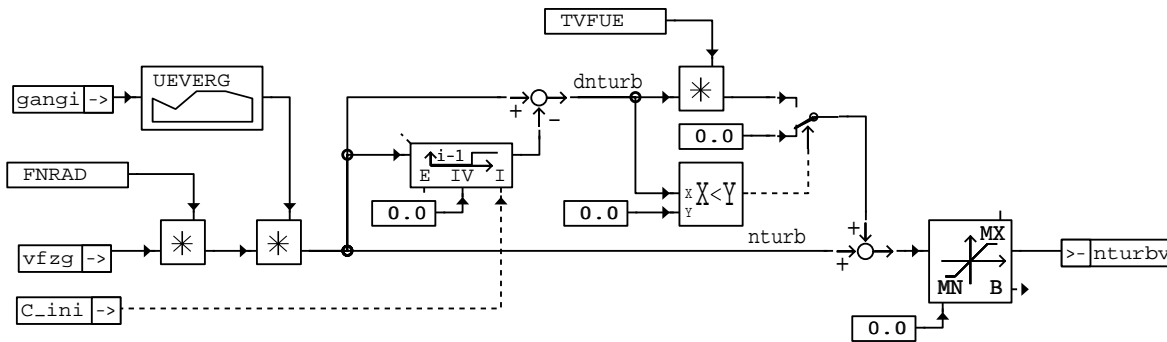
## MDWAN 1.30 Torque of the AT-converter

### FDEF MDWAN 1.30 Function definition



mdwan-mdwan

mdwan-mdwan



mdwan-nturb

mdwan-nturb

### ABK MDWAN 1.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FABMDWA	QNTNS		KL	Factor to decrease the converter torque depending of nturb
FMDWAT	TWAN		KL	Factor to calculate the converter torque depending of oil temperature
FNRAD			FW	Factor between wheel speed and vehicle speed f(circumference)
TVFSAM	TWAN		KL	Delay time after DRIVE-position switch off
TVFSEM	TWAN		KL	Delay time after DRIVE-position switch on
TVFUE			FW	Delay for the cylinder filling
UEVERG	GANGI		KL	Gear ratio depending of the gear
ZKMDWA			FW	Time constant for converter torque change
Variable	Source		Type	Description
B_FS	BBGANG		EIN	Condition driving state (automatic gear box)
B_FSU	MDWAN		DOK	Condition: Gear selection, switchover
B_JNI			EIN	Condition initialization
C_JNI	SWADAP		EIN	ECU-condition for intialisation
DNTURB	MDWAN		LOK	Speed difference of the converter turbine
GANGI	SWADAP		EIN	Engaged gear
MDWAN_W	MDWAN		AUS	Torque request of the torque converter
NSOL	LLRNS		EIN	idle reference speed
NTURB	MDWAN		LOK	Converter turbine speed
NTURBV	MDWAN		LOK	Expected converter turbine speed
QNTNS	MDWAN		LOK	Quotient of turbine speed by target speed at idle
S_FS	SWADAP		EIN	Drive position selected



Variable	Source	Type	Description
TWAN	SWADAP	EIN	Converter oil temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)

### FW MDWAN 1.30 Fixed Values

Parameter	Value	Description
FNRAD		Factor between wheel speed and vehicle speed f(circumference)
TVFUE		Delay for the cylinder filling
ZKMDWA		Time constant for converter torque change

### FB MDWAN 1.30 Detailed description of function

If the vehicle is at rest with At in 'drive', the engine must produce a definite torque to compensate the resistance of the torque converter of the AT. This resistant torque can be calculated as follow:

$$md = FMDWAT(twan) * FABMDWA(qntns) * nsol^2$$

with twan = oil temperature of the converter  
qntns = nturbv / nsol, quotient of the expected converter turbine speed and the engine target speed at idle.

The expected converter turbine speed is calculated as follow:

$$nturbv = \begin{cases} nturb, & \text{if the turbine speed is constant or increasing} \\ nturb + \Delta nturb * TVFUE, & \text{if the turbine speed is decreasing} \end{cases}$$

The converter turbine speed nturb ist calculated as follow:

$$nturb = UEVERG * nrad \quad \text{with} \quad nrad = FNRAD * vfzg.$$

where UEVERG = f(gangi) is the gear-ratio in the actual gear and FNRAD is a function of the wheel circumference.

If the driver drives away slowly, the turbine is rotated by the wheels. If the turbine speed approaches the engine speed, the resistant torque of the converter becomes smaller.

If the wheels are decelerated, the turbine speed decreases and the resistant torque of the converter increases (mdwan\_w must increase too). To achieve a quick filling of the intake manifold in order to compensate the change of converter torque, the torque is predicted by using the turbine speed change (see above).

An increase of the converter torque must be taken into account without filtering (the torque must be present as soon as possible), the reduction of the converter torque can be filtered (comfort).

### APP MDWAN 1.30 Application hint

FABMDWA: The factor is 1 if qntns is 0. The factor varies from 0 to 1 if the turbine speed approaches the target speed nsol. 0 < qntns < 1, the factor is 0 if qntns is 1.

FMDWAT: With decreasing oil temperature the factor becomes greather because the internal friction of the converter increases.

TVFUE: Delay time for the filling of the cyclinders at idle and low load.

$$UEVERG: \quad \text{example: gear ratio in 5th gear} = \frac{nTurbine}{nCardan\_Shaft} = 3.7 \quad \text{und rear axle ratio} = \frac{nCardan\_Shaft}{nWheel} = 0.8$$

The total ration in 5. gear is the given by UEVERG(5) = 3.7 \* 0.8 = 2.96.

FNRAD: example: for a circumference of 2m fnrad is given by: nrad = 1 r/min = 2 m/min = 120 m/h = 0.12 km/h = vfzg

$$FNRAD = \frac{nWheel \cdot 1 \text{ rpm}}{vfzg \cdot 0.12 \text{ km/h}} = \frac{1 \text{ rpm}}{0.12 \text{ km/h}} = 8.33 \text{ km/h}$$

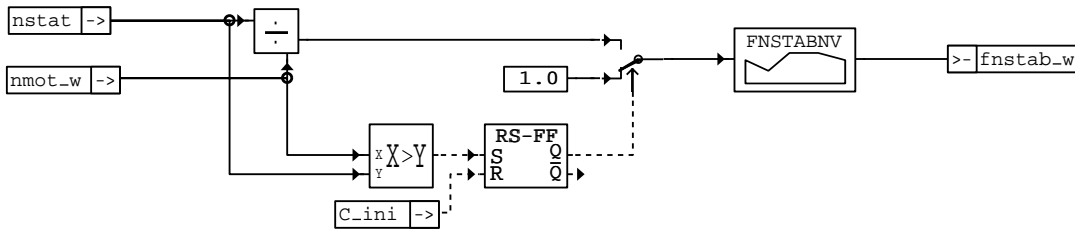
TVFSAM:

TVFSEM:

ZKMDWA:

## MDNSTAB 1.10 Torque: engine-speed stabilization

### FDEF MDNSTAB 1.10 Function definition



mdnstab-mdnstab

### ABK MDNSTAB 1.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FNSTABNV	NVER		KL	Factor for engine speed stabilisation by torque
Variable	Source		Type	Description
C_INI	SWADAP		EIN	ECU-condition for intialisation
FNSTAB_W	MDNSTAB		AUS	Factor for speed stabilization
NMOT_W	SWADAP		EIN	engine speed
NSTAT	LLRNS		EIN	Stationary reference speed

### FW MDNSTAB 1.10 Fixed Values

Parameter	Value	Description

### FB MDNSTAB 1.10 Detailed description of function

In order to achieve a self-stabilization of the speed, the indicated torque is weighted with the factor `fnstab_w`. The factor `fnstab_w` is obtained from the characteristic `FNSTABNV`. After the initialization the factor remains at 1 until the actual speed `nmot` has exceeded the desired speed `nsol`.

### APP MDNSTAB 1.10 Application hint

Adjustment of `FNSTABNV`: The characteristic `FNSTABNV` makes it possible to achieve an arbitrary stabilization function for the speed. Dependent on the quotient of the desired speed and on the actual speed of the engine, it is possible to determine a weighting factor for the demanded torque. The values for speed quotients greater than 1 must also be greater than 1, for quotients less than 1 they must also be less than 1. All characteristics belong to a group and they all intersect the point `quotient=1` and `fnstab_w=1`. When the desired speed is reached, no correction is to be performed. If the performance output of the engine is to be kept constant (opening cross-section of the throttle valve remains constant at over-critical pressure ratios), then data is to be entered into `FNSTABNV` as the first bisector. For example:

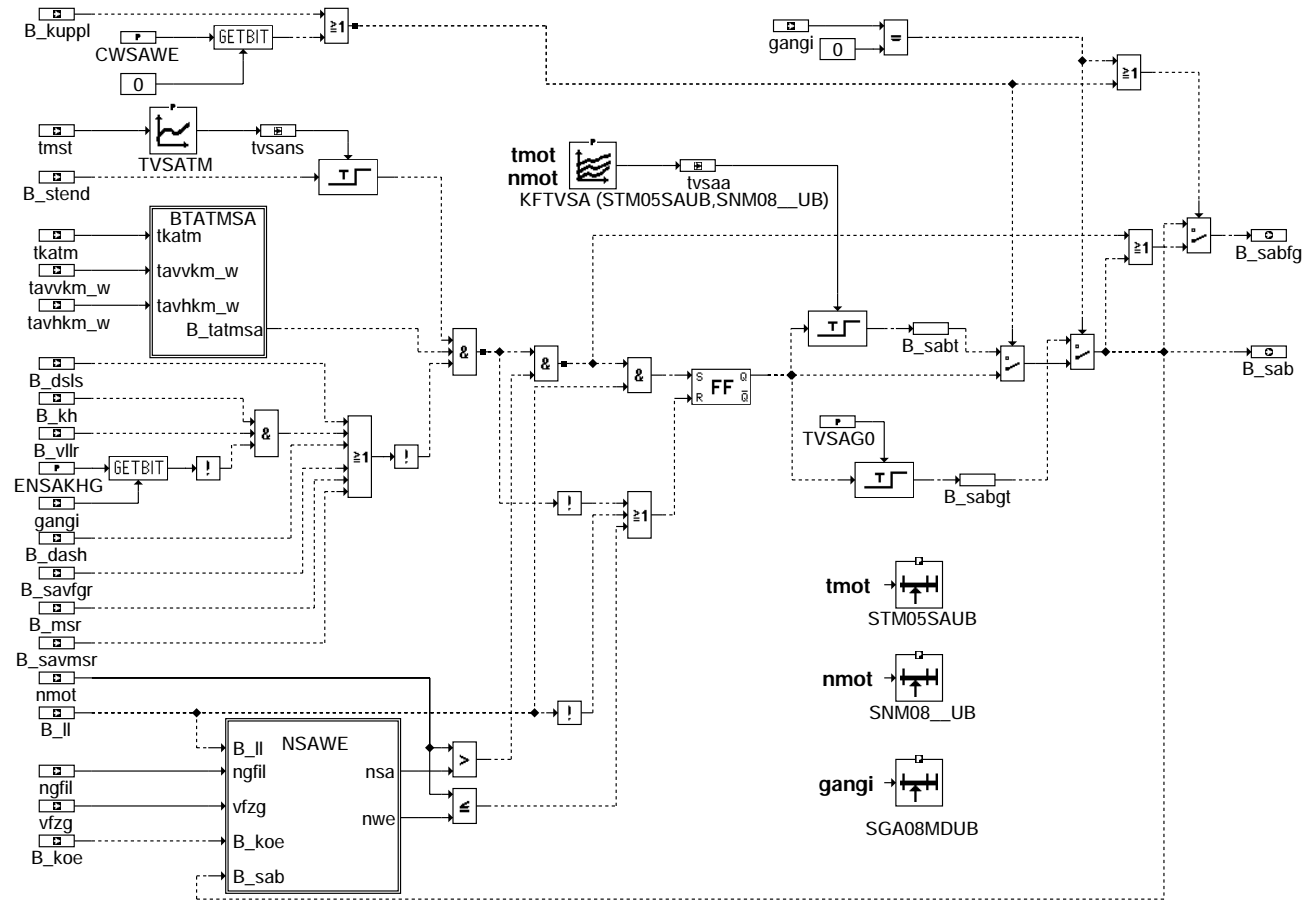
Quotient = 0	1.0	2.0	3.0	4.0	5.0
FNSTABNV = 0	1.0	2.0	3.0	4.0	5.0

By influencing the factors above and below 1, it is possible to improve the speed distribution around the desired speed. For this, however, an exact analysis of the speed distribution should be performed. The above-mentioned characteristic should be used when starting the application.

## BBSAWE 18.110 Conditions for fuel cut-off / cut-in

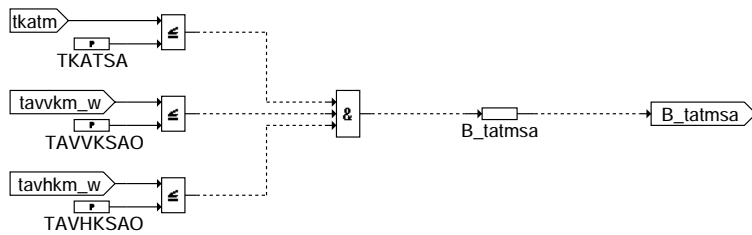
### FDEF BBSAWE 18.110 Function definition

BBSAWE: overview



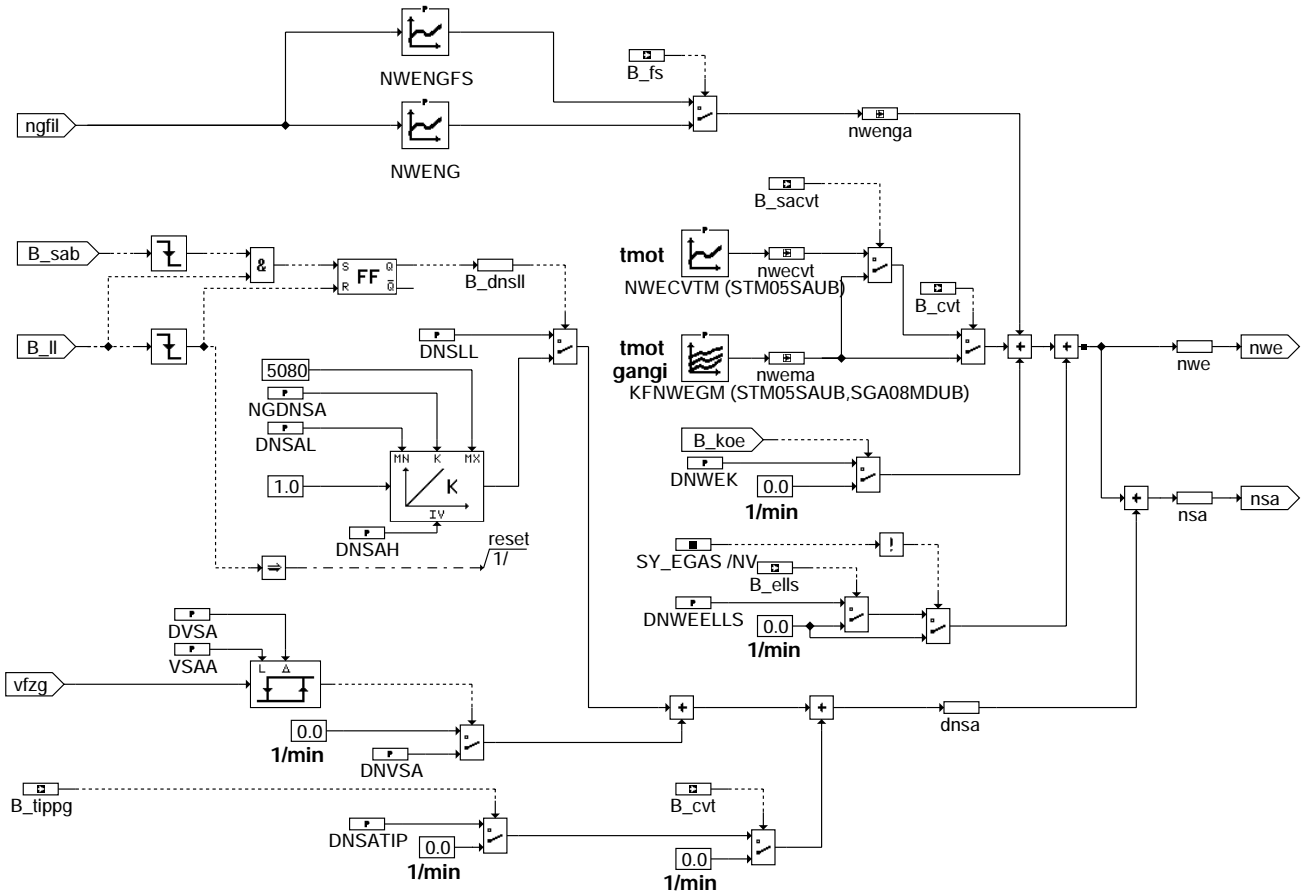
#### bbsawe-main

BTATMSA: Release for fuel cut-off by exhaust gas temperature model



#### bbsawe-btatmsa

NSAWE: Calculation of the engine speed thresholds



bbsawe-nsawe

### ABK BBSAWE 18.110 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWSAWE			FW	code word to enable fuel cut off - fuel restart
DNSAH			FW	Delta n overrun cut-off high with reference to n reinstatement
DNSAL			FW	Delta n overrun cut-off low with reference to n reinstatement
DNSATIP			FW	cut off engine speed increase at tip gutter
DNSLL			FW	Overrun cut-off hysteresis for reinstatement at idle
DNVSA			FW	cut off engine speed increase at low vehicle speed
DNWEELLS			FW	delta cut-in speed at error of throttle by-pass valve
DNWEK			FW	Delta n for reinstatement with air conditioning
DVSA			FW	delta vehicle speed for cut off engine speed increase
ENSAKHG			FW	enabling fuel cut off dependent on gear during catalyst heating
KFNWEGM	TMOT	GANGI	KF	Fuel cut in map depending on rpm
KFTVSA	TMOT	NMOT	KF	Retard time for overrun fuel cut-off
NGDNSA			FW	Engine speed gradient during decreasing the cut-off hysteresis
NWECVTM	TMOT		KL	Fuel restart-speed at CVT
NWENG	NGFIL		KL	Fuel cut-in engine speed
NWENGFS	NGFIL		KL	Delta Fuel cut-in engine speed with Drive
SY_EGAS			SYS (REF)	System constant E-GAS present
TAVHKSAB			FW	upper limit exhaust gas temperature before main catalyst
TAVVKSAB			FW	upper limit exhaust gas temperature before pre catalyst
TKATSA			FW	Catalyst temperature threshold for fuel cut-off
TVSAGO			FW	delay fuel cut off at gear 0
TVSATM	TMST		KL	delay time after cranking for fuel cut off
VSAA			FW	vehicle speed threshold for cut off engine speed increase
Variable	Source		Type	Description
B_CVT	PROKON		EIN	Condition continuously variable transmission
B_DASH	MDFAW		EIN	condition: limitation of negative torque gradient active
B_DNSLL	BBSAWE		LOK	condition fuel cut off engine speed hysteresis DNSLL
B_DSLS			EIN	condition for active diagnosis of secondary air system
B_ELLS			EIN	Condition: error idle speed actuator
B_FS	BBGANG		EIN	Condition driving state (automatic gear box)
B_KH	BBKHZ		EIN	condition catalyst heating activated
B_KOE	KOS		EIN	Condition for AC-compressor ON



Variable	Source	Type	Description
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_LL	MSF	EIN	Condition idle
B_MSR	MDKOG	EIN	Condition MSR
B_SAB	BBSAWE	AUS	Condition fuel cut-off requested
B_SABFG	BBSAWE	AUS	condition fuel cut-off enable or release
B_SABGT	BBSAWE	LOK	Condition fuel cut-off requested at gear 0
B_SABT	BBSAWE	LOK	Condition fuel cut-off requested
B_SACVT		EIN	condition support of the fuel cut of for CVT-gearbox
B_SAVFGR	FGRUE	EIN	Condition: prohibited trailing throttle fuel cut-off by cruise control
B_SAVMSR		EIN	Condition: Fuel cut off forbidden when MSR request
B_STEND	BBSTT	EIN	condition end of start
B_TATMSA	BBSAWE	LOK	condition: temperatures from ATM permit fuel cut-off
B_TIPPG		EIN	Condition Gear lifter in position "Tippgasse"
B_VLLR	LLRBB	EIN	Condition vehicle is moving with engaged gear
DNSA	BBSAWE	LOK	time depending overrun hysteresis
GANGI	SWADAP	EIN	Engaged gear
NGFIL	SWADAP	EIN	filtered engine-speed gradient
NMOT	SWADAP	EIN	engine speed
NSA	BBSAWE	LOK	Engine speed for fuel cut-off
NWE	BBSAWE	LOK	engine speed for fuel cut-in
NWECVT	BBSAWE	LOK	engine speed fuel restart at CVT
NWEMA	BBSAWE	LOK	engine speed fuel restart
NWENGA	BBSAWE	LOK	engine speed fuel restart
TAVHKM_W		EIN	Exhaust gas temperature in front of main catalyst out of model
TAVVKM_W		EIN	Exhaust gas temperature in front of pre-catalyst out of model
TKATM	ATM	EIN	catalyst temperature (model)
TMST	GGTFM	EIN	engine temperature at start
TVSAA	BBSAWE	LOK	delay fuel cut-off
TVSANS	BBSAWE	LOK	delay fuel cut-off duriing post cranking
VFZG	SWADAP	EIN	vehicle speed (km/h)

### FW BBSAWE 18.110 Fixed Values

Parameter	Value	Description
CWSAWE		code word to enable fuel cut off - fuel restart
DNSAH		Delta n overrun cut-off high with reference to n reinstatement
DNSAL		Delta n overrun cut-off low with reference to n reinstatement
DNSATIP		cut off engine speed increase at tip gutter
DNSLL		Overrun cut-off hysteresis for reinstatement at idle
DNVSA		cut off engine speed increase at low vehicle speed
DNWEELLS		delta cut-in speed at error of throttle by-pass valve
DNWEK		Delta n for reinstatement with air conditioning
DVSA		delta vehicle speed for cut off engine speed increase
ENSAKHG		enabling fuel cut off dependent on gear during catalyst heating
NGDNSA		Engine speed gradient during decreasing the cut-off hysteresis
TAVHKSAO		upper limit exhaust gas temperature before main catalyst
TAVVKSAAO		upper limit exhaust gas temperature before pre catalyst
TKATSA		Catalyst temperature threshold for fuel cut-off
TVSAGO		delay fuel cut off at gear 0
VSAA		vehicle speed threshold for cut off engine speed increase



## FB BBSAW 18.110 Detailed description of function

### Function:

This function recognizes the speed range where fuel cut-off is admissible. This is signaled by the condition "Ready for fuel cut-off",  $B_{sab} = 1$ . Otherwise,  $B_{sab} = 0$ .

#### 1. Generation of the condition "Ready for fuel cut-off"

The condition "Ready for fuel cut-off" ( $B_{sab} = 1$ ) requires the following states and conditions:

engine speed  $n_{mot}$  is above the fuel cut-off speed threshold  $n_{sa} = n_{we} + d_{nsa}$  &  
after start-up, a time  $TVSATM$  has finished which depends on the engine temperature &  
the modeled converter temperatures are below the related upper limits ( $B_{tatmsa} = true$ ) &  
the condition idle operation  $B_{ll}$  is set &  
the condition Dashpot  $B_{dash}$  is not set &  
no fuel cut-off lock by FGR  $B_{savfgr}$ , no SLS diagnosis and no converter heating &  
the condition  $B_{msr}$  is not set.

When the above conditions are met and the clutch switch makes contact, the condition  $B_{sab}$  is only set after an activation delay  $KFTVSA$  which depends on temperature and engine speed. This prevents fuel cut-off during gear changes. If the clutch switch brakes contact and the above conditions are met, the condition  $B_{sab}$  is set immediately. The code word  $CWSAW[Bit0] = 1$  activates the delay  $KFTVSA$  independently of the clutch switch. This allows to avoid the fuel cut-off during gear changes on projects without clutch switch. In gear 0, the fuel cut-off can be delayed by an applicable time,  $TVSAG0$ . If the above conditions are no longer met, or if the engine speed goes below the resume speed  $n_{we}$ ,  $B_{sab}$  is reset without delay.

The condition  $B_{sabfg}$  is required as an intermediate value in function  $\%MDFAW$ .

#### 2. Calculation of the speed thresholds

The resume engine speed  $n_{we}$  and the fuel cut-off hysteresis  $d_{nsa}$  are thresholds for fuel cut-off and resume:

-  $n_{we}$ : required if speed goes below resume value.  
-  $n_{sa} = n_{we} + d_{nsa}$ : fuel cut-off is admissible if this engine speed is exceeded,  
the resume speed  $n_{we}$  depends on engine temperature  $t_{mot}$  and on engine speed gradient  $ngfil$  ( $NWENG$ ). The engine speed scarcely drops on cars with automatic transmission if "Drive" is selected. The resume speed needs to be increased only a little in these cases ( $NWENGFS$ ). The resume speed is furthermore additionally increased if the compressor of the air conditioner is connected ( $B_{koe}$ ).

On systems of the non-E-Gas type, the resume speed can be increased in the event of an error in the LL positioner  $B_{ells}$  ( $DNWEELLS$ ). This prevents the engine from going out at closed positioner if the filling is too scarce during resume.

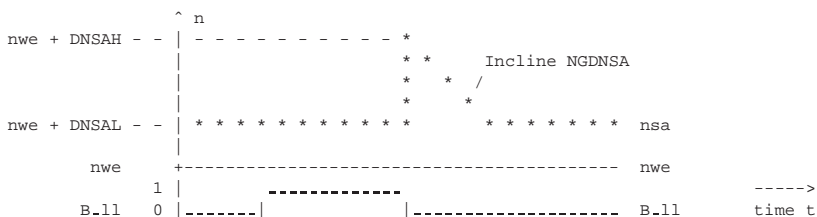
On projects with CVT transmission ( $B_{cvt} = true$ ), either  $KFNWEGM$  or  $NWECVIM$  is selected according to the condition  $B_{sacvt}$ .

When the idle operation range is exceeded, the hysteresis is steadily reduced from  $DNSAH$  to  $DNSAL$  according to a ramp function.  $NGDNSA$  states the (negative) gradient used in this reduction.

When the engine resumes in idle operation, the fuel cut-off speed is increased by the value  $DNSLL$ . This prevents, in particular on automatic transmissions, that the engine speed overshoot during resume causes another fuel cut-off.

At low vehicle speed ( $vfzg < VSAA$ ), the hysteresis range is additionally enlarged by  $DNVSA$ .  
When the vehicle speed exceeds the threshold  $VSAA + DVSA$ , this increment is reset.

For projects with CVT transmission ( $B_{cvt} = true$ ), the fuel cut-off engine speed can be increased by the value  $DNSATIP$  if the vehicle is within the selected target speed range ( $B_{tippg} = 1$ ).



Time diagram of the threshold  $n_{sa}(t)$  depending on  $B_{ll}$  for constant resume engine speed  $n_{we}$  and without increase at low vehicle speed.



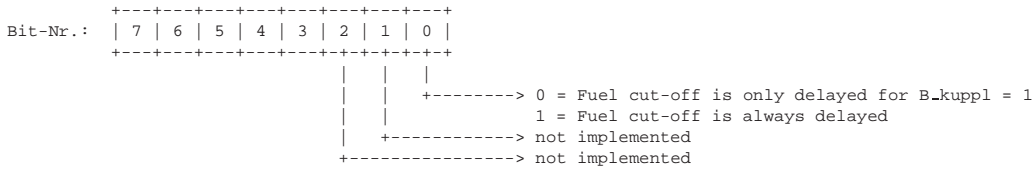


## APP BBSAWE 18.110 Application hint

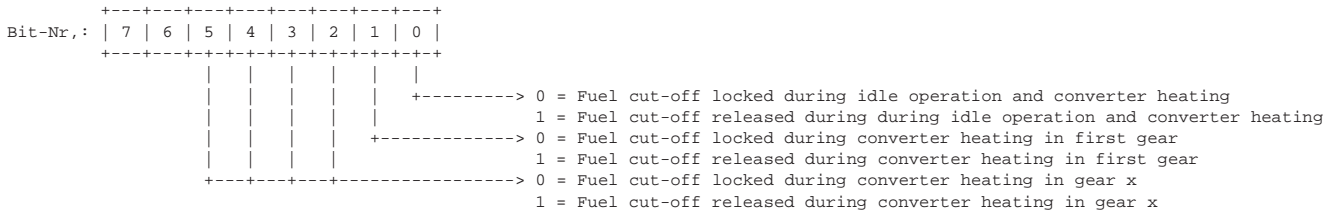
### NOTE:

KFNWEGM(tmot, gangi) offers the possibility to lock the fuel cut-off according to the gear by increasing the resume speed. A general resume lock is impermissible for gear 0 since otherwise, the vfzg diagnosis is no longer possible !!!  
In gear 0, the fuel cut-off can be delayed for an applicable time TVSAG0. This allows to implement a cut-off lock during Tip-In.

The function can be configurated using the code word CWSAWE:

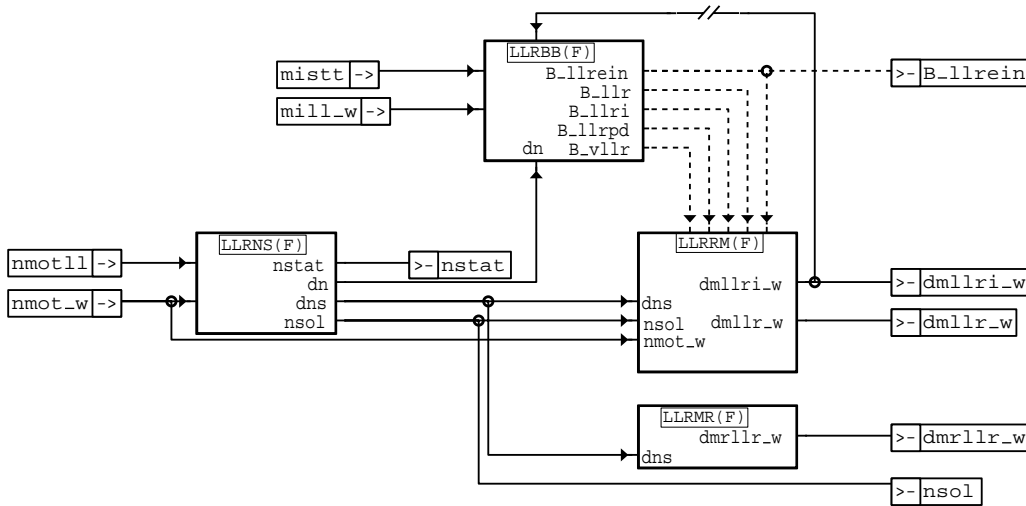


During converter heating, bitmask ENSAKHG allows to give the release for fuel cut-off only according to the selected gear:



## LLRMD 1.4 Torque-based idle-speed control

### FDEF LLRMD 1.4 Function definition



llrmd-llrmd

### ABK LLRMD 1.4 Abbreviations

Variable	Source	Type	Description
B_LL	LLRMD	LOK	condition idle speed control
B_LLREIN	LLRMD	AUS	Condition idle speed control is active
B_LLRI	LLRMD	LOK	Condition activation of I-part of idle speed control
B_LLRPD	LLRMD	LOK	Condition activation of PD-part of idle speed control
B_VLLR	LLRMD	LOK	Condition vehicle is moving with engaged gear
DMLLR_W	LLRMD	AUS	desired torque change from the idle speed control (I-)
DMLLR_W	LLRMD	AUS	desired torque change from the idle speed control (PD-part)
DMRLLR_W	LLRMD	AUS	torque reserve for idle speed control
DN	LLRMD	LOK	speed deviation at idle speed control
DNS	LLRMD	LOK	LLR: difference of idle speed precontrol
DN_W	LLRMD	LOK	speed deviation at idle speed control
MILL_W	MDMIN	EIN	Indicated engine torque at idle
MISTT		EIN	Starting torque
NMOTLL	BGNMOT	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed



Variable	Source	Type	Description
NSOL	LLRMD	AUS	idle reference speed
NSTAT	LLRMD	AUS	Stationary reference speed

### FW LLRMD 1.4 Fixed Values

Parameter	Value	Description
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### FB LLRMD 1.4 Detailed description of function

The block LLRNS calculates the target speed *nsol*, the dynamic speed difference *dn\_w* (*dn*) and the stationary speed difference *dns*.

The block LLRRM contains the idle speed controller.

The block LLRBB determines the operation conditions of the idle speed control.

The block LLRMR calculates the desired torque reserve for the idle speed control.

### APP LLRMD 1.4 Application hint

## LLRNS 534.10 Idle control; Nominal engine speed for idle speed control

### FDEF LLRNS 534.10 Function definition

No text for FDEF available!

### ABK LLRNS 534.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CNFLRNS			FW	Config.-byte for determination of target engine speed at idle
CWNSTAT			FW	Codeword for the Filtration of <i>nstat</i>
DNSNFST			FW	speed threshold of <i>nsol</i> -limitation in start
DNSNFX			FW	Offset to determine the upper limit of target speed
DTAHL			FW	Delta tans for stopping hot idling
DTMHLL			FW	Delat <i>tmot</i> for stopping hot idling
FNSNF			FW	factor for desired engine-speed correction
FNSSTKM	TMOT		KL	Factor to weight the desired speed at start during catalyst heating
FNSSTM	TMOT		KL	Faktor for target engine speed during start
KFNLLNST	TMOT	TMOT	KF	idle speed after start
KFZNSM	TMOT	DNS	KF	time constant for decay of reference speed
KLDFOFF			FW	Threshold to switch off generator load
KLDFON			FW	Threshold to switch on generator load
KNSNF			FW	Engine speed follow-up inhibition band
LBZO1			FW	Threshold of <i>lbz</i> to increase the target engine speed when leaving idle
LBZO2			FW	Threshold of <i>lbz</i> to increase the target engine during ideling
LBZU			FW	Threshold of <i>lbz</i> to decrease the target engine speed when leaving the idle
NFHZ			FW	Idle speed increase during wind screen heating activ
NFHZFS			FW	Idle speed increase during wind screen heating activ and <i>B_fs=1</i>
NFS2M	TMOT		KL	Target idle speed 2, <i>B_fs = 1</i>
NFSKLD			FW	Desired speed at generator load active and <i>B_fs=1</i>
NFSKO			FW	desired engine speed with AC-system when <i>B_fs=1</i>
NFSKS			FW	Target engine speed for preventing boiling ( <i>B_fs=1</i> )
NFSLPWG			FW	Desired speed at malfunctioning of PWG-signal when <i>B_fs=1</i>
NFSM	TMOT		KL	desired engine speed DRIVE-position switch on
NFSMIN			FW	Minimal allowed engine speed at idle with AT in drive
NFSNLDG			FW	Target-speed increase for speed-sensor limp-home
NFSSL			FW	Desired speed when power steering switch is active and <i>B_fs=1</i>
NGNSNF			FW	Threshold of speed gradient for starting dynamic target idle speed calculation
NKLD			FW	Desired speed when generator load is active
NLL2M	TMOT		KL	Target engine speed 2
NLLCVTMXV	VFZG		KL	Limitation of the target speed (CVT transmission)
NLLM	TMOT		KL	desired engine speed
NLLMIN			FW	Minimal allowed engine speed at idle
NSAC			FW	desired engine speed with air conditioner on ( <i>S_AC = 1</i> )
NSACFS			FW	desired engine speed with air conditioner on ( <i>S_AC = 1</i> ) and AT in Drive ( <i>S_fs=1</i> )
NSHLL			FW	Minimal target speed for hot idling
NSKO			FW	desired speed for AC-system
NSKS			FW	Target speed to prevent boiling
NSL			FW	debit idle-speed at power steering active
NSLBZFS			FW	desired engine speed when battery is discharged when <i>B_fs=1</i>
NSLBZLL			FW	desired engine speed when battery is discharged when
NSLBZS			FW	Engine speed threshold to switch the target speed due to <i>lbz</i>
NSLPP	PSL		KL	Target speed depending on the pump pressure of power steering
NSLPPFS	PSL		KL	Target speed depending on the pump pressure of power steering with <i>B_fs=1</i>
NSLPWG			FW	Desired speed when PWG-signals malfunction
NSNLDG			FW	Target-speed increase for speed-sensor limp-home
NSNOT			FW	Target engine speed while <i>B_nnot=1</i>
NZHDTL	RL		KL	Speed threshold for decrementing time counter for hot idling
NZHITL	RL		KL	Speed threshold for incrementing time counter for hot idling
SNS06LLSB	DNS		SV	Datapoint distribution, set-speed deviation, 06 datapoints., idle-speed control.
STM06LLUB	TMOT		SV	Datapoint distribution, engine temperature, 6 datapoints



Parameter	Source-X	Source-Y	Type	Description
STN06LLUB	TNST		SV	distribution: time after start; for determination of idle speed after start
TAHLL			FW	tans threshold for increased target speed at hot idling
TMHLL			FW	tmot threshold for increased target speed at hot idling
TMLLX			FW	Threshold for boiling prevention
TMRZHLL			FW	tmot threshold for resetting the time counter for hot idling
VSL			FW	car speed threshold for compensation power steering
ZHLLA			FW	Time counter for stopping increased speed in hot idling
ZHLL E			FW	Time counter threshold for increased speed at hot idling
ZKNS			FW	Time constant for target engine speed when changing target
ZNSUB			FW	time constant for desired engine speed at low voltage
Variable	Source		Type	Description
B_DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP		EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_FHZ			EIN	Condition flag windshield heating
B_FS	BBGANG		EIN	Condition driving state (automatic gear box)
B_HLL	LLRNS		LOK	Condition hot idling
B_KHN			EIN	condition catalyst heating idle speed
B_KLDF	LLRNS		LOK	Increase speed active for generator load
B_KO			EIN	condition AC compressor authorised
B_LL	MSF		EIN	Condition idle
B_LLREIN	LLRMD		EIN	Condition idle speed control is active
B_LLRST	LLRRM		EIN	speed reaches nstat first time after start
B_NAC	KOS		EIN	condition for increased idle-speed at AC
B_NLDG			EIN	condition limp-home function speed sensor
B_NS2	LLRNS		LOK	Condition target speed 2 active
B_NS2A	LLRNS		LOK	Condition target speed 2 requested
B_NSKS	LLRNS		LOK	Condition for increasing target speed (prevent from boiling)
B_NSSL	LLRNS		LOK	Condition: Set speed increase for power steering
B_NSWO1	PROKON		EIN	condition engine speed > NSWO1
B_PWF			EIN	Condition for powerfail
B_SL			EIN	Condition power steering
B_SPSMIN	GGPED		EIN	message to SR: '1' = pedal-travel sensor limphome with SPSMIN
B_ST	SWADAP		EIN	condition for start
B_STEND	BBSTT		EIN	condition end of start
B_WKAUF			EIN	Condition for open lock up clutch
DNS	LLRNS		AUS	LLR: difference of idle speed precontrol
E_TA	GGTFA		EIN	error flag: TANS
E_TM	GGTFM		EIN	Error flag: engine temperature tmot
KLDFPWM			EIN	generator signale as PWM-signale filtrated
LBZ	EGAG		EIN	charge state of the battery
NFSKH	SWADAP		EIN	Idling speed driving level for catalyzer heating
NGFIL	SWADAP		EIN	filtered engine-speed gradient
NLLCVT1			EIN	Target speed from CVT gear box
NLLCVT2	LLRNS		LOK	Target speed from CVT gear box after limitation
NLLKH	BBKHZ		EIN	Idling speed for catalyzer heating
NMOT	SWADAP		EIN	engine speed
NMOTLL	BGNMOT		EIN	engine speed
NSFSMN	LLRNS		LOK	LLR: minimal target speed for AT in drive
NSLBZ	LLRNS		LOK	Target engine speed dependin on lbz
NSLFA	LLRNFA		EIN	Set speed for short trip
NSLLMN	LLRNS		LOK	LLR: minimal target speed during idling
NSNF	LLRNS		LOK	LLR: followed-up target speed
NSOL	LLRNS		AUS	idle reference speed
NSST	LLRNS		AUS	Initialisation value for desired RPM during start
NSTAT	LLRNS		AUS	Stationary reference speed
NSTAT2	LLRNS		AUS	stationary desired idle-speed after limitation
NSTAT3	LLRNS		LOK	Stationary desired idle-speed pre filter
NSTATFIL	LLRNS		AUS	Stationary reference speed filtered
PSL			EIN	Oil pressure of the power steering system
RL	SWADAP		EIN	relative air charge
S_AC			EIN	A/C stand-by position
S_KO	SWADAP		EIN	A/C compressor active
TANS	SWADAP		EIN	Intake air temperature
TMOT	SWADAP		EIN	Engine temperature
TMST	GGTFM		EIN	engine temperature at start
TNST			EIN	time after end of start
VFZG	SWADAP		EIN	vehicle speed (km/h)
VSNS	VS_VERST		EIN	Change of target engine speed with calibrating tool VSxy
VSTCNS			EIN	Code-word adaptation, set idle-speed switchover
VSTNLS			EIN	Adjusting idle target speed (tester interface)
ZHLL	LLRNS		LOK	Time counter for hot idling

### FW LLRNS 534.10 Fixed Values

Parameter	Value	Description
CNLLRNS		Config.-byte for dtermination of target engine speed at idle
CWNSTAT		Codeword for the Filtration of nstat
DNSNFST		speed threashold of nsol-limitation in start
DNSNFX		Offset to determine the upper limit of target speed
DTAHL		Delta tans for stopping hot idling

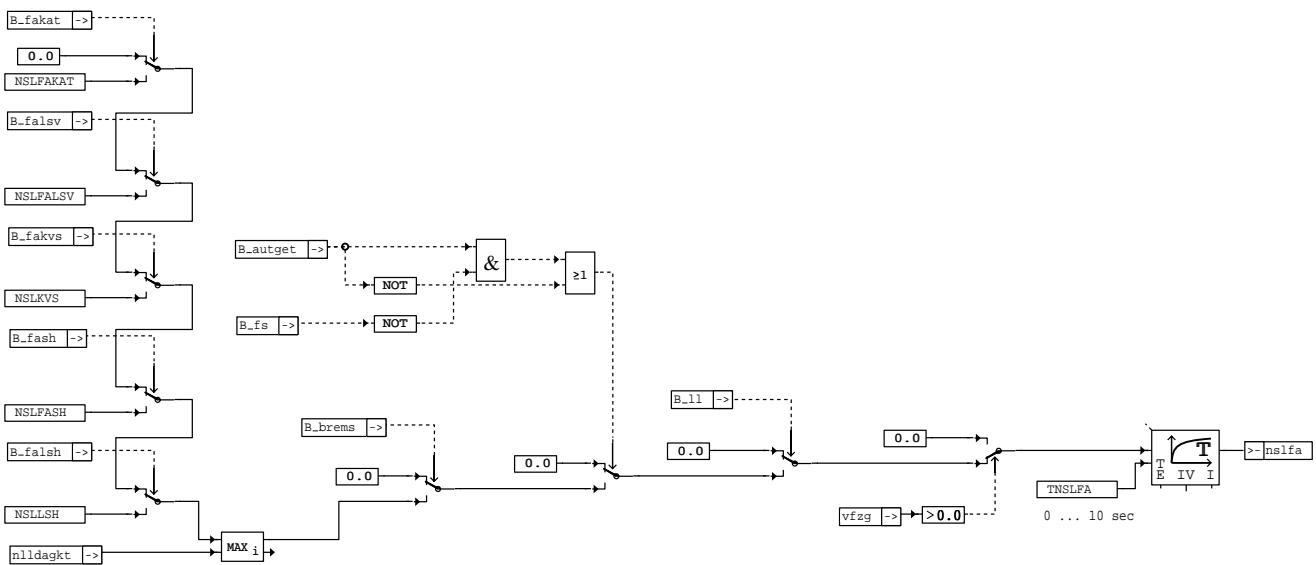
Parameter	Value	Description
DTMHLL		Delat tmot for stopping hot idling
FNSNF		factor for desired engine-speed correction
KLDFOFF		Threshold to switch off generator load
KLDFON		Threshold to switch on generator load
KNSNF		Engine speed follow-up inhibition band
LBZO1		Threshold of lbz to increase the target engine speed when leaving idle
LBZO2		Threshold of lbz to increase the target engine during ideling
LBZU		Threshold of lbz to decrease the target engine speed when leaving the idle
NFHZ		Idle speed increase during wind screen heating activ
NFHZFS		Idle speed increase during wind screen heating activ and B_fs=1
NFSKLDFF		Desired speed at generator load active and B_fs=1
NFSKO		desired engine speed with AC-system when B_fs=1
NFSKS		Target engine speed for preventing boiling (B_fs=1)
NFSLPWG		Desired speed at malfunctioning of PWG-signal when B_fs=1
NFSMIN		Minimal allowed engine speed at idle with AT in drive
NFSNLDG		Target-speed increase for speed-sensor limp-home
NFSSL		Desired speed when power steering switch is active and B_fs=1
NGNSNF		Threshold of speed gradient for starting dynamic target idle speed calculation
NKLDF		Desired speed when generator load is active
NLLMIN		Minimal allowed engine speed at idle
NSAC		desired engine speed with air conditioner on (S_AC = 1)
NSACFS		desired engine speed with air conditioner on (S_AC = 1) and AT in Drive (S_fs=1)
NSHLL		Minimal target speed for hot idling
NSKO		desired speed for AC-system
NSKS		Target speed to prevent boiling
NSL		debit idle-speed at power steering active
NSLBZFS		desired engine speed when battery is discharged when B_fs=1
NSLBZLL		desired engine speed when battery is discharged when
NSLBZS		Engine speed threshold to switch the target speed due to lbz
NSLPWG		Desired speed when PWG-signals malfunction
NSNLDG		Target-speed increase for speed-sensor limp-home
NSNOT		Target engine speed while B_nnot=1
TAHLL		tans threshold for increased target speed at hot idling
TMHLL		tmot threshold for increased target speed at hot idling
TMLLX		Threshold for boiling prevention
TMRZHLL		tmot threshold for resetting the time counter for hot idling
VSL		car speed threshold for compensation power steering
ZHLLA		Time counter for stopping increased speed in hot idling
ZHLLI		Time counter threshold for increased speed at hot idling
ZKNS		Time constant for target engine speed when changing target
ZNSUB		time constant for desired engine speed at low voltage

### FB LLRNS 534.10 Detailed description of function

### APP LLRNS 534.10 Application hint

## LLRNFA 1.50

### FDEF LLRNFA 1.50 Function definition



llrnfa-llrnfa

llrnfa-llrnfa



## ABK LLRNFA 1.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
NSLFAKAT			FW	desired speed during quick trip catalyst diagnosis
NSLFALSV			FW	desired speed during quick trip Lambda sensor upstream catalyst
NSLFASH			FW	desired speed during quick trip oscillation test
NSLKVS			FW	desired speed during quick trip diagnosis of fuel supply
NSLLSH			FW	desired speed during quick trip Lambda sensor downstream catalyst
TNSLFA			FW	filter-time constant for nsfa
Variable	Source		Type	Description
B_AUTGET	PROKON		EIN	condition automatic gearbox
B_BREMS	GGEGAS		EIN	condition: brake operated
B_FAKAT			EIN	condition function request catalyst monitoring
B_FAKVS			EIN	condition function request diagnoses fuel supply system
B_FALSH			EIN	condition function request downstream oxygen sensor diagnosis
B_FALSV			EIN	condition function request oxygen sensor diagnosis
B_FASH			EIN	condition diagnosis oxygen sensor aging downstream catalyst function request
B_FS	BBGANG		EIN	Condition driving state (automatic gear box)
B_LL	MSF		EIN	Condition idle
NLLDAGKT			EIN	Speed increase for diagnostic routine in the short test
NSLFA	LLRNFA		AUS	Set speed for short trip
VFZG	SWADAP		EIN	vehicle speed (km/h)

## FW LLRNFA 1.50 Fixed Values

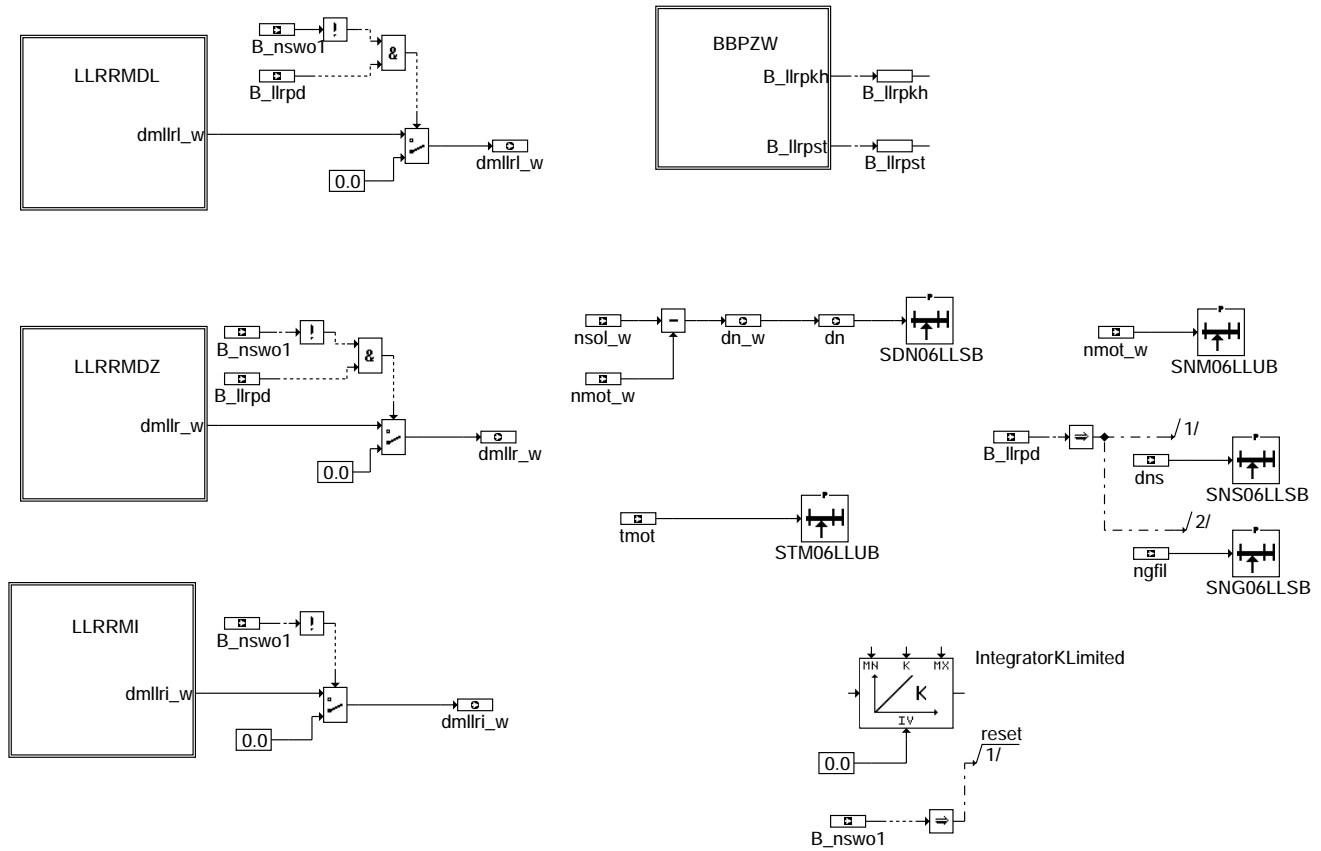
Parameter	Value	Description
NSLFAKAT		desired speed during quick trip catalyst diagnosis
NSLFALSV		desired speed during quick trip Lambda sensor upstream catalyst
NSLFASH		desired speed during quick trip oscillation test
NSLKVS		desired speed during quick trip diagnosis of fuel supply
NSLLSH		desired speed during quick trip Lambda sensor downstream catalyst
TNSLFA		filter-time constant for nsfa

## FB LLRNFA 1.50 Detailed description of function

Beim Anreizen eines Kurztrips über B\_fa kann die Soll Drehzahl auf nsfa erhöht werden. Aus Überwachungsgründen muß diese Drehzahl unter 1500 1/min liegen. Die Drehzahlanhebung ist nur bei getretener Bremse, getretener Kupplung oder Automatikgetriebe in P/N-Stellung im Stand und im LL zulässig.

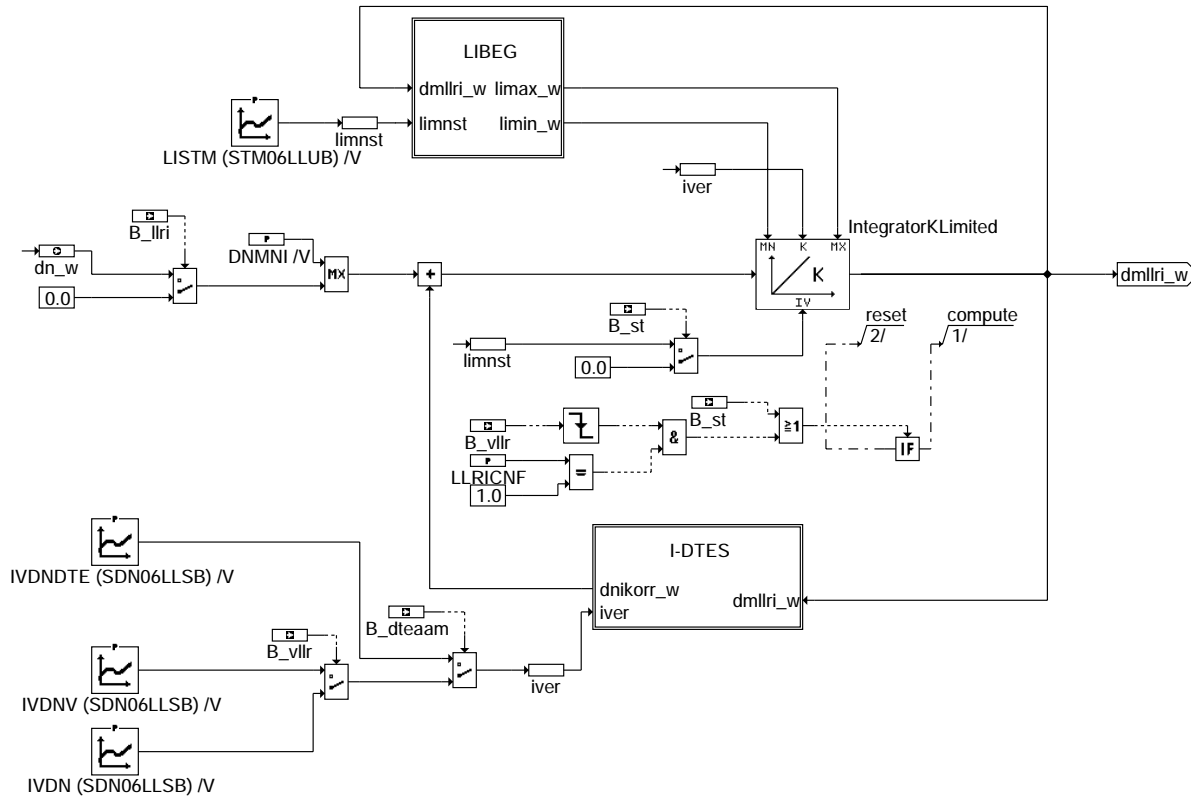
## LLRRM 6.110 Idle speed control: torque controller

### FDEF LLRRM 6.110 Function definition



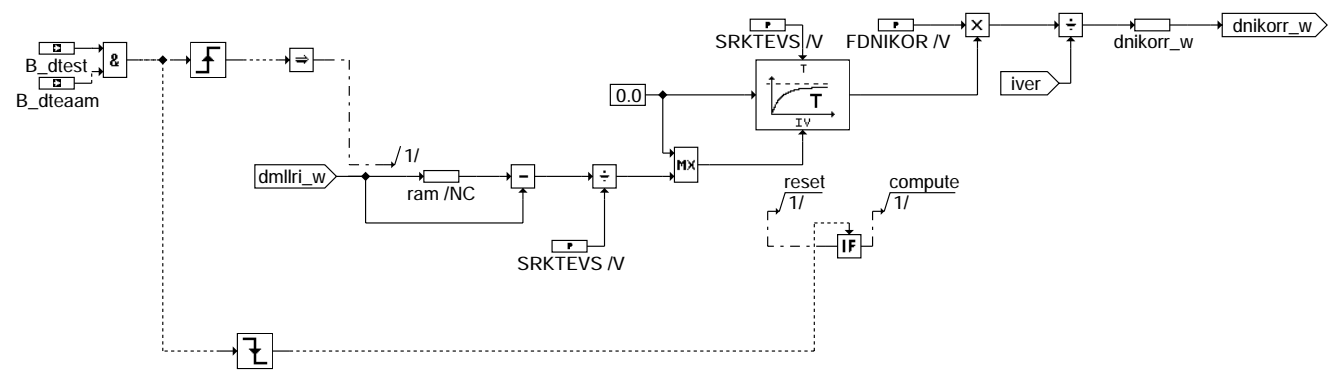
### llrm-llrm

Idle speed controller: PID-controller



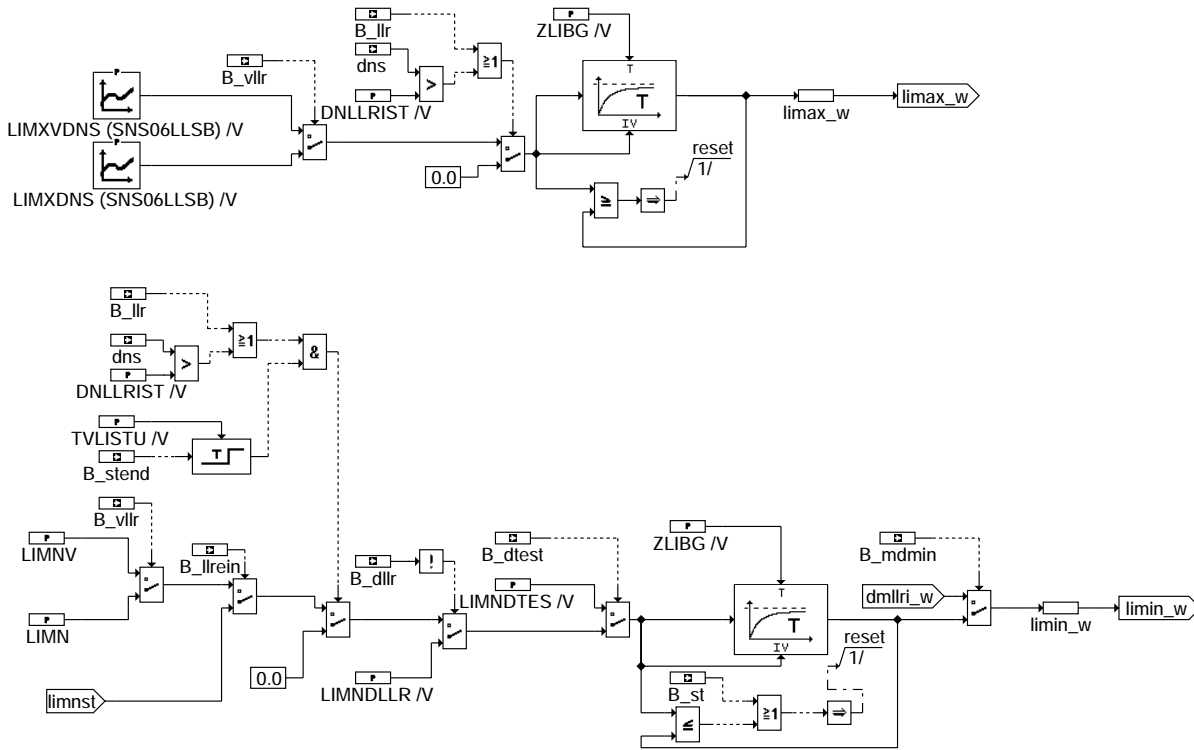
**llrm-llrmi**

Subfunction LRRMI: Idle speed controller integral part



**llrm-i-dtes**

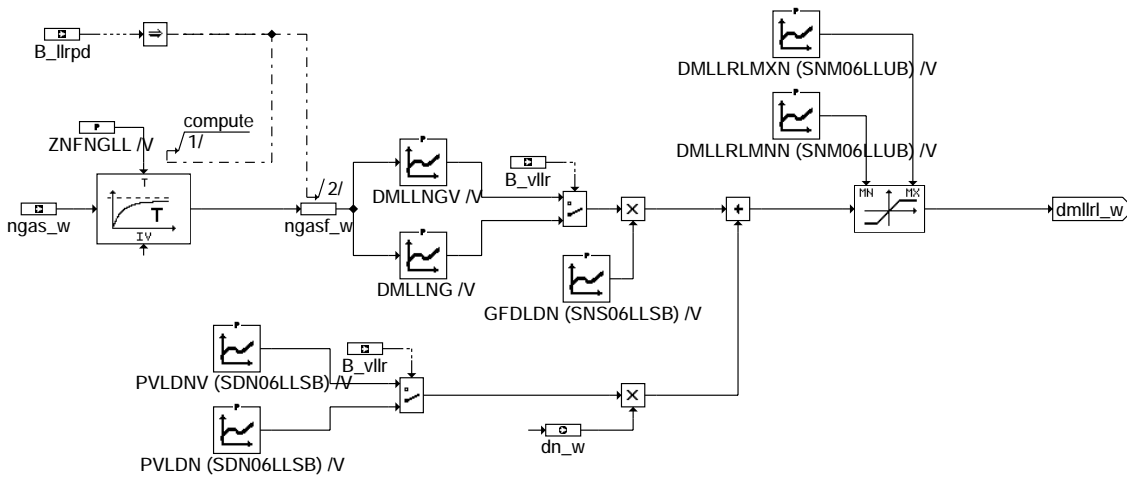
Subfunction I-DTES: Reset if the interator at the end of the diagnosis of the canister purge



### llrm-libeg

Subfunction LIBEG: Limitation of the integral part

Subfunction LLRRMD: Idle speed controller: differential part



### llrm-llrmdl

Subfunction LLRRMDL: Idle speed controller: differential part on the air

### ABK LLRRM 6.110 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWLLRPA			FW	codeword: selection of idle speed control proportional part
DMLLNG	NGASF_W		KL	LLR: D-gain depending of ngasf for air path
DMLLNGV	NGASF_W		KL	LLR: D-gain depending of ngasf for air path
DMLLRMNN	NMOT_W		KL	Lower limit for dmlrl
DMLLRMXN	NMOT_W		KL	Safety concept: upper limit for dmlrl





Parameter	Source-X	Source-Y	Type	Description
DMLLRMNN	NMOT_W		KL	Lower limit for dmlr_w
DMLLRMXN	NMOT_W		KL	Safety concept: upper limit for dmlr
DNLLRIST			FW	Overspeed threshold for integrator reset
DNLLST			FW	speed threshold to disable proportional parameter in start
DNMNI			FW	Lowest possible value for dn for the I-controller
DVNG	NGFIL		KL	LLR: D-gain depending of ngfil for vehicle at rest
DVNGV	NGFIL		KL	LLR: D-gain depending of ngfil for vehicle rolling
FDDN	DNS		KL	LLR: weightning factor for D-amplification
FDNIKOR			FW	Factor for the correction on the I-part by dn
GFDLND	DNS		KL	LLR: weightning factor for D-amplification on the air path
IVDN	DN		KL	LLR: I-gain for vehicle at rest
IVDNDTE	DN		KL	LLR: I-gain at DTEV
IVDNV	DN		KL	LLR: I-gain for vehicle rolling
LIMN			FW	lower integrator limit for standing car
LIMNDLLR			FW	lower integrator limit for diagnostic of idle speed control
LIMNDTES			FW	lower integrator limit for DTES
LIMNV			FW	lower integrator limit for rolling car
LIMXDNS	DNS		KL	upper integrator limit for standing car
LIMXVDNS	DNS		KL	upper integrator limit for rolling car
LISTM	TMOT		KL	value of idle speed control integrator during start
LLRICNF			FW	Configuration byte for ISC integrator
PVDN	DN		KL	LLR: P-gain for vehicle at rest
PVDNKH	DNS		KL	proportional ISC when secondary air activ
PVDNST	DN		KL	proportional ISC in start
PVDNV	DN		KL	LLR: P-gain for vehicle rolling
PVLDN	DN		KL	LLR: P-gain for vehicle at rest (air path)
PVLDNV	DN		KL	LLR: P-gain for vehicle at rest (air path)
SDN06LLSB	DN		SV	10 Sst.
SNG06LLSB	NGFIL		SV	Datapoint distribution, speed gradient, 6 datapoints
SNM06LLUB	NMOT_W		SV	distribution of engine speed
SNS06LLSB	DNS		SV	Datapoint distribution, set-speed deviation, 06 datapoints., idle-speed control.
SRKTEVS			FW	Manifold time constant when closing the canister purge valve
STM06LLUB	TMOT		SV	Datapoint distribution, engine temperature, 6 datapoints
TVLISTU			FW	Time during witch a negative integrator value is forbidden
TVLLRPST			FW	delay to disable proportional parameter in start
TVPKH			FW	delay: proportional parameter for kathalyst-heating
ZKLLRD			FW	Time constant for the decrease of the differential part of the controller
ZLIBG			FW	filter time constant for adjusting integrator limits
ZNFNGLL			FW	filter time constant for speed gradient on air path (LLR)

Variable	Source	Type	Description
B_DLLR	SWADAP	EIN	Active diagnostic: ISC-actuator diagnostic
B_DTEAAM	DTEV	EIN	Condition diagnosis CPV by opening the CPV active possible
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_KHA	BBKHZ	EIN	request of activated catalyst heating
B_LLR	LLRBB	EIN	condition idle speed control
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_LLR1	LLRBB	EIN	Condition activation of I-part of idle speed control
B_LLRPD	LLRBB	EIN	Condition activation of PD-part of idle speed control
B_LLRPKH	LLRRM	LOK	proportional paramter for cathalyst-heating activ
B_LLRPST	LLRRM	LOK	proportional parameter in start activ
B_LLRST	LLRRM	AUS	speed reaches nstat first time after start
B_JMDMIN	SWADAP	EIN	Condition minimal possible indicated torque reached
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_TRKH	BBKHZ	EIN	Flag for catalyst fast heating
B_VLLR	LLRBB	EIN	Condition vehicle is moving with engaged gear
DMLLRD_W	LLRRM	AUS	desired torque change from the idle speed control (D-part)
DMLLRL_W	LLRRM	AUS	desired torque change from the idle speed control (I-)
DMLLRL_W	LLRRM	AUS	desired torque change from the idle speed control (part on the air path)
DMLLRP_W	LLRRM	AUS	desired torque change from the idle speed control (P-part)
DMLLR_W	LLRRM	AUS	desired torque change from the idle speed control (PD-part)
DN	LLRRM	AUS	speed deviation at idle speed control
DNIKORR_W	LLRRM	LOK	Correcting value on the integrator after diagnostic
DNS	LLRNS	EIN	LLR: difference of idle speed precontrol
DN_W	LLRRM	AUS	speed deviation at idle speed control
IVER	LLRRM	LOK	Integrator amplification
LIMAX_W	LLRRM	LOK	Idle speed control integrator upper limit
LIMIN_W	LLRRM	LOK	Idle speed control integrator lower limit
LIMNST	LLRRM	LOK	Idle speed control integrator lower limit during after start
NGASF_W	LLRRM	LOK	engine speed gradient during one working cycle (filtered value)
NGAS_W	BGNG	EIN	engine speed gradient during one working cycle
NGFIL	SWADAP	EIN	filtered engine-speed gradient
NMOT_W	SWADAP	EIN	engine speed
NSOL_W		EIN	idle reference speed ,word
NSTAT	LLRNS	EIN	Stationary reference speed
TMOT	SWADAP	EIN	Engine temperature



## FW LLRRM 6.110 Fixed Values

Parameter	Value	Description
CWLLRPA		codeword: selection of idle speed control proportional part
DNLLRIST		Overspeed threshold for integrator reset
DNLLST		speed threshold to disable proportional parameter in start
DNMNI		Lowest possible value for dn for the I-controller
FDNIKOR		Factor for the correction on the I-part by dn
LIMN		lower integrator limit for standing car
LIMNDLLR		lower integrator limit for diagnostic of idle speed control
LIMNDTES		lower integrator limit for DTES
LIMNV		lower integrator limit for rolling car
LLRICNF		Configuration byte for ISC integrator
SRKTEVS		Manifold time constant when closing the canister purge valve
TVLISTU		Time during witch a negative integrator value is forbidden
TVLLRPST		delay to disable proportional parameter in start
TVPKH		delay: proportional parameter for kathalyst-heating
ZKLLRD		Time constant for the decrease of the differential part of the controller
ZLIBG		filter time constant for adjusting integrator limits
ZNFNGLL		filter time constant for speed gradient on air path (LLR)

## FB LLRRM 6.110 Detailed description of function

### Idle speed controller

The idle speed controller is a controller of PID-type (proportional, integral and differantial controller). The three parts P, I and D are strictly separated from each other.

**D-Part:** The differential part of the controller is triggered by the input value. The input value is given by the product of the engine speed gradient  $ngfil$ , the differential gain  $DVNG$  (resp.  $DVNGV$  for  $B_{vllr}=1$ ) an a weightning factor  $FDDN$  depending on the difference of the actual engine speed to the stationary target speed. This input value is the start value of a low-pass filter. The output of the low-pass filter is the differential part  $dmlld_w$  and the time constant is givent by the fix-value  $ZKLLRD$ . If a new input value, abolutely grather than the actual filter output value is calculated, the filter is initialised to the new input value.

**D-part on the air path:** to achieve a quicker filling of the empty manifoild, a special D-part in the air-path is generated. The manifoild ist still filled with air when the normal speed controller needs the higher torque. A too large amount of air can not cause a too high output-torque because the torque coordinator will compensate it by retarding the spark advance.

**P-part:** The proportional part of the controller delivers a torque correction  $dmlrp_w$  proportional to the speed difference  $dn_w$ . The gain is taken from the characteristic line  $FVDN$  for  $B_{vllr}=0$  and from  $FVDNV$  for  $B_{vllr}=1$ . Both lines depend of the speed difference  $dn$ .

The controller output is the sum of the P-part  $dmlrp_w$  and the D-part  $dmlld_w$  if  $B_{llrpd}$  is true. If  $B_{llrpd}$  is false, the controller output  $dmlr_w$  is zero (for  $B_{llrpd}$  see  $\%LLRBB$ ).

**I-part:** The input of the integral part is the speed difference  $dn_w$ . The integrator ist enabled if  $B_{llri}$  is true. If  $B_{llri}$  is false, the integrator is stopped (for  $B_{llri}$  see  $\%LLRBB$ ).

The gain of the I-part is taken from the characteristic lines  $IVDN$  for  $B_{vllr}=0$  and from  $IVDNV$  for  $B_{vllr}=1$ . Both lines depend of the speed difference  $dn$ .

During start ( $B_{st}=1$ ) the integral part is set to the value  $limst$  issued from the characteristic line  $LISTM$  depending of the engine coolant temperature.

The integrator is limited between the upper limit  $limax_w$  and the lower limit  $limin_w$ . These limits can change if necessary. A reduction of the interval is allways filtered, an increase is never filtered. The filter time constant used is  $ZLIBG$ .

If the controller is not active ( $B_{llr}$  is false) the integrator limits (upper and lower limit) are filtered towards the end-value zero. The integral part is so disabled.

For active controller ( $B_{llr}$  is true) the limits are issued from the fixed values  $LIMN$  and  $LIMX$  for  $B_{vllr}=0$  and from  $LIMNV$  and  $LIMXV$  for  $B_{vllr}=1$ .

During start and until the controller is enabled ( $B_{llrein}=1$ ), the lower limit of the integral part is set to the value  $limst$ .

In the special case, when the diagnostic supposes a blocked idle speed control device the lower limit of the integral part is set to  $LIMNDLLR$  as long as  $B_{dllr}=1$ .

During the diagnosis of the canister purge system ( $B_{dtes}=1$ ) a specific lower integrator limit  $LIMNDTES$  is active.

If the minimal possible indicated torque or the maximum limit of the I-Part  $DMLLRIMXN(nmot)$  is reached ( $B_{mdmin}$  or  $B_{llrimx}$  is true), the appropriate limit of the integrator is set to the actual integrator value. So the integrator can't contieue to work in the torque limited direction.



## APP LLRRM 6.110 Application hint

Before calibrating the controller for car at rest:

The following precautions have to be taken before calibrating the controller:

- \* switch off the D-part of the controller: characteristic DVNG set to zero, characteristic FDDN set to 1.
- \* switch off the P-part of the controller: characteristic PVDN set to zero
- \* switch off the adaptation of torque requirement: set TMDMAD to a value greater than 120 °C.
- \* Be shure that the lowest target speed is selected. The engine must be warm, the torque reserve has to be determined. If it is not, set the torque reserve to a value between 3% and 4%.  
ATTENTION: For the calibration of the controller it is important to have a low engine speed with a low load because under these conditions the dead time of the system is at its maximum and the system tends to be instable..
- \* Calibrate a slow I-part of the controller to enable the system to reah exactly the low target speed.  
IVDN = 0.01 for all points of the characteristic.  
Then, when the target speed is reached, set the gain of the integral part to zero. The controller is then stopped. The engine should turn with the target speed.

Calibrating the controller:

ATTENTION: The load of the engine mus be as low as possible to have a big dead time in the system. During the calibration resp. the evaluation of the results, no additional load (AC-compressor, electrical load like fans or the power steering) must be switched on. For engines with low internal friction it could be necessary to press the clutch pedal to reduce additionnaly the engine load.

Calibration of the P-part: Increase the proportional gain by increasing the values of PVDN. Make a perturbation by tipping-in or switching on and off a load like the AC-compressor or the power steering. Increase the P-gain until the engine speed oscillates stationnary with a constant amplitude after an exitation. Now decrease progressively the P-gain until the engine speed stops oscillating. Verify the behaviour of the engine speed with a tip-in. The speed shoule reach the target value with at maximum 2 or 3 oscillations. The P-again is then calculated from:

$$PVDN = 0.5 * \text{limit\_gain} \quad (\text{all values of the characteristic must be the same}).$$

Calibration of the I-part: The integral part is calibrated after having done the first calibration of the proportional part. The P-part remains active during the calibration of the I-part. The calibration is done in the same way as for the proportinal part. The limit gain where the engine just doen't oscillate is searched.

The P-gain is the given by:

$$IVDN = 0.5 * \text{limit\_gain} \quad (\text{all values of the characteristic must be the same}).$$

With this calibration of the PI-controller the switching on or off of load like the AC-compressor, the power steering or the electrical cooling fan should not result in a engine speed oscillation. The speed drop could of course still be too large. This can be now reduced using the differential part of the controller.

Calibration of the D-part: The differential gain should be kept as small as possible to be shure that the system doesn't become nervous.

- \* In a dead zone of about  $\pm 20$  rpm about the target speed, the D-part shoule stay at zero, to avoid a nervous idling. Therefore calibrate the characteristic FDDN as follows:

dn	.....	-50	-20	20	50	...
FDDN	1.0	1.0	0	0	1.0	1.0

In a range of 20 rpm above and below the target speed the D-part is zero, between 20 rmp and 50 rpm of deviation the D-part increases and reaches it's maximum for speed deviations of more than 50 rpm.

- \* Increase slowly the differential gain DVNG of the controller an observe the speed drop when using power steering (keep the steering wheel forced to the right or left buffer to keep the load konstant). There should be no speed overshoot. Increase the D-gain until the speed drop is minimal and the speed behaviour is correct.
- \* If the behaviour of the engine speed after cranking or after a tip-in leads to an undershoot, ist is necessary to reduce te D-gain for engine speed above the target speed. In the characteristic FDDN the values for negative dn have to be reduced (for example 0.5 or even less).

After these calibrations the controller normally gives good results. It is still possible that under specific conditions like driving away without accelerating the reaction of the controller is insuffisant. The parameter of the controller have the to be optimized. For big speed deviations it is the necessary to increase the P- and I-gain. A limit for the gain is given by 75% of the limit gain mesasured preliminary. For small engines it is possible to increase the gain until the limit gain is reached. For these engines the gain for small speed deviations is more oriented towards the 75% of the limit gain.

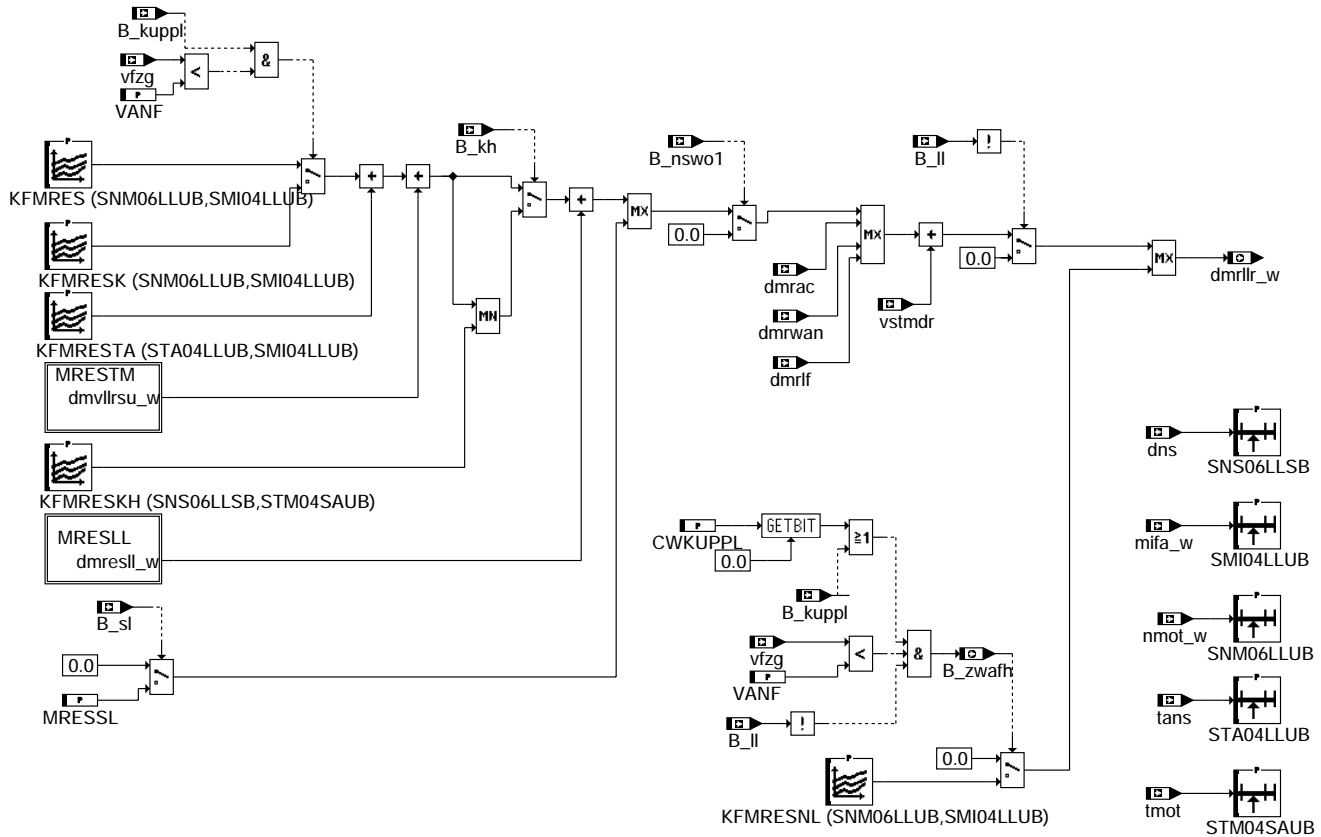
The calibration of the gain for driving car have to be smaller like them for car at rest (tendence of stucking). As initial values take the values for car at rest (just calibrated). The gain should not excced 50% of the limit gain. In practice it would either be only 25%.

IMPORTANT REMARK:

When judging the speed behaviour after a tip-in it is important that the dynmical following of the target speed is well calibrated. When an engine returns to it's target speed without any external load the controller shouldn't do any corrections. If necessary (I-part becomes too negative) increase the time TVDK to start the controller later after reaching the idle status (B.ll = 1).

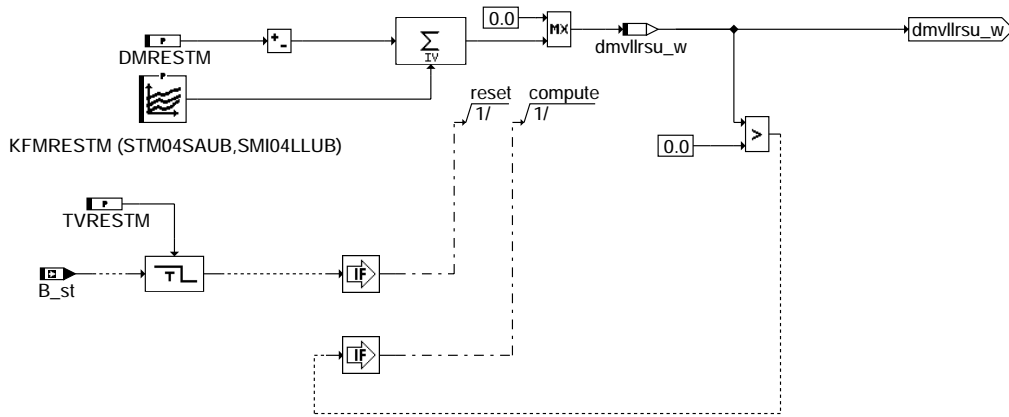
## LLRMR 12.40 Torque reserve for idle speed control

### FDEF LLRMR 12.40 Function definition



#### llrmr-llrmr

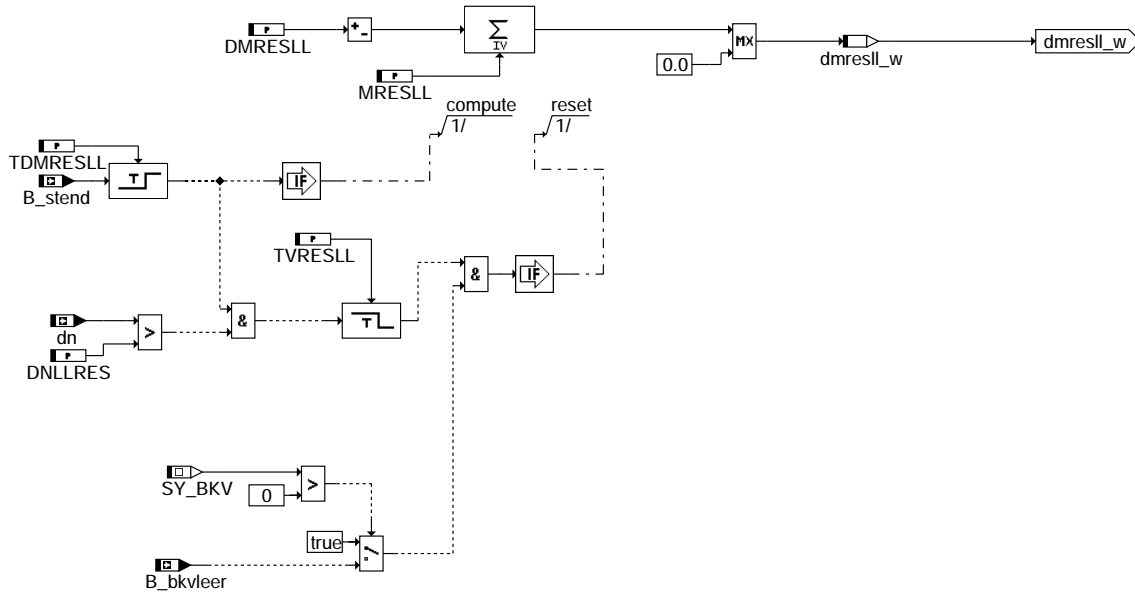
Calculation of the torque reserve during idling



#### llrmr-mrestm

Calculation of the torque reserve after the start-up phase

### Increase torque reserve after speed undershoot



### brake booster without enough vacuum

llrmr-mresll

Calculation of the torque reserve after a drop in speed

### ABK LLRMR 12.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWKUPPL			FW	Code word for clutch
DMRESLL			FW	LLR: reduction rate for increased torque reserve
DMRESTM			FW	Increment to reduce the torque reserve after start-up
DNLLRES			FW	LLR: dn threshold for increasing the torque reserve at idle
KFMRES	NMOT_W	MIFA_W	KF	LLR: torque reserve at idle and near-idle zone
KFMRESK	NMOT_W	MIFA_W	KF	LLR: torque reserve at idle and near-idle zone clutch disengaged
KFMRESKH	DNS	TMOT	KF	Torque reserve during catalyst heating
KFMRESNL	NMOT_W	MIFA_W	KF	Torque reserve in non idling state
KFMRESTA	TANS	MIFA_W	KF	Torque margin dependent on tans
KFMRESTM	TMOT	MIFA_W	KF	Map temp-dependent limiting of torque reserve
MRESLL			FW	LLR: increased torque reserve at idle after speed undershoot
MRESSL			FW	Torque reserve for power steering
SMI04LLUB	MIFA_W		SV	distribution: ind. torque for torque-reserve
SNM06LLUB	NMOT_W		SV	distribution of engine speed
SNS06LLSB	DNS		SV	Datapoint distribution, set-speed deviation, 06 datapoints., idle-speed control.
STA04LLUB	TANS		SV	distribution: tans for torque reserve
STM04SAUB	TMOT		SV	Datapoint distribution, engine temperature, 4 datapoints
SY_BKV			SYS	system constant: brake booster
TDMRESLL			FW	Inhibition time for the increased torque reserve after engine start
TVRESLL			FW	Hold time for increased torque reserve after engine speed drop
TVRESTM			FW	Initialization period: torque reserve after start-up
VANF			FW	Speed threshold for approach support

Variable	Source	Type	Description
B_BKVLCEER		EIN	condition brake booster without enough vacuum
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_LL	MSF	EIN	Condition idle
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_SL		EIN	Condition power steering
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_ZWAFH	LLRMR	AUS	enabling spark operation for vehicle drive-up-support
DMRAC	MDVERB	EIN	Torque reserve for AC-compressor
DMRESLL_W	LLRMR	LOK	increased Torque reserve at idle after speed undershoot
DMRLF	MDVERB	EIN	Torque reserve for cooling fan
DMRLLR_W	LLRMR	AUS	torque reserve for idle speed control
DMRWAN		EIN	Torque reserve for torque converter
DMVLLRSU_W	LLRMR	LOK	torque reserve after start
DN	LLRRM	EIN	speed deviation at idle speed control
DNS	LLRNS	EIN	LLR: difference of idle speed precontrol
MIFA_W	MSF	EIN	desired indicated engine torque
NMOT_W	SWADAP	EIN	engine speed



Variable	Source	Type	Description
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)
VSTMDR		EIN	Adjusting the torque reserve (tester interface)

### FW LLRMR 12.40 Fixed Values

Parameter	Value	Description
CWKUPPL		Code word for clutch
DMRESLL		LLR: reduction rate for increased torque reserve
DMRESTM		Increment to reduce the torque reserve after start-up
DNLLRES		LLR: dn threshold for increasing the torque reserve at idle
MRESLL		LLR: increased torque reserve at idle after speed undershoot
MRESSL		Torque reserve for power steering
TDMRESLL		Inhibition time for the increased torque reserve after engine start
TVRESLL		Hold time for increased torque reserve after engine speed drop
TVRESTM		Initialization period: torque reserve after start-up
VANF		Speed threshold for approach support

### FB LLRMR 12.40 Detailed description of function

The purpose of the torque reserve is to determine the operating point of the engine such that the ignition angle is not at its optimum ignition. It is assured by this that an increase in torque towards the optimum is still possible by a jump in the ignition angle towards the optimum. This function defines how large the possible torque reserve shall be:

In the normal case, the torque reserve is taken from the map KFMRES (dependent on dns and on tmot).  
As a rule, it is endeavored to keep this as small as possible so as not to unnecessarily worsen the engine's efficiency.

So as to be able to provide more torque when driving off if the driver is about to stall the engine, a switchover is made when the clutch has been depressed ( $B_{kuppl} = 1$ ) and at low driving speeds ( $vfzg < VANF$ ) to a torque reserve from the map KFMRESK. This switchover on operating the clutch is made without any filtering, the switch-back on releasing the clutch is however with filtering.

If a drop in speed then occurs because the idle-speed control has not managed to compensate for an additional load during key-ON, then the torque reserve is increased to a higher value MRESLL. The higher torque reserve is retained for the time TVRESLL before being gradually decreased over the ramp DMRESLL to the normal value. DMRESLL is a negative value! The described functionality is helpful when the steering assistance is stressed. The first stress when the speed drops increases the torque reserve, such that there is only a small drop in speed occurring caused by subsequent stresses (e.g. during parking maneuvers).

A torque reserve, dmrac, is built before air-conditioner compressor cuts in. This is so that the compressor's cut-in point can be designed to be almost independent of the speed.  
The engine is brought to an operating point with a higher torque reserve before the load is switched on.

A lower limit for the torque reserve is set to MRESSL if the information  $B_{sl}$  is received from power steering.

The torque reserve can be adjusted in the workshop using vstmdr (see %TKMWL).

The largest torque reserve demanded is always selected.

Partial shutdown of the function follows in case the bit  $B_{nswol}$  is set, whereby only that torque reserve when the air-conditioner compressor cuts in is considered further.

If the vehicle is not at its idle speed, then a torque can also be demanded from the map KFMRESNL when the clutch is depressed. This can be helpful, e.g. if the driver presses only slightly on the accelerator pedal when driving off or if the engine is likely to be stalled by this.

The map KFMRESKH can be used for catalytic-converter heating concepts with thermo-reactors. This constitutes an upper limit during idling for the torque reserve. This can be meaningful in order to limit the adjustment to retarded of the ignition angle.

The map KFMRESTA can be used to realize an additional adjustment to retarded of the ignition angle that is not dependent on the ambient temperature. This can be beneficial for engines where the knocking tendency is high, e.g. turbo-charged engines.

A torque reserve that is dependent on the engine temperature is calculated during the start-up phase in the block MRESTM. This is then gradually decreased after the end of the start-up phase to zero again.

### APP LLRMR 12.40 Application hint

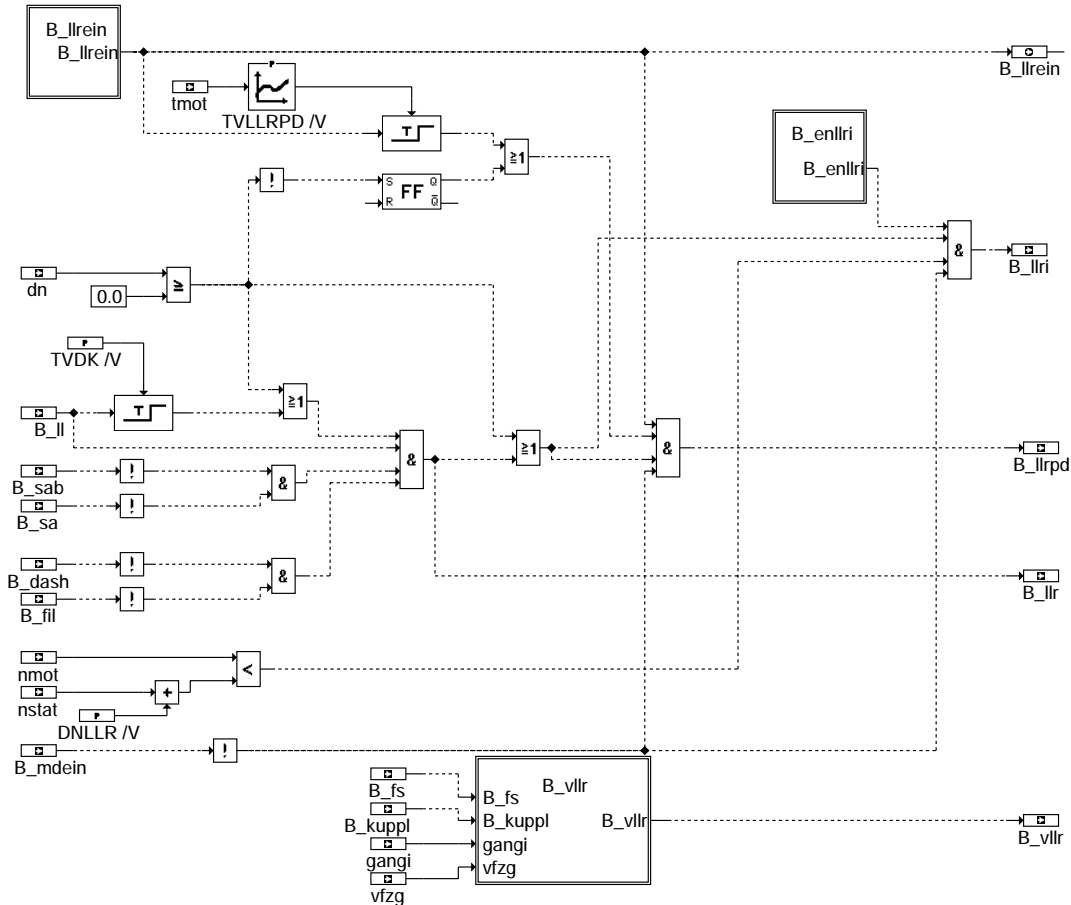
Adaptation of KFMRES: KFMRES constitutes the desired torque reserve in the range close to the idle speed. Since a torque reserve can also mean a deterioration of the engine's efficiency, the attempt is made to keep this as small as possible. On the other hand, the torque reserve helps to brake a sudden drop in the speed when load torque's suddenly occur (alternator when the electric fan cuts in, power steering, ...). A minimum torque must however be provided for the ignition over the fast path. The magnitude of this torque has to be determined by carrying out tests with the vehicle by quickly switching on the largest load. The engine engine may not be stalled by this. Neither may the engine speed drop below a set limit. The torque reserve is maintained at a constant value up to speeds of about 300 RPM above the set speed. The torque reserve is quickly reduced to zero at speeds up to 500 RPM.  
There shall be no torque reserve demanded by idle-speed control, LLR, at partial loads.  
Typical values for the torque reserve are about 3 % to 4 %.

Adaptation of DNLLRES, TVRESLL, MRESLL and DMRESLL:

DNRESLL: Negative differences from the set speed that can just still be tolerated. The torque reserve is increased if the engine speed falls below this threshold. Typical value is approx. 120 RPM  
TVRESLL: Time during which the increased torque reserve stays at the higher value. Typically, this time shall be sufficiently long such that a normal driver can park the vehicle (several power-steering maneuvers needed). This time is normally about 30 seconds.  
MRESLL: Absolute value for the torque-reserve increase. A additional torque reserve of 4 % is often sufficient here.  
DMRESLL: The torque-reserve increase is removed again after elapse of the hold time. This gradual decrease of the torque reserve should be completed within a time period of 10 seconds.  
DMRESLL is a negative variable.

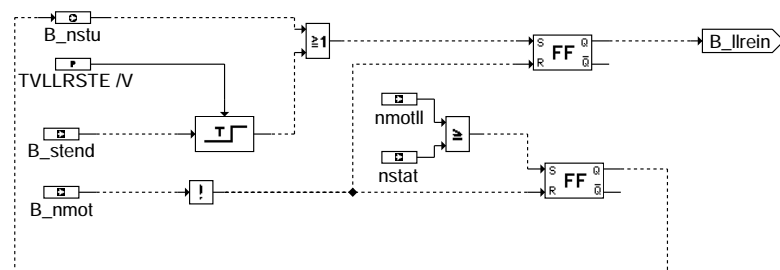
## LLRBB 505.10 Operating conditions of idle speed control

### FDEF LLRBB 505.10 Function definition



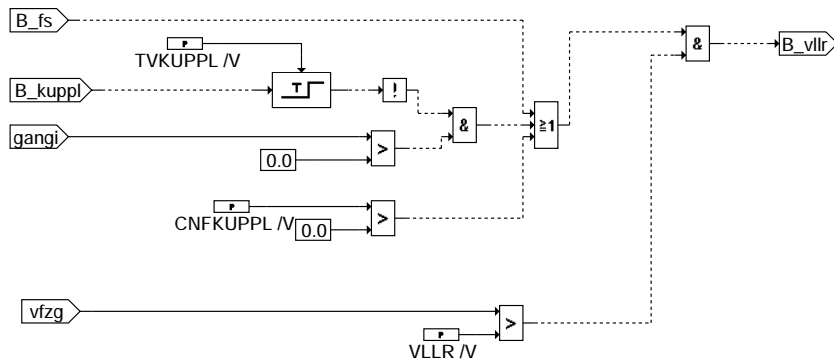
#### llrb-b-llrb

Formation of the Activation Conditions of the Idle Control



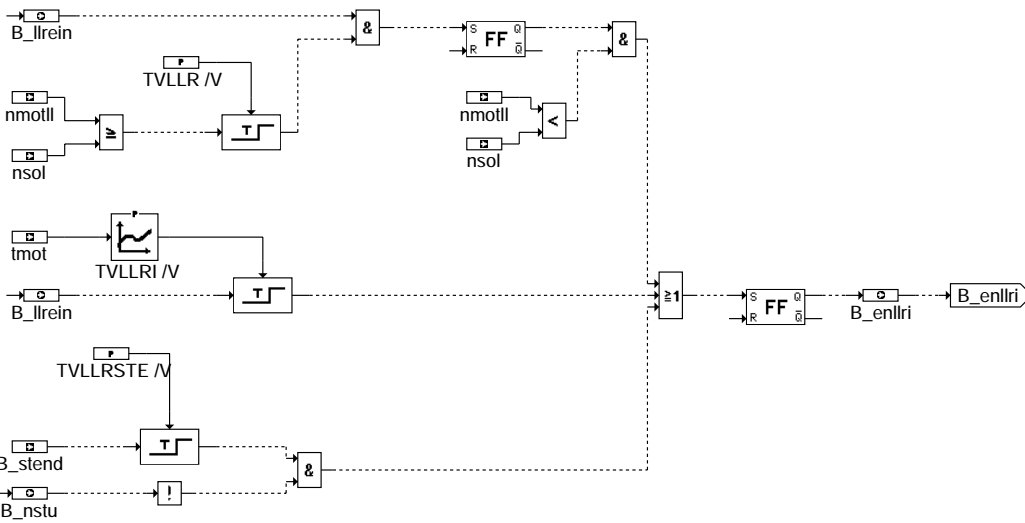
#### llrb-b-llrein

Enabling of the Idle Control after Start:



**llrb-b-vllr**

Detection, Whether a Frictional Connection Exists Between Engine and Drive Shaft



**llrb-b-enlri**

Enabling of the I Component

**ABK LLRBB 505.10 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CNFKUPPL			FW	Configuration flag for the evaluation of the clutch switch in the ISC
DNLLR			FW	Engine speed range above nstat to enable the ISC
NMIN			FW	minimum engine speed
TVDK			FW	delay time after closing of the throttle
TVKUPPL			FW	Delay time for the clutch information
TVLLR			FW	turn-on delay: B_llri at engine speed overshoot
TVLLRI	TMOT		KL	delay time to enable I-component after start-up
TVLLRPD	TMOT		KL	Maximal delay time to enable PD components after start-up
TVLLRSTE			FW	enable idle speed control after start
VLLR			FW	vehicle speed limit for idle speed control
Variable	Source		Type	Description
B_DASH	MDFAW		EIN	condition: limitation of negative torque gradient active
B_ENLLRI	LLRBB		AUS	enable integrator: idle speed controller
B_FIL	MDFAW		EIN	condition: low pass filter for transition to or from fuel cut-off active
B_FS	BBGANG		EIN	Condition driving state (automatic gear box)
B_KUPPL	SWADAP		EIN	EGAS Condition clutch is disengaged
B_LL	MSF		EIN	Condition idle
B_LLR	LLRBB		AUS	condition idle speed control
B_LLREIN	LLRBB		AUS	Condition idle speed control is active
B_LLRI	LLRBB		AUS	Condition activation of I-part of idle speed control
B_LLRPD	LLRBB		AUS	Condition activation of PD-part of idle speed control
B_MDEIN	MDKOG		EIN	Condition actions on the torque are active
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_NSTU	LLRBB		AUS	Changeover of rotational speed from nstat to nmot after start
B_SA	MDRED		EIN	Condition fuel cut-off





Variable	Source	Type	Description
B_SAB	MSF	EIN	Condition fuel cut-off requested
B_STEND	BBSTT	EIN	condition end of start
B_VLLR	LLRBB	AUS	Condition vehicle is moving with engaged gear
DN	LLRRM	EIN	speed deviation at idle speed control
GANGI	SWADAP	EIN	Engaged gear
NMOT	SWADAP	EIN	engine speed
NMOTLL	BGNMOT	EIN	engine speed
NSOL	LLRNS	EIN	idle reference speed
NSTAT	LLRNS	EIN	Stationary reference speed
TMOT	SWADAP	EIN	Engine temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)

### FW LLRBB 505.10 Fixed Values

Parameter	Value	Description
CNFKUPPL		Configuration flag for the evaluation of the clutch switch in the ISC
DNLLR		Engine speed range above nstat to enable the ISC
NMIN		minimum engine speed
TVDK		delay time after closing of the throttle
TVKUPPL		Delay time for the clutch information
TVLLR		turn-on delay: B_llri at engine speed overshoot
TVLLRSTE		enable idle speed control after start
VLLR		vehicle speed limit for idle speed control

### FB LLRBB 505.10 Detailed description of function

The activation conditions for the idle control are formed in this functional block.  
Listed, these are:

- B\_llrein:** Enabling of the idle control after start takes place, once the engine speed has reached the steady-state desired nstat for the first time. If the engine is running, but cannot reach nstat, then B\_llrein TVLLRSTE is set after end of start. B\_llrein is reset, if a software initialization takes place or if the engine speed drops below the threshold NMIN (engine stalled or turned off, but ECU after-run not yet terminated)
- B\_vllr :** Condition vehicle is rolling at engaged gear: If the vehicle speed exceeds the threshold VLLR and if the clutch is not operated, the bit B\_vllr is set.  
If no gear is engaged, the vehicle is at standstill or the clutch is operated (B\_kuppl=1), the bit is cleared. The bit B\_vllr is set, if a frictional connection exists between the engine and the drive shaft.  
ATTENTION: Since the clutch switch already activates at the most minor clutch pedal movements on some vehicles, this information is of no use for the LLR. The evaluation of the clutch switch is suppressed via CNFKUPPL > 0. B\_vllr is then only set dependent on the vehicle speed.
- B\_llr :** Condition for idle control: This bit indicates, whether the idle control has been enabled (B\_llr = 1) or whether it is still blocked (B\_llr = 0).  
Enabling of the idle control takes place if: The idle bit has been set (B\_ll = 1), no request for fuel cut-off on overrun is given (B\_sab = 0), no fuel cut-off is given (B\_sa = 0), already TVDK seconds have passed since the idle bit has been reset, underspeed is given (dn > 0), no dashpot is active, no external torque interventions (MSR or ASR) take place (B\_mdein=0), no torque filtering for SAWE takes place (B\_fil=0) and the engine speed is within a range below of nstat+DNLLR.
- B\_llrpd :** Condition for enabling of the P and D component of the idle controller: The proportional and differential components of the idle controller are enabled, if no external torque intervention takes place and if the LLR is active (B\_llrein=1) and if the controller is active (B\_llr=1) or if underspeed is given.  
The P component is only enabled after engine start, if the engine has made a speed overshoot or if the end of start bit (B\_stend) has been set since a time greater than TVLLRPD.
- B\_llri :** Condition for enabling of I component of the idle controller: The integrator of the idle controller is enabled, if the controller has been enabled (B\_llr = 1), no torque intervention is active (B\_mdein = 0) and B\_enllri is set.
- B\_enllri:** This bit ensures that the I component is not active during the start overshoot. The I component is only to be activated, once nmot drops below the desired speed nsol for the first time.  
If nmot remains above nsol for longer than TVLLRI, the I component is activated.  
If the engine is running, but remains below nsol, the I component is also activated to "pull up" the speed.

## APP LLRBB 505.10 Application hint

Adjustment of VLLR: VLLR should be chosen as small as possible, so as to already detect a slowly rolling vehicle as not being at standstill. The state vehicle is rolling at idle in the 1st gear must definitely be detected, also in case of underspeed. The speed threshold necessary for this can be estimated as follows:

$$VLLR = (nsol\_minimum\ value - 200) * v1000 / 1000$$

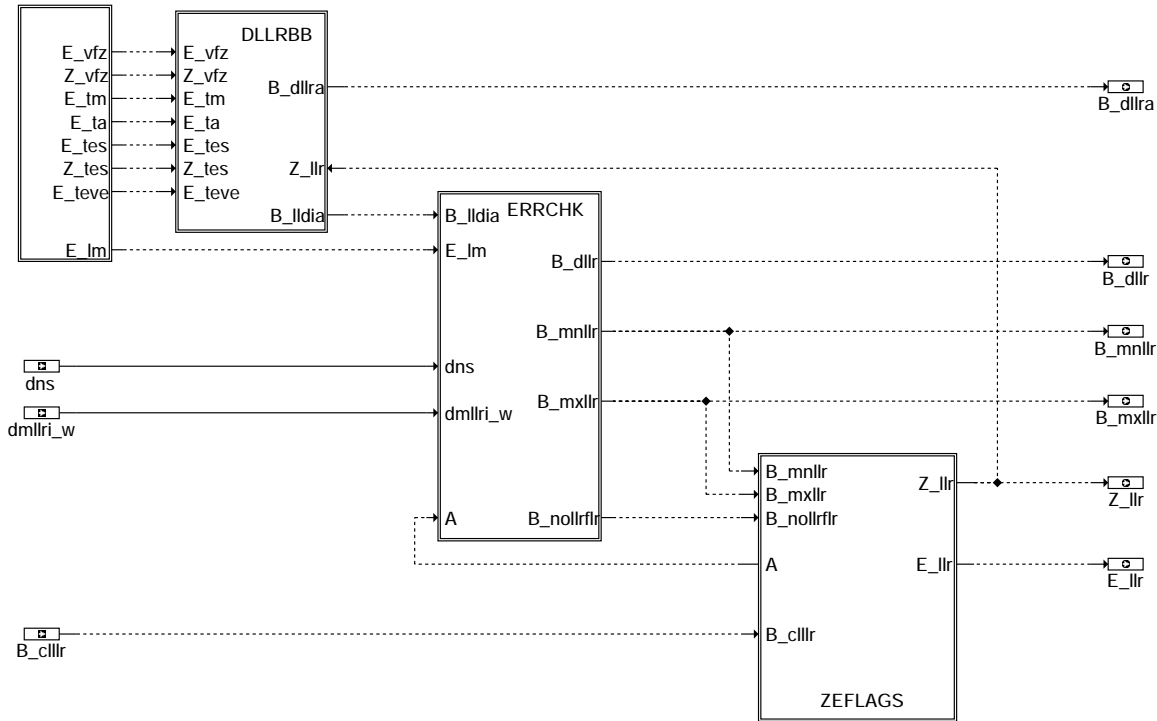
where v1000 is the vehicle speed at 1000 rpm in the 1st gear. (This usually lies between 7 km/h and dependent on the fitted tiers and the transmission design).

Adjustment of TVDK: This controller blocking time is to prevent the controller from already starting to operate immediately after the throttle valve having been closed, but at still high speed. After a tip-in with a final speed close to the maximum speed (about 6000 rpm), TVDK must be chosen that large that the controller only starts operating in the capture range of the desired speed correction. From experience values for TVDK lie between 0.5 and 1 second. If TVDK is too small, an undesired underswing of the speed may occur after tip-in, since the too early started controller has already reached a too large negative component, which must now be reduced again.

Adjustment of TVKUPPL: This delay time for the clutch information is necessary, since the clutch switch at the pedal already switches when the pedal is touched, but since the actual disengagement is only reached once the clutch pedal has been nearly completely floored. The time TVKUPPL should lie at about 100 ms.

## DLLR 28.80 Diagnosis: idle speed control, recognising a blocked actuator

### FDEF DLLR 28.80 Function definition

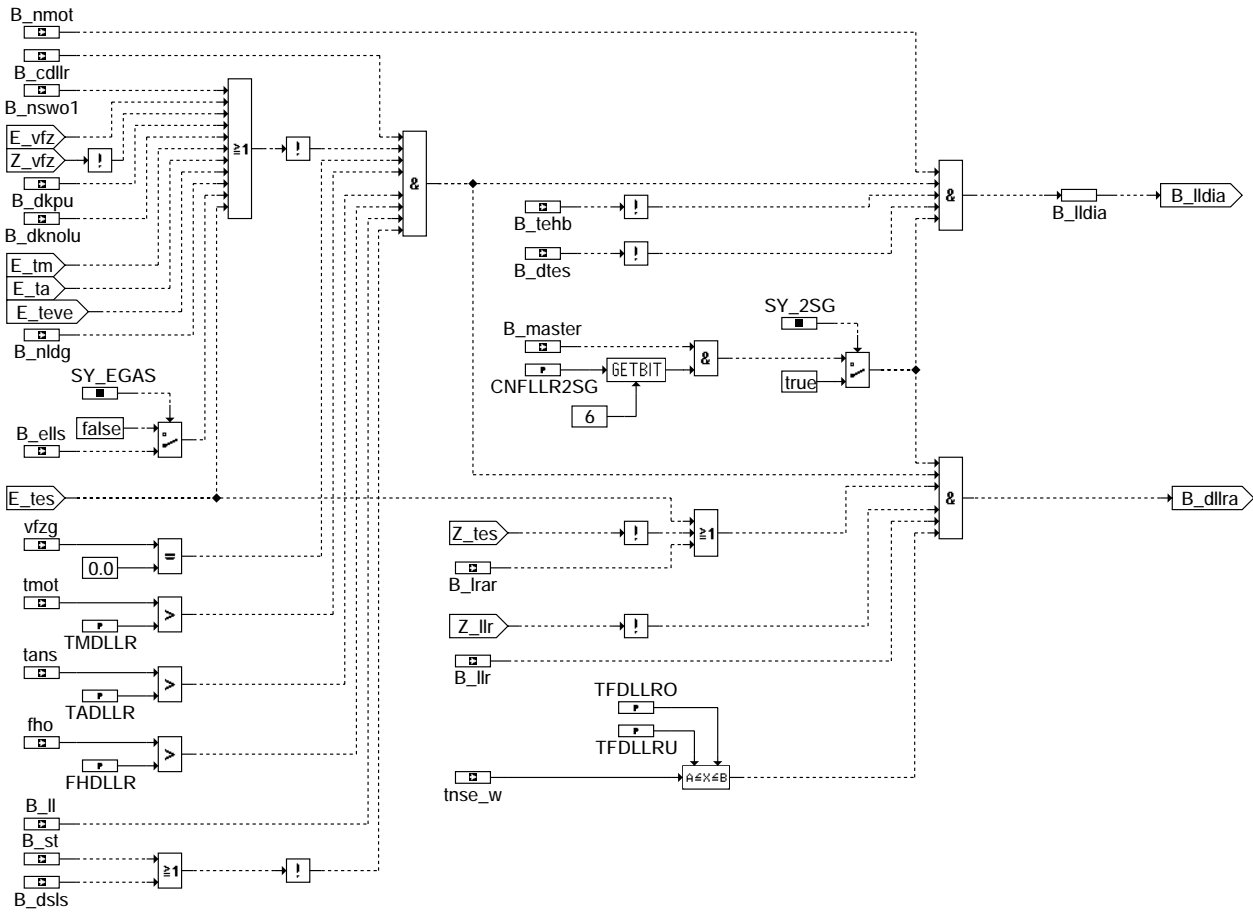


dllr-dllr

General view of the idle speed control diagnosis

The diagnosis of the idle speed control is divided into three parts:

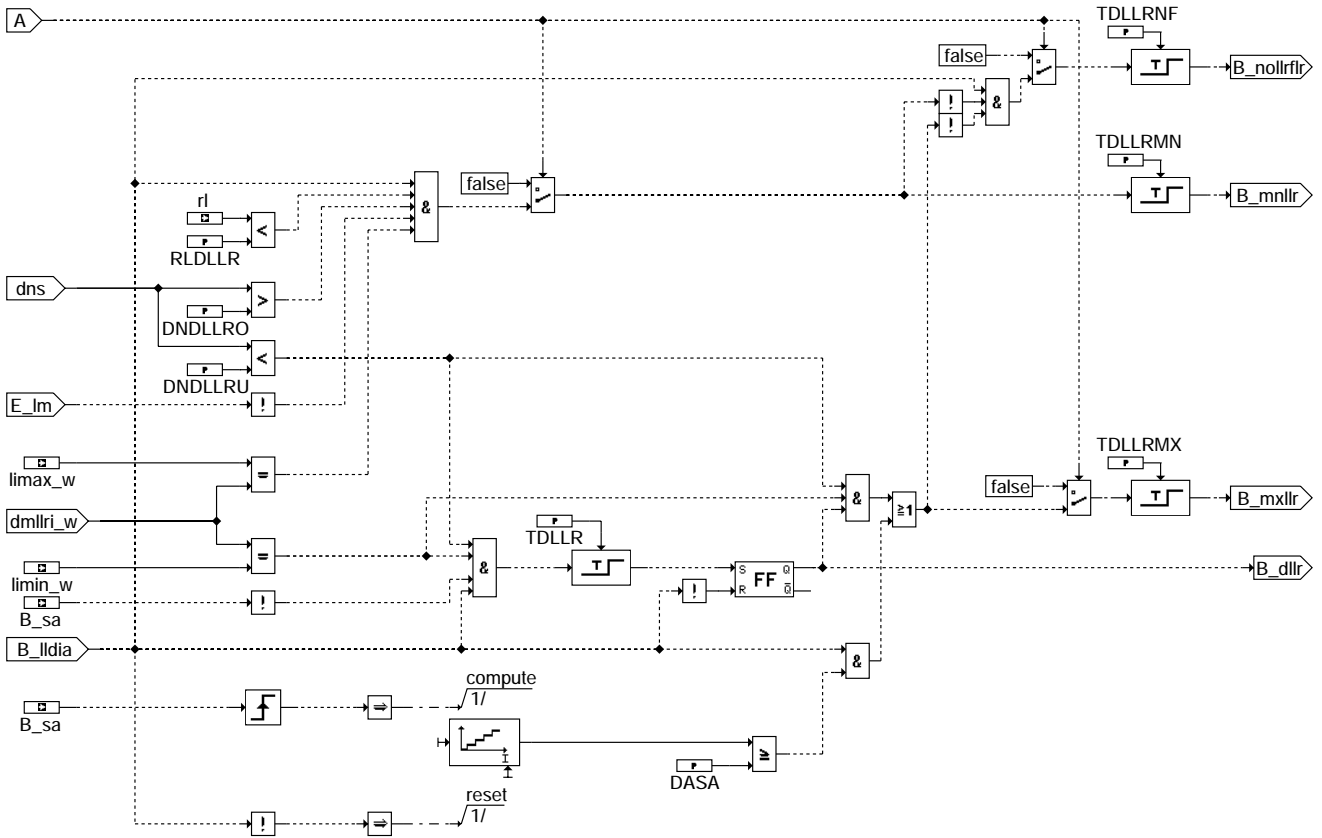
1. DLLRBB : conditions to activate the function
2. ERRCHK : error check of the idle speed control
3. ZEFLAG : management of the error and cycle flags



**dllr-dllrbb**

DLLRBB: conditions to activate the function

- The function is activated when:
1. the EURO code sets the flag B\_cdllr
  2. other functions have no errors detected (upper OR-gatter)
  3. the engine operates under predefined conditions (lower part of the figure)
- The diagnosis is enabled when the flag B\_lldia is true (set to 1).



**dllr-errchk**

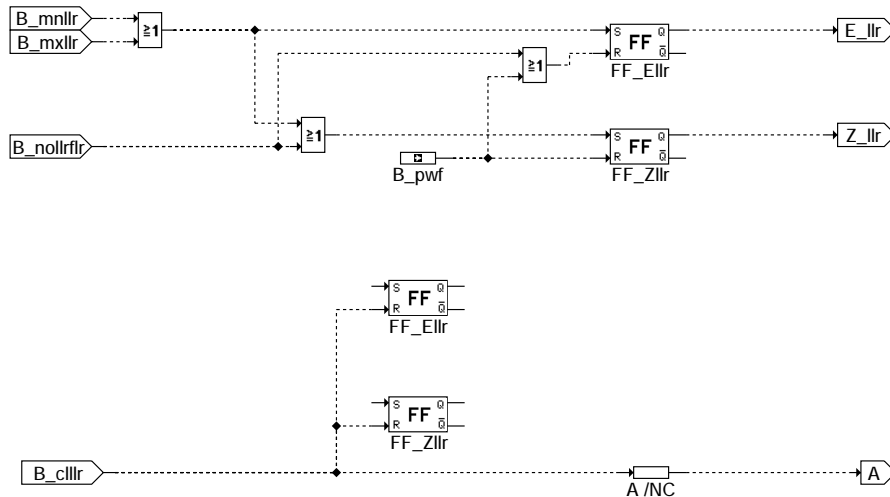
ERRCHK: error check of the idle speed control

This part of the function works only if B\_lldia is set to 1 (see above).

In the upper part of the figure (upper AND-gatter) occurs the check for engine speed too low. If the engine speed remains more than DNDLLRO rpm under the target speed and the ISC-integrator reaches the upper limit DMLLRIDU for a time longer than TDLLRMN, the error-flag B\_mnlir is set.

In the lower part of the figure the check for engine speed to high is made. If the integrator remains at its lower limit DMLLRIDU and the engine speed difference ist DNDLLRU the flag B\_dllr is set after the time TDLLR. This causes the lower limit of the integrator to be changed to LIMNDLLR (see %LLRMD, LIBEG). If now the limit DMLLRIDU2 is reached for more than TDLLRMX seconds, the flag B\_mxllr is set.

This flag is also set if during one continuous diagnosis phase (B\_lldia set) the flag B\_sa is set more than DASA times. This is normally impossible vehicle at rest without opening the throttle.



**dllr-zeflags**



ZEFLAGS: management of the error and cycle flags

If the diagnosis worked one time completely, independently if an error occurred, the cycle flag is set.  
If an error occurred the error-flag is set additionally.

## ABK DLLR 28.80 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CNFLLR2SG			FW	Configuration word for idle speed control 2-ECU-concept (slave)
DASA			FW	number of fuel cut-out phases to detect ISC-actuator error
DNDLLRO			FW	Maximal speed deviation (low speed) for diagnosis of idle speed control
DNDLLRU			FW	Maximal speed deviation (high speed) for diagnosis of idle speed control
FHDLLR			FW	altitude threshold for performing of ISC-actuator diagnosis
RLDLLR			FW	Cylinder filling threshold for ISC diagnosis
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_EGAS			SYS (REF)	System constant E-GAS present
TADLLR			FW	intake air temperature threshold for ISC-actuator diagnosis
TDLLR			FW	Time delay for setting the condition diagnosis of ISC-actuator
TDLLRMM			FW	Time delay before storing error of closed ISC-actuator
TDLLRMX			FW	Time delay before storing the error ISC-actuator open
TDLLRNF			FW	Time delay before storing ISC-actuator with no error
TFDLLRO			FW	Upper limit for time window for DLLR
TFDLLRU			FW	Lower limit for time window for DLLR
TMDLLR			FW	Engine temperature threshold for ISC-actuator diagnosis
Variable	Source		Type	Description
B_CDLLR	PROKON		EIN	function active per codeword CDLLR
B_CLLLR			EIN	condition clear failure path DLLR
B_DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP		EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DLLR	DLLR		AUS	Active diagnostic: ISC-actuator diagnostic
B_DLLRA	DLLR		AUS	Condition DLLR request
B_DSLS			EIN	condition for active diagnosis of secondary air system
B_DTES	GKRA		EIN	Condition for active diagnosis of canister purge system
B_ELLS			EIN	Condition: error idle speed actuator
B_LL	MSF		EIN	Condition idle
B_LLDIA	DLLR		LOK	Diagnosis of idle speed control released
B_LLR	LLRBB		EIN	condition idle speed control
B_LRAR	TEB		EIN	condition for reduced correction ranges at LRA
B_MASTER			EIN	Condition MASTER-ECU
B_MNLLR	DLLR		AUS	Error 'Idle speed too low'
B_MXLLR	DLLR		AUS	Error 'Idle speed too high'
B_NLDG			EIN	condition limp-home function speed sensor
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_NSWO1	PROKON		EIN	condition engine speed > NSWO1
B_PWF			EIN	Condition for powerfail
B_SA	MDRED		EIN	Condition fuel cut-off
B_ST	SWADAP		EIN	condition for start
B_TEHB	TEB		EIN	condition for canister purge system with high canister load
DFP_LM	DLLR		DOK	ECU-internal fault path no.: main-load sensor
DFP_TA	DLLR		DOK	ECU int fault path no.: air intake temperature TANS
DFP_TES	DLLR		DOK	Internal error path number evap system monitoring, pcv Struck open
DFP_TVE	DLLR		DOK	Internal fault path number: canister purge valve power stage
DFP_TM	DLLR		DOK	Internal fault path number: engine temperature
DFP_VFZ	DLLR		DOK	ECU int. fault path no.: vehicle speed signal
DMLLR1.W	LLRRM		EIN	desired torque change from the idle speed control (I-)
DNS	LLRNS		EIN	LLR: difference of idle speed precontrol
E_LLR	DLLR		AUS	Error flag: idle speed control
E_LM	EGFE		EIN	Error flag: main load sensor
E_TA	GGTFA		EIN	error flag: TANS
E_TES	DTEV		EIN	error flag: canister purge system diagnosis
E_TVE	DTEVE		EIN	error flag: canister purge valve power stage
E_TM	GGTFM		EIN	Error flag: engine temperature tmot
E_VFZ	EGAG		EIN	Error flag: vehicle speed signal
FHO	BGPU		EIN	Correction factor altitude
LIMAX_W			EIN	Idle speed control integrator upper limit
LIMIN_W			EIN	Idle speed control integrator lower limit
RL	SWADAP		EIN	relative air charge
TANS	SWADAP		EIN	Intake air temperature
TMOT	SWADAP		EIN	Engine temperature
TNSE_W	BBSTT		EIN	time counter at end of start (16 bit)
VFZG	SWADAP		EIN	vehicle speed (km/h)
Z_LLR	DLLR		AUS	cycle flag: diagnostic ISC-actuator
Z_TES	DTEV		EIN	cycle flag of canister purge system
Z_VFZ	EGAG		EIN	cycle flag: vehicle speed signal



## FW DLLR 28.80 Fixed Values

Parameter	Value	Description
CNFLLR2SG		Configuration word for idle speed control 2-ECU-concept (slave)
DASA		number of fuel cut-out phases to detect ISC-actuator error
DNDLLRO		Maximal speed deviation (low speed) for diagnosis of idle speed control
DNDLLRU		Maximal speed deviation (high speed) for diagnosis of idle speed control
FHDLLR		altitude threshold for performing of ISC-actuator diagnosis
RLDLLR		Cylinder filling threshold for ISC diagnosis
TADLLR		intake air temperature threshold for ISC-actuator diagnosis
TDLLR		Time delay for setting the condition diagnosis of ISC-actuator
TDLLRMN		Time delay before storing error of closed ISC-actuator
TDLLRMX		Time delay before storing the error ISC-actuator open
TDLLRNF		Time delay before storing ISC-actuator with no error
TFDLLRO		Upper limit for time window for DLLR
TFDLLRU		Lower limit for time window for DLLR
TMDLLR		Engine temperature threshold for ISC-actuator diagnosis

## FB DLLR 28.80 Detailed description of function

The diagnosis of the idle speed control is enabled only if the flag B\_lldia is set.

The DLLR-function controls the behaviour of the ISC-integrator dmlri\_w in dependence of the engine speed.

If the engine speed difference is greather than DNDLLRO and the integrator is greather than DMLLRIDO the flag B\_llrmn is set after waiting the time TDLLRMN.

If the engine speed difference is lower than DNDLLRU and the integrator dmlri\_w is lower than DMLLRIDU the lower integrator limit is set to LIMNDLLR after the time TDLLR. If the integrator reaches the new limit DMLLRDIU2 and stays there for more than TDLLRMX seconds, the flag B\_llrmx is set.

If the throttle stays too much opened (still with B\_ll=1), the engine speed can rise until fuel cut-off occurs. The speed oscillations and the fuel cut-off phases disable the integrator to reach a lower limit. Therefore the function monitors the times of appearing of the flag B\_sa. If this flag ist set and reset more than DASA times the flag B\_mxllr is also set.



## APP DLLR 28.80 Application hint

The detection of an idle speed control error has to occur before other functions who need the ISC have their diagnosis working. The time disposable for the DLLR during the FTP-cycle is only 26 seconds (this is the longest idle phase with warm engine at second 620).

TMDLLR: set to 80°C

RDLLR: bigger than rl at idle. Is used to detect if the driver tries to hold his car at the hill using the clutch and having an engine speed under the target speed.

DNDLLRO: 100 rpm: engine speed more than 100 rpm under the target speed must be detected as an error.

DMLLRIDO: <= LIMX

DNDLLRU: 200 rpm: engine speed more than 200 rpm above the target speed must be detected as an error.

DMLLRIDU: >= LIMN

DASA: minimum equal to 2

DMDLLIDU2: approx. 5% lower than LIMN = LIMNDLLR

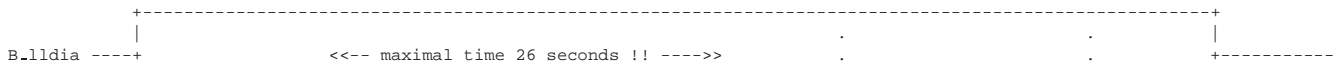
TDLLRNF: max. 20 sec.

TDLLRMX: TDLLRMX and the time needed by the integrator to reach the limit DMLLRIDO when engine speed is 100 rpm too low (depends of the integral gain of the controller) must be less than TDLLRNF.

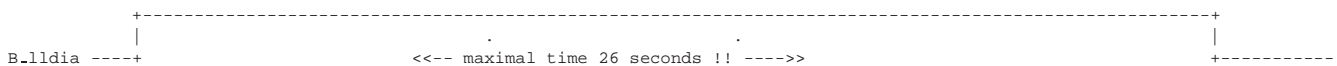
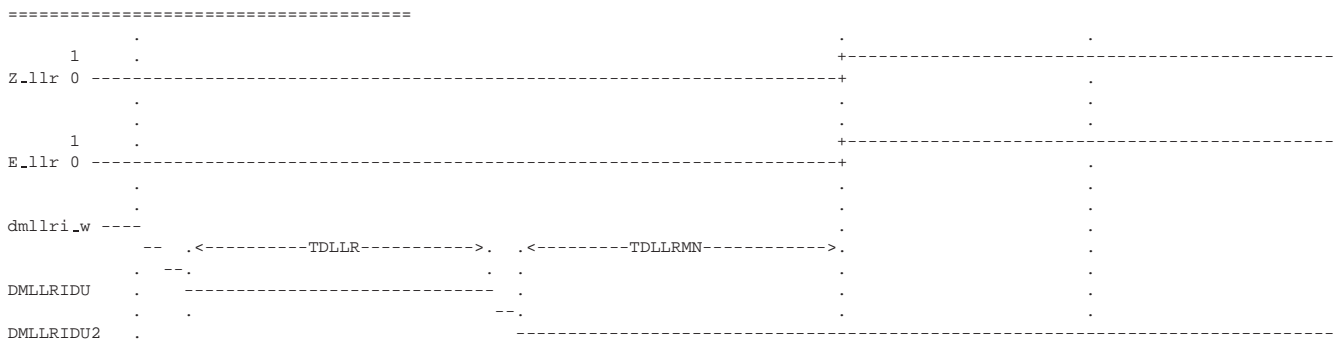
TDLLRMN: TDLLRMN and the time needed by the integrator to reach its upper limit DMLLRIDU when engine speed is 200 rpm too high and

TDLLR: TDLLR, and the time the integrator needs to reach the new limit DMDLLIDU2 when engine speed is still 200 rpm too high must be lower than TDLLRNF.

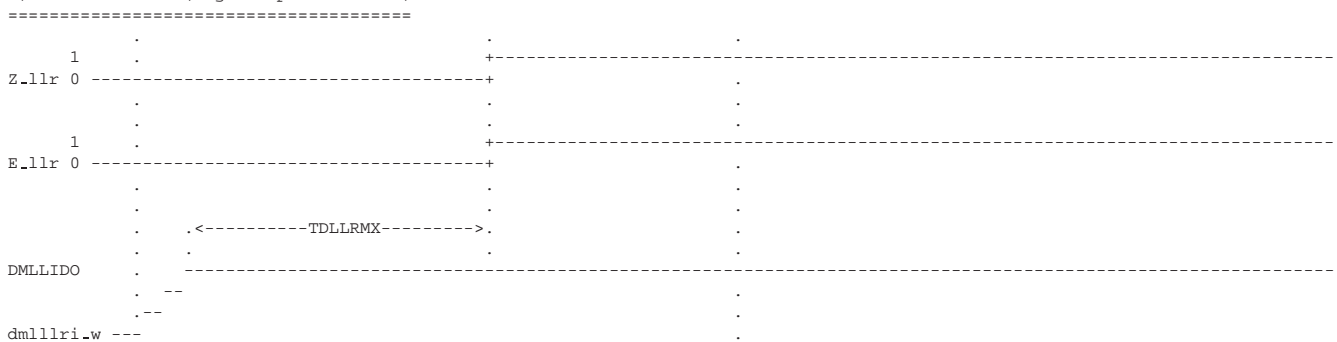
The available time during the FTP cycle is schematically the following:



1) Case n > nsol (engine speed too high)

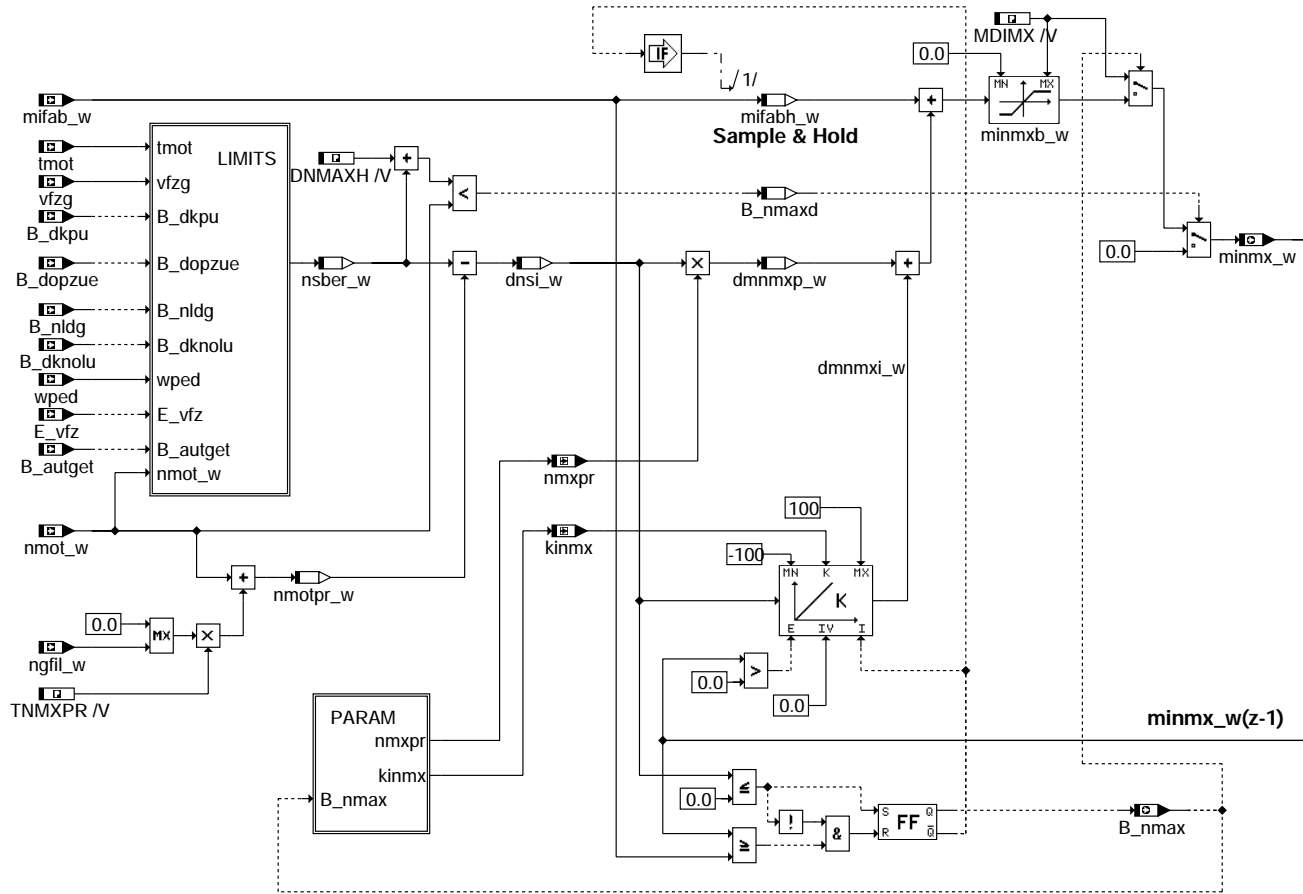


2) Case n < nsol (engine speed too low)



## NMAXMD 18.20 Torque calculation during maximum speed control

### FDEF NMAXMD 18.20 Function definition



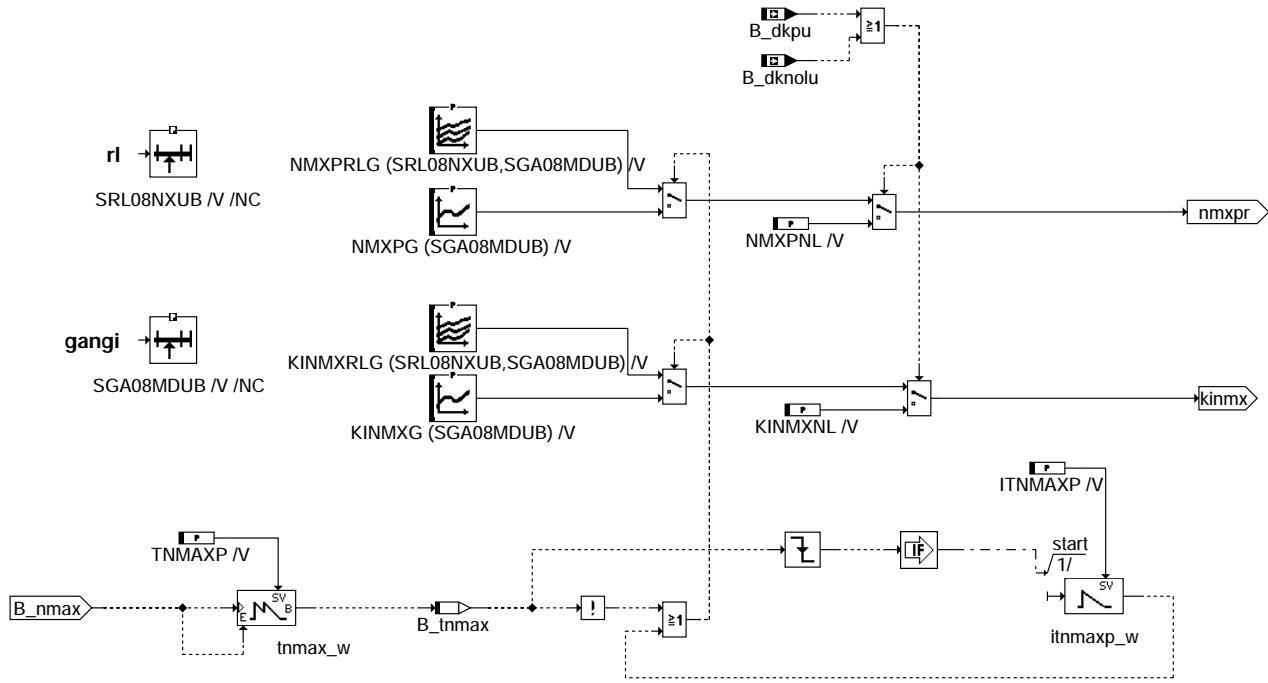
nmaxmd-nmaxmd

nmaxmd-nmaxmd





Subfunction PARAM: Controller parameter



nmaxmd-param

### ABK NMAXMD 18.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DNMAX			FW	engine speed threshold for engine speed limitation, transient limit
DNMAXDZ			FW	delta for diminution of engine speed limit
DNMAXH			FW (REF)	hysteresis for hard rpm limiting
ITNMAXP			FW	duration of alternative tuning of engine speed limitation
ITNMXH			FW	dwel time below lower engine speed limit before activation of upper limit
KINMXG	GANGI		KL	gain of integral component for NMAX control
KINMXNL			FW	integrator gain for engine speed limitation in case of throttle actuator error
KINMXRLG	RL	GANGI	KF	gain of integral component for NMAX control
MDIMX			FW (REF)	maximum limit indicated engine torque
NMAX			FW (REF)	engine-speed limitation, transient limit
NMAXDV			FW (REF)	engine speed limit at fault of the vehicle speed signal
NMAXDVG	GANGI		KL	rpm limit in case of fault detection velocity signal
NMAXDZ			FW	engine speed limit for condition double ignition
NMAXNL			FW	engine speed limit for limp-home function speed sensor
NMAXOG			FW	raised engine speed limit
NMAXSGS			FW	
NMXDAEF	WPED		KL	maximum permitted engine speed for throttle actuator substitute function
NMXDKPU			FW (REF)	Maximum permitted engine speed in case of unknown or wrong throttle position
NMXPGL	GANGI		KL	P component for NMAX control
NMXPNL			FW	P component for engine speed limitation in case of throttle actuator error
NMXPRLG	RL	GANGI	KF	P component for NMAX control
SGA08MDUB	GANGI		SV (REF)	base point distribution of actual gear 8 b.pt.
SRL08NXUB	RL		SV (REF)	
TMOTNMX			FW	temperature threshold for activation of raised engine speed limitation
TNMAXP			FW	dwel time NMAX limit until activation of alternative tuning
TNMXH			FW	duration of raised engine speed limit
TNMXPR			FW (REF)	rpm prediction horizon for NMAX control
VNMX			FW	vehicle speed threshold for activation of raised engine speed limit

### Variable

Variable	Source	Type	Description
B_AUTGET	PROKON	EIN	condition automatic gearbox
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DOPZUE	NLPH	EIN	Condition double ignition
B_NLDG		EIN	condition limp-home function speed sensor
B_NMAX	NMAXMD	AUS	1 = maximum engine speed exceeded
B_NMAXD	NMAXMD	LOK	condition rpm limiting with injection masking
B_SELESPED		EIN	condition: car with selespeed
B_SGSNL		EIN	demand for engine speed limitation from SGS
B_TNMAX	NMAXMD	LOK	Bit, timer for parameter switch has run down
DMNMXPR_W	NMAXMD	LOK	torque P-component for NMAX control
DNSLW	NMAXMD	LOK	difference between nominal and actual engine speed
E_BUOF	CAN	EIN	



Variable	Source	Type	Description
E_CHKUP		EIN	error flag: CAN-bus, timeout clutch
E_MUTE	CAN	EIN	
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
KINMX	NMAXMD	LOK	gain of integral component for NMAX control
MIFABH_W	NMAXMD	LOK	limited desired indicated engine torque (sample & hold)
MIFAB_W	MDKOG	EIN	limited desired indicated engine torque
MINMX_W	NMAXMD	AUS	indicated nominal torque for NMAX limiting
NGFIL_W	SWADAP	EIN	filtered engine-speed gradient
NMAXDVG_W	NMAXMD	LOK	gear dependant rpm limit in case of fault detection velocity signal
NMOTPR_W	NMAXMD	LOK	engine speed
NMOT_W	SWADAP	EIN	engine speed
NMXPR	NMAXMD	LOK	P component for NMAX control
NSBER_W	NMAXMD	LOK	Calculated requested engine speed of the NMAX controller
TMOT	SWADAP	EIN	Engine temperature
VFZG	SWADAP	EIN	vehicle speed (km/h)
WPED	GGPED	EIN	Standardized accelerator pedal angle

### FW NMAXMD 18.20 Fixed Values

Parameter	Value	Description
DNMAX		engine speed threshold for engine speed limitation, transient limit
DNMAXDZ		delta for diminution of engine speed limit
ITNMAXP		duration of alternative tuning of engine speed limitation
ITNMXH		dwel time below lower engine speed limit before activation of upper limit
KINMXNL		integrator gain for engine speed limitation in case of throttle actuator error
NMAXDZ		engine speed limit for condition double ignition
NMAXNL		engine speed limit for limp-home function speed sensor
NMAXOG		raised engine speed limit
NMAXSGS		
NMXPNL		P component for engine speed limitation in case of throttle actuator error
TMOTNMX		temperature threshold for activation of raised engine speed limitation
TNMAXP		dwel time NMAX limit until activation of alternative tuning
TNMXH		duration of raised engine speed limit
VNMX		vehicle speed threshold for activation of raised engine speed limit

### FB NMAXMD 18.20 Detailed description of function

A PI controller with rpm prediction is used to limit the engine speed.  
The actual engine speed predicted over a time horizon TNMXPR (prediction only with positive engine speed gradient) is compared with the maximum engine speed NMAX. If the predicted actual engine speed nmotpr\_w exceeds the maximum permitted value NMAX, then a PI controller is used to calculate the delta torques dnmnxp\_w and dnmnxi\_w, and add them with the indicated driver torque to minmxb\_w so that the actual engine speed is limited to NMAX.  
The torque mifabh\_w which is used for the limitation is only updated when the permissible torque minmxb\_w is greater than the actual limited driver torque mifab\_w. This stabilizes the torque minmxb\_w and prevents the driver from exciting a torque oscillation with the pedal. The output variable minmxb\_w is limited to between the minimum value 0 and the maximum value MDIMX.  
If minmx\_w(z-1) equals zero, then the integrator of the PI controller is stopped. If the predicted actual engine speed is less than NMAX (dnsi\_w < 0) and the torque minmx\_w is greater than or equal to the driver torque mifab\_w, then the condition B\_nmax is revoked and the indicated torque minmx\_w is switched to the default value MDIMX, so that no intervention occurs.  
If the engine speed exceeds the threshold NMAX, then the condition B\_nmax is set. This permits cylinder masking when air and ignition angle intervention is no longer sufficient (see %MDRED).

Subfunction PARAM:

The control parameters can be defined as functions of the relative charge rl and the actual gear gangi. At the end of a retriggerable time interval TNMAXP the controller parameters are switched. This can be used to change the control response from smooth to uncomfortable to signal the driver. The second set of parameters is active for the time ITNMAXP even if B\_nmax changes meanwhile.

Subfunction LIMITS:

In case of error velocity signal the engine speed is limited to NMAXDV. With automatic transmission the limitation can be given as a function of the actual gear with the characteristic curve NMAXDVG.

In case of an error of the engine speed sensor the engine speed limit is NMAXNL (limb home function, error engine speed sensor). If B\_dknolu = 1 (limb home air position) leads to a smaller engine speed limit the MIN value is chosen.

Raised engine speed limit, valid for a limited time:

If tmot>TMOTNMX and vfzg>VNMX the engine speed limit NMAXOG is activated (initialization of the ramp with NMAXOG), otherwise NMAX is valid. The timer tnmhx\_w counts down the time when nmot\_w is higher than NMAX. If nmot\_w is lower than NMAX only for a short time tnmhx\_w is not reinitialised. If tnmhx\_w expired (TNMXH) a ramp for nmax\_w is started. The variable nmax\_w is reduced in steps of DNMAX until it reached its lower limit NMAX.

A reinitialisation of the ramp with NMAXOG and a restart of the timer tnmhx\_w is not allowed, until the engine speed is below NMAX for at least the time ITNMXH without interruption. At the time of reinitialisation the engine speed has to be below NMAX.

With double ignition (B\_dopzue) a ramp for the diminution of the engine speed limitation is activated. In steps of DNMAXDZ the engine speed is reduced to NMAXDZ.

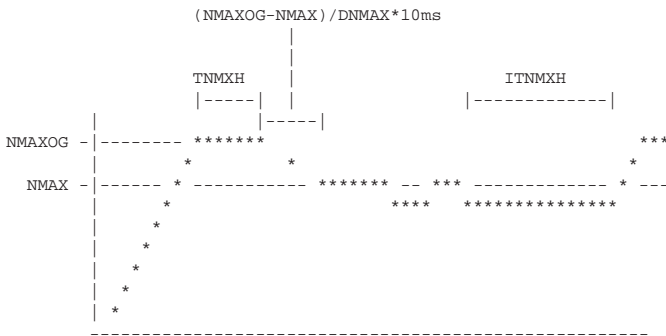
## APP NMAXMD 18.20 Application hint

The control parameters NMXPG, NMXPRLG, KINMXG, KINMXRLG and TNMXPR should be programmed so that the transient recovery time or the overshoot of the engine speed does not exceed the requested values and the system remains stable.  
For a basic application all values in the respective characteristic curve (or map) must be the same.

Typical values:

NMAX = 6500 rpm, MDIMX = 99.6%, DNMAXH = 100 rpm, NMAXDV <= NMAX  
ITNMXH = 3 \* TNMXH, DNMAX = 1 rpm,  
TMOTNMX = 80 °C, VNMX = 20 km/h (raised engine speed not allowed for stationary vehicle)

( Default values: )  
( TMOTNMX = 143.25 °C, VNMX = 318.75 km/h, NMAXOG = 5000 rpm, )  
( ITNMXH = 0 s, TNMXH = 0 s, )  
( NMAXNL = 2000 rpm )  
( NMAXDZ = 10000 U/min, DNMAXDZ = 0 U/min )

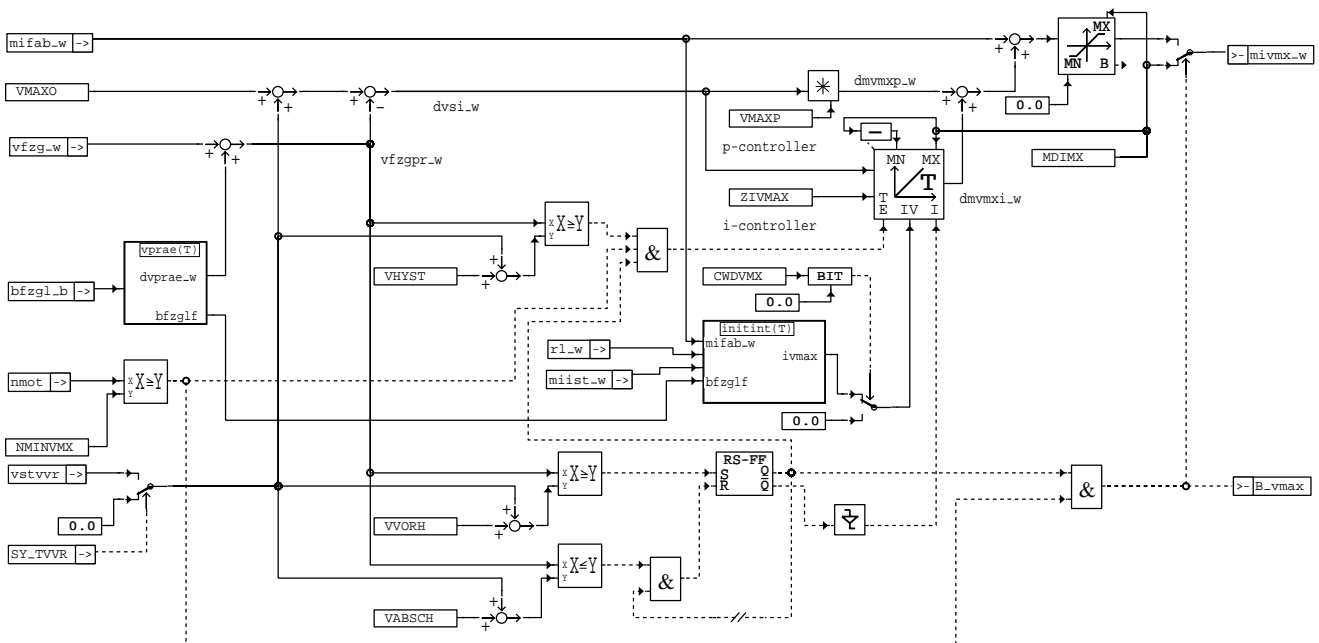


Choosing NMAXOG = NMAX deactivates the raised engine speed limit.

Attention: A high engine speed overshoot activates the hard limit DNMAXH (B\_nmaxh=1 => maximum injection suppression).  
The maximum engine speed up to B\_nmaxd=1 is: nmot\_w = NMAXOG + DNMAXH .

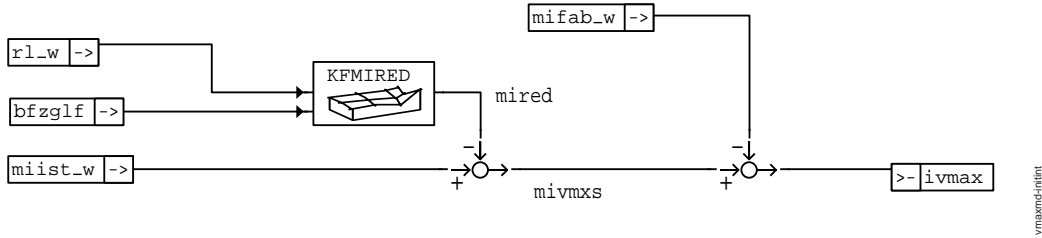
## VMAXMD 1.30 Torque request of Vmax regulation

### FDEF VMAXMD 1.30 Function definition



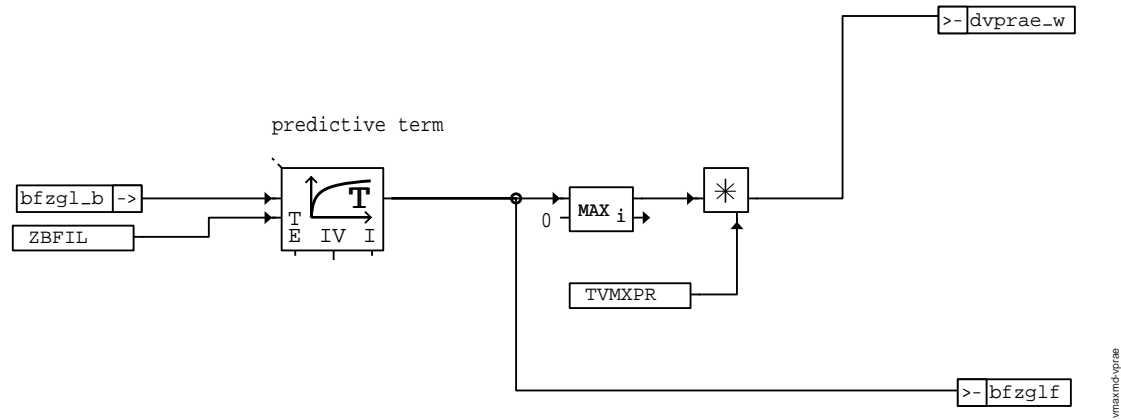
vmaxmd-vmaxmd

vmaxmd-vmaxmd



**vmaxmd-initint**

Partial function INITINT: Calculation of the initialization value for the integral action component



**vmaxmd-vprae**

Partial function VPRAE: Calculation of a predicted speed component

**ABK VMAXMD 1.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWDVMX			FW	code word SW-switch for integrator initialization during VMAX control
KFMIRED	RL_W	BFZGLF	KF	Map of decreasing torque for VMAX control
MDIMX			FW	maximum limit indicated engine torque
NMINVMX			FW	Minimum engine speed threshold for the VMAX control
TVMXPR			FW	Speed prediction horizon for VMAX control
VABSCH			FW	Vmax controller shut-down threshold, variant-coded
VHYST			FW	Vmax hysteresis threshold, variant-coded
VMAXO			FW	Vmax limiting value (line with 16 variants)
VMAXP			FW	P element for VMAX control
VVORH			FW	Vmax guide threshold, variant-coded
ZBFIL			FW	Time constant for acceleration filter
ZIVMAX			FW	I gradient for VMAX control

Variable	Source	Type	Description
BFZGLF	VMAXMD	LOK	Vehicle acceleration , filtered
BFZGL_B	GGVFZG	EIN	Automobile acceleration in the longitudinal direction
B_VMAX	VMAXMD	AUS	flag VMAX limitation active
DMVMX_I_W	VMAXMD	LOK	Torque value I-part during VMAX regulation
DMVMXP_W	VMAXMD	LOK	Torque value P-part during VMAX regulation
DVPRAE_W	VMAXMD	LOK	Predicted speed component
DVSI_W	VMAXMD	LOK	Difference between desired and predicted vehicle speed
IVMAX	VMAXMD	LOK	Initial value for integrator for Vmax regulation
MIFAB_W	MDKOG	EIN	limited desired indicated engine torque
MIIST_W	MSF	EIN	indicated real engine torque
MIRED	VMAXMD	LOK	Indicated torque reduction for VMAX regulation
MIVMXS	VMAXMD	LOK	Indicated desired torque for integrator initialisation of VMAX regulation
MIVMX_W	VMAXMD	AUS	indicated nominal torque for VMAX control
NMOT	SWADAP	EIN	engine speed
RL_W	EGFE	EIN	relative air charge (Word)
SY_TVVR	PROKON	EIN	system constant tester connection to vmax-control
VFZGPR_W	VMAXMD	LOK	Predicted vehicle speed
VFZG_W	GGVFZG	EIN	Vehicle speed
VSTVVR		EIN	Speed offset for the VMAX control



## FW VMAXMD 1.30 Fixed Values

Parameter	Value	Description
CWDVMX		code word SW-switch for integrator initialization during VMAX control
MDIMX		maximum limit indicated engine torque
NMINVMX		Minimum engine speed threshold for the VMAX control
TVMXPR		Speed prediction horizon for VMAX control
VABSCH		Vmax controller shut-down threshold, variant-coded
VHYST		Vmax hysteresis threshold, variant-coded
VMAXO		Vmax limiting value (line with 16 variants)
VMAXP		P element for VMAX control
VVORH		Vmax guide threshold, variant-coded
ZBFIL		Time constant for acceleration filter
ZIVMAX		I gradient for VMAX control

## FB VMAXMD 1.30 Detailed description of function

In order to limit the vehicle speed a PI controller with speed prediction and torque derivation is used.

The basis of this function is the vehicle speed  $v_{fzgr\_w}$ , which is predicted in the partial function TVMXPR by a prediction horizon TVMXPR (prediction only with positive vehicle acceleration). If this predicted vehicle speed exceeds the threshold VVORH, then the VMAX control becomes active. The output B\_vmax of the RS flip-flop is set to one. The initialization value IVMAX is pre-assigned into the integrator, the delta torques  $dmvmxp\_w$  and  $dmvmxi\_w$  are calculated in the controller and added to the indicated torque  $mifab\_w$ .

If the engine speed falls short of a hysteresis threshold VHYST, then the integrator is stopped. Stopping the integrator shall prevent an escalation of the controller, which may occur due to decelerating and then accelerating again.

So as to prevent the engine from stopping while the clutch is operated and the engine speed having decreased, the VMAX control is deactivated as from an engine speed threshold.

When the switch-off threshold VABSCH is undershot the controller becomes inactive, the output of the RS flip-flop B\_vmax is reset to zero.

The value of the integrator is limited between -MDIMX and MDIMX.

The calculation of the initialization value of the integrator is performed in the partial function INITINT. Dependent on the filtered vehicle acceleration  $bfzglf$  and the relative charge  $rl\_w$  a reduction torque is calculated from a characteristic map. This reduction torque contains the specific torque characteristics of the engine independent of the vehicle mass. By subtracting the reduction torque from the actual torque  $miist$  that torque is obtained, which is needed by the engine to maintain the maximum speed.

Via the interface  $vstvvr$  a minor change of the control speed is possible.

## APP VMAXMD 1.30 Application hint

Hints regarding the initial application:

The controller parameters VMAXP and ZIVMAX are to be adjusted such that the stabilization time resp. the overshoot of the vehicle speed do not exceed the requested values and that the system remains stable.

When starting the control care must be taken at first that the speed signal and the acceleration signal have smooth signal profiles. For this at first the function GGVFZG needs to be adjusted.

For the initial application the prediction horizon TVMXPR should lie at 100 ms and the filter time constant ZBFIL at 500 ms. The integrator initialization and the speed prediction shall improve the control quality with regard to the stabilization behaviour.

At high limiting speeds and small torque reserve of the engine at that speed an initialization of the integrator is not absolutely necessary.

The map KFMIREED is to be adjusted in the following way:

At first the speed VMAXO is to be reached by driving on a flat stretch of road with the controller being switched off. The actual torque  $miist$  ( $VMAXO, bfzgl=0$ ) measured in the process serves as a basis for the further application. Now the speed threshold VMAXO is exceeded at different accelerations, while the controller is still deactivated. In the process the load  $rl$  and the actual torque  $miist$  ( $VMAXO, bfzgl$ )

0) are measured. The reduction value, which corresponds to this  $rl$  and to this acceleration results with regard to

$$mired(rl, bfzgl) = miist(VMAXO, bfzgl)$$

$$0) - miist(VMAXO, bfzgl = 0)$$

For the controller adjustment the controller initialization can be switched off by means of the code word CWDVMX.

Typical application:

Example for a typical application

Version coding:

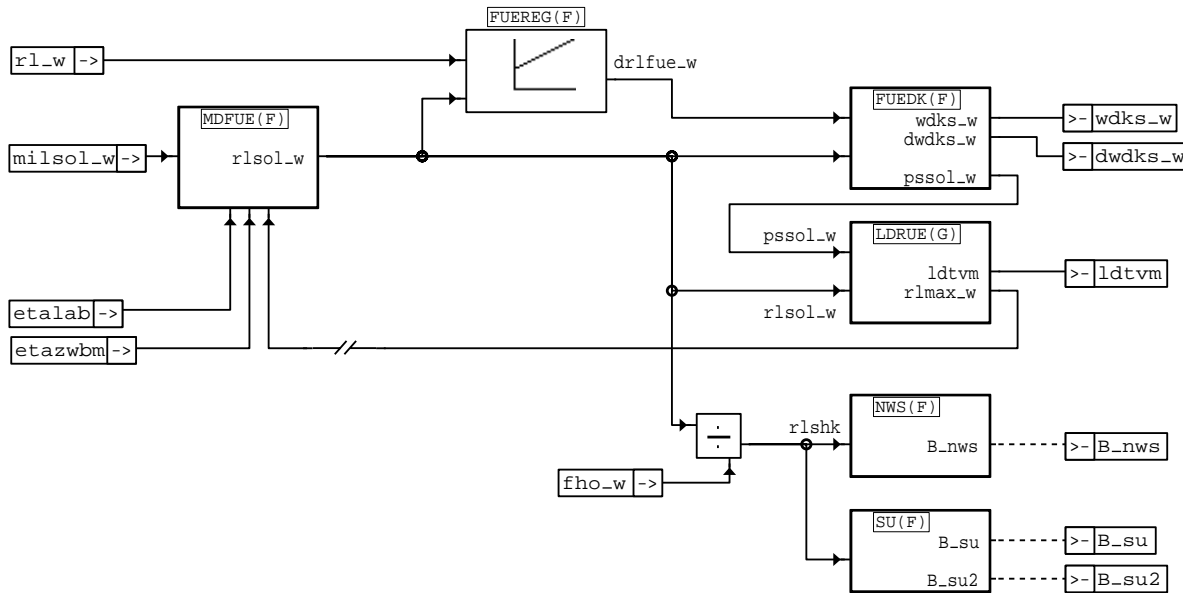
In order to obtain different vmax control speeds for different versions the following labels are activated via a version coding:

Vehicle dependency:

VMAXO
VHYST
VABSCH
VVORH
VMAXP
ZIVMAX
KFMIREED
NMINVMX

## FE 3.10 Charging interventions

### DDEF FE 3.10 Function definition



fe-fe

### ABK FE 3.10 Abbreviations

Variable	Source	Type	Description
B_NWS	FE	AUS	Condition camshaft control
B_SU	FE	AUS	condition intake manifold switch-over
B_SU2	FE	AUS	condition intake manifold switch over, 2.flap
DRLFUE_W	FE	LOK	correction offset by air mass controller
DWDKS_W	FE	AUS	modification of desired throttle angle
ETALAB	MDBAS	EIN	Lambda effectiveness without intervention w.r.t. to optimum torque at Lambda=1
ETAZWBW	MDBAS	EIN	mean ignition angle effectiveness of basic ignition angle
FHO_W	BGPU	EIN	correction factor: altitude
LDTVW	FE	AUS	Boost control duty cycle ( endvalue )
MILSOL_W	MDKOL	EIN	driver torque request for charge
PSSOL_W	FE	LOK	Set intake manifold pressure
RLMAX_W	FE	LOK	maximum attainable charge with turbo
RLSHK	FE	LOK	desired relative air charge corrected by altitude
RLSOL_W	FE	LOK	desired relative air charge
RL_W	EGFE	EIN	relative air charge (Word)
WDKS_W	FE	AUS	desired throttle angle w.r.t. to lower mechanical stop

### FW FE 3.10 Fixed Values

Parameter	Value	Description
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### FB FE 3.10 Detailed description of function

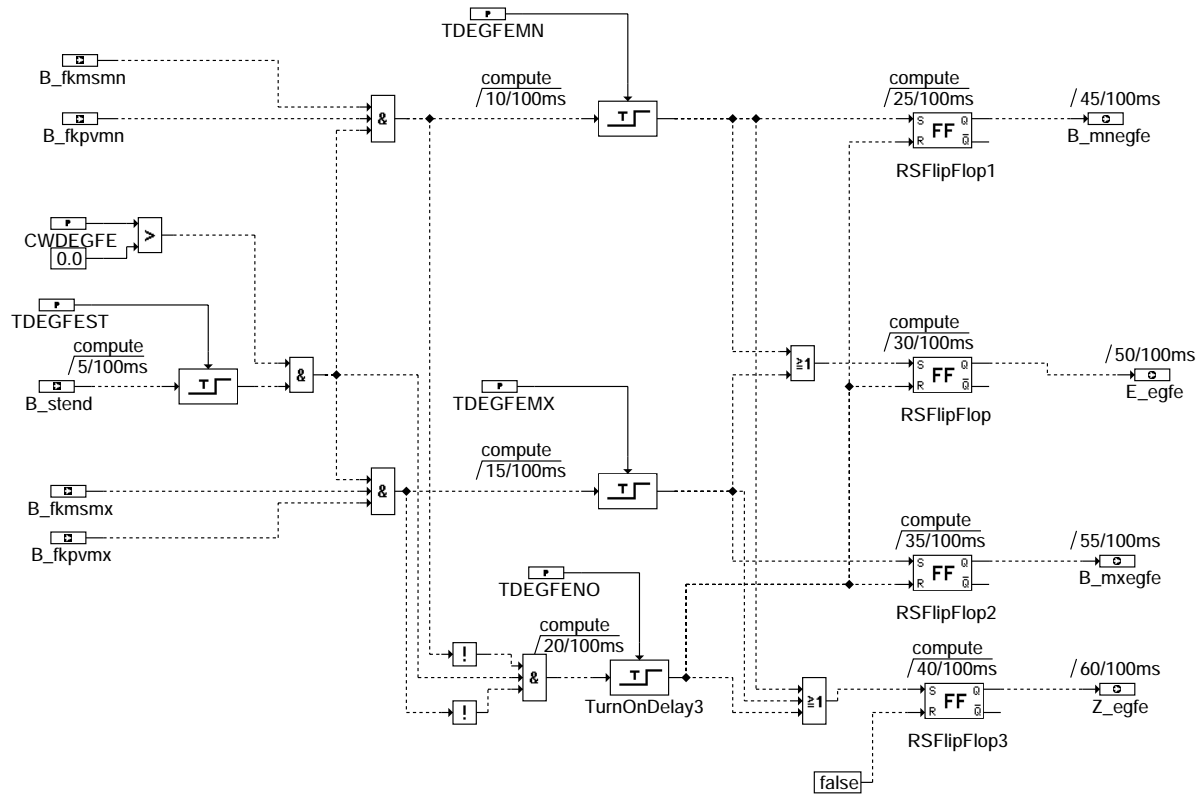
The torque `milsol_w`, which is to be set via the charge path at the basic ignition angle and effectiveness, is converted in the function `MDFEU` into the nominal charge `rlsol_w`, which belongs to the desired working point. The stationary matching between the nominal charge and actual charge `rl_w` occurs with the aid of the charge controller `FUEREG`. Both signals are used in the function `FUEDK` to calculate the corresponding values of intake manifold pressure `pssol_w` and throttle valve angle `wdks_w`.

The desired charge `rlsol_w` and desired intake manifold pressure are the guide variables for charge pressure control. Intake manifold switchover `SU` and camshaft control `NWS` use the desired air charge corrected by altitude to determine their switching points.

## APP FE 3.10 Application hint

## DEGFE 2.10 Diagnosis of input variables for charge detection

### FDEF DEGFE 2.10 Function definition

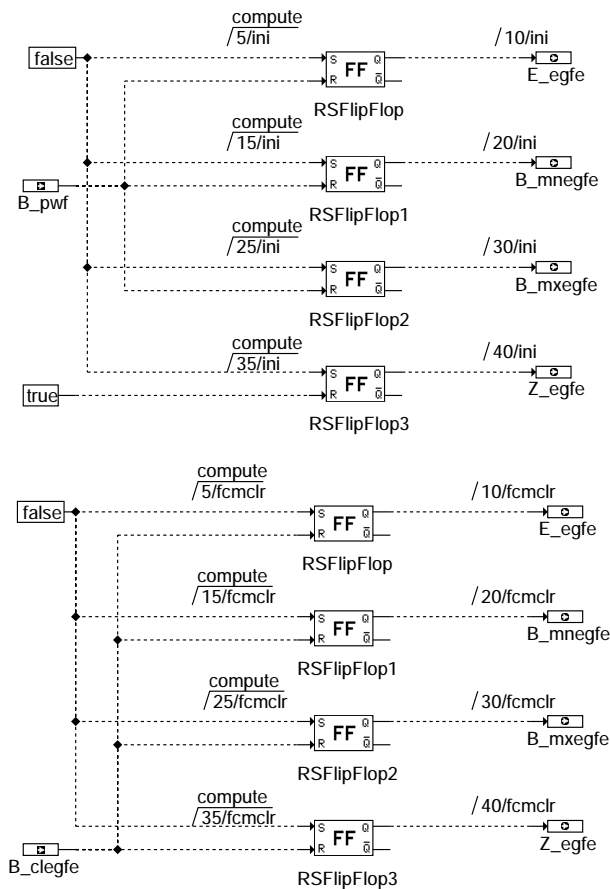


degfe-main

degfe-main



Initialization block



degfe-init

**ABK DEGFE 2.10 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWDEGFE			FW	code word for shutdown of the function %DEGFE
TDEGFEMN			FW	Time delay for setting the MIN fault
TDEGFEMX			FW	Time delay for setting the MAX fault
TDEGFENO			FW	Time delay for setting NO fault
TDEGFEST			FW	Time delay after start-up
Variable	Source		Type	Description
B_CLEGFE			EIN	condition clear fault path EGFE
B_FKMSMN	BGMSZS		EIN	Quick adaption of the mass flow fkmsdks at the lower arrester
B_FKMSMX	BGMSZS		EIN	Quick adaption of the mass flow fkmsdks at the upper arrester
B_FKPVMM	BGMSZS		EIN	Slow mass flow adaption fkpvdK at the lower arrester
B_FKPVMX	BGMSZS		EIN	Slow mass flow adaption fkpvdK at the upper arrester
B_MNEGFE	DEGFE		AUS	Condition: MIN fault input parameters charging detection
B_MXEGFE	DEGFE		AUS	Condition: MAX fault input parameters charging detection
B_PWF			EIN	Condition for powerfail
B_STEND	BBSTT		EIN	condition end of start
E_EGFE	DEGFE		AUS	Error flag: input parameters for charging detection
Z_EGFE	DEGFE		AUS	Cycle flag: Input variables for charging detection

**FW DEGFE 2.10 Fixed Values**

Parameter	Value	Description
CWDEGFE		code word for shutdown of the function %DEGFE
TDEGFEMN		Time delay for setting the MIN fault
TDEGFEMX		Time delay for setting the MAX fault
TDEGFENO		Time delay for setting NO fault
TDEGFEST		Time delay after start-up



## FB DEGFE 2.10 Detailed description of function

The function %DEGFE serves the diagnosis of the input variables for the charging detection. The fundamental concept of the function is based on an evaluation of the factors `fkmsdks_w` (rapid equalization) and `fkpvdks_w` (slower equalization) from the function %BGMSZS.

The error bit `E_degfe` is then set if the integrators of the massflow equalization in der %BGMSZS have run either in their lower limits, i.e. the bits `B_fkmsmn` & `B_fkpvmn` are TRUE, or if the integrators of the massflow equalization in the %BGMSZS have run in their upper limits, i.e. the bits `B_fkmsmx` & `B_fkpvmx` are set.

A shutdown of the function is possible by the code word `CWDEGFE`. The code word must be assigned the value of 0 for this. `CWDEGFE` shall be assigned the value of 1 if the function is to be activated.

## APP DEGFE 2.10 Application hint

Prerequisite for putting the function into operation is the correct application of the charging detection.

Particular attention shall be paid to assignment of the correct data for the following labels in the %BGMSZS:

- `FKMSDKMX`, `FKMSDKMN`, `FKPVDKMX`, `FKPVDKMN`, `MSALLMX`, `MSALLMN`, `MSLG`, `ZKMSDK` and `ZKPVDK`

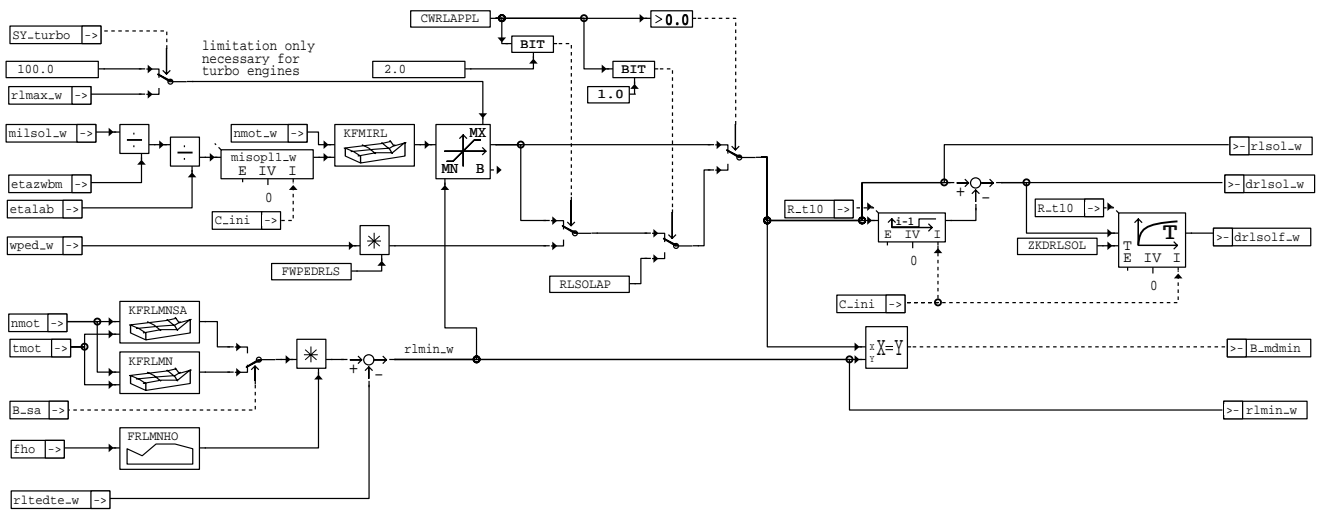
(Refer to the application in the %BGMSZS for proposed values)

Guiding values for the first application:

TDEGFEMN	2 sec.
TDEGFEMX	2 sec.
TDEGFENO	2 sec.

## MDFUE 8.50 Nominal-value input from nominal torque for airmass

### DDEF MDFUE 8.50 Function definition



mdfue-mdfue

### ABK MDFUE 8.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWRLAPPL			FW	codeword rlsol_w from Test-bench for Applikation
FRLMNH0	FHO		KL	correction factor rlm_min depending on altitude
FWPEDRLS			FW	factor to generate rlsol (application use only)
KFMIRL	NMOT_W	MISOPL1_W	KF	map for calculation of nominal charge
KFRLMN	NMOT	TMOT	KF	Minimum charge during fuel on
KFRLMNSA	NMOT	TMOT	KF	Minimum r_l during fuel cut off
RLSOLAP			FW	desired relative air charge (application mode)
ZKDRLSOL			FW	time constant for drlsol-integrator

Variable	Source	Type	Description
B_MDMIN	MDFUE	AUS	Condition minimal possible indicated torque reached
B_SA	MDRED	EIN	Condition fuel cut-off
C_INI	SWADAP	EIN	ECU-condition for intialisation
DRLSOLF_W	MDFUE	AUS	filtered change of desired charge
DRLSOL_W	MDFUE	AUS	change of nominal charge
ETALAB	MDBAS	EIN	Lambda effectiveness without intervention w.r.t. to optimum torque at Lambda=1
ETAZWBW	MDBAS	EIN	mean ignition angle effectiveness of basic ignition angle
FHO	BGPU	EIN	Correction factor altitude
MILSOL_W	MDKOL	EIN	driver torque request for charge
MISOPL1_W	MDFUE	LOK	nominal air torque, recalculated for Lambda=1 and zwopt
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
RLMAX_W		EIN	maximum attainable charge with turbo
RLMIN_W	MDFUE	AUS	minimum permissible r_l
RLSOL_W	MDFUE	AUS	desired relative air charge
RLTEDTE_W	DTEV	EIN	from DTEV calculated relative charge through the purge control valve



Variable	Source	Type	Description
R_T10		EIN	Time schedule 10 ms
SY_TURBO	PROKON	EIN	system constant for turbocharged engine
TMOT	SWADAP	EIN	Engine temperature
WPED_W	SWADAP	EIN	normed angle acceleration pedal

### FW MDFUE 8.50 Fixed Values

Parameter	Value	Description
CWRLAPPL		codeword rlsol_w from Test-bench for Applikation
FWPEDRLS		factor to generate rlsol (application use only)
RLSOLAP		desired relative air charge (application mode)
ZKDRLSOL		time constant for drlsol-integrator

### FB MDFUE 8.50 Detailed description of function

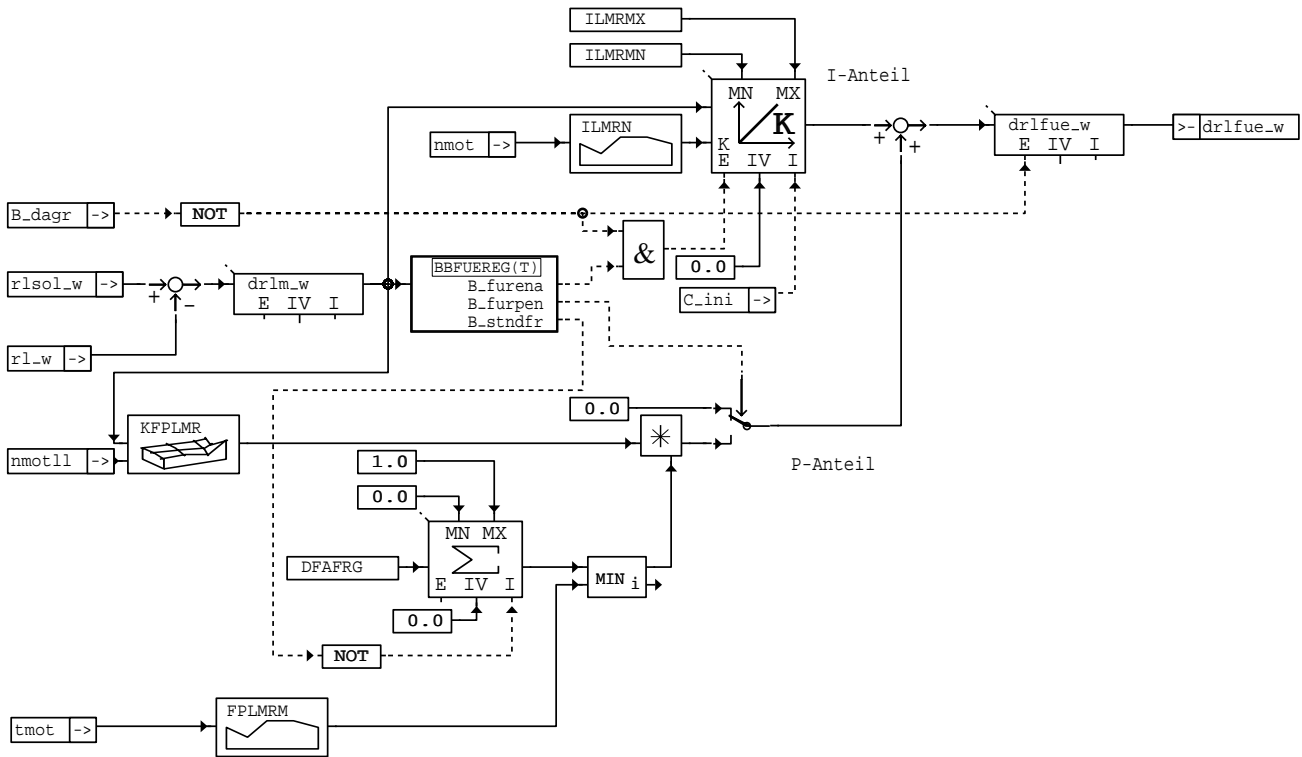
The torque  $milsol_w$ , which is to be set via the charge path at the basic ignition angle and effectiveness, is converted into the torque  $misopl1_w$ , which corresponds to the optimum torque at  $\lambda=1$ . With the aid of the map  $KFMIRL$  the charge belonging to this operating point is calculated. This charge is limited to the minimum permissible value  $rlmin_w$ . If this limit is reached the Condition  $B\_mdnm$  stops the integral part of the idle speed controller (cf.  $LLRRM$ ). In the case of a turbocharger, the charge is limited to the maximum permissible charge  $rlmax_w$ . The result is the nominal charge  $rlsol_w$ .

### APP MDFUE 8.50 Application hint

The map  $KFMIRL$  is inverse to the map  $KFMIOF$  in the section  $\%MDBAS$ . Application hint, see  $\%MDBAS$ .

## FUEREK 4.30 Charge controller

### FDEF FUEREK 4.30 Function definition

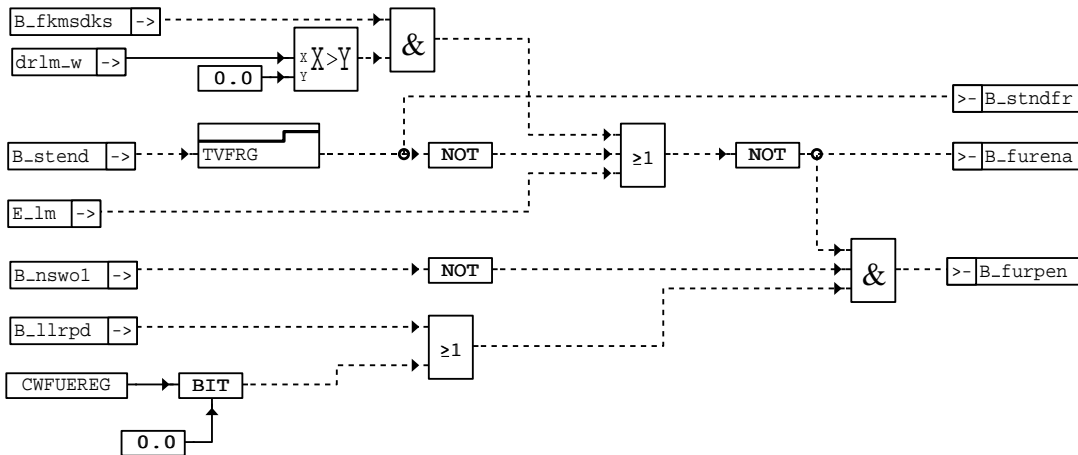


fuereg-fuereg

fuereg-fuereg



Operating range of the charge controller



fuereg-bbfuereg

fuereg-bbfuereg

**ABK FUEREK 4.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWFUEREG			FW	Code word charge controller active outside of idle
DFAFRG			FW	Increasing control factor after the charge controller was activated
FPLMRM	TMOT		KL	weighting factor for P component of air-mass controller
ILMRMN			FW	minimum value of air mass controller
ILMRMX			FW	maximum value of air mass controller
ILMRN	NMOT		KL	integrator gain of air mass controller
KFPLMR	DRLM_W	NMOTLL	KF	P-component of air mass controller
TVFRG			FW	Delay time after end of start until charge controller is enabled

Variable	Source	Type	Description
B_DAGR		EIN	Condition EGR diagnostic routine
B_FKMSDKS	FUEDK	EIN	stop for integration of fkmsdk
B_FURENA	FUEREK	LOK	condition activation of charge controller
B_FURPEN	FUEREK	LOK	condition charge controller P component active
B_LLRPD	LLRBB	EIN	Condition activation of PD-part of idle speed control
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_STEND	BBSTT	EIN	condition end of start
B_STNDFR	FUEREK	LOK	enabling of charge controller after start
C_INI	SWADAP	EIN	ECU-condition for intialisation
DRLFUE_W	FUEREK	AUS	correction offset by air mass controller
DRLM_W	FUEREK	LOK	nominal / actual value difference of air mass controller
E_LM	EGFE	EIN	Error flag: main load sensor
NMOT	SWADAP	EIN	engine speed
NMOTLL	BGNMOT	EIN	engine speed
RLSOL_W	MDFUE	EIN	desired relative air charge
RL_W	EGFE	EIN	relative air charge (Word)
TMOT	SWADAP	EIN	Engine temperature

**FW FUEREK 4.30 Fixed Values**

Parameter	Value	Description
CWFUEREG		Code word charge controller active outside of idle
DFAFRG		Increasing control factor after the charge controller was activated
ILMRMN		minimum value of air mass controller
ILMRMX		maximum value of air mass controller
TVFRG		Delay time after end of start until charge controller is enabled

**FB FUEREK 4.30 Detailed description of function**

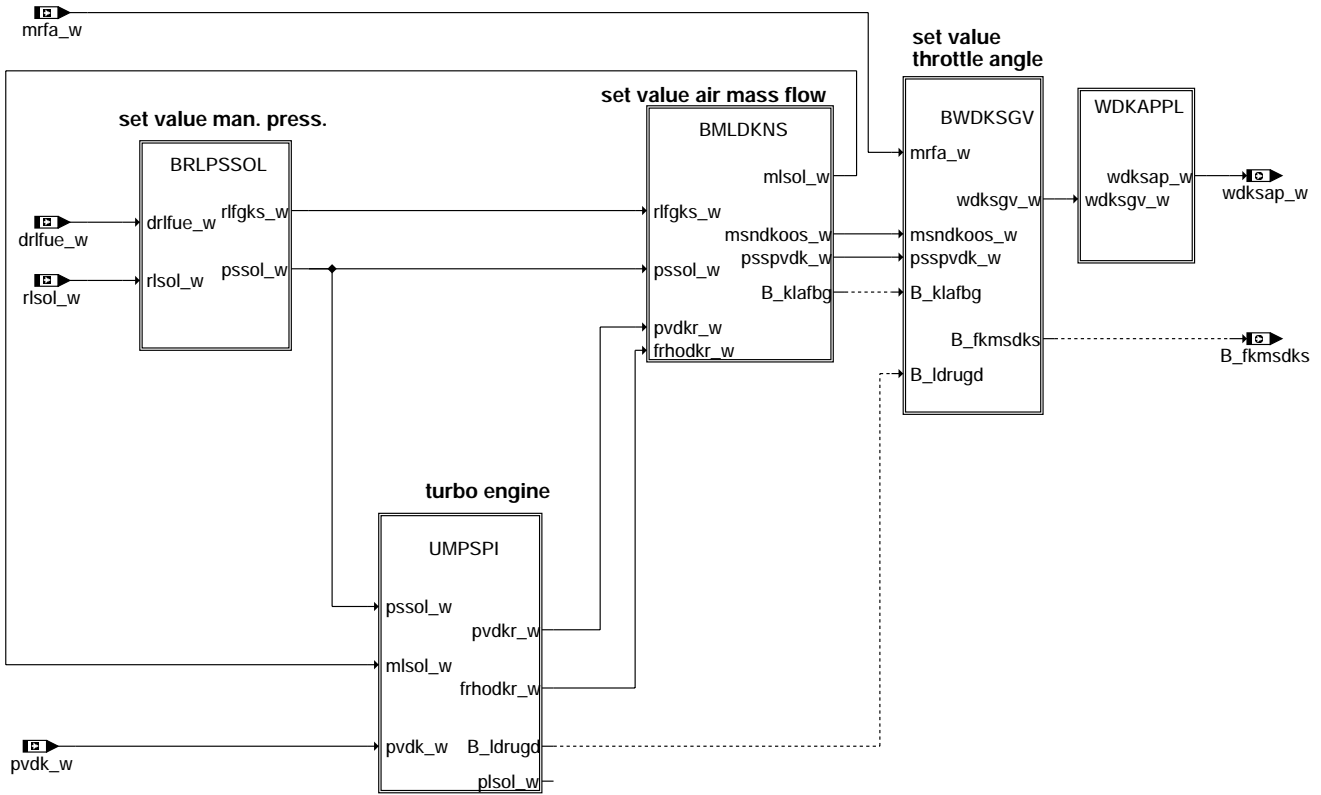
The charge controller takes care of stationary matching of the actual charge *rl\_w* to the nominal charge *rlsol\_w*. The parameters of the P and I components are RPM-dependent. The controller is activated by the condition *B\_furena* (-> sub function *BBFUEREK*), if the engine is not running in unthrottled mode, and no cranking and no fault in the calculation of the air mass is present.

APP FUEREG 4.30 Application hint

## FUEDK 21.30 Charge control (calculation of nominal throttle-valve angle)

FDEF FUEDK 21.30 Function definition

%FUEDK 21.20: Overview



fuedk-fuedk

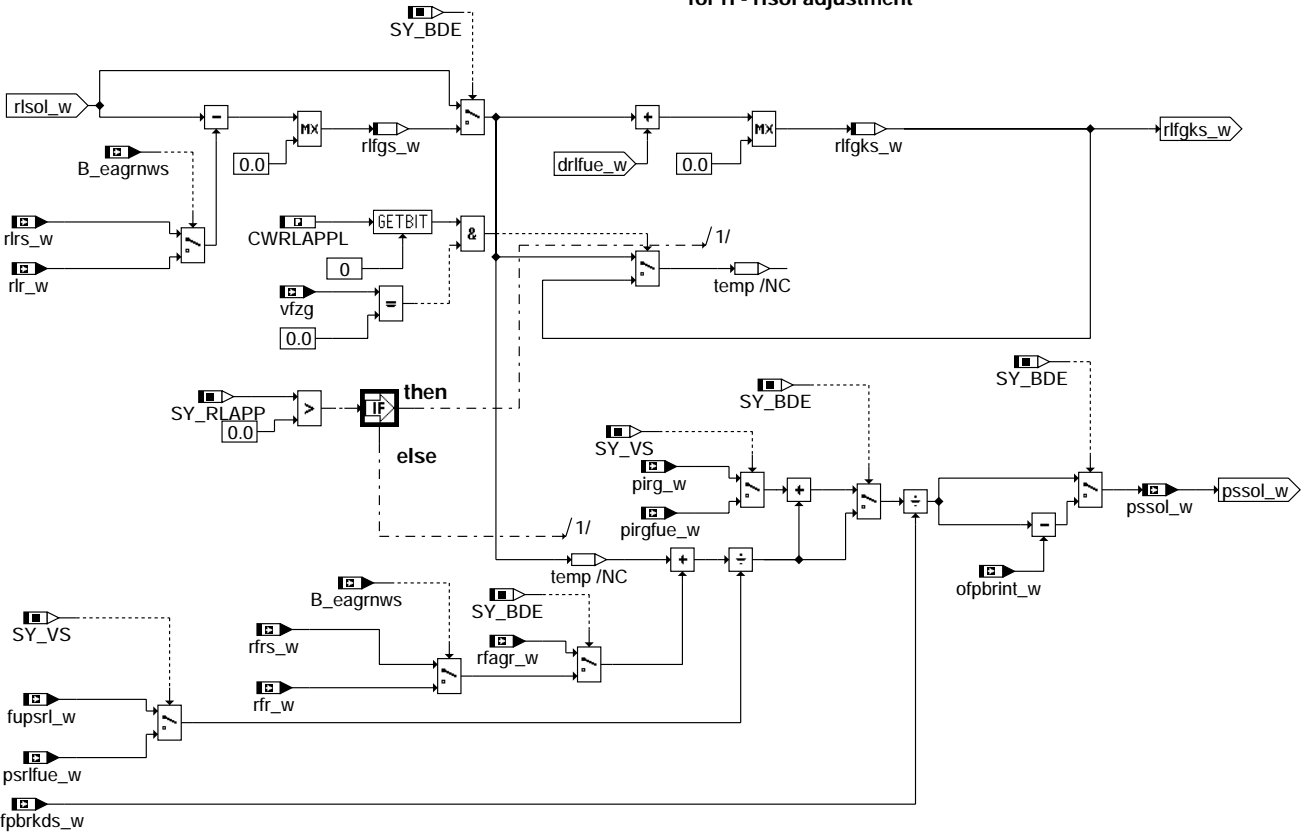
fuedk-fuedk



**BDE**  
**BRLPSSOL: Set value manifold pressure**

**CWRLAPPL Bit0 = true & SY\_RLAPP > 0**

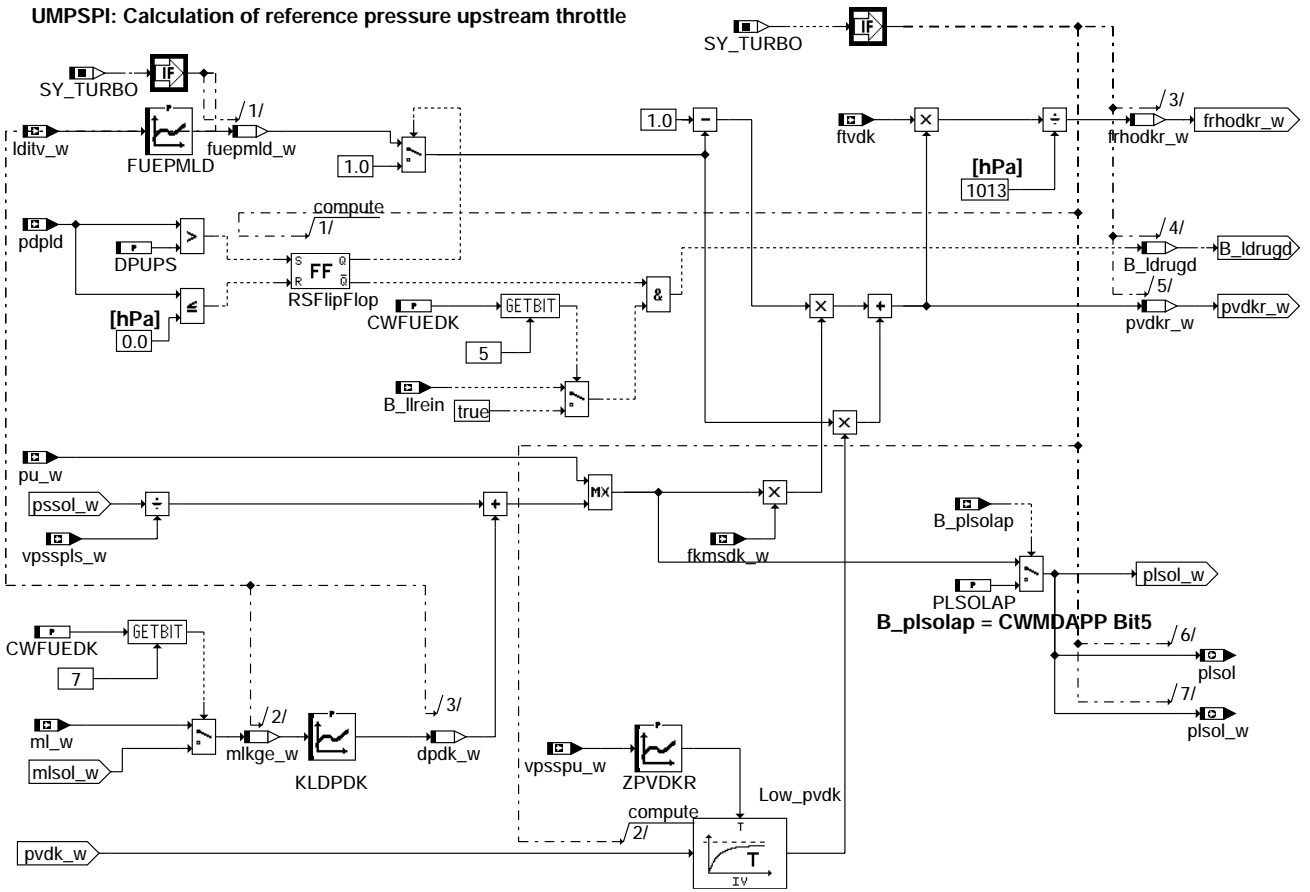
**only used for application at test bench  
for rl - risol adjustment**



fuedk-brlpsol

fuedk-brlpsol

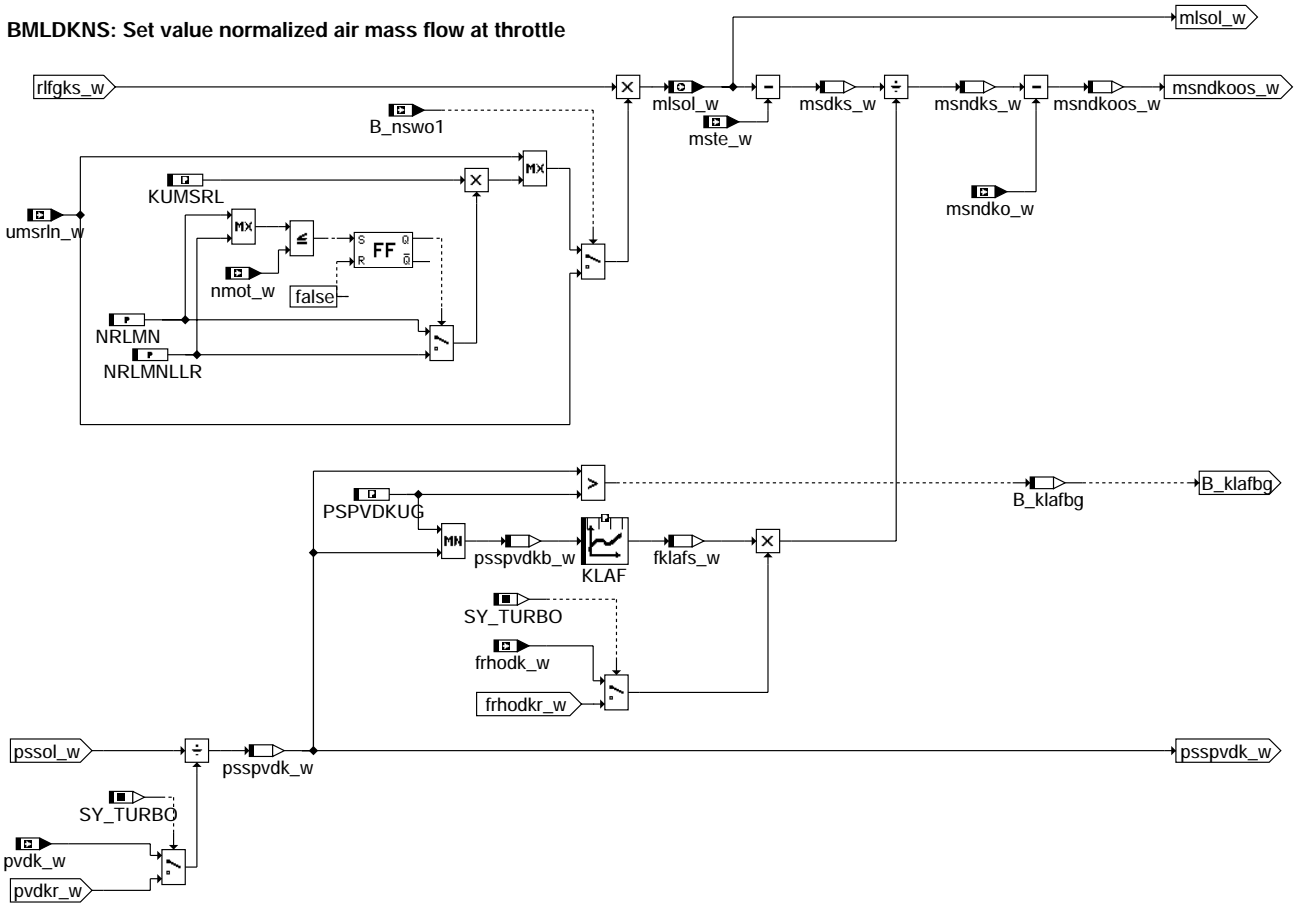
### UMPSPi: Calculation of reference pressure upstream throttle



fuedk-umpspi

fuedk-umpspi

### BMLDKNS: Set value normalized air mass flow at throttle



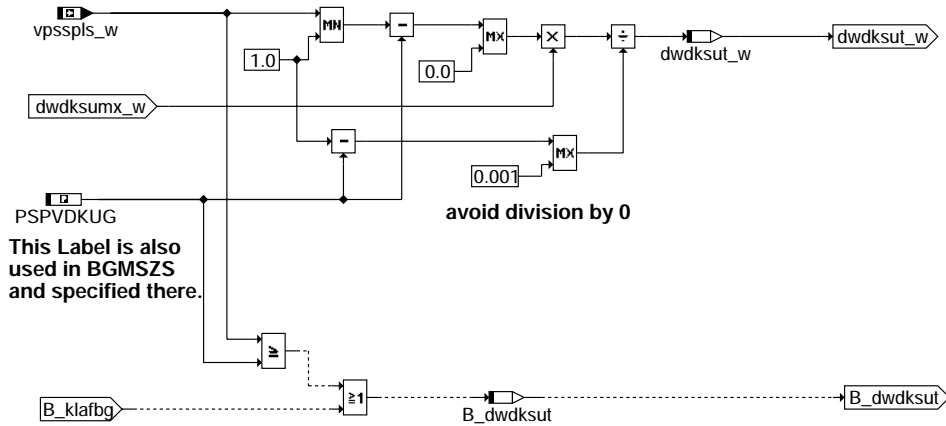
fuedk-bmlDKNS

fuedk-bmlDKNS



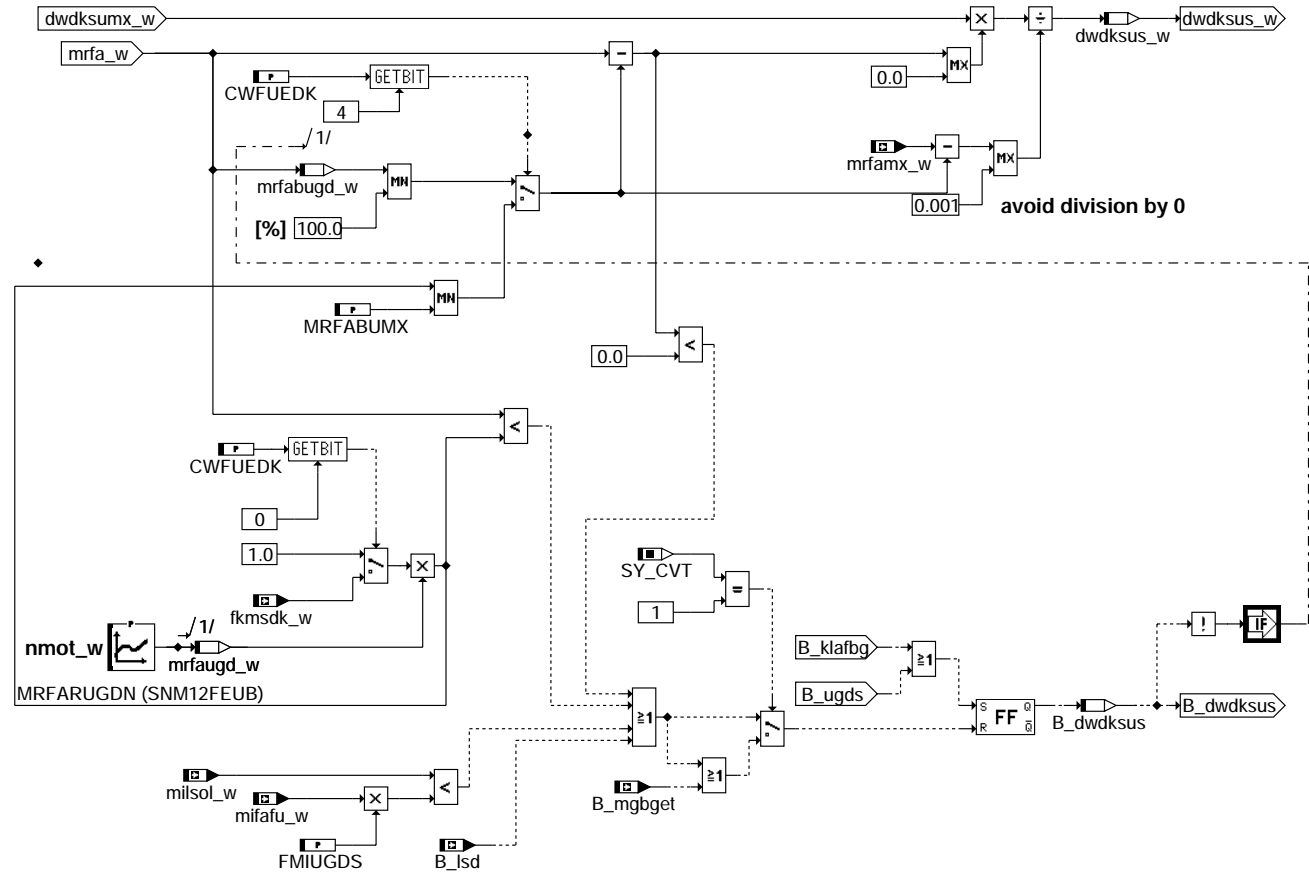


**WDKSUGDT: difference of desired throttle angle referred to 95% charge at Turbo engine**

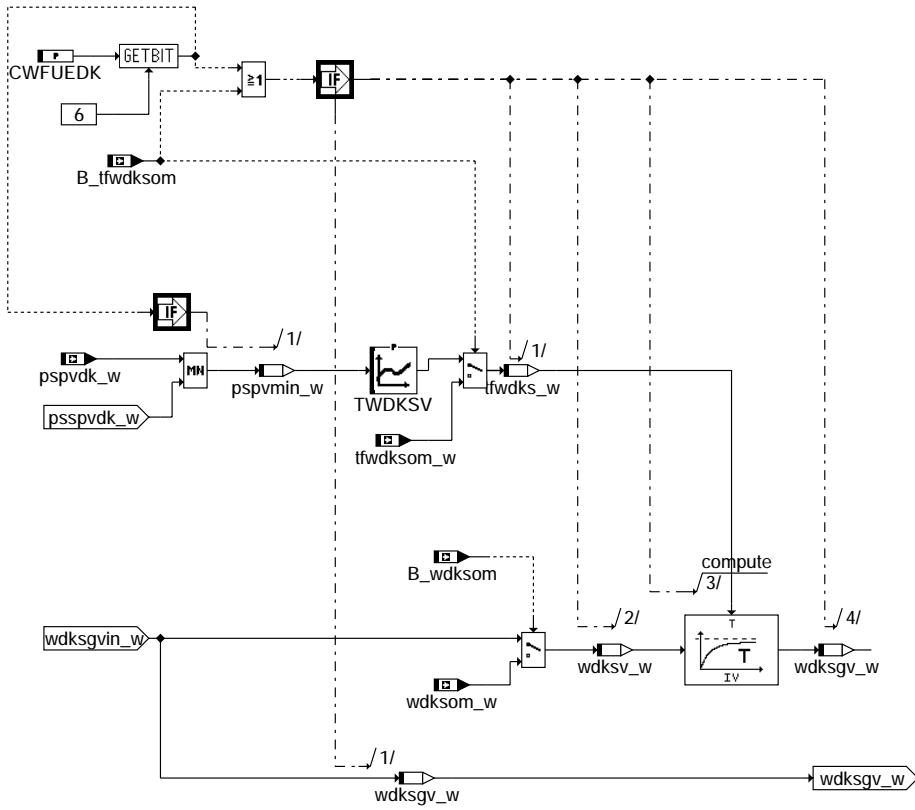


fuedk-wdksugdt

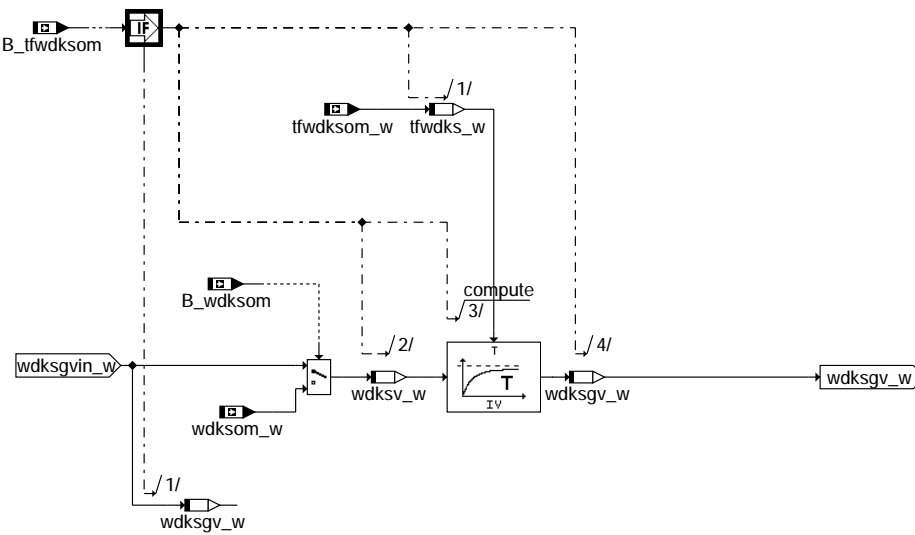
**WDKSUGDS: difference of desired throttle angle referred to 95% charge at induction engine**



fuedk-wdksugds



fuedk-wdksgv

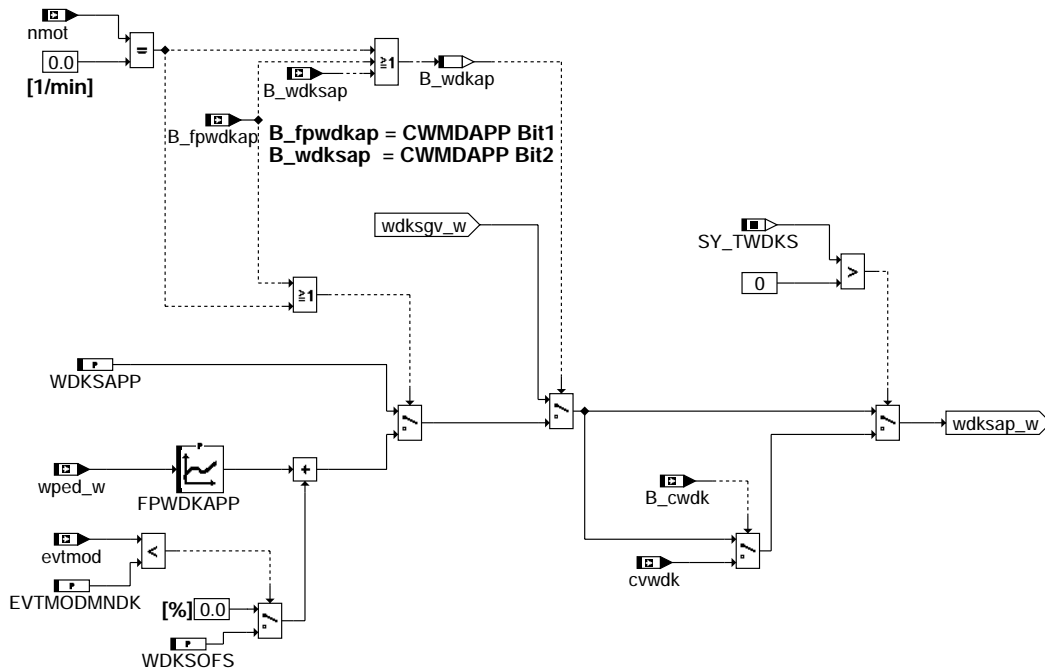


fuedk-bde-wdksgv

fuedk-wdksgv

fuedk-bde-wdksgv

### WDKAPPL: Calibration interface



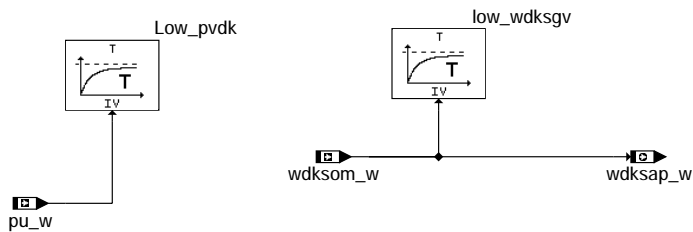
fuedk-wdkappl

### NACHLAUF: calculation of desired throttle angle at SKI15 = off



fuedk-nachlauf

### INIT: Initialisation of function



fuedk-init

### ABK FUEDK 21.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWFUEDK			FW	codeword FUEDK
CWRLAPPL			FW (REF)	codeword rlsol_w from Test-bench for Applikation
DPUPS			FW	delta pressure threshold for switching of reference pressure upstreams throttle
DRLSOLMF			FW	threshold delta rlsol for Medianfilter
EVTMODMNDK			FW	min. temperature of offset-addition to DK-map (if nmot=0)
FMIUGDS			FW	factor correction maximum torque at full load
FPWDKAPP	WPED_W		KL	throttle angle dependent on accelerator pedal position, only for calibration
FUEPMLD	LDITV_W		KL	Factor for gliding transition average pressure (reference pressure turbo)
KFWDKMSN	MLWDKNF_W	NMOT_W	KF	Map for the desired throttle blade angle
KFWDKSMX	NMOT_W	FHO_W	KF	max. desired throttle angle
KLAF	PSSPVDKB_W		KL (REF)	characteristic of Saint-Venant
KLDPDK	MLKGE_W		KL	pressure drop at throttle blade
KUMSRL			FW (REF)	conversion constant from mass flow to relative air charge



Parameter	Source-X	Source-Y	Type	Description
MRFABUMX			FW	Max. threshold of drivers demand for linear calculation of pedal value at WOT
MRFARUGDN	NMOT_W		KL	Reset threshold for linear pedal travel in the non-reduced DK range
NRLMNM			FW	lowest engine speed for calculation of umsrln
NRLMNLRL			FW	lowest engine speed for calculation of umsrln at idle speed
PLSOLAP			FW	calibration value for reference boost pressure
PSPVDKUG			FW (REF)	Ratio pspvdk not reduced
SNM12FEUB	NMOT_W		SV (REF)	set points of WDKSMX, WDKUGDN
SY_BDE			SYS (REF)	system constant GDI
SY_CVT			SYS (REF)	system constant: CVT transmission exists
SY_RLAPP			SYS (REF)	rlsol control during application possible
SY_TURBO			SYS (REF)	system constant for exhaust-gas turbocharger
SY_TWDKS			SYS (REF)	system constant: input of desired angle DVE via tester is possible
SY_VS			SYS (REF)	system constant valve stroke control: no, 2 position
TWDKSV	PSPVMIN_W		KL	time constant for filtering of reference throttle blade position
WDKSAPP			FW	throttle angle for calibration tasks
WDKSOF5			FW	Offset added to appl. value of desired throttle position at low temperature
ZPVDKR	VPSSPU_W		KL	time constant for filtering of pvdkr

Variable	Source	Type	Description
B_CWDK		EIN	device control DCPIDCM
B_DWDKSUS	FUEDK	LOK	difference of desired throttle angle refered at 95% to 100% charge active
B_DWDKSUT	FUEDK	LOK	difference of desired throttle angle refered at 95% to 100% charge active
B_EAGRNWS		EIN	Condition: Error EGR or camshaftcontrol ->use of actual value of EGR-control
B_FKMSDKS	FUEDK	AUS	stop for integration of fkmsdk
B_FPWDKAP	PROKON	EIN	throttle-valve control by accelerator pedal
B_KLAFBG	FUEDK	LOK	input value of KLAF limited
B_LDRUGD	FUEDK	LOK	Condition unthrottled, Eneable from LDR
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_LSD	MDFAW	EIN	condition: limitation of positive torque gradient active
B_MFACT	FUEDK	LOK	condition medianfilter activ
B_MGBGET		EIN	Condition torque gradient limitation active
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_PLSOLAP		EIN	condition: calibration of referece boost pressure
B_TFWDKSOM	WDKSOM	EIN	time constant to filter desired throttle angle without torque structure active
B_JGDS	FUEDK	LOK	set value throttle angle near full load
B_WDKAP	FUEDK	LOK	Condition: desired throttle position from appl. characteristic line or at start
B_WDKSAP	PROKON	EIN	throttle-blade contol by fixed value, bit 1 has priority
B_WDKSOM	WDKSOM	EIN	desired throttle angle without torque structure active
CVWDK		EIN	device control value DCPIDCM
DPDK_W	FUEDK	LOK	pressure drop at throttle blade
DRLFUE_W	FUEREG	EIN	correction offset by air mass controller
DRLSOLMF_W	FUEDK	LOK	delta desired relative air charge for medianfilter
DWDKSUMX_W	FUEDK	LOK	difference of desired throttle angle between 95% and 100% charge
DWDKSUS_W	FUEDK	LOK	difference of desired throttle angle refered to 95% charge induction engine
DWDKSUT_W	FUEDK	LOK	difference of desired throttle angle refered to 95% charge at turbo engine
EVTMOD	BGTEMPK	EIN	modelled temperature at inlet valve
FHO_W	BGPU	EIN	correction factor: altitude
FKLAFS_W	FUEDK	LOK	Factor saint venant (KLAF) for calculation of wdks
FKMSDK_W	BGMSZS	EIN	correction factor for mass-flow substitute load signal
FPBRKDS_W	BGSRM	EIN	factor for determination of combustion chamber pressure
FRHODKR_W	FUEDK	LOK	factor correction air density for throttle blade correction
FRHODK_W	EGFE	EIN	factor correction air density for throttle valve flow f(intake air temp.,altit.)
FTVDK	SWADAP	EIN	correction factor for temperature upstream of throttle valve
FUEPMLD_W	FUEDK	LOK	factor for gliding transition average pressure (reference pressure) turbo
FUPSRL_W	EGFE	EIN	factor system related transformation pressure to load (16-Bit)
LDITV_W		EIN	I-quota (on/off ratio) for boost control
MIFAFU_W	MDKOL	EIN	driver torque request for charge
MILSOL_W	MDKOL	EIN	driver torque request for charge
MLKGE_W	FUEDK	LOK	Input of characteristic line KLDPPDK
MLSOL_W	FUEDK	AUS	set air mass flow
MLWDKNF_W	FUEDK	LOK	filtered normed air mass flow for desired value of throttle blade
ML_W	EGFE	EIN	air mass flow filtered (Word)
MRFABUGD_W	FUEDK	LOK	relative driver request torque at beginn of 95% air charge
MRFAMX_W	MDFAW	EIN	Relative torque request by driver maximum value
MRF AUGD_W	FUEDK	LOK	rel. driver request torque for linear moving acceleration pedal at WOT
MRFA_W	MDFAW	EIN	relative driver request torque from cruise control and pedal, =0 in limp-home
MSDKS_W	FUEDK	LOK	set air mass flow through throttling valve
MSNDKOOS_W	FUEDK	LOK	normed air mass flow for desired value of throttle blade
MSNDKO_W	EGFE	EIN	norm leakage air mass flow through throttle blade
MSNDKS_W	FUEDK	LOK	normed set air mass flow through throttling valve
MSTE_W	BGTEV	EIN	mass flow purge control into the manifold
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
OFPBINT_W		EIN	Offset correction of pbrintuk_w HFM/DSS adaptation
PDPLD		EIN	predicted delta pressure (overswing pressure)
PIRGFUE_W		EIN	Partial pressure of residual gas in internal AGR (for FUEDK)
PIRG_W	EGFE	EIN	partial pressure residual exhaust gas internal EGR (16-Bit)
PLSOL	FUEDK	AUS	Reference boost pressure
PLSOL_W	FUEDK	AUS	Reference boost pressure
PSPVDK_W	EGFE	EIN	quotient: int.manif.pressure divided by pressure upstream of throttle valve
PSPVMIN_W	FUEDK	LOK	selection (minimum) from pspvdk and pspvdk



Variable	Source	Type	Description
PSRLFUE_W		EIN	Conversion pressure into filling (for FUEDK)
PSSOL_W	FUEDK	AUS	Set intake manifold pressure
PSSPVDKB_W	FUEDK	LOK	ratio of set manifold pressure and pressure upstreams throttle limited
PSSPVDK_W	FUEDK	LOK	ratio of set manifold pressure and pressure upstreams throttle
PU_W	BGPU	EIN	Ambient pressure
PVDKR_W	FUEDK	LOK	reference pressure upstreams throttle
PVDK_W	EGFE	EIN	pressure upstream of throttle valve, 16-bit
RFAGR_W	BGSRM	EIN	relative load by external exhaust gas reduction
RFRS_W		EIN	desired relative charge (residual gas + air) caused by int. and ext. EGR
RFR_W		EIN	Relative filling (inert gas + air) via internal and external EGR
RLFGKS_W	FUEDK	LOK	Corrected rel. desired air charge (air from throttle and EEC)
RLFGS_W	FUEDK	LOK	rel. desired air charge (air from throttle and EEC)
RLRS_W		EIN	desired relative air charge caused by int. and ext. EGR
RLR_W		EIN	relative air-load over int. and ext. EGR
RLSOL_W	MDFUE	EIN	desired relative air charge
TFWDKSOM_W	WDKSOM	EIN	time constant to filter desired throttle angle without torque structure
TFWDKS_W	FUEDK	LOK	time constant of wdk filtering
UMSRLN_W	BGMSZS	EIN	calculation factor load to mass flow
VFZG	SWADAP	EIN	vehicle speed (km/h)
VPSSPLS_W		EIN	ratio of set manifold pressure and boost pressure
VPSSPU_W		EIN	Desired pressure ratio ambient/intake manifold
WDKSAP_W	FUEDK	AUS	desired throttle position from application value
WDKSGV_W	FUEDK	LOK	desired throttle blade before application interface( filtered)
WDKSMX_W	FUEDK	LOK	max. desired throttle angle
WDKSOM_W	WDKSOM	EIN	desired throttle angle without torque structure
WDKSV_W	FUEDK	LOK	desired throttle angle before application interface (unfiltered)
WDKUGD_W	BGMSZS	EIN	Throttle valve angle during which 95% charge is reached
WPED_W	SWADAP	EIN	normed angle acceleration pedal

### FW FUEDK 21.30 Fixed Values

Parameter	Value	Description
CWFUEDK		codeword FUEDK
DPUPS		delta pressure threshold for switching of reference pressure upstreams throttle
DRLSOLMF		threshold delta rlsol for Medianfilter
EVTMODMNDK		min. temperature of offset-addition to DK-map (if nmot=0)
FMIUGDS		factor correction maximum torque at full load
MRFABUMX		Max. threshold of drivers demand for linear calculation of pedal value at WOT
NRLMN		lowest engine speed for calculation of umsrln
NRLMNLRL		lowest engine speed for calculation of umsrln at idle speed
PLSOLAP		calibration value for reference boost pressure
WDKSAPP		throttle angle for calibration tasks
WDKSOFS		Offset added to appl. value of desired throttle position at low temperature

### FB FUEDK 21.30 Detailed description of function

Task of the function is the calculation of the desired throttle valve angle either for a turbo or for an aspirated engine with intake manifold or direct injection (BDE). The control is performed via the system constant SY\_TURBO and SY\_BDE. Main input values are the relative desired charge and the correction requested by the charge controller. Various other signals such as correction factors for pressure and temperature or informations about canister purging and exhaust gas recirculation are taken from the manifold model of the charge sensing or from the predetermined desired values for AGR (in the case of BDE). For this reason, there is a close connection between the calculation of the throttle valve setpoint and the charge sensing.

Sub function BRLPSSOL: Calculation of the desired manifold pressure (pssol\_w) and cor. desired fresh air charge via DK (rlfgks\_w)

For BDE, the relative desired charge rlsol\_w is reduced by the relative air charge of the external and internal AGR. Since for engines with intake manifold injection no air is contained in the internal or external AGR, the relative AGR-air charge =0 and is thus not considered.

Via the portion drlfue out of the function FUEREG (charge controller), actual charge rl\_w and desired charge rlsol\_w are adjusted. The variable rlfks\_w constitutes the fresh air portion flowing via the throttle valve or the canister purging system to the engine. The calculation of the desired manifold pressure for BDE includes the desired fresh air charge via throttle valve and canister purging system and the total charge (air and inert gas) divided by the residual gas of the internal and external AGR. With the conversion factor fupsrl\_w, the manifold pressure related to the total filling is calculated. In the case of engines with intake manifold injection, the relative desired charge rlsol\_w is increased by the relative charge for external AGR (rfagr\_w). Via the conversion factor fupsrl\_w, the manifold pressure belonging to this total charge is calculated. By means of a correction with the internal AGR-partial pressure pigr\_w, the desired manifold pressure pssol\_w is obtained.

Sub function UMSPI: Calculation of the desired reference pressure upstream the throttle valve for turbo engines (pvdkr\_w):

Turbo engine:

Desired reference pressure, see description below  
Factor air density correction frhodkr\_w = ftdvk \* pvdkr\_w / 1013 hPa

The desired reference pressure for the pressure upstream the throttle valve pvdkr\_w is formed for the turbo from the maximum selection of ambient pressure pu\_w and the desired boost pressure plsol\_w or the actual pressure upstr. the throttle valve pvdk\_w. The desired pressure results from pssol\_w/vpsspls\_w, where vpsspls\_w is the pressure ratio requested by the boost pressure control. As from vpsspls\_w > 0.95, the throttle valve is controlled linearly so as to minimize the pressure drop at the throttle valve at active boost pressure control (see sub function WDKGSUGT). Via the air mass dependent characteristic KLDPPDK, the pressure drop at the throttle valve is taken into account. The result is a higher value for the desired boost pressure which is changed to the actual boost pressure in the lambda control. Via the characteristic FUEPMLD, it is possible to change ramp-like from the actual pressure to the desired pressure. If the predicted boost pressure difference pdpld exceeds the threshold DPUPS, then



a switch-over to the actual pressure `pvdk,w` is performed, since here an overcharge fault exists (`Bldrugd = false`). The actual boost pressure is filtered by the TP filter during the transition from pu to basic boost pressure, since pressure pulsations can be triggered in this range due to a wastegate that does not close tightly.

Sub function BMLDKNS: Calculation of the standardized desired air mass flow through the throttle valve (`mlwdknsw`)

The desired air mass flow `mlsolw` is calculated by a multiplication of the cor. desired charge `rlfgksw` with `umsrln,w`. Since the charge of the engine is taken from the intake manifold at the beginning of start, at first it would not be necessary to open the throttle valve (`umsrln,w = KUMSRL*nmot = 0`). Via the threshold `KUMSRL*NRLMN`, a minimum amount of air is given (to be adjusted by means of the throttle valve) so that the throttle valve does not close at the beginning of start to open again with beginning engine speed. In the process, the threshold `NRLMN` is set to 400 rpm, since a start is assumed up to this threshold. The threshold `NRLMNL` prevents a closing of the throttle valve in the case of an engine speed drop e.g. due to starting from rest.

The desired air mass flow is reduced by the air mass flow `mstew`, which is led into the intake manifold by the canister purging, since this absolute value must not be adjusted by means of the throttle valve. By a division of the desired air mass flow through the throttle valve `msdksw` by the density-corrected `KLAF`, the standardized air mass flow through the throttle valve `msndksw` is calculated.

The leakage air of the throttle valve actuator `msndkow`, which is learned by an adaptation in the function `BGMSZS` is subtracted from this air mass flow. The thus remaining standardized air mass flow `msndkoow` is converted to a desired angle for the throttle valve by the characteristic `WDKMSN` in the sub function `BWDKSGV`. The outflow characteristic `KLAF` is addressed to the desired pressure ratio `psspvdk,w`. This desired pressure ratio consists of the minimum of `psspvdk,w = pssolw/pvdk,w` (turbo) - `psspvdk,w = pssolw/pvdk,w` (for asp.engine) - and `PSPVDKUG`. This means that the desired throttle valve angle is only calculated via the `KLAF` up to the non-reduced range `psspvdk,w = 0.95`. The clearance is calculated in the sub function `WDKSUGS` for the aspirated engine and in `WDKSUGT` for the turbo engine.

Sub function BWDKSGV: Setpoint DK-angle (`wdksgvw`):

The desired angle `wdksgvw` for the triggering of the throttle valve is calculated from the standardized desired air mass `msndkoow` in this sub function. The desired angle is determined by the map `KFWDKMSN` up to the angle for the non-reduced operation `wdkugdw`. This is the inverse map of `KFMSNWDK` and it is adjusted to the mounted throttle valve actuator. The calculation of the standardized air mass `msndkoow` is described in the sub function `BMLDKNS`. The non-reduced angle range of the throttle valve is given by the pressure ratio (pressure downstream the throttle valve) to (pressure upstream the throttle valve)  $> 0.95$  (`PSPVDKUG`). The throttle valve angle belonging to this pressure ratio is stored in the engine speed dependent characteristic `WDKUGDN` and is available as `wdkugdw` (function `BGMSZS`). If the angle from `WDKMSN` calculated via the standardized desired air mass is greater than the angle `wdkugdw`, then the condition for non-reduced operation `Bugds = true`. Once the condition `Bugds` is set, the charge controller is deactivated (see section `FUEREG`).

If the desired pressure ratio is  $> 0.95$ , then it is no longer possible to determine the standardized air mass flow and thus also not the desired angle for the throttle valve by means of the outflow characteristic `KLAF` for numerical stability reasons. For the remaining desired angle of the throttle valve from `wdkugdw` up to 100% a different residual angle determination `dwkdsusw` resp. `dwkdsutw` is performed for aspirated and turbo engines. This residual value is added to `wdkugdw` in the non-reduced range. Via the maximum permitted desired throttle valve angle `KFWDKSMX`, the desired angle is - if necessary - limited and made available as `wdksvw`. This can be used for power reduction or for dimming intake noise. In order to increase the lifetime of the DVE-actuator, the standardized air mass flow `msndkoow` is smoothed by means of a median filter for little `rlsolw` changes in the sub function `FILTER`. If  $\Delta \text{rlsol}$  (`drlsolmf = abs(rlsolw - rlsol(t-40ms))`) ranges below the threshold `DRLSOLMF`, meaning rather small desired torque changes, the filter is active (`Bmfact = true`). The actual value of `msndkoow` is intermediately stored in the 5-values large input filter buffer. The values are stored in a 5-value output filter buffer in decreasing values. If the old filter value `mlwdknfw` is not situated within the range of the min. and max. values of this output buffer, it is centered to the mid-value of this buffer. If the threshold `drlsolmfw > DRLSOLMF`, the filter output value `mlwdknfw` is directly set to the filter input value `msndkoow`. In addition, the filter input value is taken over by the filter input buffer.

For special cases, e.g. start and after-run it is required to predetermine an angle that is independent of the torque calculation. In this case, the input `wdksomw` is utilized, when `Bwdksom` is active. Via the switch `Btfwdksom`, a switch-over to the filter time constant `tfwdksom` can be effected. The TP (LP) filter is needed for the transition between "start angle" and "torque-based" operation. In the case of engines with intake manifold injection, the filter can also be switched on during the operation via the code word `CWFUEDK` (bit 6) with changing time constant `tfwdksw`.

Turbo engine: Sub function WDKSUGT

Since for the turbo engine the charging is performed in the non-reduced range via the boost pressure control, the throttle valve should be completely open in this range to avoid throttle losses. For this the pressure ratio `vpssplsw` is given in dependency of desired manifold pressure/ambient pressure in the boost pressure control. If `vpssplsw > 0.95`, i.e. `vpssplsw > PSPVDKUG`, the non-reduced range starts. The throttle valve clearance `wdksumxw` = difference between the non-reduced desired angle `wdkugdw` and the maximum permitted desired angle `WDKSMX` is linearly scaled by the ratio  $(1 - vpsspls<sub>w</sub>) / (1 - PSPVDKUG)$ . The value for `PSPVDKUG` is 0.95 (see function `BGMSZS`). The bit `Bwdkdsut`, which is used as `Bfkmsdks` for the stop of the `fkmsdk`-integrator in the function `BGMSZS`, is set with active throttle valve clearance.

Aspirated engine: Sub function WDKSUGDS

Here a so-called pedal overtravel is introduced:

Bit4 of `CWFUEDK`=false:

If the desired pressure ratio `psspvdk,w` is  $> PSPVDKUG$  (i.e. `Bklafbg = true`), or `Bugds = true`, the pedal overtravel begins (`Bdwkugd = true`). `mrfaw` at the beginning of the overtravel is frozen in `mrfabugw`. The throttle valve clearance `wdksumxw` = difference between the non-reduced desired angle `wdkugdw` and the maximum permitted desired angle `WDKSMX` is linearly scaled between `mrfabugw` and `mrfamxw` by the ratio for the pedal overtravel  $[\text{mrfa}_w - \min(100\%, \text{mrfabugd})] / [\text{mrfamx}_w - \min(100\%, \text{mrfabugd})]$ , as soon as `Bwdkdsus = true`. The value `wdkdsusw` is added to `wdkugdw` and made available as desired angle `wdksvw`. `wdksvw` can be `WDKSMX` at the maximum. The end of the pedal overtravel is reached, if e.g. `mrfaw` is again  $< \text{mrfabugd}_w$  or if `milsolw` is  $< \text{FMIUGDS} * \text{mifafu}_w$  ( $0.95 * \text{mifafu}_w$ ) or for vehicles with



CVT-transmission B\_mgbget=true.

For a positive load change, an excessive increase in torque is predetermined with the air path (mifal) via the function 'driver's demand calculation' for a fast DK-opening. This excess - on the DK-side - has the effect that the non-reduced range is reached via the pressure ratio psspvdK. If the desired driver torque is stored, it is at that particular moment too low, since it does not contain the excess. The storage is therefore prevented by B\_lsd until this dynamic precontrol has decreased again. The map MRFARUGDN prevents that the value 0 is stored in mrfabugd\_w during start, if mrfa\_w = 0 and psspvdK\_w > 0.95. Thus it is prevented that the pedal overtravel is activated, if wped is close to 0. The fkmsdk-integrator is stopped in the function BGMSZS via B\_fkmsds with active throttle valve clearance ( B\_dwdksut = true ).

Bit4 CWFUEDK=true:

-----  
The pedal overtravel is not calculated depending on mrfabugd\_w, but directly depends on the characteristic MRFARUGDN. The point in time at which the pedal overtravel is switched on/off depends on the same conditions as for bit 4 of CWFUEDK=false.

Sub function WDKAPPL: Application management

-----  
The application management enables the deactivation of the normal calculation of the desired DK angle, which necessitates the functionality of the torque management (fixed value CWMDAPP). The desired DK angle is instead only dependent on the pedal value or it is even set to a fixed value. The desired throttle valve angle is directly dependent on the pedal wped in the case of an engine speed = 0 rpm. By this, it is possible to achieve a movement of the throttle valve actuator via the pedal, e.g. in the workshop. Via the system constant SY\_TWDKS, a program part can be integrated which enables the triggering of the throttle valve via a tester by means of a predetermined desired angle cvwdk. For this, the tester must transfer the desired angle in cvwdk and the bit B\_cwdk must be set. !!!! When using this feature, it must be absolutely ensured that the vehicle is not accelerating. !!!! This can e.g. be assured by checking e.g. brake switch, clutch switch, engine speed = 0, vehicle speed = 0 ! !!!!  
If it is switched over to the map FPWDKAPP, an offset WDKSOFs is added to the characteristic for evtmod<EVTMODKMNDK. Thus a wrong learning of the DK e.g. through ice is avoided.

Sub function NACHLAUF: Calculation of the desired throttle valve angle during after-run

-----  
In the after-run an angle is preset independently of the torque structure. This angle wdksom\_w is defined in the function WDKSOM. For systems with integrated main relay and DK-actuator this angle is acutated, if a current supply is guaranteed in the after-run. This way a smooth engine shut-down is assured.

## APP FUEDK 21.30 Application hint

Aspirated engine and turbo:

-----  
KLAF: see charge sensing  
KFWDKMSN: inverse to KFMSNWDK  
KUMSRL: see charge sensing

CWFUEDK: Bit 0: asp. engine, fkmsdk-correction at pedal overtravel  
Bit 1: no used in this FDEF (platform development of the start function nstat\*KUMSRL)  
Bit 2: no used in this FDEF (B\_dwdksus before and after flip-flop evaluation)  
Bit 3: no used in this FDEF (B\_dwdksus before and after flip-flop evaluation)  
Bit 4: asp. engine, for pedal overtravel dwdksus\_w calculated via mrfabugd\_w or mrfaugd  
Bit 5: only for turbo: B\_ldrugd can be set independently of B\_llrein  
Bit 6: only for NOT BDE: TP(LP)-filter before wdksgv\_w is only switched on during start (or always switched on)  
Bit 7: only for turbo: input of the characteristic KLDPPK is switched over by mlsol\_w auf ml\_w

CWFUEDK=192 (Bit0=false: functionality as %FUEDK 18.20  
Bit4=false: functionality as %FUEDK 18.20  
Bit5=false: functionality as %FUEDK 18.20  
Bit6=true: as %FUEDK 18.20, if Bit6=false --> running time reduction  
Bit7=true: then functionality as %FUEDK 18.20)

CWRLAPPL: only for test bench (switch over of pssol\_w with or without the influence of the charge controller)

EVTMODMNDK = 5 °C

WDKSOFs = 5 %

FPWDKAPP wped_w [%]	1.5	6.25	11.0	15.63	23.43	31.25	39.0	46.87	54.69	62.5	70.3	78.13	82.86	85.94	89.84	93.75
wdksv_w [%]	1.7	7.1	11.16	15.25	20.0	31.0	39.0	47.0	55.0	62.0	70.0	78.0	82.00	86.0	90.0	99.9

WDKSAPP 2 %

TWDKSV: pspvmin_w	0.990	0.992	0.996	0.998	1.0	1.02
	0.01	0.1	0.15	0.2	0.25	0.0

NRLMN: 400 1/min ( defined via umsrl\_w / the throttle valve opening during start) The throttle valve opening is limited by wdkgud\_w.  
NRLMNLRLR: 100 1/min below low idle speed (700 1/min)

KFWDKSMX: engine speed interpolation points are chosen as for WDKUGDN. It must be observed that at the throttle valve angle limitation for power reduction the interpolation distances in the reduction range are possibly chosen more tightly. Altitude interpolation points: the upper interpolation point for altitude must be selected such that it corresponds to the altitude for which a power reduction should take place. In the range of the power reduction KFWDKSMX < 100% must be entered in such a way that the max. desired engine power is obtained through the thus effected throttling. The lower interpolation point must be selected such that it corresponds to the altitude for which - due to the lower atmospheric density - the natural power reduction corresponds to the desired rated power.





As an orientation, a 10% power reduction for an increase in altitude of 1000 m can be assumed ( $\Delta \rho_{w} = -0.1$ ).

At this interpolation point  $K_{FWDKSMX} = 100\%$  must be entered for the whole speed range.  
nmot\_w: 240, 760, 1000, 1520, 2000, 2520, 3000, 3520, 4000, 6000 1/min  
rho\_w: 0.8, 0.9, 1.0

Values:  $K_{FWDKSMX} = 100\%$  -> angle limitation not active.

Determination of the switch-on threshold for median filters:

1) Median filter switch-off:  $D_{RLSOLMF} = 0$  ;

Determination of the max.  $d_{rlsolmf\_w}$  as value 1 for idling.

Then slow acceleration out of the idle operation (low dynamics), determination of the resulting  $d_{rlsolmf\_w}$  as value 2.  
Turning of the power steering up to the limit during idling, determination of the resulting  $d_{rlsolmf\_w}$  as value 3.

Vehicle acceleration (at load with higher dynamics), determination of the resulting  $d_{rlsolmf\_w}$  as value 4.

From the max. value of value 1 and 2 and the min. value for value 3 and 4, the threshold  $D_{RLSOLMF}$  is determined.

This threshold will mostly be situated in the range of value 4.

Suggested value  $D_{RLSOLMF}$ : 2%

For the application of the charge sensing at the test bench, engine speed/load interpolation points should be reached automatically.

The desired value predetermination in  $\%MDFUE$  is realized with a fixed  $r_{lsol}$  or an accelerator pedal value. So that the preset  $r_{lsol}$  is converted in a real  $r_l$  with the same value, the charge controller is used with a changed parameter set for the adjustment:  $r_l - r_{lsol}$ . This functionality is only valid, if the system constant  $S_{V\_RLAPP}$  in the function  $PROKON$  has been set to a value  $> 0$ . With bit 0 of  $C_{WRLAPPL}$ , the functionality is then finally activated. The combination with the vehicle speed ensures that the adjustment function can only be activated for a vehicle at rest or at the test bench engine.

Only asp. engine:

-----

$M_{RFABUMX} = 100\%$

$M_{RFAUGDN}$  (SNM12FEUB)

nmot\_w

Values all at 80 %

$F_{MIUGDS} = 0.95$

Only turbo:

-----

$F_{UEPMLD}$	$l_{ditv\_w}$	3	6	10	20
Values		0.999	0.8	0.2	0

$Z_{PVDKR}$	interpol. points	$p_{sspu\_w}$	0.9	1.0	1.1	1.2	1.3	1.4	
Values			0	0	0	2	2	0	s

$D_{PUPS} >= 250$  hPa

$K_{LDPK} = 0$  hPa at all interpolation points

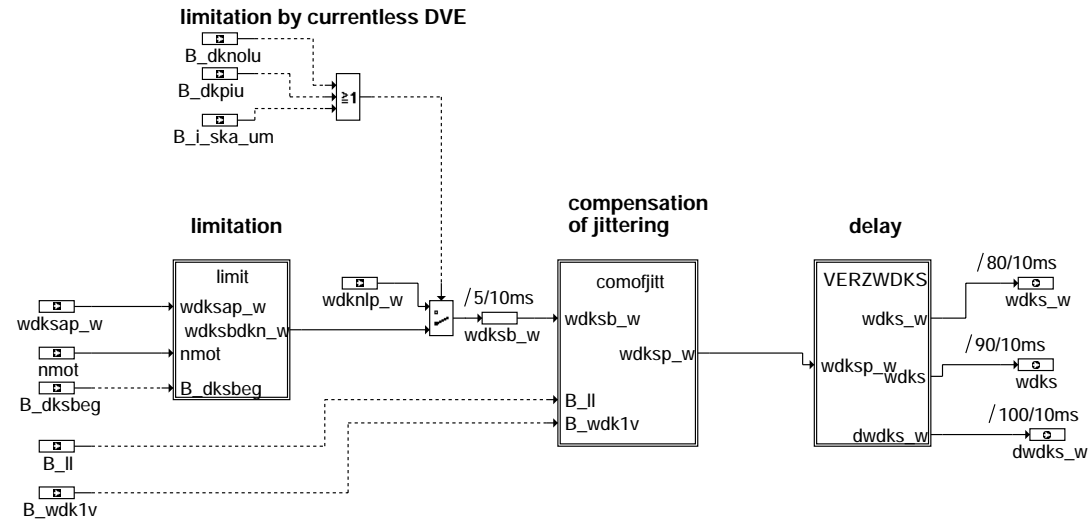
Application: Measurement of pressure drop at throttle valve - esp. for high air mass flows. Then determination of 16  $m_{lkge\_w}$  interpolation points and take-over of the respective pressure drop in the characteristic

$P_{LSOLAP} = 0$  hPa. If during the application phase a desired boost pressure should be preset,  $B_{plsolap}$  = Bit 5 of  $C_{WMDAPP}$  must be set to true and the desired boost pressure must be predetermined via  $P_{LSOLAP}$ .

$P_{SPVDKUG}$  see function  $B_{GMSZS}$

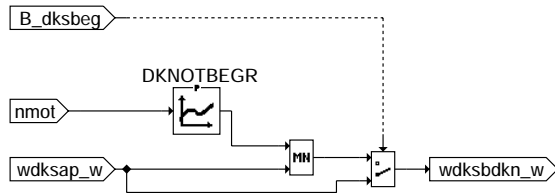
## FUEDKSA 1.20 Influence of air charge by throttle blade, processing throttle-valve angle

### FDEF FUEDKSA 1.20 Function definition FUEDKSA 1.20



#### fuedksa-fuedksa

Limitation for DK-Poti-limp home:  
=====



#### fuedksa-limit

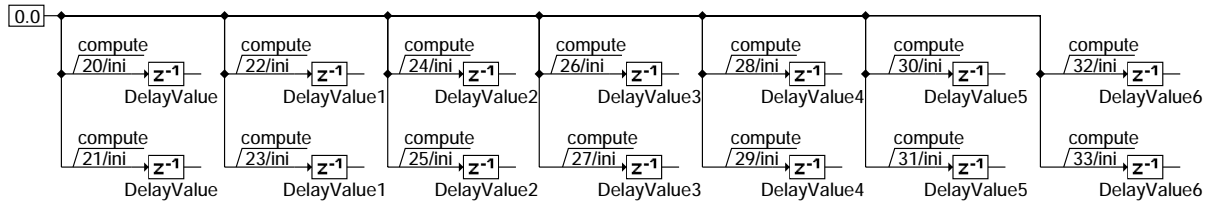
fuedksa-fuedksa

fuedksa-limit





Initialization:  
=====



**fuedksa-init**

**ABK FUEDKSA 1.20 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWWDKSPE			FW	Code word: Predicted throttle-valve target-value de-jittering active
DKNOTBEGR	NMOT		KL	Limitation of set value as f(nmot) if B_dknot = true
ENTDKLL			FW	De-jitter threshold (inc.) for throttle-valve target value during idling (B_I1)
ENTDKNLL			FW	De-jitter thresh. (inc.) for throttle-valve target value outside idling (!B_I1)
TVWDKS			FW	delay time for desired throttle angle

**Variable Source Type Description**

Variable	Source	Type	Description
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKPIU	SREAKT	EIN	Condition: irreversible SKA
B_DKSBEG	GGDVE	EIN	condition: limiting throttle-valve setpoint value
B_J_SKA_UM	UFREAC	EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_LL	MSF	EIN	Condition idle
B_WDK1V		EIN	Condition: amplified signal from potentiometer 1 used to calc. throttle angle
DWDKS_W	FUEDKSA	AUS	modification of desired throttle angle
NMOT	SWADAP	EIN	engine speed
WDKINK_W	FUEDKSA	LOK	Current increment of throttle-valve target value
WDKNLP_W	BGDVE	EIN	throttle angle in the limphome air position
WDKS	FUEDKSA	AUS	desired throttle angle w.r.t. to lower mechanical stop
WDKSAP_W	FUEDK	EIN	desired throttle position from application value
WDKSBA2_W	FUEDKSA	LOK	Throttle-valve target angle after limiting, value from computing schedule n-2
WDKSBA_W	FUEDKSA	LOK	Throttle-valve target angle after limiting, value from computing schedule n-1
WDKSB_W	FUEDKSA	LOK	Throttle-valve target angle after limiting
WDKSFL	FUEDKSA	LOK	Flank-change indicator for throttle-valve target value wdksap_w
WDKSPA_W	FUEDKSA	LOK	Predicted throttle-valve angle, value from computing schedule n-1
WDKSP_W	FUEDKSA	AUS	predicted desired throttle angle
WDKSVFL	FUEDKSA	LOK	Flank-change indicator for throttle-valve target value wdksp_w
WDKSWE_W	FUEDKSA	LOK	Throttle-valve nominal-value threshold for predicted de-jittering
WDKS_W	FUEDKSA	AUS	desired throttle angle w.r.t. to lower mechanical stop

**FW FUEDKSA 1.20 Fixed Values**

Parameter	Value	Description
CWWDKSPE		Code word: Predicted throttle-valve target-value de-jittering active
ENTDKLL		De-jitter threshold (inc.) for throttle-valve target value during idling (B_I1)
ENTDKNLL		De-jitter thresh. (inc.) for throttle-valve target value outside idling (!B_I1)
TVWDKS		delay time for desired throttle angle



## FB FUEDKSA 1.20 Detailed description of function

### 1. Desired value limitation for DK-Poti limp home (sub function limitation):

For DVE-actuator operation at zero current ( B\_dknolu or B\_dkpiu or B\_i\_ska\_um = true), the angle for the limp home position (wdknlp\_w) is considered as desired angle. That way it is assured that e.g. the load prediction with constant desired angle wdks\_w does not predict throttle valve dynamics.

### 2. Predictive desired angle de-jittering (sub function comofjitt):

The predictive desired angle de-jittering is used for smoothing the desired DK value. The operating cycles for the DV-E5 are thus reduced. The desired anlge de-jittering only applies to that extent that no physical effect on the whole system occurs.

The de-jittering thresholds (wdkswe\_w) are formed depending on B\_ll and B\_wdklv. 4 different de-jittering thresholds depending on the dating of ENTDKLL and ENTDKNLL 4 are the result.

Matrix of resulting de-jittering thresholds wdkswe\_w:

		B_wdklv	
		0	1
B_ll	0	0,1007 * ENTDKNLL	0,0259 * ENTDKNLL
	1	0,1007 * ENTDKLL	0,0259 * ENTDKLL

/END

BILD /SYM PRINZ-ENTJ  
TEXT/ANF

### 3. Sub function VERZWDKS: Desired DK deadtime:

The desired DK value (wdks\_w) is transferred to the load prediction. For the DK position controller, a delayed value is calculated in the sub function VERZWDKS (wdks\_w). The deadtime can be adjusted between 0 and 50 ms .  
With the un-delayed desired DK value, the manifold pressure and the relative charge in the function BGRLP are predicted. A fuel quantity relative to this charge is calculated. By delaying the throttle valve angle, it is assured that at the ignition the advanced fuel quantity fits to the relative cylinder charge.

## APP FUEDKSA 1.20 Application hint

### 1. Deactivation of function parts

Label	Passive value	deactivated...
DKNOTBEGR	100 %DK	desired angle limitation during DK-Poti limp home
CWWDKSPE	0	predictive desired angle de-jittering
TVWDKS	0 ms	desired angle delay

### 2. Others

TVWDKS: fixes the deadtime between wdks\_w and wdks\_w  
0: no delay; 1: 10 ms; 2: 20 ms; ...; 5 or more: 50 ms delay

### 3. Suggested values

CWWDKSPE = 1  
ENTDKLL = 4  
ENTDKNLL = 6  
  
TVWDKS\_W = 0.01s, application see %BGRLP  
DKNOTBEGR = 100% for interpolation points nmot: 0, 500, 1000, 2000, 2500, 3000, 4000 rpm

## WDKSOM 2.40 calculatiof of desired throttle angle without torque structure

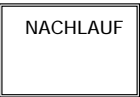
### FDEF WDKSOM 2.40 Function definition

WDKSOM 2.20

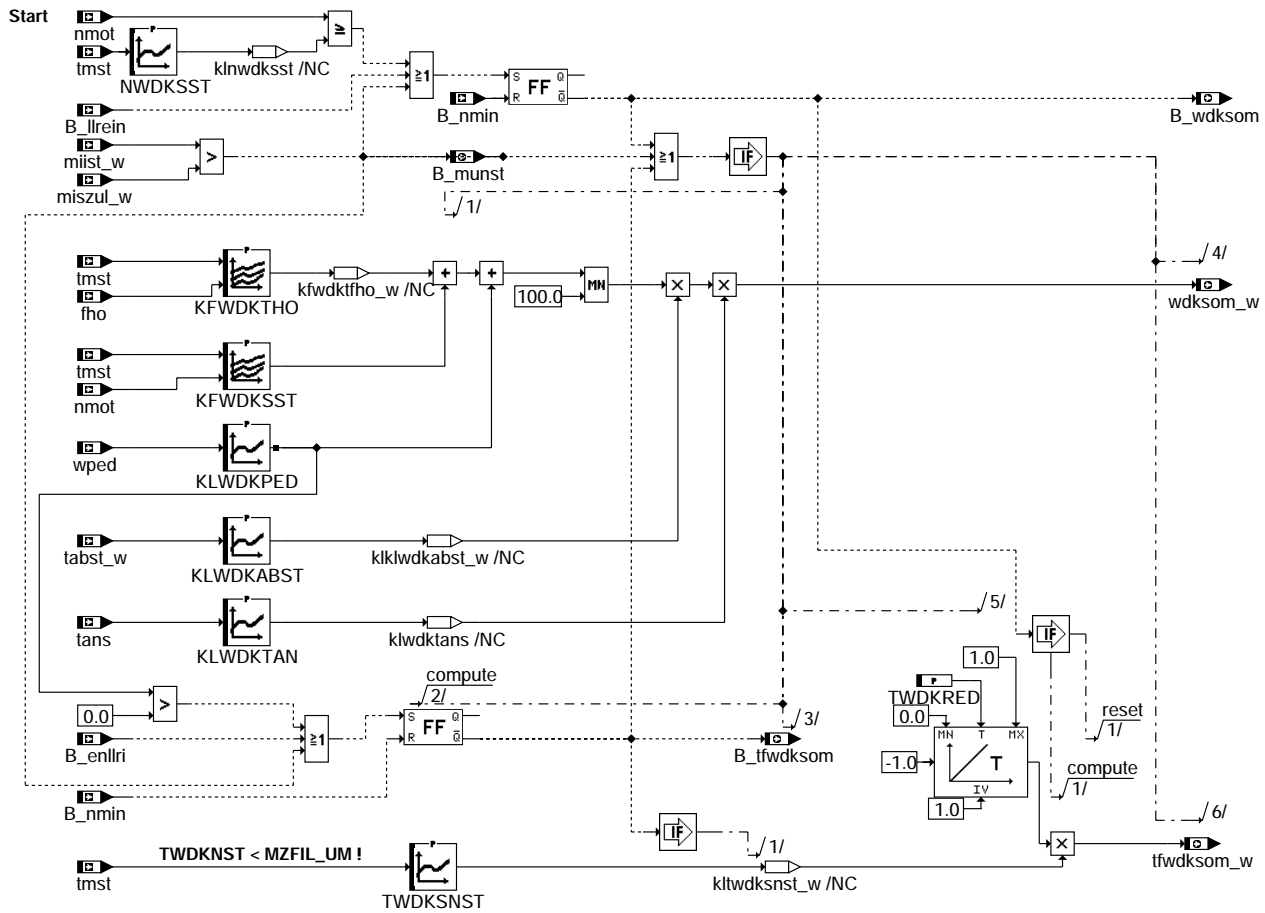
normal engine operation (SKI15 = on)



engine operation after ignition off (SKI15 = off)



wdksom-main



wdksom-start

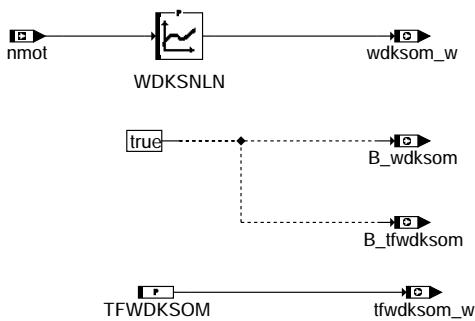
wdksom-main

wdksom-start

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Subfunction Block 1: Set Value of Throttle Valve during Start

Nachlauf



wdksom-nachlauf

Subfunction Block 2: Set Value of Throttle Valve during ECU After-Run

ABK WDKSOM 2.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFWDKSST	TMST	NMOT	KF	desired throttle position at start-up
KFWDKTHO	TMST	FHO	KF	desired throttle position at start-up - f (high, engine start temperatur)
KLWDKABST	TABST_W		KL	Weighting desired throttle position at start-up
KLWDKPED	WPED		KL	Offset desired throttle position at start-up
KLWDKTAN	TANS		KL	weight of throttle position at start up with intake air temperatur
NWDKSST	TMST		KL	threshold for deactivation desired throttle position without torque structur
TFWDKSOM			FW	time constant for filtering desired throttle angle at kl15 off
TWDKRED			FW	Weighting time constant for filtering of reference throttle blade position
TWDKSNST	TMST		KL	time constant for filtering of reference throttle blade position
WDKSNLN	NMOT		KL	desired throttle angle at kl15 off

Variable	Source	Type	Description
B_ENLLRI	LLRBB	EIN	enable integrator: idle speed controller
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_MUNST	WDKSOM	AUS	Condition allow intervention of torque monitoring
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_TFWDKSOM	WDKSOM	AUS	time constant to filter desired throttle angle without torque structure active
B_WDKSOM	WDKSOM	AUS	desired throttle angle without torque structure active
FHO	BGPU	EIN	Correction factor altitude
MIIST_W	MSF	EIN	indicated real engine torque
MISZUL_W	MDZUL	EIN	maximum permissible indicated torque
NMOT	SWADAP	EIN	engine speed
TABST_W	BGTABST	EIN	soak time
TANS	SWADAP	EIN	Intake air temperature
TFWDKSOM_W	WDKSOM	AUS	time constant to filter desired throttle angle without torque structure
TMST	GGTFM	EIN	engine temperature at start
WDKSOM_W	WDKSOM	AUS	desired throttle angle without torque structure
WPED	GGPED	EIN	Standardized accelerator pedal angle

FW WDKSOM 2.40 Fixed Values

Parameter	Value	Description
TFWDKSOM		time constant for filtering desired throttle angle at kl15 off
TWDKRED		Weighting time constant for filtering of reference throttle blade position

**FB WDKSOM 2.40 Detailed description of function**

The function WDKSOM calculates a desired angle `wdksom_w` for the throttle position of the DVE actuator during start and during ECU after-run.

**Start:**

The set value for the throttle position is mainly dependent on the engine temperature during start.

Since the drag torque of the engine is distinctly higher at cold engine than at warm conditions, the engine is throttled later by a larger opening of the throttle valve during the starting procedure.

The dependence of the throttle position on the engine start temperature can be combined with the influence of the high (KFWDKTHO) or with the influence of the engine turning speed (KFWDKSST). If both characteristic maps should be used, the values are added. The influence of high (less air density) is considered with the map KFWDKTHO amongst the influence of the engine start-temperature. The map dates are taken into account that the factor for high itself is dependent on the temperature (not a linear connection).

As by short soak times the drag torque of the engine is lower, the set value for the throttle position can be reduced (KLWDKABST). An additional interaction by the driver is possible (KLWDKPED).

The influence of an changed cylinder charge is partially considered with the correction for high (KFWDKTHO). The influence of the intake air temperature on the cylinder charge and with it the influence on the throttle position can additional be wighted with the map KLWDKTAN. This especially is important for hot start-up of the engine.

When the speed threshold NWDKSST is exceeded or the idle control is active (B\_llrein) the set value for the throttle position is switched to the set value from the torque structure.

The transition takes place with an adjustable time constant TWDKSNST, which is dependent on the engine starting temperature.

The time constant can be reduced (TWDKRED) during the transitional phase. So a leap of `wdks_w` by switching to the torque structure can be prevented.

When the integrator component of the idle control (B\_enllri) is activated this time constant is switched to the value for normal operation (tfwdks\_w).

If the indicated real engine torque `miist_w` exceeds the maximum permissible indicated torque `miszul_w`, there is switched immediately to the torque structure. So a intervention of the torque monitoring functionality is possible.

**ECU After-run:**

During the ECU after-run (at engine run-on, if SK15 OFF) throttling is generated by closing of the throttle valve.

The transition from normal operation to the value in the ECU after-run WDKSNLN is performed by a filtering with the time constant TFWDKSOM. This makes a faster engine standstill possible.

By the throttling also vibrating of the engine due to higher compression pressures without throttling is prevented.





## APP WDKSOM 2.40 Application hint

WDKSNLN: Base points nmot\_w: 200, 400, 600, 800, 1000, 2000, 3000, 4000 rpm  
Values: 2, 2, 2, 2, 2, 7.5, 15, 20 %

TFWDKSOM: 0.01 s --> no filtering

NWDKSST: Base points tmst: -30 -20 -10 0 20 90 Grad C  
Values: 1100 1000 900 800 700 650 rpm

The threshold should be between (B\_stend, see NSTNM in %BBSTT) and activation of the idle control (B\_llrein, see %LLRBB). In NWDKSST must not be values greater than 1200 rpm, because then the torque structure is activated to late and an intervention of the torque monitoring functionality is possible.

KFWDKTHO: Base points tmst : -30 -25 -20 -15 -10 -5 0 20 40 60 90 110 Grad C  
fho : 0.7 0.8 0.9 1.0  
values (for all high): 30 25 20 13  
(at sea level 1.0, with high increasing)

KFWDKSST: Base points tmst : -30 -25 -20 -15 -10 -5 0 20 40 60 90 110 Grad C  
nmot : 100 500 750 1000 1/min  
all values : 0 %

A constant presetting is recommended by RB via the speed, since otherwise the throttle valve will be moved at speed dynamics (e.g. by misfiring).

KLWDKABST: Base points : tabst\_w: 0 300 3600 18000  
Values : 0.9 0.95 1.0 1.0

KLWDKTAN Base points tmst : -20 0 30 80 °C  
values : 1 1 1 1

KLWDKPED: Base points: wped\_w : 0 20 99 %  
Values : 0 0 99 %

Since the driver should not move the throttle valve at start there will be no reaction to the driver's request up to a certain pedal value, e.g. 20% and the start is performed purely by control. Above this value the throttle valve is opened linear up to the maximum value so that, e.g. after flooding the driver can take measures. As soon as this characteristic becomes effective a simultaneous switch to the fast time constant for the filtering of the throttle valve set value is performed (normal operation).

TWDKSNST: Base points: tmst: -30 -20 -10 0 20 90 degrees C  
Values: 0.4 0.4 0.3 0.3 0.2 0.2 sec.

The time constant for the filtering of the throttle valve set value becomes slower, the lower the ambient temperature. With slow movement of the throttle valve attention has to be paid, however, that in general more dynamics is necessary at the ignition angle in order to obtain a good speed curve.

Caution:  
-----

The values in TWDKSNST have to be less than MZFIL\_UM (c. 405 msec). This is claimed by the torque monitoring functionality.

TWDKRED: Value: 5 sec.  
The value gives the time after that filtering finished.

## SU 62.10 Intake manifold switch-over

### FDEF SU 62.10 Function definition

No text for FDEF available!

### ABK SU 62.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CSU			FW	Codeword for intake manifold switch over
KFSU	NMOT	RLSHK	KF	Load/speed performance characteristics for suction tube switchover
KFSU2	NMOT	RLSHK	KF	map for intake manifold switch over, flap 2
SUMODE0			FW	no activation of intake manifold flaps
SUMODE1			FW	activation of flap 1, no activation of flap 2
SUMODE2			FW	no activation of flap 1, activation of flap 2
SUMODE3			FW	activation of flap 1 and 2
TASUS			FW	intake air temperatur threshold for intake manifold switch over
TMSUS			FW	engine temperature threshold for intake manifold switch over
TMSUSV			FW	temperatur threshold for intake manifold switch over with response delay
TVSU			FW	delay time for intake manifold switch over, flap 1
TVSU2			FW	delay time for intake manifold switch over, flap 2
TVSUM	TMOT		KL	delay time for intake manifold switch over in dependence of engine temperatur
TVSUST			FW	delay time for intake manifold switch over after start
Variable	Source		Type	Description
B_STEND	BBSTT		EIN	condition end of start
B_SU	SU		AUS	condition intake manifold switch-over
B_SU2	SU		AUS	condition intake manifold switch over, 2.flap
B_SUKP	SU		LOK	condition enable manifold intake switch over flap 1
B_SUKP2	SU		LOK	condition enable intake manifold switch over flap 2
E_DK	DDVE		EIN	Error flag: throttle position sensor

Variable	Source	Type	Description
E_TA	GGTFA	EIN	error flag: TANS
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
NMOT	SWADAP	EIN	engine speed
RLSHK		EIN	desired relative air charge corrected by altitude
SUMODE	SU	AUS	status of the intake manifold switch over
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature

### FW SU 62.10 Fixed Values

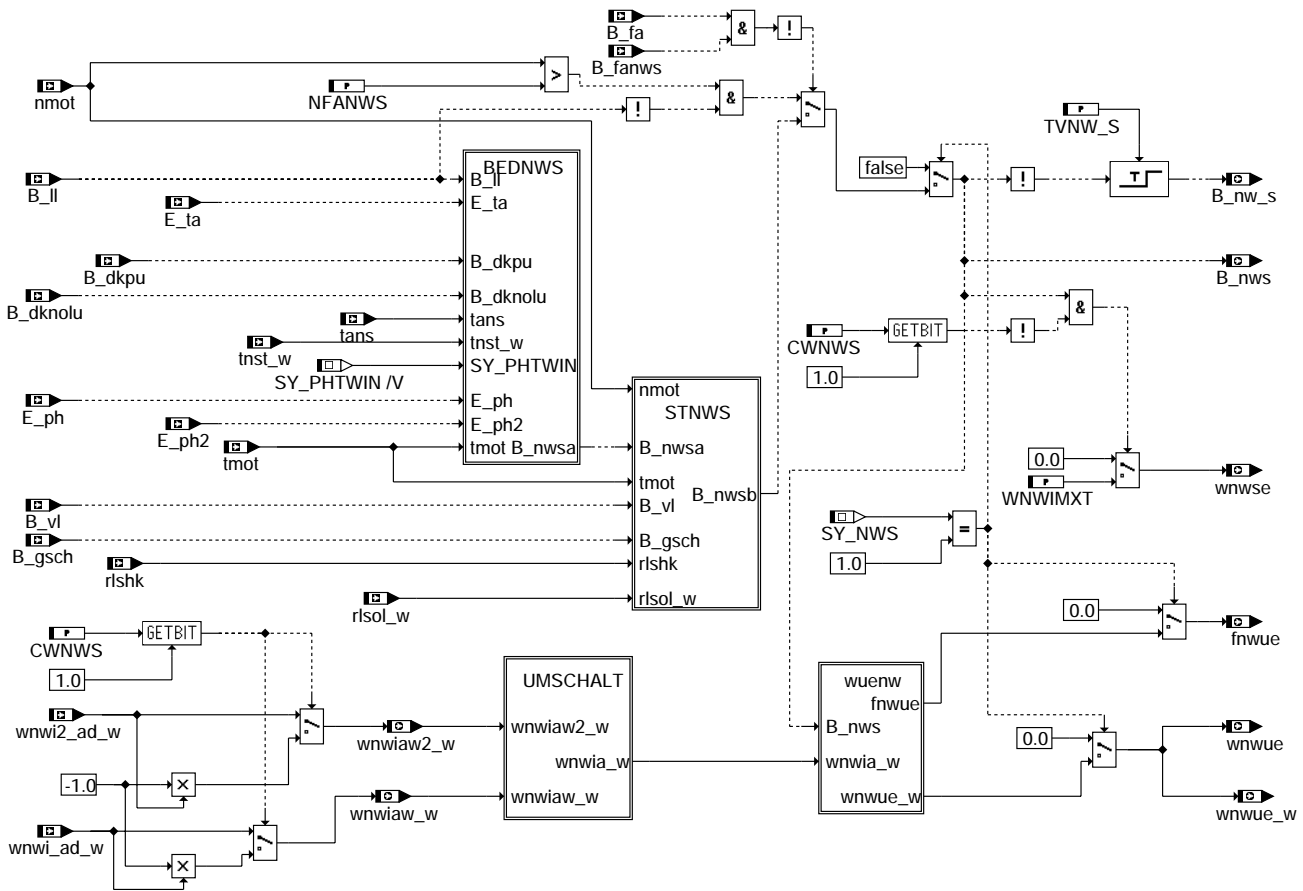
Parameter	Value	Description
CSU		Codeword for intake manifold switch over
SUMODE0		no activation of intake manifold flaps
SUMODE1		activation of flap 1, no activation of flap 2
SUMODE2		no activation of flap 1, activation of flap 2
SUMODE3		activation of flap 1 and 2
TASUS		intake air temperature threshold for intake manifold switch over
TMSUS		engine temperature threshold for intake manifold switch over
TMSUSV		temperature threshold for intake manifold switch over with response delay
TVSU		delay time for intake manifold switch over, flap 1
TVSU2		delay time for intake manifold switch over, flap 2
TVSUST		delay time for intake manifold switch over after start

### FB SU 62.10 Detailed description of function

### APP SU 62.10 Application hint

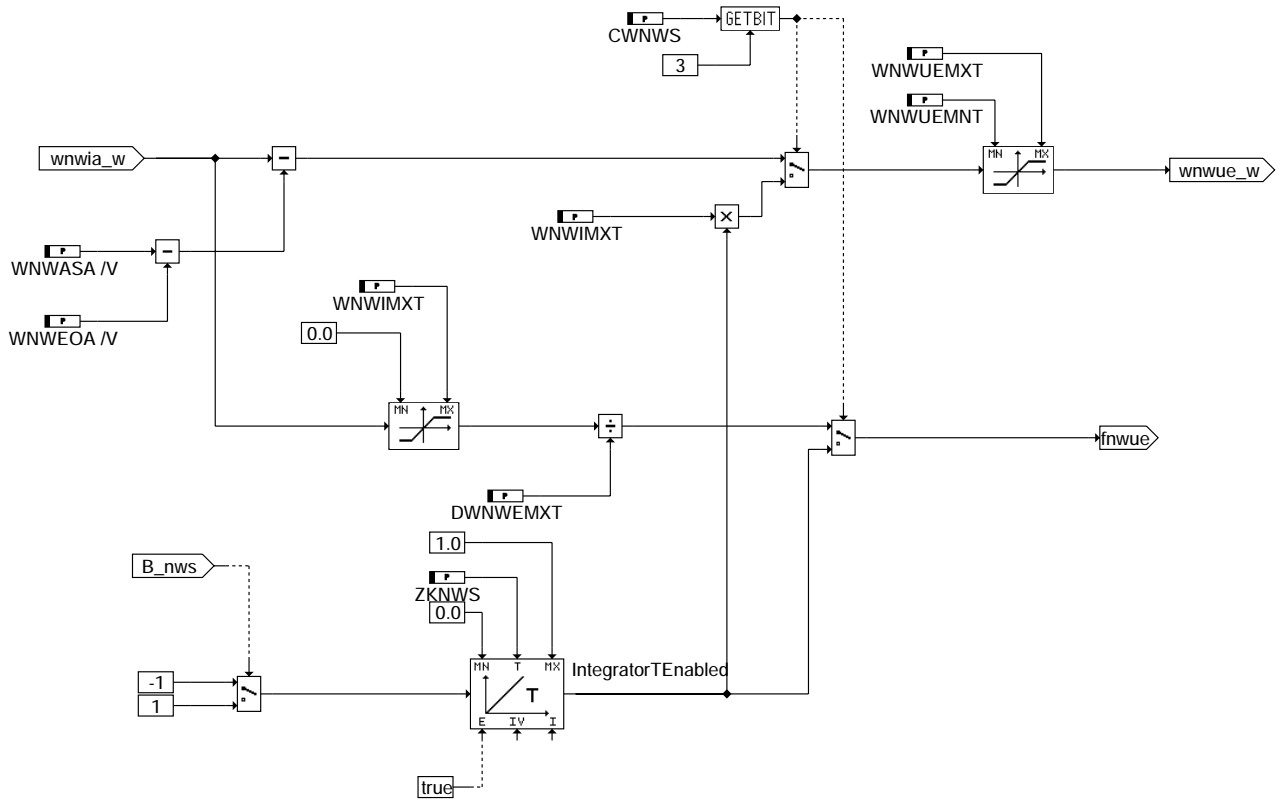
### NWS 55.60 Camshaft control

### FDEF NWS 55.60 Function definition

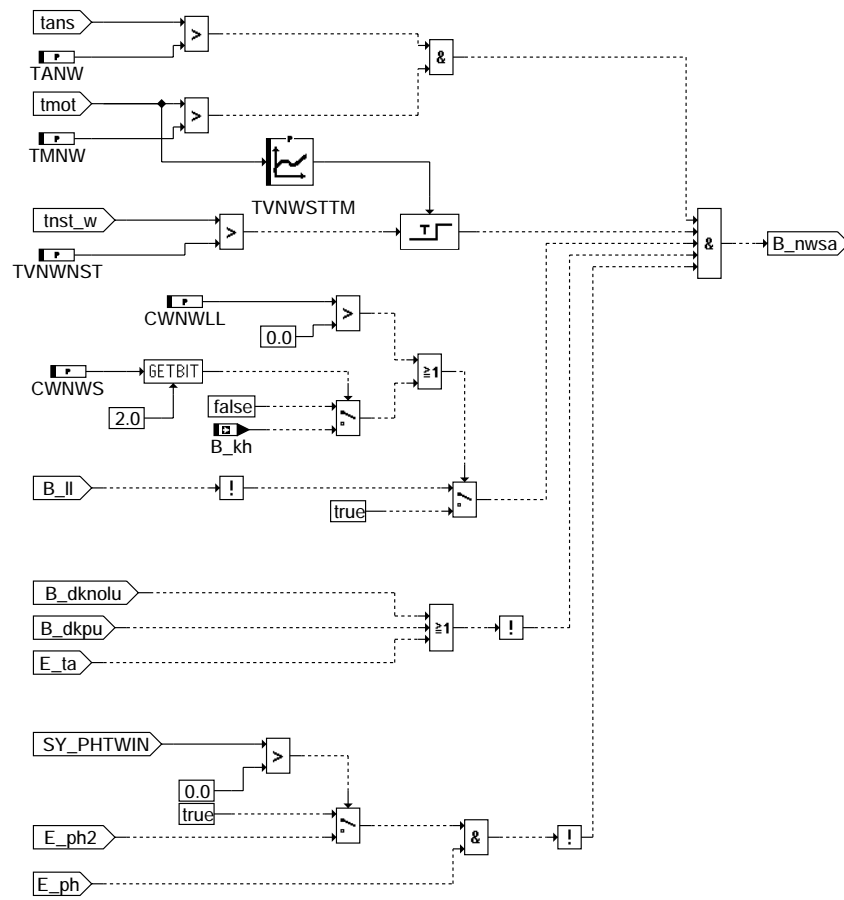


nws-nws

nws-nws



### nws-wuenw

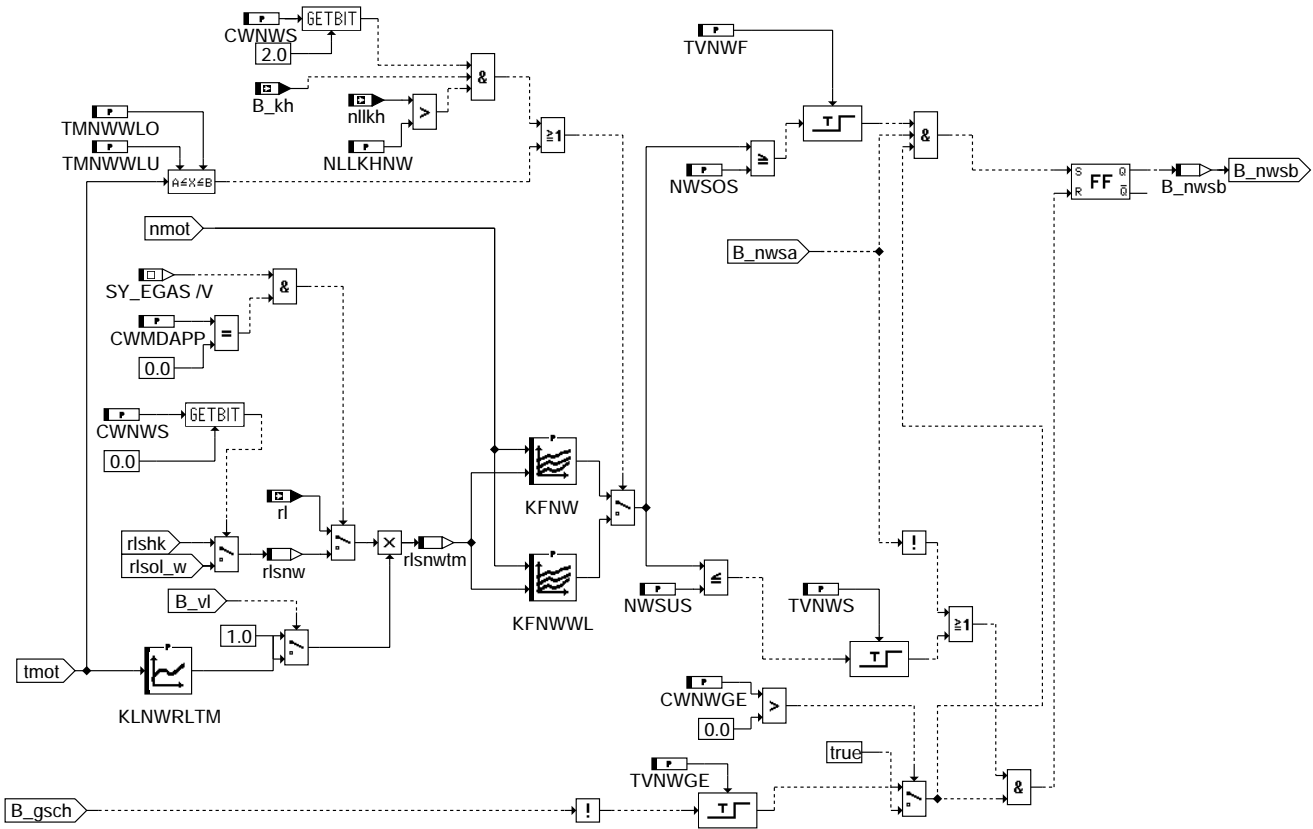


### nws-bednws



nws-wuenw

nws-bednws



nws-stnws

### ABK NWS 55.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWMDAPP			FW	code word for calibration without torque structure
CWNWGE			FW	code word camshaft control at transmission control operation
CWNWLL			FW	code word for deactivation of camshaft-control in idle
CWNWWS			FW	code word: camshaft control
DWNWEMXT			FW	Theor. max. delta between retarded and advanced adjustment of the intake valve
KFNW	NMOT	RLSNWTM	KF	characteristic map for variable camshaft spread
KFNWWL	NMOT	RLSNWTM	KF	
KLNWRLTM	TMOT		KL	Weighting of relative nominal filling over engine temp. for addressing KFNWS
NFANWS			FW	Speed threshold for function request NWS
NLLKHNW			FW	engine threshold for catalyst heating during idle position to change over
NWSOS			FW	Camshaft control upper switching threshold
NWSUS			FW	Camshaft control lower switching threshold
SY_EGAS			SYS	System constant E-GAS present
SY_NWS			SYS	system constant camshaft control: none, 2 point, continous
SY_PHTWIN			SYS	system constant 1/2 phase sensing system (sensor, wheel)
TANW			FW	Suction air temperature threshold for camshaft adjustment
TMNW			FW	Engine temperature threshold for camshaft adjustment
TMNWWLO			FW	
TMNWWLU			FW	
TVNWF			FW	Delay time until camshaft switchover enable to advanced
TVNNGE			FW	Delay time until switchover enable following transmission intervention
TVNWNST			FW	delay time : enable condition of camshaft control
TVNWS			FW	Delay time for camshaft adjustment
TVNWSSTM	TMOT		KL	delay time : enable of camshaft control after start, depending on engine temp
TVNW_S			FW	Delay time after the inlet valve is in retarded position with certainty
WNWASA			FW	Angle outlet valve closes at NW limit
WNWEOA			FW	Angle inlet valve opens at NW limit
WNWIMXT			FW	Theoretical maximum wnw (angle camshaft is)
WNWUEMNT			FW	theoretical minimum camshaft overlapping angle
WNWUEMXT			FW	Theoretical maximum camshaft overlapping angle
ZKNWS			FW	time constant for reproduction of the camshaft control
ZKWNWI			FW	Time constant for filtering wnw

Variable	Source	Type	Description
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_FA		EIN	condition general function request



Variable	Source	Type	Description
B_FANWS		EIN	condition general function request for diagnosis camshaft control
B_GSCH		EIN	Condition gear-shift in process
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_LL	MSF	EIN	Condition idle
B_NWS	NWS	AUS	Condition camshaft control
B_NWSB	NWS	LOK	Condition camshaft control before B_fa condition
B_NW_S	NWS	AUS	state information: camshaft control in retarded position
B_VL	MSF	EIN	Condition for wide open throttle
E_PH	DPH	EIN	error flag: phase sensor
E_PH2	DPH	EIN	error flag: phase sensor 2
E_TA	GGTFA	EIN	error flag: TANS
FNWUE	NWS	AUS	Weighting factor camshaft overlap
NLLKH	BBKHZ	EIN	Idling speed for catalyzer heating
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RLSHK		EIN	desired relative air charge corrected by altitude
RLSNW	NWS	LOK	selection between rlsol_w and rlsk for map KFNW
RLSNWTM	NWS	LOK	
RLSOL_W	MDFUE	EIN	desired relative air charge
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
TNST_W	BBSTT	EIN	time after end of start
WNWI2_AD_W	WANWKW	EIN	difference in crank angle between adapted and current 2. phase edge (word)
WNWIAW2_W	NWS	AUS	
WNWIAW_W	NWS	AUS	
WNWIA_W	NWS	AUS	Selection between wnw_i_w and wnw_i2_w
WNWILAD_W	WANWKW	EIN	difference in crank angle between adapted and current phase edge (word)
WNWSE	NWS	AUS	Nominal angle for camshaft inlet valve
WNWUE	NWS	AUS	camshaft overlap angle of inlet and outlet valve opening
WNWUE_W	NWS	AUS	camshaft overlap angle of inlet and outlet valve opening

### FW NWS 55.60 Fixed Values

Parameter	Value	Description
CWMDAPP		code word for calibration without torque structure
CWNWGE		code word camshaft control at transmission control operation
CWNWLL		code word for deactivation of camshaft-control in idle
CWNWS		code word: camshaft control
DWNWEMXT		Theor. max. delta between retarded and advanced adjustment of the intake valve
NFANWS		Speed threshold for function request NWS
NLLKHNW		engine threshold for catalyst heating during idle position to change over
NWSOS		Camshaft control upper switching threshold
NWSUS		Camshaft control lower switching threshold
TANW		Suction air temperature threshold for camshaft adjustment
TMNW		Engine temperature threshold for camshaft adjustment
TMNWWLO		
TMNWWLU		
TVNWF		Delay time until camshaft switchover enable to advanced
TVNWGE		Delay time until switchover enable following transmission intervention
TVNWNST		delay time : enable condition of camshaft control
TVNWS		Delay time for camshaft adjustment
TVNW_S		Delay time after the inlet valve is in retarded position with certainty
WNWASA		Angle outlet valve closes at NW limit
WNWEOA		Angle inlet valve opens at NW limit
WNWIMXT		Theoretical maximum wnw_i (angle camshaft is)
WNWUEMNT		theoretical minimum camshaft overlapping angle
WNWUEMXT		Theoretical maximum camshaft overlapping angle
ZKNWS		time constant for reproduction of the camshaft control
ZKWNWI		Time constant for filtering wnw_i

## FB NWS 55.60 Detailed description of function

### 1. Bildung des Freigabebits B\_nwsa

Die Bildung des Freigabebits B\_nwsa ist Voraussetzung für ein Verstellen der Nockenwelle in Abhängigkeit von der Drehzahl nmot und der höhenkorrigierten Sollfüllung rlskh. Das Setzen des Freigabebits erfolgt wenn folgende Bedingungen erfüllt sind:

- a.) -Wenn die Motortemperatur tmot größer als eine programmierbare Temperaturschwelle TMNW und die Ansauglufttemperatur tans größer als eine programmierbare Temperaturschwelle TANW sind.
- b.) -Wenn die Errorflags für die Drosselklappe E\_dk, für den Ansauglufttemperaturfühler E\_tans oder für den Motortemperaturfühler E\_tm nicht gesetzt sind.
- c.) -Wenn nach dem Startende eine programmierbare Zeit TVNWST vergangen ist.
- d.) -Wenn die Bedingung B\_ll nicht gesetzt ist.
- e.) -Wenn das Codewort CWNWS größer 0 ist.

### 2. Bestromung des Ventils für die Nockenwellensteuerung:

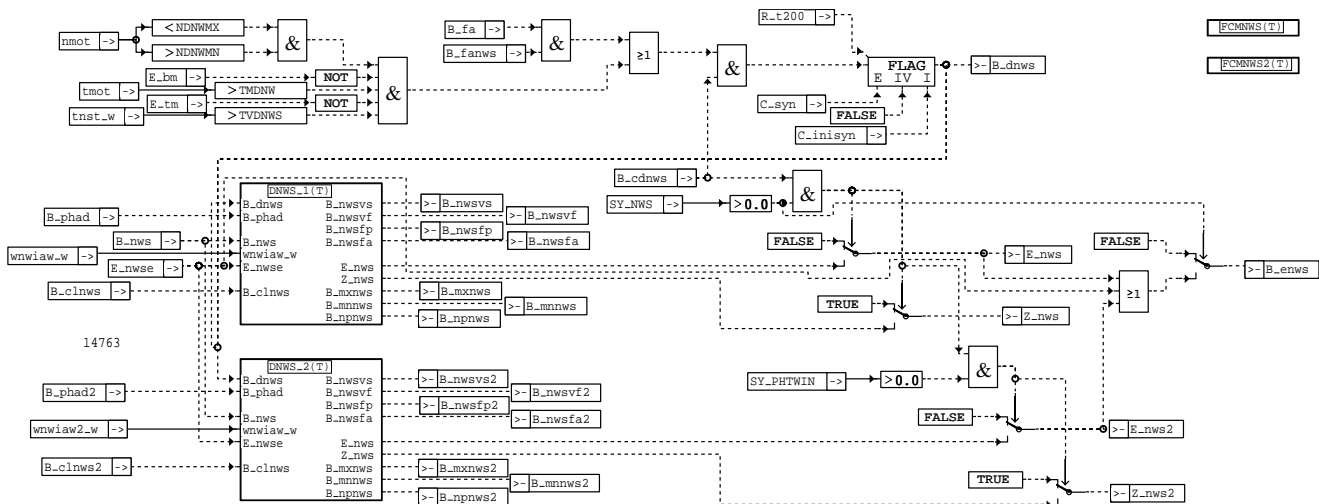
Wenn das Freigabebit für die Nockenwellensteuerung B\_nwsa gesetzt ist, wird in Abhängigkeit von der Drehzahl und der höhenkorrigierten Sollfüllung rlskh das Ventil für die Nockenwellensteuerung bestromt oder nicht. Dazu ist ein Kennfeld KPNW, das über die Drehzahl und der höhenkorrigierten Sollfüllung rlskh aufgespannt ist, mit den Zahlenwerten 0, 1 und 2 gefüllt. Der Zahlenwert 0 steht für nicht Bestromen des Ventils, der Wert 2 für ein Bestromen des Ventils und der Wert 1 dient als Hysteresewert. Entsprechend den jeweiligen Zahlenwert des Kennfeldes wird der Ausgang des RS-FF gesetzt oder rückgesetzt. Sollte der Ausgang des Kennfeldes KPNW gleich 2 sein, d.h. bestromen des Ventils, wird dieses erst nach einer programmierbaren Zeit TVNW durchgeschaltet. Dadurch soll verhindert werden, daß bei nur kurzfristigen Anfahren eines Umschaltpunktes ein hin- und herfahren der Nockenwellensteuerung erfolgt. Sollte vom Kunden gewünscht sein, daß bei der Bedingung B\_ge eine Veränderung der Nockenwellenstellung untersagt ist, so muß das Codewort CWNWGE größer Null gesetzt werden. Sollte das Bit B\_ge keinen Einfluß auf die Nockenwellenstellung haben, so muß das Codewort CWNWGE gleich Null gesetzt werden.

## APP NWS 55.60 Application hint

## DNWS 10.60 Diagnosis camshaft control

### FDEF DNWS 10.60 Function definition

Die Diagnose der Nockenwellensteuerung erfolgt über eine Prüfung des Verstellwinkels der Nockenwelle. Ein Unter- bzw. Überschreiten von Schwellwerten ist in der jeweiligen Lage der Nockenwelle erforderlich, um die korrekte Funktion der Nockenwellenverstellung anzuzeigen. Die Freigabe der Diagnose Nockenwellensteuerung erfolgt über die Bedingung B\_dnws.



### dnws-dnws

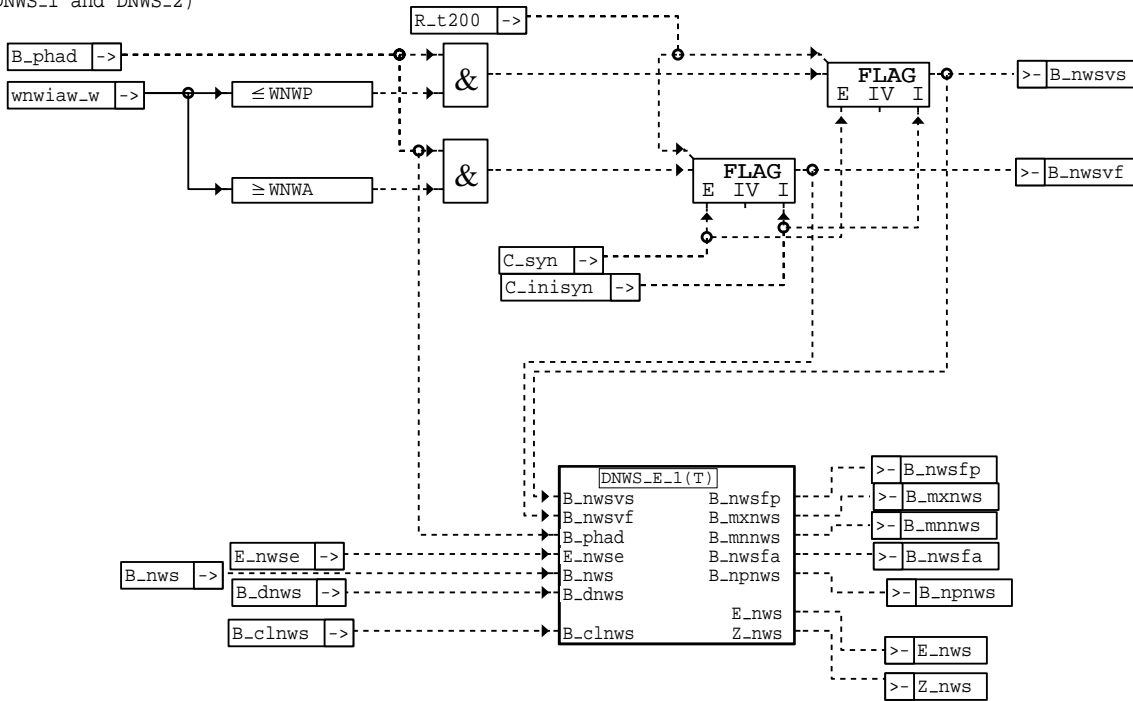
Bei Systemen ohne eine Nockenwellenverstellung wird keine Diagnose durchgeführt. Eine Initialisierung der Zyklus- und Fehlerbedingungen erfolgt dann entsprechend dem Schalter mit der Systemkonstanten SY\_NWS. Gleiches gilt, wenn die Diagnose über die Bedingung B\_cdnws ausgeblendet ist (Definition in %PROKON).

Bei Systemen mit nur einer diagnosefähigen Nockenwelle (z.B. Reihenmotoren, Systeme mit einer gemeinsamen Verstell-einrichtung oder mit nur einem Nockenwellensensor) werden die Bedingungen für die zweite Bank über den Schalter aus der Systemkonstante SY\_PHTWIN gesetzt.

Der Subfunktionblock DNWS\_\* wird für jede Bank einzeln gerechnet. Im nachfolgenden ist nur die Berechnung einer Bank beschrieben. Die Größen für die zweite Bank sind durch eine 2 am Ende gekennzeichnet, z.B. E\_ews2.

subfunctionblock DNWS\_\*:

(valid for both subfunctionblocks  
DNWS\_1 and DNWS\_2)



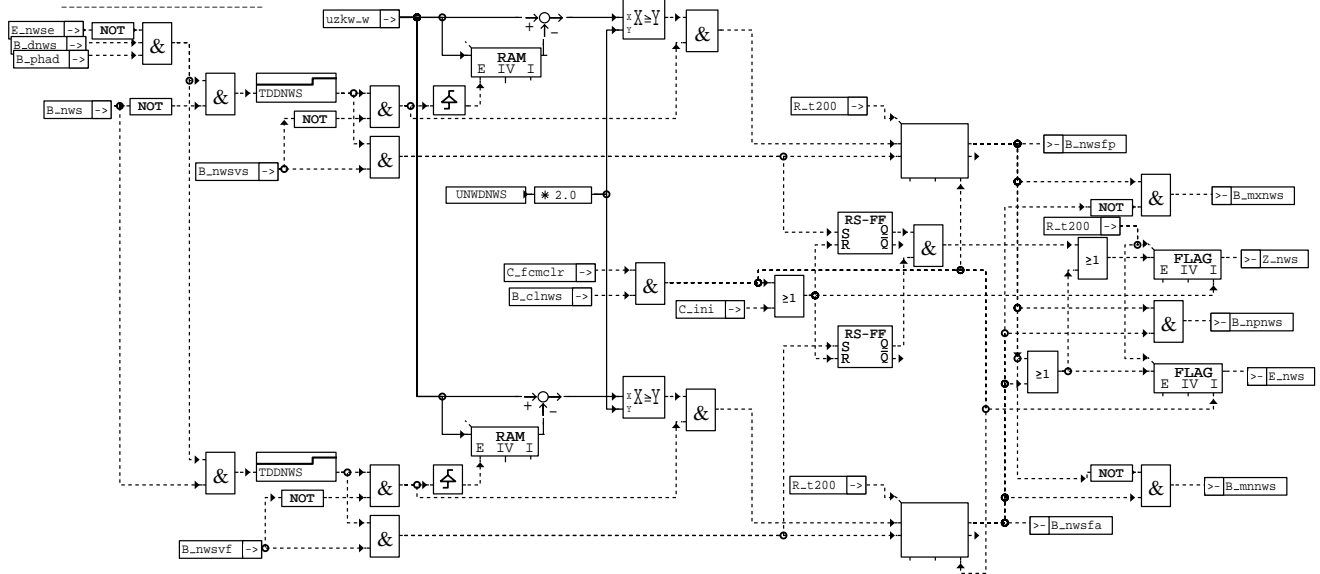
dnws-dnws-1

dnws-dnws-1

Ermittlung der Nockenwellenstellung: aus %NWS: B\_nws = false -----> Passiv-/Spätstellung: B\_nwsvs = true  
B\_nws = true -----> Aktiv-/Frühstellung: B\_nwsvf = true  
undefinierte Stellung: (B\_nwsvs = false) & (B\_nwsvf = false)  
oder: (B\_nwsvs = true) & (B\_nwsvf = true)

Der Verstellwinkel wnwi\_w wird in %WANWKW im Phasen-Interrupt (R\_ph) gebildet. Die Bedingungen B\_nwsvs und B\_nwsvf werden im Hintergrund-Programm zur Verfügung gestellt. Die Nockenwellensteuerung kann auf diese Größen zugreifen und abhängig von der Nockenwellenstellung Maßnahmen ergreifen.

subfunctionblock: DNWS\_E\_\*:



dnws-dnws-e-1

dnws-dnws-e-1



**Bildung der Fehlerbedingung E\_nws\* und der Fehlerart:**

Fehler: B\_mxnws\* Wenn B\_nws=0 anliegt (Passiv- / Spätstellung) und die Sollposition nicht erreicht wird.  
 B\_mnnws\* Wenn B\_nws=1 anliegt (Aktiv- / Frühstellung) und die Sollposition nicht erreicht wird.  
 B\_npnws Wenn sowohl die Passiv-/Spätstellung als auch die Aktiv-/Frühstellung nicht erreicht wurde.  
 E\_nws\*=0 & Z\_nws\*=0 Beide Positionen wurden mindestens einmal angefahren (B\_nws=0 und B\_nws=1) und  
 und beide Sollpositionen sind erreicht worden.

Die Fehlerbedingung E\_nws gibt nur einen Stellerfehler wieder. Wird aufgrund eines Endstufenfehlers nicht verstellt, so führt dies nicht zu einem Fehlereintrag bei E\_nws (siehe hierzu auch %DNWSE).

**Fehlerspeicherverwaltung:**

Status Fehlerpfad NWS:	SFPNWS	Status Fehlerpfad NWS2:	SFPNWS2
Errorflag NWS:	E_nws	Errorflag NWS2:	E_nws2
Zyklusflag NWS:	Z_nws	Zyklusflag NWS2:	Z_nws2
Fehlerart NWS:	B_mxnws	Fehlerart NWS2:	B_mxnws2
	B_mnnws		B_mnnws2
	B_npnws		B_npnws2

Löschen Fehlerpfad:	C_fmclr & B_clnws	Löschen Fehlerpfad:	C_fmclr & B_clnws2
Fehlerpfad NWS :	CDTNWS	Fehlerpfad NWS2 :	CDTNWS2
Fehlerklasse NWS:	CLANWS	Fehlerklasse NWS2:	CLANWS2
Fehlerschwere NWS:	TSFNWS	Fehlerschwere NWS2:	TSFNWS2
Carb-Code NWS:	CDCNWS	Carb-Code NWS2:	CDCNWS2
Umweltbedingungen NWS:	FFTNWS	Umweltbedingungen NWS2:	FFTNWS2

**ABK DNWS 10.60 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CDCNWS	BLOKNR		KL	code word CARB: camshaft control
CDCNWS2	BLOKNR		KL	code word CARB: camshaft control bank 2
CDTNWS			FW	code word tester: camshaft control
CDTNWS2			FW	code word tester: camshaft control (bank 2)
CLANWS			FW	fault class: camshaft control
CLANWS2			FW	fault class: camshaft control bank 2
FFTNWS	BLOKNR		KL	freeze frame table: camshaft control
FFTNWS2	BLOKNR		KL	freeze frame table: camshaft control bank 2
NDNWMN			FW	minimum engine speed for diagnosis camshaft control
NDNWMX			FW	maximum engine speed for diagnosis camshaft control
TDDNWS			FW	distortion time for camshaft control diagnosis enable in end positions
TMDNW			FW	minimum engine temperature for camshaft control diagnosis
TSFNWS			FW	fault active time: camshaft control
TSFNWS2			FW	fault active time: cam shaft control bank 2
TVDNWS			FW	wait time from end of start to DNWS permitted
UNWDNWS			FW	camshaft rotations for debouncing diagnosis NWS
WNWA			FW	limit angle for camshaft actuator active
WNWP			FW	limit angle for camshaft actuator passive
Variable	Source		Type	Description
BLOKNR			EIN	DAMOS source for block number
B_CDNWS	PROKON		EIN	function active per codeword CDNWS
B_CLNWS			EIN	condition clear fault path camshaft control
B_CLNWS2			EIN	condition clear fault path camshaft control 2
B_DNWS	DNWS		AUS	active diagnosis: camshaft control
B_ENWS	DNWS		AUS	condition error camshaft control
B_FA			EIN	condition general function request
B_FANWS			EIN	condition general function request for diagnosis camshaft control
B_MNNWS	DNWS		AUS	fault type: camshaft control advanced position not reached
B_MNNWS2	DNWS		AUS	fault type: camshaft control 2 advanced position not reached
B_MXNWS	DNWS		AUS	fault type: camshaft control retarded position not reached
B_MXNWS2	DNWS		AUS	fault type: camshaft control 2 retarded position not reached
B_NPNWS	DNWS		AUS	fault type camshaft control undefined position
B_NPNWS2	DNWS		AUS	fault type camshaft control 2 undefined position
B_NWS	NWS		EIN	Condition camshaft control
B_NWSFA	DNWS		AUS	condition NWS actuator diagnosis fault in active position
B_NWSFA2	DNWS		AUS	condition NWS actuator diagnosis fault in active position of camshaft 2
B_NWSFP	DNWS		AUS	condition NWS actuator diagnosis fault in passive position
B_NWSFP2	DNWS		AUS	condition NWS actuator diagnosis fault in passive position of camshaft 2
B_NWSVF	DNWS		AUS	condition camshaft control in advanced end position
B_NWSVF2	DNWS		AUS	condition camshaft control of bank 2 in advanced end position
B_NWSVS	DNWS		AUS	condition camshaft control in retarded end position
B_NWSVS2	DNWS		AUS	condition camshaft control of bank 2 in retarded end position
B_PHAD	WANWKW		EIN	adaptation crankshaft/camshaft performed
B_PHAD2	WANWKW		EIN	adaptation crankshaft/camshaft 2 performed
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_JNISYN			EIN	ECU-condition for intialisation of angle synchronization
C_SYN			EIN	ECU-condition angle synchronization available
E_BM	DDG		EIN	error flag: reference mark sensor
E_NWS	DNWS		AUS	error flag: camshaft control
E_NWS2	DNWS		AUS	error flag: camshaft control bank 2





Variable	Source	Type	Description
E_NWSE	DNWSE	EIN	error flag: power stage of camshaft control valve
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
NMOT	SWADAP	EIN	engine speed
R_T200		EIN	Time schedule 200 ms
SFPNWS	DNWS	AUS	status fault path: camshaft control
SFPNWS2	DNWS	AUS	status fault path: camshaft control bank 2
SY_NWS	PROKON	EIN	system constant camshaft control: none, 2 point or continuous
SY_PHTWIN	PROKON	EIN	system constant 1/2 phase sensing system (sensor, wheel)
TMOT	SWADAP	EIN	Engine temperature
TNST_W	BBSTT	EIN	time after end of start
UZKW_W	GGDPG	EIN	revolution counter crankshaft
WNWIAW2_W	NWS	EIN	
WNWIAW_W	NWS	EIN	
Z_NWS	DNWS	AUS	cycle flag: camshaft control
Z_NWS2	DNWS	AUS	cycle flag: camshaft control bank 2

### FW DNWS 10.60 Fixed Values

Parameter	Value	Description
CDTNWS		code word tester: camshaft control
CDTNWS2		code word tester: camshaft control (bank 2)
CLANWS		fault class: camshaft control
CLANWS2		fault class: camshaft control bank 2
NDNWMN		minimum engine speed for diagnosis camshaft control
NDNWMX		maximum engine speed for diagnosis camshaft control
TDDNWS		distortion time for camshaft control diagnosis enable in end positions
TMDNW		minimum engine temperature for camshaft control diagnosis
TSFNWS		fault active time: camshaft control
TSFNWS2		fault active time: cam shaft control bank 2
TVDNWS		wait time from end of start to DNWS permitted
UNWDNWS		camshaft rotations for debouncing diagnosis NWS
WNWA		limit angle for camshaft actuator active
WNWP		limit angle for camshaft actuator passive

### FB DNWS 10.60 Detailed description of function

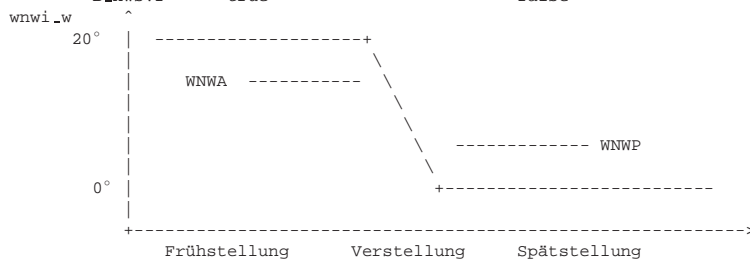
Diese Diagnose berücksichtigt V-Motoren mit 2-Banksystemen mit je einer verstellbaren Einlaßnockenwelle pro Bank. Bei der Verstellung gibt es die 2 Sollzustände "passiv" (B\_nws=0) und "aktiv" (B\_nws=1). Die Istzustände werden in den Bedingungen B\_nwsvs (passiv/spät) bzw. B\_nwsvf (aktiv/früh) wiedergegeben.

1. Für NWS : Der Verstellwinkel wnwi\_w gibt die Verstellung der Nockenwelle 1 an.
2. Für NWS2: Der Verstellwinkel wnwi2\_w gibt die Verstellung der Nockenwelle 2 an.

Darstellung der Eingangssignale wnwi\_w, B\_nws und der Zeiger über die gemessene Istposition B\_nwsvs, B\_nwsvf:

Beispielwerte: Nockenwellenverstellwinkel: wnwi\_w = 0 (B\_nws=0) bis 20 Grad KW (B\_nws=1)

Stellsignal aus %NWS:	B_nws	true	false
Istposition aus %DNWS:	B_nwsvs	false	true
	B_nwsvf	true	false





Ablauf:	Freigabe Diagnose	spät und früh ok	Spätposition nicht erreicht	Fehlereintrag spät	spät wieder ok
B_dnws	-----+ .	.	.	.	.
B_nwsfp	-----+ .	.	.	.	.
Entprellung in NWU: .<-- UNWDNWS -->					
kein Fehler	-----+ .	.	.	.	.
B_mxnws	-----+ .	.	.	.	.
B_mnnws	-----+ .	.	.	.	.
Z_nws	-----+ .	.	.	.	.
E_nws	-----+ .	.	.	.	.

## APP DNWS 10.60 Application hint

Anhaltswerte für Erstapplikation:

TVDNWS:	10 sec		
NDNWMX:	4500 U/min		
NDNWMN:	700 U/min ( < Leerlaufdrehzahl)		
TMDNW:	50°C		
TDDNWS:	1 sec		
UNWDNWS:	4 NWU		
WNWP:	9 °KW (bei Nockenwellen-Verstellwinkel: 21°)		
WNWA:	12 °KW (bei Nockenwellen-Verstellwinkel: 21°)		
CDTNWS:	174	CDTNWS2:	178
CLANWS*:	3		
TSFNWS*:	255		
CDCNWS:	-	CDCNWS2:	-
FFTNWS*:	nmot, ub		

### Funktionsprüfung:

Bei der Funktionsprüfung ist jede Bank getrennt zu untersuchen. Hierzu ist nachfolgende Prüfung durchzuführen:

#### 1. Meßgrößen: Prüfung, ob alle Ramzellen und Labels per VS100 verfügbar.

digitale Größen: nmot, tmot, E\_tm, tnst\_w, B\_dnws, B\_phad\*, wnwi\_w, B\_nwsvs\*, B\_nwsvf\*, E\_nwse, B\_nws, uzkw\_w, B\_nwsfp\*, B\_nwsfa\*, B\_mnnws\*, B\_mxnws\*, B\_npnws\*, E\_nws\*, Z\_nws\*  
Labels: alle Labels aus ABK-Liste  
Meßdatenerfassung: Erfassung per VS100 - VSO

#### 2. Meßreihe:

Um die Nockenwellenverstellung einfach auszulösen, ist das Verstellkennfeld in %NWS im Leerlaufbereich (untere Drehzahl, untere Last) auf Frühverstellung zu setzen. Über den Leerlaufschalter (B\_ll) kann dann die Nockenwellenverstellung einfach per Gaspedal ausgelöst werden.  
Alternativ ist die Verstellung über B\_fa und B\_fanws möglich, falls diese Größen in der Funktion %NWS zur Ansteuerung der Nockenwellenverstellung für Prüfzwecke eingebunden ist.

##### 2.1 Prüfung der Diagnose-Freigabe über B\_dnws:

- Änderung der Labels NDNWMX, NDNWMN, TMDNW so, daß das Ein-/Ausschalten von B\_dnws bei der aktuellen Drehzahl nmot und Temperatur tmot verursacht wird.
- Prüfung, ob im Nachstart bei Erreichen der Nachstartzeit tnst\_w=TVDNWS B\_dnws gesetzt wird.
- Ausschalten B\_dnws über E\_tm: Ändern der oberen Temperaturschwelle in %GGTFM um E\_tm zu setzen.

##### 2.2 Prüfung der Bedingungen für Früh- und Spätverstellung: B\_nwsvf, B\_nwsvs

- Plausibilität B\_phad (true) und wnwi\_w (0..max. Verstellwinkel in °KW) prüfen: sonst %WANWKW überprüfen;
- Leerlauf (Spätstellung) / Teillast (Frühstellung) führt zur Änderung von wnwi\_w und zum abwechselnden Setzen von B\_nwsvs und B\_nwsvf

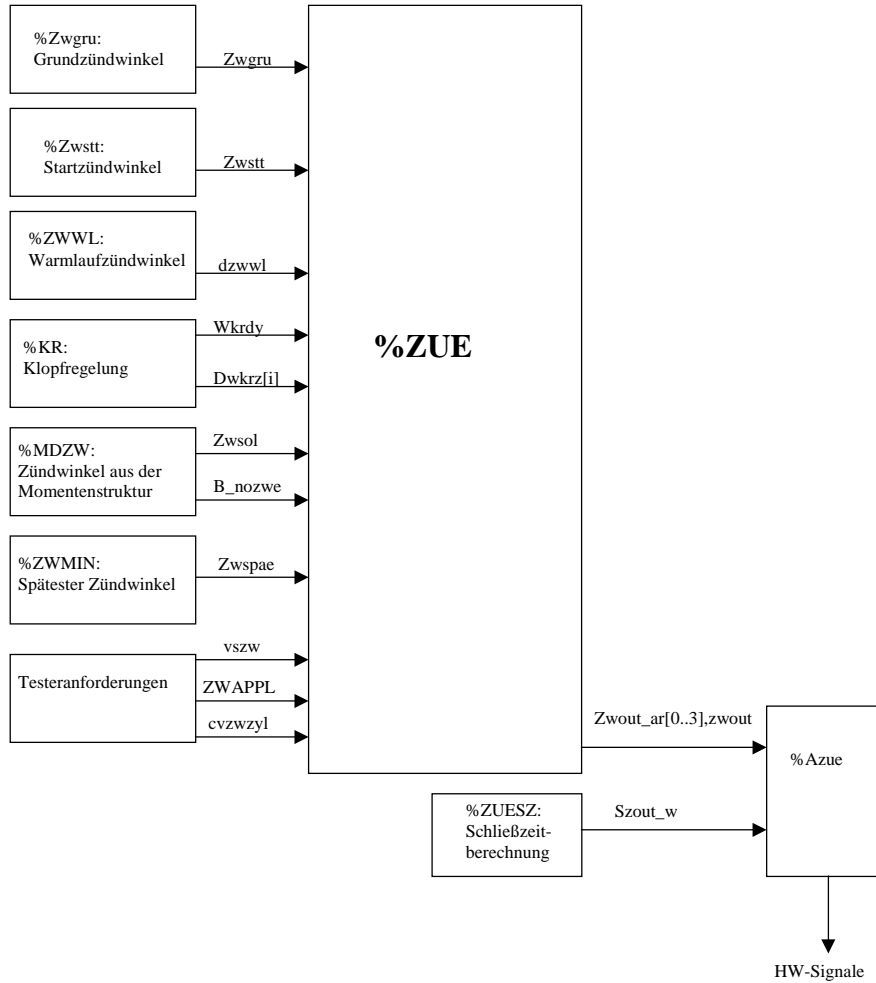
##### 2.3 Prüfung der Bedingungen für Fehler Aktiv/Früh- und Passiv/Spätverstellung: B\_nwsfa, B\_nwsfp

- Wechseln in Spätstellung (Leerlauf) / Frühstellung (Teillast) und WNWP= 9°, WNWA= 12°  
-----> B\_nwsfp=false, B\_nwsfa=false, B\_\*nws=false, E\_nws=false, Z\_nws=true;
- In Spätstellung (Leerlauf) WNWP= -10°, WNWA= 12° setzen  
-----> B\_nwsfp=true, B\_nwsfa=false, B\_mxnws=true, E\_nws=true, Z\_nws=true;
- In Frühstellung (Teillast) WNWP= 9°, WNWA= 50° setzen  
-----> B\_nwsfp=false, B\_nwsfa=true, B\_mnnws=true, E\_nws=true, Z\_nws=true;
- Wechseln in Spätstellung (Leerlauf) / Frühstellung (Teillast) und WNWP= -10°, WNWA= 50°  
-----> B\_nwsfp=true, B\_nwsfa=true, B\_npnws=true, E\_nws=true, Z\_nws=true;

## ZUE 258.130 Basic function - ignition

### FDEF ZUE 258.130 Function definition

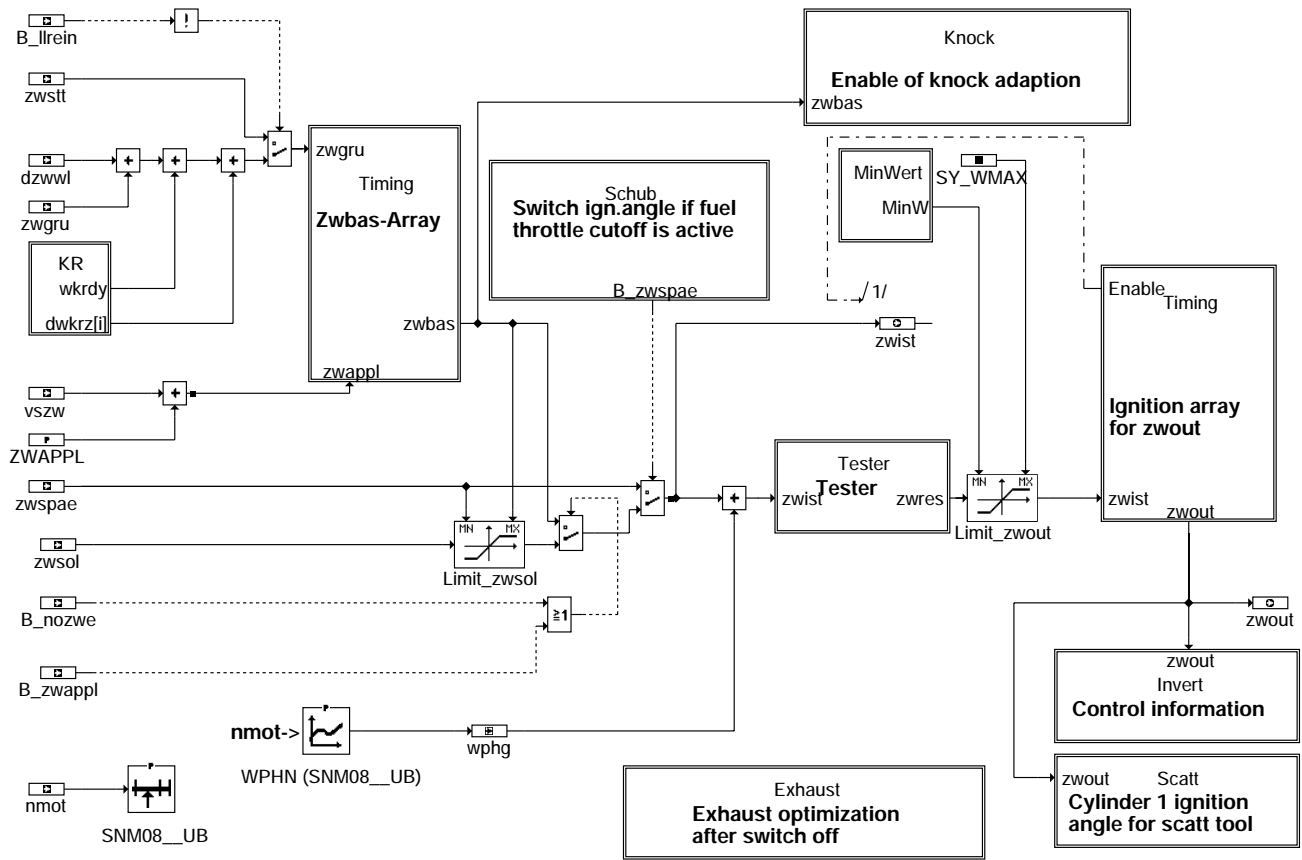
#### Übersicht Zündung:



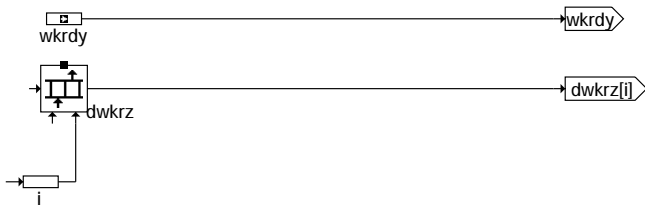
zue-uebers

zue-uebers

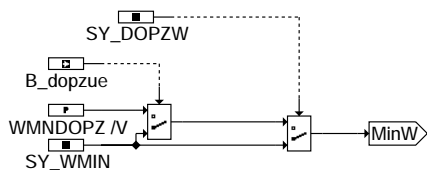
Source: ZUE 258.130



zue-main

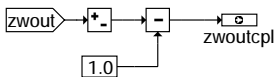


zue-kr



**If limp-home function for cylinder-synchronisation is active, the latest possible ignition angle has to be limited to earlier limits. In case of a limp-home function ignition signals are outputted in a 360° interval instead of 720° this can lead to an ignition into the opened inlet valve if ignition angle is too late during gas exchange.**

zue-minwert



**Complement of zwout is needed for the supervisory module to make a plausibility check**

**Control information**

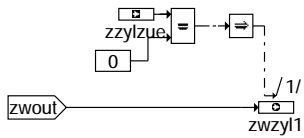
zue-invert

zue-main

zue-kr

zue-minwert

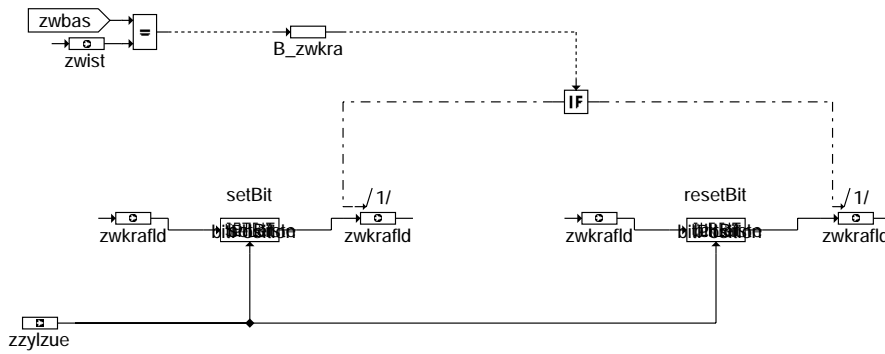
zue-invert



**Ignition angle for cylinder 1  
is needed for scatt tool**

### Cylinder 1 ignition-angle for scatt-tool

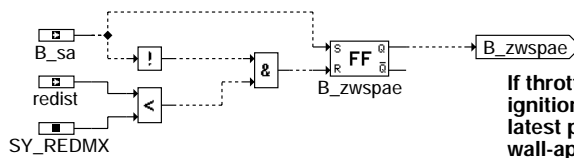
zue-scatt



Bit **B\_zwkra** is set if **zwist** equals **zwbas**. If **B\_zwkra** is set a cylinderspecific bit inside flag byte **zwkrafld** is also set. **B\_zwkra = TRUE** means that knock control is able to control the ignition angle.

### Enable of knock adaptation

zue-knock

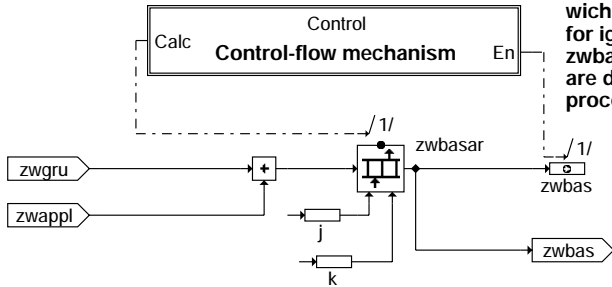


If throttle fuel cutoff is active the ignition angle is switched to the latest possible angle in order to ignite wall-applied fuel film with best burning conditions for the catalyst

Switch ign. angle if fuel throttle cutoff is active

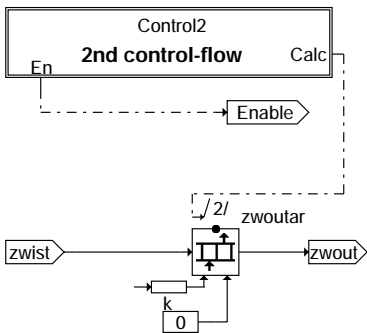
zue-schub

Because of dwell-time overlapping an ignition angle array is needed. The **zwbas**-array is calculated in the synchro-task in a process before calculation of torque-coordination. **zwsol** is calculated out of torque-coordination which is based on **zwbas** as reference for ignition-angle efficiency. **zwbas**, **zwsol** and the phase shift **wphn** are defining **zwout** which is calculated in a synchro process after torque coordination.



### zwbas-array

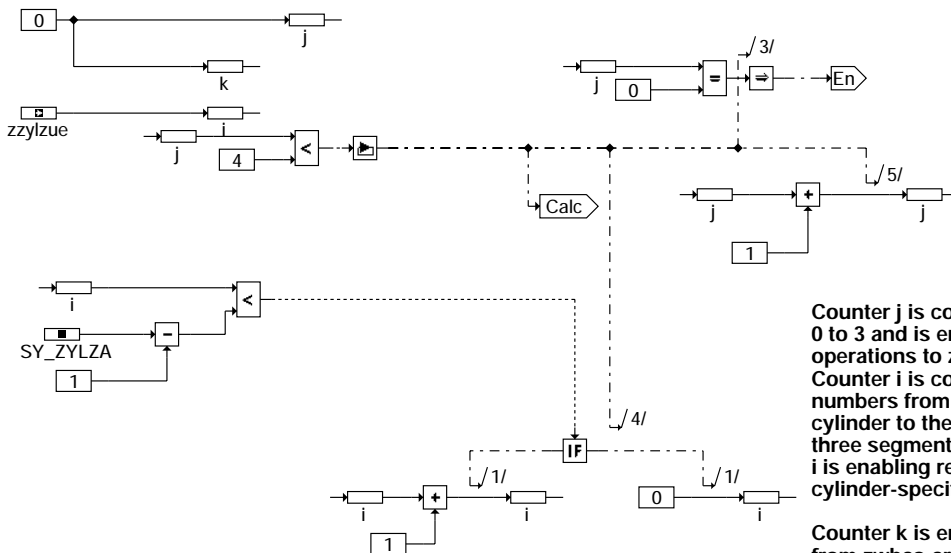
zue-timing1



For overlapping mode a four element ignition array is needed. The **zwout**-array is calculated in a special **zwout**-sequence after calculation of **zwbas**.

### Ignition array for zwout

zue-timing2



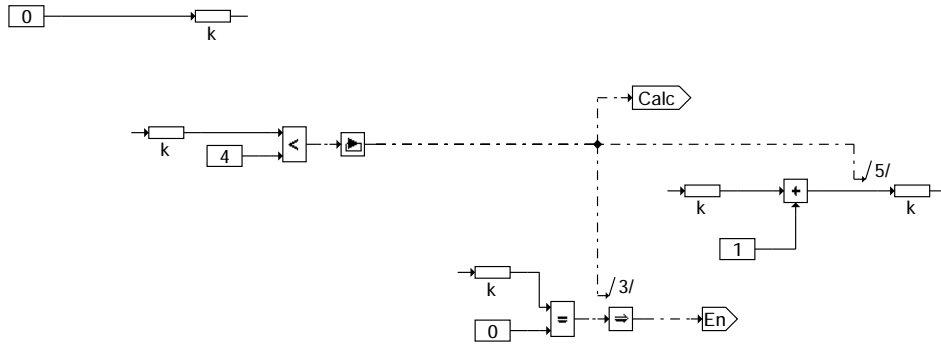
Counter **j** is counting from 0 to 3 and is enabling write operations to **zwbas**-array. Counter **i** is counting cylinder numbers from the latest cylinder to the cylinder number three segments ahead. Counter **i** is enabling read-operations from cylinder-specific knock-offsets.

Counter **k** is enabling read-operations from **zwbas**-array and is set to 0 in order to start read-operations at element 0.

The control flow sequence is calculated in process **syn\_zwbas** this means that the mentioned counters are active before torque-coordination starts.

### Control-flow mechanism

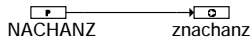
zue-control



Counter k is calculated in a angle synchronous process after torque-coordination. kth element zwout-array is calculated out of kth element of zwbas-array zwsol and zwspae. If k equals zero zwist and zwout are calculated out of element 0 of zwbasar.

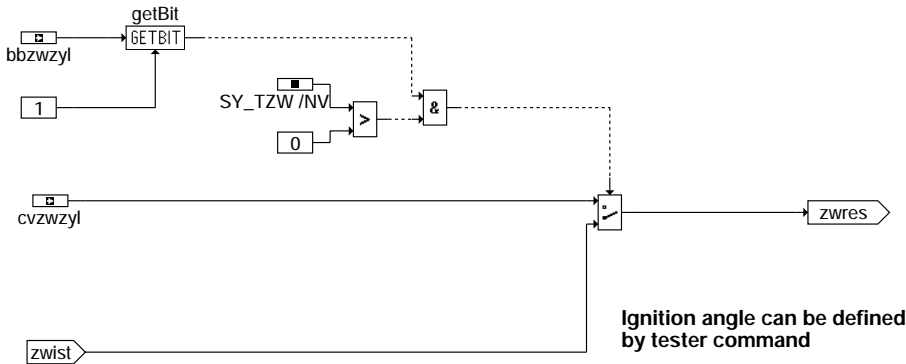
### 2nd control-flow

#### zue-control2



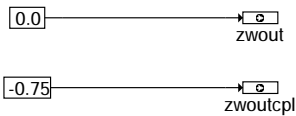
### Exhaust optimization after switch off

#### zue-exhaust



### Tester

#### zue-tester



#### zue-initialize

### ABK ZUE 258.130 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SNM08_UB	NMOT		SV	Base point distribution engine speed, 8 base points
SY_DOPZW			SYS (REF)	System constant doubled ignition output included
SY_REDMX			SYS (REF)	system constant: max. cylinder cutoff step
SY_TZW			SYS (REF)	System constant tester manipulation of zwist included
SY_WMAX			SYS (REF)	System constant earliest ignition timing that can be outputted
SY_WMIN			SYS (REF)	System constant latest ignition timing that can be outputted
SY_ZYLZA			SYS (REF)	system constant number of cylinders
WMNDOPZ			FW	Latest ignition angle at limp-home mode for phase detection
WPHN	NMOT		KL	phase correction
ZWAPPL			FW	Applications interface ignition angle adjustment



Variable	Source	Type	Description
BBZWZYL		EIN	Condition Flag ingition angle manipulation by tester
B_DOPZUE	NLPH	EIN	Condition double ignition
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_NOZWE	MDZW	EIN	condition no ignition angle intervention of torque structure
B_SA	MDRED	EIN	Condition fuel cut-off
B_ZWAPPL	PROKON	EIN	Condition ignition-timing applications without torque intervention
B_ZWKRA	ZUE	LOK	condition: ignition angle of the KC is active
CVZWZYL		EIN	device control value ignition
DWKRZ	KRRA	EIN	cyl.-spec. ignition-timing retardation with retardation for dynamics
DZWWL	ZWWL	EIN	delta ignition angle from warm-up
NMOT	SWADAP	EIN	engine speed
REDIST	BGEVAB	EIN	real cylinder cut-off step
VSZW	VS_VERST	EIN	Ignition-timing correction by adjusting system
WKRDY	KRDY	EIN	ignition retard during dyn-function of knock control
WPHG	ZUE	LOK	ignition angle DG phase correction
ZNACHANZ	ZUE	AUS	Amount of ignitions after KL15 off
ZWBAS	ZUE	AUS	basic ignition angle
ZWBASAR	ZUE	AUS	basic ignition angle array
ZWGRU	ZWGRU	EIN	basic ignition angle
ZWIST	ZUE	AUS	real ignition angle
ZWKRAFLD	ZUE	AUS	bit pattern of the cylinder-individually stored B.zwkra
ZWOUT	ZUE	AUS	Ignition angle output value
ZWOUTAR	ZUE	AUS	Ignition angle output array
ZWOUTCPL	ZUE	AUS	Single complement of the ignition angle for function monitoring
ZWSOL	MDZW	EIN	desired ignition angle from torque intervention
ZWSPAЕ	ZWMIN	EIN	retarded ignition angle
ZWSTT	ZWSTT	EIN	Ignition angle during start
ZWZYL1	ZUE	AUS	ignition angle cylinder 1
ZZYLZUE		EIN	SW-zylinder counter for ignition calculation

### FW ZUE 258.130 Fixed Values

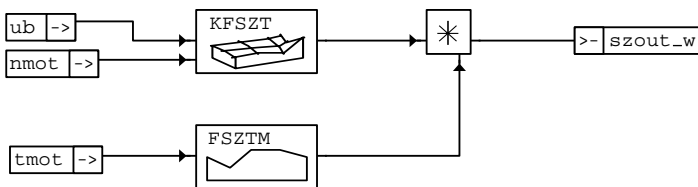
Parameter	Value	Description
WMNDOPZ		Latest ignition angle at limp-home mode for phase detection
ZWAPPL		Applications interface ignition angle adjustment

### FB ZUE 258.130 Detailed description of function

### APP ZUE 258.130 Application hint

## ZUESZ 1.50 Ignition, calculation of coil closing time

### FDEF ZUESZ 1.50 Function definition



zuesz-zuesz

### ABK ZUESZ 1.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CW_FUBND			FW	Code word for interval ignition
FFLDZ	UB		KL	Follow-on ignition charging time
FSZTM	TMOT		KL	Factor dwell angle correction tmot depending
FTMFFANZ	TMOT		KL	Follow-on ignition weighting factor
FUBAOF			FW	Opening time for interval ignition
FWNMOT			FW	Turn on limit nmot for interval ignition
KFFFANZ	NMOT	TMOT	KF	Number of sequential sparks
KFFFANZUB	UB	NMOT	KF	Number of sequential sparks
KFSZT	UB	NMOT_W	KF	Dwell angle characteristic map
SY_FFZ			SYS (REF)	system constant interval ignition
SY_ME7			SYS (REF)	system constant ECU
SY_TZW			SYS (REF)	System constant tester manipulation of zwist included
SZOUTMIN			FW	Minimum dwell time

Variable	Source	Type	Description
BBZWZYL		EIN	Condition Flag ingition angle manipulation by tester
B_FF	ZUESZ	AUS	Condition sequential sparks ignition
CVFUBAANZ		EIN	
CVOFFZ_W		EIN	





Variable	Source	Type	Description
CVSZFUBA_W		EIN	
FUBAANZ	ZUESZ	AUS	Amount of ignitions
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
OFFZ_W	ZUESZ	AUS	Opening time
SZFUBA_W	ZUESZ	AUS	dwel time interval ignition
SZOUT_W	ZUESZ	AUS	dwel time
SZTCALC_W	ZUESZ	AUS	Dwell period in timer 1 increments
TMOT	SWADAP	EIN	Engine temperature
UB	SWADAP	EIN	battery voltage

### FW ZUESZ 1.50 Fixed Values

Parameter	Value	Description
CW_FUBND		Code word for interval ignition
FUBAOF		Opening time for interval ignition
FWNMOT		Turn on limit nmot for interval ignition
SZOUTMIN		Minimum dwell time

### FB ZUESZ 1.50 Detailed description of function

#### 1. Introduction:

Sufficient ignition energy must be made available in order that the sparking plug can ignite the mixture. This is realized by closing the primary circuit of the ignition coil in good time so that the coil can charge up sufficiently. On the other hand, the closing time shall not be too long as this can otherwise lead to the ignition output stage overheating (particularly critical for internal output stages). After closing, the primary current  $i$  increases exponentially with time. The period of time from the primary circuit closing to opening again (sparking) is referred to as the dwell time.

The energy stored in the magnetic field is given by :

$$W = 1/2 * L * i^2 \quad (L: \text{inductance, } i: \text{current flowing at the point in time that the primary circuit opens})$$

#### 2. Calculation of the dwell time:

The dwell time  $szout$  is calculated from a map that depends on the speed and battery voltage, corrected by a factor depending on the engine temperature (from characteristic  $FSZTM$ ).

#### 3. Dependency of the dwell time:

- ub: The primary current  $i$  flows through the primary winding of the ignition coil. This is determined by the battery voltage  $ub$  and the resistance of the coil.
- nmot: Above an engine-speed threshold, the dwell time is computed as a dwell angle and output at an angle level. Thus a speed-dependent lead by the dynamics is required here so that a sufficiently long dwell time is still given even in the event of maximum speed dynamics. The dynamics lead is taken into account in the map  $KFSZT$ . The dynamics lead required is lower at higher engine speeds. No dynamics lead is necessary in the lower engine-speed range (dwell time output). It can also be meaningful to have a shorter dwell time at higher speeds for thermal reasons.
- tmot: The ignition coil temperature changes with the engine temperature.



## APP ZUESZ 1.50 Application hint

If the dwell time is too short, then the energy will not suffice to ignite the mixture.  
A dwell time that is too long can endanger the ignition output stages.

Application proposal:

Data from a 8-cylinder engine: For KFSZT:

	4.99	6.03	8.01	9.99	11.96	14.04	16.01	17.05
50.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
150.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
450.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
675.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
1000.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
2000.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
3000.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15
6350.	19.97	19.86	7.17	4.81	3.58	2.76	2.25	2.15

BLOCK ANM

TEXT/ANF

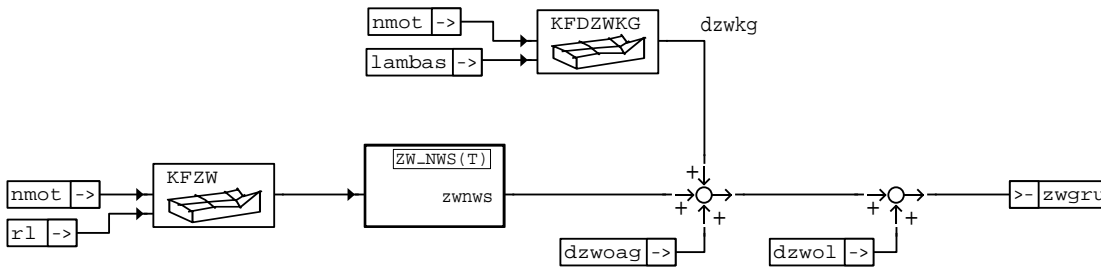
RAM cell	Physical range	Quantization	Calc. freq.	Init value	Remarks
szout_w	0...6553.5 ms	16 bit, 0.1 ms	20 ms	0	

In the SW module szout\_w is converted or re-quantized into the corresponding timer quantization.  
The minimum value of szout\_w is still limited to 0.3 ms, i.e. szout\_w is always > 0.3 ms.

Parameter	Physical range	Permiss. range	Quantization	Calc. frequency	Remarks
KFSZT	0...25.5 ms		8 bit, 0.1 ms	20 ms	
FSZTM	0...2		8 bit, 0.0078	20 ms	

## ZWGRU 19.30 Basic ignition angle

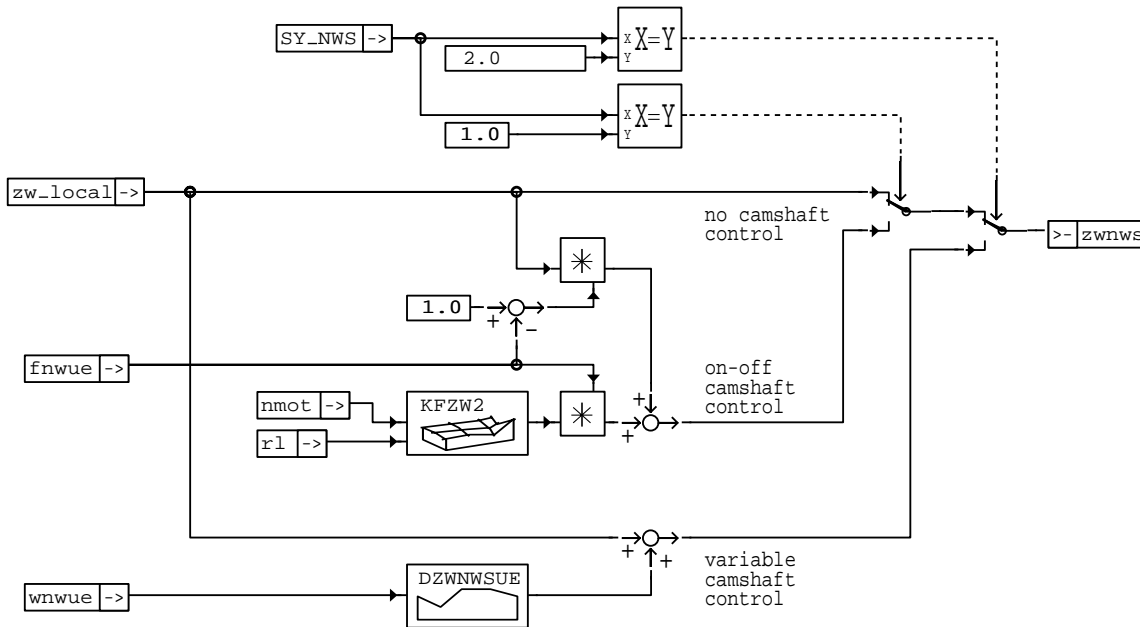
### FDEF ZWGRU 19.30 Function definition



zwgru-zwgru

zwgru-zwgru

Teilfunktion ZW\_NWS: Berücksichtigung einer ggf. vorhandenen 2-Punkt- oder stetigen Nockenwellensteuerung



zwgru-zw-nws

zwgru-zw-nws

### ABK ZWGRU 19.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DZWNWSUE	WNWUE		KL	Delta ignition angle dependent on the camshaft overlap
KFDZWKG	NMOT	LAMBAS	KF	ignition angle correction due to knock limit shift
KFZW	NMOT	RL	KF	Ignition advance-angle characteristic map
KFZW2	NMOT	RL	KF	Ignition angle performance characteristics variant 2

Variable	Source	Type	Description
DZWKG	ZWGRU	LOK	delta ignition angle knock limit shift
DZWOAG	MDBAS	EIN	exhaust recirculation rate-dependent correction of optimum ignition angle
DZWOL	MDBAS	EIN	Lambda-dependent correction of optimum ignition angle
FNWUE	NWS	EIN	Weighting factor camshaft overlap
LAMBAS	SWADAP	EIN	basic Lambda
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
SY_NWS	PROKON	EIN	system constant camshaft control: none, 2 point or continuous
WNWUE	NWS	EIN	camshaft overlap angle of inlet and outlet valve opening
ZWGRU	ZWGRU	AUS	basic ignition angle
ZWNWS	ZWGRU	LOK	basic ignition angle with camshaft control

### FW ZWGRU 19.30 Fixed Values

Parameter	Value	Description
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### FB ZWGRU 19.30 Detailed description of function

Bereitstellung des Grundzündwinkels aus dem Kennfeld KFZW. Die Teilfunktion ZW\_NWS beschreibt die Berücksichtigung einer ggf. vorhandenen Nockenwellensteuerung (NWS). Bei 2-Punkt-NWS wird über den Faktor fnwue stetig zwischen KFZW und dem Kennfeld KFZW2 umgeschaltet. Im Fall einer stetigen NWS wird abhängig vom Überschneidungswinkel wnwue eine Zündwinkelkorrektur DZWNWSUE zu KFZW addiert. Die jeweils gültige NWS-Variante wird über die Systemkonstante SY\_NWS bei der SW-Erstellung festgelegt:

```

SY_NWS = 0:   keine NWS
           = 1:   2-Punkt-NWS
           = 2:   stetige NWS
           > 2:   nicht definiert.
    
```

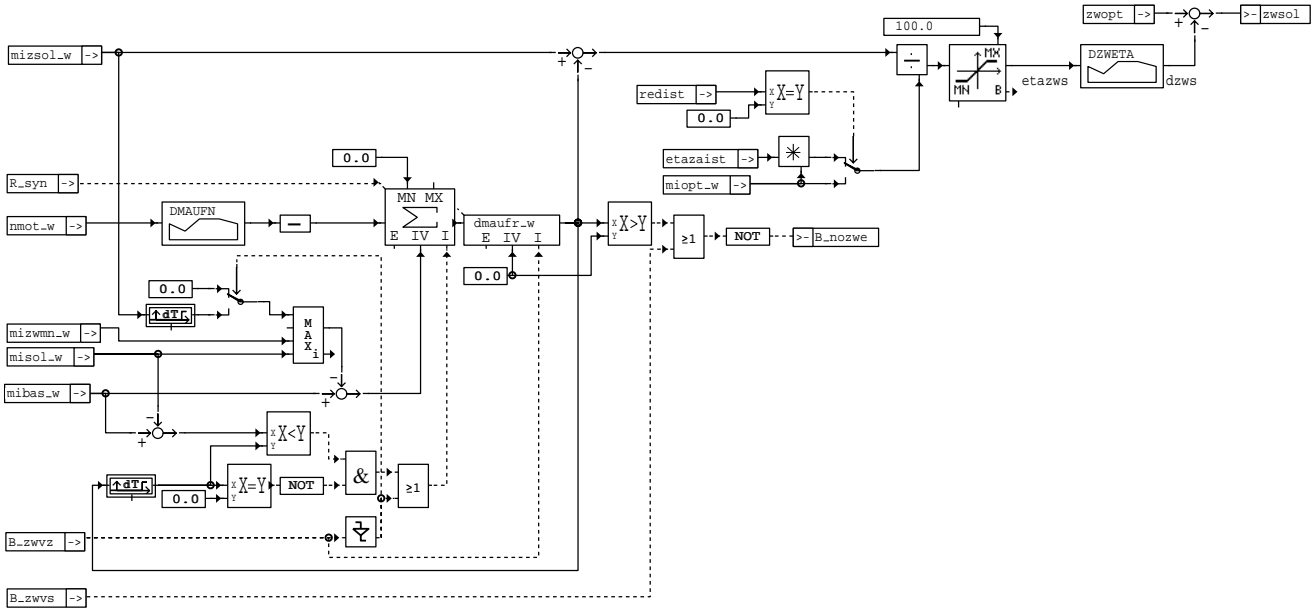
Die SW wird bedingt übersetzt, d.h. es ist immer nur eine Variante im EPROM vorhanden. SY\_NWS ist nicht im EPROM nicht applizierbar. Durchführung der gleichen additiven Zündwinkelkorrekturen wie bei der Berechnung des optimalen Zündwinkels (siehe %MDBAS), d.h. Berücksichtigung von AGR- und Lambdaabhängigkeit. Die Temperaturabhängigkeit wird in einer gesonderten Funktion (%ZWWL) berücksichtigt.

## APP ZWGRU 19.30 Application hint

Die Kennfelder KFZW, ~2 werden bei betriebswarmen Motor für die jeweilige NWS-Position appliziert, AGR inaktiv, Lambda=1. Falls der Motor nicht klopft, Eintrag des optimalen Zündwinkels. Bei Klopfendem Motor Eintrag der Klopfgrenze.

## MDZW 1.120 Calculation of torque in nominal ignition timing

### FDEF MDZW 1.120 Function definition



mdzw-mdzw

### ABK MDZW 1.120 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DMAUFN	NMOT_W		KL	delta torque rise after torque intervention
DZETA	ETAZWS		KL	delta ignition angle from efficiency
Variable	Source		Type	Description
B_NOZWE	MDZW		AUS	condition no ignition angle intervention of torque structure
B_ZWVS	MDKOG		EIN	condition for fast external ignition angle intervention of torque interface
B_ZWVZ	MDKOG		EIN	condition for ignition angle intervention of torque interface
DMAUFR_W	MDZW		LOK	delta torque rise
DZWS	MDZW		LOK	difference ignition timing (between zwopt and zwsol)
ETAZAIST	MSF		EIN	actual cylinder masking effectiveness
ETAZWS	MDZW		LOK	nominal ignition angle effectiveness
MIBAS_W	MDBAS		EIN	indicated basic torque
MIOPT_W	MDBAS		EIN	optimum indicated torque
MISOL_W	MSF		EIN	indicated resultant nominal torque
MIZSOL_W	MSF		EIN	indicated resultant nominal torque for ignition angle intervention
MIZWMN_W	MDRED		EIN	indicated engine torque at the latest spark angle
NMOT_W	SWADAP		EIN	engine speed
REDIST	BGEVAB		EIN	real cylinder cut-off step
R_SYN	GGDPG		EIN	Synchro schedule
ZWOPT	MSF		EIN	optimal ignition angle
ZWSOL	MDZW		AUS	desired ignition angle from torque intervention

### FW MDZW 1.120 Fixed Values

Parameter	Value	Description
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## FB MDZW 1.120 Detailed description of function

With the calculation of the desired ignition angle three cases have to be considered:

1. Torque intervention through ignition angle active (B\_zwvs=1)
2. Turning-off of torque intervention after being active (B\_zwvs=0, dmaufr\_w>0)
3. Torque intervention not active (B\_nozwe=1)

### 1. Active torque intervention

The condition B\_zwvs is set and the condition for deactivation of ignition angle intervention B\_nozwe is false. The desired ignition angle is being calculated from the torque request mizsol\_w for the ignition angle path. The contribution of the ramp of torque rise dmaufr\_w is zero.

The torque request mizsol\_w is converted to the nominal ignition angle effectiveness etazws. This occurs through division by the optimum torque, which is calculated by multiplying miopt\_w by the effectiveness etazaist. The nominal ignition angle effectiveness etazws is converted to a delta ignition angle dzws using the inverted characteristic curve DZWETA. From the difference between the optimal ignition angle zwopt and dzws the nominal ignition angle zwsol is calculated.

### 2. Turning-off of torque intervention

When the torque intervention is turned off (B\_zwvs=1 -> 0, see function %MDKOG) the nominal torque mizsol\_w can jump to a higher value. This jump has to be prevented because of driveability. For that in the moment B\_zwvs turns zero a ramp dmaufr\_w is started, which is initialized with the height of the jump and declines with speed dependent velocity until it turns zero. This ramp is subtracted from mizsol\_w and produces a smooth transition into the state without ignition intervention. In this state B\_zwvs is false. However the turn-off condition for ignition intervention B\_nozwe is not set until after the ramp is run out.

A special case is the anti-jerk intervention in which B\_zwvs, but not B\_zwvsz is set. If the torque request of the anti-jerk function ceases there is no jump in the input variable mizsol\_w. Therefore no turn-off ramp is necessary.

### 3. Torque intervention not active

In this case no request is active (B\_zwvs=0) and the ramp dmaufr\_w came to an end. The turn-off condition for the ignition angle intervention B\_nozwe is set. The nominal ignition angle zwsol is not considered by the ignition (see %ZUE) and its calculation can therefore be omitted.

## APP MDZW 1.120 Application hint

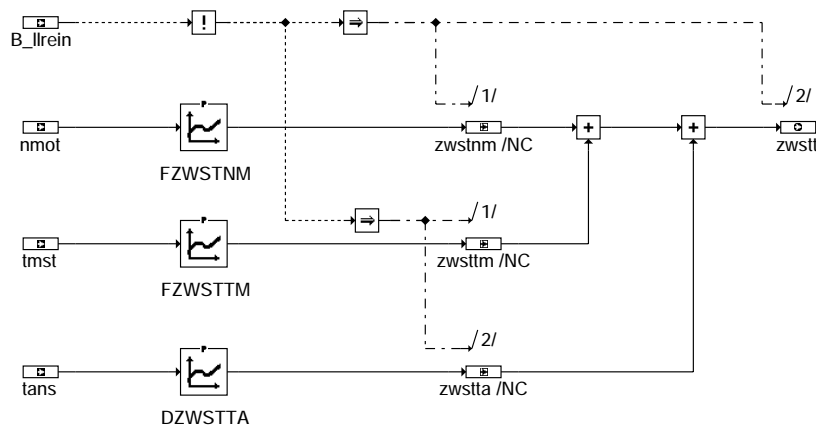
The characteristic DZWETA is the inverse of the characteristic ETADZW.

The data in DMAUFN have to be chosen preliminary in such a way that there is a gradient of approximately 5%/sec.

## ZWSTT 4.20 Igniton at start

### FDEF ZWSTT 4.20 Function definition

Source: ZWSTT 4.20



zwstt-main



zwstt-initialize

zwstt-main

zwstt-initialize



### ABK ZWSTT 4.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DZWSTTA	TANS		KL	Delta ignition angle during start
FZWSTNM	NMOT		KL	Ignition angle during start
FZWSTTM	TMST		KL	Ignition angle during start

Variable	Source	Type	Description
B.LLREIN	LLRMD	EIN	Condition idle speed control is active
NMOT	SWADAP	EIN	engine speed
TANS	SWADAP	EIN	Intake air temperature
TMST	GGTFM	EIN	engine temperature at start
ZWSTNM	ZWSTT	LOK	ignition angle during start nmot-dependent part
ZWSTT	ZWSTT	AUS	Ignition angle during start
ZWSTTA	ZWSTT	LOK	ignition angle during start tans-dependent part
ZWSTTM	ZWSTT	LOK	ignition angle during start tmst-dependent part

### FW ZWSTT 4.20 Fixed Values

Parameter	Value	Description
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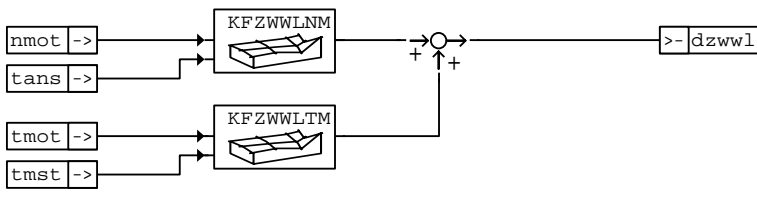
### FB ZWSTT 4.20 Detailed description of function

At start the ignition angle output value zwout is the result of zwstt and the ignition angle DG phase correction wphg (see %ZUE). The ignition angle during start zwstt is calculated until B.llrein is true.

### APP ZWSTT 4.20 Application hint

### ZWWL 4.10 Ignition during warm-up

#### FDEF ZWWL 4.10 Function definition



zwwl-zwwl

### ABK ZWWL 4.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFZWWLNM	NMOT	TANS	KF	Delta ignition sparc advance during engine warm up phase
KFZWWLTm	TMOT	TMST	KF	Delta ignition sparc advance during engine warm up phase

Variable	Source	Type	Description
DZWWL	ZWWL	AUS	delta ignition angle from warm-up
NMOT	SWADAP	EIN	engine speed
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start

### FW ZWWL 4.10 Fixed Values

Parameter	Value	Description
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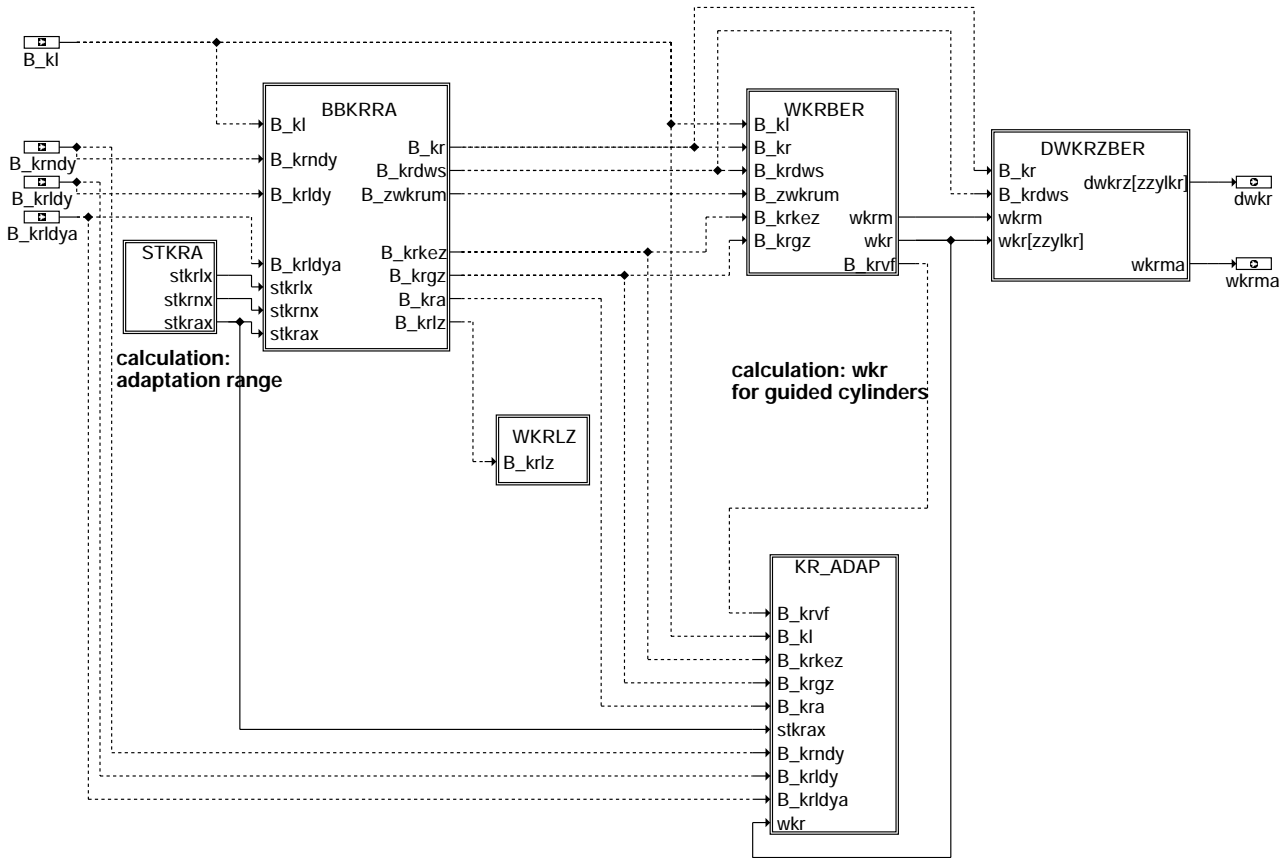
### FB ZWWL 4.10 Detailed description of function

The function offers the possibility to modify the basic ignition sparc advance zwbas by an additive value dzwwl. This offset is dependent on engine start temperature, intake air temperature and engine speed.

APP ZWWL 4.10 Application hint

## KRRA 18.70 Adaptive knock control

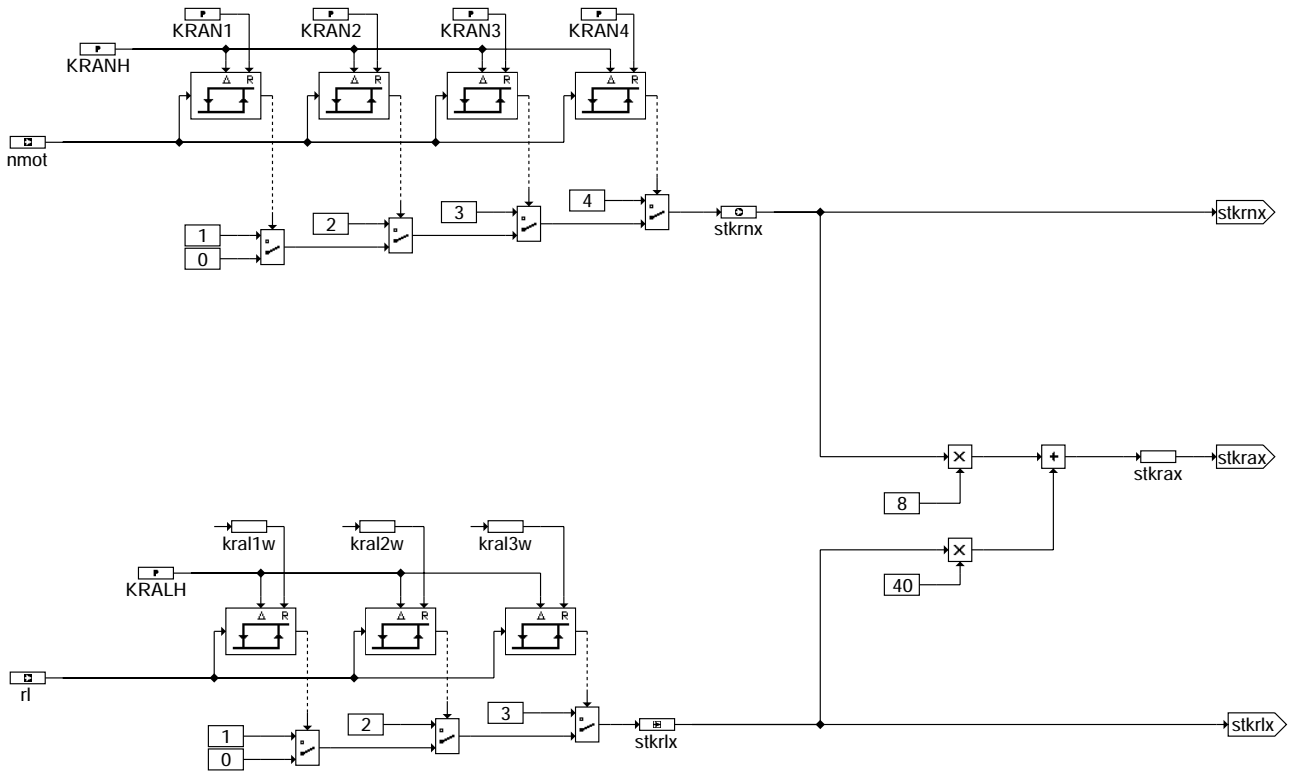
### FDEF KRRA 18.70 Function definition



kr-ra-main

kr-ra-main

## STKRA: Detection of load- and speed range



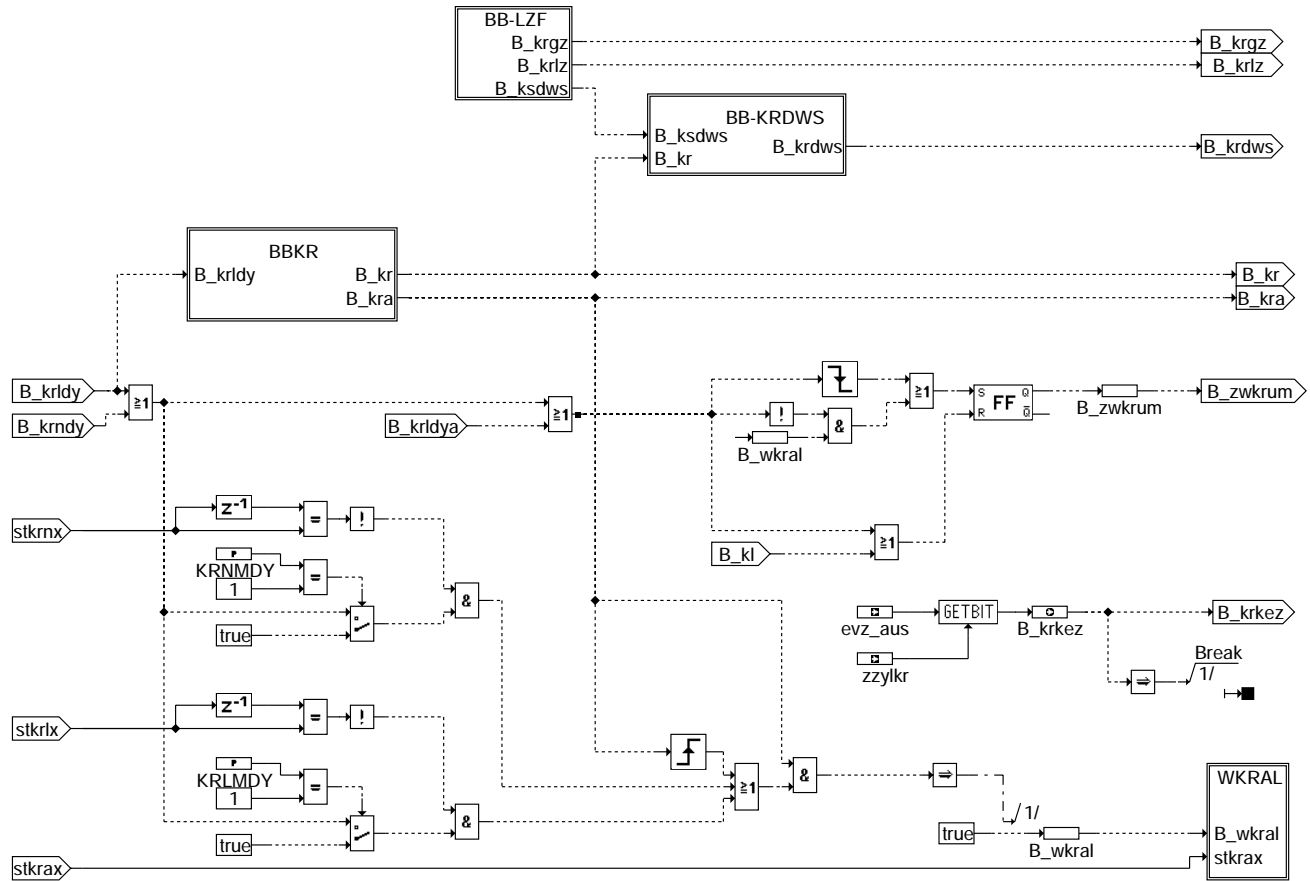
krra-stkra

krra-stkra





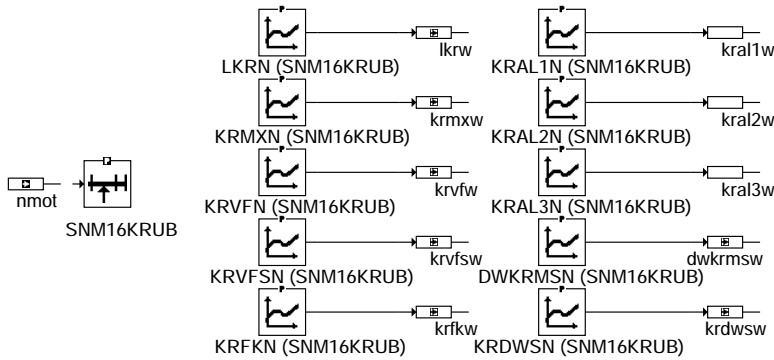
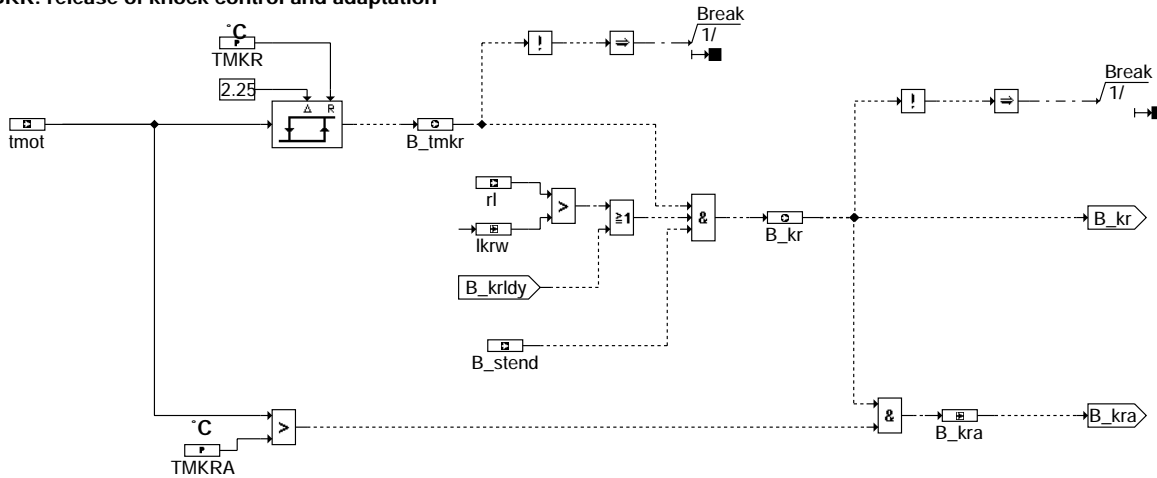
## BBKRRR: release of knock control and adaptation



krra-bbkrra

krb-bbkrra

## BBKR: release of knock control and adaptation

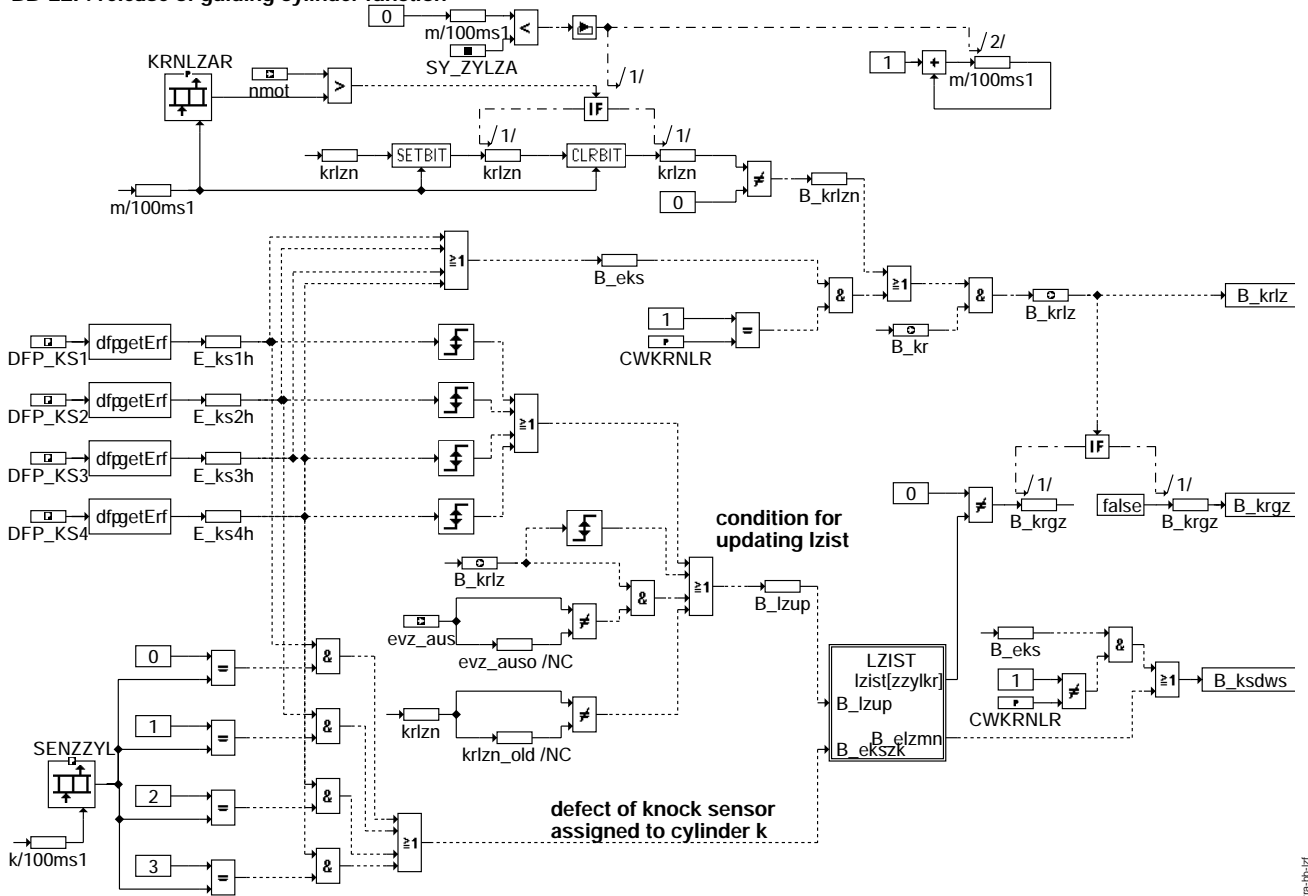


kr-ra-bbkr

kr-ra-bbkr



### BB-LZF: release of guiding cylinder function

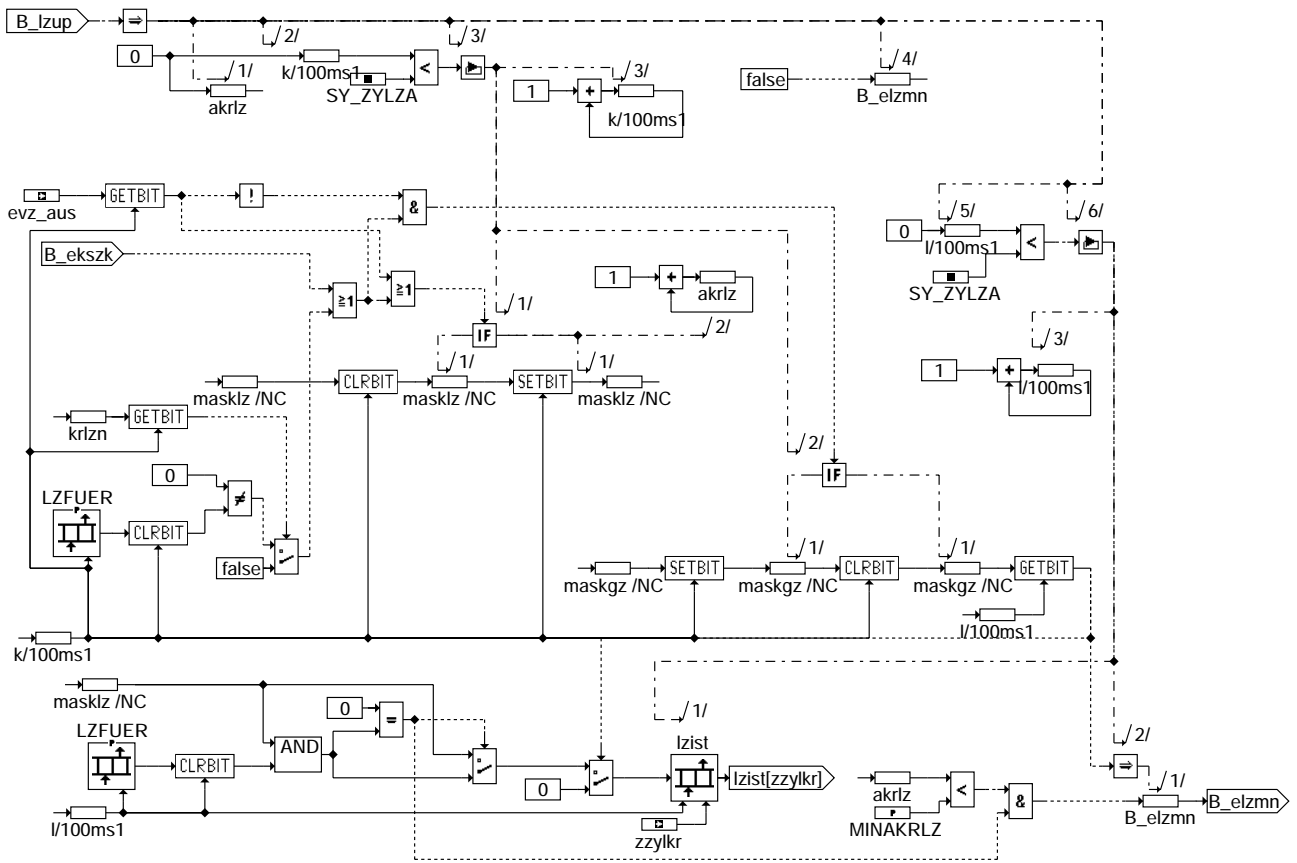


kr-ra-bb-lzf

kr-ra-bb-lzf

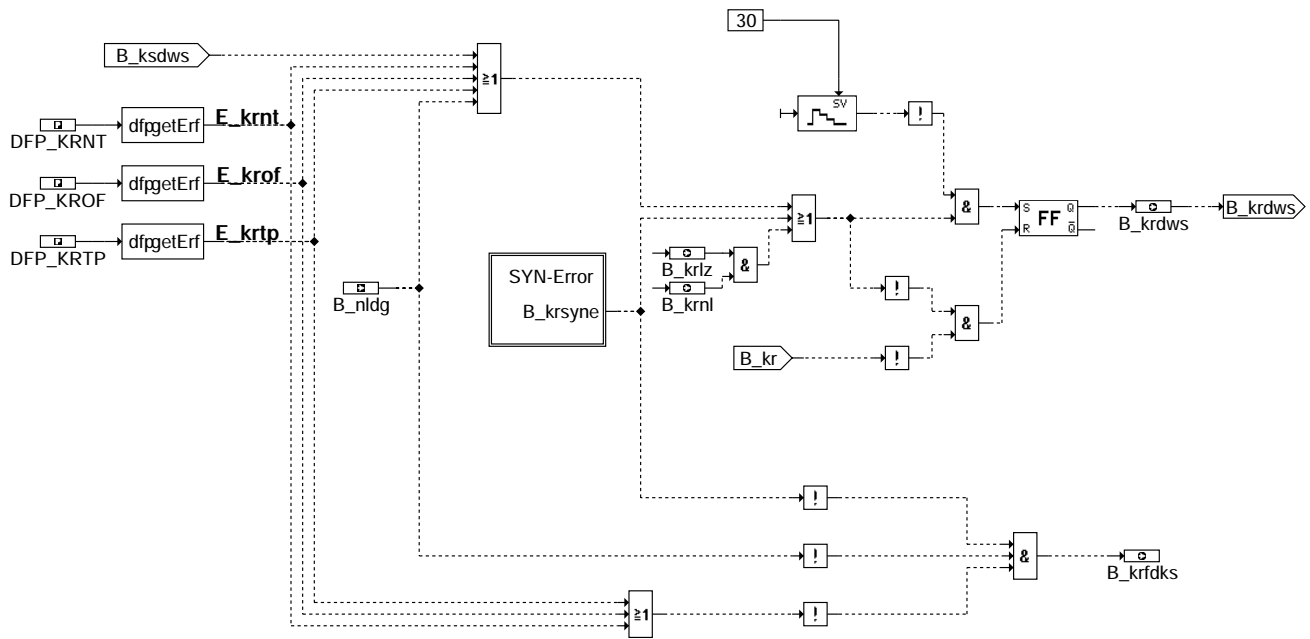


### LZIST: determination of guided and guiding cylinders



kr-ra-lzist

### BB-KRDWS: condition for safety retard of ignition

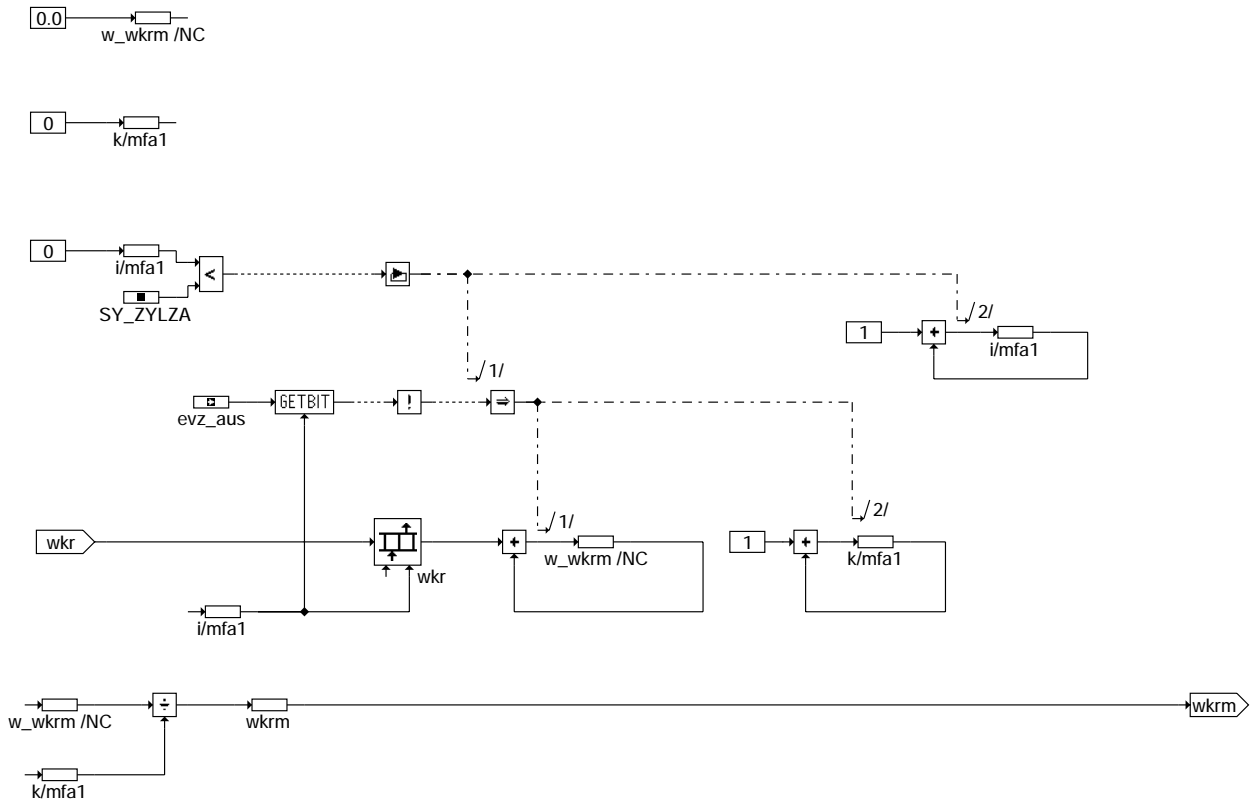


kr-ra-bb-krdws



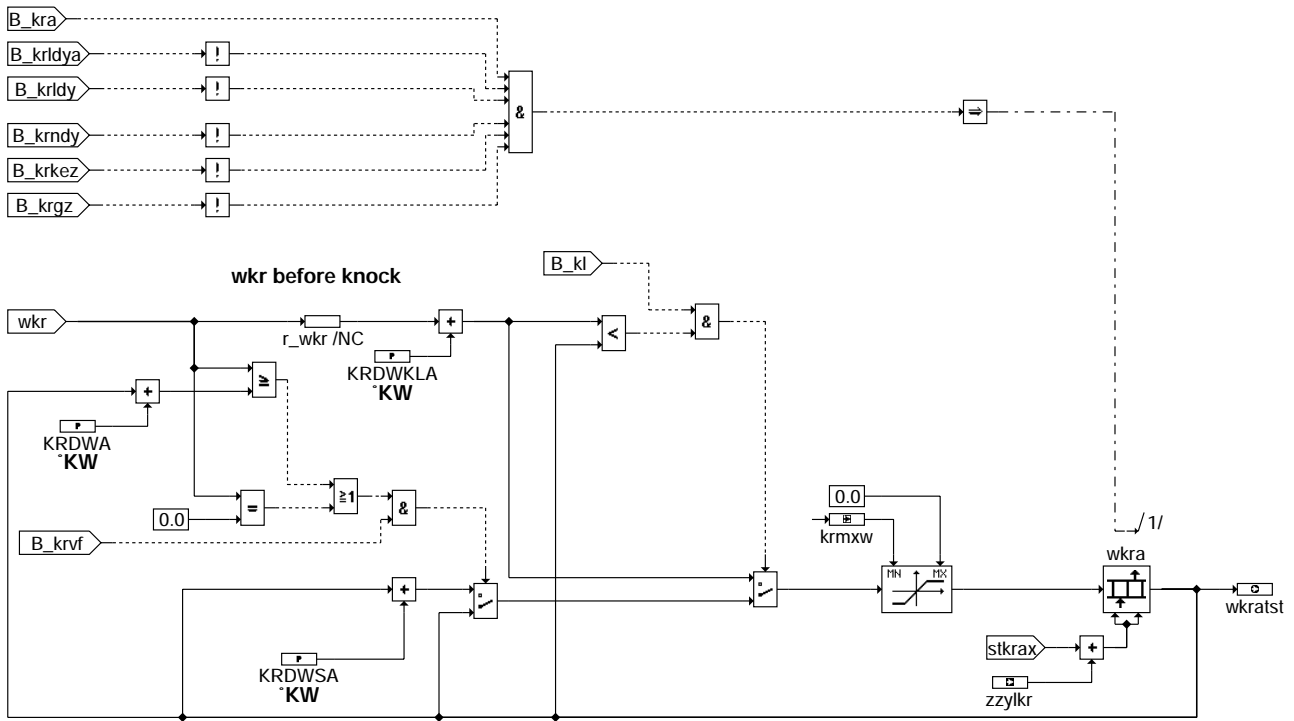


## WKRI: Calculation of the average ignition retard



krra-wkri

## KR\_ADAP: Adaptation of ignition retard



krra-kr-adap

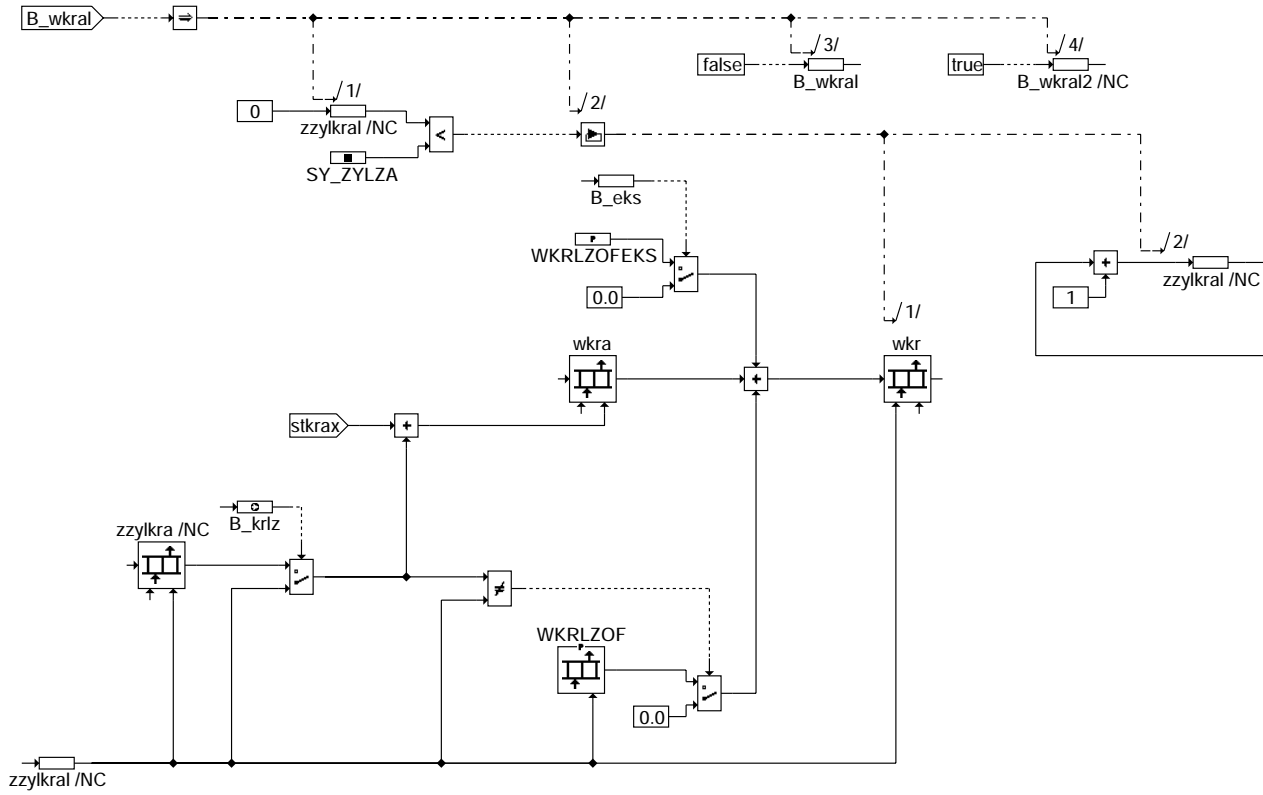
krra-wkri

krra-kr-adap





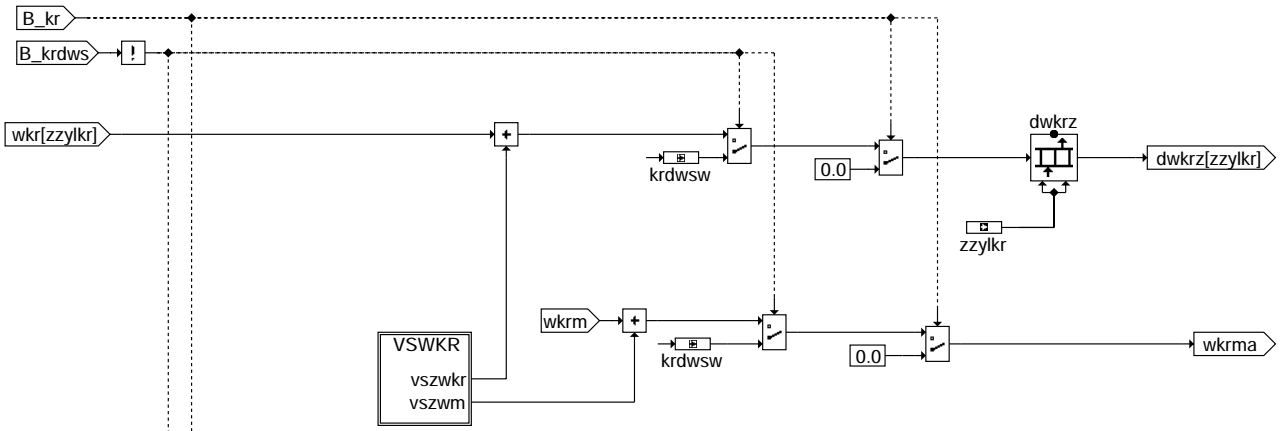
## WKRAL: Update of the cylinder selective ignition retard at adaptation area change (wkra --> wkr)



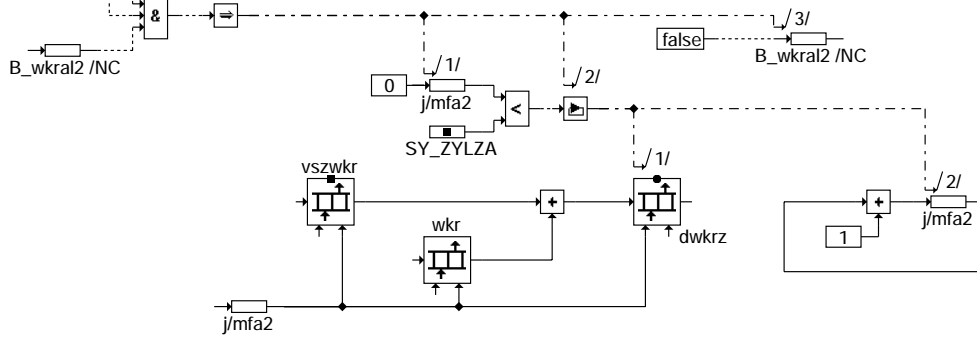
zzykral / NC  
krra-wkral

krra-wkral

## DWKRZBER: determination of ignition retard dwkrz for different operating conditions



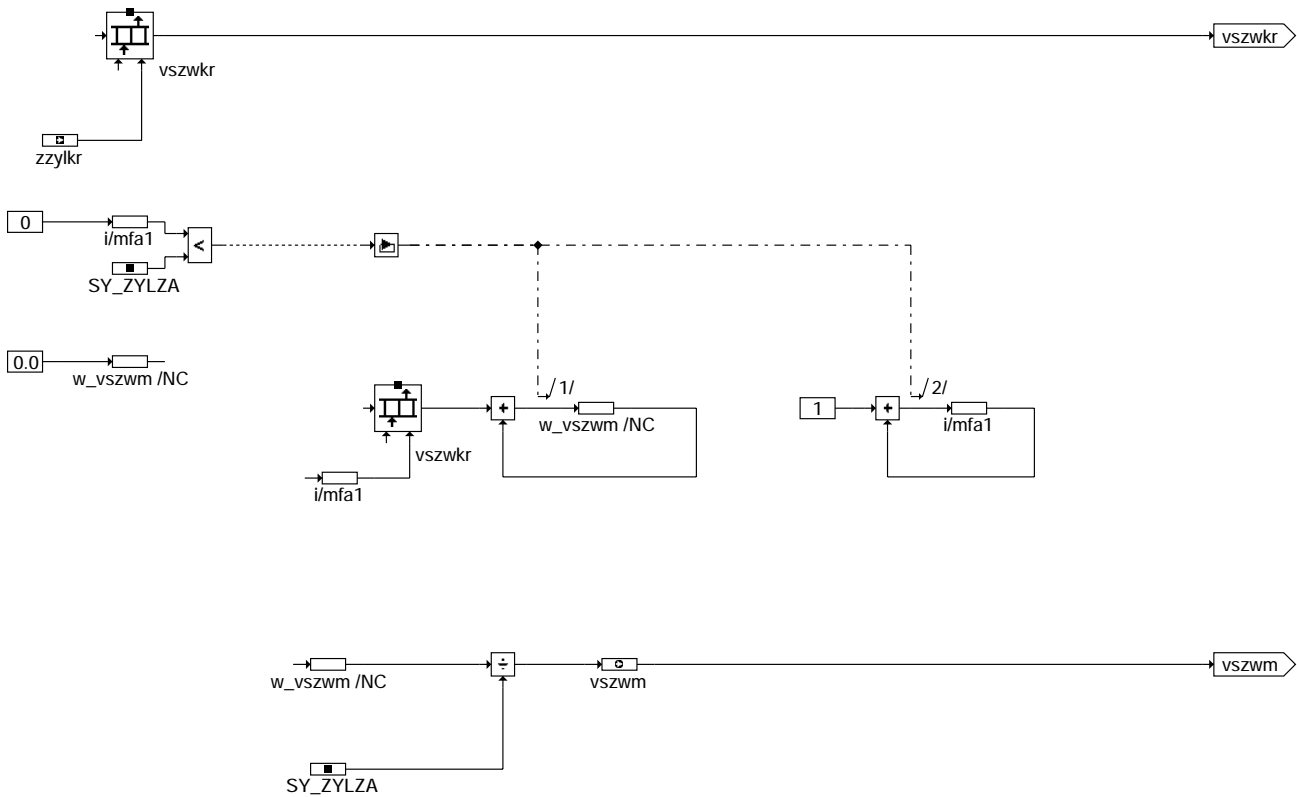
### fast update of dwkrz in case of reading the adaptation map (B\_wkral: wkra => wkr)



kr-ra-dwkrzber

kr-ra-dwkrzber

## VSWKR: Ignition adjustment with VS2x



kr-ra-vswkr

### ABK KRRA 18.70 Abbreviations

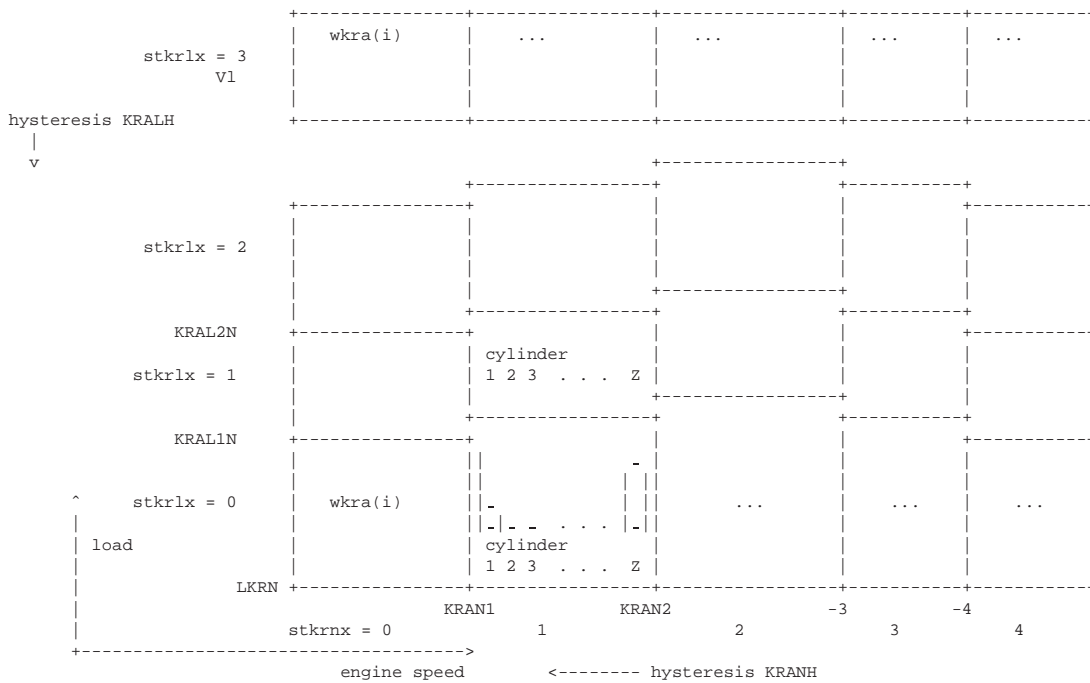
Parameter	Source-X	Source-Y	Type	Description
CWKRNLR			FW	code word for limp home in case of 1 out of 2 knock sensors fails
DWKRMSN	NMOT		KL	delta ignition angle knock control distance from mean retarding
KRAL1N			KL	load range for adaption maps 1
KRAL2N	NMOT		KL	load range dor adaption maps 2
KRAL3N	NMOT		KL	load range for adaption maps 3
KRALH			FW	load hysteresis for adaptation maps
KRAN1			FW	speed range for adaption maps, Stützstelle 1
KRAN2			FW	speed range for adaption maps, Stützstelle 2
KRAN3			FW	speed range for adaption maps, Stützstelle 3
KRAN4			FW	speed range for adaption maps, Stützstelle 4
KRANH			FW	n hysteresis for adaptation maps
KRDWA			FW	knock control difference current ignition angle to adaption map
KRDWKLA			FW	The SV-learning value for KR adaption after knocking detected
KRDWSA			FW	The FV-learning value for KR adation when wkra-wkr > KRDWA
KRDWSN	NMOT		KL	knock control delta angle safety
KRFKN	NMOT		KL	retard step knock occurrence
KRLMDY			FW	Read if change of load range: always or only if dynamic active
KRMXN	NMOT		KL	maximum retard adjustment
KRN LZAR			KWB	cylinder individual rpm limit for lead by leading cylinder
KRNMDY			FW	Read if change of speed range: allways or only if dynamic active
KRVFN	NMOT		KL	number of firings/cyl. or time for ignition advancing
KRVFSN	NMOT		KL	number of firings/cyl. or delay-time during fast ignition advancing of the KC
KSZA			FW	number of knock sensor
LKRN	NMOT		KL	load-signal threshold knock control
LZFUER	ZZYLKR		KL	guide cylinder assignment
MINAKRLZ			FW	minimum number of possible KC guide cylinders
SENZZYL			KWB (REF)	knock sensor for sw-cylinder counter 0-7
SNM16KRUB	NMOT		SV (REF)	datapoint distribution engine speed, 16 datapoints
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TMKR			FW	engine-temperature threshold to enable knock control
TMKRA			FW	engine temperature threshold for adaptive knock control
WKRLZOF	ZZYLKR		KL	Bloc of fixed values: ignition reatard offset for guided cylinder
WKRLZOFEKS			FW	ignition retard offset for guided cylinders in case of knock sensor error
Variable	Source		Type	Description
AKRLZ	KRRA		LOK	number of possible guide cylinders
B_DOPZUE	NLPH		EIN	Condition double ignition
B_EKS	KRRA		LOK	knock sensor defect detected



Variable	Source	Type	Description
B_ELZMN	KRRA	LOK	number of possible KC guide cylinders below minimum
B_KL	KRKE	EIN	condition for knocking
B_KR	KRRA	AUS	condition for knock control active
B_KRA	KRRA	LOK	condition for aktive KR-adaptation
B_KRDWS	KRRA	AUS	condition knock control safety ignition retarding
B_KRFDKS	KRRA	AUS	condition permission for knock sensor diagnosis
B_KRGZ	KRRA	LOK	Filled cylinder
B_KRKEZ	KRRA	AUS	injection valve of current cylinder switched off
B_KRLDY	KRDY	EIN	Condition load dynamics for knock detection active
B_KRLDYA	KRDY	EIN	Condition load dynamics retard and dynamics adaptation active
B_KRLZ	KRRA	AUS	condition for knock control guide-cylinder function active
B_KRLZN	KRRA	LOK	speed threshold for knock control guide-cylinder function exceeded
B_KRNDY	KRDY	EIN	condition speed dynamics for knock detection active
B_KRNL	KRRA	AUS	emergency operation of knock detection for emergency operation of phase sensor
B_KRSYNE	KRRA	LOK	knock control synchronisation error at phase error
B_KRVF	KRRA	LOK	condition for adjustment of kc-ignition timing to a less retarded value
B_LZUP	KRRA	LOK	update of lzist
B_NLDG		EIN	condition limp-home function speed sensor
B_PWF		EIN	Condition for powerfail
B_STEND	BBSTT	EIN	condition end of start
B_SYNPH	GGDPG	EIN	condition synchronization phase
B_TMKR	KRRA	AUS	Condition temperature (tmot) for knock control achieved
B_WKRAL	KRRA	LOK	condition to read wkr from knock control adaption map
B_ZWKRAA	KRRA	AUS	condition ignition angle of the KC is given
B_ZWKRUM	KRRA	LOK	flag: fast ignition advance KC
DFP_KRNT	KRRA	DOK	internal failure path number: knck control zero test
DFP_KROF	KRRA	DOK	internal failure path number: knock control offset
DFP_KRTP	KRRA	DOK	internal failure path number: knock control test pulse
DFP_KS1	KRRA	DOK	internal failure path number: knock sensor 1
DFP_KS2	KRRA	DOK	internal failure path number: knock sensor 2
DFP_KS3	KRRA	DOK	internal failure path number: knck sensor 3
DFP_KS4	KRRA	DOK	internal failure path number: knock sensor 4
DWKR	KRRA	AUS	cylinder-specific ignition-timing retardation
DWKRMSW	KRRA	LOK	current value for mean value limitation of the retarding
DWKRZ	KRRA	AUS	cyl.-spec. ignition-timing retardation with retardation for dynamics
EVZ_AUS	AEVAB	EIN	injection cut off pattern
E_KRNT	DKRNT	EIN	error flag: knock control zero test
E_KROF	DKRNT	EIN	Errorflag: knock control offset
E_KRTP	DKRTP	EIN	error flag: knock control test pulse
E_KS1	DKRS	EIN	error flag: knock sensor 1
E_KS1H	KRRA	LOK	auxiliary error flag KS1
E_KS2	DKRS	EIN	error flag: knock sensor 2
E_KS2H	KRRA	LOK	auxiliary error flag KS2
E_KS3	DKRS	EIN	error flag: knock sensor 3
E_KS3H	KRRA	LOK	auxiliary error flag KS3
E_KS4	DKRS	EIN	error flag: knock sensor 4
E_KS4H	KRRA	LOK	auxiliary error flag KS4
KRAL1W	KRRA	LOK	current value load adaptation range 1
KRAL2W	KRRA	LOK	current value load adaptation range 2
KRAL3W	KRRA	LOK	current value load adaption range 3
KRDWSW	KRRA	LOK	momentan characteristic-value for safety retard
KRFBW	KRRA	LOK	current value of KRFBW
KRLZN	KRRA	LOK	cylinder individual rpm threshold of guide cylinder function exceeded
KRMXW	KRRA	LOK	current value for retard limitation of the retarding
KRVFSW	KRRA	LOK	initialization value for quick advancing
KRVFW	KRRA	LOK	initialization value for normal advancing
LKRW	KRRA	LOK	current value of the load threshold knock control
LZIST	KRRA	LOK	array: momentaneous assignment of guiding and guided cylinders
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
STKRAX	KRRA	LOK	index for kc adaptation map
STKRLX	KRRA	LOK	load range adaption map KC
STKRNX	KRRA	AUS	speed range adaption map KC
SY_ZNDAUS	PROKON	EIN	System constant ignition timing output (single or double fir.)
TMOT	SWADAP	EIN	Engine temperature
TPNT_AKTIV	EGKE	EIN	activation of kc-functions
VSZWKR	VS_VERST	EIN	cylinder individual adjustment of ignition angle by VS2x
VSZWM	KRRA	AUS	mean value of adjustment ignition angle with VS2x
WKR	KRRA	LOK	cylinderindividual ignition retarding value knock control
WKRA	KRRA	LOK	adaption map of wkr, speed- and load-dependent
WKRA_TST	KRRA	AUS	wkra updated with synchro
WKRMA	KRRA	LOK	average value of individual ignition retarding by knocking
WKRMA	KRRA	AUS	Average value of ignition retarding by KC, generally(limpe home with safety)
WKR_TST	KRRA	AUS	cylinder-individual ignition angle retarding, druming
ZKRVF	KRRA	LOK	counter determines the frequency of the cylinder-individual ignition angle adv.
ZWKRAFLD	ZUE	EIN	bit pattern of the cylinder-individually stored B.zwkra
ZZYLKR	GGKS	EIN	cylinder counter KC







For the indexing of the wkra(i) - RAM-cells the following specification is used in the SW:

$i = \text{zzylkr} + 8 * \text{stkrnx} + 40 * \text{stkrlx}$        $\text{zzylkr} = 0 \dots 7$ , so at the max. 8 cylinders can be represented  
 $\text{stkrnx} = 0 \dots 4$ , 5 engine speed ranges  
 $\text{stkrlx} = 0 \dots 3$ , 4 load ranges

**Storage:**

3 conditions for the updating of the adaptation map are distinguished:

1. During each knock occurrence the retarding of the corresponding cylinder is stored in the current load/engine speed range of the adaptation map immediately after knocking has occurred if this retarding is later than that stored in wkra. By means of KRWKRUM it is decided whether the retarding which led to the knock occurrence (=knock border) is stored or whether the current retarding after the knock occurrence (retarded by KRFPKN) is stored. KRWKRUM=0 ignition angle after the knock occurrence; KRWKRUM=1 ignition angle before the knock occurrence.
2. If the current retarding wkr(i) is earlier by at least KRDWA than the latest value stored in the adaptation map and if the advancing counter zkrvf(i) = 0 then the retarding is changed by KRDWA towards advance in the adaptation map.
3. If  $\text{wkra}(i) + \text{KRDWA} > 0$ , if the current retarding  $\text{wkr}(i) = 0$  and if the advancing counter  $\text{zkrvf}(i)=0$ , then  $\text{wkra}(i)$  is set to  $\text{wkr}(i) = 0$ .

The adaptation of the characteristic map is only performed during steady-state and during not active safety retarding ( $\text{B\_krdws}=0$ ). The adaptation does not take place if the ignition angle is drawn further towards retard by the torque management than would be necessary for the KC ( $\text{B\_zwkraa} = 0$ ).

**Reading:**

During active adaptation the retarding of all cylinders wkr(i) is overwritten by the values from wkra(i) if one of the following conditions is fulfilled:

1. Transition from !B.kra to B.kra
2. Load range changes  
 It is possible to choose via label whether during the change of the load adaptation range without dynamic response the value wkr(i) from the just left range is kept or whether it is taken over from the new range wkra(i). The change-over is performed via the fixed value KRLMDY:  
 $\text{KRLMDY}=0$  take-over of wkr(i) from wkra(i) always during load range changes  
 $\text{KRLMDY}=1$  take-over of wkr(i) from wkra(i) only during load range changes with dynamic response.
3. Engine speed changes  
 It is possible to choose via label whether during the change of the engine speed adaptation range without dynamic response the value wkr(i) from the just left range is kept or whether it is taken over from the new range wkra(i). The change-over is performed via the fixed value KRNMDY:  
 $\text{KRNMDY}=0$  take-over of wkr(i) from wkra(i) always during engine speed range changes  
 $\text{KRNMDY}=1$  take-over of wkr(i) from wkra(i) only during engine speed range changes with dynamic response.



Knock control in case of active dynamic response (KRRR, KR\_ADAP, BBKR)  
=====

In case of active dynamic response ( B\_krldy, B\_krldya, B\_krndy, s. %KRDY ) the further adaptation of the steady-state values wkra(i) is blocked. A change of the adaptation ranges leads to an updating of wkr(i) with the values adjusted in wkra(i). Each knocking combustion ( B\_kl ), like so far, leads to a retarding by KRFKN and is therefore added to the cylinder-individual retarding in wkr(i).  
For B\_krldya additionally an adaptive dynamic response derivation wkrdy (s. %KRDY, %ZUE) is added.

Safety retarding during active knock control (KRRR)  
=====

If the safety flag of the KC, B\_krdws, is set ( see %DKRS, %DKRNT, %DKRTP ), dwkrz(i) and wkrma are overwritten by KRDWS if the knock control is active.  
wkra(i), wkr(i) and wkrm are not updated as long as B\_krdws is set.  
If B\_krdws is again reset dwkrz(i) is overwritten by wkr(i), wkrma by wkrm.

#### APP KRRR 18.70 Application hint

Cylinder-individual and load/engine speed range-dependent values are marked by (i) in the description corresponding to their realization in the ECU-code, e.g. wkr(i). The corresponding RAM-cell which can be read via VS100 is indicated in the ASCET-picture by \_i, e.g. wkr.i.

The cylinder counter zzylkr generated in the %GGKS serves as control variable for the index i of the cylinder-individual RAM-cells (wkr(i), dwkrz(i), zkrvf(i), with the exception of wkra(i), s.b.).

The knock control can be switched off via the label TMKR: TMKR > tmot ==> !B.kr





For the application the following typical values are suggested:  
=====

KRFKN -3 ° KW is a value for the retarding of the ignition angle. Experience shows that it is a sufficient value to safely run the engine at the knock border with stabilized adaptation.

KRMXN -12 ° KW is a value which is sufficient for most applications. When fixing this characteristic line it must be noted though that the engine can be operated absolutely knock-free with the programmed value under worst-case conditions (tmot, tans, fuel with lowest octane number).  
In the process attention must be paid to the maximum permitted exhaust gas temperature.

KRVFN approx. 4 sec/°KW advancing is a typical value. The control speed of the KC during quasi-steady-state engine running results from this characteristic line in connection with KRFKN. The aim here is to determine a time constant which is larger than the thermic time constant of the engine so as to avoid a thermic strain.  
When adjusting KRVFN it must be taken into consideration that the thermic strain of the engine increases with increasing engine speed so that a larger period should be chosen for higher engine speeds.  
KRVFN = 1 Inc. \* n / (120 \* x) with 1 Inc. in ° KW  
n in rpm  
x in ° KW / sec - "speed" for the advance adjustment

KRVFSN to be adjusted dependent of KRDKWLA in order to enable a quick advancing of the adaptation map values in case of changed operating conditions without provoking an increased knock frequency.  
KRDKWLA = -3 °KW: approx. 1 sec/°KW advancing or approx. 1/4 \* KRVFN  
KRDKWLA = 0 °KW: approx. 2 sec/°KW advancing or approx. 1/2 \* KRVFN

TMKR approx. 40 °C is the value during which on many engines knocking combustions can already occur.

TMKRA: Below an engine temperature threshold TMKRA it is not useful to update wkra since experience has shown that within this operating range the knock tendency of the engine is very low. If adaptation would be permitted the necessary values learned in the normal operating range would be lost which means that the knock frequency is again increased when this operating range is reached again.  
Usually this engine temperature threshold lies at TMKRA = 80 ° C.

LKRN approx. 30% rl is a typical value. The lowest load threshold during which knocking combustions can occur is stored in this characteristic line.

KRDWCLA 0 °KW <= |KRDWCLA| <= |KRFKN|

KRDWA |KRDWA| >= |KRDWCLA|

KRDWSA 0 °KW < |KRDWSA| und |KRDWSA| <= |KRDWA| - |KRDWCLA|

the following set of parameters is recommended:

KRDWCLA	KRDWA	KRDWSA	
°KW	°KW	°KW	
0	2.25	2.25	=> Adaptation of the knock border
-1.5	3	1.5	=> Adaptation of the knock border + safety retarding of 1.5 °KW
-3	4.5	1.5	=> Adaptation of the knock border + safety retarding of 3 °KW

DWKRMSN approx. -3 ° KW is a typical value to maintain the engine smoothness and to avoid misfire misdetection; if the values get smaller the cylinder-individual character of the knock control is increasingly lost.

KRLMDY = 0: reading of the adaptation map in case of load range changes is always performed (independent of dynamic response)

KRNMDY = 1: reading of the adaptation map in case of engine speed range changes is only performed during simultaneous dynamic response

KRDWSN approx. -12 ° KW, knocking must definitely be avoided under worst-case conditions

KRALH In order to avoid a jitter at the range limits a hysteresis was introduced for decreasing load.  
Typical value for KRALH 3 %.

KRANH In order to avoid a jitter at the range limits a hysteresis was introduced for decreasing engine speed.  
Typical value for KRANH 120 RPM.



When determining the ignition characteristic map special attention must be paid to the knowledge in which range an enrichment function (  $\lambda < 1$  ) is active since the knock border shifts due to the enrichment. So as not to endanger a stable knock control the determination of the ignition angles and the enrichment function must be adjusted such that in the entire operating range of the engine a constant distance is kept to the knock border(  $< 3^\circ$  KW ).

Hints regarding load

The load is given in percent.

Needed measured values:

- B\_kl
- B\_kr
- B\_kra
- B\_krldy .krldya .krndy
- B\_zwkraa
- B\_zwkrum
- stkrlx
- stkrnx
- wkr\_0 - x
- wkra\_0 - x
- wkrdy\_0 - x
- zkrvf\_0 - x

The existence of some values/RAMs is determined by the representation in ASCET (block hierarchy, course of control). They are not realized in the SW resp. they cannot be measured definitely by means of VS100 due to their special realization:

- B\_wkral cannot be measured definitely
- B\_krvf not realized
- zkrvf(i)=0 cannot be measured, this state can only be detected indirectly via the performed RESET of the counter from zkrvf(i) = 1 to zkrvf(i) = KRVP(S)N
- zzylkral not realized

Distinction wkrm/wkrma

wkrm represents the mean value of the each time SY\_ZYLZA latest calculated wkr(i) (possibly incl. mean value vswzm) while wkrma represents the mean value of the dwkrz(i) (without wkrdy) which was passed on to the ignition during the SY\_ZYLZA latest combustions.

Adaptation characteristic map wkra

When choosing the map values a compromise has to be found between the possibly varying knock tendency of the engine at different load and engine speed ranges and the time by which the characteristic map is updated during normal driving. If the adaptation map wkra is chosen to large (i.e. many rl-nmot-ranges) a longer period is needed in order to update all ranges. Thus in case of changed operating conditions which lead to a larger knock tendency it is inevitable that the knock frequency increases.

Generally a characteristic map with 3 load and 5 engine speed ranges is sufficient for wkra. In this map a RAM-cell is provided for each load/ engine speed range per cylinder.

( Example 4-cylinder-engine:  $3 \times 5 \times 4 = 60$  RAM-cells for wkra )

For the indexing of the wkra(i) - RAM-cells the following specification is used in the SW:

$$i = zzylkr + 8 * stkrnx + 40 * stkrlx \quad (zzylkr = 0..7, \text{ so at the max. } 8 \text{ cylinders can be represented})$$

In case of special customers need the number of adaptation ranges can be varied but at the maximum to  $4 \times 8$  load/engine speed ranges (change of above-mentioned indexing may possibly be necessary).

Cylinder-individual ignition angle timing with VS20

By means of VS20 a cylinder-individual additional timing vszw(i) can be performed (s.a. %VS\_VERST) so that the following applies:

$$dwkrz(i) = wkr(i) + wkrdy + vszwkr(i) \quad \text{if } B\_kr \ \& \ !B\_krdws$$

Label	timing range	quantization	initialization/neutral value
vszwkr_i	see %VS_VERST	0.75 °KW	0 °KW

vszwkr\_i | see %VS\_VERST | 0.75 °KW | 0 °KW

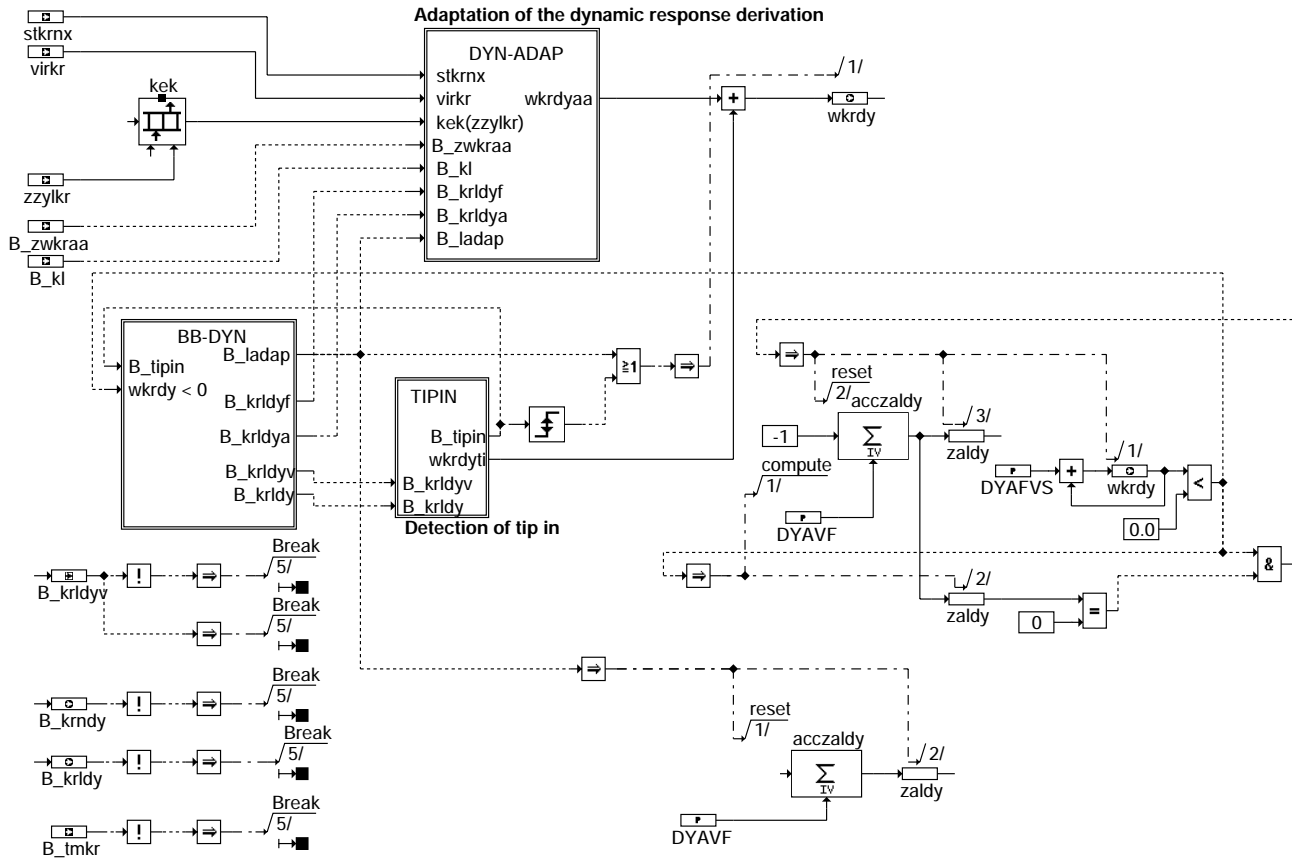
i = 0 ... SY\_ZYLZA - 1

- Attention:
1. No automatic limitation of vszwkr(i) is performed - please observe engine and catalyst protection during the timing!
  2. The earliest possible ignition angle is under all circumstance determined by the knock control, i.e. it is possible that the minimum permitted (due to temperature reasons) ignition angle may be undershot (s. %ZUE, %ZWMIN). Please observe engine and catalyst protection !

## KRDY 10.90 Knock control for load dynamics

### FDEF KRDY 10.90 Function definition

KRDY: Overview KC-dynamic response

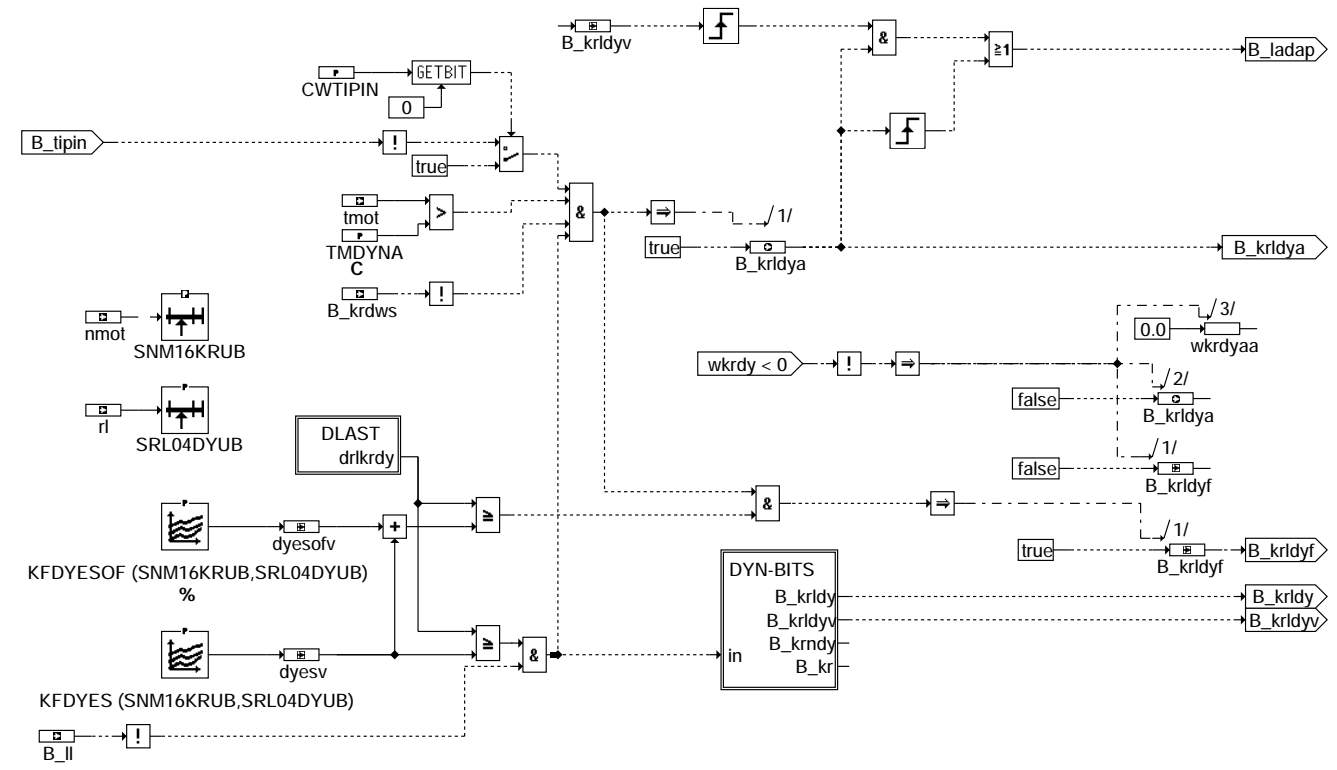


krdy-main

krdy-main



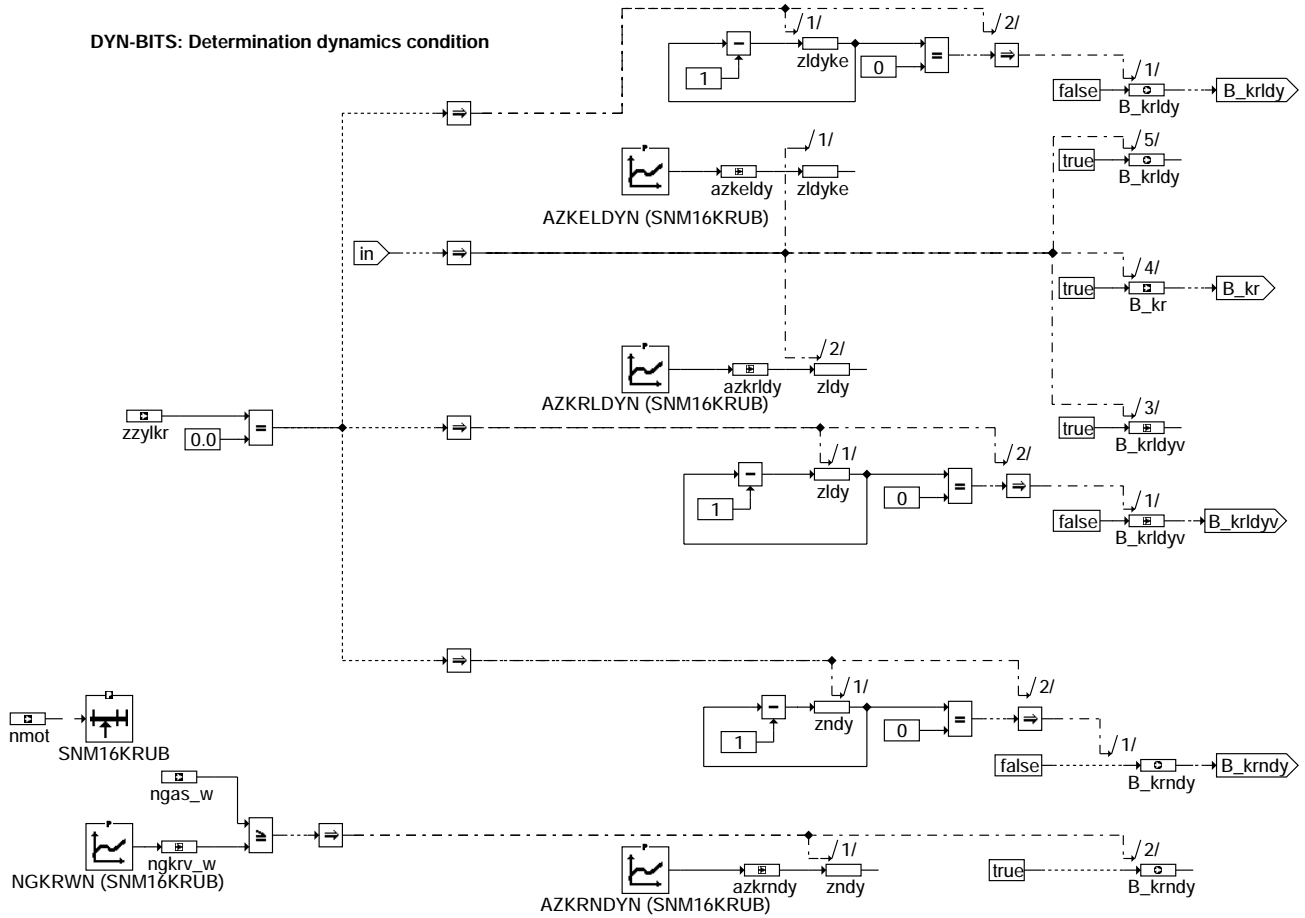
### BB-DYN: Detection load and engine speed dynamic response, enabling adaptation



krdy-bb-dyn

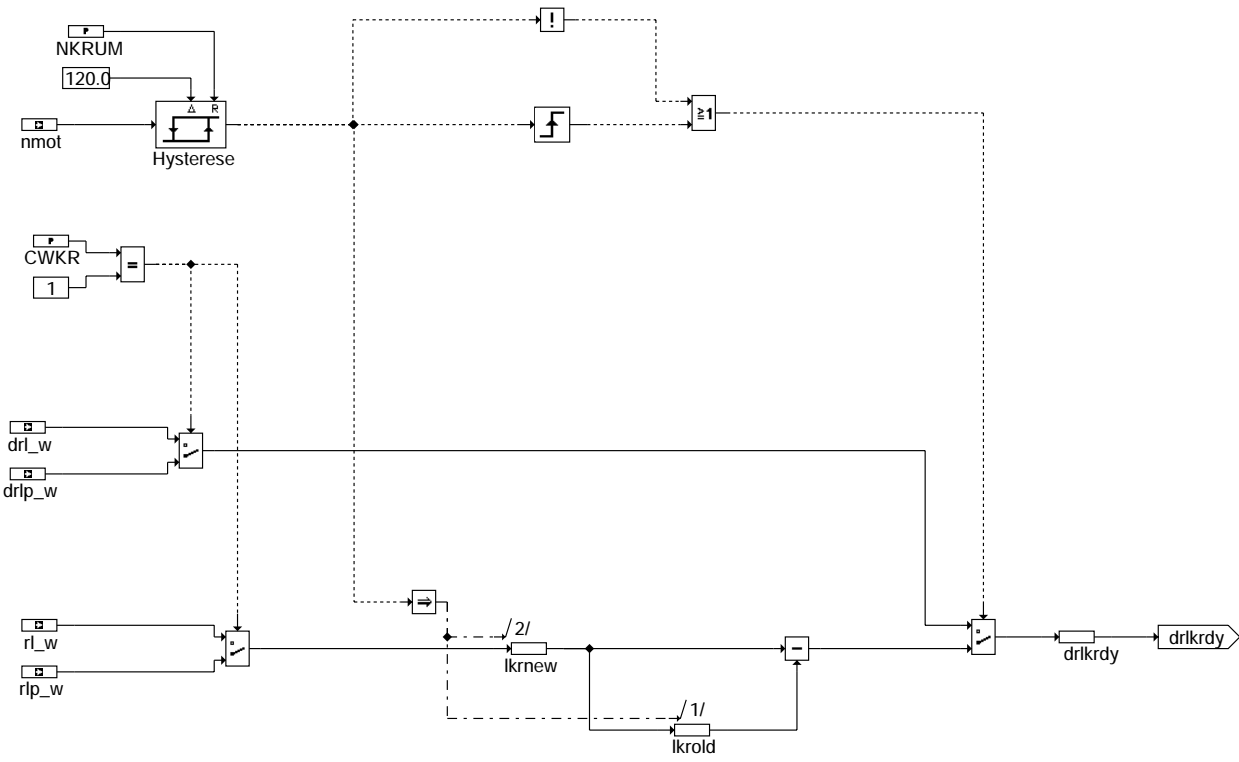
krdy-bb-dyn

### DYN-BITS: Determination dynamics condition



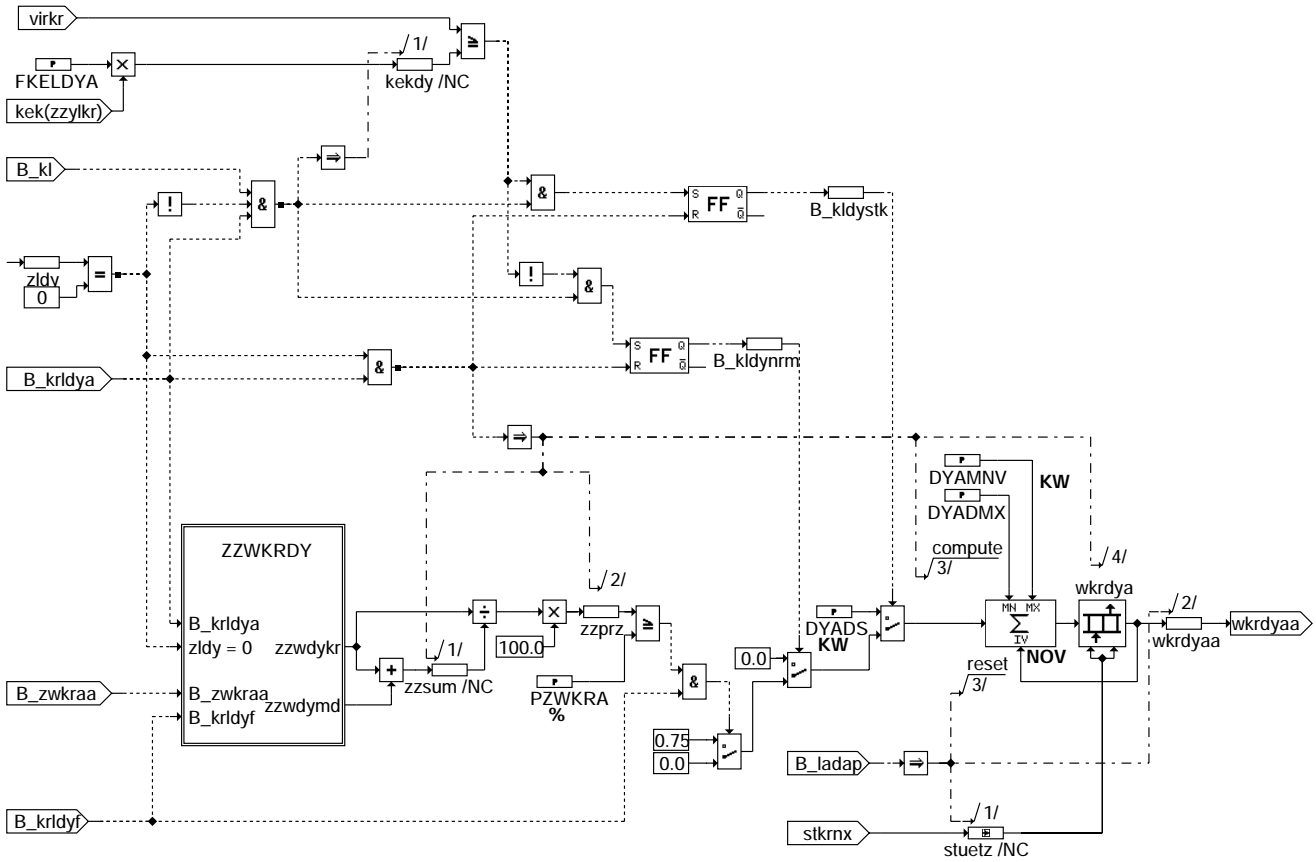
### krdy-dyn-bits

### DLAST: Determination load gradient



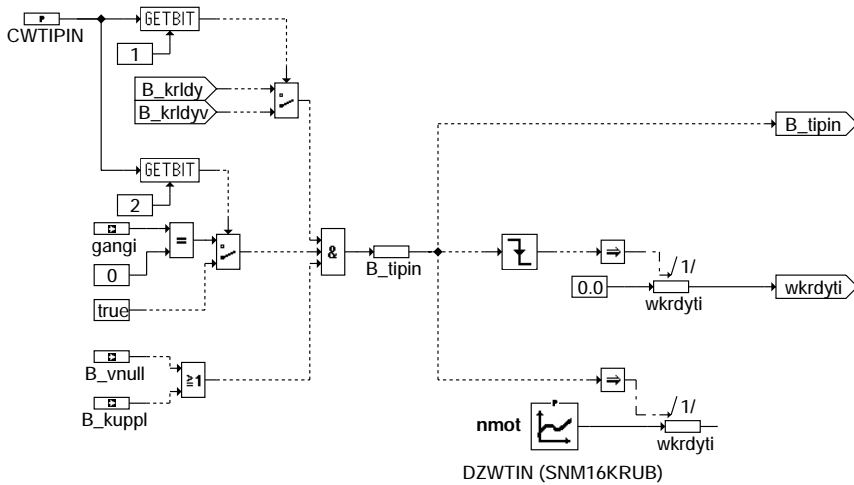
### krdy-dlast

### DYN-ADAP: Adaptation of the dynamic response derivation



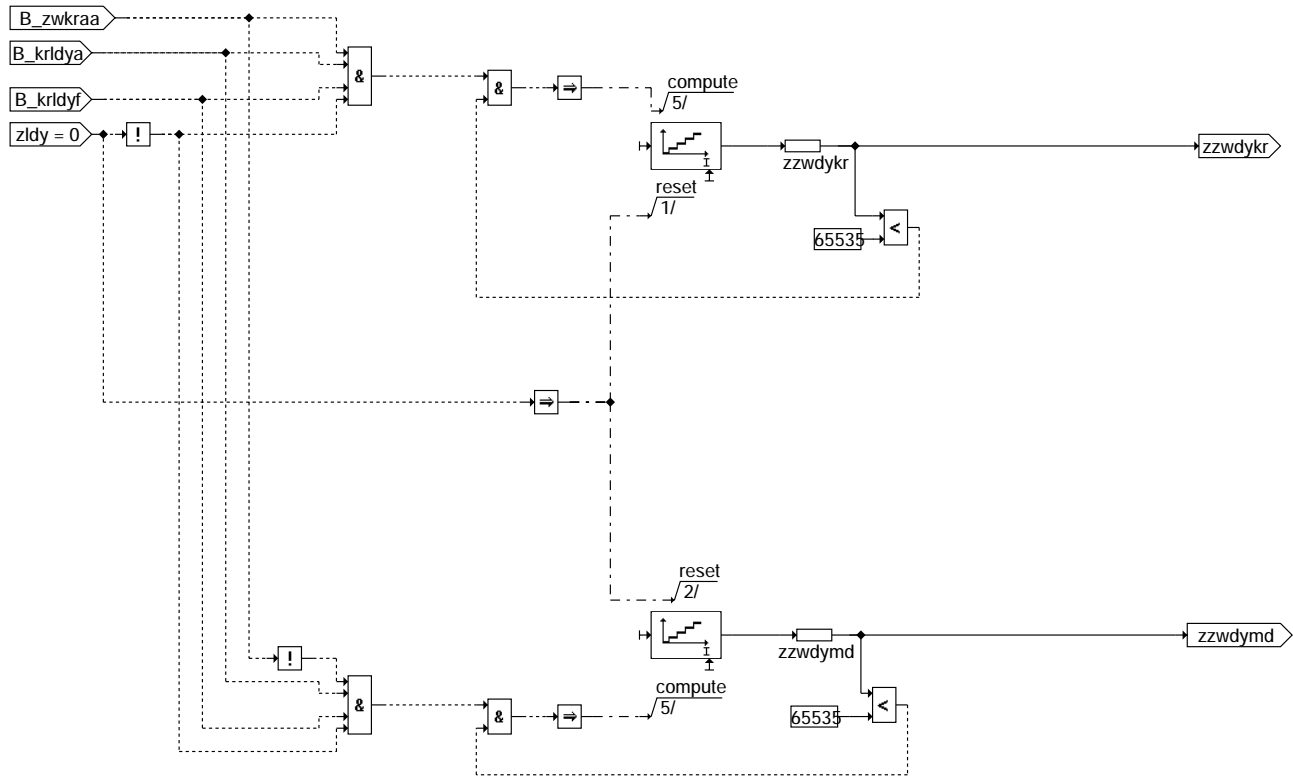
### krdy-dyn-adap

#### TIPIN: Detection of tip ins



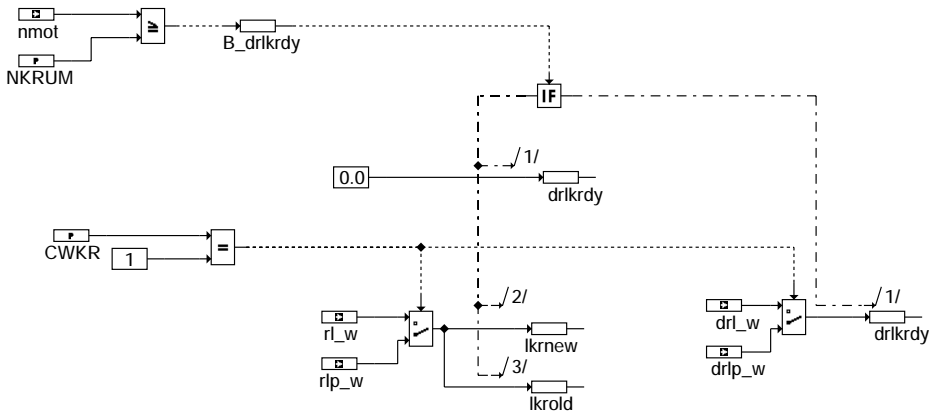
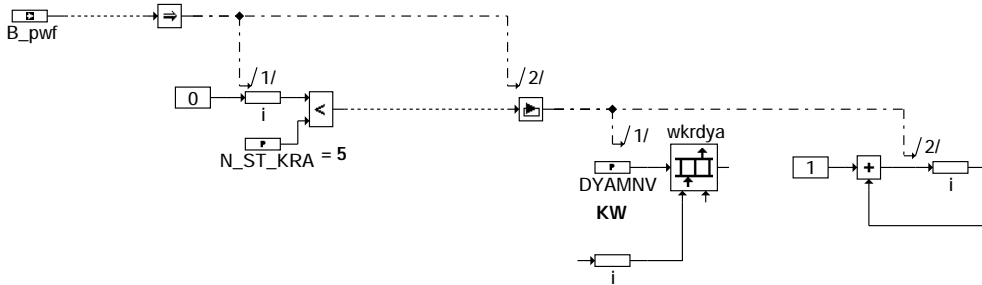
### krdy-tipin

### ZZWKRDY: percentage of ignition retard adjustment caused by KC



### krdy-zzwkrdy

#### Initialization



### krdy-initialize

krdy-zzwkrdy

krdy-initialize



## ABK KRDY 10.90 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
AZKELDYN	NMOT		KL (REF)	ignition per cylinder for load dynamics => knock detection
AZKRLDYN	NMOT		KL (REF)	number of ignition per cyl. during knock control load dynamic
AZKRNDYN	NMOT		KL (REF)	number of ignition for knock control engine speed dynamic
CWKR			FW	code word knock control
CWTIPIN			FW	Codeword for tip in function
DYADMX			FW	max. value of dynamic response derivation
DYADS			FW	add. retarding per cycle through adapt. dynamics
DYAFVS			FW	advance step for deactivation of dynamic response
DYAMNV			FW	min. value of dynamic response derivation
DYAVF			FW	deactivation period for dynamics retardation
DZW TIN	NMOT		KL (REF)	delta ignition angle at tip-in
FKELDYA			FW	Corrective factor for knock detection threshold for adaptation of load dynamic
KFDYES	NMOT	RL	KF	Threshold for dynamic presetting values
KFDYESOF	NMOT	RL	KF	Offset threshold for dynamic presetting values
NGKRWN	NMOT		KL (REF)	threshold revolution gradient for dynamics detection
NKRUM			FW	revolution threshold for change of delta load signal for load dynamics
N_ST_KRA			FW	number of speed ranges in kc adaptation map
PZWKRA			FW	percentage frequency of ignition angle output by KC during dyn. adaption
SNM16KRUB	NMOT		SV (REF)	datapoint distribution engine speed, 16 datapoints
SRL04DYUB	RL		SV	basepoint distribution of rl, 4 basepoints
TMDYNA			FW	engine temperature threshold to enable load dynamic adaptation

Variable	Source	Type	Description
AZKELDY	KRDY	LOK	value of cl AZKELDYN
AZKRLDY	KRDY	LOK	value of cl AZKRLDYN
AZKRNDY	KRDY	LOK	value of cl AZKRNDYN
B_DRLKRDY	KRDY	LOK	Flag for n > NKRUM
B_KL	KRKE	EIN	condition for knocking
B_KLDYNRM	KRDY	LOK	Condition normal knocking with adapted load dynamic
B_KLDYSTK	KRDY	LOK	Condition heavy knocking with adapted load dynamic
B_KR	KRDY	AUS	condition for knock control active
B_KRDWS	KRRA	EIN	condition knock control safety ignition retarding
B_KRLDY	KRDY	AUS	Condition load dynamics for knock detection active
B_KRLDYA	KRDY	AUS	Condition load dynamics retard and dynamics adaptation active
B_KRLDYF	KRDY	LOK	condition adaptation load dynamics retard towards advance released
B_KRLDYV	KRDY	LOK	condition threshold for additional load dynamics retard exceeded
B_KRNDY	KRDY	AUS	condition speed dynamics for knock detection active
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_LL	MSF	EIN	Condition idle
B_PWF		EIN	Condition for powerfail
B_TIPIN	KRDY	LOK	Tip-in detected
B_TMKR	KRRA	EIN	Condition temperature (tmot) for knock control achieved
B_VNULL	GGVFZG	EIN	condition vehicle at stillstand
B_ZWKRAA	KRRA	EIN	condition ignition angle of the KC is given
DRLKRDY	KRDY	LOK	load gradient for activating kc load dynamics
DRLP_W	BGRLP	EIN	delta predicted load for injection time calculation (word)
DRL_W	SWADAP	EIN	charge change (Word)
DYESOFV	KRDY	LOK	current value offset for load dynamic response detection threshold
DYESV	KRDY	LOK	current value of load dynamic response detection threshold
GANGI	SWADAP	EIN	Engaged gear
I	KRDY	LOK	Vector for initialization flags (ECU model only)
KEK	KRKE	EIN	knock detection threshold corrected
LKRNEW	KRDY	LOK	value of load at time t
LKROLD	KRDY	LOK	value of load at time t-dt
NGAS_W	BGNG	EIN	engine speed gradient during one working cycle
NGKRV_W	KRDY	LOK	instantaneous value of threshold speed dynamics
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RPL_W	BGRLP	EIN	rel. air charge predicted for injection calculation (Word)
RL_W	EGFE	EIN	relative air charge (Word)
STKRNX	KRRA	EIN	speed range adaption map KC
TMOT	SWADAP	EIN	Engine temperature
VIRKR	KRKE	EIN	Ratio: integrator / reference level knock control
WKRDY	KRDY	AUS	ignition retard during dyn-function of knock control
WKRDYA	KRDY	LOK	Adapted ignition timing for KC dynamic
WKRDYAA	KRDY	LOK	adaptation part of dynamic ignition retard
WKRDYTI	KRDY	LOK	tip in part of dynamic ignition retard
ZALDY	KRDY	LOK	Ignition counter for deactivation of load dynamics
ZLDY	KRDY	LOK	Ignition counter for load dynamic
ZLDYKE	KRDY	LOK	ignition counter for load dynamics => knock detection
ZNDY	KRDY	LOK	ignition counter for rpm-dynamics
ZZPRZ	KRDY	LOK	percentage of ignitions with kc determined ignition angle during dynamics
ZZWDYKR	KRDY	LOK	ignition counter for KC with bit B_zwkra=1 set during KC dynamic
ZZWDYMD	KRDY	LOK	ignition counter for KC with bit B_zwkra=0 not set during KC dynamic
ZZYLKR	GGKS	EIN	cylinder counter KC





## FB KRDY 10.90 Detailed description of function

### Load dynamic response

The load dynamic response is marked by two phenomena:

- increased knock tendency (in case of corresponding temperature)
- quick noise increase

which are responded to by an additional ignition retarding (dynamic response derivation wkrdy) resp. by a quicker following-up of the reference level and increased knock detection threshold (s. %KRKE).

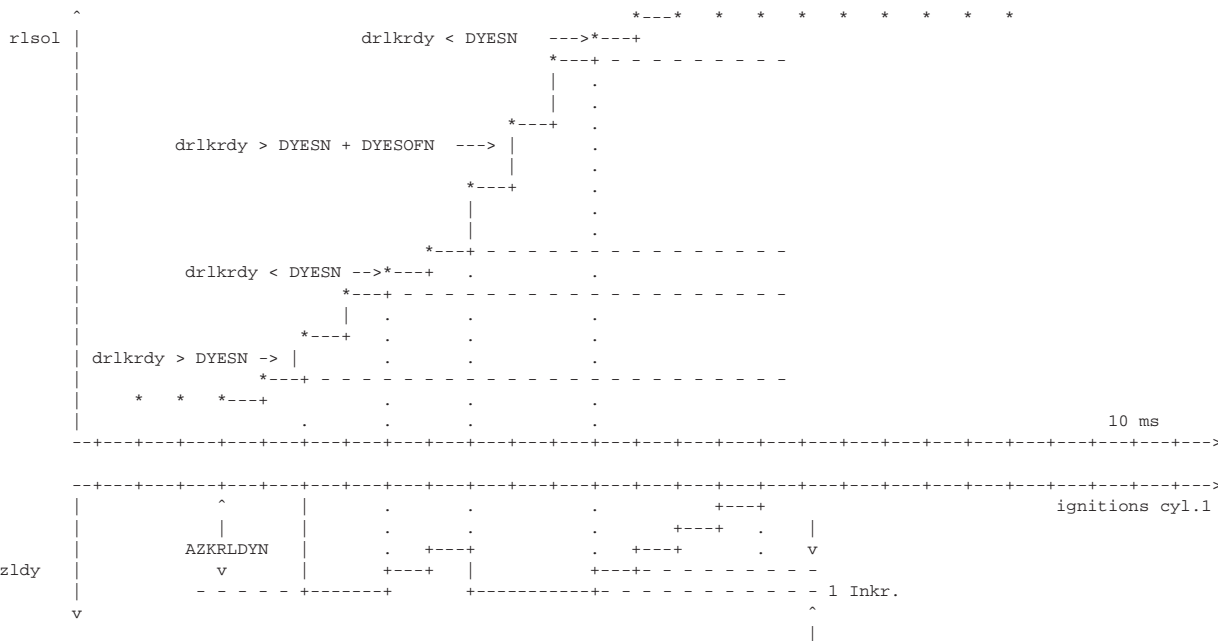
### Detection load dynamic response and enabling of the dynamic response adaptation (BB\_DYN)

When introducing countermeasures two temperature ranges are distinguished:

- Temperature range 1: (TMKR < tmot < TMDYNA): knock control load dynamic response without adaptation of ignition angle --->  
B\_krldy & !B\_krldya
- Temperature range 2: (tmot > TMDYNA): knock control load dynamic response with adaptation of ignition angle --->  
B\_krldy & B\_krldya

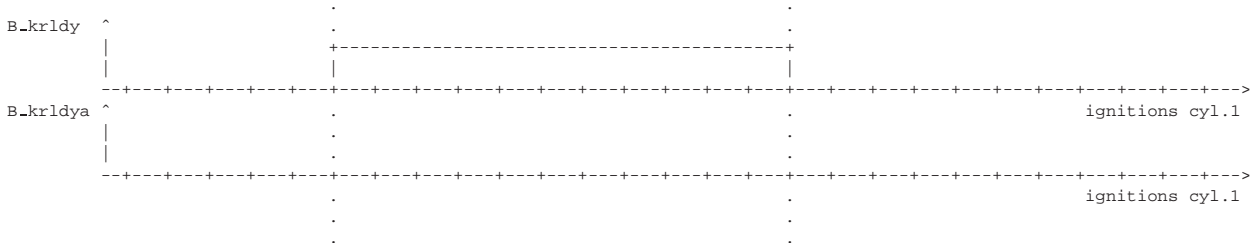
In both ranges the load dynamic response B\_krldy is triggered via the positive load difference between equidistant instants (=load gradient). If during an acceleration the difference drlkrdy of the nominal load signal between two consecutive scannings in the 10ms-grid is larger than the 1. dynamic response detection threshold DYESN then the timer zldy is set to the starting value AZKRLDYN. As soon as drlkrdy < DYESN, zldy is decremented by 1 increment per working cycle until zldy = 0 is reached. As long as zldy > 0 and TMKR < tmot <= TMDYNA, only the condition B\_krldy=1 applies. For zldy > 0 and tmot > TMDYNA the condition B\_krldya=1 additionally applies and this is done until wkrdy is completely controlled back to 0. The dynamic response detection threshold DYESN and the starting value for the timer AZKRLDYN are engine speed-dependent and each taken from a fixed characteristic line. During idling (B\_ll) no dynamic response may be detected (e.g. due to LLR). In addition zldy=0 leads to the dynamic phase being stopped.

Triggering conditions for load dynamic response: Temperature range 1 ---> (TMKR < tmot < TMDYNA) & (drlkrdy > DYESN) & !B\_ll  
Temperature range 2 ---> (tmot > TMDYNA) & (drlkrdy > DYESN) & !B\_ll

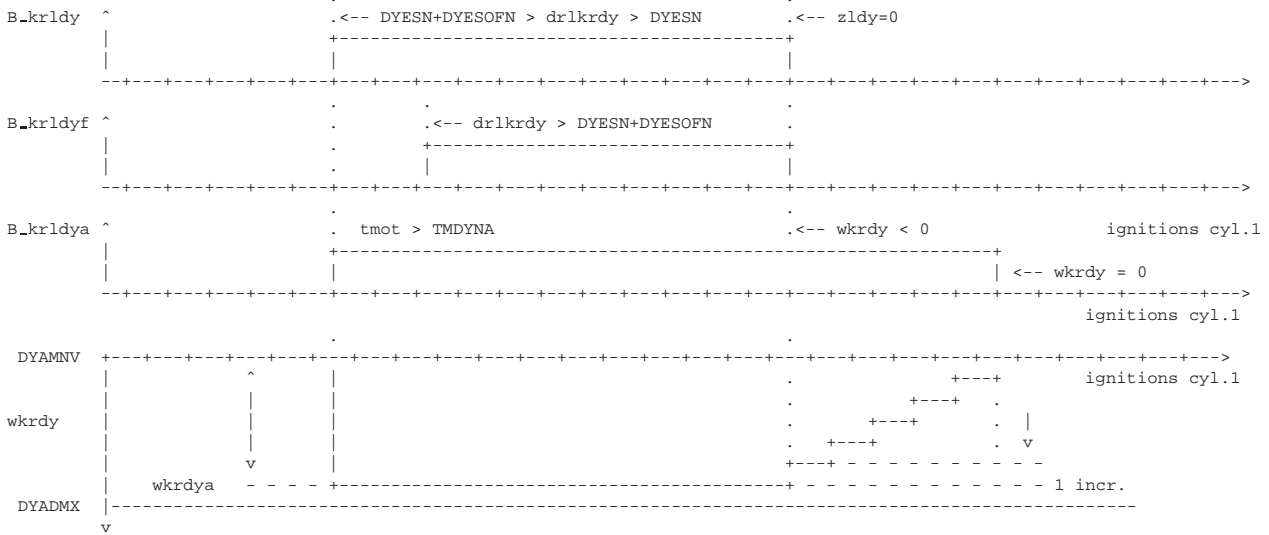




for temperature range 1 without adaptation of the ignition angle as long as  $zldy > 0$ : B\_krldy & !B\_krldya applies



for temperature range 2 with adaptation of the ignition angle as long as  $zldy > 0$ : B\_krldy & B\_krldya applies



### Influence of load dynamic response on knock detection and control

When triggering load dynamic response the following functions become effective independent of the temperature range (TMKR <  $t_{mot} \leq TMDYNA$  or  $t_{mot} > TMDYNA$ ):

1. The cylinder-selective reference level calculations are performed by means of the label KRFTP3 (see %KRKE) => quicker following-up of reference level.
2. The knock detection thresholds  $ke(i)_w$  are increased by the factor FKELDY. Corrected knock detection thresholds  $kek(i)$  result (see %KRKE).
3. For each detected knocking combustion the ignition angle is retarded by the value KRFKN cylinder-selectively (see %KRRA). For enabled steady-state adaptation the stored retardings are read from the each time current adaptation map range in case of range changes. Writing access to the characteristic map of the steady-state adaptation is, however, forbidden (see %KRRA).

In temperature range 1 (TMKR <  $t_{mot} \leq TMDYNA$ ) no additional dynamic response retarding of the ignition angle is performed !!



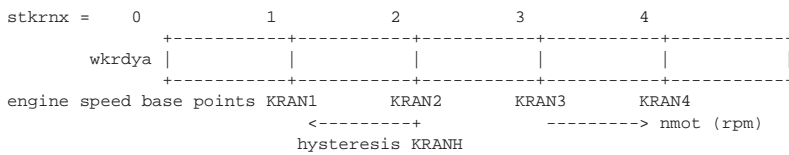
Load dynamic response adaptation (DYN\_ADAP)

=====

If load dynamic response is triggered in temperature range 2 (tmot > TMDYNA ==> B\_krldya) the following functions additionally become effective:

4. Adaptive dynamic response retarding of the ignition angle for a 1 1 cylinders (KRDY and %KRRA).  
In addition to the steady-state cylinder-selective KC retarding the ignition angle for a 1 1 cylinders is retarded by wkrdy for the time zldy > 0 if dynamic response was detected. Here wkrdy is read engine speed-dependent from the RAM-area wkrdya. If zldy = 0 this additional dynamic response retarding wkrdy is reduced by 1 increment per DYAVF combustions.
- 5.1 If load dynamic response is triggered without exceeding of the 2. dynamic response threshold (DYESN < drlkrdy < DYESN+DYESOFN ==> B\_krldy & B\_krldya), then the enabling of the adaptation to retard (BB\_DYN) is performed for the starting value of the dynamic response retarding wkrdy. That means that by strong knocking B\_kldystk a new adaptation of wkrdya is performed for the next dynamic procedure (wkrdya(new) = wkrdya(old) + krfkw, limited to DYADMX).  
In case of exclusively normal knocking B\_kldynrm the adaptation value remains unchanged and also if no knocking occurs (DYN\_ADAP).
- 5.2 If the 2. dynamic response threshold is also exceeded (drlkrdy > DYESN + DYESOFN ==> B\_krldyf) then in addition to the measures from 4 and 5.1 also the adaptation of the dynamic response retarding is enabled to advance (BB\_DYN).  
During the active dynamic phase (B\_krldyf = 1) two counters zzwdykr and zzwdynd are started. For each set bit B\_zwkraa = 1 (i.e. ignition angle of the KC was given out) zzwdykr is incremented, for each not set bit B\_zwkraa = 0 (i.e. ignition angle of the torque management was given out) zzwdynd is incremented. At the end of the dynamic phase (B\_krldyf = 0) the ratio zzwdykr / (zzwdykr + zzwdynd) is determined, the two counters zzwdykr and zzwdynd are thereafter reset to 0 (DYN\_ADAP).  
If no knocking combustion occurs during the active dynamic phase (B\_krldyf = 1) which is detected by the knock detection threshold kek (s. %KRKE) and if zzwdykr / (zzwdykr + zzwdynd) >= PZWKRA (adjustable fixed value) then the adaptive dynamic response derivation starting value wkrdya is adjusted towards advance by 1 increment, however, in the process it is limited to the value DYAMNV.

The RAM-area wkrdya is subdivided into 5 engine speed ranges stkrnx.



The engine speed ranges are identical to those of the steady-state adaptation map (s. %KRRA). The engine speed limits apply directly with rising engine speed. The engine speed hysteresis KARANH is only deducted with decreasing engine speed (identical to %KRRA).

The dynamic response derivation calculated again each time is written into the RAM-area wkrdya and there into the engine speed range which is valid at the time of the triggering of the dynamic response (!B\_krldya ==> B\_krldya). It is then available as wkrdy for the next dynamic procedure which starts in this engine speed range.

With 'ignition off' all retardings are preserved in the RAM-area wkrdya until the engine is started again.

Tip in (TIPIN)  
=====

Tipin is an increase of engine speed at almost zero load while the engine is declutched. This results in a maximum of engine speed- and load dynamics which leads to a increased knocking tendency. On the other side the torque requested by the driver is not used to accelerate the vehicle. Therefore it is allowed to retard the ignition timing later as knock borderline. The reduced torque due to the ignition retard is irrelevant. Therefore a tipin ignition retard wkrdyti = DZWTIN(nmot) is added to the actual ignition angle.

A tipin is detected if load dynamics (B\_krldyv) is detected and the relation of engine speed to vehicle speed results in gangi=0 and the the engine is declutched.

The tipin function can be configurated by CWTIPIN:

Bit 0 = 0 => wkrdy = wkrdyaa + wkrdyti, ignition retard during dynamics is the sum of adative and pre-controlled share  
Bit 0 = 1 => wkrdy = wkrdyti, dynamics adaptation is disabled, only the pre-controlled tip in-share is ausgegeben

Bit 1 = 0 => max. duration of tip in is determined by AZKRLDYN (B\_krldyv)  
Bit 1 = 1 => max. duration of tip in is determined by AZKELDYN (B\_krldy) with AZKRLDYN <= AZKELDYN

Bit 2 = 0 => tip in detection is enabled even if gangi=0 is not detected, then tip in can be detected during the gearshift process  
Bit 2 = 1 => tip in detection is enabled by gangi = 0, tip in can not be detected during the gearshift process



## Engine speed dynamic response

=====

If the engine temperature  $t_{mot} > TMKR$  and the engine speed gradient  $ngas_w$  are larger than the engine speed dynamic response detection threshold  $DNKRDYSN$  then the timer  $zndy$  is set to the starting value  $AZKRDYN$ .

If  $ngas_w < DNKRDYSN$ ,  $zndy$  is decremented up to zero for each ignition of cylinder 1. The condition  $B_{krndy}=1$  applies until  $zndy > 0$ .

As long as  $B_{krndy}=1$  the following applies:

1. The cylinder-selective reference level calculations are performed with the label  $KRFTP2$  (see  $\%KRKE$ ) => quicker following-up of reference level.
2. The knock detection thresholds  $ke(i)_w$  are increased by the factor  $FKENDY$ . Corrected knock detection thresholds  $kek(i)$  result (see  $\%KRKE$ ).
3. For each detected knocking combustion the ignition angle is retarded by the value  $KRFKN$  cylinder-selectively (see  $\%KRRA$ ). For enabled steady-state adaptation the stored retardings are read from the each time current adaptation map range in case of range changes. Writing access to the characteristic map of the steady-state adaptation is, however, forbidden (see  $\%KRRA$ ).

The triggering of the load dynamic response may also take place during engine speed dynamic response active and vice versa. It is decided in  $\%KRKE$  resp.  $\%KRRA$  which of the then introduced measures takes priority.

**APP KRDY 10.90 Application hint**

Application aim load dynamic response: Adjustment so that performance is optimized but no audible "dynamic knocking" in the vehicle. The adjustment should be performed resp. checked under "worst-case conditions" (summer test, fuel with lowest enabled octane number).

The following values taken from experience can be used for a rough adjustment:

$TMKR$  approx. 40 degrees C  
 $TMDYNA$  approx. 80 degrees C  
 $DYESN$  no values have yet been gained  
 $DYESOFN$  no values have yet been gained, tough demand:  $DYESN + DYESOFN \leq 767 \%$  for all base points  $nmot$  !  
 $AZKRLDYN$  should be chosen in such a way that the dynamic condition approx. 300-600 ms applies.  
Guidance values are: 2-5 working cycles (AS) at 1000 rpm and 15-25 working cycles at 6000 rpm.  
 $DYADMX$  approx. -8 ... -10 degrees crankshaft ( $^{\circ}KW$ )  
 $FKELDYA$  1.2 - 1.3  
 $DYAVF$  should be chosen such that during each working cycle adjustment to advance is performed by approx. 4 increments at most (so  $DYAVF$  must be equal to or exceed no. of cylinders / 4,  $DYAVF$  is an integer and  $DYAVF > 0$  is demanded!)

Application aim engine speed dynamic response: Avoiding of misdetections due to a very fast increase in engine speed and a thus resulting abrupt noise increase (especially critical: gear shifting on powerful vehicles with automatic gearbox)

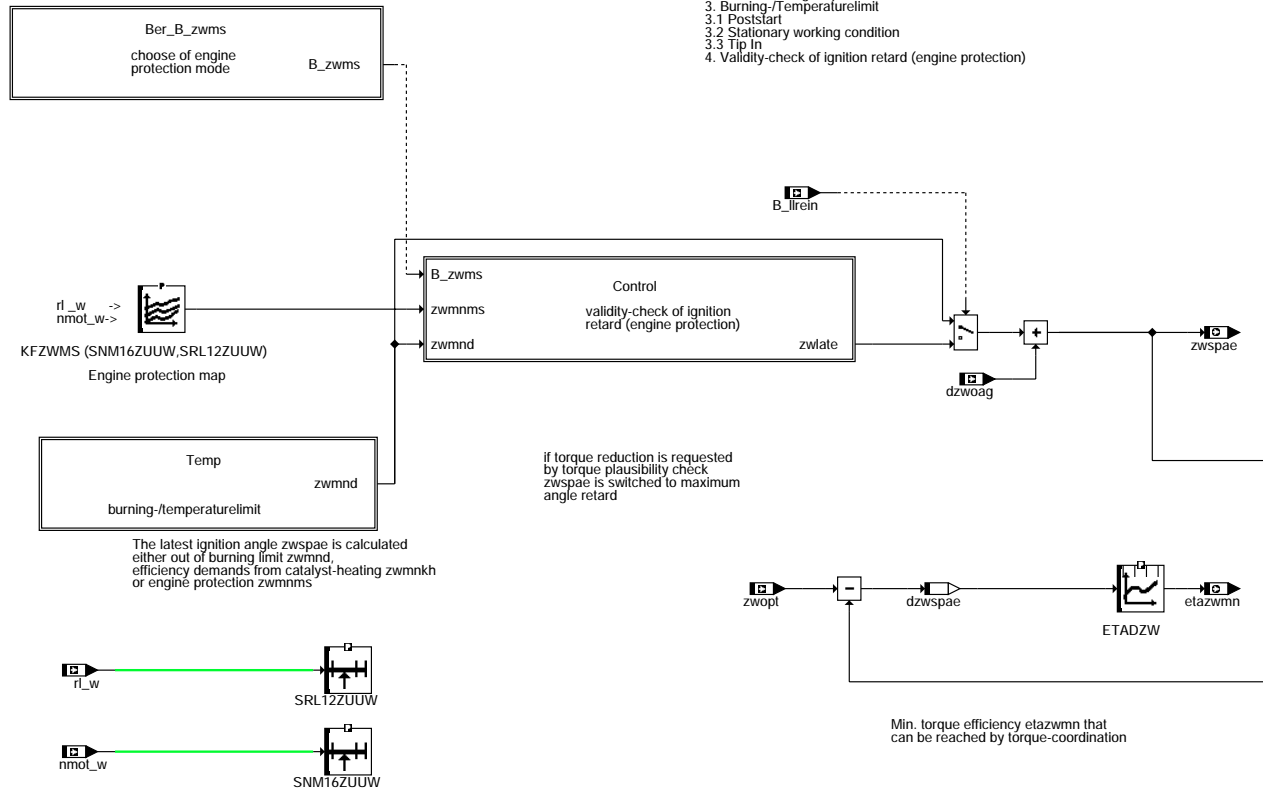
$DNKRDYSN$  approx. 500 - 1000 rpm/s;  
 $AZKRDYN$  should be chosen such that the dynamic response condition approx. 300-600 ms applies.  
Guidance values are: 2-5 working cycles at 1000 rpm and 15-25 working cycles at 6000 rpm.

## ZWMIN 3.140 Calculation of maximum retarded spark limitation

### FDEF ZWMIN 3.140 Function definition

Source: ZWMIN 3.140

- Contents:
1. Basic Structure
  2. Choose of engine protection-mode
  3. Burning-/Temperaturelimit
    - 3.1 Poststart
    - 3.2 Stationary working condition
    - 3.3 Tip In
  4. Validity-check of ignition retard (engine protection)



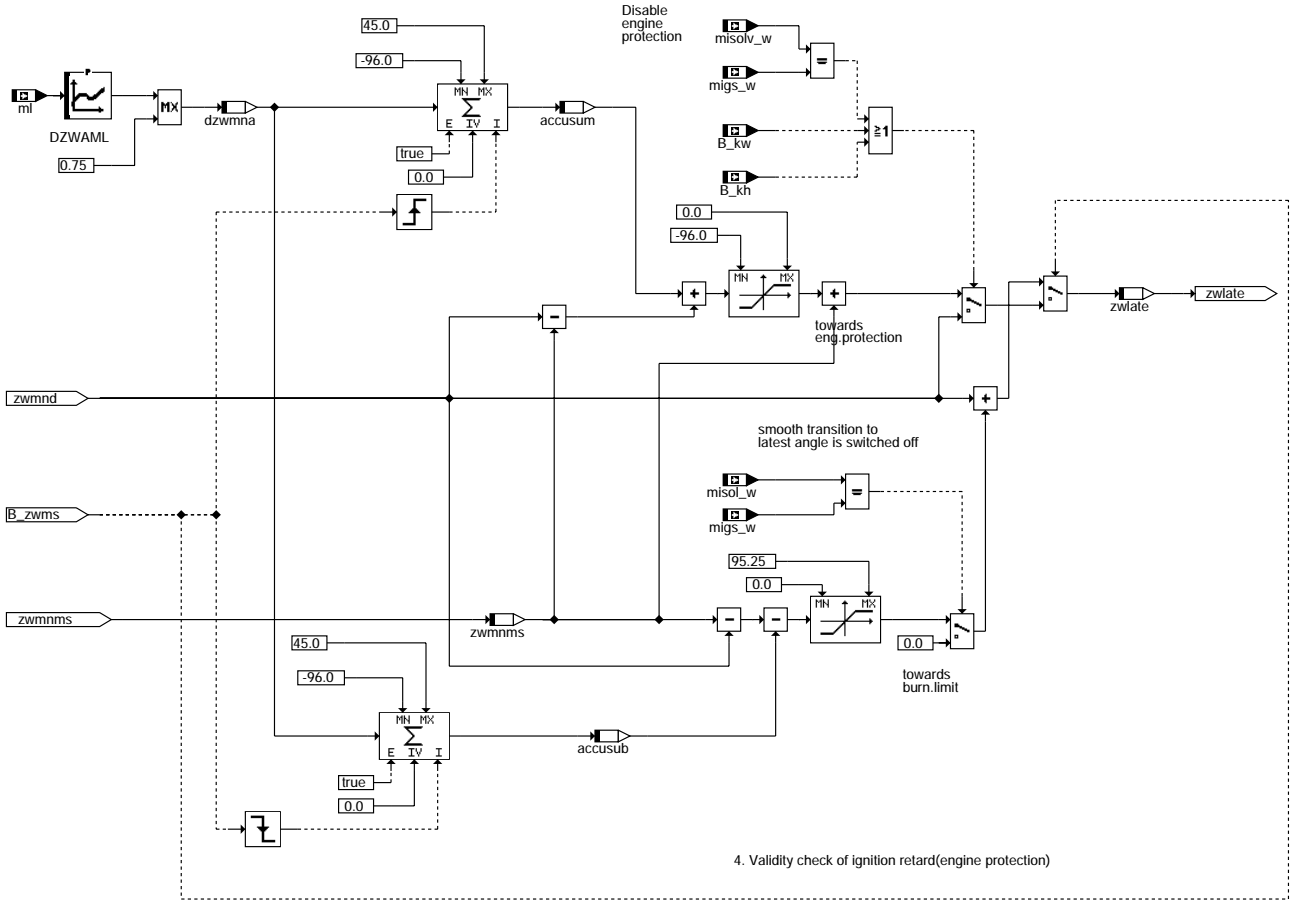
The latest ignition angle  $zwspace$  is calculated either out of burning limit  $zwmnd$ , efficiency demands from catalyst-heating  $zwmnk$  or engine protection  $zwmnms$

Min. torque efficiency  $etazwmn$  that can be reached by torque-coordination

1. Basic Structure

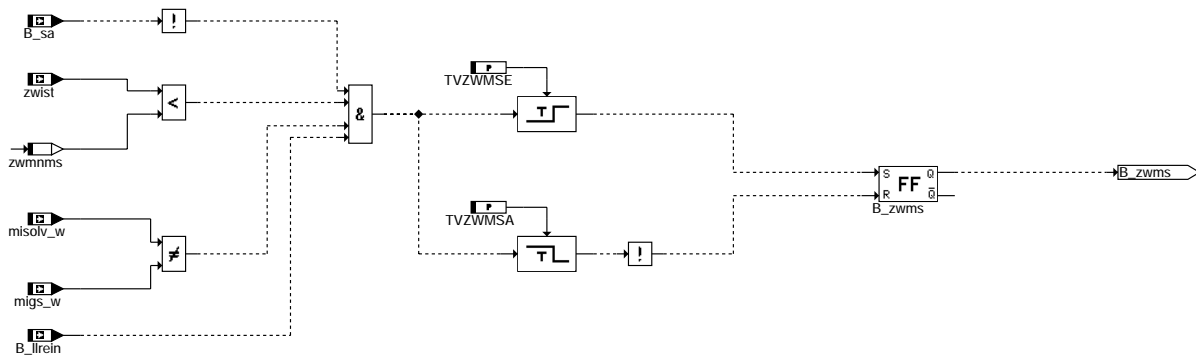
zwmin-main

zwmin-main



zwm-in-control

**zwm-in-control**



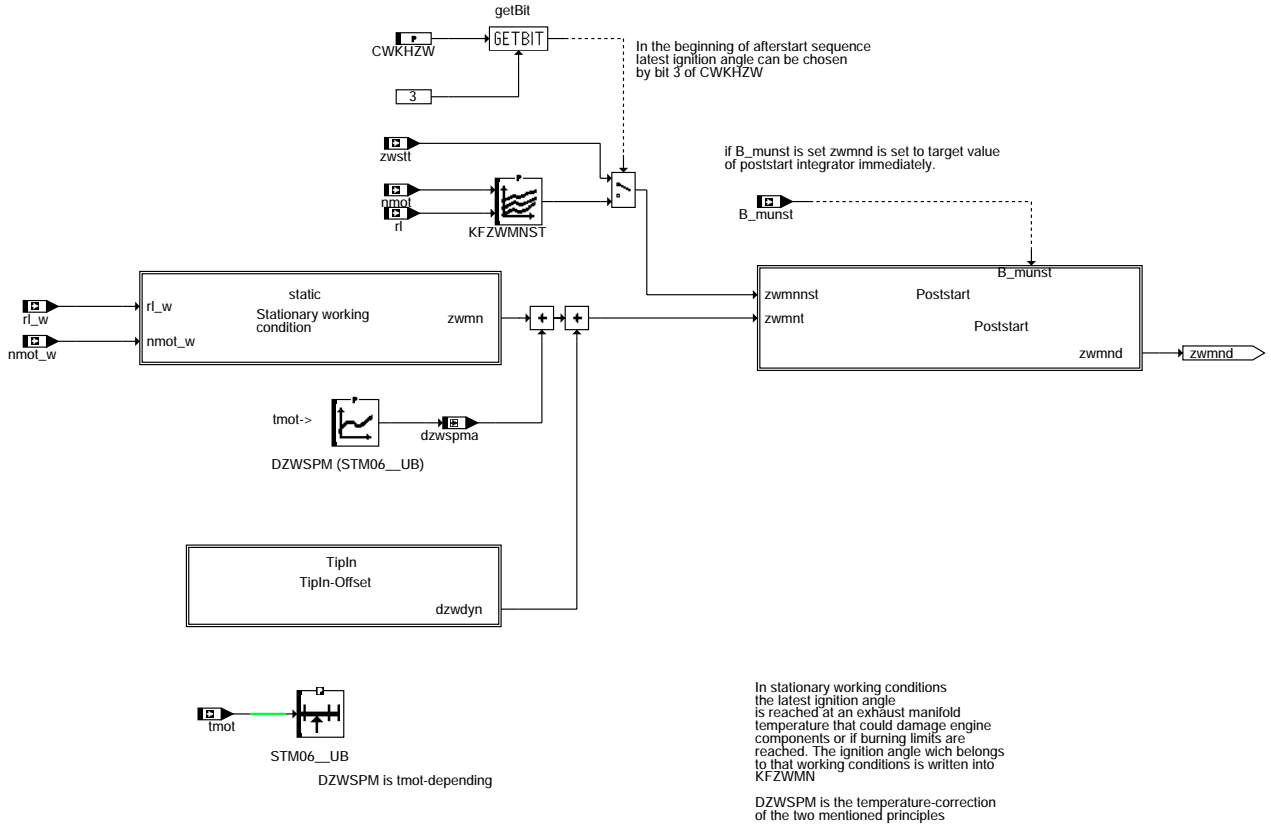
Engine protection B\_zwms is switched on if zwst is retarded to angles smaller than zwmnms (engine protection ignition angle) and no trailing throttle fuel cutoff (B\_sa) is on and no torque reduction from the automatic gear box is demanded

If B\_zwms is TRUE then the latest ignition angle is advanced from zwmnd to zwmnms. If catalyst warm-up or hold of catalyst temperature is active or automatic gear box is demanding torque reduction then the ignition angle is switched to zwmnd immediately.

2. Choose of engine protection mode

**zwm-in-ber-b-zwms**

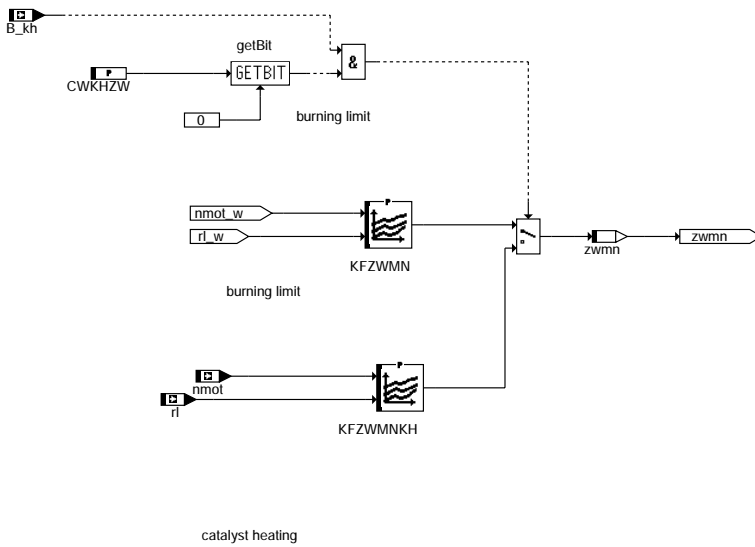
zwm-in-ber-b-zwms



3. Burning-/temperatur condition

**zwmin-temp**

If catalyst warm-up is active, a extended limit for the latest ignition angle could be necessary. This area is only active in a small low dynamic r/nmot-window.

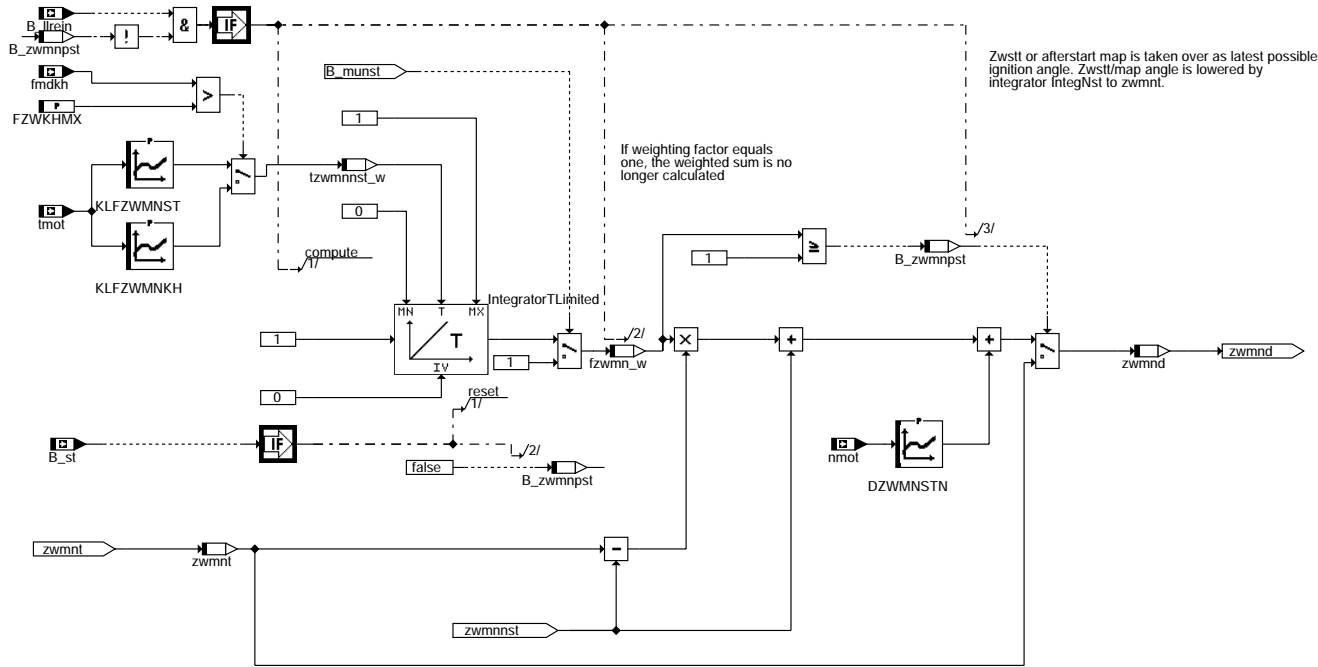


3.2 Stationary working condition

**zwmin-static**

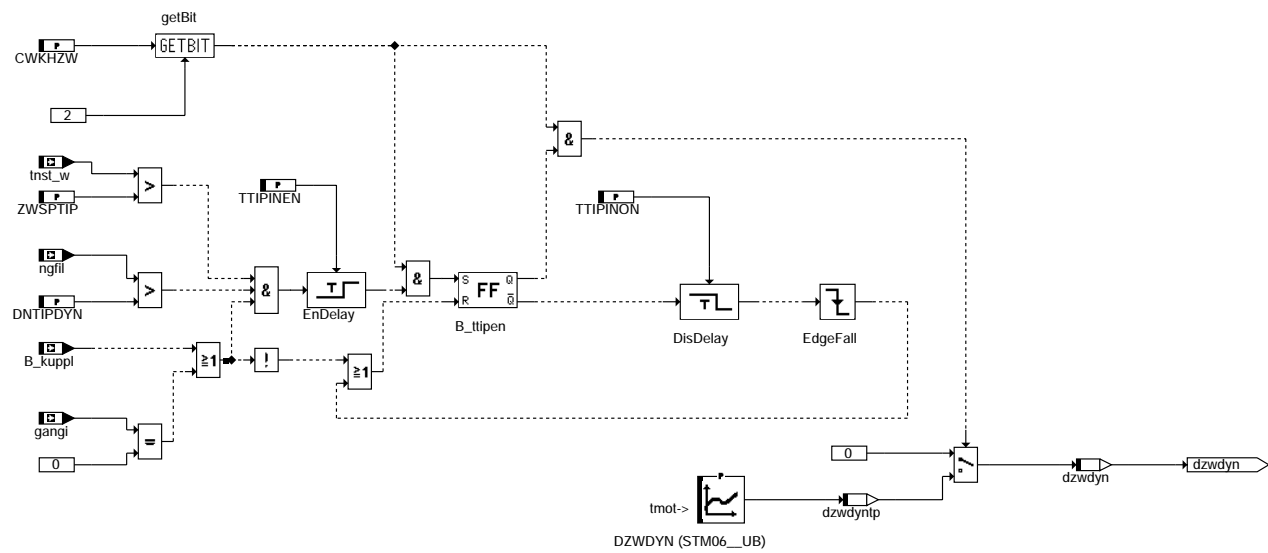
zwmin-temp

zwmin-static



3.1 poststart

**zwmin-poststart**



3.3 Tip In

**zwmin-tipin**



**zwmin-initialize**

zwmin-poststart

zwmin-tipin

zwmin-initialize





## ABK ZWMIN 3.140 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWKHZW			FW	Codeword for calculation of latest ign.angle out of catalyst warm-up
DNTIPDYN			FW	Turn on limit for Tip-In offset on max. spark retard
DZWAML	ML		KL	Up/down regulation speed between the maps of limitation
DZWDYN	TMOT		KL	Spark advance for burning-limit angle at tip-in
DZWMNSTN	NMOT		KL	nmot dependent offset on latest ign. angle during start
DZWSPM	TMOT		KL	delta latest ignition angle relative to engine temperature
ETADZW	DZWSPA		KL (REF)	ignition efficiency depending on delta ignition angle
FZWKHMX			FW	Normalization factor torque reserve for catalyst heating
KFZWMMN	NMOT_W	RL_W	KF	Map for minimal ignition angle
KFZWMNKH	NMOT	RL	KF	Map for minimal ignition angle catalyst warm-up
KFZWMNST	NMOT	RL	KF	minimal ignition spark advance for engine start and after start
KFZWMS	NMOT	RL	KF	Map for ignition value as latest possible value
KLFZWMNKH	TMOT		KL	Spark retard gradient of burning limit during after-start at cat.heating
KLFZWMNST	TMOT		KL	Spark retard gradient of burning limit during after-start
SNM16ZUUW	NMOT_W		SV (REF)	break point distribution engine speed, 16 base pts.
SRL12ZUUW	RL_W		SV (REF)	break point distribution of relative air charge, 12 base points
STM06_UB	TMOT		SV (REF)	Datapoint distribution, engine temperature, 6 datapoints
TTIPINEN			FW	Time delay for consideration of torque transmission after nmot-dynamik
TTIPINON			FW	On-Time for tip-in offset on max. spark retard
TVZWMSA			FW	Time until transition to continuously retarded limiting
TVZWMSE			FW	Time until transition to dynamic retarded limiting
ZWSPTIP			FW	Enable time for tipin offset on latest ignition angle

Variable	Source	Type	Description
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_KUPPL	SWADAP	EIN	EGAS Condition clutch is disengaged
B_KW	BBKHZ	EIN	Condition catalyst warming
B_LLREIN	LLRMD	EIN	Condition idle speed control is active
B_MUNST	WDKSOM	EIN	Condition allow intervention of torque monitoring
B_SA	MDRED	EIN	Condition fuel cut-off
B_ST	SWADAP	EIN	condition for start
B_ZWMMNPST	ZWMIN	LOK	condition afterstart referring latest ignition angle is reached
DZWDYNTP	ZWMIN	LOK	tip-in correction latest ignition angle
DZWMNA	ZWMIN	LOK	delta ignition angle minimum
DZWOAG	MDBAS	EIN	exhaust recirculation rate-dependent correction of optimum ignition angle
DZWSPA	ZWMIN	LOK	correction ignition angle for latest permissible ignition angle
ETAZWMMN	ZWMIN	AUS	minimum ignition angle effectiveness
FMDKH	BBKHZ	EIN	Weighting factor torque reserve for catalyst heating
FZWMN_W	ZWMIN	LOK	fade out factor for latest ignition angle during afterstart
GANGI	SWADAP	EIN	Engaged gear
MIGS_W	SWADAP	EIN	desired indicated torque form GS for quick intervention
MISOLV_W	MDKOG	EIN	indicated resultant nominal torque before torque limitation
MISOL_W	MSF	EIN	indicated resultant nominal torque
ML	SWADAP	EIN	air mass flow
NGFIL	SWADAP	EIN	filtered engine-speed gradient
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RL_W	EGFE	EIN	relative air charge (Word)
TMOT	SWADAP	EIN	Engine temperature
TNST_W	BBSTT	EIN	time after end of start
TZWMMNST_W	ZWMIN	LOK	time constant for fade out ramp latest ignition angle
ZWIST	ZUE	EIN	real ignition angle
ZWLATE	ZWMIN	LOK	Latest ignition angle after engine protection plausibilisation
ZWMN	ZWMIN	LOK	retarded ignition timing
ZWMND	ZWMIN	LOK	Latest possible dynamic sparc retard
ZWMNMS	ZWMIN	LOK	Latest possible continuous sparc retard
ZWMNT	ZWMIN	LOK	ignition angle at burning limit plus temperature and dynamic-correction
ZWOPT	MSF	EIN	optimal ignition angle
ZWSPA	ZWMIN	AUS	retarded ignition angle
ZWSTT	ZWSTT	EIN	Ignition angle during start

## FW ZWMIN 3.140 Fixed Values

Parameter	Value	Description
CWKHZW		Codeword for calculation of latest ign.angle out of catalyst warm-up
DNTIPDYN		Turn on limit for Tip-In offset on max. spark retard
FZWKHMX		Normalization factor torque reserve for catalyst heating
TTIPINEN		Time delay for consideration of torque transmission after nmot-dynamik
TTIPINON		On-Time for tip-in offset on max. spark retard
TVZWMSA		Time until transition to continuously retarded limiting
TVZWMSE		Time until transition to dynamic retarded limiting
ZWSPTIP		Enable time for tipin offset on latest ignition angle

**FB ZWMIN 3.140 Detailed description of function**

This function supplies the ignition angle retarded as much as possible zwspae and the most retarded ignition-angle efficiency etazwmn for the ignition-angle limitation.

The ignition angle retarded as much as possible is either calculated from the combustion limit KFZWMN, a special catalyst heating map or from the engine protection map. The catalyst heating map is activated optionally via the code word CWKHZW dependent on the catalyst heating concept and on the combustion behavior of the engine.

The map KFZWMN contains the absolutely most retarded ignition angle, at which the engine still combusts. The ignition angles result, if the permissible temperature in the exhaust manifold is being exceeded or if combustion misses occur in the engine due to the retarded position of the ignition angle.

Clearly audible combustions can be observed in the exhaust-system branch during start and during post-start with the ignition angles in KFZWMN. This longer afterburning at cold engine and bad carburation is compensated by the ignition angle at start resp. by the map KFZWMNST. KFZWMNST resp. the ignition angle at start zwstt is controlled down via a ramp to KFZWMN during the post-start. Via the characteristics KLFZWMNST resp. KLFZWMNKH the duration in seconds is set, which is needed by the ramp to travel from a factor zero to 100%. If the catalyst heating reserve fmdkh has been completely built-up, the control duration is set via a catalyst heating characteristic. KFZWMNST/ZWSTT limits the lift of the torque control into the direction retarded in the speed overshoot during the transition from start to idle.

Afterburning occurs more often in the exhaust-system branch at cold temperatures, therefore it is often useful to perform a timing advance on the most retarded ignition angle at cold engine. The shift of the retarding limit via tmot is performed in DZWSPM.

If retarded ignition angles are needed for the catalyst heating function immediately after the start, then these can often only be driven in an rl, nmot-window. In case of load change e.g. such a catalyst heating angle can lead to distinct noise in the exhaust-system branch. A special catalyst heating limitation of the ignition angle can for this reason be performed via KFZWMNKH.

The engine protection map is activated, if the ignition angle was more retarded than the engine protection ignition angle for longer than a debouncing time.

The most retarded ignition angles calculated from the maps are checked for long-term compatibility in another calculation step. That means, an angle KFZWMS that in the long-term does not lead to the engine being damaged may not be exceeded. If fuel cut-off is active or if the automatic transmission requests a torque reduction, the engine protection check is deactivated. Activation and deactivation of the engine protection check are delayed via time constants to prevent jittering of the ignition angle, when the most retarded ignition angle is reached.

If the engine protection check is active, then the ignition angle is controlled via a ramp to the value in KFZWMS, provided it is less than the value in KFZWMS. The increasing control is performed during the post-start phase. If catalyst heating, keeping catalyst warm or torque reduction is performed there by transmission intervention, then immediately branching to the most retarded ignition angle from the combustion criteria is performed in this phase.

The ignition angle is controlled down to zwmd again, if the engine protection check is deactivated. If transmission intervention occurs during the decreasing control phase, an immediate jump to zwmd takes place.

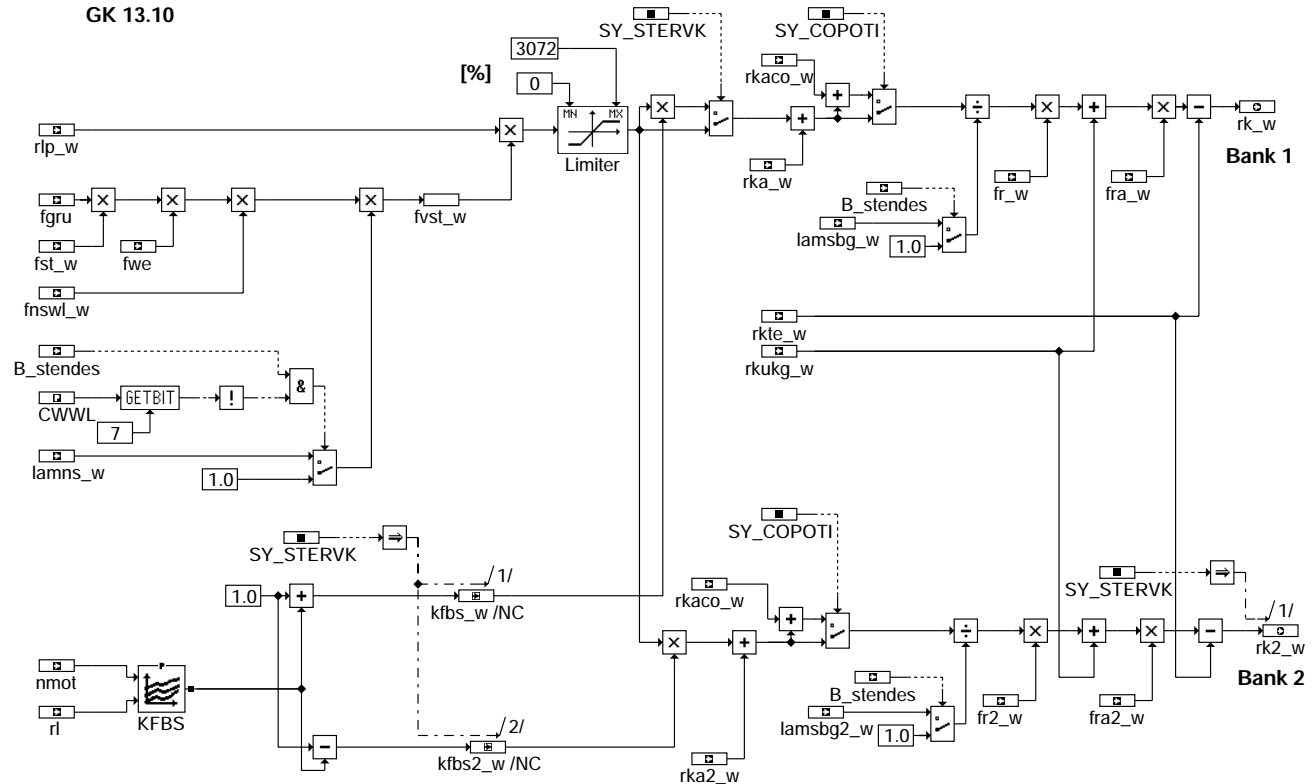
**APP ZWMIN 3.140 Application hint**

The map KFZWSP and the characteristic DZWSPM are to be adjusted such that no misfiring will occur at the respective operating point with the ignition angle retarded as much as possible.

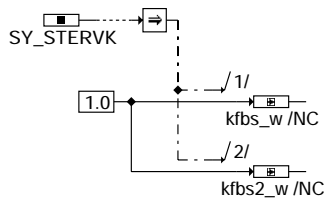
## GK 13.10 mixture control

### FDEF GK 13.10 Function definition

#### GK 13.10



#### gk-main



#### gk-init

### ABK GK 13.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWWL			FW (REF)	code word for warm-up control
KFBS	NMOT	RL	KF	bank-selective mixture factor
SY_COPOTI			SYS (REF)	System constant CO-Poti present
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat

Variable	Source	Type	Description
B_STENDES	ESSTT	EIN	Condition end of start injection
FGRU	ESVST	EIN	factor: basic pilot control
FNSWL_W	ESNSWL	EIN	Factor afterstart and warm-up
FR2_W	LR	EIN	Lambda controller output (word)
FRA2_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FRA_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FR_W	LR	EIN	Lambda controller output (word)
FST_W	ESVST	EIN	start-injection factor
FVST_W	GK	LOK	factor: pilot control
FWE	ESWE	EIN	reinjection factor
KFBS2_W	GK	LOK	Distribution factor bank selective (bank2)
KFBS_W	GK	LOK	Distribution factor bank selective (bank1)
LAMNS_W	ESVST	EIN	lambda engine nominal during afterstart
LAMSBG2_W	LAMSOLL	EIN	required lambda limitation Bank2



Variable	Source	Type	Description
LAMSBG_W	LAMSOLL	EIN	Desired Lambda limitation (word)
NMOT	SWADAP	EIN	engine speed
RK2_W	GK	AUS	relative fuel mass Bank2
RKA2_W	LRA	EIN	additive adaptive correction of the relative fuel amount bank 2
RKACO_W		EIN	Additive correction of the rel. fuel mass for setting idle-speed CO
RKA_W	LRA	EIN	additive adaptive correction of the relative fuel amount
RKTE_W	TEB	EIN	relative fuel part of the purge control
RKUKG_W	ESVST	EIN	rel. fuel mass transition compensation
RK_W	GK	AUS	relative fuel mass
RL	SWADAP	EIN	relative air charge
RLP_W	BGRLP	EIN	rel. air charge predicted for injection calculation (Word)

### FW GK 13.10 Fixed Values

Parameter	Value	Description
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### FB GK 13.10 Detailed description of function

The function GK calculates the relative fuel mass  $rk\_w$  necessary for the predicted relative air charge  $rlp\_w$  of a cylinder, for combustion at  $\Lambda = 1.0$ . The standardisation of the two variables  $rlp\_w$  and  $rk\_w$  was chosen such that, at 100% air charge 100% fuel is also required for combustion with the engine at operating temperature and where  $\Lambda = 1.0$ . The stoichiometric ratio of air mass to fuel mass in the cylinder is designated here as  $\lambda$  combustion chamber, as opposed to  $\lambda$  sensor, which is measured on the  $\lambda$  sensor and may deviate from  $\lambda$  combustion chamber due to the introduction of secondary air. In normal engine operation  $\lambda$ -combustion chamber =  $\lambda$ -sensor.

The function ESVST delivers the pre control values  $fgru$ ,  $fst\_w$ ,  $fswl\_w$ ,  $fwe$  for  $\lambda$ -combustion chamber = 1.0.

This  $\lambda$  combustion chamber can be shifted to "rich" or "lean" by way of the desired value of  $\lambda$  LAMSOLL to improve engine running (engine protection, lean running limit) or to comply with exhaust specifications.

The function GKRA includes mixture adaptation ( $rka\_w$ ,  $fra\_w$ ), canister purge ( $rkte\_w$ ), canister purge diagnosis and  $\lambda$  control ( $fr\_w$ ).

The continuous  $\lambda$  controller controls each bank to the required  $\lambda$  ( $lamsbg\_w$ ,  $lamsbg2\_w$ ), which is formed in the function overview LAMSOLL.

During secondary air the input for  $\lambda$  controller is  $lamsbg\_w = lamsons\_w$ ,  $lamsbg2\_w = lamsons2\_w$ ,  $\lambda$ -combustion chamber is # 1.0.

At Systems with a two-point  $\lambda$  controller, the  $\lambda$  controller is stopped during  $lamsbg\_w$ ,  $lamsbg2\_w$  # 1.0.

The desired value of  $\lambda$  at  $\lambda$  sensor deviates from  $\lambda$  combustion chamber during secondary air mode.

Calculation of the relative fuel mass  $rk\_w$ :

-----  
The factors  $fgru$ ,  $fst\_w$ ,  $fswl$ ,  $fwe$  are multiplied together and are available for the application as a RAM cell pre-control factor ( $fvst\_w$ ). Multiplication of this pre-control factor by the relative air charge  $rlp$  produces the pre-control value of the relative fuel mass  $rk$  for  $\lambda$ -combustion chamber = 1.0.  
A difference in charge in two-bank systems is corrected by multiplication by means of the bank-selective correction KFBS. Positive values in KFBS signify "enrichment" of Bank1 with simultaneous "enleanment" of Bank2 by the same amount, because the charges of the two banks are composed of the total charge measured by the HFM.

The additive portion  $rka\_w$  from the mixture control GKRA is intended to correct any leakage air which may be present, so that pre-control is also to  $\lambda$ -combustion chamber = 1.0 in this case.

These pre-control values are then corrected bank-selectively to the  $\lambda$  ( $lamsbg\_w$ ,  $lamsbg2\_w$ ) specified by the desired value of  $\lambda$  infunction LAMSOLL.  
The continuous  $\lambda$  controller controls to this specified  $\lambda$  and corrects any deviation by the controller factor  $fr\_w$ ,  $fr2\_w$  bank-selectively.  
In two-point  $\lambda$  control, the controller is stopped ( $fr\_w = 1.0$ ) at a required  $\lambda$  # 1.0, and pre-control defines  $\lambda$  # 1.0.

The transition compensation corrects dynamic effects in the intake manifold wall-applied film by way of the additive intervention  $rkukg\_w$ .

Long-term deviations (errors in the fuel path dominant) from the required  $\lambda$  are adapted as factors  $fra\_w$ ,  $fra2\_w$ .

Finally, the fuel portion directed into the intake manifold by the canister purge is subtracted from this relative fuel demand calculated for the required  $\lambda$  ( $lamsbg\_w$ ), and is delivered for output as  $rk\_w$ ,  $rk2\_w$ .

At systems without  $\lambda$  controller, the pre-control can be correctet by Tester via RAM-cell  $rkaco\_w$ . This fearture is only available if SY\_COPOTI is true.

Switch B\_stendes separates the influence between  $fst$  and  $lamsbg$  during Start. It means: if B-stendes = false -> pre-control is defined by  $fst$ .



## APP GK 13.10 Application hint

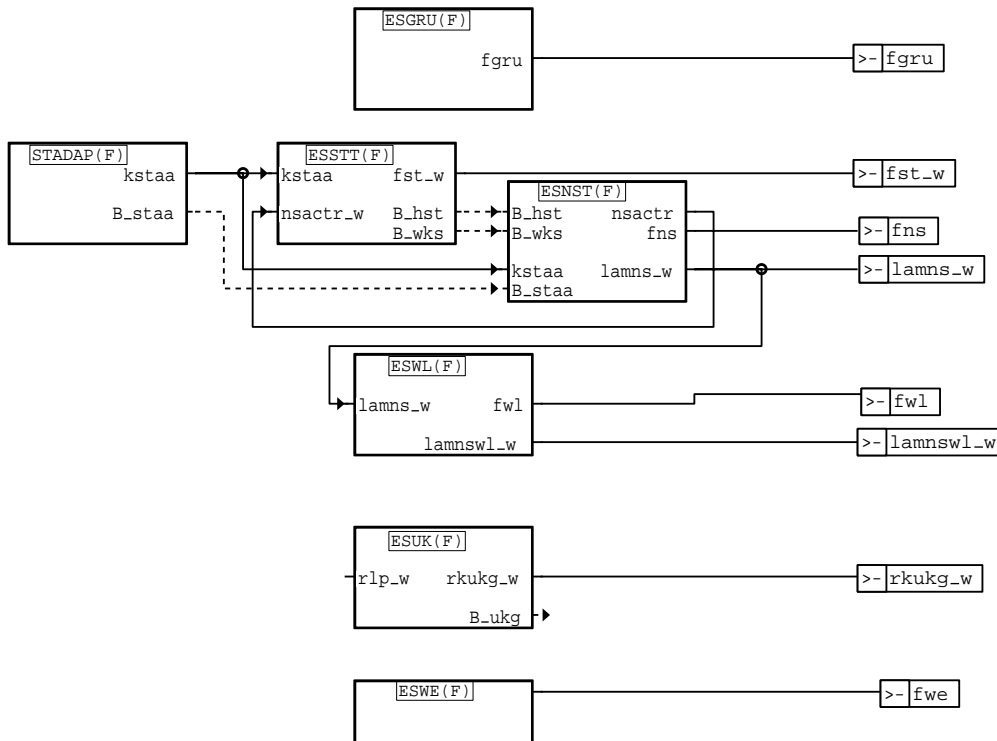
Line KFBS is only available if SY\_STERVK = true

KFBS: Values at Axis-Points: 800, 1200, 1600, 2000, 2500, 3000, 4000, 5000 1/min  
Values of Line: Neutral value is 0.  
Factor 0.1 corresponds to 10% enrichment on Bank1 with simultaneous 10% enleanment on Bank2

CWWL Bit 7: 0 -> lamns\_w is calculated  
CWWL Bit 7: 1 -> lamns\_w has no influence

## ESVST 4.20 Fuel injection pre-control

### FDEF ESVST 4.20 Function definition



esvst-esvst

### ABK ESVST 4.20 Abbreviations

Variable	Source	Type	Description
B_HST	ESVST	LOK	condition hot start
B_STAA	ESVST	LOK	starting fuel adaptation active at afterstart
B_UKG	ESVST	LOK	condition transient control activated
B_WKS	ESVST	LOK	Condition cold restart
FGRU	ESVST	AUS	factor: basic pilot control
FNS	ESVST	AUS	afterstart factor
FST_W	ESVST	AUS	start-injection factor
FWE	ESVST	AUS	re injection factor
FWL	ESVST	AUS	warm up factor
KSTAA	ESVST	LOK	currently used start mixture adaptation factor
LAMNSWL_W	ESVST	AUS	lambda engine nominal at afterstart and warming up
LAMNS_W	ESVST	AUS	lambda engine nominal during afterstart
NSACTR	ESVST	LOK	afterstart counter/filter
NSACTR_W	ESVST	LOK	afterstart counter 16-bit
RKUKG_W	ESVST	AUS	rel. fuel mass transition compensation
RLP_W	ESVST	LOK	rel. air charge predicted for injection calculation (Word)

### FW ESVST 4.20 Fixed Values

Parameter	Value	Description
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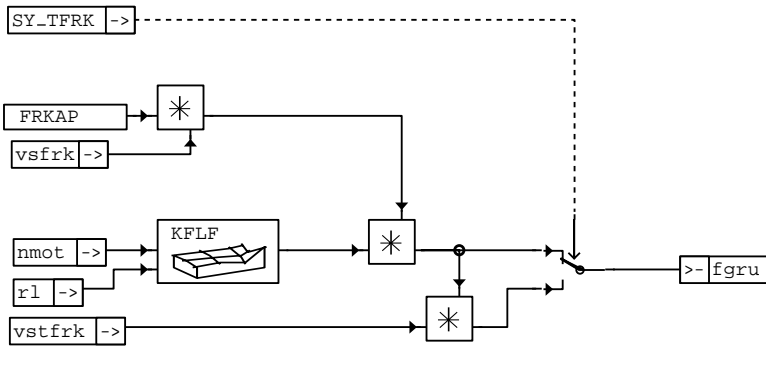
## FB ESVST 4.20 Detailed description of function

The function ESVST provides an overview of the injection pre-control for a combustion chamber Lambda of 1.0, and is composed of the basic injection factor  $fgru$ , the start injection factor  $fst_w$ , the post-start factor  $fns$  and the warm-up factor  $fwl$ . The transition compensation ESUK corrects wall-applied film effects in case of dynamics above the additional or reduced quantity  $rkug_w$ . The additional quantity after cutin of cylinders is calculated as  $fwe$  in function ESWE.

## APP ESVST 4.20 Application hint

## ESGRU 23.30 Basic function injection

### FDEF ESGRU 23.30 Function definition



esgru-esgru

### ABK ESGRU 23.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FRKAP			FW	factor, relative fuel mass for application
KFLF	NMOT	RL	KF	lambda characteristic map at part load
Variable	Source		Type	Description
FGRU	ESGRU		AUS	factor: basic pilot control
NMOT	SWADAP		EIN	engine speed
RL	SWADAP		EIN	relative air charge
SY_TFRK	PROKON		EIN	system constant service device correction of relative fuel mass rk
VsFRK	VS_VERST		EIN	Correction of the relative fuel mass by adjusting systems
VSTFRK			EIN	Correction of the relative fuel mass by tester

### FW ESGRU 23.30 Fixed Values

Parameter	Value	Description
FRKAP		factor, relative fuel mass for application

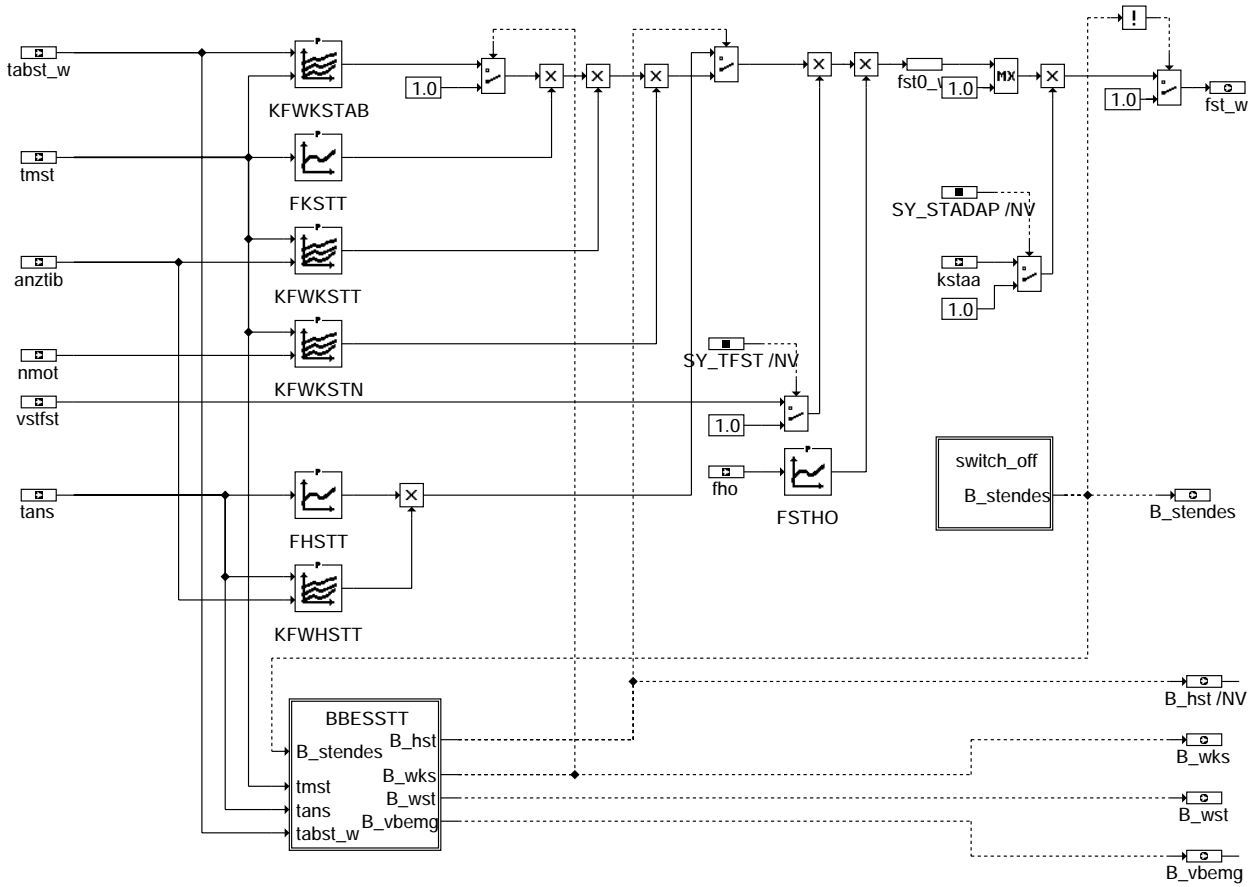
### FB ESGRU 23.30 Detailed description of function

The KFLF map should not be used for intervening in the mixture, because the relative air charge  $rl$  must be balanced to the engine demand via the pulsation map KFPUP. If  $rl$  is corrected by KFPUP faktor  $fgru$  has to be 1.0. The two interventions  $vsfrk$  and  $FRKAP$  are multiplying interventions via application devices.  $FRKAP$  is changed by VS100 adjustment;  $vsfrk$  by VS20 or via the serial interface. These two interventions must be set to neutral during definition after start of production

APP ESGRU 23.30 Application hint

ESSTT 22.10 Injection duration at start

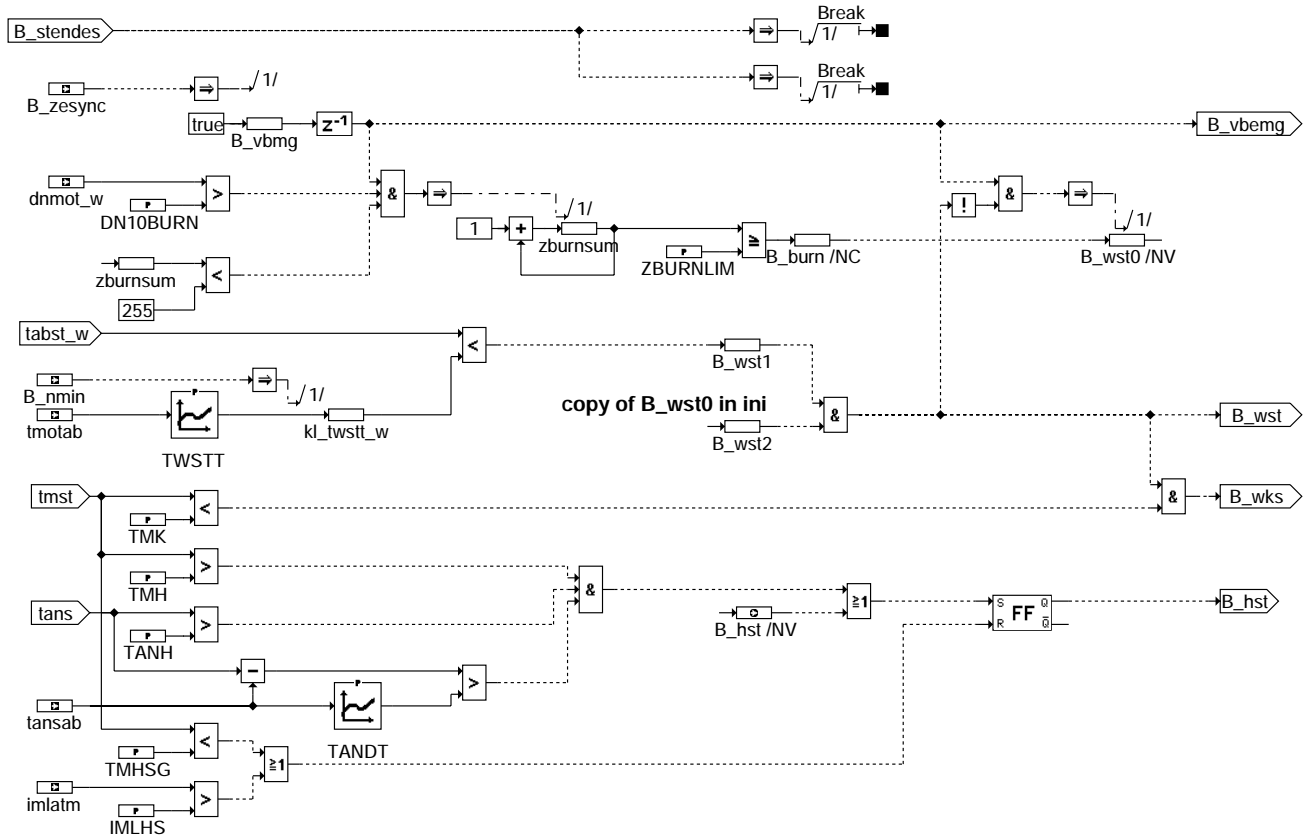
FDEF ESSTT 22.10 Function definition



esstt-main

esstt-main

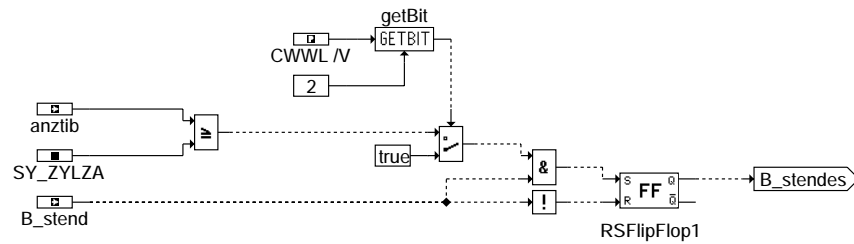
Subfunctionblock 1: Conditions



esstt-bbesst

Subfunctionblock 2: Switch off of start injection

switch off start-up injection



esstt-switch-off

Injection during start-up:

The function is broken down into cold/warm start-up and hot start-up. In the hot start-up, effects from hot gasoline (enleanments) from increased precontrol can be compensated for to a certain degree. The function permits an adaptation of the start-up specific to the temperature for the start-up factor and the controlled decrease of the quantity of fuel during start-up. A uniform wall build-up and a uniform start-up mixture can be realized for all cylinders by the anztib-dependent weighting/controlled decrease. The states of hot and repeated cold start-up are also transferred to the afterstart and warm up function %ESNSWL. It shall be assured for those projects where there is no tester intervention required in the start-up enrichment for the constant describing the system that SY.TFST = false. With Codeword CWWL(bit 2) it is possible to decide whether this function is switched off when B\_stend = true or to wait until in each cylinder was injected at least one start injection. Especially with engines with many cylinders and a fast rewinding up it is possible that B\_stend is set before each cylinder got a start injection. In order to ensure that each cylinder gets a start injection CWWL(bit 2) can be set to 1.





## Hot start-up:

The aim is the certain detection of a hot start-up. Hot start-up conditions are given when the engine temperature is high for a start-up and the fuel system could heat up (detection by means of the temperature increase in the intake air between shutdown and repeated start). A reset is only then meaningful when the engine has accordingly cooled down again or a certain time has elapsed (flow of a certain air mass) and such that the fuel supply system has been purged. The reset path must therefore also be computed outside of the start-up when there was a hot start-up given. If the hot start-up conditions are still prevailing after the engine has been turned off, then B\_hst is set again during the subsequent start-up if the engine start-up temperature tmst is greater than or equal to TMHSG.

## Restart:

After engine has been switched off, the temperature in the combustion chamber is the same as the engine temperature (cooling water) only after elapse of a certain period of time. If the engine is started again during this time (restart), then the mixture shall be leaned in order make allowance for the higher temperature conditions in the combustion chamber in comparison with tmot.

Two independent criteria play a role for the condition restart. For a restart, both the saved shutdown time tabst\_w must lie below the threshold TWSTT (B\_wst1=1) and the number detected firings in the previous start/running or attempted start-up zburnsum must have exceeded the threshold ZBURNLIM, i.e., it shall apply that B\_wst2 = 1 (warming up of the combustion chamber). B\_wst2 is calculated during initialization from B\_wst0. B\_wst0 is calculated in the current start-up for the next cycle and is set by zburnsum exceeding the threshold ZBURNLIM. At restart conditions B\_wst0 is not calculated. So by an unsuccessful start another restart is possible.

If the shutdown time tabst\_w is only determined by means of a control-unit afterrun, then attention shall be paid to conformity of the characteristic curves TWSTT and TNLSGM (refer to %BGTABST). B\_wst1 is formed between the start of the initialization and the detection of start-up (B\_st = 1) since the shutdown time tabst\_w is formed during this time. B\_wst1 remains fixed for a running engine when B\_st is set.

The condition combustion possible B\_vbm is formed by B\_zesync (ignition is synchron to injection). A combustion detection is possible one synchro later. This is expressed by the condition combustion detection possible B\_vbmg. As soon as B\_vbmg is set, the combustion counter is clocked in every synchro process. Firing is detected when an increase in the speed dnmot\_w greater than DN10BURN is given. The condition B\_vbmg is also used for adaptation of the start-up quantity.

If during start-up, B\_wst = 1 and tmst < TMK, i.e. B\_wks = 1, then the start-up factor is weighted with KFWKSTAB. KFWKSTAB depends on the shutdown time tabst\_w and the engine temperature tmst. The conditions B\_wks and B\_hst are also used for the repeated afterstart-up.

## ABK ESSTT 22.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWWL			FW (REF)	code word for warm-up control
DN10BURN			FW	minimum engine-speed difference for ackcn. combustion
FHSTT	TANS		KL	factor hot start
FKSTT	TMST		KL	factor cold start
FSTHO	FHO		KL	weighting of factor start
IMLHS			FW	integrated flow of air-mass at hot start
KFWHSTT	TANS	ANZTIB	KF	map weighting of hot start factor
KFWKSTAB	TABST_W	TMST	KF	factor cold re-start for reduction of starting fuel
KFWKSTN	TMST	NMOT	KF	map weighting of factor cold start
KFWKSTT	TMST	ANZTIB	KF	map weighting of factor cold start
SY_STADAP			SYS (REF)	system constant start adaptation
SY_TFST			SYS (REF)	system constant service device intervention start factor
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TANDT	TANSAB		KL	threshold difference intake air temperature for hot start
TANH			FW	intake air temperature - threshold warm
TMH			FW	engine-temperature - threshold warm
TMHSG			FW	engine temp. hot-start limit
TMK			FW	engine-temperature - threshold cold
TWSTT	TMOTAB		KL	threshold soak time for re-start
ZBURNLIM			FW	threshold detected combustions for re-start
Variable	Source		Type	Description
ANZTIB	ACIFI		EIN	injection counter limited
B_HST	ESSTT		AUS	condition hot start
B_NMIN	GGDPG		EIN	condition lower speed: n < NMIN
B_PWF			EIN	Condition for powerfail
B_STEND	BBSTT		EIN	condition end of start
B_STENDES	ESSTT		AUS	Condition end of start injection
B_VBEMG	ESSTT		AUS	condition detection of combustion possible
B_VBMG	ESSTT		LOK	condition combustion possible
B_WKS	ESSTT		AUS	Condition cold restart
B_WST	ESSTT		AUS	condition for re-start
B_WST0	ESSTT		LOK	Condition restart (part 1: combustions detected)
B_WST1	ESSTT		LOK	Condition restart (part 2: soak time)
B_WST2	ESSTT		LOK	Condition restart (part1: combustions detected in last cycle)
B_ZESYNC	AZUE		EIN	Condition ignition synchronized
DNMOT_W	BGNG		EIN	engine speed difference between two following segments
FHO	BGPU		EIN	Correction factor altitude
FST0_W	ESSTT		LOK	precontrolled start factor 16 bit
FST_W	ESSTT		AUS	start-injection factor
IMLATM	ATM		EIN	integrated air mass flow from engine start to maximum value



Variable	Source	Type	Description
KL_TWSTT_W	ESSTT	LOK	output characteristic line TWSTT
KSTAA	STADAP	EIN	currently used start mixture adaptation factor
NMOT	SWADAP	EIN	engine speed
TABST_W	BGTABST	EIN	soak time
TANS	SWADAP	EIN	Intake air temperature
TANSAB	GGTFA	EIN	Intake air temperature when engine is shut-off
TMOTAB	GGTFM	EIN	engine coolant temperature at engine stop or cut-off cranking
TMST	GGTFM	EIN	engine temperature at start
VSTFST		EIN	adjustment factor start (service device interface)
ZBURNUM	ESSTT	LOK	sum of detected combustions during start

### FW ESSTT 22.10 Fixed Values

Parameter	Value	Description
DN10BURN		minimum engine-speed difference for ackn. combustion
IMLHS		integrated flow of air-mass at hot start
TANH		intake air temperature - threshold warm
TMH		engine-temperature - threshold warm
TMHSG		engine temp. hot-start limit
TMK		engine-temperature - threshold cold
ZBURNLIM		threshold detected combustions for re-start

### FB ESSTT 22.10 Detailed description of function

#### APP ESSTT 22.10 Application hint

##### Prerequisites:

- Torque coordination applied, in particular the frictional losses.
- Basic adaptation for warm engine applied.
- Total filling detection applied.
- Idle-speed control adapted for a warm engine.
- Basic ignition timing, ignition timing during start-up and afterstart as well as torque reserve defined.
- Desired throttle blade position ( with torque structure not active, see %WDKSOM) adapted to a warm engine.

##### Preparatory work:

- Specify fuel and engine oil to be used for the application.
- Shut down start-quantity adaptation %STADAP ( --> kstaa = 1.0).
- Disconnect tank ventilation valve and shut down the tank ventilation function.
- Shut down lambda control and lambda adaptation.
- Shut down the catalyzer heating function.
- Shut down torque loss adaptation.
- For absolutely lambda nominal at afterstart and warm up (CWVL Bit 7 = 1), define lambda nominal for afterstart and warm up in %LANSWL.  
By using a lambda description (CWVL Bit 7 = 0) set lamns-w to 1.0.
- Check the running limits (lalgm > 1, lalgf < 1).
- Define advanced position and type of injection (%ESVW).
- Execute powerfail to reset the values learned.

Cold / warm start-up:  
-----

The start-up factor is stored in FKSTT and weighted with the values from KFWKSTT and KFWKSTN (controlled decrease). Interpolation is not in KFWKSTT but rather the value of the first datapoint is included in the calculations until the next datapoint has been reached. The anzti datapoints shall be selected as whole-number multiples of the number of cylinders. A uniform wall film build-up over all cylinders is thus possible by this. The rl dependency is however to be observed when considering the injection times (ti).

Example.: 4-cylinder --> Datapoints: 0, 4, 8, 12, 16, 20  
6-cylinder --> Datapoints: 0, 6, 12, 18, 24, 30

Proposal for tmst datapoints:  
-30 / -25 / -20 / -15 / -7 / 0 / 15 / 20 / 25 / 40 / 60 / 90 degrees C

Adjustment of the first injection per cylinder: The quantity of fuel for the first injections should already be sufficiently large that a firing is achieved following ignition (to be detected by an increase in the speed after each ignition). To do this, the value 1.0 is entered in KFWKSTT for anzti = 0 for all temperature datapoints and the necessary enrichment factor is described in FKSTT.

The start-up quantity can be (greatly) reduced after the first major injection per cylinder because a wall film has already been built up and heating has thus occurred because of the first firing. It is advisable to make the controlled decrease so steep such that, after approximately 3 injections per cylinder, a "flooding" of the engine is ruled out. It is thus assured by this that the engine can also be started again with certainty even for a restart. The corresponding values are to be entered in KFWKSTT on a temperature-specific basis to do this.

An evaluation of the selected data can be performed using the course for the engine speed.

A correction may be necessary for a start-up at high altitude because of the changed wall-film behavior during the transition from start-up to afterstart. This can be realized by means of the characteristic FSTHO.

In addition to a controlled decrease in the start-up enrichment via anztib, reduction of the start-up factor can be realized with KFWKSTN = f(tmst, nmot). This map can simplify the transfer of data from earlier projects with a start-up factor for a controlled decrease in the speed. Wherever possible for new applications, the data shall be assigned such that KFWKSTN = 1.0.

Repeated cold start-up:  
-----

The condition repeated cold start-up B\_wks is then fulfilled when the condition B\_wst is fulfilled and the engine temperature during start-up tmst is less than the threshold TMK (e.g. 20°C). The condition restart B\_wst is in turn made up of the partial conditions B\_wst2 and B\_wst1. B\_wst2 is then fulfilled when more than one minimum number of firings (e.g. 2) have been detected in the previous start-up or attempted start-up and hence it can be assumed that the combustion chamber have warmed up in comparison with the coolant temperature. The condition B\_wst0 is stored non-volatile and is written to B\_wst2 in the following initialization. So the information is hence always available in B\_wst2 for the next start-up or attempted start-up. B\_wst1 is then fulfilled when the shutdown of the engine has not yet exceeded the threshold TWSTT = f(tmotab) (refer also to %BGTABST). The duration shall be entered in TWSTT, as for how long the restart conditions are given after shutting down or stalling the engine.

In the event of repeated cold start-up the precontrol factor can be reduced by means of the map KFWKSTAB = f(tabst-w, tmst). Values < 1.0 are to be entered in KFWSTAB to do this so that a course for the speed will still be achieved as for a normal start-up at the same start-up temperature tmst.

Hot start-up:  
-----

Hot start-up conditions are present when the fuel supply system (in particular in the region of the injection valves) has heated up considerably. Injection valves shall be installed with a temperature-measuring point near to the tips of the injection valves for clear detection of the hot start-up conditions.

The threshold of the engine temperature tmot, as of which hot start-up conditions can occur, shall be entered in TMH. The threshold of the intake air temperature, as of which hot start-up conditions can occur, shall be entered in TANH. A heating-up of the fuel supply system is deduced by observing the increase in the intake-air temperature tans since shutting down the engine (tansab).

If the increase exceeds the threshold TANDT = f(tansab), then hot start-up conditions can be present.

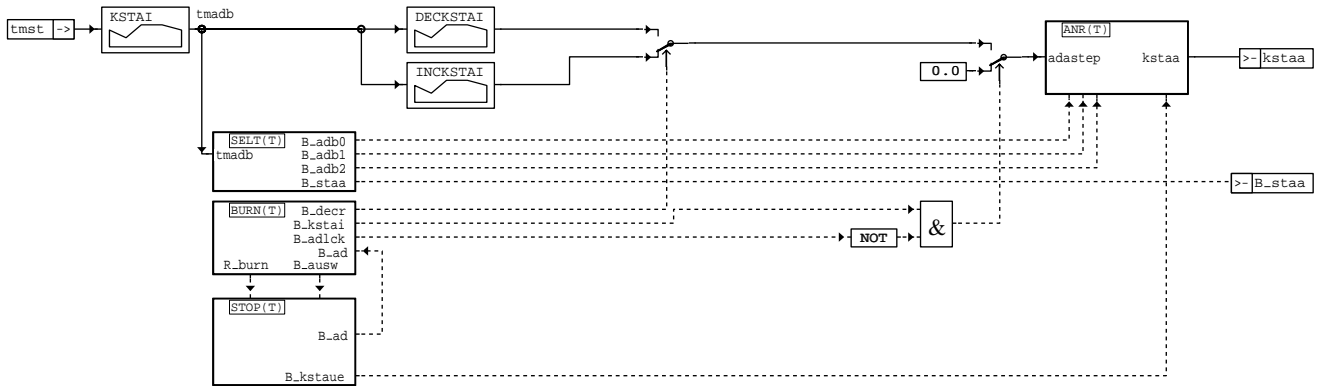
Hot start-up conditions are no longer present if

- a) The engine has been shut down for a certain length of time and hence the fuel supply system has been purged. This is detected by an assessment of the air mass integral imlatm. That value for the integrated air mass shall be entered in IMLHS, as of which a sufficient purging has been carried out. B\_hst is then reset while the engine is still running. The following start-up can again be hot start-up if the conditions for setting have been fulfilled.
- b) The engine has been shut down under hot start-up conditions (B\_hst set) for such a time that the fuel supply has been able to cool down again. The corresponding engine temperature for this shall be entered in TMHSG. For the start-up, B\_hst is reset prior to the first output of ti.

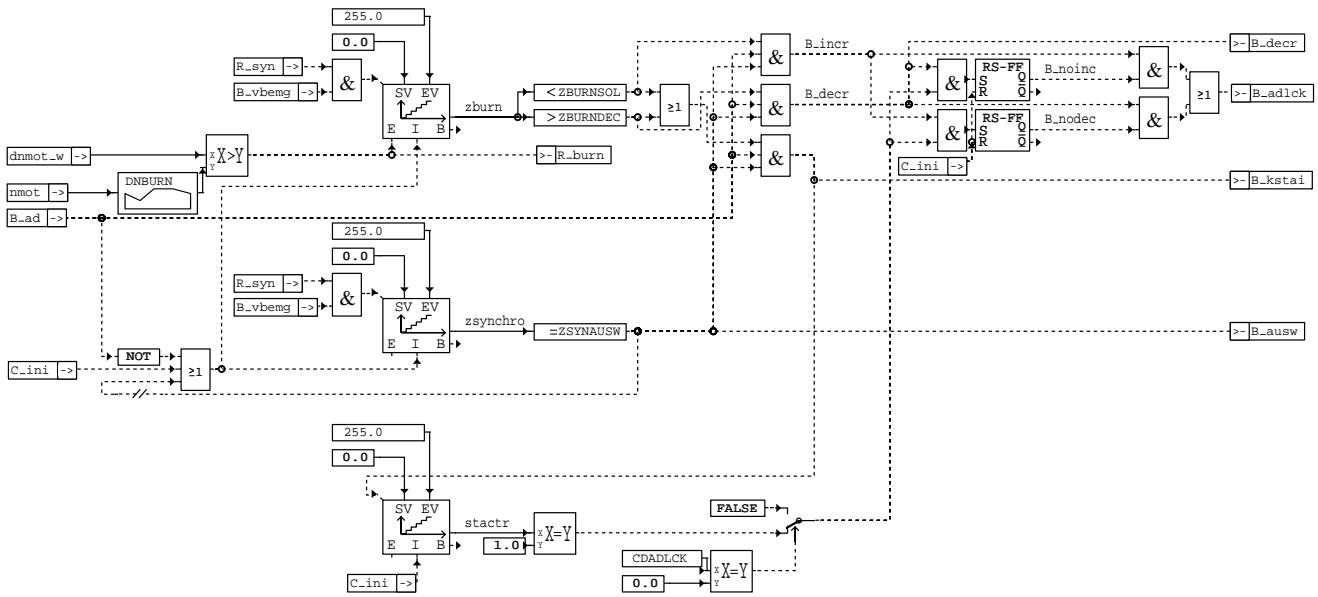
If there are hot start-up conditions prevailing (B\_hst set), then in analogy to a cold start-up adaptation, FHSTT and KFWHSTT shall be applied, though as a dependency on the intake-air temperature tans instead of on the engine temperature tmst. For the application, first the start-up data for tmst = tans shall be taken from the warm adaptation from FKSTT and KFWKSTT (e.g. tmst = 90°C). B\_hst shall be blocked by TMH = 143.25°C. The next step is to check as of which tmst, tans, tansab and injection-valve peak temperatures, the hot start-up problems occur (amongst others, to be detected by using the course for the speed and for lambda). The conditions for setting can be specified by this and the start-up data can be corrected in FHSTT and KFWHSTT on the basis of the lambda course (LSU, pre-heated).

## STADAP 6.30 Starting fuel adaptation

### FDEF STADAP 6.30 Function definition

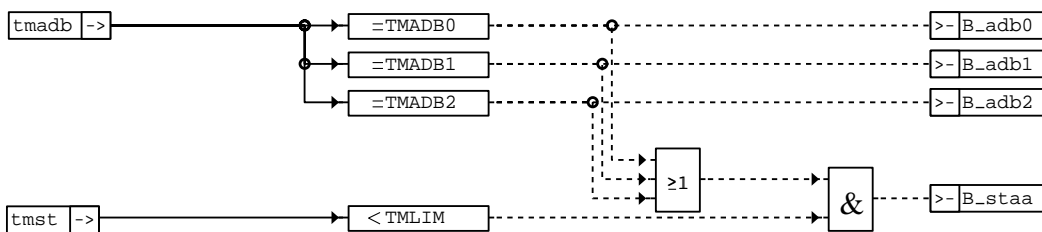


### stadap-stadap



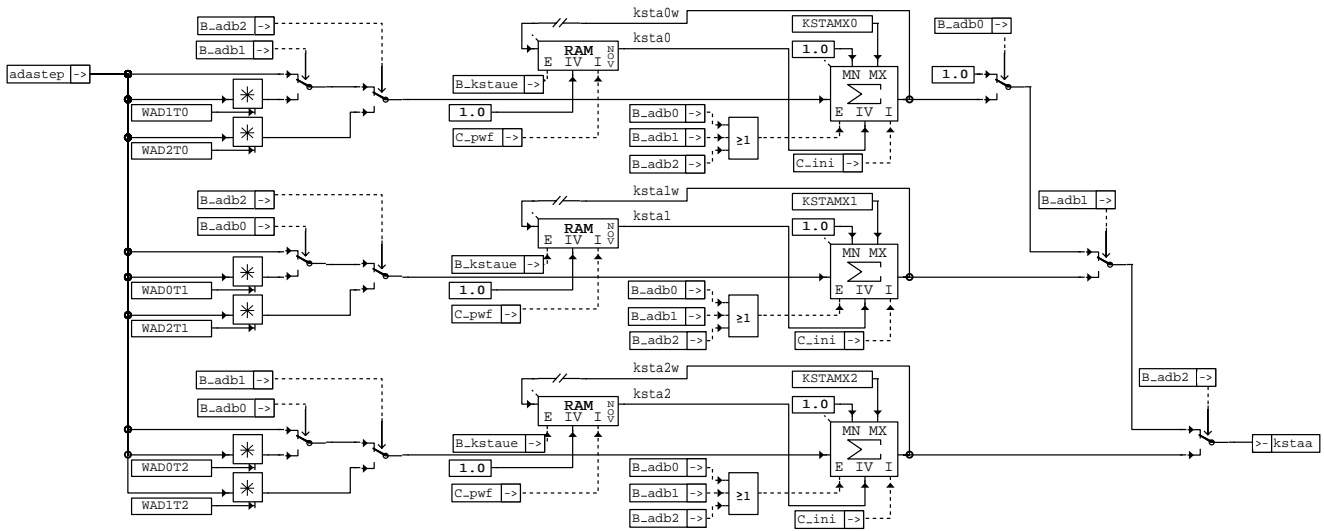
### stadap-burn

Sub-function BURN(T): Evaluation after detected combustion



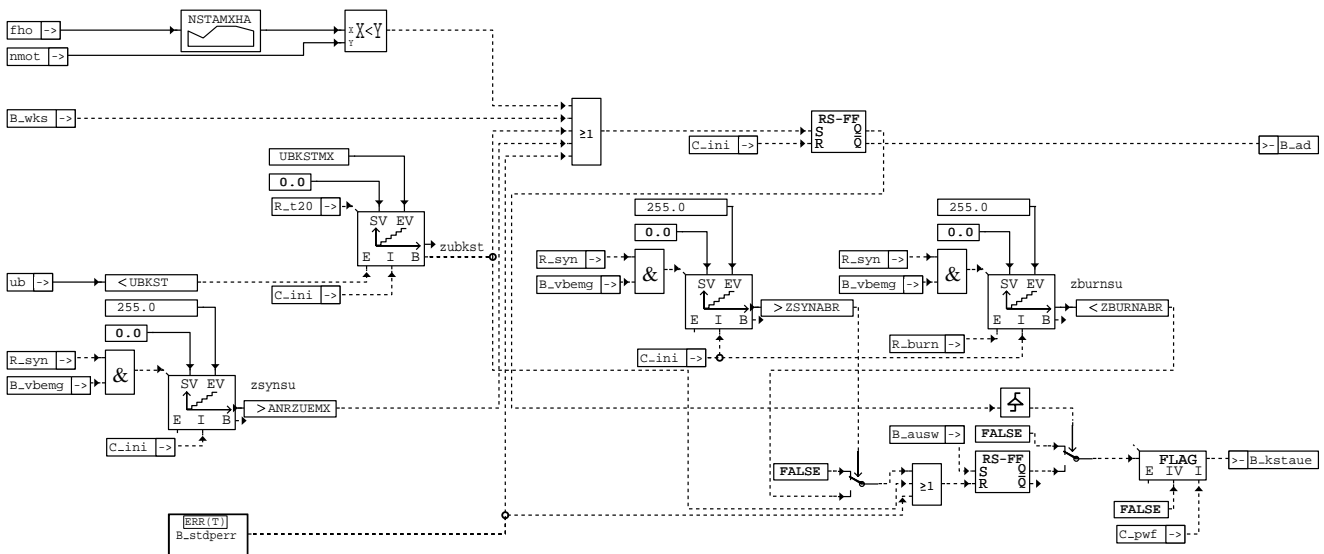
### stadap-selt

Sub-function SELT(T): Choice of temperature range



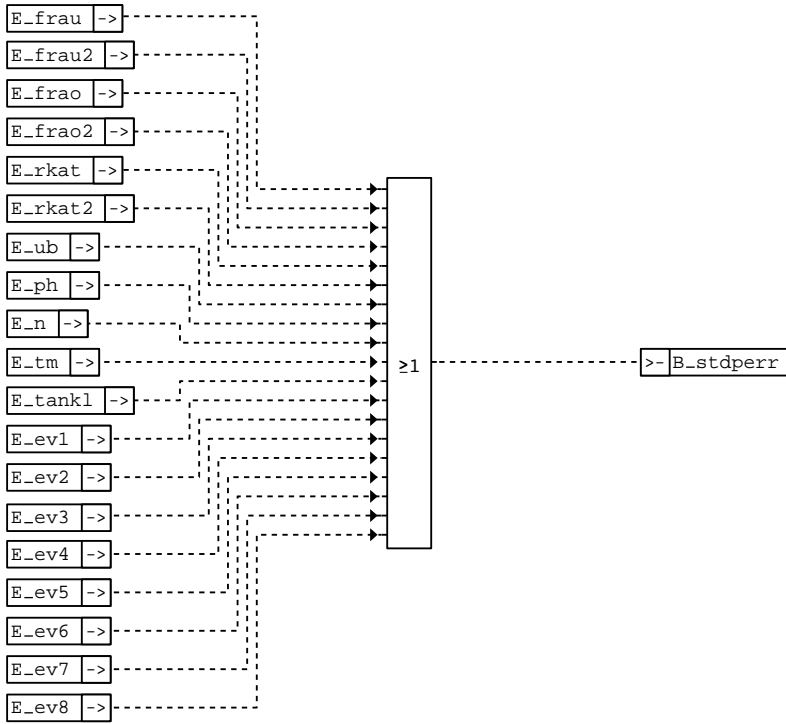
stadap-anr

Sub-function ANR(T): Determination of enrichment factor kstaa



stadap-stop

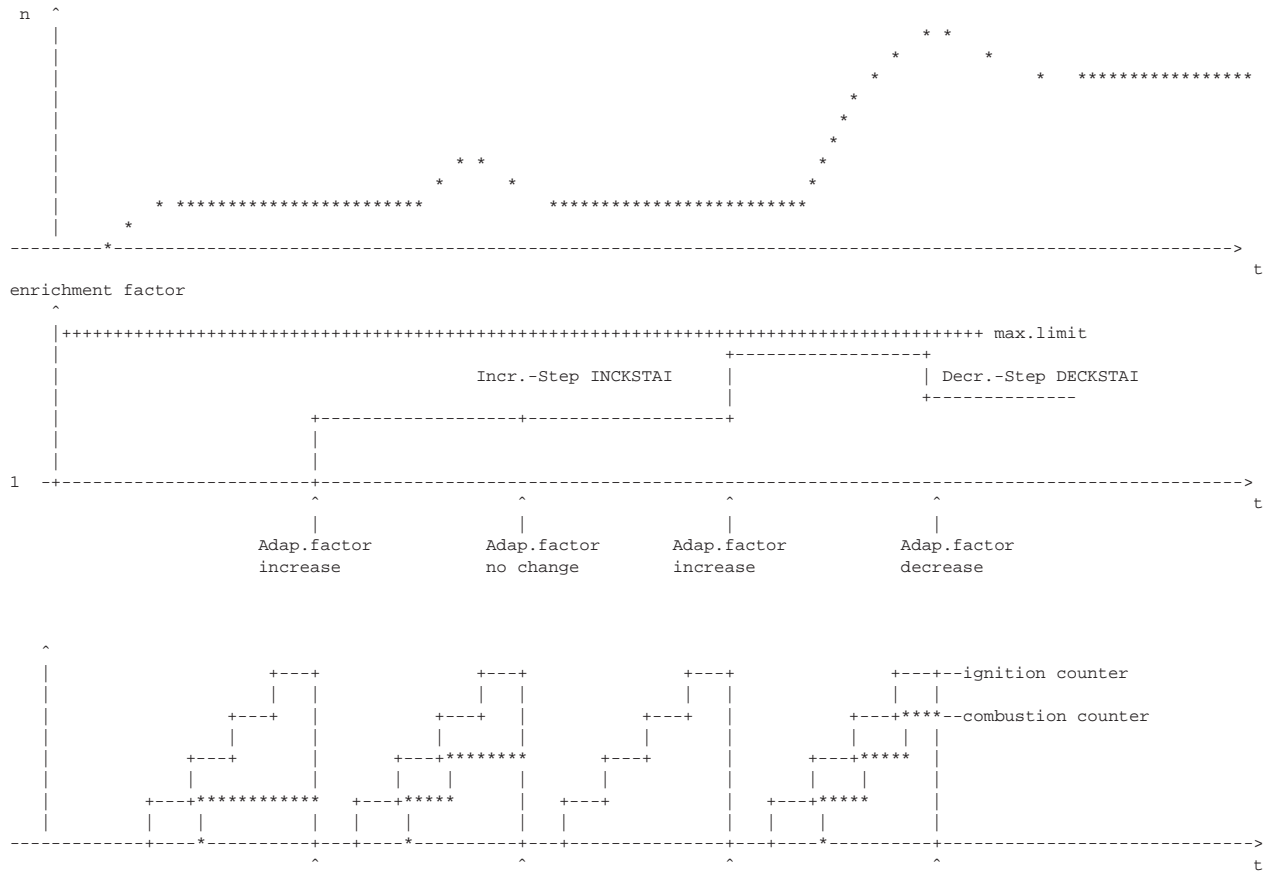
Sub-function STOP(T): Determination of adaption aborting



stadap-err

**stadap-err**

Sub-function ERR(T): Errorflags for adaption aborting



The number of combustions is compared to the limits ZBURNSOL and ZBURNDEC after ZSYNAUSW ignitions. Depending on the result, the adaptation factor is increased, decreased or no change is made.

**General:**

There is a great variety of fuel qualities in the field. Bad fuel qualities can lead to major starting problems, which only can be compensated by enrichment. With the starting fuel adaptation it is possible to adapt an emission-optimized start without any security-offsets. Fill-up of "bad" fuel results in mixture enrichment with STADAP. After re-fill with "good" fuel the function is learning back to the initial value.

**ABK STADAP 6.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
ANRZUEMX			FW	ignition counter limit until STADAP is active
CDADLCK			FW	Code word: Adaptation only in one direction
DECKSTAI	TMADB		KL	decrement-step for STADAP-factor
DNBURN	NMOT		KL	Minimum difference in engine-speed for detected combustion
INCKSTAI	TMADB		KL	increment-step for STADAP factor
KSTAI	TMST		KL	workingrange for STADAP factor
KSTAMX0			FW	Maximum limit of STADAP factor in range 0
KSTAMX1			FW	Maximum limit of STADAP factor in range 1
KSTAMX2			FW	Maximum limit of STADAP factor in range 2
NSTAMXHA	FHO		KL	engine speed limit until STADAP is active depend. on altitude
TMADB0			FW	Range 0 of engine temperature for STADAP calculation
TMADB1			FW	Range 1 of engine temperature for STADAP calculation
TMADB2			FW	Range 3 of engine temperature for STADAP calculation
TMLIM			FW	TMOT threshold for KSTAA active at after start
UBKST			FW	battery-voltage limit for ZUBKSTMX
UBKSTMX			FW	Threshold number of Ubat measurements lower than UBKST for adaptation blocking
WAD0T1			FW	Factor weighting range 0 to 1
WAD0T2			FW	Factor weighting range 0 to 2
WAD1T0			FW	Factor weighting range 1 to 0
WAD1T2			FW	Factor weighting range 1 to 2
WAD2T0			FW	Factor weighting range 2 to 0
WAD2T1			FW	Factor weighting range 2 to 1
ZBURNABR			FW	number of combustions for decision adaptation stop
ZBURNDEC			FW	number of combustions for decrease factor
ZBURNSOL			FW	number of combustions for no change of factor



Parameter	Source-X	Source-Y	Type	Description
ZSYNABR			FW	number of ignitions for stop of STADAP
ZSYNAUSW			FW	number of ignitions until evaluation
Variable	Source		Type	Description
ADASTEP	STADAP		LOK	Adaptation step for STADAP factor
B_AD	STADAP		LOK	Condition adaptation permitted
B_ADB0	STADAP		LOK	Condition adaptation range 0
B_ADB1	STADAP		LOK	Condition adaptation range 1
B_ADB2	STADAP		LOK	Condition adaptation range 2
B_ADLCK	STADAP		LOK	Blocking of an adaptation-step depending on its direction
B_AUSW	STADAP		LOK	Condition evaluation of combustions
B_DECR	STADAP		LOK	Condition decrementation of STADAP factor
B_INCR	STADAP		LOK	Condition incrementation of STADAP factor
B_KSTAI	STADAP		LOK	Condition incrementation/decrementation of STADAP factor
B_KSTAUE	STADAP		LOK	adaption value of start quantity valid at next start
B_NODEC	STADAP		LOK	Condition no decrementation of STADAP factor during current start
B_NOINC	STADAP		LOK	Condition no incrementation of STADAP factor during current start
B_STAA	STADAP		AUS	starting fuel adaptation active at afterstart
B_STDPERR	STADAP		LOK	condition adaptation stopped due to detected error
B_VBEMG	ESSTT		EIN	condition detection of combustion possible
B_WKS	ESSTT		EIN	Condition cold restart
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
DNMOT_W	BGNG		EIN	engine speed difference between two following segments
E_EV1	DEVE		EIN	error flag: injection valve of cyl. 1
E_EV2	DEVE		EIN	error flag: injection valve of cyl. 2
E_EV3	DEVE		EIN	error flag: injection valve of cyl. 3
E_EV4	DEVE		EIN	error flag: injection valve of cyl. 4
E_EV5	DEVE		EIN	error flag: injection valve of cyl. 5
E_EV6	DEVE		EIN	error flag: injection valve of cyl. 6
E_EV7	DEVE		EIN	error flag: injection valve of cyl. 7
E_EV8	DEVE		EIN	error flag: injection valve of cyl. 8
E_FRAO	DKVS		EIN	error flag: upper multiplicative mixture adaption factor frao
E_FRAO2	DKVS		EIN	error flag: upper multiplicative mixture adaption factor frao2
E_FRAU	DKVS		EIN	error flag: lower multiplicative mixture adaption factor frao
E_FRAU2	DKVS		EIN	error flag: lower multiplicative mixture adaption factor frao2
E_N	DDG		EIN	error flag: engine speed sensor
E_PH	DPH		EIN	error flag: phase sensor
E_RKAT	DKVS		EIN	error flag DKVS (additive correction per unit of time)
E_RKAT2	DKVS		EIN	error flag DKVS (additive correction per unit of time, bank 2)
E_TANKL			EIN	Error flag: OBDII error due to an empty canister
E_TM	GGTFM		EIN	Error flag: engine temperature tmot
E_JUB	GGUB		EIN	error flag: power supply voltage UB
FHO	BGPU		EIN	Correction factor altitude
KSTA0	STADAP		LOK	coldstart enrichment range 0, buffered
KSTA0W	STADAP		LOK	coldstart enrichment range 0, currently used
KSTA1	STADAP		LOK	coldstart enrichment range 1, buffered
KSTA1W	STADAP		LOK	coldstart enrichment range 1, currently used
KSTA2	STADAP		LOK	coldstart enrichment range 2, buffered
KSTA2W	STADAP		LOK	coldstart enrichment range 2, currently used
KSTAA	STADAP		AUS	currently used start mixture adaptation factor
NMOT	SWADAP		EIN	engine speed
R_BURN	STADAP		DOK	Schedule of detected combustions for starting fuel adaptation
R_SYN	GGDPG		EIN	Synchro schedule
R_T20			EIN	Time schedule 20 ms
STACTR	STADAP		LOK	STADAP counter
TMADB	STADAP		LOK	Range of engine temperature for starting fuel adaptation
TMST	GGTFM		EIN	engine temperature at start
UB	SWADAP		EIN	battery voltage
ZBURN	STADAP		LOK	number of combustions
ZBURNSU	STADAP		LOK	number of all combustions while ZSYNABR
ZSYNCHRO	STADAP		LOK	number of ignitions till combustion evaluation
ZSYNSU	STADAP		LOK	Counter of ignitions for limitation of STADAP factor
ZUBKST	STADAP		LOK	counter: Ub < UBKST

### FW STADAP 6.30 Fixed Values

Parameter	Value	Description
ANRZUEMX		ignition counter limit until STADAP is active
CDADLCK		Code word: Adaptation only in one direction
KSTAMX0		Maximum limit of STADAP factor in range 0
KSTAMX1		Maximum limit of STADAP factor in range 1
KSTAMX2		Maximum limit of STADAP factor in range 2
TMADB0		Range 0 of engine temperature for STADAP calculation
TMADB1		Range 1 of engine temperature for STADAP calculation
TMADB2		Range 3 of engine temperature for STADAP calculation
TMLIM		TMOT threshold for KSTAA active at after start
UBKST		battery-voltage limit for ZUBKSTMX
UBKSTMX		Threshold number of Ubat measurements lower than UBKST for adaptation blocking
WAD0T1		Factor weighting range 0 to 1
WAD0T2		Factor weighting range 0 to 2





Parameter	Value	Description
WAD1T0		Factor weighting range 1 to 0
WAD1T2		Factor weighting range 1 to 2
WAD2T0		Factor weighting range 2 to 0
WAD2T1		Factor weighting range 2 to 1
ZBURNABR		number of combustions for decision adaptation stop
ZBURNDEC		number of combustions for decrease factor
ZBURNSOL		number of combustions for no change of factor
ZSYNABR		number of ignitions for stop of STADAP
ZSYNAUSW		number of ignitions until evaluation

## FB STADAP 6.30 Detailed description of function

Function definition:

Main issue of the function is the evaluation of combustions. A combustion is detected when the difference in engine-speed from one segment to the next is higher than DNBURN.

After B.vbemg is set an ignition- and a combustion-counter are activated. If the number of ignitions equals ZSYNAUSW a check is made if the number of combustions is lower than ZBURNSOL or higher than ZBURNDEC. Mixture was too lean when the number of combustions is lower than ZBURNSOL, the start-adaptation factor is incremented by INCKSTAI.

The enrichment can be limited to the values KSTAMXi.

No change to the adaptation factor is done if the number of combustions is between ZBURNSOL and ZBURNDEC. Exceeding of ZBURNDEC results in decrementing the adaptation-factor by DECKSTAI because the mixture seems just right. After this verification ignition- and combustion-counter are reset.

With CDADLCK it can be decided if learning is allowed only in one direction during a single start. If CDADLCK = 1 the first learning appoints in which direction the adaptation is permitted. For example B.nodec is set if it is an incrementation. If zburn > ZBURNDEC (decrementation) appears later during this start, B.nodec prevents a decrementation with B.adlck blocking the adaptation. If CDADLCK = 0, adaptation is permitted in both directions during a single start.

The start-adaptation factor is only used during start (B.st = 1). Parts of the mixture result in wall-wetting from the first start-ti, therefore it's necessary to continue with the adaptation until engine-speed NSTAMXHA is reached. The information about fuel quality can also be considered in afterstart (see %ESNST).

Applications with long starting times and steep start-ti-regulation can lead to maximum enrichment KSTAMXi at the first start attempt. To prevent this, the adaptation is stopped after ANRZUEMX ignitions.

For better consideration of different fuel characteristics an adaptation factor can be calculated for three different temperature ranges. Beyond these ranges the function can be blocked. INCKSTAI, DECKSTAI and KSTAMXi can also be pretended individually for each temperature range. It is also possible to consider adaptation values learned in range x in the other adaptation ranges by pretention of weighting factors WADxTy.

Example: An increase of the adaptation factor in range 1 of 0.1 is calculated during one start. WAD1T0 = 0.5 leads to an increase of the adaptation factor in range 0 of 0.05.

A strict separation of adaptation ranges is possible if all weighting factors WADxTy = 0.

STADAP not allowed

A successful start is uncertain if the battery voltage at start is lower than UBKST for ZUBKSTMX times. The start adaptation is then blocked, a learned adaptation factor is not stored in kstai.

No adaptation is done if cold re-start is detected (B.wks = 0).

Detection of errors (E\_\* = 1) leads to no adaptation; the adaptation factor already learned during this start or start-attempt is not stored in kstai, the last regular adaptation value is used for the following start.

If an engine start is impossible or not required (reason: compression test, empty tank, defects in loom etc.) a wrong adaptation of mixture is prevented by:

After ZSYNABR ignitions the number of detected combustions zburnsu is lower than ZBURNABR and kstai is not stored in kstai because B.kstae = 0. The last regular (error-free) value is used for the following start.

**APP STADAP 6.30 Application hint**Data recommendation  
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	From 1. test suitable for 6 cylinder:	From 6 cylinder test derived for 4 cylinder:
ANRZUEMX	: 42	36
DNBURN	: 30 rpm	30 rpm
UBKST	: 8.5 V	8.5 V
ZBURNDEC	: 3	2
ZBURNSOL	: 3	2
ZSYNAUSW	: 6	4
ZUBKSTMX	: 6	4
ZSYNABR	: 36	28
ZBURNABR	: 2	2

NSTAMXHA : This speed threshold must be selected in the way that the engine speed can reach it during speed increase or overshoot (e.g. for sealevel 900 rpm). In high altitude tests are necessary to find out what speed level can be reached depending on engine temperature. For a certain altitude the minimum must be selected. In most cases the lowest engine temperature where STADAP is active determines this speed threshold.

The adaptation can be controlled variable by choice of data.

Exampes: High values of DNBURN lead to fast enrichment in the adaptation range, low values result in low adaptation-increase and fast adaptation decrease of start enrichment.

At cold re-start the function is not active.

Recommendation for definition of adaptation ranges:

adaptation range 0: -10 ... 0 °C  
adaptation range 1: 0 ... 15 °C  
adaptation range 2: 15 ... 30 °C

KSTAI = 0 within temperature limits for adaptation range 0  
KSTAI = 1 within temperature limits for adaptation range 1  
KSTAI = 2 within temperature limits for adaptation range 2

TMADB0 = 0 for adaptation range 0  
TMADB1 = 1 for adaptation range 1  
TMADB2 = 2 for adaptation range 2

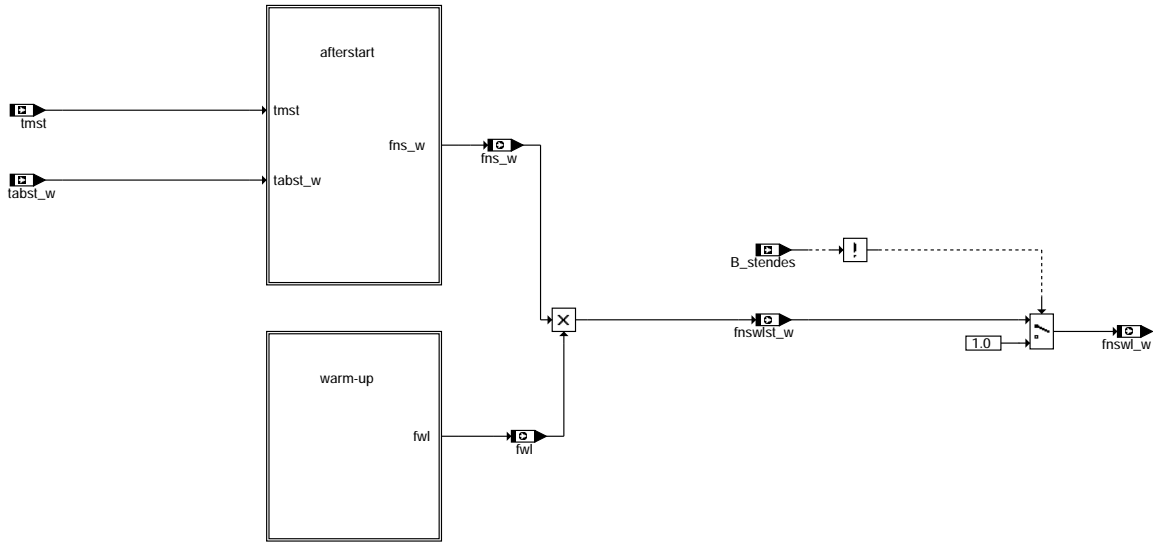
DECKSTAI setpoint = 0 for adaptation range 0  
DECKSTAI setpoint = 1 for adaptation range 1  
DECKSTAI setpoint = 2 for adaptation range 2

INCKSTAI setpoint = 0 for adaptation range 0  
INCKSTAI setpoint = 1 for adaptation range 1  
INCKSTAI setpoint = 2 for adaptation range 2

With application TMLIM = -48 °C the adaptation factor kstaa is not considered in afterstart.

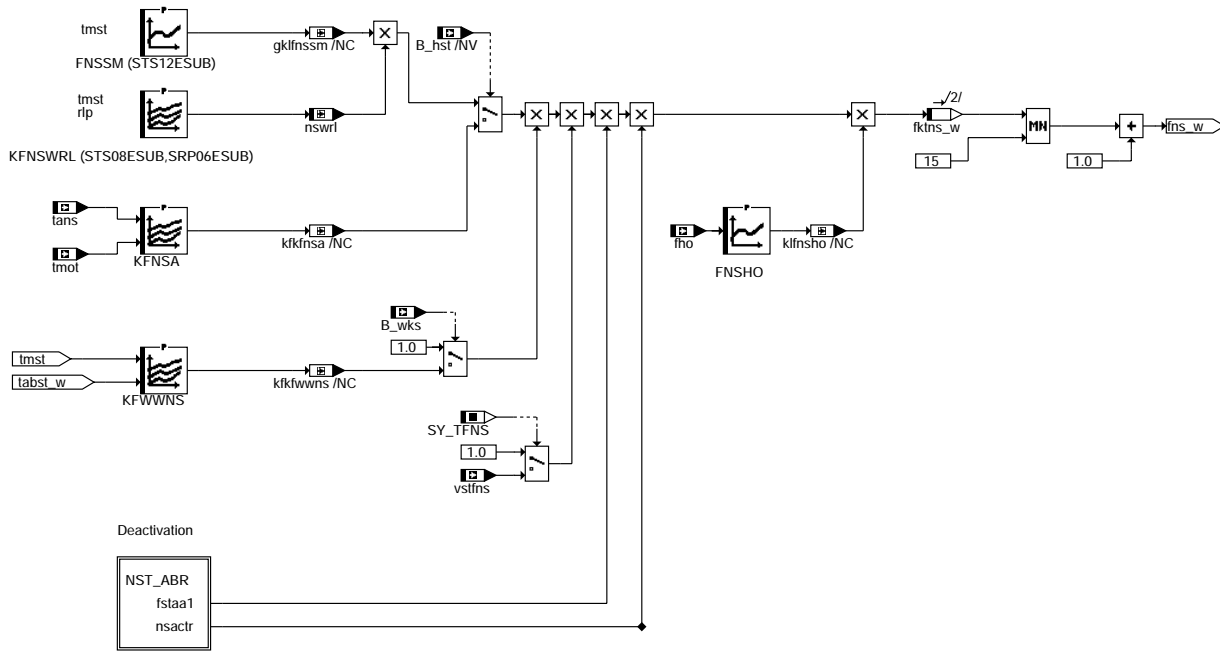
## ESNSWL 2.30 injection during afterstart and warm-up

### FDEF ESNSWL 2.30 Function definition



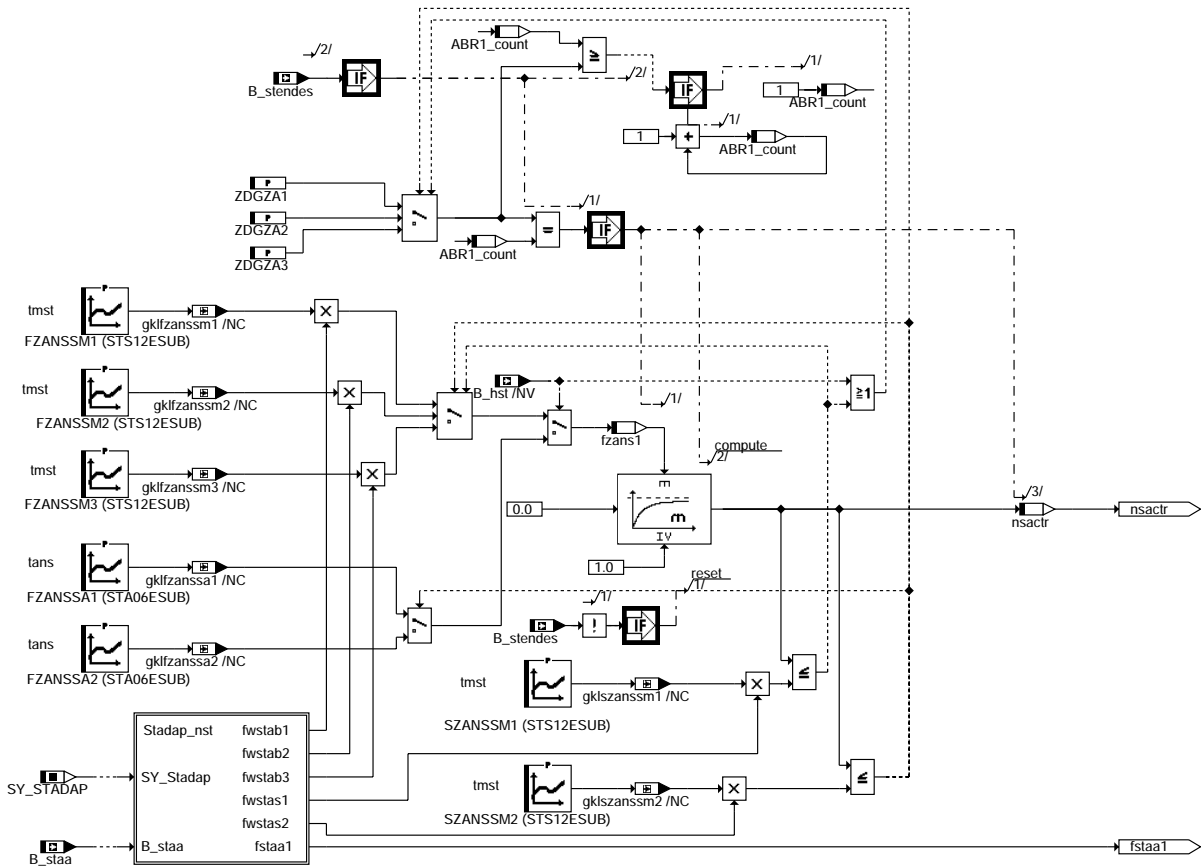
### esnswl-main

#### Subfunctionblock 1: Afterstart



### esnswl-afterstart

## Subfunctionblock 2: Controlled decrease function

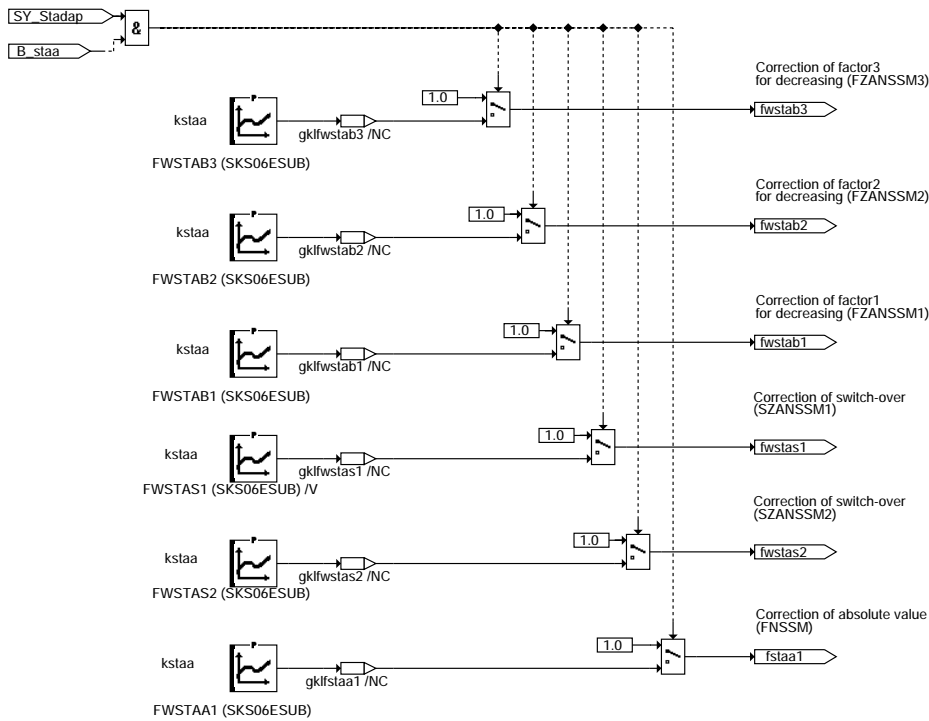


esnswl-nst-abr

esnswl-nst-abr

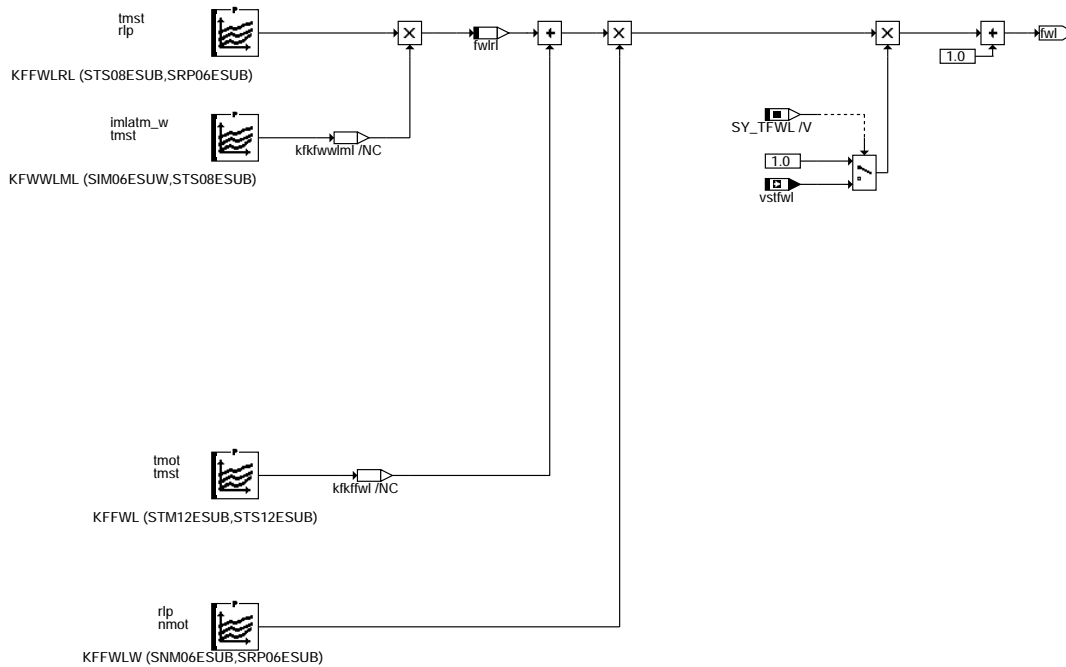
Subfunctionblock 3: Correction of decrease function with active start adaptation function

Afterstart deactivation as function of start adaptation factor kstaa



esnswl-stadap-nst

Subfunctionblock 4: Warm-up



Map KFFWLW is implemented for downward compatibility. For new calibration use KFFWLW as characteristic line = f (nmot)

esnswl-warm-up



## ABK ESNSWL 2.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FNSHO	FHO		KL	weighting of afterstart enrichment
FNSSM	TMST		KL	after start increase
FWSTAA1	KSTAA		KL	afterstart correction
FWSTAB1	KSTAA		KL	weighting afterstart decrease range 1
FWSTAB2	KSTAA		KL	weighting afterstart decrease range 2
FWSTAB3	KSTAA		KL	weighting afterstart decrease range 3
FWSTAS1	KSTAA		KL	correction of threshold 1 for afterstart
FWSTAS2	KSTAA		KL	correction of threshold 2 for afterstart
FZANSSA1	TANS		KL	factor for ign. sync. decreasing of afterstart enrichment at hot start range 1
FZANSSA2	TANS		KL	factor for ign. sync. decreasing of afterstart enrichment at hot start range 2
FZANSSM1	TMST		KL	factor for ign. sync. decreasing of afterstart enrichment above SZANSSM
FZANSSM2	TMST		KL	factor for ign. sync. decreasing of afterstart enrichment below SZANSSM
FZANSSM3	TMST		KL	factor for ign. sync. decreasing of afterstart enrichment in range 3
KFFWL	TMOT	TMST	KF	map warm-up factor
KFFWLRL	TMST	RLP	KF	map warm-up factor load dependent fraction
KFFWLW	NMOT	RLP	KF	map weighting warm-up factor
KFNSA	TANS	TMOT	KF	after start increase
KFNSWRL	TMST	RLP	KF	weighting of afterstart enrichment
KFWWLML	IMLATM_W	TMST	KF	map weighting warm-up factor
KFWWNS	TMST	TABST_W	KF	repeated start time factor
SIM06ESUW	IMLATM_W		SV (REF)	Distribution for integrated air massflow since end of start
SKS06ESUB	KSTAA		SV (REF)	Distribution for the start adaption factor kstaa
SNM06ESUB	NMOT		SV (REF)	Distribution for engine speed
SRP06ESUB	RLP		SV (REF)	Distribution for relative air charge
STA06ESUB	TANS		SV (REF)	Distribution for the air temperature in the intake manifold
STM12ESUB	TMOT		SV (REF)	Distribution for the engine coolant temperature tmot
STS08ESUB	TMST		SV (REF)	Distribution for engine coolant temperature at start
STS12ESUB	TMST		SV (REF)	Distribution for engine coolant temperature at start
SY_STADAP			SYS (REF)	system constant start adaptation
SY_TFNS			SYS (REF)	system constant service device intervention afterstart factor
SY_TFWL			SYS (REF)	system constant service device intervention warm-up factor
SZANSSM1	TMST		KL	switching level 1 of afterstart enrichment
SZANSSM2	TMST		KL	switching level 2 of afterstart enrichment
ZDGZA1			FW	Number of ignitions for decrease in range 1
ZDGZA2			FW	Number of ignitions for decrease in range 2
ZDGZA3			FW	Number of ignitions for decrease in range 3

Variable	Source	Type	Description
ABR1_COUNT	ESNSWL	LOK	afterstart deactivation counter 1
B_FNSOFF	ESNSWL	LOK	Condition switch off calculation of afterstart
B_HST	ESSTT	EIN	condition hot start
B_STAA	STADAP	EIN	starting fuel adaptation active at afterstart
B_STENDES	ESSTT	EIN	Condition end of start injection
B_WKS	ESSTT	EIN	Condition cold restart
FHO	BGPU	EIN	Correction factor altitude
FKTNS_W	ESNSWL	LOK	after start enrichment
FNSWLST_W	ESNSWL	AUS	Factor afterstart and warm-up for max. selection at start
FNSWL_W	ESNSWL	AUS	Factor afterstart and warm-up
FNS_W	ESNSWL	AUS	after start factor
FWL	ESNSWL	AUS	warm up factor
FWLRL	ESNSWL	LOK	Factor warm-up load dependend fraction
FZANS1	ESNSWL	LOK	factor decrease of afterstart
GKLFNSSM	ESNSWL	LOK	output of characteristic line FNSSM (afterstart enrichment depending on tmst)
KFKFWWNS	ESNSWL	LOK	output of map KFWWNS (decrease of afterstart enrichment in case of cold restart)
NSACTR	ESNSWL	LOK	afterstart counter/filter
NSWRL	ESNSWL	LOK	Output KF KFNSWRL weighting of afterstart enrichment
TABST_W	BGTABST	EIN	soak time
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
VSTFNS		EIN	adjustment factor afterstart (service device interface)
VSTFWL		EIN	adjustment factor warm-up (service device interface)

## FW ESNSWL 2.30 Fixed Values

Parameter	Value	Description
ZDGZA1		Number of ignitions for decrease in range 1
ZDGZA2		Number of ignitions for decrease in range 2
ZDGZA3		Number of ignitions for decrease in range 3

**FB ESNSWL 2.30 Detailed description of function**

## General description:

-----

During cold start it must be considered that there are mixture losses from blowby, wall-applied film etc. The required fuel mass to compensate these mixture losses decreases rapidly during afterstart. The mixture losses depend mainly from the temperature in the combustion chamber. In subfunction afterstart the mixture losses are compensated by enrichment depending on starting temperature `tmst`.

Long time mixture losses depend mainly on the engine coolant temperature `tmot`. The compensation of these mixture losses occurs in subfunction warm up. The compensation depends mainly on the engine coolant temperature `tmot`. The subfunctions afterstart and warm up compensation are working together complementary.

The required compensation depends on the injection timing and on the rail pressure.  
For this reason it is necessary to regard the injection timing described in function `%ESVW` too.

Since the engine, as defined in `%LAMKO`, shall always be precontrolled to lambda combustion compartment = 1, the deviation is given towards "rich" by means of a lambda setpoint defined by `lamnswl_w` in function `%LANSWL`. This lambda setpoints enables to precontrol a burnable mixture during cold start. In `%ESNSWL` there should be only a compensation of the mixture losses. But the shift of the lambda setpoint value has do be done in function `%LANSWL`.

## Subfunction afterstart

-----

The function enables compensation by means of an enrichment of the mixture depending on the start-up temperature. The enrichment is gradually decreased by the number of ignitions. The controlled-decrease factor can be selected as a dependency on the engine start-up temperature and on the adaptation factor for the start-up quantity.

The afterstart enrichment can be weighted individually as a dependency of the load for a better allowance of the wall film behavior.

The afterstart mixture can be reduced during a cold restart. The restart detection `B_wks` originates from the start-up function `%ESSTT`.

Enleanments in a hot restart from the formation of bubbles can also be compensated for up to a certain degree by an enrichment of the mixture.

The hot start-up detection `B_hst` originates from the start-up function `%ESSTT`.

Critical fuel qualities also require a change in the afterstart adaptation. The possibility exists to modify the afterstart quantity as a dependency of the adaptation values of the start-up adaptation (`%STADAP`) learned in the start-up.

## Details:

The factors `FWSTAB1..3`, `FWSTAS1..2` and `FWSTAA1` can be specified as a dependency on the start-up adaptation values `kstaa`.

The course for the afterstart factor `fns` can be influenced by this.

`B.staa` comes from `%STADAP`. The functional branch with influence on the fuel quality can be disabled here with `TMLIM`. `TMLIM` is the engine temperature threshold, above which there is no influence on the afterstart factor by the learned adaptation value `kstaa`.

For Projects without `%STADAP` it must be ensured, that `SY_STADAP` = false.

## Subfunction warm up

-----

In subfunction warm up there are two main parts. Depending on the engine temperature at start up and the current engine temperature in map `KFFWL` there is the enrichment for the operation range near to idle.

When the load is higher an additional enrichment depending on the load is possible to compensate worse mixture preparation and different behaviour in wall wetting at the combustion chamber-wall and the piston top. Therefore an additional offset can be calibrated as function of engine temperature at start and relative air charge.

This additional enrichment can be decreased with an increase of the integrated mass of intake air since end of start.

This considers the heat up of the combustion chamber and the components near to the combustion chamber by an increasing number of combustions. A weighting of the enrichment as function of the engine speed is possible, because the conditions for mixture preparation can change at higher engine speed.

## Tester intervention:

-----

It shall be assured for projects where there is no tester intervention in the warm-up enrichment that the constant describing the system `SY_TFWL` and `SY_TFNS` = false. Tester intervention is to be prevented for those projects with continuous lambda control since the tester intervention only acts on the precontrol factor. The variable `lamns_w` acting on the lambda setpoint continues however to be based on the original application, such that the tester manipulation when turning on the lambda control can lead to an offset of the lambda control factor.



## APP ESNSWL 2.30 Application hint

### Prerequisites:

- Refer to %ESSTT

### Preparatory work:

- Refer to %ESSTT
- Lambda setpoint must be defined in %LANSWL

### Notes:

- %ESSTT, %ESNSWL and %LANSWL cannot be applied independently of one another. Therefore approach the nominal lambda from the "rich" side.
- The influence of the the start adaptation (%STADAP) on the afterstart can only be applied, when the application of the start adaptation occurs or is already done.

### Afterstart adaptation in cold / warm start-up:

- Set KFNSWRL(.../...) temporarily to 1.0. The map can subsequently serve to compensate for changes in the load for the transition from start-up into afterstart.  
If afterstart factors greater than 4 are required for low temperatures tmst, this can be realized by values in KFNSWRL between 1.0 and 2.0 (FNSSM already assigned data with the maximum value 4).
- Select FNSSM on the basis of the lambda course in the range of permissible measurement values such that jumps will be avoided and an approximation to the desired lambda lamnswl\_w = lamnswl\_w will be realized from the slightly "richer" side.
- The controlled decrease of the afterstart factor fns is performed by multiplication with the afterstart counter nsactr. This is calculated from:  
$$nsactr\_new = nsactr\_old * (1 - fzans)$$
- The controlled decrease can occur in three ranges.  
The first controlled range for decrease serves to calibrate the transition start-up -> afterstart individual (FZANSSM1).  
The second range serves to compensate for the "fuel losses" during the warm-up phase of the components near to the combustion compartment and hence to take the faster effects into account compared to the cooling water warming up (FZANSSM2).  
The third range of controlled decrease is required in the fine application for a smooth transition into the pure warming-up phase. Should the range of values of FZANSSM3 not suffice in order to reach the desired slow controlled decrease, then a compensation for this can be made by a correction of ZDGZA3 to larger values.
- The level of the controlled afterstart decrease at which changeover to the second range shall take place is specified in the characteristic SZANSSM1 = f(tmst). SZANSSM1 = 0.7 for example, leads to changeover into the second range as soon as the afterstart counter has fallen below the value nsactr = 0.7. The changeover in the third range is defined in SZANSSM2=f(tmst). SZANSSM2 = 0.3 for example, leads to changeover into the third range as soon as the afterstart counter has fallen below the value nsactr = 0.3.  
The values in SZANSSM2 should be smaller than in SZANSSM1.
- The synchro interval can be defined individually for each range of controlled decrease at which the afterstart counter shall be calculated.  
The corresponding values shall be entered in ZDGZA1, ZDGZA2 and ZDGZA3 to do this. ZDGZA1, ZDGZA2 = cylinder number and ZDGZA3 = 2\*cylinder number are proposed as the basis for starting.
- By calibration the afterstart deactivation can be done in two ranges as in previous afterstart functions.  
Then the first deactivation range should be deactivated (SZANSSM1 = max. value, ZDGZA1 = ZDGZA2).
- For a start-up at higher altitudes, a correction of the afterstart factor may be necessary for the transition from the start-up into afterstart because of the changes in the applied evaporation behavior of the fuel. As the influence of a higher altitude is considered in the relative air charge rl, at start-up at higher altitudes an enrichment may be necessary. This can be realized values greater than 1.0 in the characteristic FNSHO.
- Termination of Subfunction afterstart:  
Calculation of afterstart factor is terminated, when the factor nsactr = 0.

### Afterstart adaptation in the restart:

- Only a low quantity of fuel is required in a restart because of the higher combustion-compartment temperatures in comparison to the cooling-water temperature.  
The afterstart enrichment can be reduced by means of KFWWNS = f(tmst/tabst\_w) to do this.

### Afterstart adaptation in the hot start-up:

- The afterstart factor FNSA = f(tans) shall be adjusted such that lambda = 1.0 is given again if possible. A different controlled decrease can also be specified than in the normal case by means of the tans-dependent characteristics FZANSSA1 and FZANSSA2. The changeover from range1 to range 2 is given by SZANSSM2.  
(SZANSSM1 and FZANSSM1 are not active by hot start condition)  
It shall be assured that an adaptation of the start-up quantity is not active in the case of a hot start-up and hence that B.staa = false.  
Refer also to %STADAP.





Afterstart adjustment for critical fuel qualities (with activated %STADAP):

-----  
- Fuel qualities are to be defined for the entire cold adjustment. RB recommends the following:

A fuel A that lies approximately in the center of the DIN standard. Orientation on the winter specification for low temperatures (<10°C), and on the summer specification for temperatures above this.

A fuel B to represent the "worst case" possible in the field, e.g. Reformulated Gasoline (RFG).

The adjustment for start-up, afterstart and warming-up is performed with fuel A. An optimum adjustment does not include any margin of safety. The adaptation of the start-up quantity must now learn during a start-up when using fuel B. Depending on the factor for start-up adaptation, the afterstart enrichment is now modified such that lambda = 1.0 is given again when using fuel B.

- For application it is necessary to enable start adaptation for the desired temperature range via TMLIM in %STADAP (B.staa set).

- The basic application can now be influenced by the factors FWSTAA1, FWSTAS1 and FWSTAS2, and FWSTAB1 to FWSTAB3 = f(kstaa). As the basis, these characteristics shall first be assigned with data of the value 1.0 at all datapoints. Hence the course for the afterstart enrichment is identical to that without any allowance made for the fuel quality.

- Attention shall be paid when defining the datapoint distribution for the Characteristic lines FWSTAA1, FWSTAS1..2 and FWSTAB1..3 (SKS06ESUB) that kstaa can only assume values between KSTAMN and KSTAMX of %STADAP. A datapoint at kstaa = 1.0 is required under all circumstances.

- In order in turn to obtain the afterstart enrichment of an unchanged fuel quality in comparison to the basic application, the value 1.0 must be entered in the characteristics FWSTAA1, FWSTAS1..2 and FWSTAB1..3 under all circumstances for kstaa = 1.0 !

- For FWSTAA1, the afterstart enrichment can in general be changed, i.e. without any influence on the decreasing control function. Values > 1.0 are to also to be applied for kstaa > 1.0 for an increase in the afterstart enrichment.

- FWSTAS1 and FWSTAS2 have an influence on the switchover in the range. Should the switchover into the second range only be at a later point in time for kstaa > 1.0, then values < 1.0 shall be applied in FWSTAS1.

- FWSTAB1, FWSTAB2 and FWSTAB3 influence the controlled decrease in the speed. A faster controlled decrease for kstaa > 1.0 is possible by using values > 1.0, whereas a slower controlled decrease can be realized for kstaa > 1.0 by using values < 1.0.

Proposal for tmot/tmst datapoints:

-----  
-30 / -25 / -20 / -15 / -7 / 0 / 15 / 20 / 25 / 40 / 60 / 90 deg. C

Application of warm up

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- KFFWL has to be calibrated for the operating range near to idle. The aim is that the actual lambda is equal to the lambda setpoint defined in %LANSWL. Now the calibration at "basic load" is done and should not be changed when the calibration at higher loads occurs. So there is less influence between the cold start calibration (e.g. at the cold start test bench) and the calibration at higher load.

- The following calibration at higher load requires a roller test bench with an own drive. With this roller test bench it is possible to set the wheels and transmission system of the car to the desired speed before starting the engine (at idle). So the desired engine speed (setpoint of KFFWLW) is reached very fast after the start-up, by closing the power transmission (engaged gear). With an external potentiometer it is possible to set the accelerator-pedal position to the desired value in order to have a relative constant load during warm up. There should be several warm ups at the same temperature with different loads. The necessary enrichment can be written in the map KFFWLRL. It should be paid attention to the calculation of fwl:  
fwl = (KFFWL + KFFWLRL \* KFWWLML) \* KFFWLW  
This part of the warm up (fwlrl) is decreased by the increasing integrated mass of the intake air (map KFWWLML).  
This Map is function of the integrated air mass since end of start and the engine temperature at start.

Remark to KFFWLW:

The engine speed dependent weighting is done with KFFWLW.

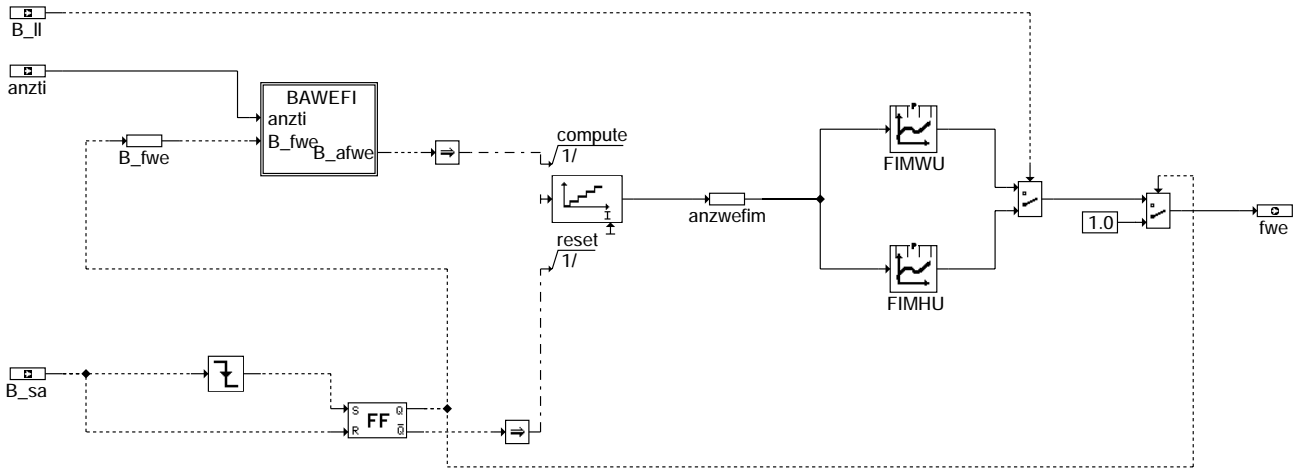
For that, in a transitional phase, KFFWLW is f (nmot, rlp) to offer the possibility to use already existing calibration data from %ESWL. In this case KFFWLRL should be zero.

For new calibration KFFWLW should be used as characteristic line = f(nmot). The enrichment at high load should then be calibrated in KFFWLRL.

## ESWE 1.60 Injection, resumption of overrun fuel cut-off

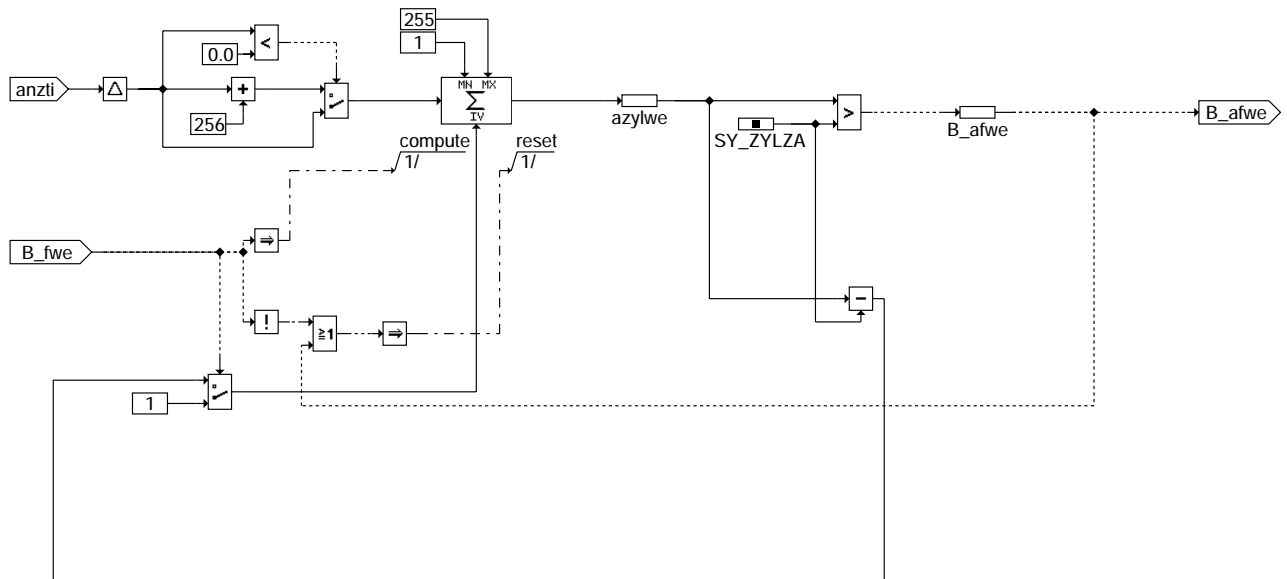
### FDEF ESWE 1.60 Function definition

Overview ESWE

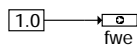


### eswe-main

Overview BAWEFI



### eswe-bawefi



### eswe-initialize

### ABK ESWE 1.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FIMHU	ANZWEFIM		KL	Factor pulse abrupt
FIMWU	ANZWEFIM		KL	Factor pulse smooth
SY_ZYLZA			SYS (REF)	system constant number of cylinders
Variable	Source		Type	Description
ANZTI	ACIFI		EIN	injection counter
ANZWEFIM	ESWE		LOK	number of processed fuel cut-in factors
AZYLWE	ESWE		LOK	number of processed cut-in cylinders
B_AFWE	ESWE		LOK	flag number of restart fuel feed factors
B_FWE	ESWE		LOK	condition factor restart fuel feed
B_LL	MSF		EIN	Condition idle
B_SA	MDRED		EIN	Condition fuel cut-off
FWE	ESWE		AUS	reinjection factor



## FW ESWE 1.60 Fixed Values

Parameter	Value	Description
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## FB ESWE 1.60 Detailed description of function

Calculation of overrun - reinjection factor

Principle:

During overrun conditions possibly the fuel wall layer is completely removed. To counteract a mixture leaning during restart fuel feed it sprays in supplementary fuel to rebuild the fuel wall layer when the injection resumes.

ESWE: Overview

During restart fuel feed (B<sub>sa</sub> changes from 1 --> 0) the first injection pulses can be enriched via a characteristic in relation to the number of released injections after the restart. When the number of injections is changing the counter which counts the restarted cylinders (azylwe) is enable. It considers the possibility of more then one injetions during one segment. The condition B<sub>ll</sub> is used to select between 2 characteristics For soft restarts (B<sub>ll</sub> = 1 ) the characteristic FIMWU applies For hard restarts (B<sub>ll</sub> = 0 ) the characteristic FIMHU applies

## APP ESWE 1.60 Application hint

Pre setting of Parameter:

FIMHU: fixed characteristic with 16 points, first point about 1.6, exponential relaxation  
FIMWU: fixed characteristic with 16 points, first point about 1.2, exponential relaxation  
no interpolation

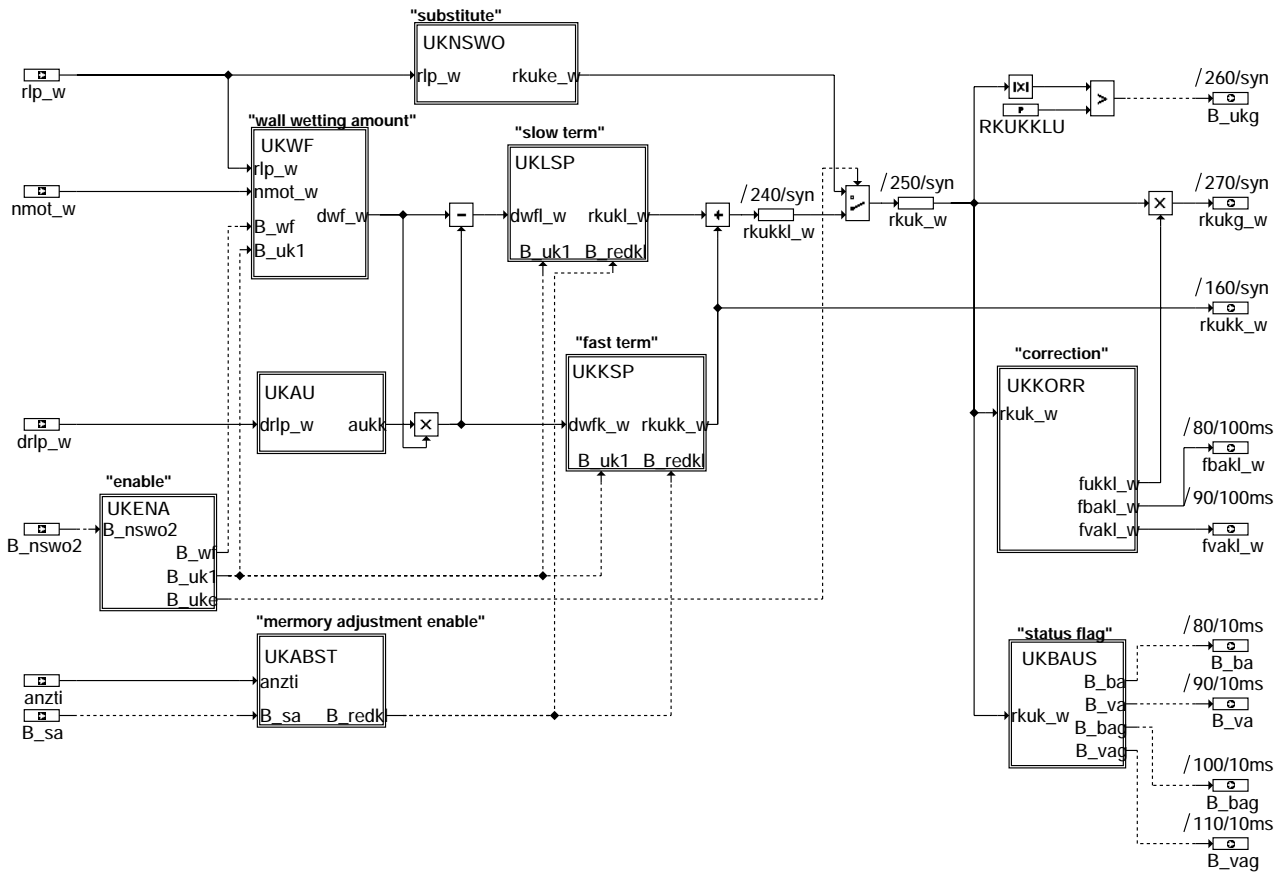
Link to other functions:

%GK :(fwe)

## ESUK 4.50 Injection: transient compensation

### FDEF ESUK 4.50 Function definition

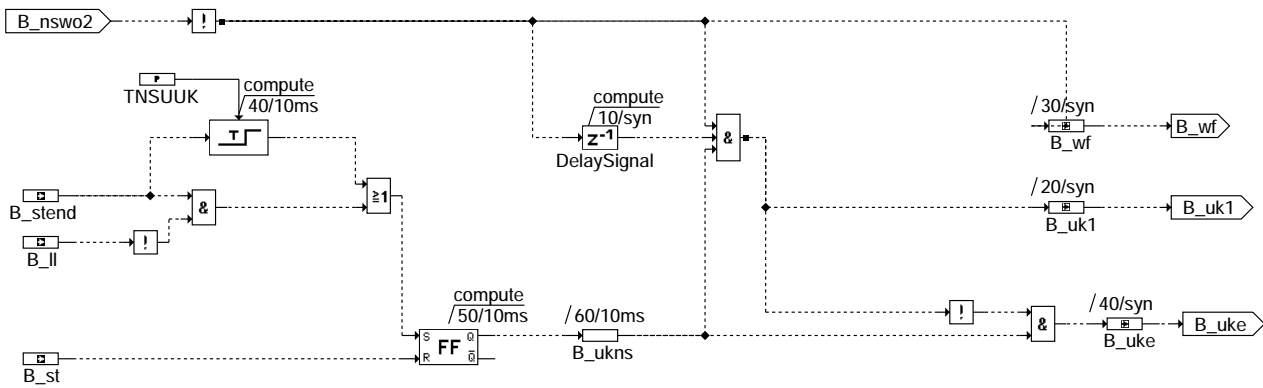
Overview Transient Compensation



esuk-main

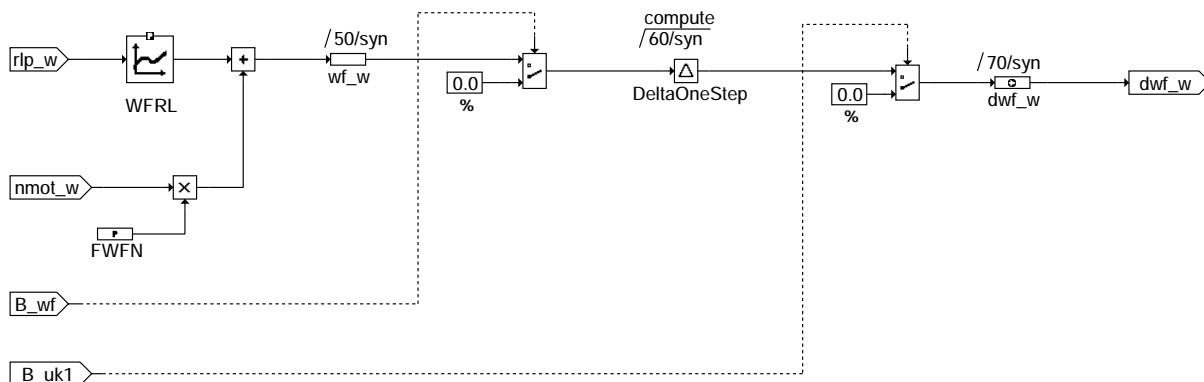
esuk-main

UKENA: transient compensation enable



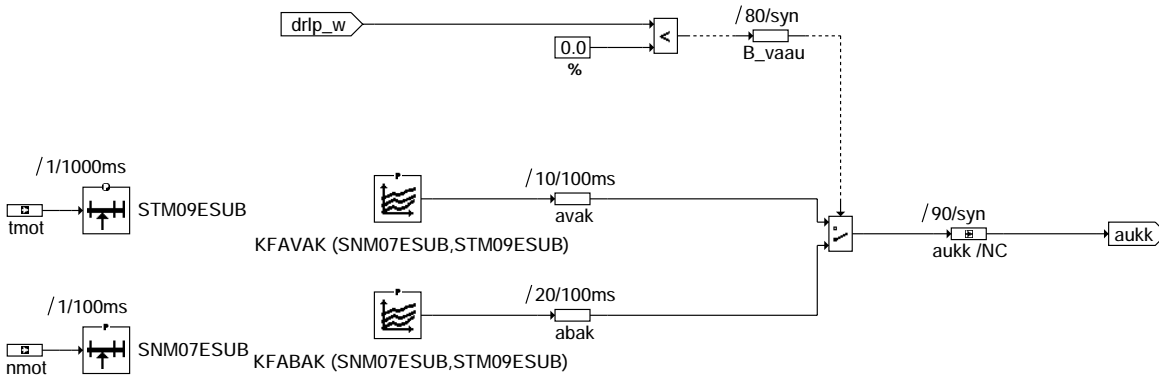
esuk-ukena

UKWF: calculation of wall wetting amount



esuk-ukwf

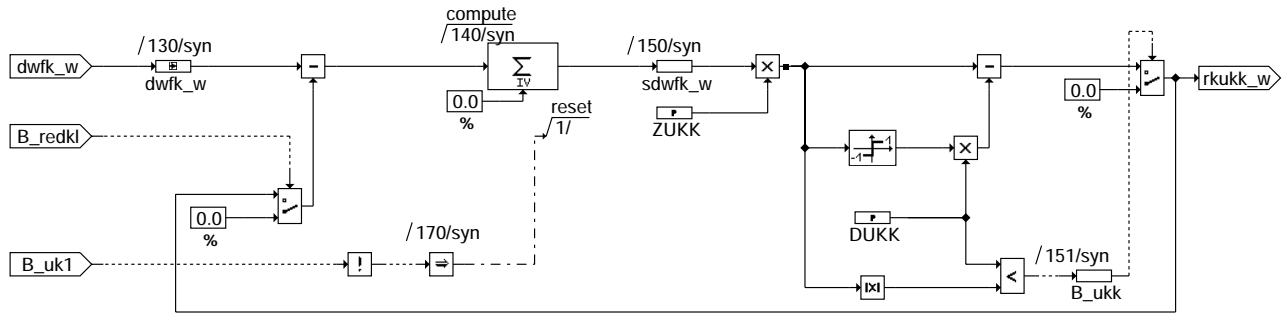
UKAU: wall wetting share factor



esuk-ukau

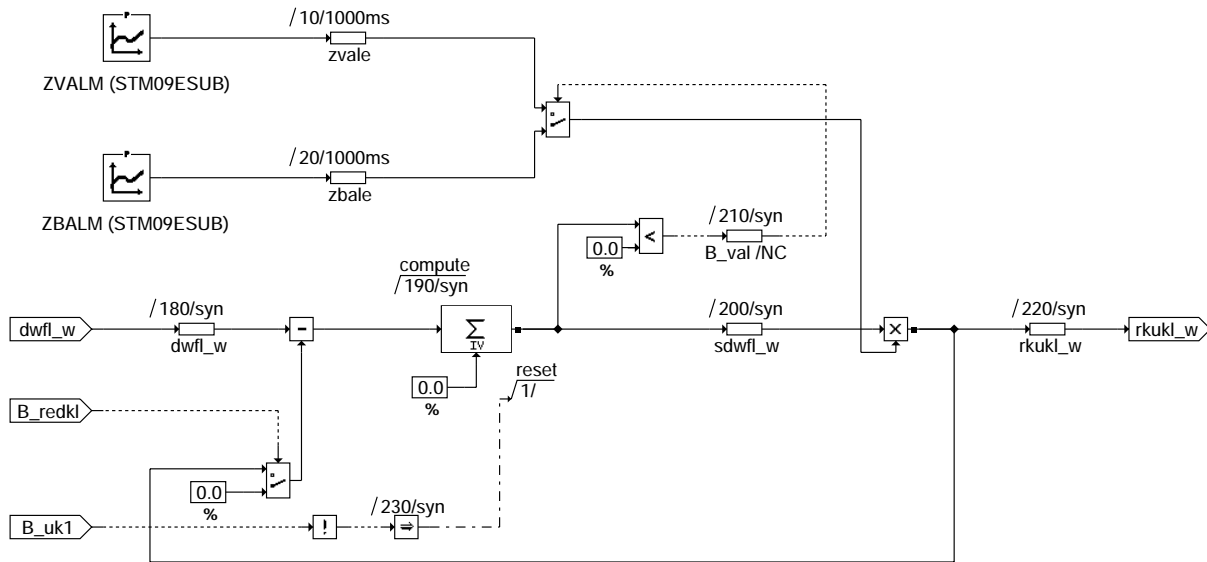


UKKSP: short term memory



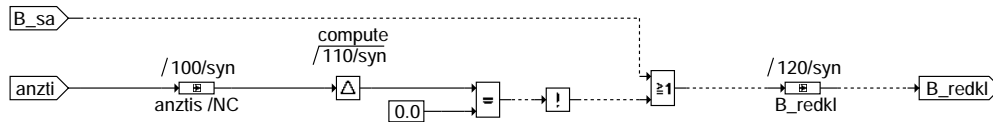
**esuk-ukksp**

UKLSP: long term memory



**esuk-uklsp**

UKABST: memory adjustment enable



**esuk-ukabst**

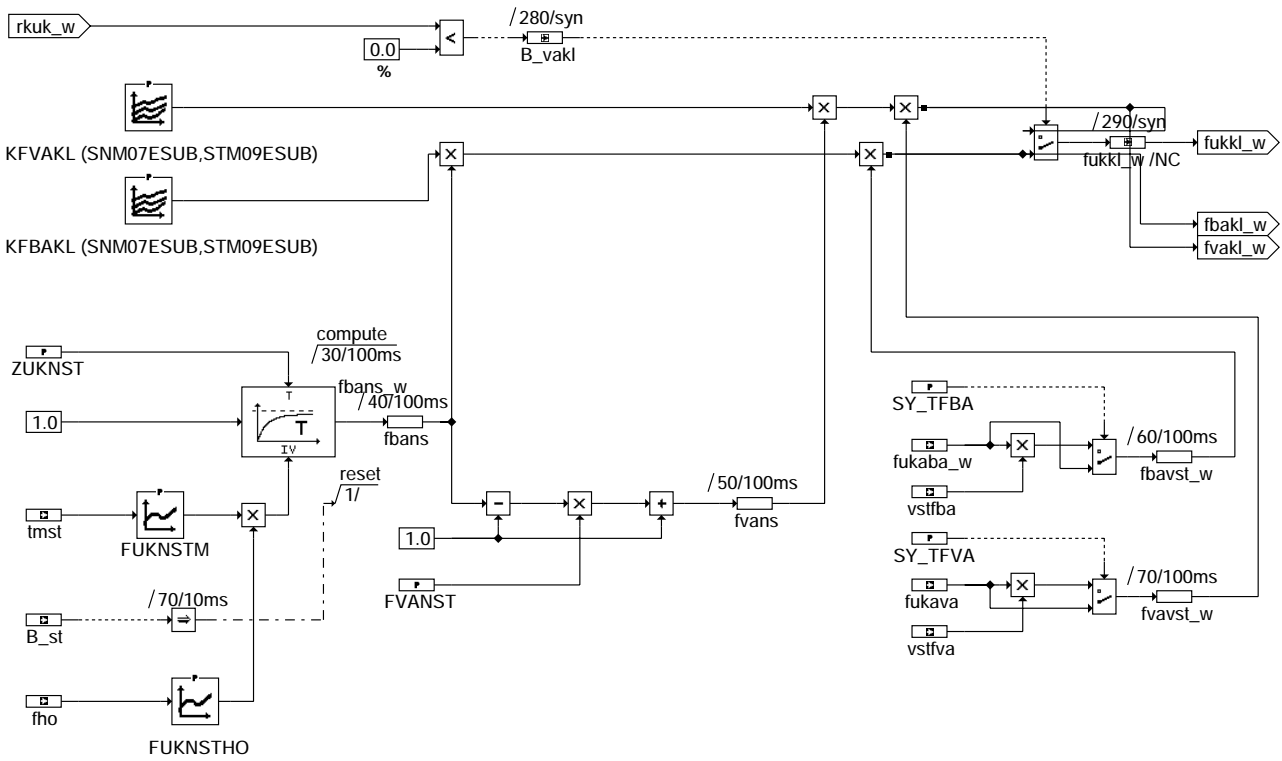
esuk-ukksp

esuk-uklsp

esuk-ukabst

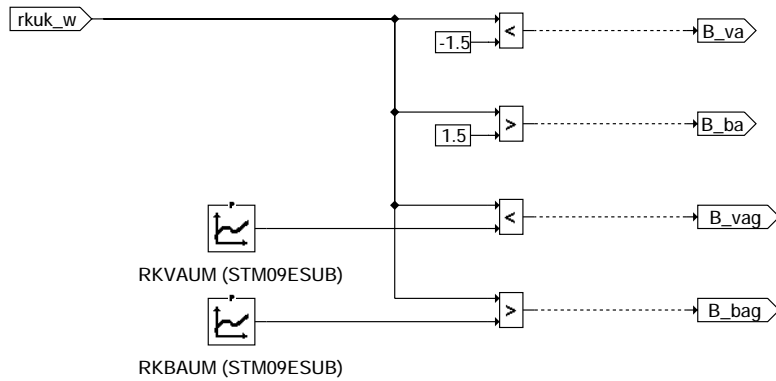


UKKORR: short+long term correction, post cranking, transient compensation adaptation



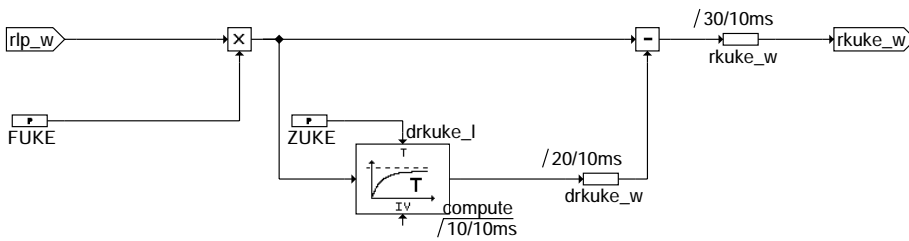
**esuk-ukkor**

UKBAUS: state bits



**esuk-ukbsw**

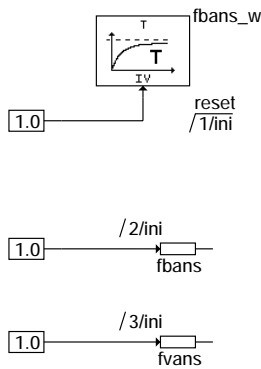
UKNSWO: substitute value for partial function switch off



**esuk-uknswo**



INITIALIZE: Initialize



esuk-initialize

### ABK ESUK 4.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DUKK			FW	threshold for short term portion
FUKE			FW	Factor transient control substitute value
FUKNSTHO	FHO		KL	altitude dependent transient control post cranking factor
FUKNSTM	TMST		KL	initial value of transient control post cranking factor
FVANST			FW	weighting factor of deceleration during post-cranking
FWFN			FW	wall wetting factor influence of rpm
KFABAK	NMOT	TMOT	KF	share factor wall wetting for acceleration enrichment
KFAVAK	NMOT	TMOT	KF	share factor wall wetting for deceleration enrichment
KFBAKL	NMOT	TMOT	KF	factor accel. enrichment (short- and long-time part)
KFVAKL	NMOT	TMOT	KF	factor decel. enrichment (short- and long-time part)
RKBAUM	TMOT		KL	rk-threshold for acceleration enrichment display
RKUKKLU			FW	threshold sum of long-/short term
RKVAUM	TMOT		KL	rk-threshold for deceleration enrichment display
SY_TFBA			SYS	system constant service device intervention accel. enrichment
SY_TFVA			SYS	system constant service device intervention decel. enrichment
TNSUUK			FW	disabling time of transient control during post-cranking
WFRL	RLP_W		KL	fuel wall hang.up
ZBALM	TMOT		KL	reduction factor L-memory (tmot) for accel. enrichment
ZUKE			FW	Time constant transient control substitute value
ZUKK			FW	reduction factor K-memory
ZUKNST			FW	time constant of transient control post cranking factor
ZVALM	TMOT		KL	reduction factor L-memory (tmot) for decel. enrichment

Variable	Source	Type	Description
ABAK	ESUK	LOK	share factor wall wetting for acceleration enrichment
ANZTI	ACIFI	EIN	injection counter
AVAK	ESUK	LOK	share factor wall wetting for deceleration enrichment
B_BA	ESUK	AUS	Condition acceleration enrichment (display)
B_BAG	ESUK	AUS	Condition large accel. enrichment
B_LL	MSF	EIN	Condition idle
B_NSWO2	PROKON	EIN	condition engine speed > NSWO2
B_REDKL	ESUK	LOK	Enable reduction of K- and L-Memory
B_SA	MDRED	EIN	Condition fuel cut-off
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_UK1	ESUK	LOK	Enable condition for transient control
B_UKE	ESUK	LOK	Enable condition for substitute value of transient control
B_UKG	ESUK	AUS	condition transient control activated
B_UKNS	ESUK	LOK	Enable condition transient contr. after cranking
B_VA	ESUK	AUS	Condition deceleration enrichment (display)
B_VAAU	ESUK	LOK	Condition decel. enrichment for partition of fuel film
B_VAG	ESUK	AUS	Condition large deceleration enrichment
B_VAKL	ESUK	LOK	Condition decel. enrichment L- and K-part
B_WF	ESUK	LOK	Condition wall wetting calculation
DRKUKE_L	ESUK	LOK	Delta of the relative fuel mass (default value)
DRKUKE_W	ESUK	LOK	Delta of the relative fuel mass (default value)
DRLP_W	BGRLP	EIN	delta predicted load for injection time calculation (word)
DWFK_W	ESUK	LOK	delta wall wetting quantity short term
DWFL_W	ESUK	LOK	delta wall wetting quantity long term
DWF_W	ESUK	AUS	Delta wall hang-up quantity
FBAKL_W	ESUK	AUS	factor short/long time part of trans.control during acceleration
FBANS	ESUK	LOK	post cranking factor of transient control during acceleration
FBANS_W	ESUK	LOK	post cranking factor of transient control during acceleration
FBAVST_W	ESUK	LOK	factor ÜK-adjustment at acceleration enrichment
FHO	BGPU	EIN	Correction factor altitude
FUKABA_W	ESUKA	EIN	factor adaptive transient control BA



Variable	Source	Type	Description
FUKAVA		EIN	factor adaptive transient control VA
FVAKL_W	ESUK	AUS	factor short/long-time part of trans.control at deceleration
FVANS	ESUK	LOK	post cranking factor of transient control during deceleration
FVAVST_W	ESUK	LOK	factor ÜK-adjustment at deceleration enleanment
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
RKUKE_W	ESUK	LOK	rel. fuel mass transition compensation substitute value
RKUKG_W	ESUK	AUS	rel. fuel mass transition compensation
RKUKKL_W	ESUK	LOK	sum of short and long term parts of transient control
RKUKK_W	ESUK	AUS	rk short term part of transient control
RKUKL_W	ESUK	LOK	rk long term part of transient control
RKUK_W	ESUK	LOK	rel. fuel mass transition compensation without adjustment
RLP	BGRLP	EIN	rel. air charge predicted for injection calculation
RLP_W	ESUK	LOK	rel. air charge predicted for injection calculation (Word)
SDWFK_W	ESUK	LOK	memory content of the wall wetting difference for short term portion
SDWFL_W	ESUK	LOK	memory content of the wall wetting difference for long term portion
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
VSTFBA		EIN	factor acceleration enrichment (service device interface)
VSTFVA		EIN	factor deceleration enleanment (service device interface)
WF_W	ESUK	LOK	wall wetting quantity
ZBALE	ESUK	LOK	reduction factor during acceleration
ZVALE	ESUK	LOK	reduction factor during deceleration enleanment

### FW ESUK 4.50 Fixed Values

Parameter	Value	Description
DUKK		threshold for short term portion
FUKE		Factor transient control substitute value
FVANST		weighting factor of deceleration during post-cranking
FWFN		wall wetting factor influence of rpm
RKUKKLU		threshold sum of long-/short term
TNSUUK		disabling time of transient control during post-cranking
ZUKE		Time constant transient control substitute value
ZUKK		reduction factor K-memory
ZUKNST		time constant of transient control post cranking factor





## FB ESUK 4.50 Detailed description of function

The transient control determines the required additional or reduced injected fuel during a change in load to compensate for wall wetting.

The transient control consists of three different portions:

- Long term portion  $rkukl_w$   
serves to compensate slow wall wetting effects. Based on predicted load signal  $rlp_w$  and engine speed. Calculation is performed segment synchronously.
- Short term portion  $rkukk_w$   
serves to compensate fast wall wetting effects. Based on predicted load signal  $rlp_w$  and engine speed. Calculation is performed segment synchronously.

The wall wetting characteristic line WFRL contains that fuel quantity, which is stored in the wall wetting for the appropriate load at steady-state conditions. If the load is changing during one segment by the value  $drlp_w = rlp_w(s) - rlp_w(s-1)$ , then the wall wetting difference  $dwf_w = WFRL(rlp_w(s)) - WFRL(rlp_w(s-1))$  has to be injected as additional fuel amount, in order to compensate the increase of wall wetting.

This additional quantity has to be distributed over time, so that Lambda remains constant during the transient. For this, the additional quantity is divided into a short time and a long time portion by means of the partition factor  $aukk$  and accumulated in the corresponding memories ( $sdwfl_w$ , long term memory resp.  $sdwfk_w$ , short term memory).

For each segment the fuel quantity  $sdwfl_w * ZBALM$  (for acceleration) resp.  $sdwfl_w * ZVALM$  (for deceleration) is taken from the long term memory. It represents the long time portion  $rkukl_w$  of  $rkukkl_w$ . Afterwards the long term memory is decremented by the same value  $rkukl_w$ , if the current value of  $rlukl_w$  has been used at least for one injection ( $B_{redkl} = 1$ ). The reduction factors ZBALM and ZVALM depend on engine temperature, since the evaporation of fuel film is much slower during warm up than at hot engine.

Equivalently, the fuel quantity  $sdwfk_w * ZUKK - DUKK$ , i.e. the amount that exceeds the threshold DUKK, is taken from the short term memory as short term portion  $rkukk_w$ . The reduction factor of the short term portion ZUKK is equal for both increasing and decreasing load. The short term memory is decremented by  $rkukk_w$  as soon as the current value  $rkukk_w$  has been used at least for one injection ( $B_{redkl} = 1$ ).

By means of this it is ensured, that the additionally injected fuel amount (due to the load change  $drlp_w = rlp_w(s) - rlp_w(s-1)$ ) corresponds exactly to the difference of the wall wetting quantities  $dwf_w = WFRL(rlp_w(s)) - WFRL(rlp_w(s-1))$ .

The sum  $rkukkl_w$  of the two portions  $rkukl_w$  (from long term memory) and  $rkukk_w$  (from short term memory) is weighted by the factor KFBACL (for acceleration) resp. KFBACL (for deceleration), a post cranking factor and the correction factor from adaptation of transient control (see later).

During cranking at a determined coolant temperature the wall of intake manifold is much cooler as if it would be during warming at the same coolant temperature (cranking at a lower temperature). That is the reason why the transient control is weighted with the factor  $fbans$  resp.  $fvans$  during post cranking. This factor is initialized with FUKNSTM during cranking and then reduced exponentially towards 1. At deceleration an additional factor FVANST is used.

The differentiation between acceleration and deceleration for the segment synchronous portions is realized as dependence on  $drlp_w$  (share factor  $aukk$ ) resp. on  $sdwfl_w$  (reduction factor  $zukul$ ).

For the change over between  $fbakl/fvakl$  the sum of the short term/long term portion  $rkukkl_w$  is used.

The transient control is not determined during cranking and for engine speeds above a speed limit ( $B_{nsw0}=1$ ).

Besides the calculation of the segment synchronous part of the transient control is turned off for an additional cycle after the the engine speed falls short of the threshold again, since the value WFRL(s-1) which is required for the calculation of the change  $dwf_w$  is not yet defined.

After transition from cranking to post cranking the transient control can be disabled during the time TNSUUK in order to prevent that errors in measured load do trigger an acceleration enrichment or a deceleration enrichment; so it is possible to calibrate the post cranking phase independent of transient control. This time will be finished at once, when idling status is left.

If the absolute value of  $rkukkl_w$  exceeds RKUKKLU, bit  $B_{ukg}$  will be set to indicate high dynamics; this information as well as Bits  $B_{bag}/B_{vag}$  are used to disable other functions.

$B_{ba}$  and  $B_{va}$  are used to show the acceleration or deceleration state, e.g. on a calibration tool like VS20.

**APP ESUK 4.50 Application hint**

## Requirements:

- steady state calibration to Lambda = 1
- injection advance angle calibrated, so that the fuel is just not yet injected into the open inlet valve (flight time of fuel (approx. 8 ms considered), i.e. the ti-end must advance for increasing engine speed; this results in a minimized actualization error and low HC-emission
- creation of load signal rlp\_w proportional to intake manifold pressure
- load prediction calibrated

## Application aids:

- Lambda-test procedure with a sample rate of < 20 ms. If a sensor LSM11 and a Lambda display LA1/LA2 is employed, the engine can be tuned for steady state condition to a Lambda value of 1.05. With it, the more accurate "lean"-branch of the LSM11 characteristic is used and the problems during rich-lean transients at Lambda = 1.0 are avoided.
- throttle actuator for defined load jumps during constant engine speed

## Presetting of the parameters:

- preset of all setpoints of n resp. t<sub>mot</sub>-dependent characteristic lines or maps to i d e n t i c a l values
- wall wetting characteristic line WFRL: lower base point: WFRL = 0.0 %, upper base point: WFRL = 1300 %; gradient around idle area approx. 1/3 of the gradient for WOT
- factor wall wetting influence of engine speed FWFN = 0.0 %/(1/min)
- reduction factor ZUKK = 0.25
- threshold short time part DUKK = 0.0 ms
- reduction factors ZBALM = ZVALM = 0.015 (4-cylinder engine) for temperatures between 100 °C .. 40 °C
  - = 0.008 (6-cylinder)
  - = 0.006 (8-cylinder)
  - should be reduced at lower temperatures
- share factors KFABAK = KFAVAK = 0.25 (for all engine speeds)
- engine temperature factors KFBACL, KFVAKL = 0.8 for t<sub>mot</sub> = 100 °C and all engine speeds
  - KFBACL, KFVAKL = 1.0 for t<sub>mot</sub> = 90 °C and all engine speeds
  - KFBACL, KFVAKL = 1.2 for t<sub>mot</sub> = 80 °C and all engine speeds
  - KFBACL, KFVAKL = 6.0 for t<sub>mot</sub> = 20 °C und N = 1500 rpm,
  - KFBACL, KFVAKL = 2.0 for t<sub>mot</sub> = 20 °C und N = 4000 rpm
- time Uk disabled after cranking TNSUUK = 2 s
- threshold disable of other functions RKUKKLU = 30 %, RKBAUM = 300 %, RKVAUM = -300 %
- transient control post cranking factor FUKNSTM = 2.0 (for t<sub>mot</sub> < 80 °C, neutral value = 1.0), FVANST = 1.0
- time constant of transient control post cranking factor ZUKNST = 22 s
- Factor substitute value for transient control FUKL = 1.1
- Time constant for substitute value ZUKE = 0.03 s

## Switch off transient control:

switch off load dependent part: KFBACL = 0; KFVAKL = 0

## Procedure:

For calibration of the transient control, the Lambda closed loop control must be turned off. Transient control adaptation (see %ESUKA resp. %ESUKAS) must be disabled and the correction factor of transient control must be set to its initial value of 1.0 .

## 1) Calibration of the hot engine at low engine speed

Prefereably, the calibration should be carried out on an externally driven chassis dynamometer or engine dyno. In case the calibration is carried out with the vehicle, then a manual transmission is required. If not available, the torque converter of the automatic transmission must be locked, so that the engine can be operated with variable load at constant engine speed. For vehicle calibration, the fuel evaporation must be sucked off. Appropriate tire equipment must be provided (the stress on tires is comparable to engine mapping).

At first the wall wetting characteristic line WFRL, the share of KFABAK, KFAVAK and the reduction factors ZUKK, ZBALM, and ZVALM are determined for the short and long term portion at a relatively low engine speed (approx. 1400 RPM).

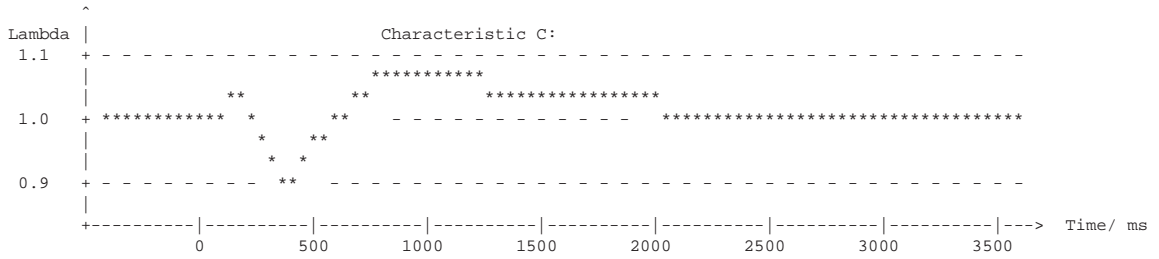
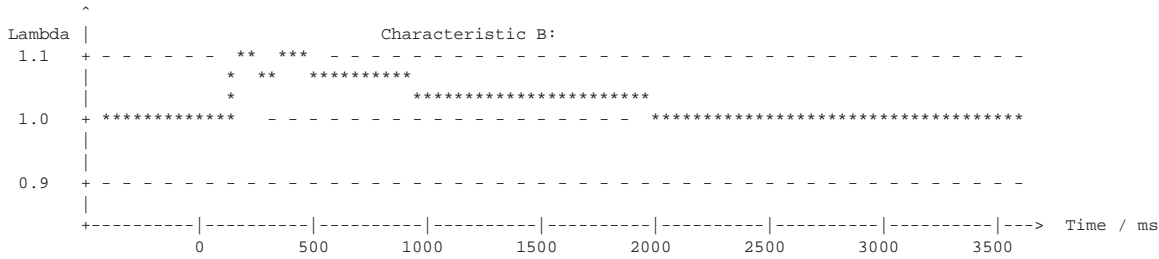
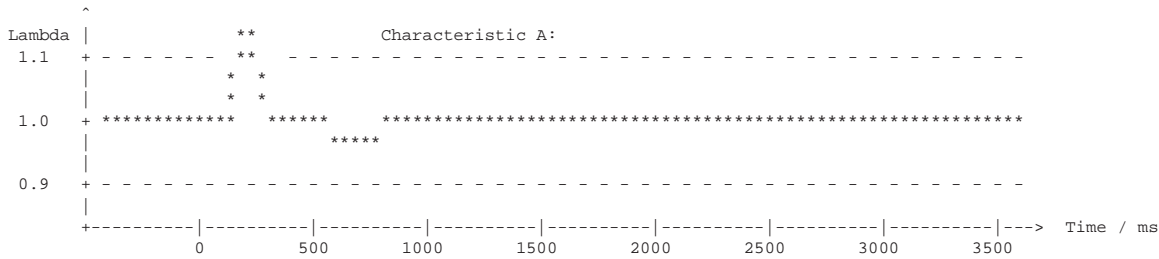
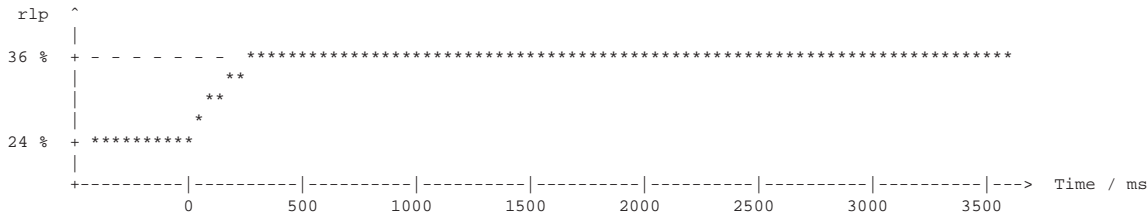
For this, fast load changes at constant speed are performed between neighbouring rlp\_w setpoints of the wall wetting characteristic WFRL (throttle plate adjustment within approx. 100 ... 200 ms). For practical reasons, the engine load and Lambda characteristic during the load change is simultaneously displayed (with oscilloscope) and recorded. Waiting time between two consecutive load steps: approx. 10 ... 20 s.

In the following the procedure, recommended for correcting the transient parameters, is explained, based on various Lambda traces occurring during acceleration.

The following load setpoints of the wall wetting characteristic are assumed:

rlp\_w = ..... 24 % / 36 % / 48 % / 60 % .....

At first the calibration is carried out at low load, e.g., with a load step from rlp\_w = 24 % --> 36 % --> 24 %.



The Lambda characteristic B indicates insufficient transient compensation for all portions. In this case the wall wetting amount WFRL should be increased. Since only the differences between consecutive calculations are used for evaluation of the wall wetting characteristic WFRL, the gradient of the wall wetting characteristic between the setpoints  $rlp_w = 24\%$  and  $rlp_w = 36\%$  must be increased. In this case the total characteristic WFRL for  $rlp_w = 36\%$  must be upshifted in a parallel direction (therefore, the characteristic of the function in the load range  $rlp_w > 36\%$  remains constant).

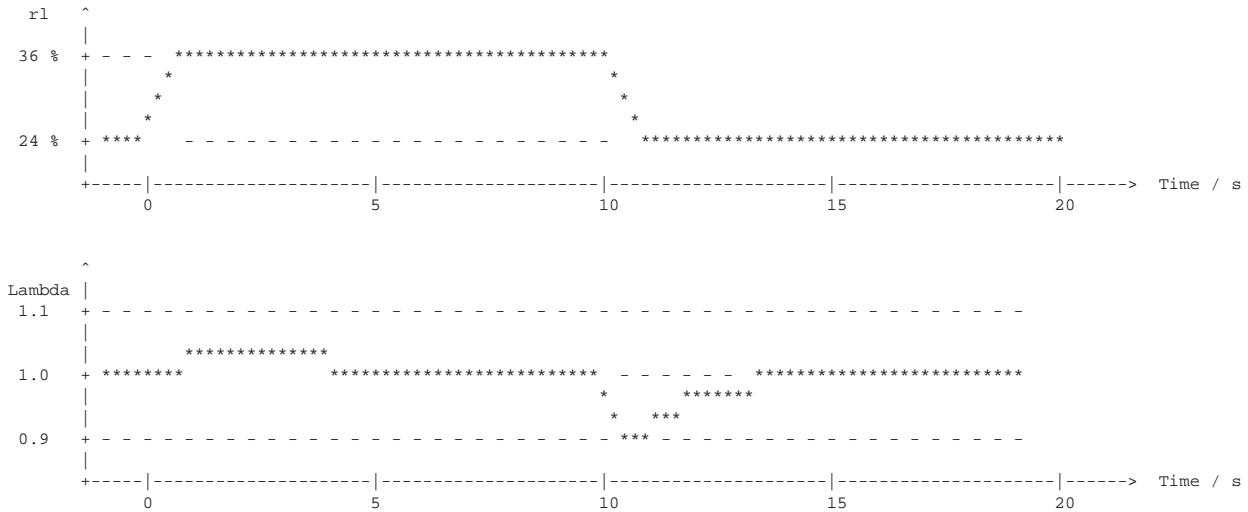
On an average, line C shows a desired Lambda characteristic. However, the split-up into short term and long term portion is considered insufficient. By reducing the split factor KFABAK, the total injected additional amount of fuel is shifted from the short term to the long term portion. By this, both the mixture deviation to the rich at  $t = 400$  ms and the following lean-out is reduced.

For negative load steps above procedure is applied accordingly. In this case, however, the opposite reaction of the transient compensation parameters must be obeyed:

Mixture lean-out after load reduction is caused by excessive deceleration lean-out, i.e., in contrary to the acceleration lean-out, the transient compensation must be reduced.



Since the wall wetting characteristic WFRL is applied to increasing and decreasing load, the acceleration as well as the deceleration parameters for a specific load range must always be optimized. In below example a significant enrichment occurs during deceleration. Accordingly, the gradient of the wall wetting characteristic WFRL for the range  $24\% < rlp_w < 36\%$  must be significantly increased. This change can be implemented, although there is no significant lean-out during acceleration. An insufficient amount of wall wetting results in significantly less mixture deviation during increasing load, since this insufficient additional amount of fuel is related to a higher load, compared to the appropriate deceleration. Therefore, it is expected that, by applying a steeper wall wetting characteristic WFRL in the range  $24\% < rlp_w < 36\%$ , at first only the deceleration enrichment will be compensated, not necessarily resulting in mixture enrichment during acceleration.





For the "decrease factors" ZUKK, ZBALM and ZVALM for the short and long term portion, generally the given pilot values are sufficient. Possible indicators for improperly chosen "decrease factors" are:

- remaining Lambda deviation after the long term portion has elapsed (in this case the long term portion must be increased, i.e., ZBALM or ZVALM must be reduced). This effect is frequently experienced with cold engine.
- short lean-out during acceleration (approx. 1 s) after load step, in the case when an increased short term portion results in an enrichment prior to the lean-out, and increased long term portion leads to an enrichment after the lean-out. In this case there is obviously a gap between the short term and long term portion.

When varying the "decrease factors", the ratio ZUKK/ZBALM or ZUKK/ZVALM should not fall short of 8 ... 10. Otherwise, both portions are dynamically too similar in order to influence the mixture characteristic by means of the short and long term portion.

Note: When calibrating the wall wetting characteristic WFRL, make sure to obtain a "plausible" characteristic (flat parabolic curve, no edges!).

As soon as all load intervals 24 % <--> 36 %, 36 % <--> 48 %, 48 % <--> 60 % etc. have been calibrated, larger load changes are applied and the Lambda characteristic is then evaluated. In case there are unacceptable Lambda deviations, at first the "small" load steps should be again verified at the appropriate area. Frequently, the deviations, occurring at large load steps, are also experienced with small load steps (smaller magnitude), however, they were yet accepted in these areas.

Short term portions KFABAK or KFAVAK exceeding 60 % are frequently caused by a dynamic error in load signal (too slow). In this case both the rl and the manifold pressure characteristic during load variation should again be compared.

Remaining Lambda deviations for load steps close to full load may indicate insufficient steady state calibration in this area. In this case the pulsation compensation and the psmax-limitation must again be verified.

## 2. Calibration with hot engine for the entire engine speed range

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Initial calibration is performed at the speed setpoint of approx. 1400 rpm. Then, the remaining speed setpoints are calibrated as well. At first the setpoints in the idle area should be calibrated, since, in some cases, improperly chosen "decrease factors" ZUKK, ZBALM, ZVALM may be discovered, resulting in verification of the speeds which have already been calibrated. If possible, neither the "decrease factors" nor the wall wetting characteristic WFRL should be changed, because there is no degree-of-freedom for different engine speed.

For significant deviations of the entire wall wetting amount, the correction should be carried out via the speed dependency in the look-up tables KFBAKL and KFVAKL.

Note: The time for build-up and reduction of wall wetting decreases at higher engine speed. This effect must be considered when choosing the parameters, compensating for Lambda deviations. At 1000 rpm, the Lambda deviation, occurring approx. 1 s after a load step, is rather allocated to the short term portion, at 3000rpm, however, the deviation is mainly influenced by the long term portion.

Time for calibration: Approx. 1 day for each speed setpoint.

## 3. Conversion engine dyno --> vehicle

-----

If the calibration of the hot engine is performed on the engine dyno, all transient compensation data must be reduced by 10 - 20 %, since the manifold temperatures for vehicle installation are slightly increased.

In order to obtain proper conversion to the vehicle, the configuration of all engine components (manifold design, camshaft, etc.) must be identical for dyno and vehicle testing. Aging conditions (intake valve deposits) should be comparable as well. If not ensured, the conversion of data must be verified, after one or two speed setpoints have been calibrated.



#### 4. Warm-up calibration

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The correspondence between engine dyno and vehicle is not ensured for the cold engine. Therefore, the warm-up calibration of the transients (accel, decel) should be performed on the chassis dyno. For this purpose, alternating acceleration and deceleration events are carried out at a constant engine speed (lower load point corresponding to approx. 400 mbar, upper load point at approx. 800 - 900 mbar manifold pressure) and the parameters: load, injection time, coolant temperature and Lambda are recorded (on-line calibration not possible!). Then, the factors KFBACL and KFVACL for the appropriate speed and temperature range are increased or decreased, depending on the Lambda characteristic (10 %-steps each, based on the previous value, e.g., increase KFBACL from 5.0 to 5.5, if there is an accel lean-out in the relevant temperature range).

In order to minimize the time required for adjusting the desired speed and load points (undesired engine heat-up), the chassis dyno adjustment, and the variation of the throttle angle are determined prior to testing (with hot engine).  
Note: With cold engine (coolant 20 deg C), the air flow for the same throttle position is approx. 10 - 15 % higher than with hot engine (increased desired idle airflow and cylinder charge with cold engine). Prior to testing, the Lambda sensor must be pre-heated (approx. 5 min).

For the temperature range > 0 deg C, a soak time of 7 to 8 hours (if possible in the cold chamber) is sufficient, allowing two measurements daily. Cooling down the engine by means of a blower (2 ..3 hours) is not recommended. In this case, the manifold would have cooled down, however, the coolant temperature, used for determining the transient compensation (TC) maps, would increase quickly due to the relatively warm engine block, causing insufficient TC calibration.  
Time for calibration: Three to four warm-up cycles required for each speed setpoint.  
Since the speed dependency shows a smooth characteristic, it is considered sufficient to calibrate 3 to 4 setpoints in the range 800 to 4000 rpm.

In many cases the long term portion must be increased at <= 20 deg C (ZBALM and ZVALM to be reduced at the appropriate temperature range). When increasing the temperature dependent factors during load reduction, it must be ensured that the injection time during transients exceeds the te-minimum value. With cold engine, in general a significant speed dependency of the wall wetting is experienced (wall wetting decreasing with increasing speed).

#### 5. Calibration of the post cranking factor

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In case the calibration of the TC is performed according to section 4, e.g., TC at 20 deg C with a start temperature of 0 deg C, then a significant undercompensation is experienced, when the engine is started at 20 deg C (poor acceleration immediately after cranking, partly misfiring at fast acceleration).  
Cause: Shortly after coldstart the temperatures of the manifold and intake valves are significantly lower compared to the temperatures occurring based on a significantly lower start temperature. This temperature effect can be compensated with the post cranking factors FUKNSTM and FVANST. In this case the post cranking factor FUKNSTM at the appropriate start temperature is increased (starting at 1.0) until satisfactory driving conditions for the warm-up stage have been obtained.

Due to high HC concentrations, Lambda measurements are very critical if carried out right after start.  
If fast gas analyzers are available, then "Lambda = constant" can also be calibrated during post cranking conditions.

#### Influenced functions:

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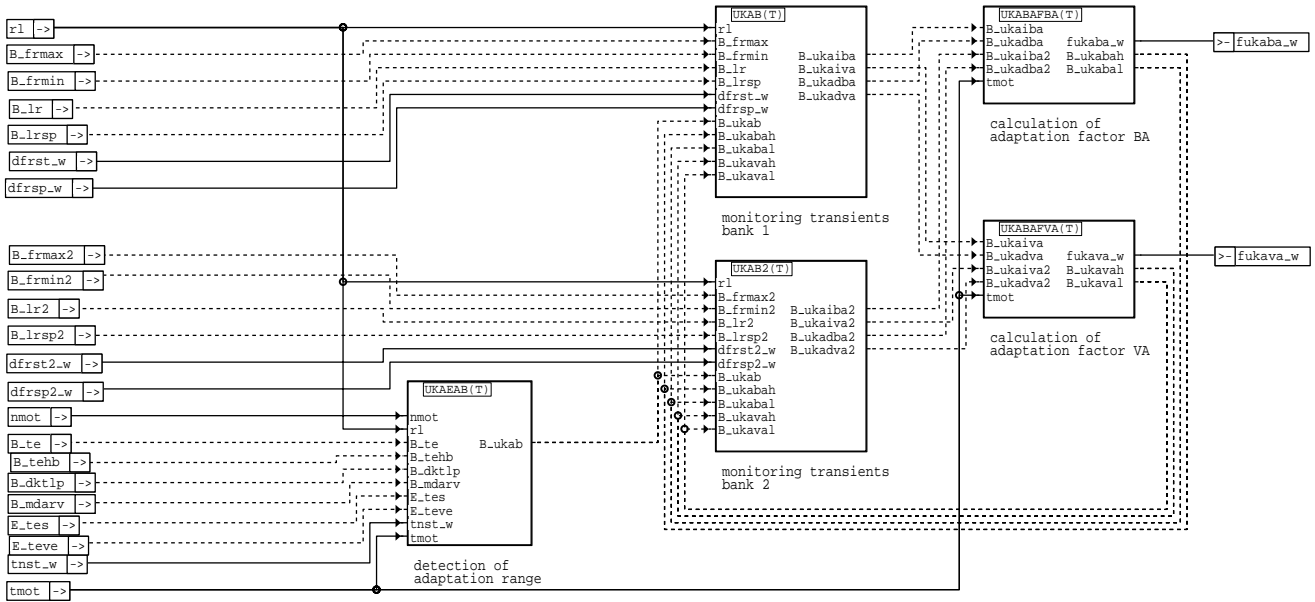
- Idle speed control: The wall wetting compensation, which is also effective during idle condition, leads to a faster increase of engine torque for opening of the idle speed actuator. This could result in cyclic speed oscillations ("sawing").

### ESUKA 13.30 Wall wetting adaptation based on ZPR

#### FDEF ESUKA 13.30 Function definition

ESUKA: Overview

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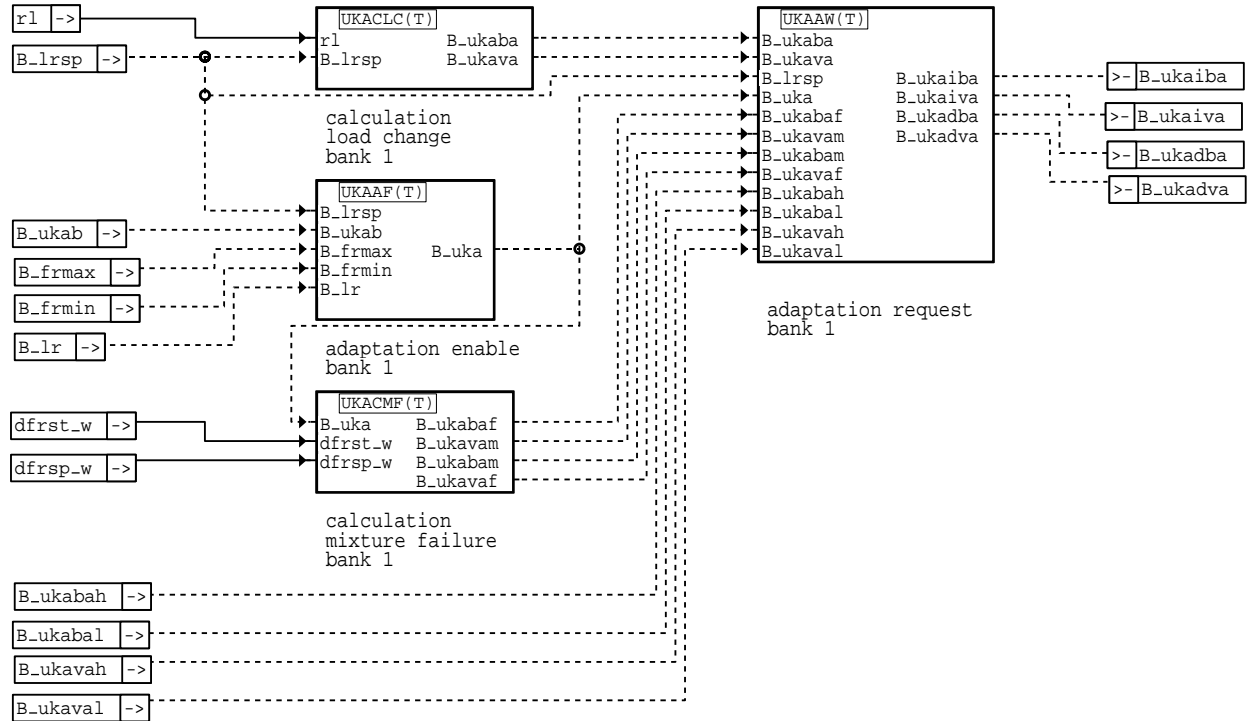


esuka-esuka

#### esuka-esuka

UKAB: Monitoring of transients bank 1

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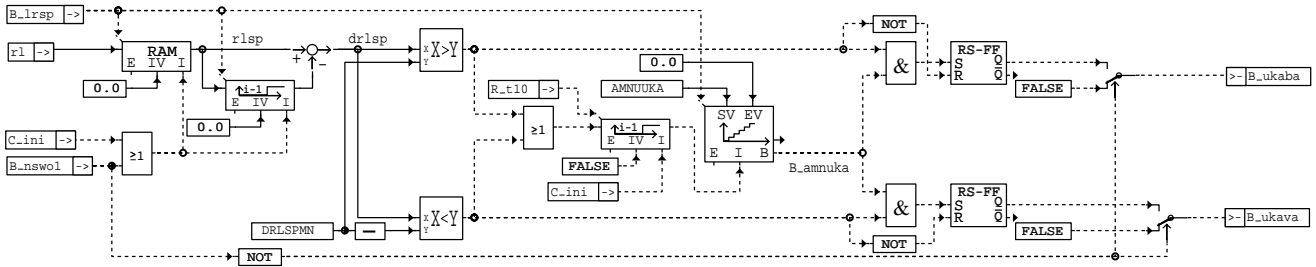


esuka-ukab

#### esuka-ukab

UKACLK: Calculation of load change bank 1

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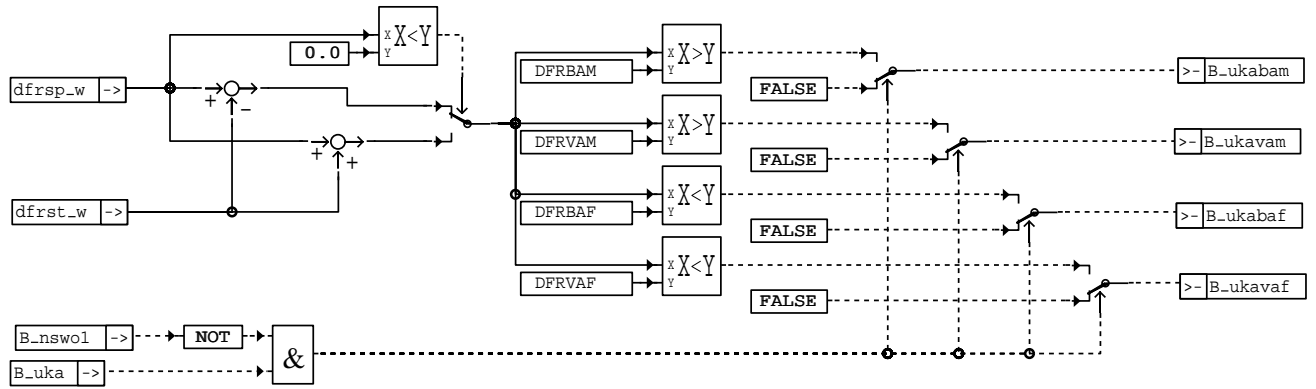


esuka-ukalc

esuka-ukalc

UKACMF: Calculation of mixture deviation bank 1

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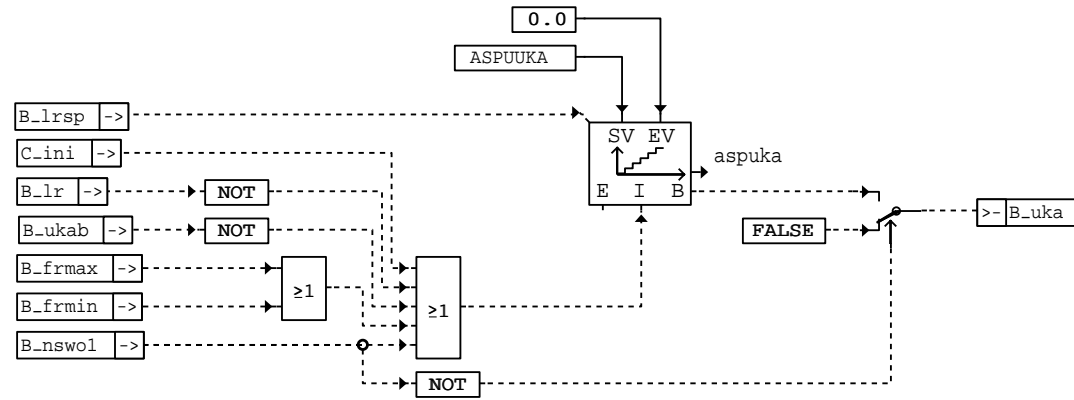
esuka-ukacmf

esuka-ukacmf

Processing in the 10-ms-cycle.

UKAAF: Adaptation release bank 1

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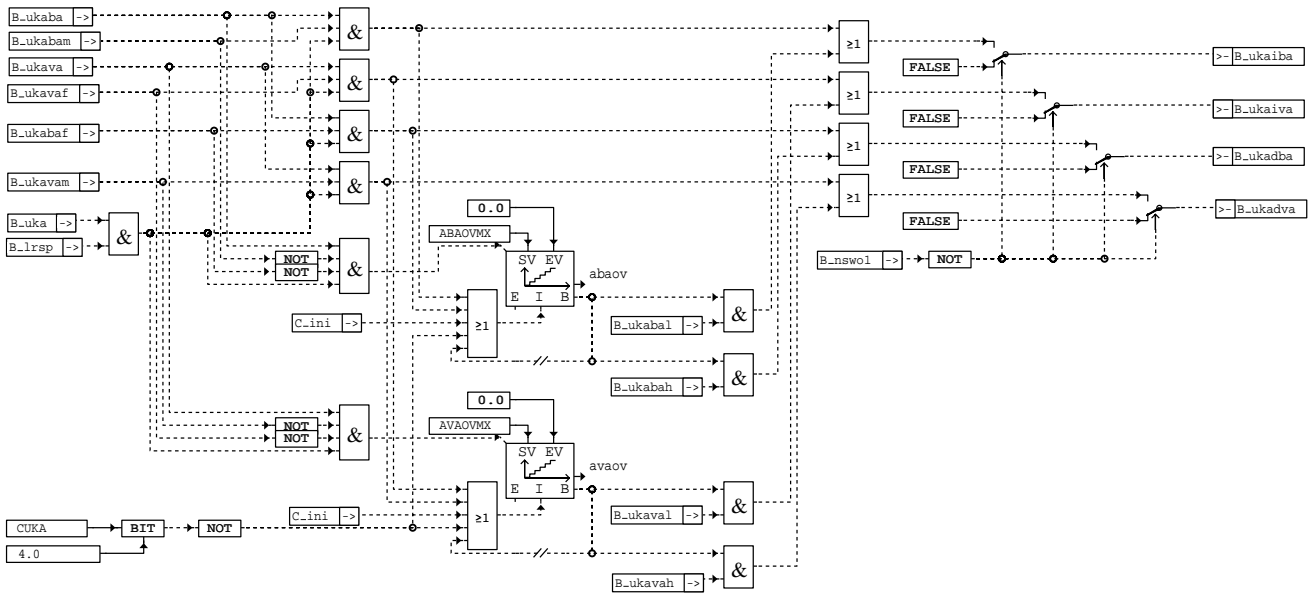
esuka-ukaaf

esuka-ukaaf

Processing in the 10-ms-cycle.

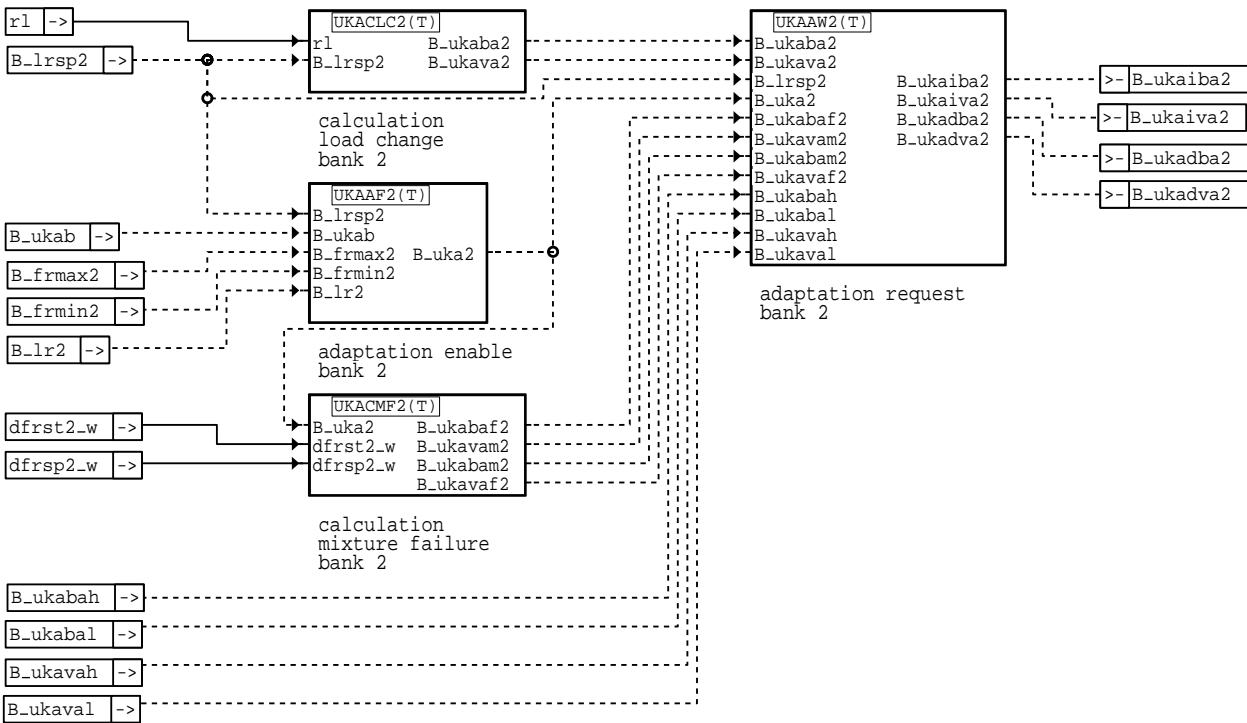


UKAAW: Adaptation request bank 1  
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**esuka-ukaaw**

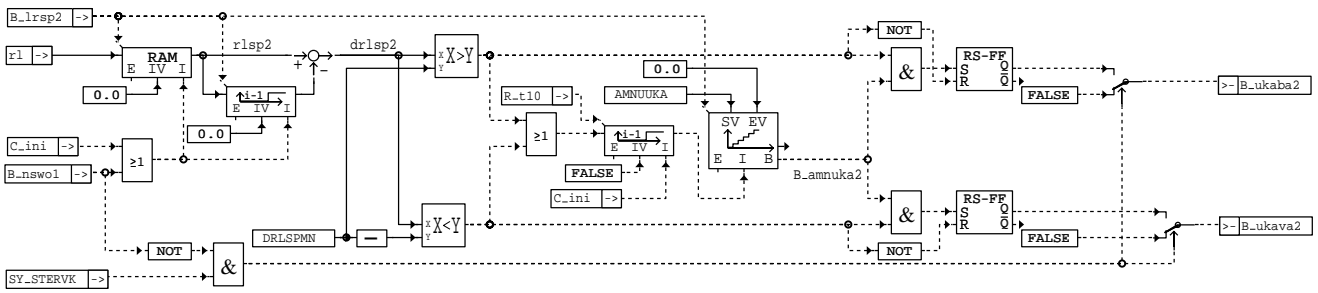
Processing in the 10-ms-cycle.  
UKAB2: Monitoring of transients bank 2  
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**esuka-ukab2**

UKACL2: Calculation of load change bank 2

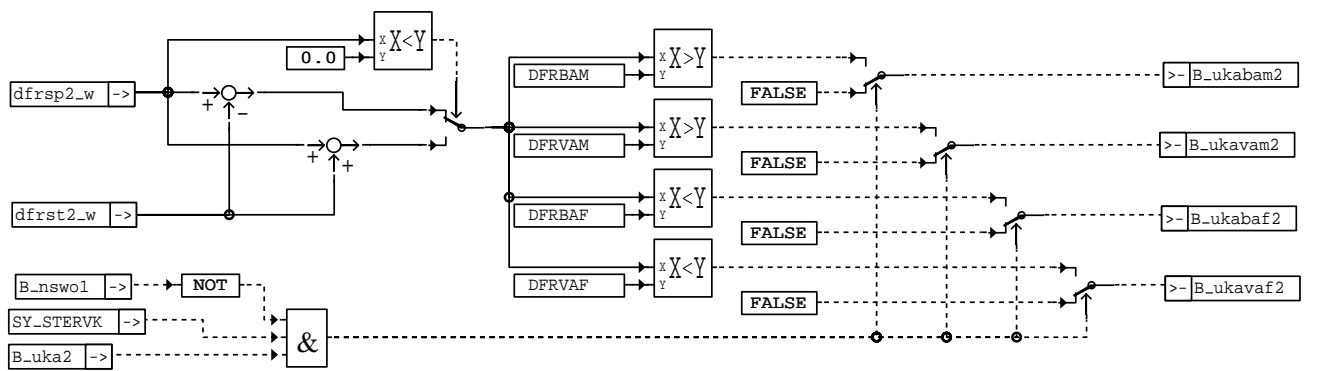
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esuka-ukacl2

UKACMF2: Calculation of mixture deviation bank 2

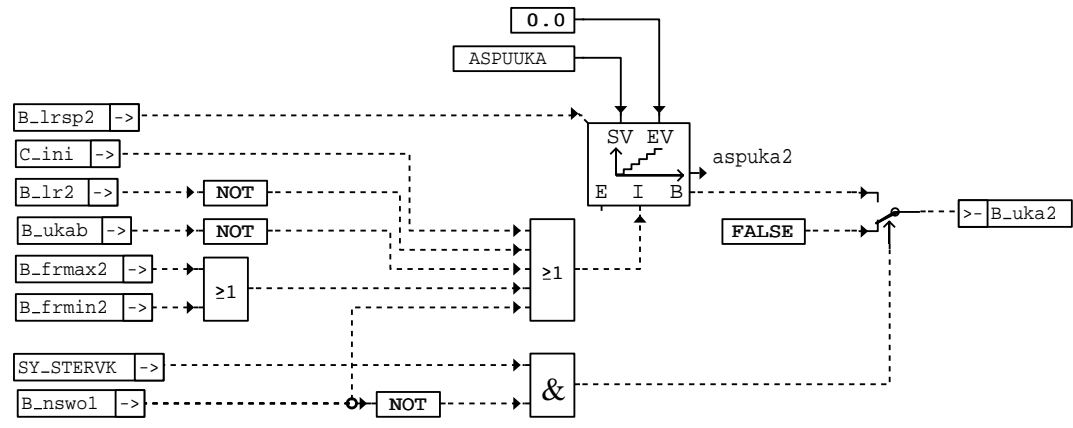
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esuka-ukacmf2

Processing in the 10-ms-cycle.  
UKAAF2: Adaptation release bank 2

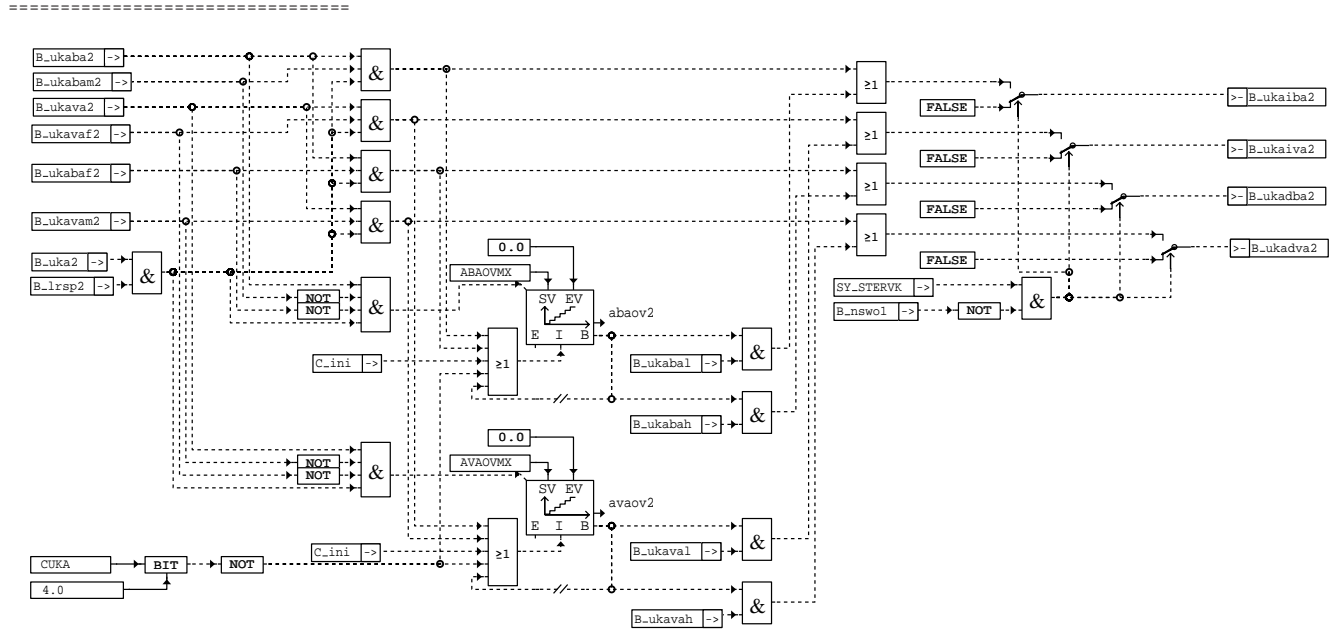
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esuka-ukaaf2

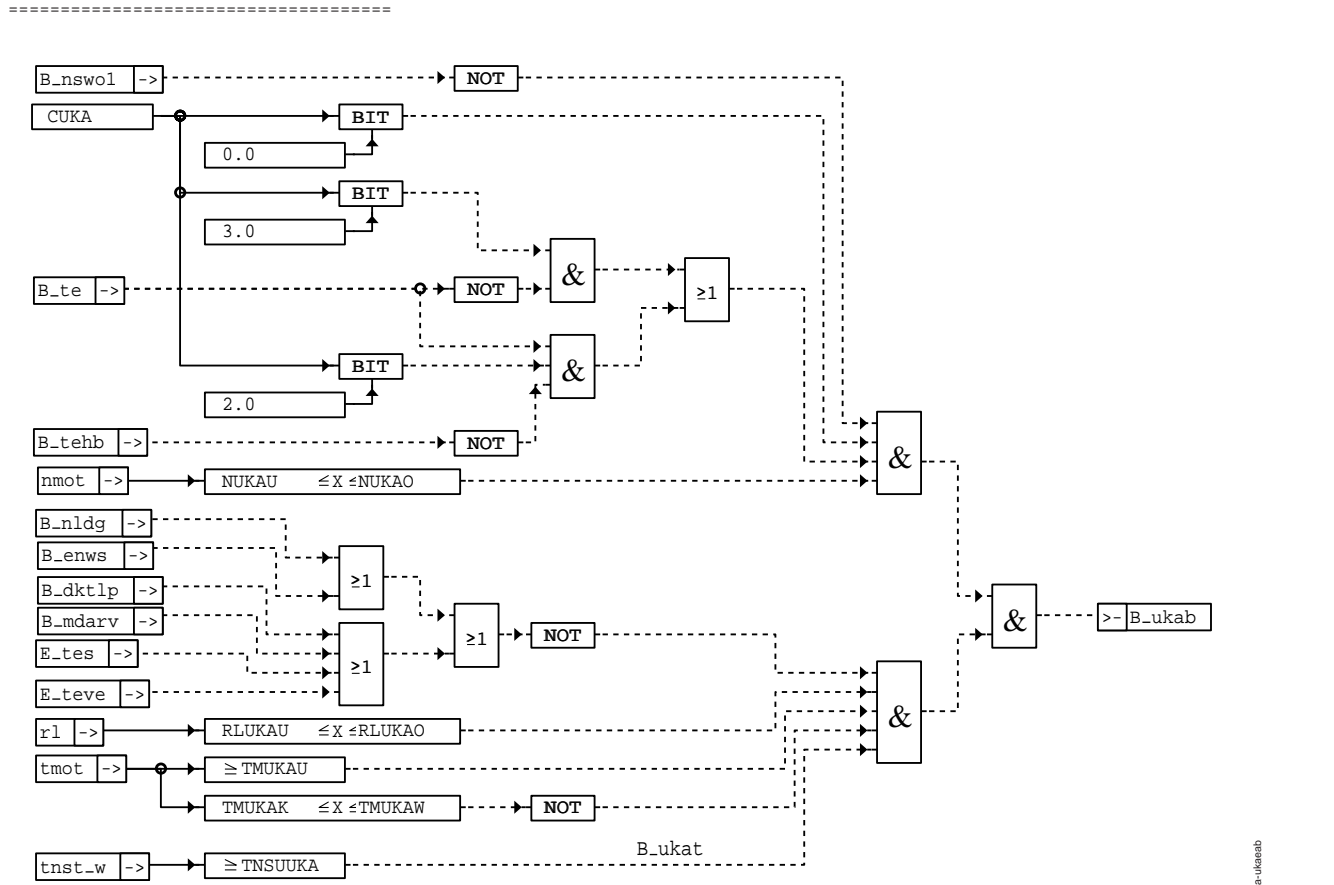
Processing in the 10-ms-cycle.

UKAAW2: Adaptation request bank 2



esuka-ukaaw2

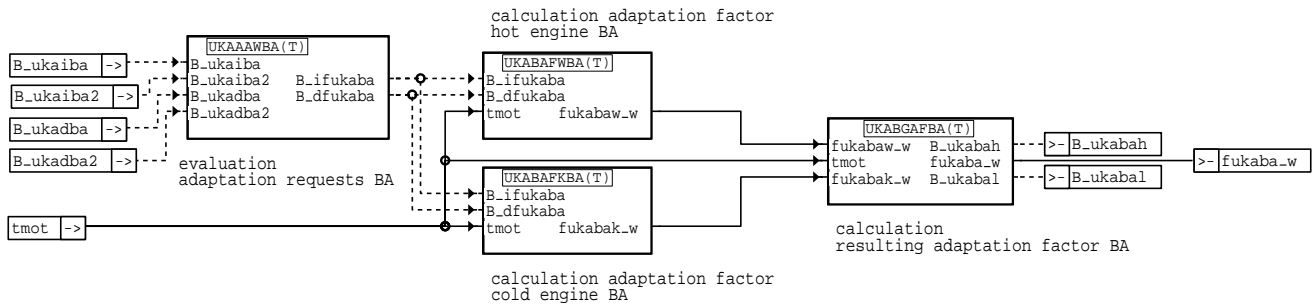
Processing in the 10-ms-cycle.  
UKAEAB: Detection of adaptation range



esuka-ukaab

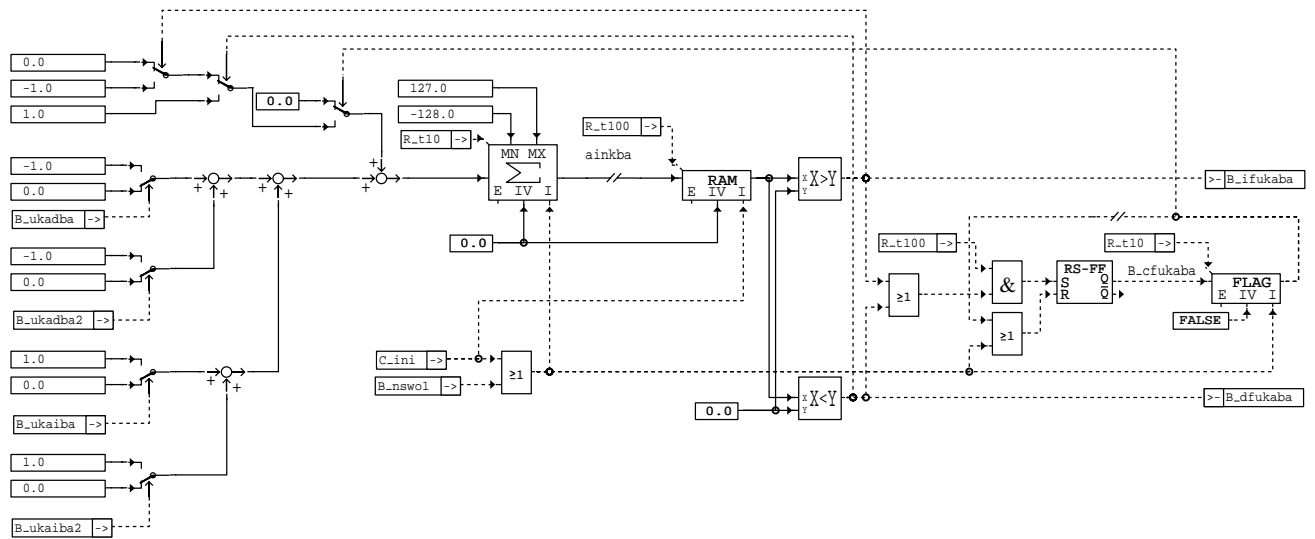
Limiting value comparison of engine speed and engine temperature, as well as scanning of the bit B\_tehb in the 100-ms-cycle.  
Remaining function in the 10-ms-cycle.

UKABAFBA: Calculation of correction factor BA



esuka-ukabafba

UKAAA(WBA): Evaluation of adaptation requests BA

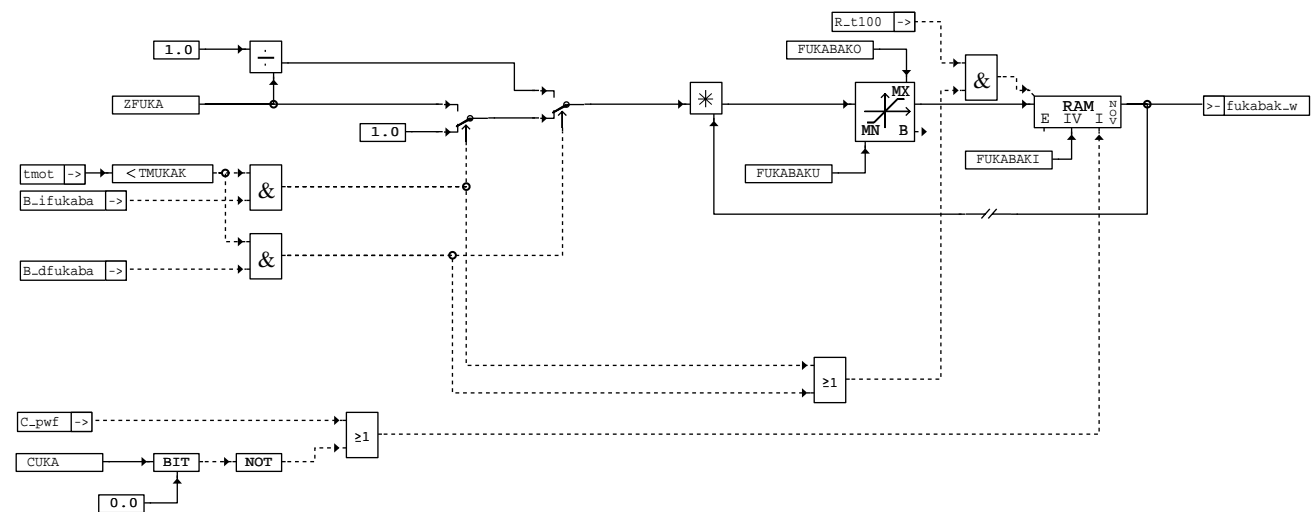


esuka-ukaaa(wba)

Scanning of B\_ukaiba and B\_ukadba and corresponding incrementing/decrementing of ainkba in the 10-ms-cycle.

Remaining partial function in the 100-ms-cycle

UKABAF(KBA): Calculation of correction factor BA cold engine

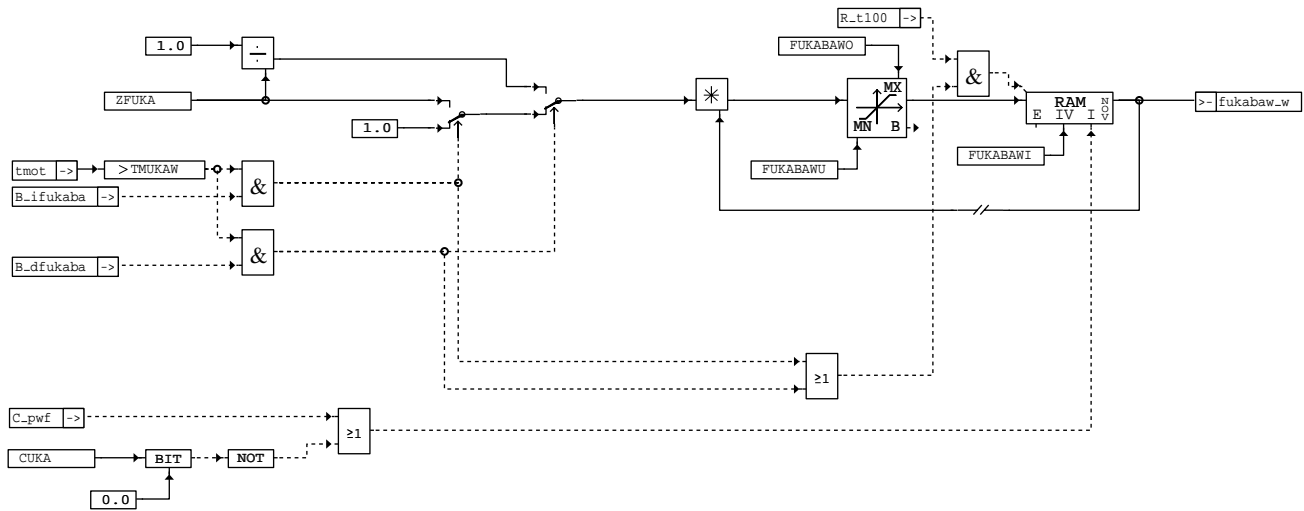


esuka-ukabafkba

Processing in the 100-ms-cycle.

UKABAFWBA: Calculation of correction factor BA hot engine

=====



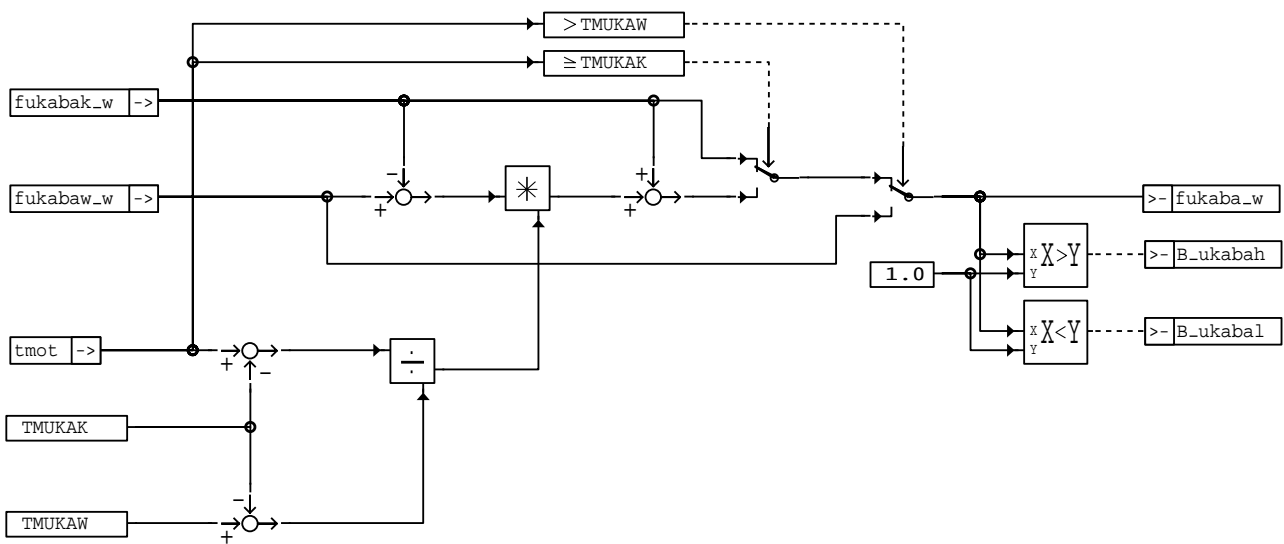
**esuka-ukabafwba**

Processing in the 100-ms-cycle.

UKABGAFBA: Calculation of total correction factor BA

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Interpolation cold/hot

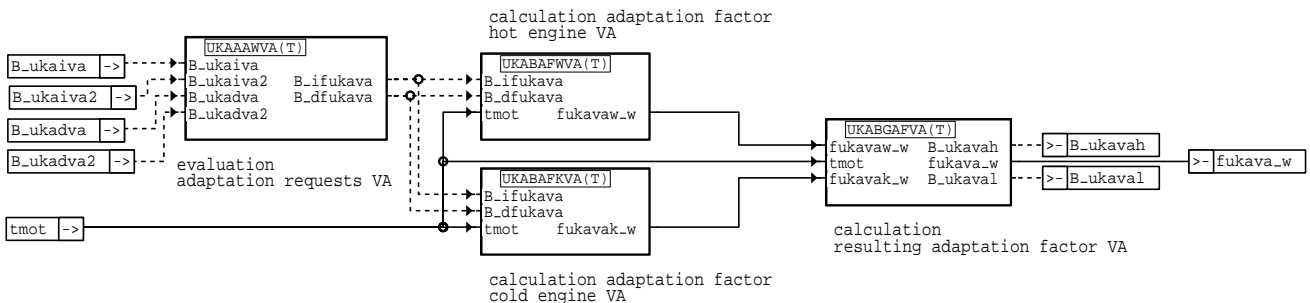


**esuka-ukabgafba**

Processing in the 100-ms-cycle.

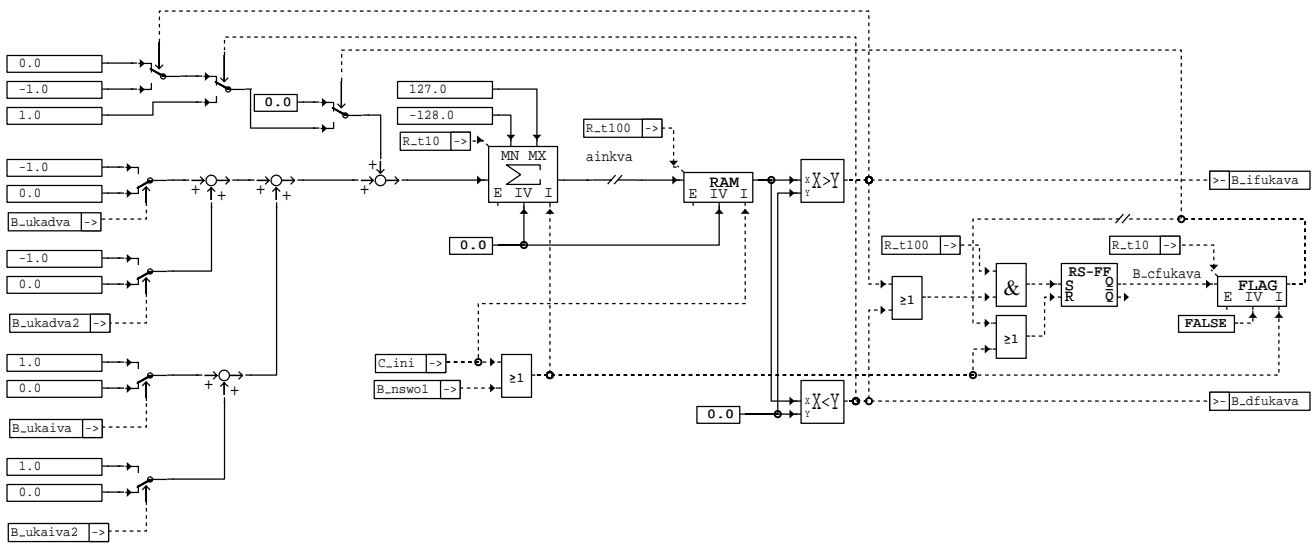
UKABAFVA: Calculation of correction factor VA

=====



**esuka-ukabafva**

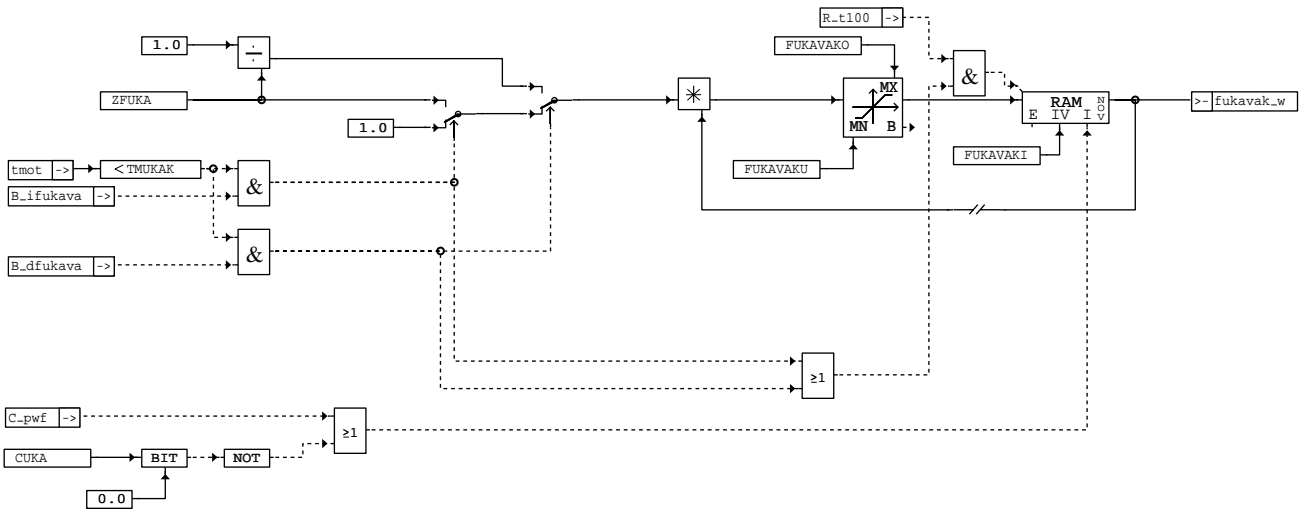
UKAAAWVA: Evaluation of adaptation requests VA  
=====



**esuka-ukaaawva**

Scanning of B\_ukaiva and B\_ukadva and corresponding incrementing/decrementing of ainkva in the 10-ms-cycl.  
Remaining partial function in the 100-ms-cycle.

UKABAFKVA: Calculation of correction factor VA cold engine  
=====

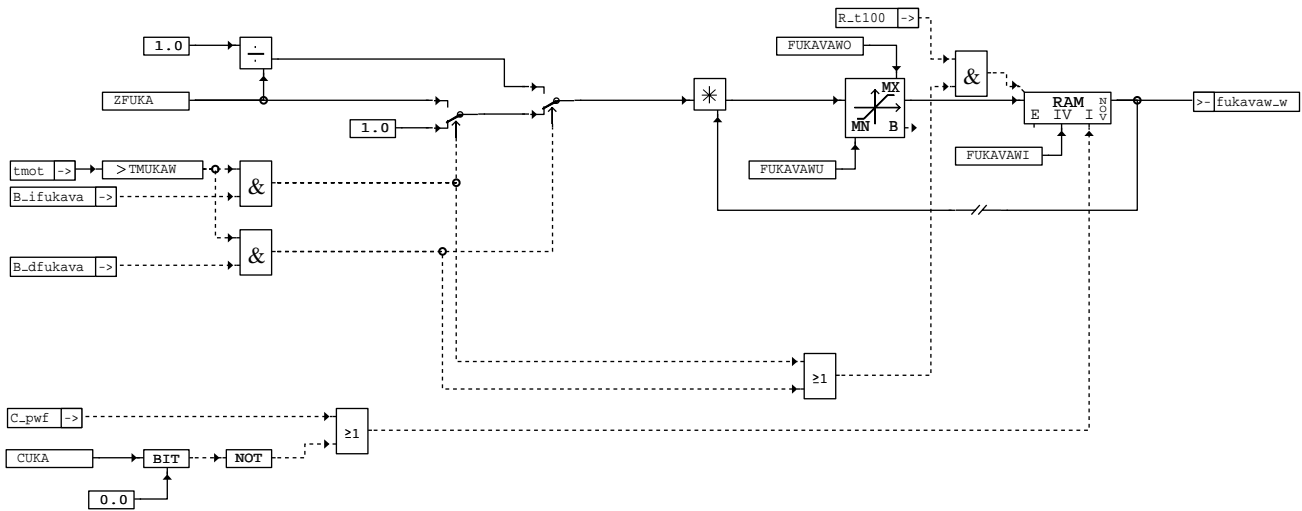


**esuka-ukabafkva**

Processing in the 100-ms-cycle.



UKABAFWVA: Calculation of correction factor VA hot engine

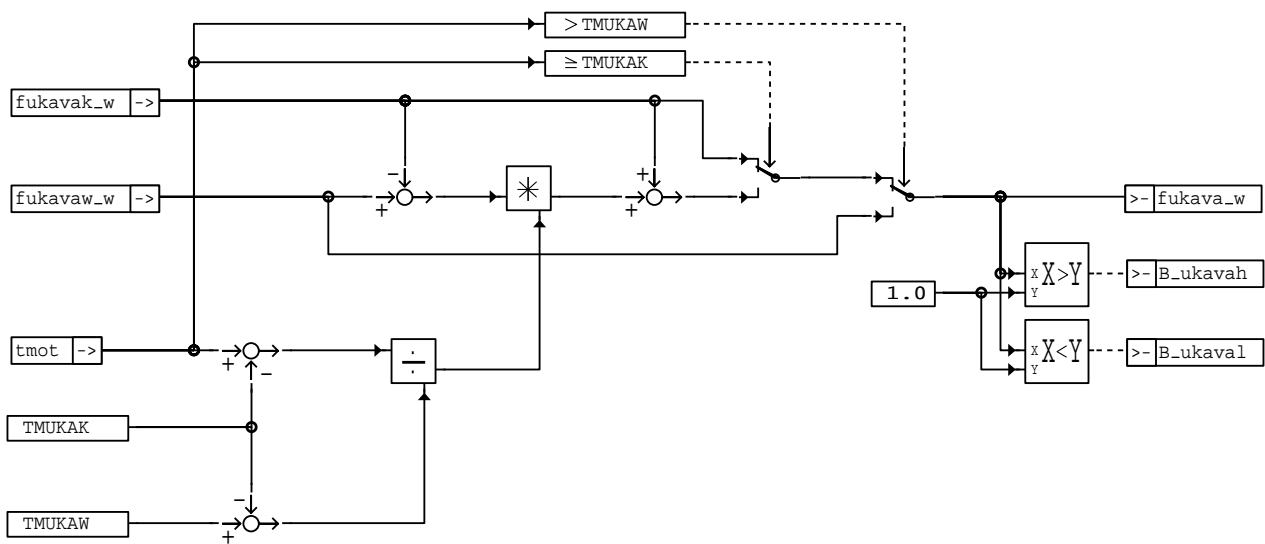


**esuka-ukabafwva**

Processing in the 100-ms-cycle.

UKABGAFVA: Calculation of total correction factor VA

Interpolation cold/hot



**esuka-ukabgafva**

Processing in the 100-ms-cycle.

**ABK ESUKA 13.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
ABAOVMX			FW	max. number accelerations without adaptation value return
AMNUUKA			FW	minimum number sensor bounces between 2 adapt. steps (trans. contr. adaptation)
ASPUUKA			FW	No. of O2 sensor signal bounces to disable adaptation of trans.contr.
AVAOVMX			FW	max. number decelerations without adaptation value return
CUKA			FW	code word for adaptation of transient control
DFRBAF			FW	delta lambda controller for detection BA rich
DFRBAM			FW	delta lambda controller for detection BA lean
DFRVAF			FW	delta lambda controller for detection VA rich
DFRVAM			FW	delta lambda controller for detection VA lean
DRLSPMN			FW	min. load change between O2 sensor sign. bounces for adaptation
FUKABAKI			FW	init.-value adaptive transient control correction factor BA (cold engine)
FUKABAKO			FW	upper limit adaptive transient control correction faktor BA (cold engine)
FUKABAKU			FW	lower limit adaptive transient control correction faktor BA (cold engine)
FUKABAWI			FW	init.-value adaptive transient control correction faktor BA (hot engine)



Parameter	Source-X	Source-Y	Type	Description
FUKABAWO			FW	upper limit adaptive transient control correction factor BA (hot engine)
FUKABAWU			FW	lower limit adaptive transient control correction factor BA (hot engine)
FUKAVAKI			FW	init.-value adaptive transient control correction factor VA (cold engine)
FUKAVAKO			FW	upper limit adaptive transient control correction faktor VA (cold engine)
FUKAVAKU			FW	lower limit adaptive transient control correction faktor VA (cold engine)
FUKAVAWI			FW	init.-value adaptive transient control correction faktor VA (hot engine)
FUKAVAWO			FW	upper limit adaptive transient control correction faktor VA (hot engine)
FUKAVAWU			FW	lower limit adaptive transient control correction faktor VA (hot engine)
NUKAO			FW	upper engine speed limit for adaptation of transient control
NUKAU			FW	lower engine speed limit for adaptation of transient control
RLUKAO			FW	upper load limit for adaptation of transient control
RLUKAU			FW	lower load limit for adaptation of transient control
TMUKAK			FW	temperature range cold engine for adaption of transient control
TMUKAU			FW	lower engine temperature limit for adaptation of trans.contr.
TMUKAW			FW	temperature range hot engine for adaptation of transient control
TNSUUKA			FW	disabling time of trans. contr. adaptation during post-cranking
ZFUKA			FW	changing rate of adaptive transient control correction factor
Variable	Source		Type	Description
ABAOV	ESUKA		LOK	number accelerations without adaptation adjustment
ABAOV2	ESUKA		LOK	number accelerations without adaptation adjustment bank 2
AINKBA	ESUKA		LOK	number of increment-wishes BA
AINKVA	ESUKA		LOK	number of increment-wishes VA
ASPUKA	ESUKA		LOK	counter sensor signal bounces at prohibition of transient control adaptation
ASPUKA2	ESUKA		LOK	counter for sensor signal bounces at prohibition of TC-adaptation (bank 2)
AVAOV	ESUKA		LOK	number decelerations without adaptation adjustment
AVAOV2	ESUKA		LOK	number decelerations without adaptation adjustment bank 2
B-AMNUKA	ESUKA		LOK	Condition: minimum number of sensor bounces between adaptation steps occurred
B-AMNUKA2	ESUKA		LOK	Condition: minimum number of sensor bounces between adapt. steps occurred bank 2
B-CFUKABA	ESUKA		LOK	calculation of adaptation-factor (transient control adaptation) BA
B-CFUKAVA	ESUKA		LOK	calculation of adaptation-factor (transient control adaptation) VA
B-DFUKABA	ESUKA		LOK	condition: decrement adaptation factor BA
B-DFUKAVA	ESUKA		LOK	condition: decrement adaptation factor VA
B-DKTLF	DKAT		EIN	Request of parameter switch over in lambda control
B-ENWS	DNWS		EIN	condition error camshaft control
B-FRMAX	LR		EIN	lambda control sets bit when lambda controller reaches its limit FRMAX
B-FRMAX2	LR		EIN	lambda control sets bit when lambda control reaches it limit FRMAX, bank2
B-FRMIN	LR		EIN	lambda control sets bit when lambda controller reaches its limit FRMIN
B-FRMIN2	LR		EIN	lambda control sets bit when lambda control reaches its limit FRMIN, bank2
B-JFUKABA	ESUKA		LOK	condition: increment adaptation factor BA
B-JFUKAVA	ESUKA		LOK	condition: increment adaptation factor VA
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRSP	LR		EIN	Flag 'O2 sensor voltage crosses threshold detected'
B_LRSP2	LR		EIN	condition for sensor signal bounce cylinderbench 2
B-MDARV	DMDMIL		EIN	critical misfire rate detected
B-NLDG			EIN	condition limp-home function speed sensor
B-NSWO1	PROKON		EIN	condition engine speed > NSWO1
B-TE	TEBEB		EIN	Condition canister purge active
B-TEHB	TEB		EIN	condition for canister purge system with high canister load
B-JKA	ESUKA		LOK	Enable flag adaptation of transient control
B-JKA2	ESUKA		LOK	enable flag for transient control adaptation bank 2
B-JKAB	ESUKA		LOK	condition valid operation range for transient control adaptation
B-JKABA	ESUKA		LOK	condition acceleration (transient control adaptation)
B-JKABA2	ESUKA		LOK	condition acceleration (transient control adaptation) bank 2
B-JKABAF	ESUKA		LOK	condition: BA fett
B-JKABAF2	ESUKA		LOK	condition: BA fett Bank 2
B-JKABAH	ESUKA		LOK	Flag BA increased by transient control adaptation
B-JKABAL	ESUKA		LOK	Flag BA decreased by transient control adaptation
B-JKABAM	ESUKA		LOK	condition: BA lean
B-JKABAM2	ESUKA		LOK	condition: BA lean bank 2
B-JKADBA	ESUKA		LOK	decrement-wish transient control adaptation BA
B-JKADBA2	ESUKA		LOK	decrement-wish transient control adaptation at BA cylinderbench 2
B-JKADVA	ESUKA		LOK	decrement-wish transient control adaptation VA
B-JKADVA2	ESUKA		LOK	decrement-wish transient control adaptation at VA cylinderbench 2
B-JKAIBA	ESUKA		LOK	increment-wish BA transient control adaptation
B-JKAIBA2	ESUKA		LOK	increment-wish BA transient control adaptation cylinderbench 2
B-JKAIVA	ESUKA		LOK	increment-wish VA transient control adaptation
B-JKAIVA2	ESUKA		LOK	increment-wish VA transient control adaptation cylinderbench 2
B-JKAT	ESUKA		LOK	timer for prohibition of transient control adaptation expired
B-JKAVA	ESUKA		LOK	deceleration condition (transient control adaptation)
B-JKAVA2	ESUKA		LOK	deceleration condition (transient control adaptation) cylinderbench 2
B-JKAVAF	ESUKA		LOK	condition: VA rich
B-JKAVAF2	ESUKA		LOK	condition: VA rich bank 2
B-JKAVAH	ESUKA		LOK	Flag VA increased by transient control adaptation
B-JKAVAL	ESUKA		LOK	Flag VA decreased by transient control adaptation
B-JKAVAM	ESUKA		LOK	condition: VA lean
B-JKAVAM2	ESUKA		LOK	condition: VA lean bank 2
C-JNI	SWADAP		EIN	ECU-condition for intialisation
C-PWF	SWADAP		EIN	ECU-condition powerfail initialisation
DFRSP2_W	LR		EIN	delta peak value lambda control factor frsp bank 2
DFRSP_W	LR		EIN	delta peak value lambda control factor frsp





Variable	Source	Type	Description
DFRST2_W	LR	EIN	A/F ratio controller output stroke in steady-state condition (cylinderbench 2)
DFRST_W	LR	EIN	A/F ratio controller output stroke (steady-state condition)
DRLSP	ESUKA	LOK	load change between 2 consecutive sensor signal bounces
DRLSP2	ESUKA	LOK	load change between 2 sensor signal bounces (bench 2)
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
FUKABAK_W	ESUKA	LOK	factor adaptive transient control (cold engine) BA
FUKABAW_W	ESUKA	LOK	actor adaptive transient control (hot engine) BA
FUKABA_W	ESUKA	AUS	factor adaptive transient control BA
FUKAVAK_W	ESUKA	LOK	factor adaptive transient control (cold engine) VA
FUKAVAW_W	ESUKA	LOK	actor adaptive transient control (hot engine) VA
FUKAVA_W	ESUKA	AUS	factor adaptive transient control VA
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
RLSP	ESUKA	LOK	load signal value at O2 sensor signal bounce
RLSP2	ESUKA	LOK	load signal at O2 sensor signal bounce (bench 2)
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TMOT	SWADAP	EIN	Engine temperature
TNST_W	BBSTT	EIN	time after end of start

### FW ESUKA 13.30 Fixed Values

Parameter	Value	Description
ABAOVMX		max. number accelerations without adaptation value return
AMNUUKA		minimum number sensor bounces between 2 adapt. steps (trans. contr. adaptation)
ASPUUKA		No. of O2 sensor signal bounces to disable adaptation of trans.contr.
AVAOVMX		max. number decelerations without adaptation value return
CUKA		code word for adaptation of transient control
DFRBAF		delta lambda controller for detection BA rich
DFRBAM		delta lambda controller for detection BA lean
DFRVAF		delta lambda controller for detection VA rich
DFRVAM		delta lambda controller for detection VA lean
DRLSPMN		min. load change between O2 sensor sign. bounces for adaptation
FUKABAKI		init.-value adaptive transient control correction factor BA (cold engine)
FUKABAKO		upper limit adaptive transient control correction faktor BA (cold engine)
FUKABAKU		lower limit adaptive transient control correction factor BA (cold engine)
FUKABAWI		init.-value adaptive transient control correction factor BA (hot engine)
FUKABAWO		upper limit adaptive transient control correction factor BA (hot engine)
FUKABAWU		lower limit adaptive transient control correction factor BA (hot engine)
FUKAVAKI		init.-value adaptive transient control correction factor VA (cold engine)
FUKAVAKO		upper limit adaptive transient control correction faktor VA (cold engine)
FUKAVAKU		lower limit adaptive transient control correction factor VA (cold engine)
FUKAVAWI		init.-value adaptive transient control correction factor VA (hot engine)
FUKAVAWO		upper limit adaptive transient control correction factor VA (hot engine)
FUKAVAWU		lower limit adaptive transient control correction factor VA (hot engine)
NUKAO		upper engine speed limit for adaptation of transient control
NUKAU		lower engine speed limit for adaptation of transient control
RLUKAO		upper load limit for adaptation of transient control
RLUKAU		lower load limit for adaptation of transient control
TMUKAK		temperature range cold engine for adaption of transient control
TMUKAU		lower engine temperature limit for adaptation of trans.contr.
TMUKAW		temperature range hot engine for adaptation of transient control
TNSUUKA		disabling time of trans. contr. adaptation during post-cranking
ZFUKA		changing rate of adaptive transient control correction factor



## FB ESUKA 13.30 Detailed description of function

Task:  
=====

On-line correction of the transient control in case of coking of the intake valves, manufacturing tolerances, changed fuel characteristics etc.

Principle:  
=====

The transient control (ÜK) is corrected by an amplitude factor, which acts on all parts of the ÜK, if in case of load changes larger deviations in the air / fuel ratio are detected. For this, the amplitude of the control oscillation is evaluated by the two-step Lambda control.

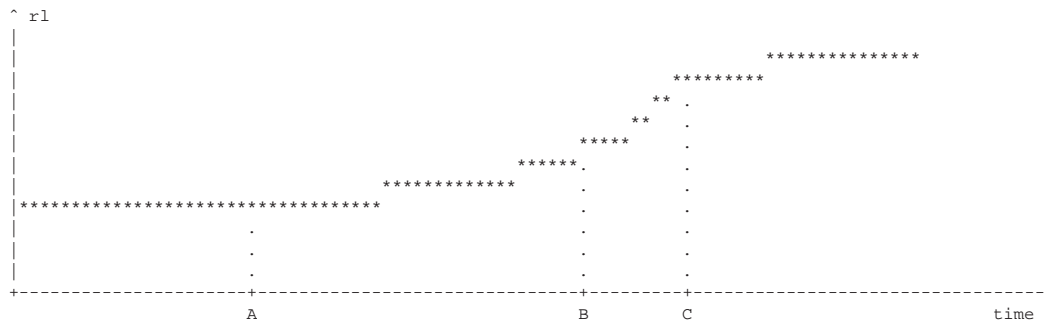
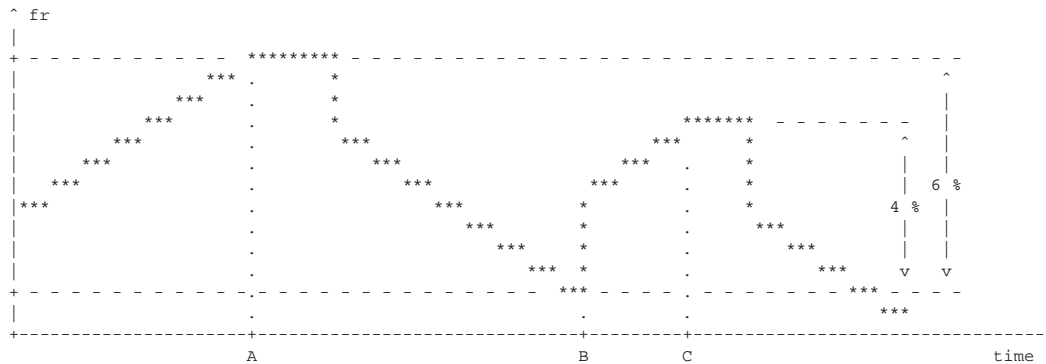
The adaptation factor is realized separately for BA (fukaba) and VA (fukava). For simplification reasons, however, only the factor fuka is mentioned in the following function description.

If there is no fault in the air / fuel ratio, then the typical control amplitude of the Lambda control is 6% (application instructions for Lambda control). If the change of the control factor deviates considerably from this value between two sensor step changes and if simultaneously a distinct load change occurs between the corresponding sensor step changes, then it is assumed that the wall wetting behaviour has changed with regard to the initial state and the correction factors fukaba with acceleration and fukava with deceleration are changed accordingly.

Example: In the course illustrated below, the control amplitude between the sensor step changes (A) and (B) is 6%, i.e. this fr-course corresponds to the application state. There is no Lambda deviation.

From sensor step (B) to (C) the control factor, however, rises by 4%, i.e. the Lambda control does not enrich as much as was expected. In this case, therefore, there must be a rich fault. Since the load rises simultaneously in the range (B) to (C), it is obvious that the acceleration enrichment is too strong. --> The factor fuka is decremented at point (C).

The position of the fr-mean value is of no significance. By this the procedure becomes independent of the basic adaptation.



On systems with stereo Lambda control the control oscillations of the two cylinder banks are evaluated independent of one another according to the above principle. However, only a common factor fuka is made available for both cylinder banks, i.e. the incrementing resp. decrementing steps determined from the fr-courses of the two cylinder banks act on the same factor fuka.

Dependent on the cause of the change of the wall wetting behaviour a different correction of the transient control needs to be performed with hot resp. cold engine. Valve coking for example necessitates about the same correction factors for the ÜK with hot and with cold engine. On the other hand some fuel types can reduce the build-up of the wall wetting as regards the application state with a hot engine and increase it with a cold engine. For the adaptive ÜK the correction factor is therefore composed of the factors fukak and fukaw for cold and for hot engine dependent on the engine temperature:





The adjustment requests for the factor fuka are determined according to the combination of the input conditions:

Acceleration and enleanment	-----> increase fuka	(B_ukai = 1)
Acceleration and enrichment	-----> decrease fuka	(B_ukad = 1)
Deceleration and enleanment	-----> decrease fuka	(B_ukad = 1)
Deceleration and enrichment	-----> increase fuka	(B_ukai = 1).

The two counters abaoov resp. avaoov accumulate the number of accelerations resp. decelerations where no mixture deviations were detected. If an applicable number ABAOVMX resp. AVAOVMX is exceeded, the corresponding adaptation factor is adjusted back in direction of its neutral value 1.0 by one increment.

An adjustment request may generally only be set if the ÜK adaptation is released for this cylinder bank.

The adjustment requests B\_ukai2 and B\_ukad2 for cylinder bank 2 are determined in the same way on the basis of the fr and rl evaluation. The adjustment requests of both cylinder banks need to be coordinated and transferred to the 100-ms-cycle, which performs the new calculation of the factor fuka (see partial function "Evaluation of adaptation requests" described below). So as to save calculation time this partial function is switched off at high engine speed (B\_nswol = 1).

Detection of adaptation range:  
=====

This partial function checks the prohibition ranges for the ÜK adaptation, in as far as they mutually apply to both cylinder banks.

The flag B\_ukab (permissible operating range for adaptation) is set, if the following conditions are fulfilled:

- Adaptation released via code word CUKA[bit 0] = 1
- B\_te = 1 and ÜK adaptation is released in the canister purging phase (CUKA(bit 2)=1) as well as no high charge of the canister purge flow: B\_tehb = 0 .
- B\_te = 0 and ÜK adaptation is released in the basic adaptation phase (CUKA(bit 3)=1)
- Engine speed within permissible range: NUKAU <= nmot <= NUKAO .
- No increase of contoller excursion at catalyst diagnosis
- No critical misfire rate
- No error of tank vent valve
- No error of tank vent valve output stage
- Load within permissible range: RLUKAU <= rl <= RLUKAO.
- Engine temperature is above a minimum value: TMUKAU <= tmot .
- Engine temperature is not in the tmot transition range TMUKAK <= tmot <= TMUKAW
- The prohibition time TNSUUKA has elapsed after end of start

The flag B\_ukat=1 indicates that the prohibition time for the ÜK adaptation during after-start has elapsed. (Only relevant for hot start. In case of cold start is must be waited anyhow until the engine temperature threshold TMUKAU and the operating readiness of the Lambda control is reached).

So as to save calculation time this partial function is switched off at high engine speed (B\_nswol = 1).

Evaluation of adaptation requests (BA/VA):  
=====

This function serves for the transfer of adjustment requests determined in the 10-ms-cycle to the 100-ms-cycle. If an increment request is detected in the 10-ms-cycle, it leads to an increase of the counter aink. In case of a decrement request the count is decreased. The adjustment requests stored in aink are processed in the subsequent runs of the 100-ms-cycle. The bit B\_ifuka indicates that the count aink is positive, i.e. the adaptation factor fuka is to be incremented. The bit B\_dfuka indicates that the count aink is negative, i.e. the adaptation factor fuka is to be decremented. So as to save calculation time this partial function (only parts in the 10-ms-cycle) is switched off at high engine speed (B\_nswol = 1).

Calculation of correction factor cold engine (BA/VA):  
=====

If the engine temperature lies below the threshold TMUKAK, the factor fukak for cold engine is changed dependent on the adjustment requests indicated by the bits B\_ifuka resp. B\_dfuka. If the transient control is too weak, the old value of the factor fukak is multiplied by ZFUKA. With too strong transient control, fukak is divided by ZFUKA. The calculated new value is limited to the adjustment range FUKAKU < fukak < FUKAKO. For quantization reasons the value of fukak shall furthermore not become less than approx. 0.1. The newly calculated value of fukak is stored in the battery-backed RAM area.

In the event of powerfail as well as in case of prohibited adaptation by the code word CUKA, fukak is set to the adjustable initialization value FUKAKI. The application engineer is responsible himself that the initialization value FUKAKI is within the permissible limits for fukak. No check is performed during the initialization.

Calculation of correction factor hot engine (BA/VA):  
=====

If the engine temperature lies above the threshold TMUKAW, the factor fukaw for hot engine is changed dependent on the adjustment requests indicated by the bits B\_ifuka resp. B\_dfuka. If the transient control is too weak, the old value of the factor fukaw is multiplied by ZFUKA. With too strong transient control, fukaw is divided by ZFUKA. The calculated new value is limited to the adjustment range FUKAWU < fukaw < FUKAWO. For quantization reasons the value of fukaw shall furthermore not become less than approx. 0.1. The newly calculated value of fukaw is stored in the battery-backed RAM area.

In the event of powerfail as well as in case of prohibited adaptation by the code word CUKA, fukaw is set to the adjustable initialization value FUKAWI. The application engineer is responsible himself that the initialization value FUKAWI is within the permissible limits for fukaw. No check is performed during the initialization.



Calculation of total correction factor (BA/VA):  
=====

With cold engine (  $t_{mot} < TMUKAK$  ) resp. with hot engine (  $t_{mot} > TMUKAW$  ) the factors fukak resp. fukaw chosen for the corresponding temperature range are selected and passed on to the ÜK as total correction factor fuka. In the transition temperature range a  $t_{mot}$ -dependent linear interpolation between fukak and fukaw is performed.  
The flags B\_ukabah, B\_ukavah, B\_ukabal and B\_ukaval show the actual position of the adaptation factors.

## APP ESUKA 13.30 Application hint

Preconditions:  
=====

- Steady-state basic application
- Application of the charge sensing
- Application of the load prediction
- Application of the transient control
- Application of the Lambda control
- Application of the canister purge control, if ÜK adaptation is released in the canister purging phase

Please adhere to the order!

Application aiding devices:  
=====

VS100

Entry of the parameter:  
=====

General:

- Code word CUKA = FF (hex.) = 255 (dec.) (adaptation released, adaptation released in canister purging and basic adaptation phase)
- Control amplitude adaptation released in Lambda control: CFRA = 1

Calculation of load change:

- min. load change for adaptation: DRLSPMN = 5 %
- min. no. of sensor step changes between two adaptation processes: AMNUUKA = 4

Calculation of mixture deviation:

- Threshold for detection BA lean: DFRBAM = 0.03
- Threshold for detection VA lean: DFRVAM = 0.03
- Threshold for detection BA rich: DFRBAF = -0.04
- Threshold for detection VA rich: DFRVAF = -0.05

Adaptation release:

- No. of sensor steps prior to the adaptation being switched on again: ASPUUKA = 4 (especially critical here is the no. of control periods after fuel cut-in).

Adaptation request:

- Maximum number of accelerations without adjustment of adaptation factor: ABAOVMX = 10
- Maximum number of decelerations without adjustment of adaptation factor: AVAOVMX = 10
- Return mechanism of adaptation factors enabled: CUKA[Bit(4)] = 1

Detection of adaptation range:

- Engine speed range: lower limit: NUKAU = 900 rpm  
upper limit: NUKAO = switch-off engine speed of the ÜK, (project-dependent, typically 4520 rpm)
- Load range: lower limit RLUKAU = 20 %  
upper limit RLUKAO = 80 %
- Engine temperature range: TMUKAU = switch-on threshold of the Lambda control. Typically  $\geq 20^\circ\text{C}$   
TMUKAK > TMUKAU + approx.  $20^\circ\text{C}$ , typically TMUKAK =  $40^\circ\text{C}$   
TMUKAW =  $70^\circ\text{C}$   
TMUKAK must be chosen with sufficient pos. clearance to the switch-on temperature TMUKAU since otherwise no adaptation of the cold factor fukak will take place !  
TMUKAW may not be chosen greater than the operating temperature of the hot engine, since otherwise no adaptation of the hot factor fukaw will take place !  
It must apply:  $TMUKAU + 20^\circ\text{C} < TMUKAK < TMUKAW < \text{operating temperature hot engine}$
- Waiting time after end of start: TNSUUKA = 20 sec

Calculation of correction factor:

- Increment for fuka-adjustment: ZFUKA = 1.015 for stereo LC  
ZFUKA = 1.03 for mono LC
- Initialization values FUKABAKI = FUKABAWI = FUKAVAKI = FUKAVAWI = 1.0
- Min. and max. limits for correction factor: FUKABAKU = 0.9, FUKABAKO = 2.0  
FUKABAWU = 0.9, FUKABAWO = 2.0  
FUKAVAKU = 0.7, FUKAVAKO = 1.1  
FUKAVAWU = 0.7, FUKAVAWO = 1.1
- Temperature ranges: TMUKAK > TMUKAU + approx.  $20^\circ\text{C}$ , typically TMUKAK =  $40^\circ\text{C}$   
TMUKAW =  $70^\circ\text{C}$   
TMUKAK must be chosen with sufficient pos. clearance to the switch-on temperature TMUKAU, since otherwise no adaptation of the cold factor fukak will take place !  
TMUKAW may not be chosen greater than the operating temperature of the hot engine, since otherwise no adaptation of the hot factor fukaw will take place !  
It must apply:  $TMUKAU + 20^\circ\text{C} < TMUKAK < TMUKAW < \text{operating temperature hot engine}$



Procedure:  
=====

- 1.) Determine the adaptation range ("Detection of adaptation range ").  
The permissible adaptation range (n, r1, ps, tmot) should cover that range, in which a satisfactory application of the transient control was possible. Problematic ranges must be deactivated. Especially the ranges idling and full load need to be deactivated. Suggested data to be entered see above.
- 2.) By selecting the thresholds DFRBAF, DFRBAM, DFRVAF and DFRVAM the tolerance range for the detection of a mixture deviation is determined. The thresholds must be chosen such that with ideal conditions (no coking, good fuel quality) no correction of the ÜK takes place. With usual "rich derivation" the thresholds for the detection of enrichment DFRBAF and DFRVAF must therefore be chosen with a greater absolute value than the thresholds for the detection of enleanment DFRBAM and DFRVAM.

Switch-off of the function:  
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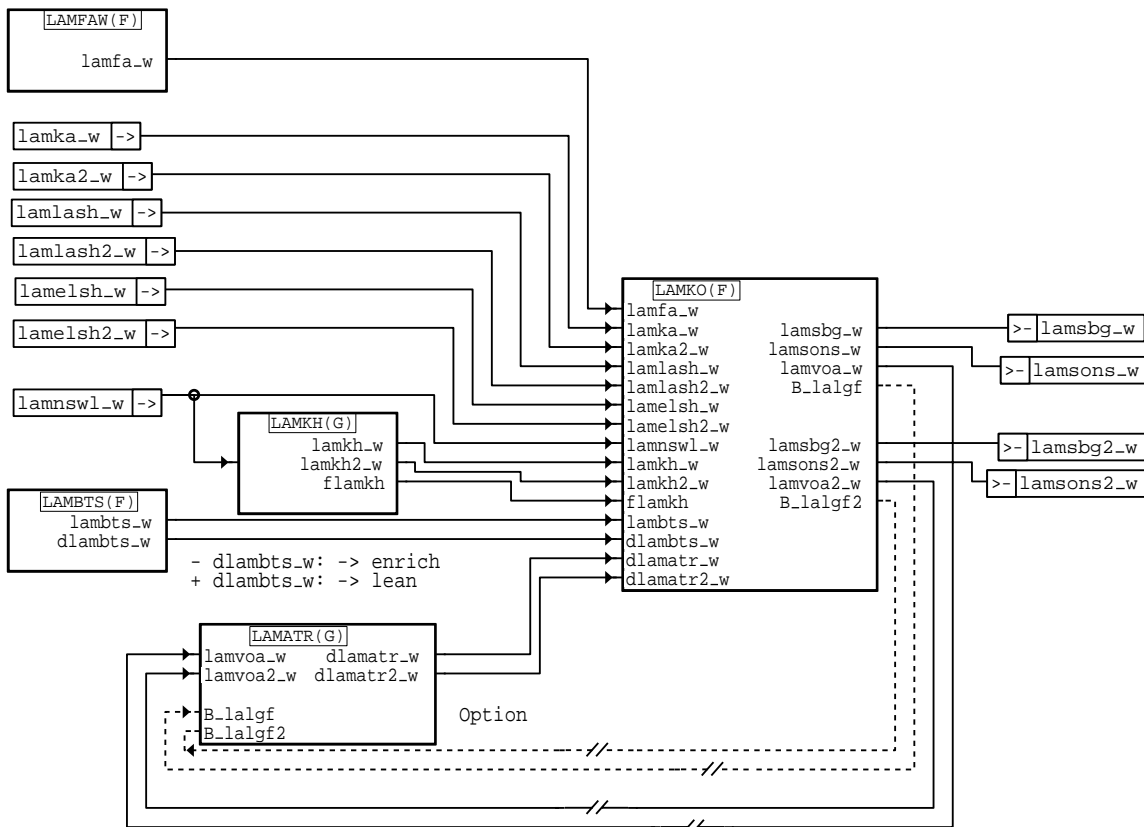
Prohibition of the ÜK adaptation: Set code word CUKA, bit 0 = 0. Adjustment of the desired values for fukaba, fukava:  
Set FUKABAKI, FUKABAWI, FUKAVAKI, FUKAVAWI to desired values

Influenced functions:  
=====

§ESUK

## LAMSOLL 1.30 Lambda setpoint input

### FDEF LAMSOLL 1.30 Function definition



lamsoll-lamsoll

lamsoll-lamsoll



The overview LAMSOLL shows the formation of the nominal values for Lambda in the combustion chamber lamsbg\_w, lamsbg2\_w and Lambda at the sensor lamsons\_w, lamsons2\_w. A nominal Lambda limited lamsbg is calculated for the advance control of a combustion chamber Lambda from the different absolute Lambda requests lamfa\_w, lamnswl\_w, lambts\_w lamkh\_w by a minimum selection as well as the additive delta Lambda requests in the function Lambda coordination LAMKO. The limitation is set by the running limit of the engine for rich (lalgf) and lean (lalgm) mixtures in the respective running state. The incorporation of the nominal lambda value lamsbg in the computation is shown in the function Mixture Control GK. All interventions for Lambda which are not equal to Lambda 1.0 are realized by means of this intervention.

Lambda post start warm up lamnswl is active for the start and during engine warm up. This is 1.0 at the end of the engine warm up cycle.

The nominal requirement for the Lambda control is lamsons = lamsbg. Regulation is to this nominal Lambda if continuous Lambda control is present, and even if Lambda is not equal to 1.0.

If secondary air is injected during the warm up, then the transition is made by the factor flamkh from lamnswl\_w to lamkh\_w. The return to lamnswl\_w is made following termination of secondary air injection. During this time, lamsbg and lamsons are different because the Lambda sensor detects "thinner" exhaust emissions due to the secondary air.

For a large charge and high speeds, the engine must be run with a Lambda < 1.0 for thermal reasons. The intervention foreseen for this is lambts\_w and is generated in the function LAMBTS ( Lambda component protection ). lambts\_w is an absolute Lambda, i.e. Lambda < 1.0 leads to enrichment.

An additive enrichment is realized by means of dlambs\_w (Function LAMBTS) as a function of the change in the ignition-timing efficiency so as not to give any thermal damage from exhaust emission temperatures which are high and attributable to poor gasoline quality and knock combustion resulting from this.

This additive Lambda nominal shift is taken into the computation with correct observance of the sign, i.e. negative values lead to a more enriched mixture.

A further enrichment additive dlamatr\_w, dlamatr2\_w is also realized for a given exhaust emission temperature control ATR by the exhaust emission temperature controller.

By the function LAMFAW, an additional engine torque request can be realized by the driver by a Lambda < 1.0.

Switchover is made to the fixed value LASOAB at the respective bank which is independent of the nominal Lambda for Ev cutoff's by the function AEVAB.

A nominal Lambda > 1.0 is given by this fixed value to ensure with certainty that no overheating of the catalyzer occurs.

### ABK LAMSOLL 1.30 Abbreviations

Variable	Source	Type	Description
B_LALGF	LAMSOLL	LOK	condition lambda limit "rich" active
B_LALGF2	LAMSOLL	LOK	condition lambda limit "rich" active
DLAMATR2_W	LAMSOLL	LOK	desired delta lambda of exhaust temperature control bank 2
DLAMATR_W	LAMSOLL	LOK	desired delta lambda of exhaust temperature control
DLAMBTS_W	LAMSOLL	LOK	delta lambda for component protection
FLAMKH	LAMSOLL	LOK	factor setting up lambda engine nominal at catalyst heating
LAMBTS_W	LAMSOLL	LOK	lambda for component protection
LAMELSH2_W	DLSH	EIN	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMELSH_W	DLSH	EIN	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMFA_W	LAMSOLL	LOK	required lambda, driver request
LAMKA2_W	LRKA	EIN	Lambdasetpoint catalyst clean out, bank2
LAMKA_W	LRKA	EIN	Lambdasetpoint catalyst o2 purge function
LAMKH2_W	LAMSOLL	LOK	Lambda engine nominal at catalyst heating, bank 2 (word)
LAMKH_W	LAMSOLL	LOK	Lambda engine nominal at catalyst heating (word)
LAMLASH2_W	DLSAHK	EIN	Desired Lambda for test oscillation check downstream catalyst bank2
LAMLASH_W	DLSAHK	EIN	Desired Lambda for test oscillation check downstream catalyst
LAMNSWL_W	ESVST	EIN	lambda engine nominal at afterstart and warming up
LAMSBG2_W	LAMSOLL	AUS	required lambda limitation Bank2
LAMSBG_W	LAMSOLL	AUS	Desired Lambda limitation (word)
LAMSONS2_W	LAMSOLL	AUS	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	AUS	required lambda referred to lambda sensor fitting location
LAMVOA2_W	LAMSOLL	LOK	lambda pilot control without additive parts
LAMVOA_W	LAMSOLL	LOK	lambda pilot control without additive parts

### FW LAMSOLL 1.30 Fixed Values

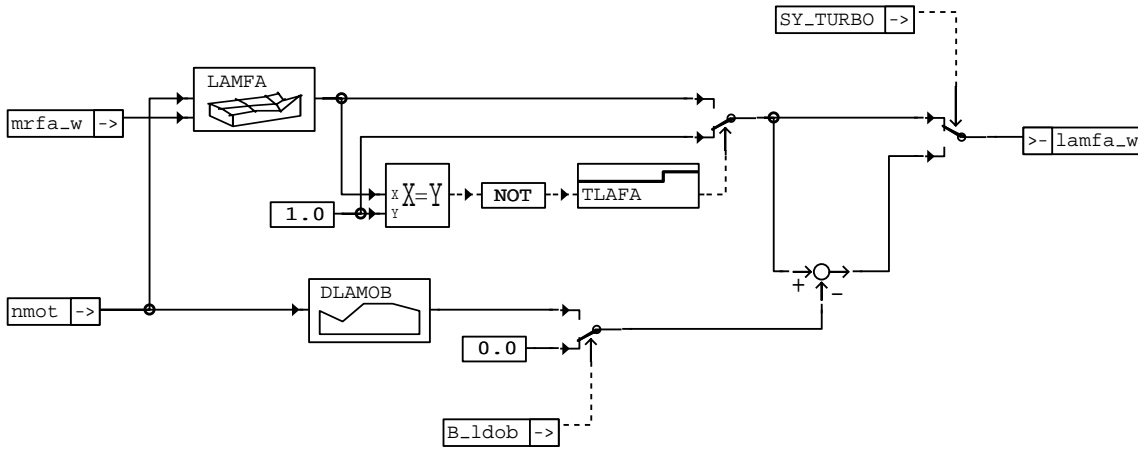
Parameter	Value	Description
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## FB LAMSOLL 1.30 Detailed description of function

## APP LAMSOLL 1.30 Application hint

## LAMFAW 2.20 Lambda vehicle-operator demand

### FDEF LAMFAW 2.20 Function definition



lamfaw-lamfaw

### ABK LAMFAW 2.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DLAMOB	NMOT		KL	delta lamda at overboost
LAMFA	NMOT	MRFA_W	KF	Lamda driver demand
TLAFA			FW	delay time for activation of lambda demand by driver

Variable	Source	Type	Description
B_LDOB		EIN	Condition overboost active
LAMFA_W	LAMFAW	AUS	required lambda, driver request
MRFA_W	MDFAW	EIN	relative driver request torque from cruise control and pedal, =0 in limp-home
NMOT	SWADAP	EIN	engine speed
SY_TURBO	PROKON	EIN	system constant for turbocharged engine

### FW LAMFAW 2.20 Fixed Values

Parameter	Value	Description
TLAFA		delay time for activation of lambda demand by driver

### FB LAMFAW 2.20 Detailed description of function

The function LAMFAW makes an enrichment if the driver wants to drive with max torque. The enrichment is made by changing the Lambda ( lamfaw\_w ) and replace the old function ' enrichment at full load '. A delay of the begin of enrichment is applicable with TLAFA. During overboost an additional enrichment is possible by the characteristic DLAMOB.

### APP LAMFAW 2.20 Application hint

TLAFA > 0 --> delay of the activation for enrichment  
TLAFA = 0 no delay of the activation for enrichment

MAP LAMFA:

nmot: 1000, 2000, 3000, 4000, 5000, 6000 1/min  
mrfa\_w : 70, 80, 90, 100, 110, 120 %

Values of MAP 1.0 --> disable of enrichment; values < 1.0 --> enrichment aktiv

With line DLAMOB an additional enrichment may be realized at turbo engines during overboost.

Line DLAMOB:

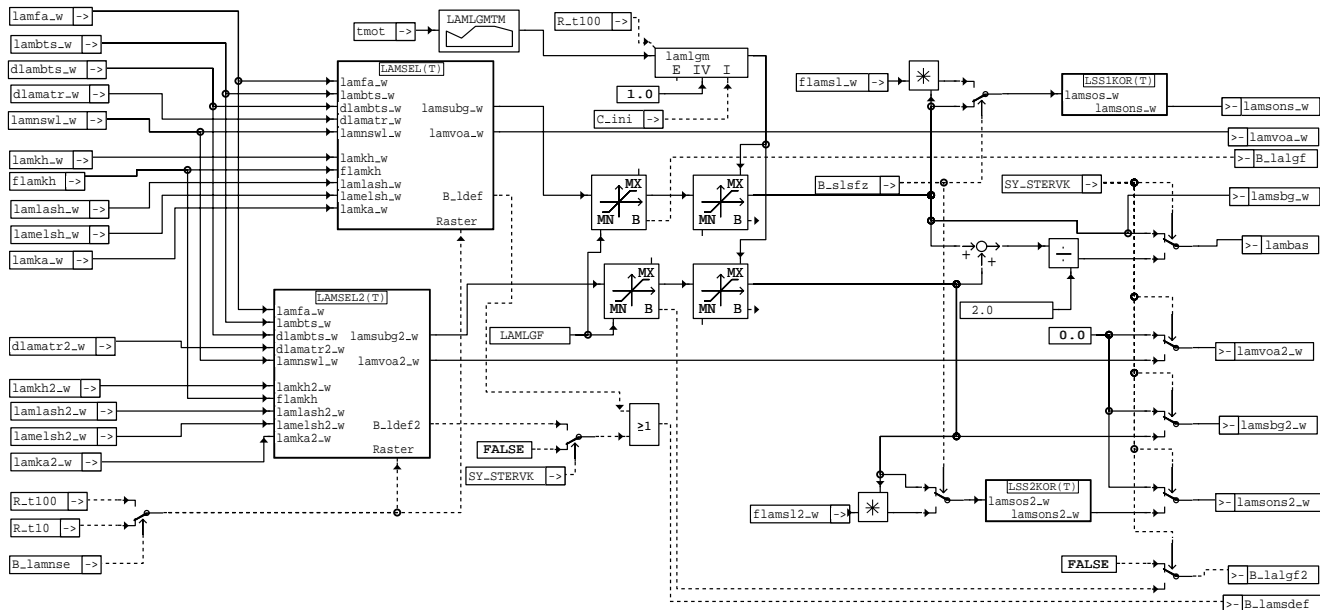
nmot: 1500, 2500, 3500, 4500, 5500, 6000  
Values 0

0: disable of enrichment; e.g. 0.1 enrichment of 10 %



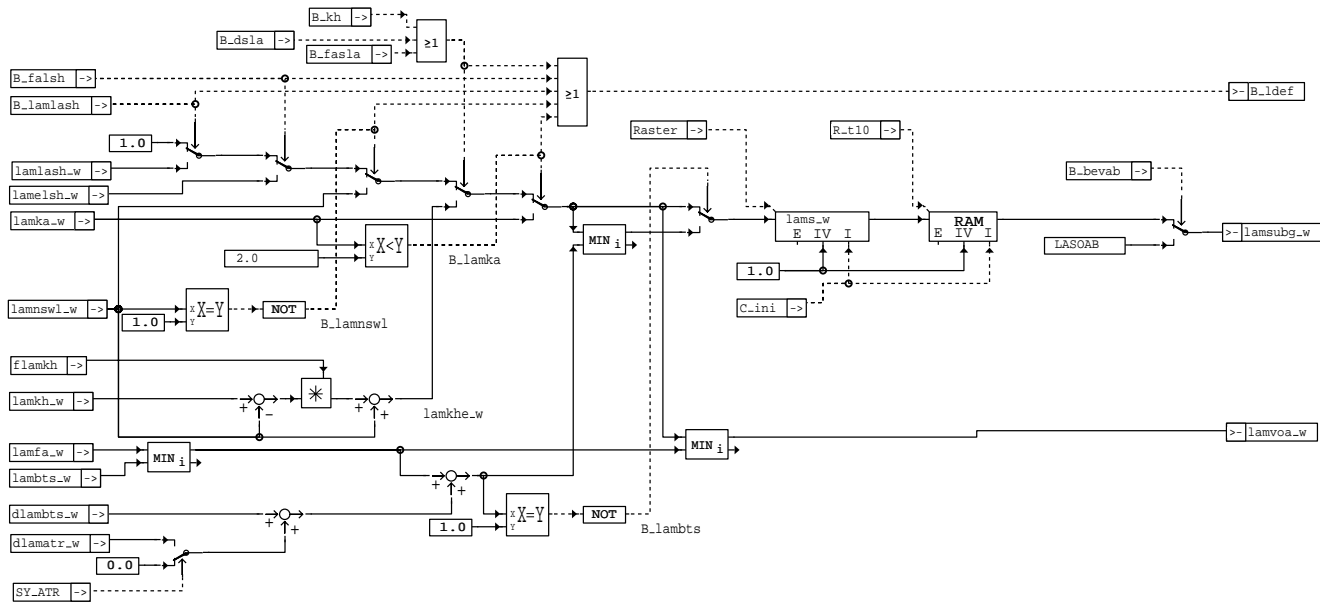
## LAMKO 3.120 Lambda coordination

### DDEF LAMKO 3.120 Function definition



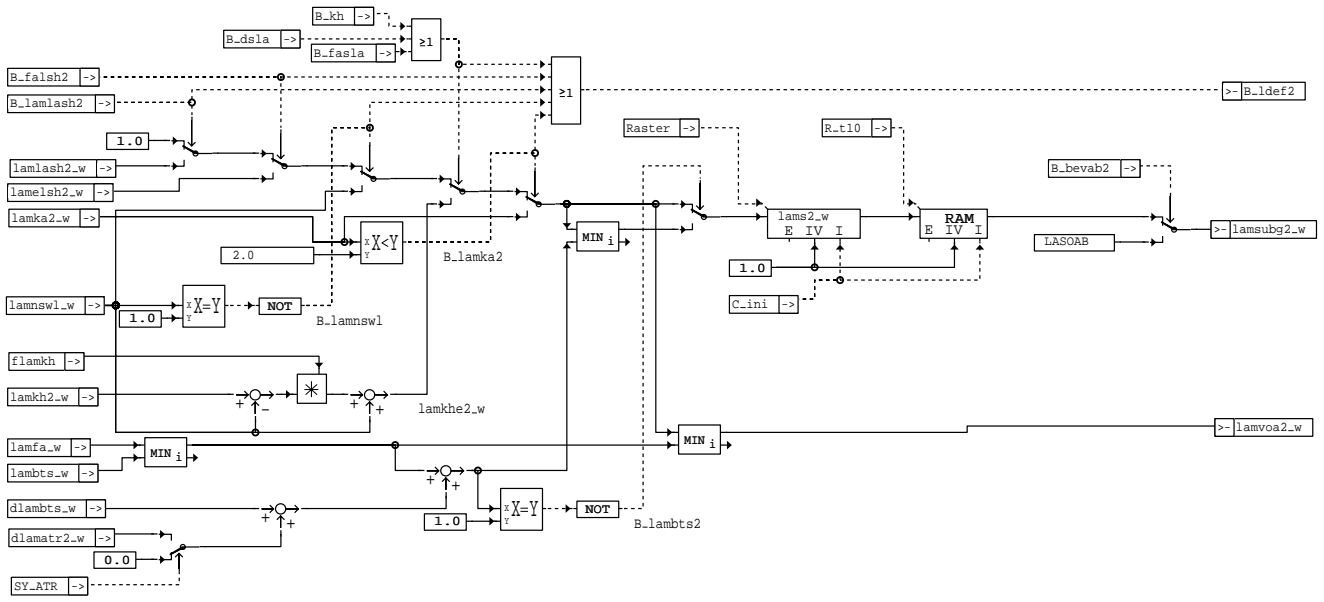
### lamko-lamko

subfunction selection of lambda at bank1: LAMSEL



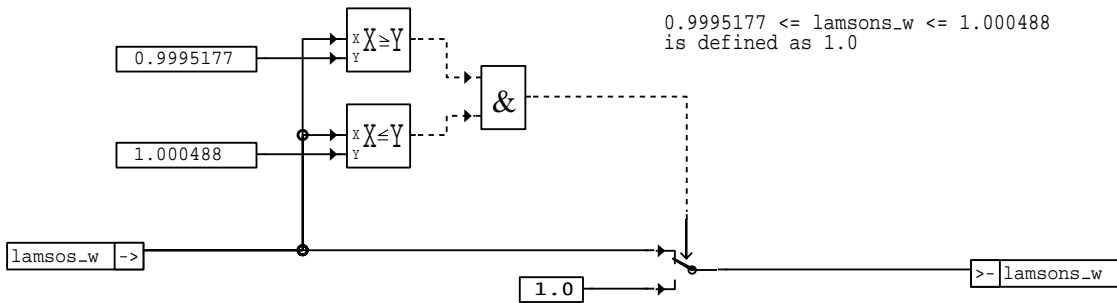
### lamko-lamsel

subfunction selection of lambda at bank2: LAMSEL2



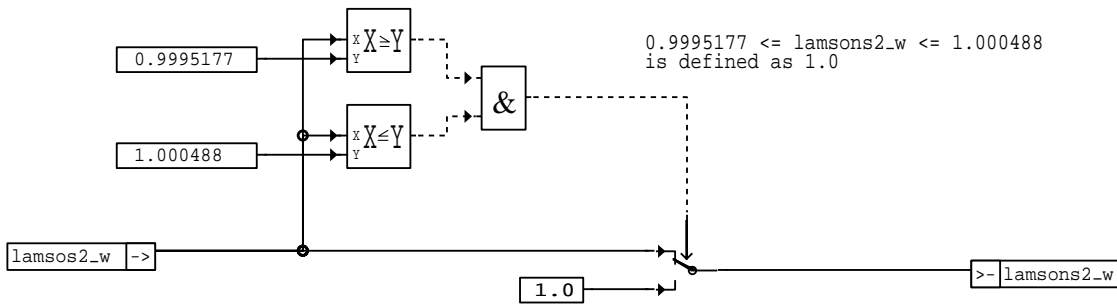
lamko-lamsel2

subfunction correction of nominal Lambda for lambdasensor bank1: LSS1KOR



lamko-lss1kor

subfunction correction of nominal Lambda for lambdasensor bank2: LSS2KOR



lamko-lss2kor

ABK LAMKO 3.120 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
LAMLGF			FW	lambda limit "rich"
LAMLGMTM	TMOT		KL	lambda limit "lean"
LASOAB			FW	target lambda value for bank shutdown
Variable	Source		Type	Description
B_BEVAB	BGEVAB		EIN	condition: Inj. valve cut off on Bank/Bank1
B_BEVAB2	BGEVAB		EIN	condition: Inj. valve cut off on Bank2
B_DSLA			EIN	adaption phase: calculation of secondary air mass



Variable	Source	Type	Description
B_FALSH		EIN	condition function request downstream oxygen sensor diagnosis
B_FALSH2		EIN	condition function request downstream oxygen sensor diagnosis bank2
B_FASLA		EIN	Condition: external request of SAI system aktiv
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_LALGF	LAMKO	AUS	condition lambda limit "rich" active
B_LALGF2	LAMKO	AUS	condition lambda limit "rich" active
B_LAMBT	LAMKO	LOK	lambda for component protection is active
B_LAMBT2	LAMKO	LOK	lambda for component protection is active (bank 2)
B_LAMKA	LAMKO	LOK	lambda for Katalyst oxygen purge is active
B_LAMKA2	LAMKO	LOK	lambda for Katalyst oxygen purge is active
B_LAMLASH		EIN	Condition for enleanment in %LAMKO
B_LAMLASH2		EIN	Condition for enleanment in %LAMKO bank2
B_LAMNSE		EIN	condition end of lamns.w calculation
B_LAMNSWL	LAMKO	LOK	lambda engine nominal at post start and warming up active
B_LAMSDEF	LAMKO	AUS	Condition: defined desired air/fuel ratio value
B_LDEF	LAMKO	LOK	Condition: defined desired value of the lambda (bank1)
B_LDEF2	LAMKO	LOK	Condition: defined desired value of the lambda (bank2)
B_SLSFZ	PROKON	EIN	condition: SLS fitted in vehicle
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DLAMATR2_W		EIN	desired delta lambda of exhaust temperature control bank 2
DLAMATR_W		EIN	desired delta lambda of exhaust temperature control
DLAMBT_W	LAMBT	EIN	delta lambda for component protection
FLAMKH	BBKHZ	EIN	factor setting up lambda engine nominal at catalyst heating
FLAMSL2_W		EIN	Factor lambda change by secondary air, bank 2
FLAMSL_W		EIN	Factor lambda change by secondary air
LAMBAS	LAMKO	AUS	basic Lambda
LAMBT_W	LAMBT	EIN	lambda for component protection
LAMELSH2_W	DLSH	EIN	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMELSH_W	DLSH	EIN	desired lambda for electrical sensor diagnosis behind catalyst (short trip)
LAMFA_W	LAMFAW	EIN	required lambda, driver request
LAMKA2_W	LRKA	EIN	Lambdasetpoint catalyst clean out, bank2
LAMKA_W	LRKA	EIN	Lambdasetpoint catalyst o2 purge function
LAMKH2_W	LAKH	EIN	Lambda engine nominal at catalyst heating, bank 2 (word)
LAMKHE2_W	LAMKO	LOK	lambda engine nominal at catalyst heating, actual, bank 2
LAMKHE_W	LAMKO	LOK	lambda engine nominal at catalyst heating, actual
LAMKH_W	MSF	EIN	Lambda engine nominal at catalyst heating (word)
LAMLASH2_W	DLSAHK	EIN	Desired Lambda for test oscillation check downstream catalyst bank2
LAMLASH_W	DLSAHK	EIN	Desired Lambda for test oscillation check downstream catalyst
LAMLGM	LAMKO	LOK	lambda limit "lean"
LAMNSWL_W	ESVST	EIN	lambda engine nominal at afterstart and warming up
LAMS2_W	LAMKO	LOK	Lambda nominal (word)
LAMSBG2_W	LAMKO	AUS	required lambda limitation Bank2
LAMSBG_W	LAMKO	AUS	Desired Lambda limitation (word)
LAMSONS2_W	LAMKO	AUS	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMKO	AUS	required lambda referred to lambda sensor fitting location
LAMSOS2_W	LAMKO	LOK	required lambda referred to lambda sensor fitting location bank2
LAMSOS_W	LAMKO	LOK	required lambda referred to lambda sensor fitting location
LAMSUBG2_W	LAMKO	LOK	Lambda nominal unlimited (word)
LAMSUBG_W	LAMKO	LOK	Lambda nominal unlimited (word)
LAMS_W	LAMKO	LOK	Lambda nominal (word)
LAMVOA2_W	LAMKO	AUS	lambda pilot control without additive parts
LAMVOA_W	LAMKO	AUS	lambda pilot control without additive parts
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_ATR	PROKON	EIN	system constant exhaust-gas temperatur controller built in
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TMOT	SWADAP	EIN	Engine temperature

### FW LAMKO 3.120 Fixed Values

Parameter	Value	Description
LAMLGF		lambda limit "rich"
LASOAB		target lambda value for bank shutdown

## FB LAMKO 3.120 Detailed description of function

Lambda = 1.0 is set in the combustion chamber by the precontrol of the injection ESVST.  
The function Lambda coordination LAMKO defines that operating point of the engine at which the engine is run at combustion chamber Lambda # 1.0.  
The position of the switches is a dimension for the selection priority of lambda.  
The priorities of lambda selection are catalyst protection, component protection, catalyst heating by secondary air.  
Lambda for catalyst protection is LASOAB.  
Component protection for manifold, exhaust valves, supercharger, catalyzer is realized by means of the two inputs lambts\_w and dlambts\_w.  
By this, lambts\_w is an intervention for an absolute Lambda, to which other protection interventions can be added.  
lambts\_w is thereby influenced by the protection for engine and exhaust manifold (full-load enrichment for engine protection), turbine protection for supercharger.  
dlambts\_w is included as an additive component in the computation for knock-protection injection, catalyst overheating prevention.  
For projects with exhaust emission temperature control by exhaust emission sensors, the control correction is included in the computation by the additive component dlamatr\_w.  
From post-start until end of warm up of the engine lamnswl\_w is active, if there is no katalyst heating.

The transition is made at the beginning of catalyzer heating from Lambda post-start/warm up (lamnswl\_w) by means of the factor flakh from %LAKH to Lambda for catalyzer heating lamnswl\_w. Return to lamnswl\_w is made by means of flakh for an abort of the catalyzer heating. For systems with secondary air injection (B\_slsfz), the nominal lambda given at the Lambda sensor lamsons\_w is calculated from the Lambda engine (lamsbg\_w) by dilution of the secondary air by multiplication with the auxiliary air dilution factor flamsl\_w.  
The Lambda requirements is given by the fixed value LASOB for injection valve cut off (B\_evab, Bevab2 = true). It can realized by this, that there is no excess HC occuring in the corresponding exhaust emission train for cylinders which have been cut off if the entire bank is operated at "lean", e.g. with LASOAB = 1.05.

The average value from both banks is provided as the basic Lambda lambas for calculation of the engine torque.  
If there is no further need for higher Lambda dynamics outside of the warm up, catalyzer heating range (B\_lamnswle = true), then a switchover is made from the 10 ms to the 100 ms computation frame.  
The lambda set by the driver request, engine protection or catalyzer heating is limited by both of the Lambda thresholds for the engine-running limit "rich" (lalgf\_w) and "lean" (lalgm\_w).

## APP LAMKO 3.120 Application hint

Initialisation Parameters for Applikation:

LASOAB = 1.05

LAMLGF = 0.77

LAMLGTM: tmot interpolation points are the same one as the tmot points in function ESWL.

values of LAMLGTM = 1.2

The inputs lamka\_w, lamka2\_w are inactive if its value is >= 2.0. The Function katalyst purge set this value to 8.0 if there is no activity.

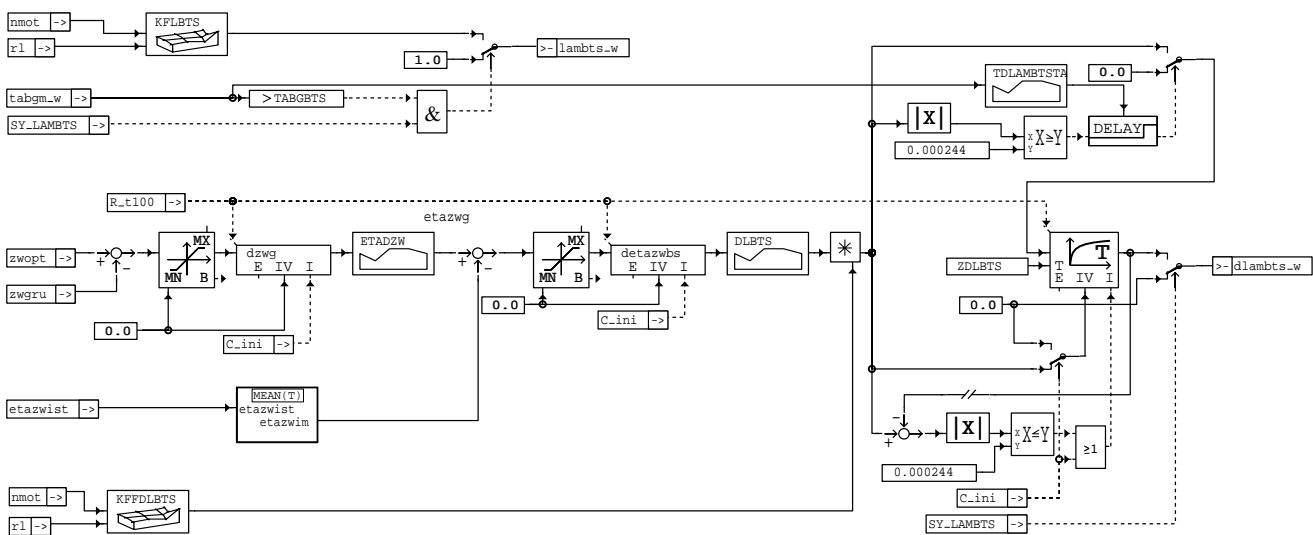
Outside warm-up and catalyzer heating, at reduced lambda dynamic requirement (B\_lamnswle = true), the calculation timing is switched from 10 ms to 100 ms.

## LAMBTS 1.60 Lambda component protection

### FDEF LAMBTS 1.60 Function definition

LAMBTS: Overview

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lambts-lambts

lambts-lambts



## ABK LAMBTS 1.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DLBTS	DETAZWBS		KL	Delta nominal Lambda for component protection
ETADZW	DZWG		KL	ignition efficiency depending on delta ignition angle
KFFDLBTS	NMOT	RL	KF	Factor delta nominal Lambda for component protection
KFLBTS	NMOT	RL	KF	Nominal Lambda for component protection
TABGBTS			FW	Exhaust temperature threshold for component protection
TDLAMBTSTA	TABGM_W		KL	delay time to enable nominal Lambda component protection
ZDLBTS			FW	Time constant delta lambda component protection

Variable	Source	Type	Description
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DETAZWBS	LAMBTS	LOK	Delta ignition angle efficiency for component protection
DLAMBTS_W	LAMBTS	AUS	delta lambda for component protection
DZWG	LAMBTS	LOK	Delta ignition timing, basis ZW to optimum ZW
ETAZWG	LAMBTS	LOK	Efficiency at basic ignition angle
ETAZWIM	LAMBTS	LOK	Mean efficiency at actual ignition angle
ETAZWIST	MDIST	EIN	actual ignition angle effectiveness
LAMBTS_W	LAMBTS	AUS	lambda for component protection
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_LAMBTS	PROKON	EIN	system constant component protection present
TABGM_W	ATM	EIN	Exhaust gas temperature in front of the catalyzer from model (Word)
ZWGRU	ZWGRU	EIN	basic ignition angle
ZWOPT	MSF	EIN	optimal ignition angle

## FW LAMBTS 1.60 Fixed Values

Parameter	Value	Description
TABGBTS		Exhaust temperature threshold for component protection
ZDLBTS		Time constant delta lambda component protection

## FB LAMBTS 1.60 Detailed description of function

Task:  
=====  
Protection of components (manifold, supercharger etc.) by mixture enrichment.

Principle:  
=====  
An exhaust emission temperature which is too high can be lowered by an enrichment of the air-fuel mixture. By this enrichment, more fuel reaches the cylinder than would be required for a stoichiometric combustion of the fuel. The fuel not burned vaporizes at the cylinder walls and thereby cools these down whereby the exhaust emission temperature also drops.

LAMBTS: Overview  
=====  
By means of the mapping KFLBTS, a lambda nominal shift towards rich can be performed as a function of the speed nmot and the cylinder fill rl.  
The enrichment is active only, if the modeled exhaust temperature exceeds the applicable threshold TABGBTS.  
  
An increase in the exhaust emission temperature can occur for a deterioration in the ignition-timing efficiency. This increase can be counteracted by an enrichment of the mixture.  
In addition to this, the ignition-timing efficiency etazwg is calculated for the basic timing zwgru and the ignition-timing efficiency etazwim for the averaged actual ignition timing.  
The difference between etazwg and etazwim gives the deterioration in the efficiency detazwbs. Depending on detazwbs, a additive enrichment can now be performed by means of the characteristic DLBTS. The enrichment can be reduced or shut off in desired regions by the mapping KFFDLBTS (nmot, rl). The efficiency of the enrichment can be filtered by the PT1-Block.

MEAN: Calculation mean value of efficiency at actual ignition angle  
=====  
Here the mean value of the ignition angle efficiencies (10ms-frame) is calculated over one 100ms-frame.

**APP LAMBTS 1.60 Application hint**

## Prerequisites:

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- \* Application of basic ignition angle (see %ZWGRU)
- \* Stationary lambda-application
- \* Application of exhaust gas temperature model (%ATM)

## Pre-assignment of the parameters:

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Shutoff of enrichment by nominal lambda value: KFLBTS = 1.0 (all nmot, all rl)  
Critical exhaust temperature: TABGBTS = 900 °C  
Shutoff of enrichment by delta nominal lambda value: DLBTS = 0.0 (all detazwbs)  
Deactivate low pass for delta enrichment: ZDLBTS = 0.2 s  
Neutralize weighting factor for delta nominal lambda value: KFFDLBTS = 1.0 (all nmot, all rl)

## Method of proceeding:

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## 1.) Application of general enrichment

-----

First set low threshold for enrichment: TABGBTS = -50 grad C. Measure modeled exhaust temperature tabgm for later application of TABGBTS at every operation point of the following maps.

The Application of the map KFLBTS must be done at basic ignition angle. For this use the following data:

- \* Neutralize warm up ignition angle shift: KFZWLLNM = KFZWLLTM = 0
- \* Switch off knock control: TMKR > tmot
- \* Disable shift of ignition angle by application constant: ZWAPPL = 0
- \* Set condition ignition angle application without torque control (B\_zwappl): CWMDAPP[Bit0] = 1

At application of the map KFLBTS the exhaust gas temperature must be measured at every operation point and must be limited by enrichment (KFLBTS values < 1) to an uncritical value.

The exhaust temperature threshold for enrichment TABGBTS must be set to the value at which an enrichment was necessary.

## 2.) Application of enrichment at shift of ignition angle

-----

At application of the time constant ZDLBTS steps of ignition angle must be done without delta-enrichment (with ZWAPPL):

- \* Make a step of ignition angle and measure the exhaust gas temperature
- \* Verify time constant and write it in ZDLBTS

## Application of enrichment characteristic DLBTS:

- \* Operate engine at the operation point where the highest general enrichment was necessary
  - \* Adjust ignition angle by ZWAPPL in direction "late" and enrich by DLBTS, if the exhaust gas temperature is too high
- The characteristic DLBTS should stay constant for further application.

The map KFFDLBTS must be applied at maximum ignition angle shift in direction late (by ZWAPPL):

- \* Operate engine at every operation point of KFFDLBTS and measure exhaust gas temperature. Reduce or switch off enrichment if necessary.

## Functions influenced:

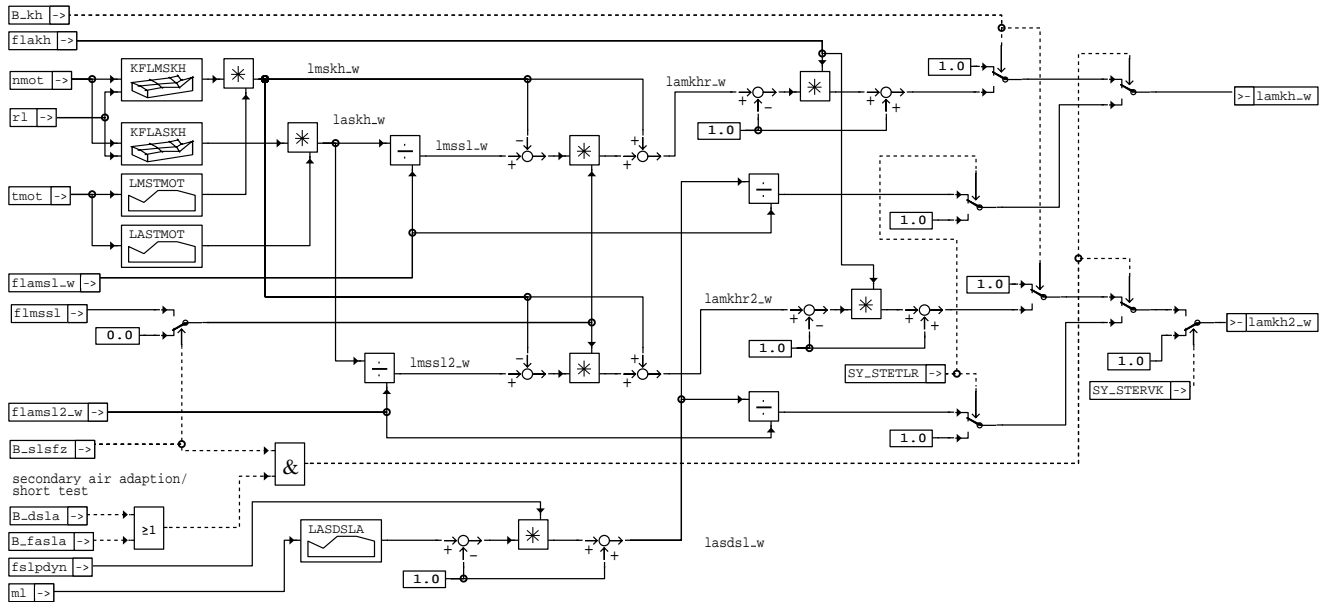
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%LAMKO by lambts\_w, dlambts\_w



## LAKH 2.30 Lambda coordination for catalyst heating

### FDEF LAKH 2.30 Function definition



lakh-lakh

### ABK LAKH 2.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFLASKH	NMOT	RL	KF	Performance characteristics lambda exhaust nominal at catalyst heating
KFLMSKH	NMOT	RL	KF	Performance characteristics lambda engine nominal at catalyst heating
LASDSLW	ML		KL	Lambda exhaust nominal at secondary air adaption/short test
LASTMOT	TMOT		KL	tmot-correction of lambda exhaust nominal
LMSTMOT	TMOT		KL	tmot-correction of lambda engine nominal
Variable	Source		Type	Description
B_DSLA			EIN	adaption phase: calculation of secondary air mass
B_FASLA			EIN	Condition: external request of SAI system aktiv
B_KH	BBKHZ		EIN	condition catalyst heating activated
B_SLSFZ	PROKON		EIN	condition: SLS fitted in vehicle
FLAKH	BBKHZ		EIN	Factor control lambda at catalyst heating
FLAMSL2_W			EIN	Factor lambda change by secondary air, bank 2
FLAMSL_W			EIN	Factor lambda change by secondary air
FLMSSL			EIN	Factor lambda engine by secondary air
FSLPDYN			EIN	Factor dynamic behavior secondary air pump
LAMKH2_W	LAKH		AUS	Lambda engine nominal at catalyst heating, bank 2 (word)
LAMKHR2_W	LAKH		LOK	Lambda engine result at catalyst heating, bank 2 (word)
LAMKHR_W	LAKH		LOK	Lambda engine result at catalyst heating (word)
LAMKH_W	LAKH		AUS	Lambda engine nominal at catalyst heating (word)
LASDSL_W	LAKH		LOK	Lambda exhaust nominal at secondary air diagnosis
LASKH_W	LAKH		LOK	Lambda exhaust nominal at catalyst heating (word)
LMSKH_W	LAKH		LOK	Lambda engine nominal at catalyst heating (word)
LMSSL2_W	LAKH		LOK	Lambda engine nominal caused by secondary air, bank 2
LMSSL_W	LAKH		LOK	Lambda engine nominal caused by secondary air (word)
ML	SWADAP		EIN	air mass flow
NMOT	SWADAP		EIN	engine speed
RL	SWADAP		EIN	relative air charge
SY_STERVK	PROKON		EIN	system constant condition: stereo exhaust system upstream of cat
SY_STETLR	PROKON		EIN	System constant condition continuous Lambda control present
TMOT	SWADAP		EIN	Engine temperature

### FW LAKH 2.30 Fixed Values

Parameter	Value	Description
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## FB LAKH 2.30 Detailed description of function

For exhaust gas reasons the engine is operated after cold start in such a way that an accelerated catalyst warm-up takes place. The quantity of heat necessary for this can be mainly supplied by thermal exhaust gas energy (exhaust gas temperature, exhaust gas mass flow), during which the engine must be operated as lean as possible, in order to minimize the raw emissions ("lean warm-up"). A further possible catalyst heating source uses thermal exhaust gas energy ("rich warm-up"). For this, the engine is operated with an excess of fuel. In combination with secondary air the rich exhaust gas reacts inside the manifold or inside the catalyst. The heat produced by this oxidation process is used for the heating of the catalyst.

An excess of air in the exhaust gas is necessary for both catalyst heating concepts.

For concepts with lean warm-up the lean Lambda engine set point  $lmskh$  (due to  $flmssl = 0$ ) from the characteristic map  $KFLMSKH$  is preassigned and made available as Lambda set point  $lamkh$ . The "control" is performed by the evaluation to  $\Lambda = 1$  by  $flakh$  from  $\%BBKHZ$ . In the Lambda coordination  $\%LAMKO$  the transition from  $lamnswl$  (Lambda after-start warm-up) to  $lamkh$  and the limitation to the actual Lambda combustion chamber  $lamsbg$  is performed by the evaluation factor  $flamkh$  from  $\%BBKHZ$ . In addition the Lambda set point  $lamsons$  for the Lambda control is calculated.

For concepts with secondary air injection ( $B\_slsfz = 1$ , code word  $CWKONABG$  from  $\%PROKON$ ) the setpoint for Lambda engine is determined for  $flmssl = 0.9961$  from the setpoint for Lambda exhaust gas  $laskh$  by the relation of  $lmssl = laskh / flamsl$  with the secondary air dilution factor  $flamsl = (1 + msl / ml)$  from  $\%SLS$ .

By the weight factor  $flmssl$  from the secondary air control  $\%SLS$  the resulting Lambda setpoint  $lamkhr$  is then obtained from:

$$lamkhr = lmskh + flmssl * (lmssl - lmskh).$$

Here  $flmssl = 0$  - in spite of secondary air - complies to the setpoint input for Lambda engine of a concept with lean warm-up. The limit  $flmssl = 0.9961$  then complies to the setpoint default selection with thermal reaction in combination with secondary air. The default selection of  $fmssl$  takes place in the secondary air control  $\%SLS$ .

The setpoint for Lambda catalyst heating  $lamkhr$  resulting from this, also evaluated by  $flakh$ , is controlled by  $flamkh$  in  $\%LAMKO$  and is made available as actual Lambda combustion chamber  $lamsbg$ . In  $\%LAMKO$  the correspondent Lambda setpoint  $lamsons$  for the Lambda control is calculated by:

$$lamsons = lamsbg * flamsl.$$

Both catalyst heating concepts ("lean warm-up", "secondary air injection") have in common, that the starting procedure must be performed with minimum raw emissions and minimum exhaust gas mass flow, that means idling of the engine must be adjusted such that maximum heat is produced in the exhaust pipe, whilst the starting procedure must take place at the lean warm-up limit with an ignition angle of optimum efficiency. As a result, the Lambda in the engine is defined by the lean limit "lalgm" from  $\%ESWL$ , especially at start of driving. For concepts with a large excess of secondary air during idling Lambda engine is additionally determined by the rich limit  $lalgf$  from  $\%WL$ . For this also see  $\%LAMKO$ .

### Secondary air adaptation/quick test:

For the secondary air diagnosis ( $\%DLSLR$  or  $\%DSLRLRS$ ) it is possible to again activate the secondary air by  $B\_dsla$  or also by the quick test request  $B\_fasla$ . The Lambda input selection is performed dependent on the secondary air diagnosis, based on the used Lambda control:

Two-state controller -> secondary air diagnosis  $\%DSLRLR$ :

Control to Lambda exhaust gas = 1 with input selection of the necessary engine enrichment due to the secondary air dilution factor  $flamsl_w$ .

At engine operation points, at which a too rich engine operation would be reached due to the little intake air mass, the Lambda exhaust gas input selection  $lasdsl_w$  can be corrected in the direction lean depending on the intake air mass. An adaptation of the secondary air mass then, however, is no longer possible due to  $lamsons_w$ , since the "measuring window" has been left. (Regarding this see  $\%DSLRLR$ .)

Continuous Lambda control -> secondary air diagnosis  $\%DSLRLRS$ :

Input selection of Lambda engine = 1 and calculation of the desired Lambda exhaust gas ( $lamsons_w$ ) from the secondary air dilution factor. In case of quicktrip request ( $B\_fasla$ ) the diagnosis is performed in combination with active control analogous to the secondary air diagnosis during catalyst heating. During the adaptation phase ( $B\_dsla$ ) the secondary air diagnosis in comparison is performed by measuring and evaluating the Lambda sensor voltage  $lamsoni_w$  at controlled operation. (Regarding this see  $\%DSLRLRS$ .)





## APP LAKH 2.30 Application hint

Precondition: Application mixture check (%GK), injection pilot control (%ESVST), secondary air control (%SLS), Application %WL in combination with catalyst heating.

### Default selection:

By the bit B\_slsfz from CWKONABG the catalyst heating concept without / with secondary air system becomes compatible:

B\_slsfz = | 0: no secondary air system, lean catalyst heating operation of the engine  
| 1: with secondary air system, rich catalyst heating operation of the engine  
Further possible secondary air variations are described in %SLS.

Lean warm-up: Default selection KFLMSKH with 1,05, transition to 1,0 resp. richer dependent on load (rl) when starting from rest and adjustment to the lean performance limit (lalgm) from %ESWL, as described in %LAMKO.

Rich warm-up : Default selection KFLASKH with 1,1 to 1,2, transition to > 1,3 when starting from rest and adjustment to the lean performance limit (lalgm) from %ESWL, as described in %LAMKO. Also see %BBKHZ.

or Lambda engine default selection by code word CWSLS in %SLS analogues to lean warm-up.

The base point distribution of KFLMSKH, KFLASKH is to be chosen such that the "catalyst heating idle range" is sufficiently covered with regard to engine speed and load at idle and that a steady transition by interpolation to partial load can be performed.

Default selection in %ESWL such that "lalgm" does not limit lalgf during catalyst heating.

### Switching off:

No catalyst heating with MLSUS = 0 in %BBKHZ

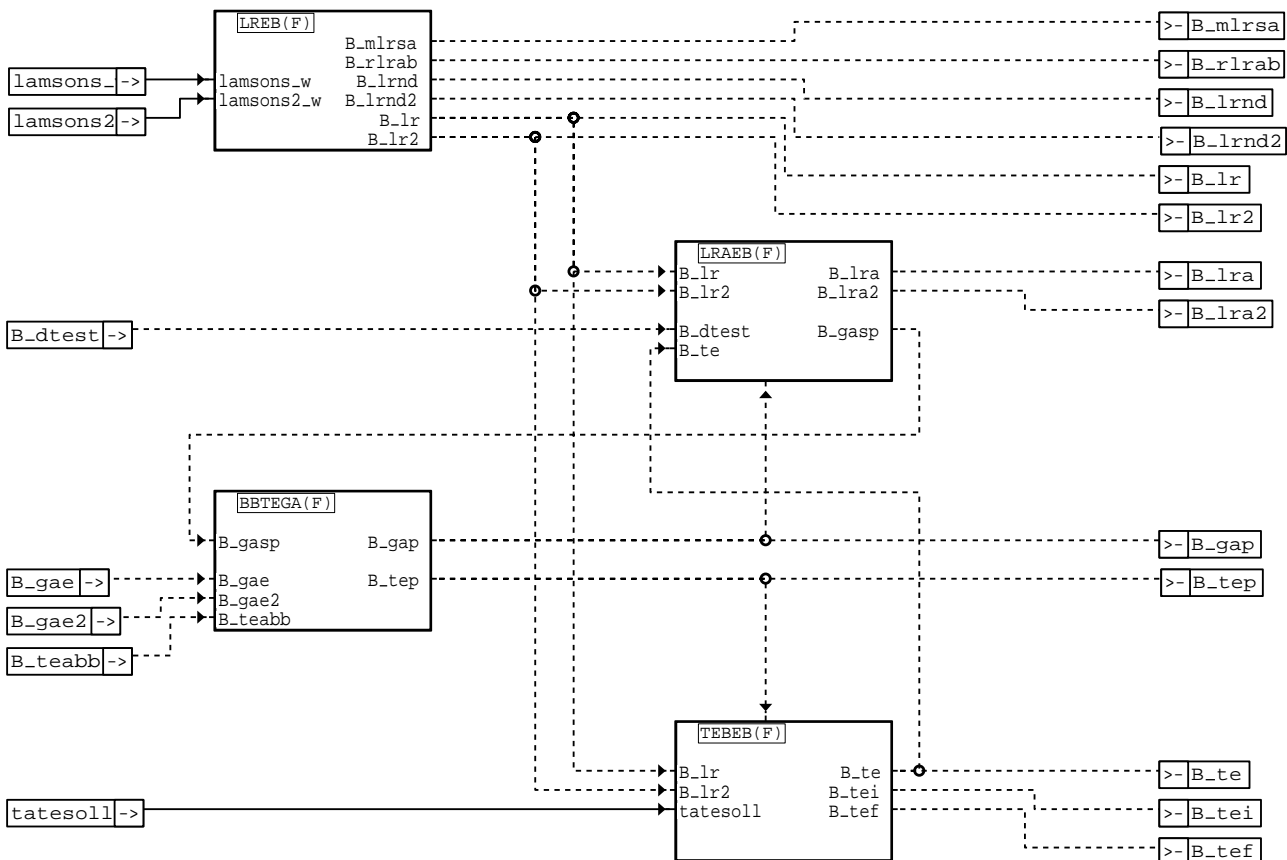
No Lambda action during lean warm-up: KFLMSKH = 1

with secondary air: MSLUB = 0 in %SLS and KFLASKH = 1.0

## GKEB 3.0 Operating condition mixture control overview

### FDEF GKEB 3.0 Function definition

Mixture Control, Adaptation - Activation Conditions:



gkeb-gkeb

gkeb-gkeb



## ABK GKEB 3.0 Abbreviations

Variable	Source	Type	Description
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_GAE	DKVS	EIN	condition for adaptive Lambda pilot control successful
B_GAE2		EIN	condition for adaptive lambda pilot control 2 successful
B_GAP	GKEB	AUS	condition mixture adaptation phase active
B_GASP	GKEB	LOK	condition for basic mixture adaptation disabled
B_LR	GKEB	AUS	LRB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	GKEB	AUS	LRB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRA	GKEB	AUS	condition for basic mixture adaptation enabled
B_LRA2	GKEB	AUS	condition for basic mixture adaption 2 enabled
B_LRND	GKEB	AUS	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_LRND2	GKEB	AUS	set control bit LR activ; request for "NORMAL" or "DIAGNOSIS"
B_MLRSA	GKEB	AUS	LRSEB: Air mass based switch off Lambda Control during and after fuel cut off
B_RLRAB	GKEB	AUS	condition LR off due to high load
B_TE	GKEB	AUS	Condition canister purge active
B_TEABB	TEB	EIN	Condition purge canister function ready to finish
B_TEF	GKEB	AUS	Condition canister purge function principally released
B_TEI	GKEB	AUS	Internal condition: canister purge function active
B_TEP	GKEB	AUS	Condition canister purge phase active
LAMSONS2_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
TATESOLL	GKRA	EIN	desired duty cycle of the PCV

## FW GKEB 3.0 Fixed Values

Parameter	Value	Description
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## FB GKEB 3.0 Detailed description of function

Functional group, mixture control, switch-on conditions (%GKEB)

Only for 2-point lambda control !!!!!!!

This functional group includes the following functions:

- %LREB - Switch-on conditions for 2-point lambda control
- %LRAEB - Switch-on conditions for mixture adaptation
- %TEBEB - Switch-on conditions for the loading-dependent tank venting
- %BBTEGA - Phase control tank venting / mixture adaptation  
(The term "phase control" designates a device which actuates the change between a mixture adaptation phase and a tank venting phase)

Remark: the switch-on conditions for the control after the catalyzer are described in the function "Control after the catalyzer" and not in %LREB.

- %LREB - Switch-on conditions for 2-point lambda control
  - A number of conditions must be fulfilled for activation of the lambda control.
  - The lambda control must remain disabled (B\_lr = FALSE) in particular for OBDII faults which have a strong influence on the mixture at the probe
  - Specific conditions must also be fulfilled however. The most important of these are, e.g.
    - B\_sbbvk (readiness for operation by the probe in front of the catalyzer)
    - B\_evloc (all EV's triggered)
- %LRAEB - Switch-on conditions for mixture adaptation
  - The mixture adaptation has specific switch-on conditions. A number of OBDII faults thereby disable the mixture adaptation.
  - A prerequisite for activation of the mixture adaptation is B\_lr
  - The mixture adaptation is furthermore only then activated when there is no tank venting active (B\_gap = 1)
- %TEBEB - Switch-on conditions for the loading-dependent tank venting
  - The tank venting valve is opened during a tank venting phase (B\_tep)
  - Furthermore, certain conditions must be fulfilled in order that the tank venting can be activated. (e.g. engine temp. > threshold). The TEV can only be opened if the bit B\_tef (condition for release of tank venting) is TRUE.
  - Furthermore, it is differentiated between controlled tank venting (e.g. the probe is defective) and regulated tank venting. A regulated tank venting (loading-dependent) is only activated for B\_tei. To the extent that B\_tef = TRUE, the TEV can also be opened for B\_tei = FALSE by controlled performance characteristics (emergency run TE).
  - The bit B\_te indicates that the TEV is still opened for "normal TEB" (regulated TE). B\_te is only the reset if the TEV is completely closed, e.g. following a TE phase.
- %BBTEGA - Phase control tank venting / mixture adaptation
 

The phase control brings about the change mixture adaptation / tank venting and shall meet OBDII requirements in particular. Hence switchover to long tank venting phase is only then made after an established mixture adaptation (B\_gae = TRUE). Tank venting can be terminated intentionally by means of a customer servicing tester and the mixture adaptation activated for diagnosis purposes.

## APP GKEB 3.0 Application hint

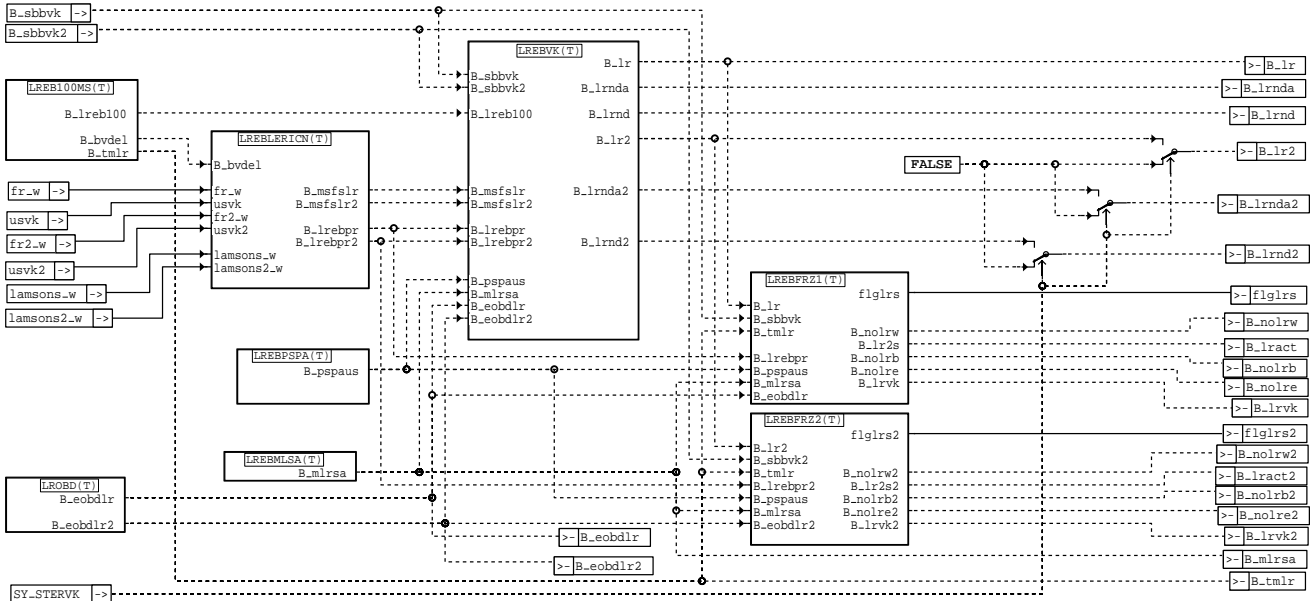
Not applicable here as all parameters are described in the appropriate functions.

## LREB 141.10 Activation conditions for lambda closed loop control

### FDEF LREB 141.10 Function definition

LREB: Switch-on conditions Lambda control upstream catalyst total overview

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### Ireb-Ireb

B\_lr shows for all sections, which evaluate this bit, the state of the Lambda control (B\_lr = TRUE means Lambda control is active).

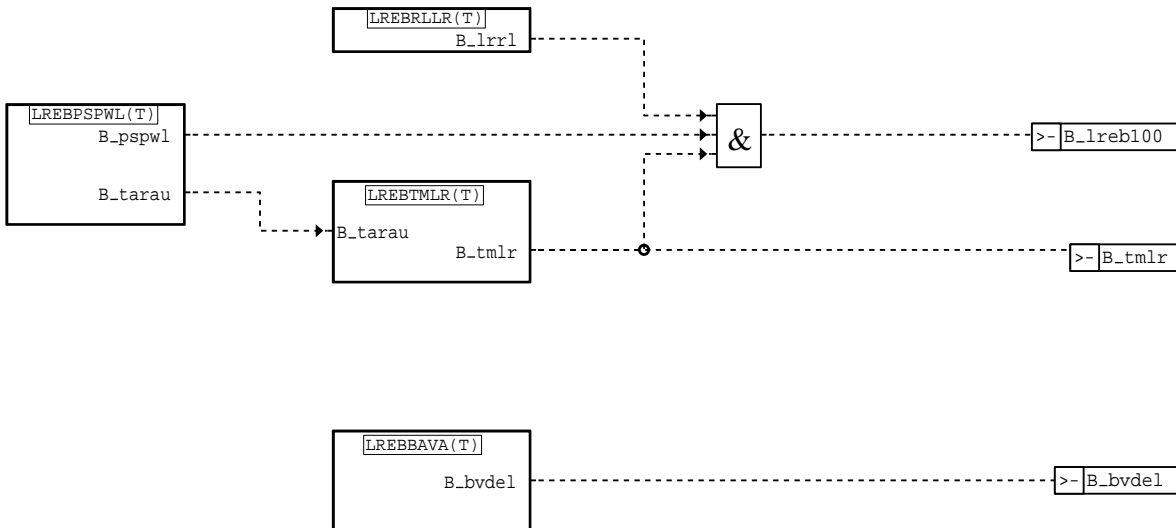
B\_lrnd is activated in addition to B\_lr as soon as the Lambda control is necessary e.g. for diagnostic purposes, the controller factor fr\_w, however, would lie in not plausible ranges or in case a lean engine operation is to be prevented for lamsons < 1 or a rich engine operation is to be prevented for lamsons > 1.

This is ensured by two paths during the formation of B\_lr and B\_lrnd:

- For lamsons <> 1 B\_lr is set to FALSE, lean/rich protection is activated by B\_lrnd = TRUE.
- LC is blocked during SLS/DSLS, with lamsons >1 rich protection is activated if necessary
- By B\_vag = TRUE OR B\_bag = TRUE (from UKSEFI) B\_lr is set to FALSE for an adjustable time. Lean protection is activated via B\_lrnd = TRUE if necessary.

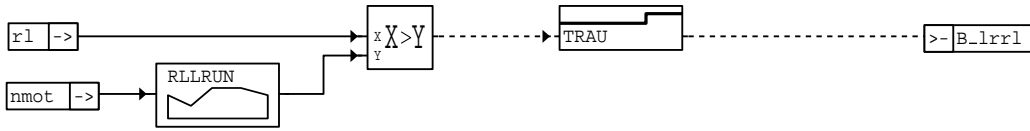
LREB100MS: Switch-on conditions for control upstream catalyst determined in the 100 ms cycle

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### Ireb-Ireb100ms

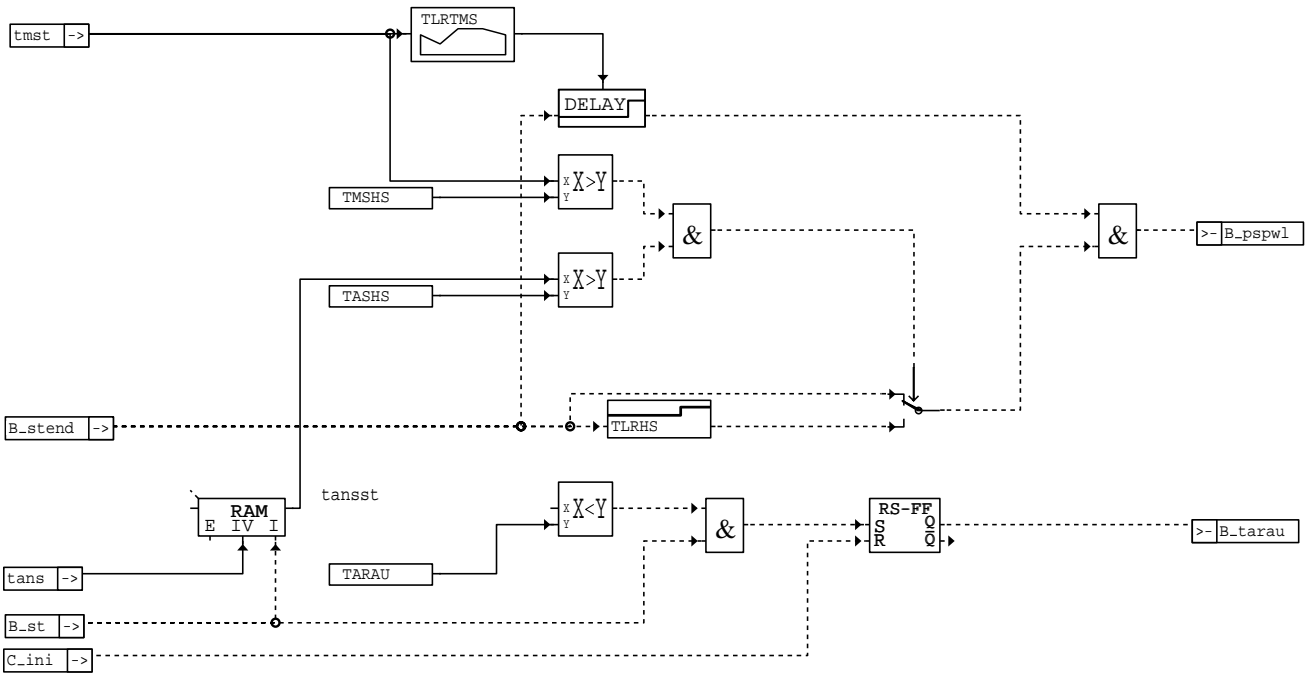
**LREBRLLR: Evaluation of load threshold**  
=====



ireb-irebrlr

**ireb-irebrlr**

**LREBPSPWL: Warm-up specific switch-on conditions for control upstream catalyst**  
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ireb-irebpswl

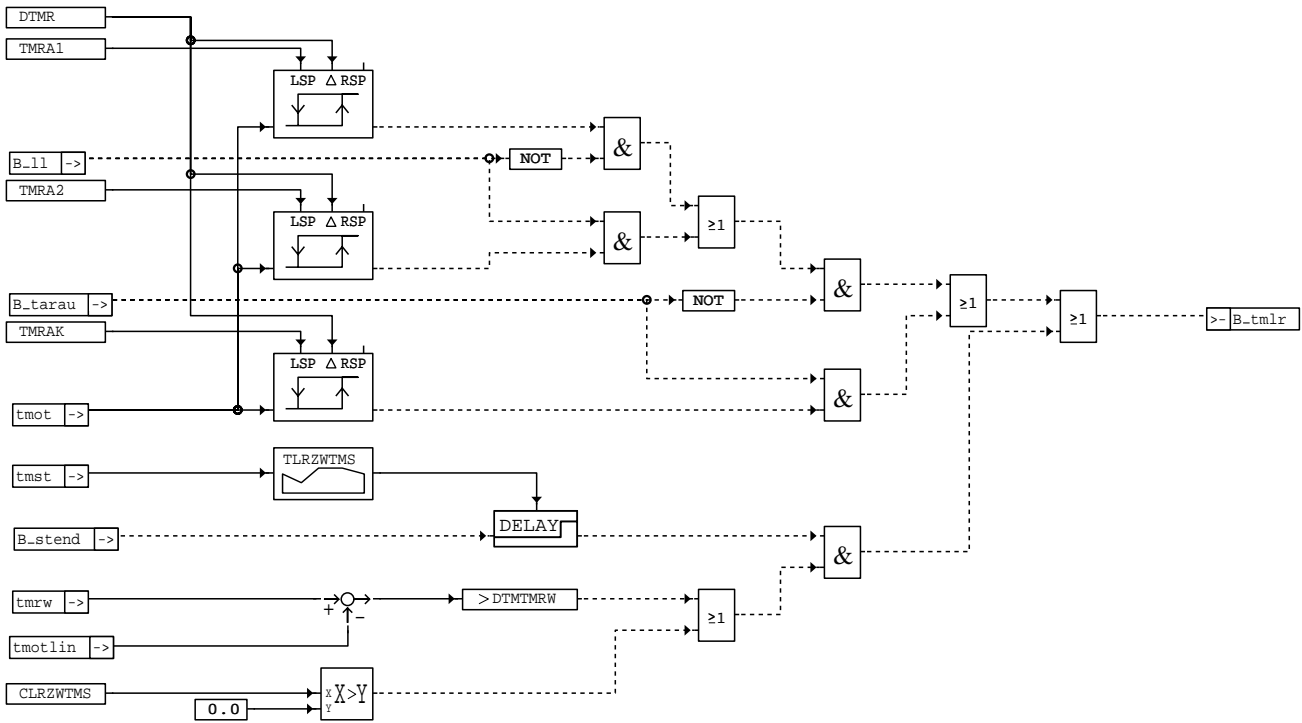
**ireb-irebpswl**

Switch-on / switch-off: - If the hot start condition  $tmst > TMSHS$  and  $tansst > TASHS$  is fulfilled during start, the delay time  $TLRHS$  is set.  $TLRHS$  runs as of end of start and accordingly delays the start of the Lambda control upstream catalyst.

Via the local bit  $B\_tarau$  it is possible to alternatively define another temperature threshold for the switch-on of the Lambda control. This may e.g. be necessary on systems with an evaluation of the intake air temperature.

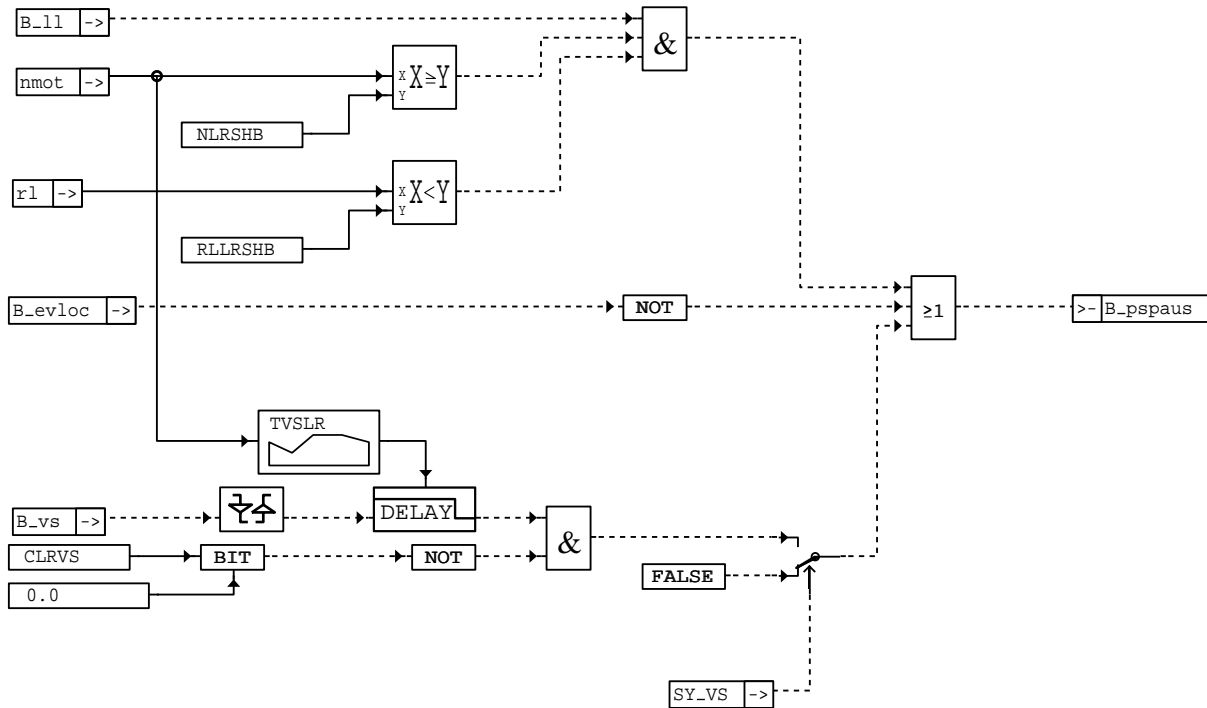


### LREBTMLR: TMOT- and TANS-dependent switch-on conditions for control upstream catalyst



### Ireb-irebtmlr

### LREBPSPA: Project-specific switch-off conditions for control upstream catalyst



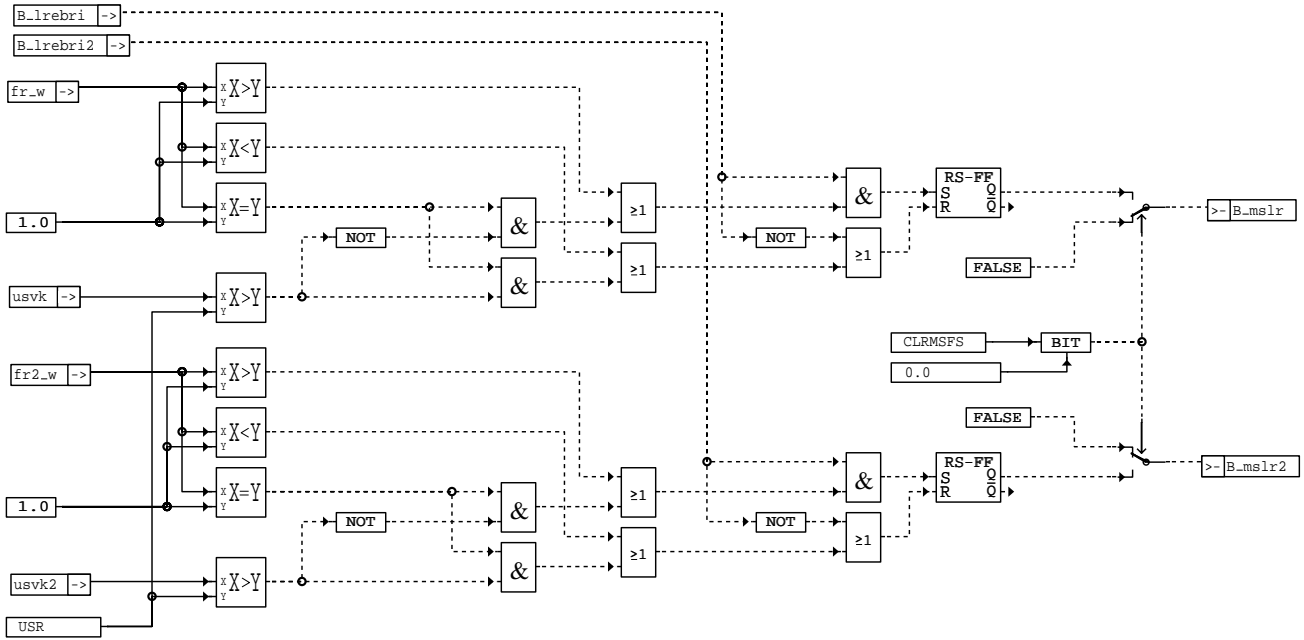
### Ireb-irebpspa





### LREBLEANPR: Subfunction lean protection

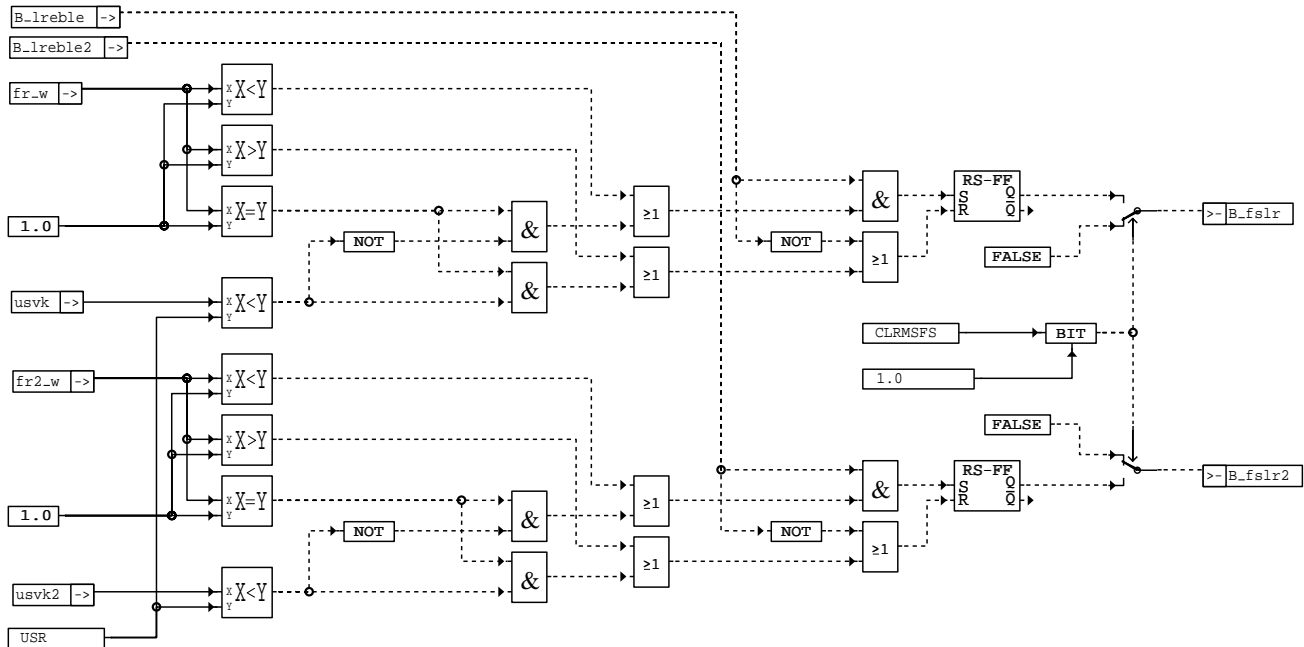
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### ireb-irebleanpr

### LREBRICHPR: Subfunction rich protection

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### ireb-irebrichpr

Conditions for lean / rich protection  
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The lean protection monitoring is activated by lamsons\_w < 1.

The lean protection function is triggered by the condition

$$((\text{usvk} = \text{"lean"}) \text{ AND } (\text{fr\_w} = 1)) \text{ OR } (\text{fr\_w} > 1)$$

The lean protection function is reset by the condition

$$((\text{usvk} = \text{"rich"}) \text{ AND } (\text{fr\_w} = 1))$$

$$((\text{B\_mslr} = \text{TRUE} \text{ \& } \text{blocking conditions} = \text{FALSE}) \text{ ---} \rightarrow \text{B\_lrnd} = \text{TRUE} \text{ and } \text{B\_lr} = \text{FALSE})$$

The rich protection monitoring is activated by lamsons\_w > 1.

The rich protection function is triggered by the condition

$$((\text{usvk} = \text{"rich"}) \text{ AND } (\text{fr\_w} = 1)) \text{ OR } (\text{fr\_w} < 1)$$

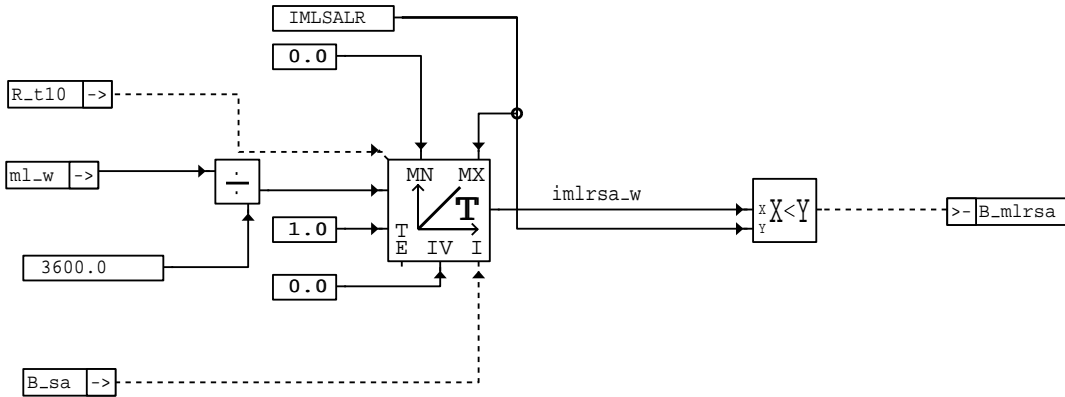
The rich protection function is reset by the condition

$$((\text{usvk} = \text{"lean"}) \text{ AND } (\text{fr\_w} = 1))$$

$$((\text{B\_fslr} = \text{TRUE} \text{ \& } \text{blocking conditions} = \text{FALSE}) \text{ ---} \rightarrow \text{B\_lrnd} = \text{TRUE} \text{ and } \text{B\_lr} = \text{FALSE})$$

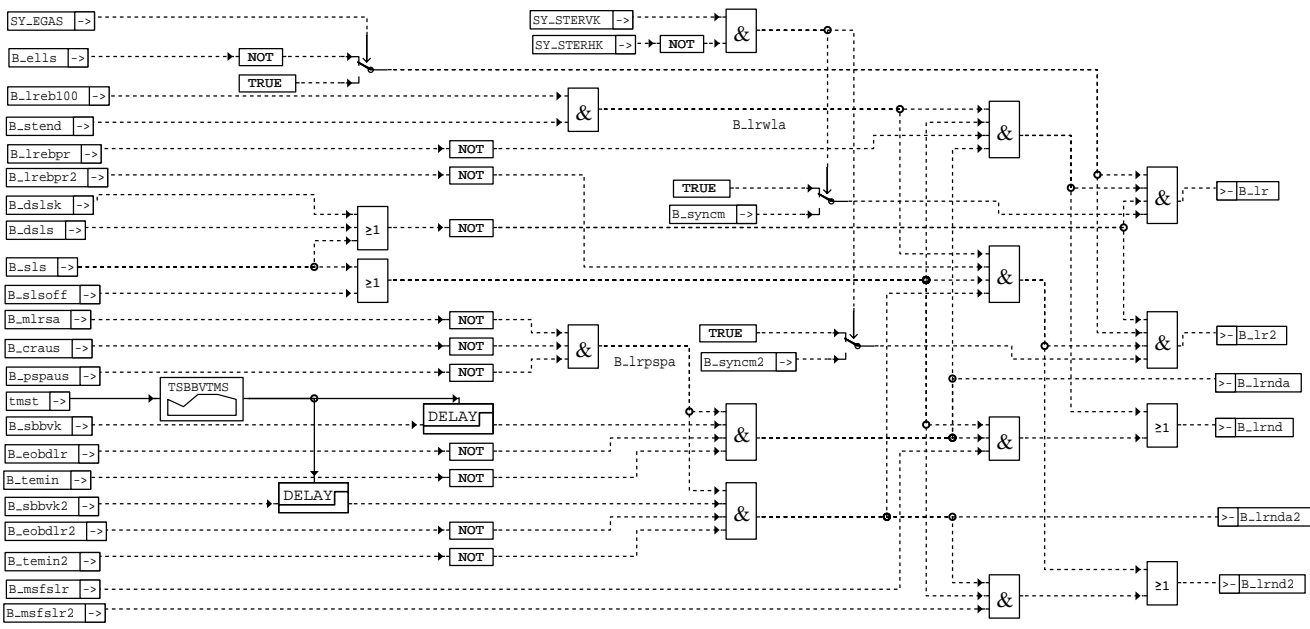
The lean protection monitoring is activated by lamsons\_w < 1.

LREBMLSA: Checking on air mass integral after fuel cut-off on overrun  
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**ireb-irebmlsa**

LREBVK: Formation of the bits B\_lr and B\_lrnd  
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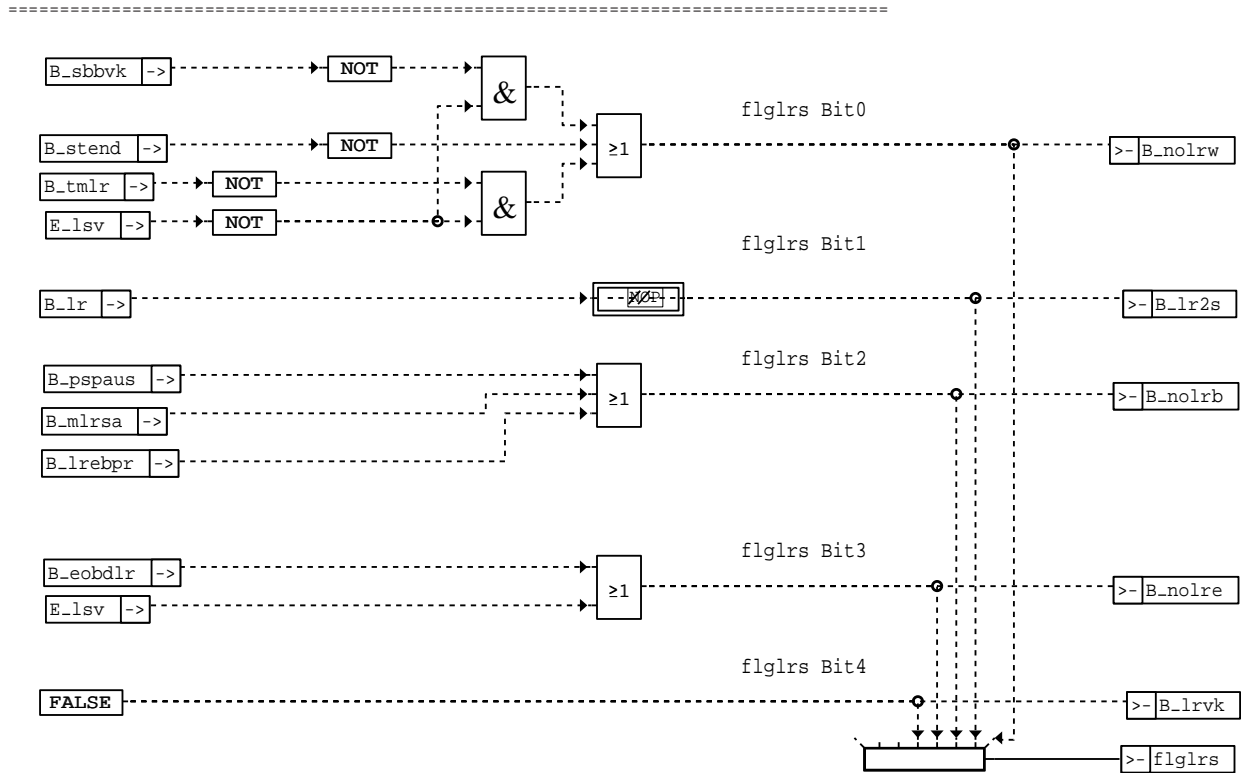


**ireb-irebvk**



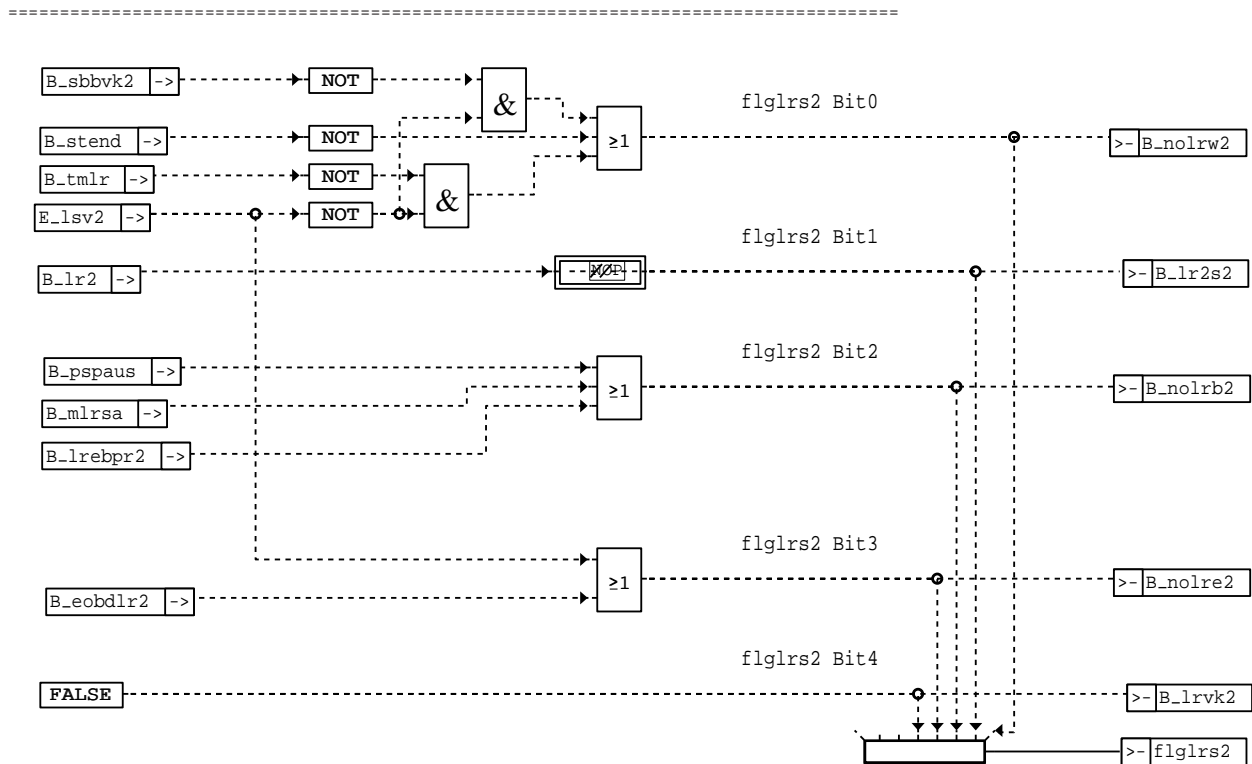


LREBFRZ1: CARB Freeze Frame - status byte of the LC, at stereo LC for bank 1 (flglrs)



### ireb-irebfrz1

LREBFRZ2: CARB Freeze Frame - status byte of the LC, at stereo LC for bank 2 (flglrs2)



### ireb-irebfrz2

Remark: The bits should be checked upon in above-mentioned order. If one of the bits Bit0, Bit1, Bit2 or Bit3 is set to TRUE, no further checking is to be performed. By the thus given priority of the evaluation it is ensured that 2 bits cannot be set simultaneously in the freeze frame byte.



## ABK LREB 141.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CLRMSFS			FW	code word for lambda closed-loop control lean/rich protection on/off
CLRVS			FW	code word for lambda closed-loop control on/off at changing of valve stroke
CLRZWTMS			FW	Codeword for hard activation of LR according to CARB
DTMR			FW	hysteresis for cut-in threshold
DTMTMRW			FW	temperature difference thresh. for detection of hard LC-switch on
IMLSALR			FW	thresh.value integr.air mass for activ.delay of lambda contr.after fuel cut-off
NLRSHB			FW	eng.speed thesh.,turn-off lamb.contr.during overrun,in connec.with idle a.TLLRSHB
RLLRSHB			FW	load thresh.,turn-off lambda contr.during sec. air,in connect.with idle a.NLRSHB
RLLRUN	NMOT		KL	char.line above nmot,lower rL control limit for controller in front of catalyst
RLRVAO			FW	Upper rI-threshold for trigger of LR stopped during transient VA
TARAU			FW	air temperature threshold for closed loop lambda - control switching on
TASHS			FW	threshold intake air temp.for trigg.of TLRHS-blocking time LC during hot start
TLRBAM	TMOT		KL	blocking time for activation LC after BA
TLRHS			FW	blocking time LC during hot start, triggered via thresholds TASHS and TMSHS
TLRTMS	TMST		KL	lock time for CL lambda control after start, depending on engine start temperatur
TLRVAM	TMOT		KL	blocking time for activation LC after VA
TLRZWTMS	TMST		KL	Time until hard LC switch on after start (CARB)
TMRA1			FW	cut-out condition (idle-speed switch = 0)
TMRA2			FW	cut-out condition (idle-speed switch = 1)
TMRAK			FW	cut-out threshold of lambda closed-loop control at low starting temperature
TMSHS			FW	threshold engine temp.for triggering of TLRHS-blocking time LC during hot start
TRAU			FW	monitoring time for lower load limit of lambda closed-loop control
TSBBVTMS	TMST		KL	time delay control readiness after sensor readiness
TVSLR	NMOT		KL	Duration of LRS downtime commanded via valve stroke control
USR			FW	controller theshold for lambda control upstream catalyst

Variable	Source	Type	Description
B_BAG	ESUK	EIN	Condition large accel. enrichment
B_BVDEL	LREB	LOK	OR-logic interconnection for the stop condition B_bag / B_vag
B_CRAUS		EIN	Tested by LREB: Workshop bit to stop LR
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DSLSK		EIN	COndition secondary air diagnosis short trip
B_EEV	DEVE	EIN	condition injector fault (power stage)
B_ELLS		EIN	Condition: error idle speed actuator
B_EOBDLR	LREB	AUS	error flag:OBDII summary fault, disables lambda control
B_EOBDLR2	LREB	AUS	error flag:OBDII summary fault, disables lambda control, bank 2
B_ESLS		EIN	Condition secondary air fault by wrong air mass flow
B_EVLOC	BGEVAB	EIN	Status: all injection valves are activated
B_FSLR	LREB	LOK	Condition LR activ/inactiv during rich open loop (lamsons_w < 1.0)
B_FSLR2	LREB	LOK	Condition LR activ/inactiv during rich open loop (lamsons_w < 1.0) bank 2
B_LL	MSF	EIN	Condition idle
B_LR	LREB	AUS	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	AUS	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LR2S	LREB	LOK	CARB freeze frame, cyl.row 1 bit 1, LR:closed loop operating with two sensors
B_LR2S2	LREB	LOK	CARB freeze frame, cyl.row 2 bit 1, LR:closed loop operating with two sensors
B_LRACT	LREB	AUS	CARB freeze frame, cyl.row 1 bit 1, LR:normal closed loop operation
B_LRACT2	LREB	AUS	CARB freeze frame, cyl.row 2 bit 1, LR:normal closed loop operation
B_LREB100	LREB	LOK	Collection bit of stop condition during a 100ms-slot
B_LREBLE	LREB	LOK	Condition LR inactiv during lean out and lambda sensor indicates "rich"
B_LREBLE2	LREB	LOK	Condition LR inactiv during lean out and lambda sensor indicats "rich" bank 2
B_LREBPR	LREB	LOK	Condition LR inactiv during enrichment and lambda sensor indicates "lean"
B_LREBPR2	LREB	LOK	Condition LR inactiv during enrichment and lambda sensor indicates "lean"
B_LREBRI	LREB	LOK	cond. lambda control inact. while open loop: lamsons_w < 1, B_vl, B_vag or B_bag
B_LREBRI2	LREB	LOK	cond. lambda control inact. while open loop: lamsons_w < 1, B_vl, B_vag or B_bag
B_LRND	LREB	AUS	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_LRND2	LREB	AUS	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_LRNDA	LREB	AUS	lambda control bank 1 active by conditions : B_Lrpspa & B_Lrksn & IE_obdlr
B_LRNDA2	LREB	AUS	lambda control bank 2 active by conditions : B_Lrpspa & B_Lrksn & IE_obdlr
B_LRPSPA	LREB	DOK	LREB: Project specific condition for lambda closed loop control upstream cat.
B_LRRL	LREB	LOK	LREB: Load dependend condition for lambda closed loop control upstream catalyst
B_LRVK	LREB	AUS	CARB freeze frame,cyl.row 1 bit 4,LR:closed loop contr. with one sensor (upstr.)
B_LRVK2	LREB	AUS	CARB freeze frame,cyl.row 2 bit 4,LR:closed loop contr. with one sensor (upstr.)
B_LRWLA	LREB	DOK	lambda control active by conditions : B_Lrll & B_tmlr & B_pspwl & B_stend
B_MDKAT	DMDMIL	EIN	cat. damaging misfire rate exceeded (for deactivation of other functions)
B_MLRSA	LREB	AUS	LRSEB: Air mass based switch off Lambda Control during and after fuel cut off
B_MSFSLR	LREB	LOK	Condition LR activ/ inactivduring rich/lean protection
B_MSFSLR2	LREB	LOK	Condition LR activ/ inactivduring rich/lean protection, bank 2
B_MSLR	LREB	LOK	Condition LR activ/inactiv during rich/lean protection
B_MSLR2	LREB	LOK	Condition LR activ/ inactiv during rich/lean protection
B_NOLRB	LREB	AUS	CARB freeze frame, cyl.row 1 bit 2, LR:open loop operating by operating condit.
B_NOLRB2	LREB	AUS	CARB FREEZE FRAME, bank2 Bit 2, LR: open loop control by operation condition
B_NOLRE	LREB	AUS	CARB freeze frame, cyl.row 1 bit 3, LR:open loop operating by system fault
B_NOLRE2	LREB	AUS	CARB FREEZE FRAME, bank2 bit 3, LR: open loop after system error
B_NOLRW	LREB	AUS	CARB freeze frame,cyl.row 1 bit 0,LR:open loop opera. start cond.not yet fulfil.
B_NOLRW2	LREB	AUS	CARB FREEZE FRAME, bank2 bit 0, LR: open loop,start condition not fulfilled
B_PSPAUS	LREB	LOK	condition lambda control inactive by project spezifc off-condition
B_PSPWL	LREB	LOK	condition lambda control inactive by project spezifc warmup condition
B_SA	MDRED	EIN	Condition fuel cut-off
B_SBBVK	DLSV	EIN	condition for lambda sensor upstream cat ready for operation
B_SBBVK2	DLSV	EIN	condition oxygen sensor upstream cat. bank2 ready for operation
B_SLS	AK	EIN	Condition for active secondary air



Variable	Source	Type	Description
B_SLSOFF	AK	EIN	Condition end of secondary air after removing secondary air
B_ST	SWADAP	EIN	condition for start
B_STEND	BBSTT	EIN	condition end of start
B_SYNCM	LR	EIN	Condition fr_w/fr2_w-synchronization active, fr_w is used as master
B_SYNCM2	LR	EIN	Condition fr-synchronization active,bank 2 is used as master
B_TARAU	LREB	LOK	LREB: condition start for low intake air temperatures
B_TEMIN	RKTI	EIN	Condition: TEMIN-limitation active, bench 1
B_TEMIN2	RKTI	EIN	Condition: TEMIN-limitation active, bench 2
B_TMLR	LREB	AUS	LREB: Engine Temperature dependend condition for lambda closed loop control u.C.
B_VAG	ESUK	EIN	Condition large deceleration enleanment
B_VS		EIN	Condition valve lift high
C_JNI	SWADAP	EIN	ECU-condition for intialisation
E_LSV	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_LSV2	DLSV	EIN	error flag: lambda sensor upstream catalyst
FLGLRS	LREB	AUS	CARB FREEZE FRAME byte, bank 1, for lambda control
FLGLRS2	LREB	AUS	CARB FREEZE FRAME byte, bank 2, for lambda control
FR2_W	LR	EIN	Lambda controller output (word)
FR_W	LR	EIN	Lambda controller output (word)
IMLRSA_W	LREB	LOK	air mass after fuel cut-off for continuous lambda control
LAMSONS2_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
ML_W	EGFE	EIN	air mass flow filtered (Word)
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
R_T10		EIN	Time schedule 10 ms
SY_EGAS	PROKON	EIN	system constant E-GAS present
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
SY_VS		EIN	system constant valve stroke control: no, 2 position
TANS	SWADAP	EIN	Intake air temperature
TANSST	LREB	LOK	Intake air temperature at cranking
TMOT	SWADAP	EIN	Engine temperature
TMOTLIN	GGTFM	EIN	Engine coolant temperature, linearised and calculated
TMRW	GGTFM	EIN	model-based reference value for plausibility check of engine temperature signal
TMST	GGTFM	EIN	engine temperature at start
USVK	GGLSV	EIN	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyst 2

Label for stereo LC

### FW LREB 141.10 Fixed Values

Parameter	Value	Description
CLRMSFS		code word for lambda closed-loop control lean/rich protection on/off
CLRVS		code word for lambda closed-loop control on/off at changing of valve stroke
CLRZWTMS		Codeword for hard activation of LR according to CARB
DTMR		hysteresis for cut-in threshold
DTMTMRW		temperature difference thresh. for detection of hard LC-switch on
IMLSALR		thresh.value integr.air mass for activ.delay of lambda contr.after fuel cut-off
NLRSHB		eng.speed thesh.,turn-off lamb.contr.during overrun,in connec.with idle a.TLLRSHB
RLLRSHB		load thresh.,turn-off lambda contr.during sec. air,in connect.with idle a.NLRSHB
RLRVAO		Upper rl-threshold for trigger of LR stopped during transient VA
TARAU		air temperature threshold for closed loop lambda - control switching on
TASHS		threshold intake air temp.for trigg.of TLRHS-blocking time LC during hot start
TLRHS		blocking time LC during hot start, triggered via thresholds TASHS and TMSHS
TMRA1		cut-out condition (idle-speed switch = 0)
TMRA2		cut-out condition (idle-speed switch = 1)
TMRAK		cut-out threshold of lambda closed-loop control at low starting temperature
TMSHS		threshold engine temp.for triggering of TLRHS-blocking time LC during hot start
TRAU		monitoring time for lower load limit of lambda closed-loop control
USR		controller theshold for lambda control upstream catalyst



## FB LREB 141.10 Detailed description of function

1.1 Switch-on / switch-off via temperature thresholds TMRA1 (partial load) TMRA2 (idling) TMRAX (no emission test)

- 1.1.1 Switch-on at  $T_{mot} > TMR_{Ax} + DTMR$   
Switch-off at  $T_{mot} < TMR_{Ax}$
- 1.1.2 If the condition  $T_{mot} > TMSHS$  and  $T_{ans} > TASHS$  is fulfilled at start, then switch-on as from end of start after a delay time  $t > TLRHS$ .
- 1.1.3 Switch on as from end of start after a delay time  $TLRTMS$  dependent on the engine temperature at start.

1.2 Sensor operating readiness

- 1.2.1 Switch on, if flag  $B_{sbbvk}$  from  $\%DLSV$  is set with the switch-on delay  $TSBBVTMS = f(tmst)$ .
- 1.2.2 Switch off, if flag  $B_{sbbvk}$  from  $\%DLSV$  is not set.

1.3 Switch-over to open-loop control under certain conditions, hence switch-over to close-loop control

Switch-over to open-loop control:

- 1.3.1 at start
- 1.3.2 at fuel cut-off on overrun ( $B_{sa} = 1$ ); until throughput of air mass  $IMLSALR$  after transition from ( $B_{sa} : 1 \rightarrow 0$ )
- 1.3.3 while UKSEFI status  $B_{bag} = 1$  OR while UKSEFI status  $B_{vag} = 1$
- 1.3.4 when exceeding a load threshold  $rl > RLLRUN(nmot)$  after a delay time  $t > TRAB$
- 1.3.5 Lambda setpoint  $lamsons_w <> 1.0$
- 1.3.6 at idling, if ( $B_{ll} = 1$ ) &  $t_l \geq TLLRSHB$  &  $n \geq NLRSHB$
- 1.3.7 while function secondary air is active, is achieved indirectly by  $lamsons_w > 1$
- 1.3.8 Lambda control is blocked after function secondary air until the bit  $B_{slsoff}$  (from  $\%DLSL$ ) has been set  
Check of Bit  $B_{slsoff}$  is blocked as long as bit  $B_{sls}$  is TRUE

Switch-over to close-loop control:

- 1.3.10 with  $lamsons_w < 1.0$  (e.g. at full load) and ready control sensor OR while UKSEFI status  $B_{bag} = 1$   
OR while UKSEFI status  $B_{vag} = 1$ ,  
and under the following conditions:  
(lean mixture,  $usvk < USR$ ) AND ( $fr \geq 1.0$ ) OR ((rich mixture, i.e.  $usvk > (USR \cdot fr > 1.0)$ )  
independent of temperature-dependent switch-on conditions

1.4 Switch-over to open-loop control during OBDII fault detection

Switch-over to open-loop control:

- 1.4.1 with fault injector power stage,  $B_{eev}$  from  $\%DEVE$
- 1.4.2 with fault catalyst damaging misfires ( $B_{mdkat}$  by  $DMDMIL4.10$ )
- 1.4.3 with fault secondary air system  $B_{esls}$  (only with spurious air due to open secondary air valve or running secondary air pump)

1.5 Switch-over to open-loop control under further project-specific switch-off conditions

Switch-over to open-loop control project-specifically:

- 1.5.1 as soon as  $B_{evloc} := 0$ ; the following applies to the following conditions
  - 1.5.1.1 at active engine speed limitation
  - 1.5.1.3 at speed limitation
- 1.5.2 As soon as bit  $B_{craus}$  is set; mode basic setting:  
Permits open-loop controlled operating of the engine by the workshop  
for diagnostic purposes

2.1 Switch-over to close-loop control at compulsory switch-on (according to CARB requirement)

- 2.1.1  $CLRZWTMS > 0$   
Switch-over to close-loop control at compulsory switch-on after  $t_{mot}$ -fault was suspected  
As soon as the difference between the model engine temperature  $t_{mrw}$  and the engine temperature raw value is greater than the threshold  $DTMTMRW$ , the LC is switched on compulsorily after the time  $TLRZWTMS = f(tms)$ .
- 2.1.2  $CLRZWTMS = 0$   
Switch-over to close-loop control at compulsory switch-on  
The LC is switched on compulsorily after the time  $TLRZWTMS = f(tms)$



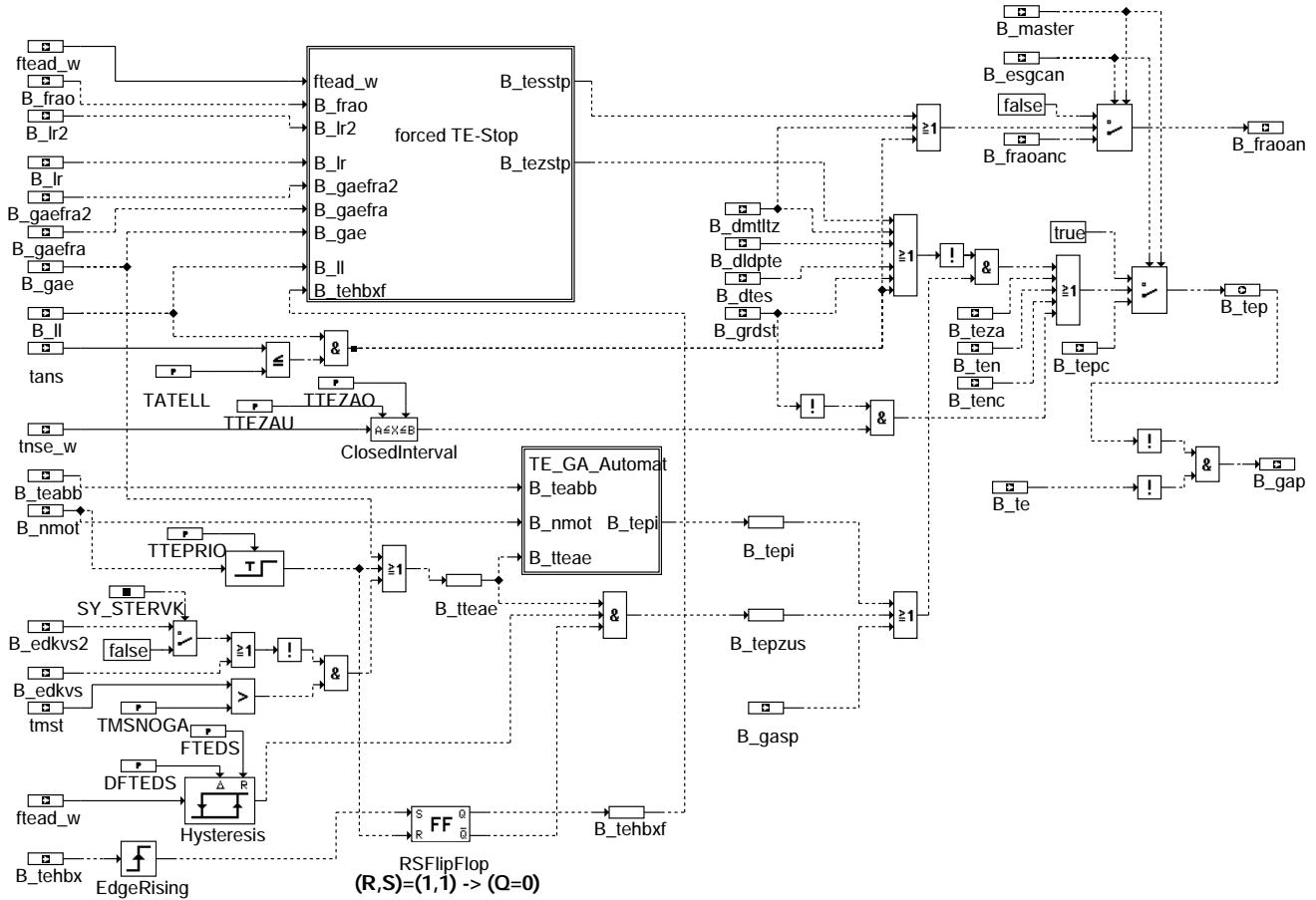


## FB LRINI 1.0 Detailed description of function

## APP LRINI 1.0 Application hint

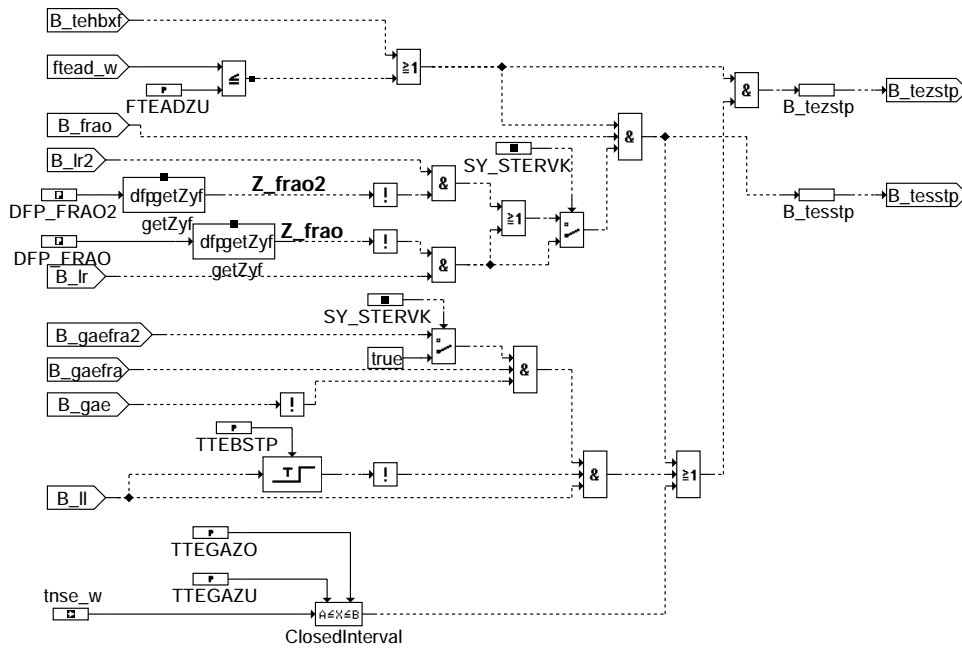
## BBTEGA 4.20 Operating conditions for purge canister control / fuel adaption

## FDEF BBTEGA 4.20 Function definition



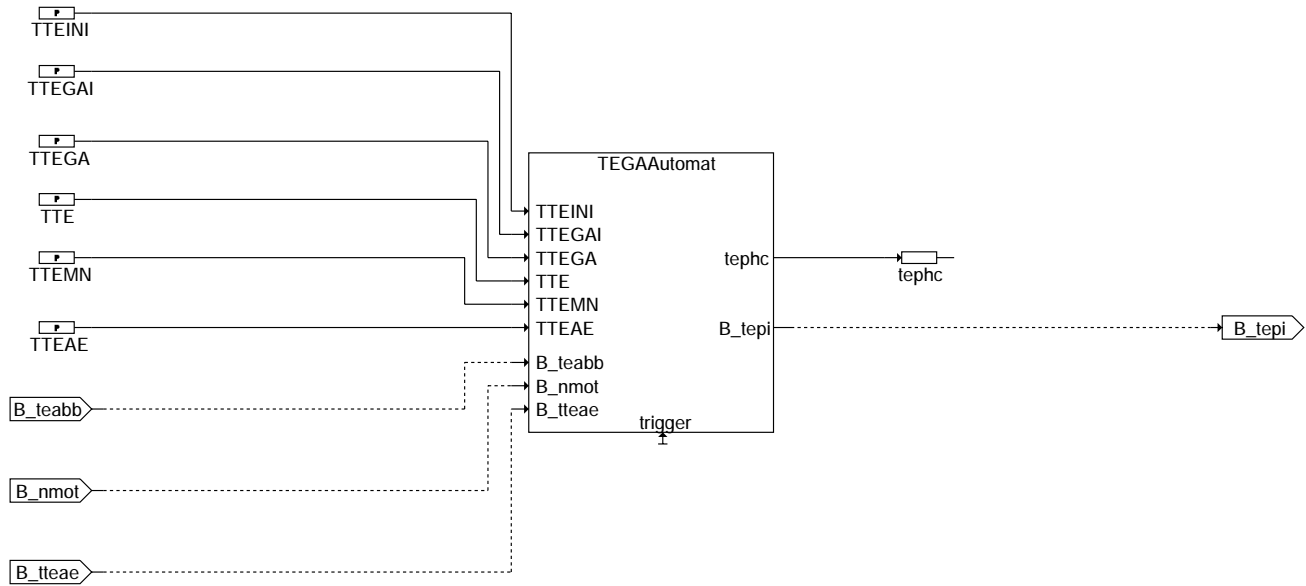


forced TE-Stop:

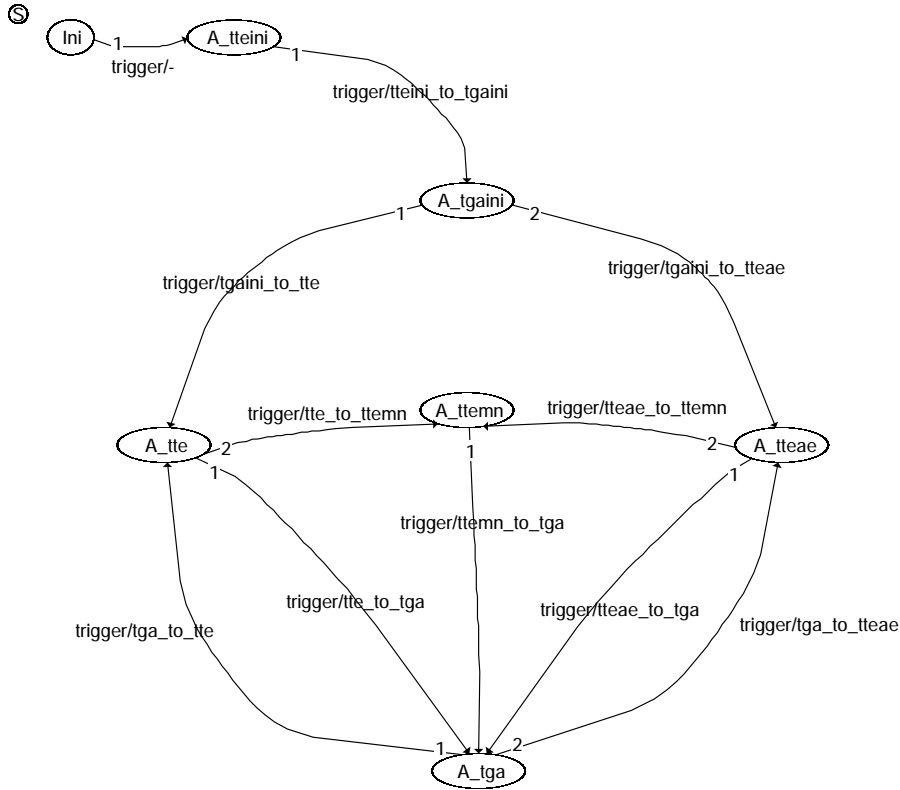


**bbtega-forcedte-s**

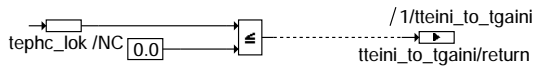
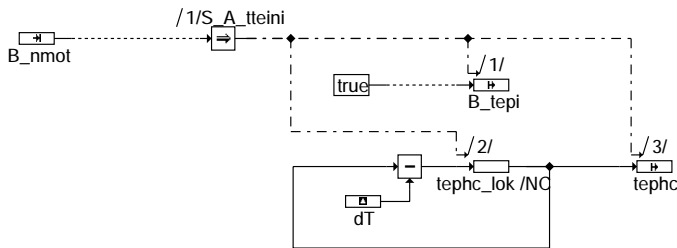
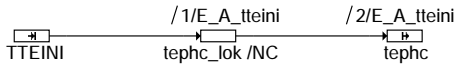
TE-GA-AUTO: Statemachine for phase control between canister purge (TE) and mixture adaptation (GA)



**bbtega-te-ga-auto**



**bbtega-statemachi**

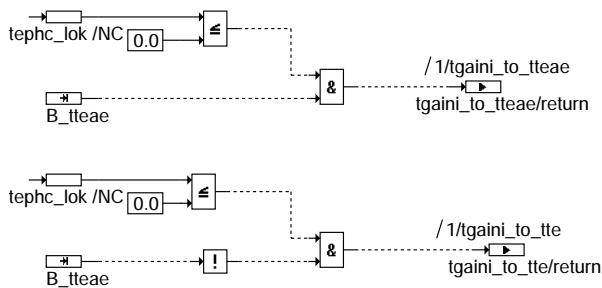
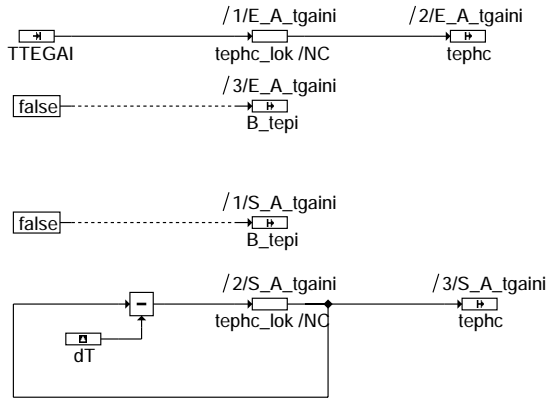


**bbtega-a-tteini**

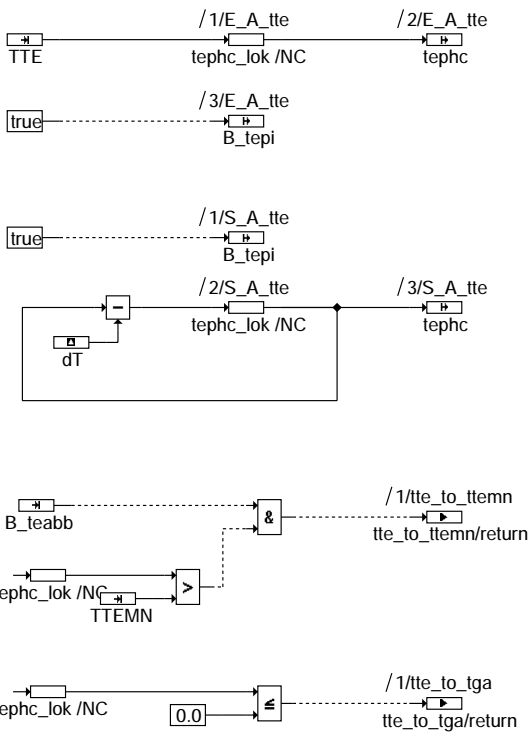
bbtega-statemachi

bbtega-a-tteini





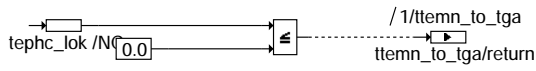
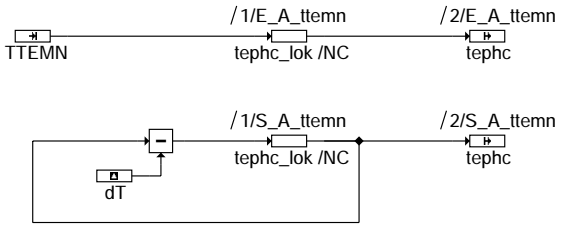
**bbtega-a-tgaini**



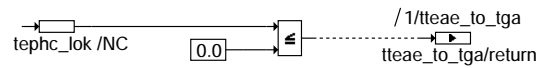
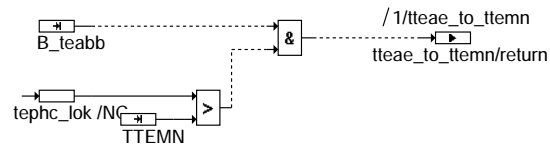
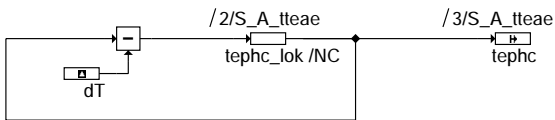
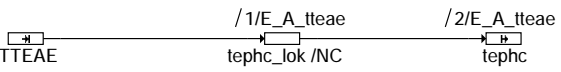
**bbtega-a-tte**

bbtega-a-tgaini

bbtega-a-tte



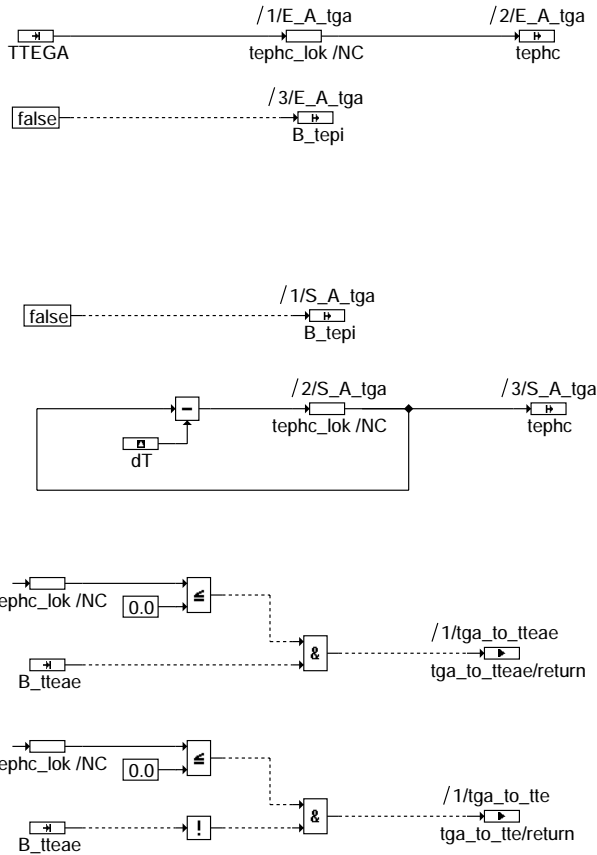
### bbtega-a-ttemn



### bbtega-a-tteae

bbtega-a-ttemn

bbtega-a-tteae



bbtega-a-tga

## ABK BBTEGA 4.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DFTEDS			FW	hysteresis width on canister charge for switching to endless purging
FTEADZU			FW	threshold canister charge for interruption of the purge phase
FTEDS			FW	threshold canister charge for switching to endless purging
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TATELL			FW	tans-threshold for canister purge control with B <sub>LI</sub> = 1
TMSNOGA			FW	threshold tms for endless purge control, if mixture adaptation without error
TTE			FW	time for canister purge phase
TTEAE			FW	duration of canister purge phase with completed mixture adaptation
TTEBSTP			FW	maximum time for purge stop at idle if the cycle flags are not set
TTEGA			FW	time during canister purge for basic adaptation
TTEGAI			FW	Duration of the first mixture adaptation phase
TTEGAZO			FW	Time for canister purge stop for lambda adaptation, upper threshold
TTEGAZU			FW	Time for canister purge stop for lambda adaptation, lower threshold
TTEINI			FW	Duration of the first purge phase
TTEMN			FW	time for canister purge phase minimum
TTEPRIO			FW	time after start for switching to endless purging
TTEZAO			FW	Time for permanent canister purge, upper threshold
TTEZAU			FW	Time for permanent canister purge, lower threshold
Variable	Source		Type	Description
B_DLDPTE	GKRA		EIN	request from evap system monitoring to shut down PCV
B_DMTLTZ			EIN	Condition TEV should be closed
B_DTES	GKRA		EIN	Condition for active diagnosis of canister purge system
B_EDKVS	DKVS		EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS		EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_ESGCAN			EIN	Condition error ecu-CAN for 2 ME-ecu's
B_FRAO	LRA		EIN	condition for enabling adaption of frao
B_FRAOAN	BBTEGA		AUS	demand CPV quickly closing for activation of mixture adaptation
B_FRAOANC			EIN	demand CPV quickly closing for mixture adaptation, signal from CAN
B_GAE	DKVS		EIN	condition for adaptive Lambda pilot control successful
B_GAEFRA	DKVS		EIN	condition for fra portion of adaptive Lambda pilot control successful
B_GAEFRA2	DKVS		EIN	condition for fra2 portion of adaptive lambda pilot control successful
B_GAP	BBTEGA		AUS	condition mixture adaptation phase active
B_GASP	LRAEB		EIN	condition for basic mixture adaptation disabled
B_GRDST			EIN	condition basic attitude
B_LL	MSF		EIN	Condition idle
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2



Variable	Source	Type	Description
B_MASTER		EIN	Condition MASTER-ECU
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_TE	TEBEB	EIN	Condition canister purge active
B_TEABB	TEB	EIN	Condition purge canister function ready to finish
B_TEHBX	TEB	EIN	Condition load integrator ftead at max. limit
B_TEHBXF	BBTEGA	LOK	Condition load integrator ftead at max. limit, filtered
B_TEN	TEBEB	EIN	condition open loop purging
B_TENC		EIN	condition open loop purging, input from CAN
B_TEP	BBTEGA	AUS	Condition canister purge phase active
B_TEPC		EIN	Condition canister purge phase active from CAN
B_TEPI	BBTEGA	LOK	Condition canister purge phase active internal
B_TEPZUS	BBTEGA	LOK	condition additional canister purge phase
B_TESSTP	BBTEGA	LOK	condition canister purge fast stop
B_TEZA		EIN	Condition forced activation of the purge control function
B_TEZSTP	BBTEGA	LOK	condition canister purge forced stop
B_TTEAE	BBTEGA	LOK	condition switch over to long purge phase
FTEAD_W	TEB	EIN	charcoal canister charge
TANS	SWADAP	EIN	Intake air temperature
TEPHC	BBTEGA	LOK	phase counter mixture adaptation / canister purge
TMST	GGTFM	EIN	engine temperature at start
TNSE_W	BBSTT	EIN	time counter at end of start (16 bit)
Z_FRAO	DKVS	EIN	cycle flag of mixture adaption factor frao
Z_FRAO2	DKVS	EIN	cycle flag of mixture adaption factor frao2 (bank 2)

### FW BBTEGA 4.20 Fixed Values

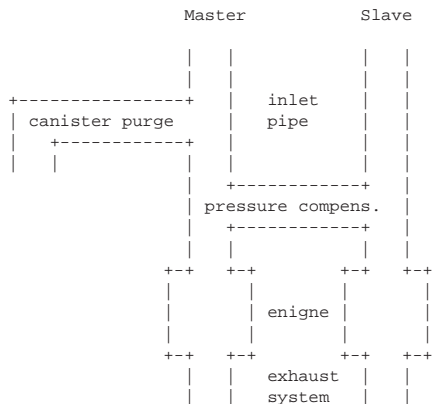
Parameter	Value	Description
DFTEDS		hysteresis width on canister charge for switching to endless purging
FTEADZU		threshold canister charge for interruption of the purge phase
FTEDS		threshold canister charge for switching to endless purging
TATELL		tans-threshold for canister purge control with B_JI = 1
TMSNOGA		threshold tms for endless purge control, if mixture adaptation without error
TTE		time for canister purge phase
TTEAE		duration of canister purge phase with completed mixture adaptation
TTEBSTP		maximum time for purge stop at idle if the cycle flags are not set
TTEGA		time during canister purge for basic adaptation
TTEGAI		Duration of the first mixture adaptation phase
TTEGAZO		Time for canister purge stop for lambda adaptation, upper threshold
TTEGAZU		Time for canister purge stop for lambda adaptation, lower threshold
TTEINI		Duration of the first purge phase
TTEMN		time for canister purge phase minimum
TTEPRIO		time after start for switching to endless purging
TTEZAO		Time for permanent canister purge, upper threshold
TTEZAU		Time for permanent canister purge, lower threshold

### FB BBTEGA 4.20 Detailed description of function

Remark on engine assembly: concept with 2 control units

- two identical engine control units (same code, same data)
- PIN-information B\_master tells the control unit if it is used as a master or as a slave control unit
- 1 canister purge valve on each side. The inlet pipes are relied down stream the 2 canister purge valves. This means that the canister purge on one side has an impact on the other side.
- Therefore canister purge must be simultaneous in both control units --> synchronization of the control units
- Calculation of BBTEGA in master control unit only. The results B\_tep and B\_fraoan are reported to the slave

##



##

Remarks on stereo lambda control:

- The FDEF below is intended for systems with stereo and mono lambda control but there is no stereo variable necessary because in DKVS B\_gae represents the both sides.



Description of phase control, mixture adaptation / canister purge (function BBTEGA):

-----  
Output variables:

- Mixture adaptation phase active: B\_gap (B\_gap = TRUE does not necessarily mean that LRA is really active)
- Canister purge phase active: B\_tep (B\_tep = TRUE does not necessarily mean that TEB is really active)  
Remark: With inactive lambda control (e.g. defective probe), the system switches to controlled purge operation. The canister purge valve is opened even in a "mixture phase". The LRA is then disabled.

Input variables:

- Load ftead for PCV closing, if
  - in idle speed the mixture adaptation has not stabilized (B\_gae = FALSE) and multiplicative adaptation has stabilized (B\_gaefra=TRUE).
  - upper multiplicative range is active, the cycle bit Z\_frao(2) = FALSE and the lambda control is active (B\_lr(2) = TRUE).
- Flags of the DKVS (B\_gae, B\_gaefra/2). The flag B\_gae corresponds to the cycle bit of DKVS. When LRA is not complete, there is greater need of adaptation at idle.
- Request bits of the diagnosis functions that can only run at idle speed (B\_dldpte, B\_dtes, B\_dmltz)
- Request bits for a quickly test: B\_grdst
- The bit B\_nmot (engine speed plausible) for initialisation of counters in the phase control
- The bits B\_teabb (purge ready to finish), B\_gasp (mixture adaptation disabled) and B\_tehbx (load at max. limit) for influencing the phase control
- The Bit B\_te from the TEBEB for detecting whether the purge valve is closed.
- tans : No canister purge control in idle speed, if manifold air temperature less then threshold TATELL
- time since end of start tse\_w for time controlled canister purge and mixture adaptation
- Bits B\_ten and B\_tenc (= B\_ten via CAN from the other control unit): canister purge at open loop (no lambda control)
- PIN-information B\_master shows, which of the 2 control units is the master that calculates the phase control.
- The bit B\_esgcan tells, if the CAN-communication between the master and the slave is OK. ##

Purpose of phase control:

- Coordination of the changeover between mixture adaptation and canister purge with the following aims:
  - a) Maximising the flush volume (in emission test and in the field) especially at high loads => activate TEB
  - b) Quickest possible detection of a DKVS fault (sufficiently long and frequent activation of mixture adaptation on faults) => activate LRA
  - c) Quickly closing of the purge valve and LRA (activate upper multiplicative range) at low load
  - d) Quickest possible activation of diagnosis functions that only run at idle speed  
=> Initiation of reset of the purge valve at B\_ll (idle switch only) and low load
  - e) Reset of the purge valve on request by DKVS (B\_gae = FALSE and multiplicative adaptation correction is completed), DLDP (B\_dldpte) and tester (B\_grdst)
  - f) Activation of TEB, if from DLDP desired (B\_teza)
  - g) Long canister purge, if the time after start greater then TTEPRIO or B\_gae = TRUE or a hotstart without a fault in fuel supply system (starttempeture higher then TMSNOGA and B\_edkvs(2) = FALSE).
  - h) Endless canister purge at high load of canister purge (ftead >= FTEDS), B\_tehbx = FALSE and long canister purge is activated (B\_tteae = TRUE).
  - i) No canister purge control in idle speed, if manifold air temperature less then threshold TATELL

Implementation of phase control:

If the CAN doesn't work (B\_esgcan = 1) both control units activate the canister purge. If the CAN does work, the master and the slave control unit have their respective tasks:  
B\_master = 0 means that in this control unit no phase control is calculated. The information "canister purge phase active" B\_tep and "quick closing of canister valve" B\_fraoanc are read via CAN from the other control unit and according to it the condition "mixture adaptation phase active" B\_gap is calculated.  
When B\_master = 1 the following phase control plays. The results B\_tep and B\_fraoanc are an output to the CAN.

- The core is a statemachine. The output of this statemachine is the bit B.tepi (internal purge phase). The main internal variable is the RAM cell tephc - phase counter for canister purge/mixture adaptation. It is set to an initial value at the start of each phase. The phase counter is decremented in each state. At zero the system generally switches to the other state.

The following process control is integrated into this statemachine:

- Start with a purge phase (B.tepi = TRUE) of length TTEINI, which cannot be aborted (state A.tteini)
- Switching to state A.tgaini: first mixture adaptation phase -> B.tepi = FALSE
- Depending on bit B.tteae (long purge phase) transition to state A.tteae (long purge phase with TTEAE) if B.tteae = TRUE, else short purge phase with TTE if B.tteae = FALSE. Both states may be exited prematurely if the remaining time is greater than TTEMN (tephc < TTEMN) and the bit B.teabb (purge ready to finish) is set. => Transition to state A.ttemn. Otherwise when the phase counter has elapsed, transition to mixture adaptation (A.tga).
- After the adaptation phase, transition to either long or short purge phase.
- Two conditions result in switching to endless canister purge (OR condition with B.tepi):
  - A) B.gasp - mixture adaptation disabled
  - B) Load greater than threshold FTEDS (hysteresis to prevent toggeling of activation of endless canister purge) and load was not at maximum limit (this condition is reset once when time TTEPRIO after start ist elapsed) and
    - time TTEPRIO after start elapsed, or
    - mixture adaptation complete or
    - the starttemperature is higher then threshold TMSNOTGA and any faults are in diagnosis fuel supply system.



- However, some conditions produce a "dominant" switching (activation) of mixture adaptation:
  - A) If the DKVS (additive correction) that is active at idle speed" has not yet finished running (B\_gae = FALSE) while already B\_gaefra(2) = TRUE and the canister load is less than a threshold (FTEADZU) with the idle switch closed. After the time TTEBSTP the adaptation is stopped and TEB is started again in order to avoid long adaptation times in long idle phases.
  - B) At active lambda control, if B\_frao = TRUE, and Z\_frao is not set, the system also switches to a mixture adaptation phase at low canister load. In this case the purge valve is closed quickly.
  - C) A "diagnosis function active at idle speed" forces a purge phase: B\_dldpte, B\_dtes, B\_dmtltz
  - D) Short test via tester: B\_grdst = TRUE
  - E) at low manifold air temperature in idle speed for a quiet operation the canister purge control is switched off.
  - F) time controlled mixture adaptation phase starting at time TTEGAZU and ending at time TTEGAZO
- Activation of TE-phase with highest priority at the following conditions.
  - A) activation from the DLDP by B\_teza
  - B) time controlled canister purge phase starting at time TTEZAU and ending at Time TTEZAO
  - C) There is canister purge at open loop (no lambda control) in one of the control units: B\_ten and B\_tenc

### APP BBTEGA 4.20 Application hint

TTEINI : 220 s  
TTEMN : 30 s  
TTEGAI : 130 s  
TTE : 60 s  
TTEAE : 300 s  
TTEGA : 60 s  
TTEPRIO : 700 s  
TTEBSTP : 40 s

TTEGAZU : 250 s for FTP75 the values lay within the TTEGAI-phase: this supplementary feature is not used ##  
TTEGAZO : 260 s

TTEGAZU : 1000 s for ECE a adaptation phase can be forced in the high load phase and the following idle time  
High engine capacity: propably the 4th range is not reached: late time TTEGAZU is enough  
Low engine capacity: eventually TTEGAZU a bit earlier to guarantee that there is enough time for the FRAU-range. ##  
TTEGAZO : 1230 s

TTEZAU : FTP: 900s DTEV assured in idle phase at 1000 s after start  
TTEZAO : FTP: 1020s

TTEZAU : ECE: 610 s DTEV has 3 chances; if only one chance needed: TTEZAU = 750 s  
TTEZAO : ECE: 840 s

TMSNOGA : 50 °C

FTEDS : 20  
DFTEDS : 5  
FTEADZU : 5 kg/m<sup>3</sup>  
MSTEOZU : 0.1 kg/h

#### Remarks on the BBTEGA concept for 2 control units

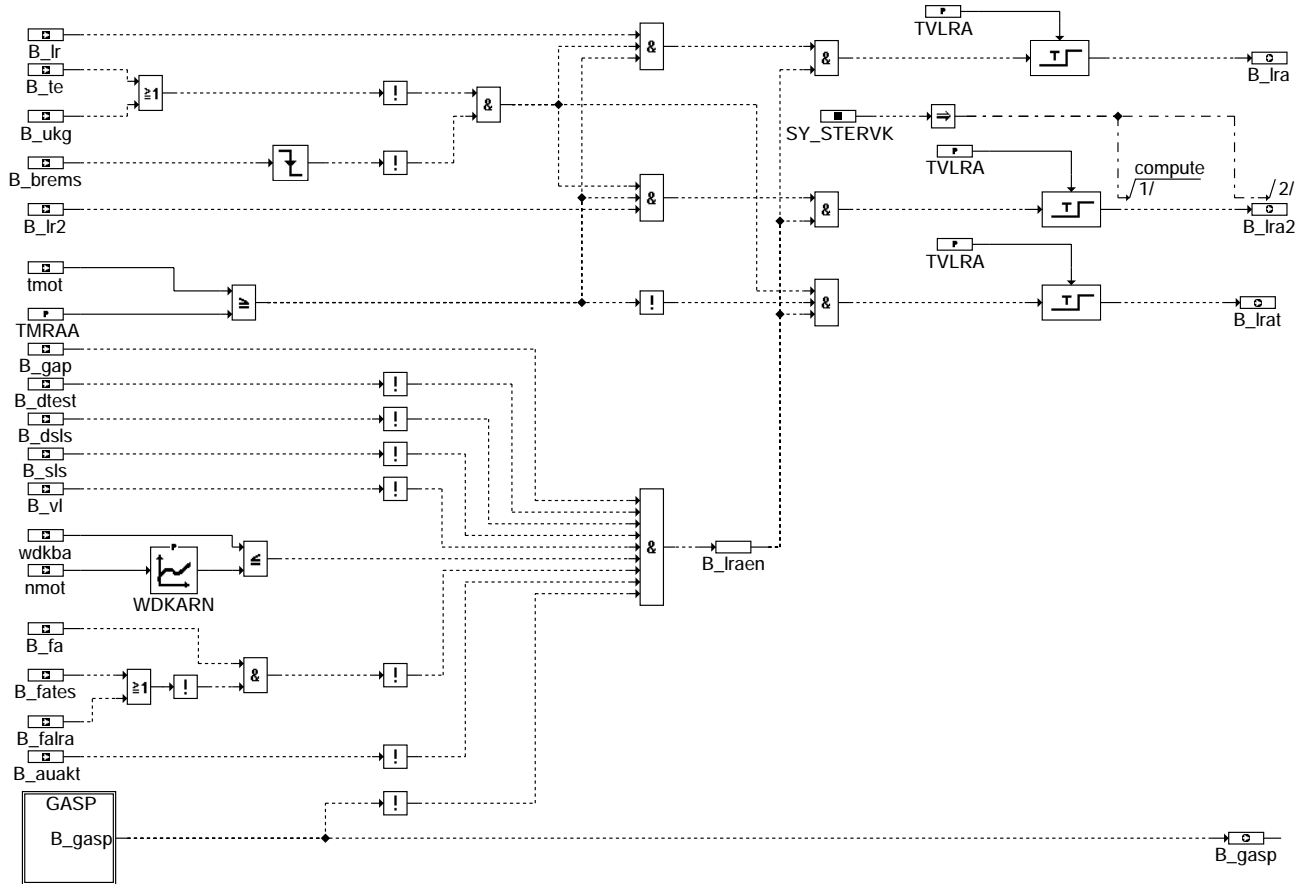
-----  
This BBTEGA was optimized for small changing cost and few communication via CAN. Therefore bear in mind to the following please:

Only the functions of the master control unit can influence the phase control. It therefore may happen that the phase control is not optimal for the slave. Though there is guarantee that the functions are undisturbed when activated:

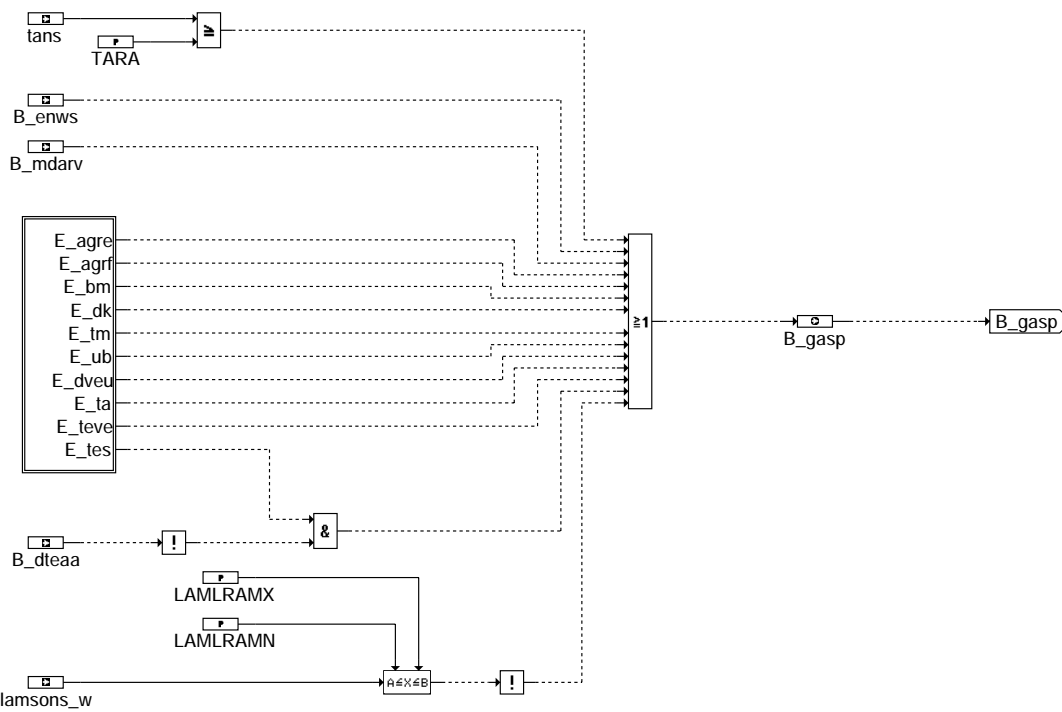
- inhibit of the LRA in both control units, if there is no lambda control in one of the control units and the canister purge is running in open loop.
- The condition B\_tep exists in both control units. Each function that requests a canister purge phase must check whether B\_tep is set before starting.

## LRAEB 4.90 Conditions adaptive pilot control

### FDEF LRAEB 4.90 Function definition



#### lraeb-main



#### lraeb-gasp



## ABK LRAEB 4.90 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
LAMLRAMN			FW	minimum of lambda threshold for mixture adaptation active
LAMLRAMX			FW	maximum of lambda threshold for mixture adaptation active
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TARA			FW	temperature threshold intake air
TMRAA			FW	cut-in temperature adaptive precontrol for lambda closed-loop control
TVLRA			FW	delay time for activation of the lambda adaption after lambda control active
WDKARN	NMOT		KL	threshold throttle angle for activation of the mixture adaptation

Variable	Source	Type	Description
B_AUAKT		EIN	condition emission check active
B_BREMS	GGEGAS	EIN	condition: brake operated
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DTEAA	DTEV	EIN	Condition diagnosis CPV by opening the CPV active
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_ENWWS	DNWS	EIN	condition error camshaft control
B_FA		EIN	condition general function request
B_FALRA		EIN	condition: requirement adaption open loop
B_FATES		EIN	condition leak detection request
B_GAP	GKEB	EIN	condition mixture adaptation phase active
B_GASP	LRAEB	AUS	condition for basic mixture adaptation disabled
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRA	LRAEB	AUS	condition for basic mixture adaptation enabled
B_LRA2	LRAEB	AUS	condition for basic mixture adaption 2 enabled
B_LRAEN	LRAEB	LOK	Condition mixture adaptation is enabled
B_LRAT	LRAEB	AUS	condition for basic mixture adaptation temperature dependet enabled
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_SLS	AK	EIN	Condition for active secondary air
B_TE	TEBEB	EIN	Condition canister purge active
B_UKG	ESUK	EIN	condition transient control activated
B_VL	MSF	EIN	Condition for wide open throttle
DFP_AGRE	LRAEB	DOK	ECU int. fault path no.: EKR power stage
DFP_AGRF	LRAEB	DOK	ECU int. fault path no.: partial pressure EGR
DFP_BM	LRAEB	DOK	ECU int. fault path no.: reference mark
DFP_DK	LRAEB	DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_DVEU	LRAEB	DOK	ECU-internal fault-path no.: DV-E failure during UMA learning
DFP_TA	LRAEB	DOK	ECU int fault path no.: air intake temperature TANS
DFP_TES	LRAEB	DOK	Internal error path number evap system monitoring, pcv Struck open
DFP_TVEV	LRAEB	DOK	Internal fault path number: canister purge valve power stage
DFP_TM	LRAEB	DOK	Internal fault path number: engine temperature
DFP_UB	LRAEB	DOK	Internal fault path number: ambient conditions
E_AGRE		EIN	error flag: EGR power stage monitoring
E_AGRF		EIN	error flag: EGR flow monitoring
E_BM	DDG	EIN	error flag: reference mark sensor
E_DK	DDVE	EIN	Error flag: throttle position sensor
E_DVEU	DDVE	EIN	Error flag: DV-E cause of failure: UMA-learning
E_TA	GGTFA	EIN	error flag: TANS
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEV	DTEVE	EIN	error flag: canister purge valve power stage
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
E_UB	GGUB	EIN	error flag: power supply voltage UB
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
NMOT	SWADAP	EIN	engine speed
TANS	SWADAP	EIN	Intake air temperature
TMOT	SWADAP	EIN	Engine temperature
WDKBA	GGDVE	EIN	throttle angle

## FW LRAEB 4.90 Fixed Values

Parameter	Value	Description
LAMLRAMN		minimum of lambda threshold for mixture adaptation active
LAMLRAMX		maximum of lambda threshold for mixture adaptation active
TARA		temperature threshold intake air
TMRAA		cut-in temperature adaptive precontrol for lambda closed-loop control
TVLRA		delay time for activation of the lambda adaption after lambda control active



**FB LRAEB 4.90 Detailed description of function**

Remarks concerning stereo lambda control:

- This FDEF is intended for systems with stereo lambda control.
- The stereo variables are identified by the suffix 2 (e.g. B\_lra -> B\_lra2).
- The FDEF is also fully applicable for mono systems. In this case B\_lr2 = FALSE. And thus B\_LRA2 = FALSE.
- At a Mono system (SY-STERVK) = FALSE B\_lra2 is automatically set to FALSE.

Description of the function LRAEB:

- The function LRAEB provides the cut-in conditions for adaptations and the bit "mixture adaptation disabled" (B\_gasp).
- For stereo systems the cut-in conditions are separate for each bank (B\_lra, B\_lra2).

Bit B\_gasp:

A series of OBDII errors prohibit mixture adaptation (E-...) . Adaptation is also prohibited at high intake air temperatures (tans>TARA) . These disable conditions are compiled in the flag B\_gasp. When B\_gasp = true the system should switch to permanent purging. This is taken into account in the relevant phase control or canister purge module.

Other cut-in conditions:

As long as B\_gasp = false, mixture adaptation is only ever enabled if for the time TVLRA the engine temperature was above the threshold TMRAA; lambda control with closed TEV (B\_te = FASLE) was uninterrupted active, (B\_lr/B\_lr2 = true & NOT B\_te); the basic adaptation phase was there (B\_gap = true); no full load (B\_vl = false) and no function / diagnosis function was running to prohibit adaptation (e.g. secondary air injection (B\_sls), secondary air diagnosis (B\_dsls) or canister purge diagnosis (B\_gttest)). The LRA is also stopped for the time TVLRA an activation of the break, so that leakage air can not disturbe rkat.w.

The learning of the mixture adaptation is prohibited by B\_ukg = TRUE at least for the time TVLRA in order to avoid an error in diagnosis %DKVS due to a strong effect from transient control.

If an off-bord tuning of the exhaust emission occur, the LRA should be stopped.

If the throttle valve is fully, or almost fully open, no adaptation may occur. In this case the load signal may be falsified by pulsations. Above the throttle valve threshold WDKARN adaptation is disabled for this reason. WDKARN is an engine-speed-dependent characteristic.

By a function request B\_fa = TRUE the LRA is stopped unless B\_fates or B\_falra are true.

The mixture adaptation is stopped, if desire lambda is more rich then LAMLRAMN or more lear then LRMLRAMX.

For temperature dependent adaptation factor is formed the bit B\_frat. It is only active, if the engine temperature is less then the switch on temperature of mixture adaptation.

**APP LRAEB 4.90 Application hint**

TMRAA: Cut-in threshold for engine temperature. LRA must always be able to be active in the large peak (FTP75). Warm running must be controlled. TMRAA: 50 - 70 ° C

TARA: Cut-off threshold for high intake air temperatures: project-specific: above 60 - 100 °C

TVLRA: Cut-in delay after tatei = 0 and B\_lr (B\_lr2) = TRUE. Avoids erroneous adaptations when idle control not yet stabilised, e.g. after purge operation or deceleration cut-off. Value: 1 - 4 s

WDKARN: Erroneous adaptations in the pulsation range must be avoided at all costs. Set WDKARN a few percent below the pulsation range.

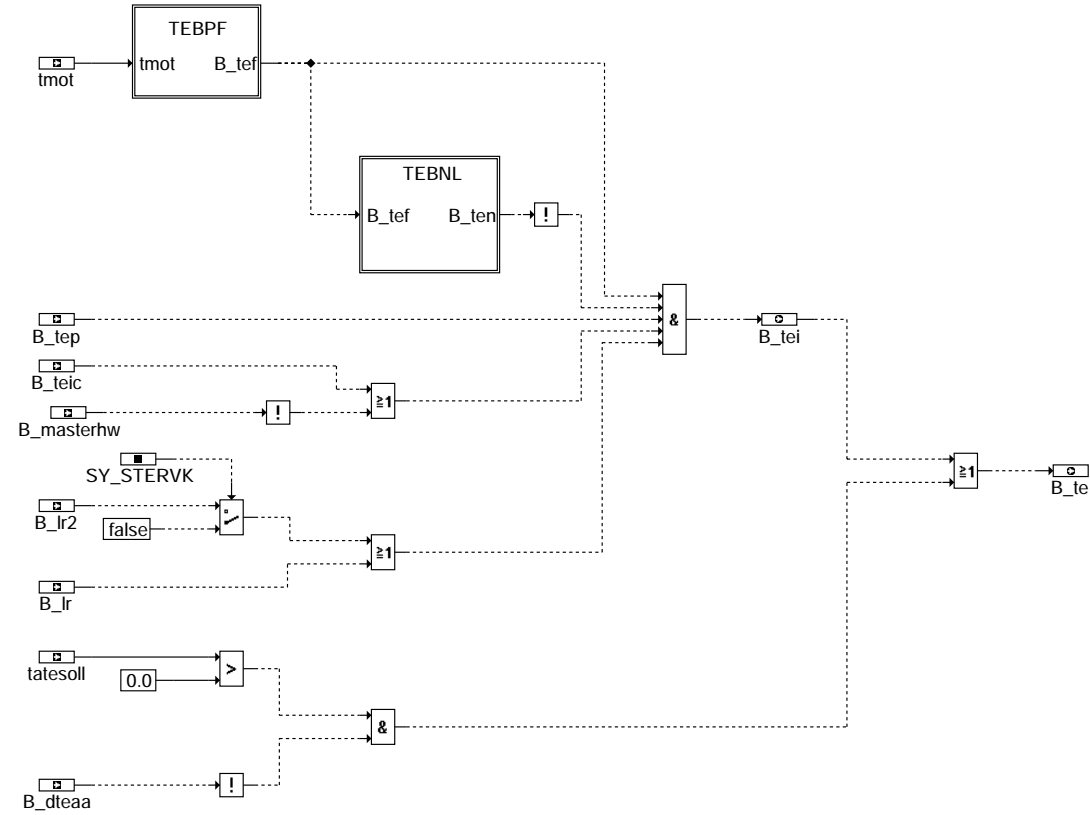
Remark: The threshold TLWARN (or TLARN) familiar from earlier FDEFs can be converted into WDKARN.

LAMLRAMN : for continue control take greater then value in LALIUSMN [0,8...0,85...0,9] and für two point control take equal 0,95

LAMLRAMX : for continue control [1,2..1,1..1,3] and for two point control take equal 1.05

## TEBEB 6.20 Switch-on conditions for purge control

### FDEF TEBEB 6.20 Function definition

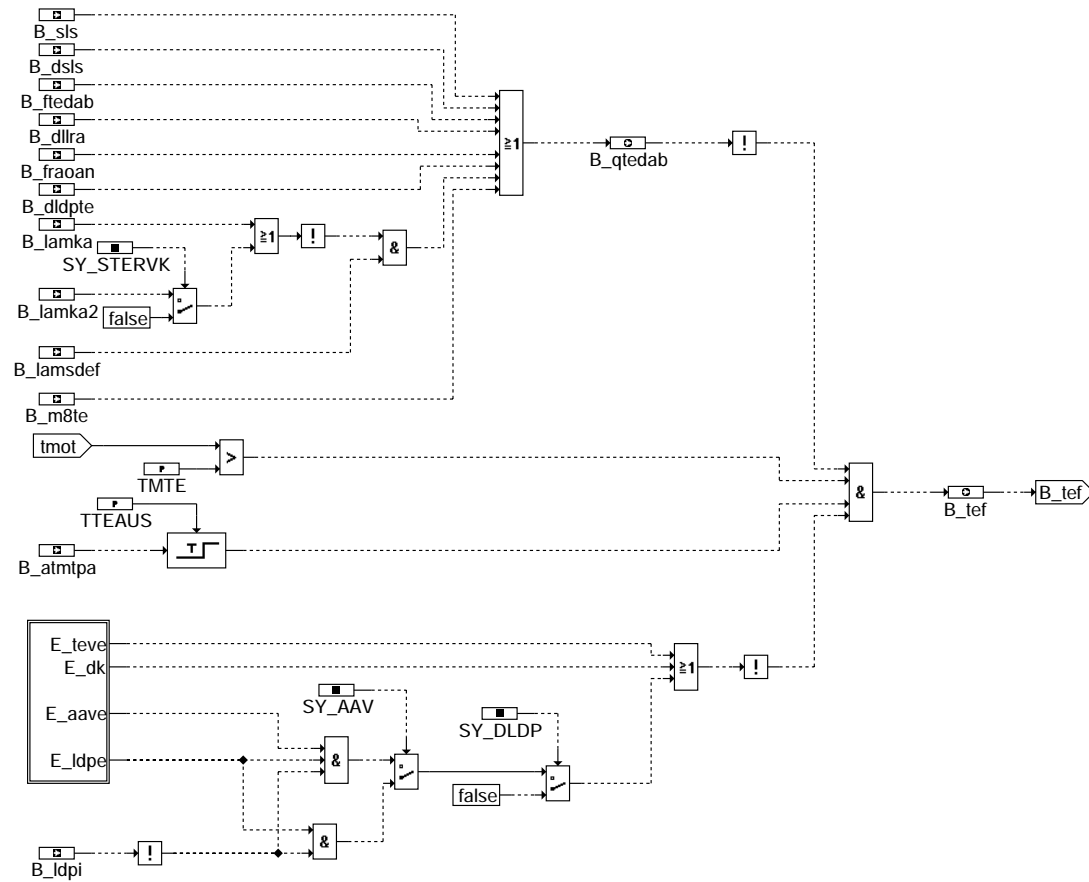


tebeb-main

tebeb-main

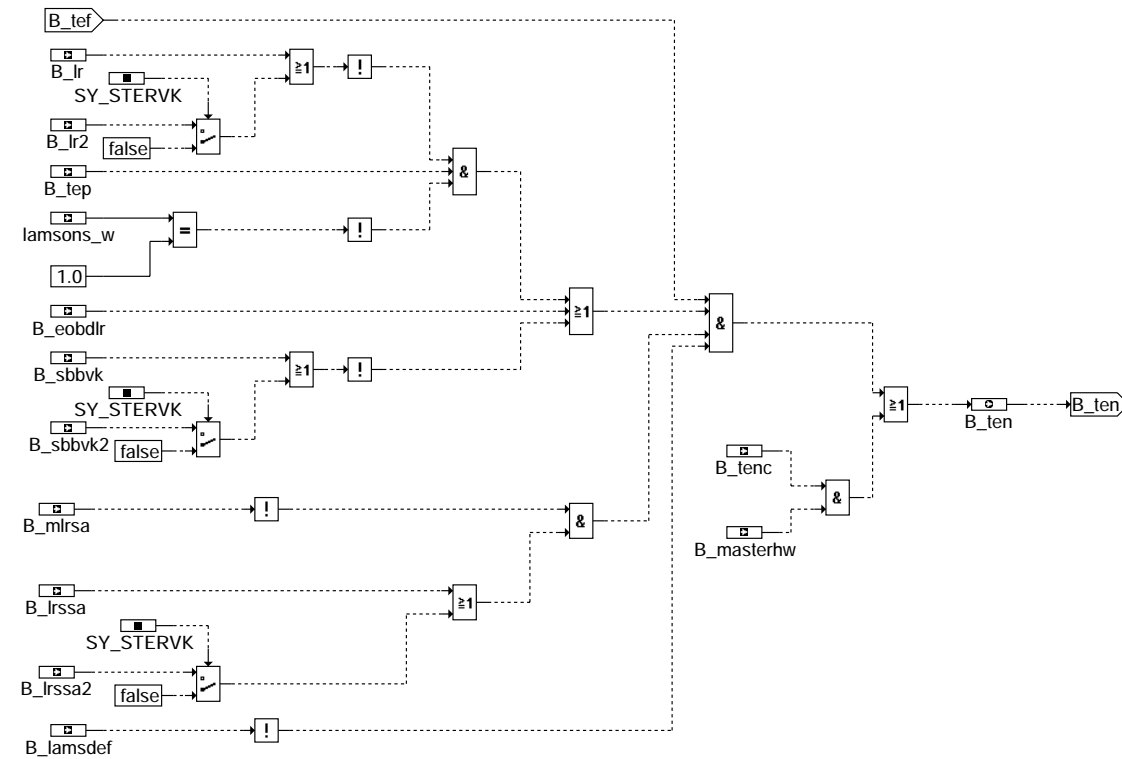


### TEBPF: Purge Control Principally Enabled



### tebeb-tebpf

### TEBNL: Purge Control at Limp-Home Operation



### tebeb-tebnl



## ABK TEBEB 6.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SY_DLDP			SYS (REF)	SY_DLDP = 1 there ist a DLDP in system
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TMTE			FW	engine-temperature threshold for canister purge
TTEAUS			FW	Delay time after engine start for activating the purge control valve
Variable	Source		Type	Description
B_ATMTPA	ATM		EIN	condition temperature upstream catalyst exceeds dew-point
B_DLDPTE	GKRA		EIN	request from evap system monitoring to shut down PCV
B_DLLRA	DLLR		EIN	Condition DLLR request
B_DSLS			EIN	condition for active diagnosis of secondary air system
B_DTEAA	DTEV		EIN	Condition diagnosis CPV by opening the CPV active
B_EOBDLR	LREB		EIN	error flag: "OBDII summary fault, disables lambda control
B_FRAOAN	BBTEGA		EIN	demand CPV quickly closing for activation of mixture adaptation
B_FTEDAB	DTEV		EIN	Condition decrease purge rate for diagnosis CPV
B_LAMKA			EIN	lambda for Katalyst oxygen purge is active
B_LAMKA2			EIN	lambda for Katalyst oxygen purge is active
B_LAMSDEF	LAMKO		EIN	Condition: defined desired air/fuel ratio value
B_LDPI			EIN	condition reed contact leakage diagnosis pump
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRSSA			EIN	LRSEB: switch onLambda after fuel cut off with slow sensor
B_LRSSA2			EIN	switch onLambda after fuel cut off with slow sensor, bank2
B_M8TE	TC8MOD		EIN	condition to enable function evap system by SAE J1879 Mode 8 TID \$01
B_MASTERHW			EIN	Condition Master-SG corresponding with code-pin (plausible)
B_MLRSA	LREB		EIN	LRSEB: Air mass based switch off Lambda Control during and after fuel cut off
B_QTEDAB	TEBEB		AUS	condition fast decrementation of purge rate
B_SBBVK	DLSV		EIN	condition for lambda sensor upstream cat ready for operation
B_SBBVK2	DLSV		EIN	condition oxygen sensor upstream cat. bank2 ready for operation
B_SLS	AK		EIN	Condition for active secondary air
B_TE	TEBEB		AUS	Condition canister purge active
B_TEF	TEBEB		AUS	Condition canister purge function principally released
B_TEI	TEBEB		AUS	Internal condition: canister purge function active
B_TEIC			EIN	Internal condition: canister purge function active (CAN-variable)
B_TEN	TEBEB		AUS	condition open loop purging
B_TENC			EIN	condition open loop purging, input from CAN
B_TEP	GKEB		EIN	Condition canister purge phase active
DFP_AAVE	TEBEB		DOK	ECU int. fault path no.: diagnosis AAVE valve power stage
DFP_DK	TEBEB		DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_LDPE	TEBEB		DOK	ECU int. fault path no.: leakage detection pump power stage
DFP_TEVE	TEBEB		DOK	Internal fault path number: canister purge valve power stage
E_AAVE			EIN	error flag: canister ventilation valve (power stage)
E_DK	DDVE		EIN	Error flag: throttle position sensor
E_LDPE			EIN	error flag: leakage detection pump power stage
E_TEVE	DTEVE		EIN	error flag: canister purge valve power stage
LAMSONS_W	LAMSOLL		EIN	required lambda referred to lambda sensor fitting location
SY_AAV	TEBEB		DOK	system constant condition : shut-off-valve available
TATESOLL	GKRA		EIN	desired duty cycle of the PCV
TMOT	SWADAP		EIN	Engine temperature

## FW TEBEB 6.20 Fixed Values

Parameter	Value	Description
TMTE		engine-temperature threshold for canister purge
TTEAUS		Delay time after engine start for activating the purge control valve



## FB TEBEB 6.20 Detailed description of function

Concept of purge control with 2 control units:

- This TEBEB is designed for a 2 ECU concept. It will operate identically in the master ECU as well as in the slave ECU. So that the operating mode can be distinguished the bit B\_masterhw was introduced. If it is TRUE, then it is the master TEBEB.
- The purge control of both ECUs is to be synchronized so that both PCVs always supply the same quantity of scavenge gas.  
=> Result: The TEB in the master ECU must orient itself according to the activation conditions of the slave.

B\_ten in the master is always set if B\_ten is set in the slave (reading of the CAN signal B\_tenc)  
B\_tei is only set in the master if B\_teic is set

### Description of the Overview:

The function TEBEB contains the enable conditions for purge control. A distinction is made between controlled purge control (Lambda control active - B\_tei = TRUE) and limp-home purge control (Lambda control OFF B\_ten = TRUE).

The TEBEB has the following output values for other functions:

- B\_tef: Principle enabling of the purge control (closed-loop controlled, open-loop controlled)
- B\_tei: Enabling of controlled purge control for opening control
- B\_te: PCV is (still) open due to triggering by TEB
- B\_ten: Limp-home purge control (Lambda control of both banks OFF)
- B\_qtedab: Quick closing control of the PCV for diagnostic functions

There are 2 partial functions: TEBPF (principle enabling) and TEBNL (enabling of limp-home). The bits B\_tei and B\_te are defined in the overview:

- B\_tei: B\_tei can only be set to TRUE if simultaneously B\_tep, B\_tef and either B\_lr or B\_lr2 (with stereo LC) is active. Furthermore B\_teic (B\_tei of the slave) must set in the master ECU.

Remark: B\_tep also already contains the inquiry for B\_dldpte, B\_dtes and B\_dllr  
In order to be able to perform deactivation at controlled purge control it must be possible to set B\_tef separately to FALSE when one of the diagnostic functions is requested.

- In contrast to B\_tei, B\_te is also TRUE if tatesoll > 0. => B\_te indicates that the PCV is open during normal purge control operation. At open PCV due to DTEV, B\_te = FALSE. This is achieved by inquiry of B\_dteaa. This is necessary so that the learning of the saturation is prohibited in TEB.

### Description of the Partial Function TEBPF (Principal Enabling of Purge Control):

Purge control is principally enabled if

- the engine temperature is above the threshold TMTE and if
- no condensed water exists in the exhaust-system branch (B\_atmtpa = TRUE) and if the time TTEAUS has elapsed.
- the following faults and conditions are not given:
  - B\_sls: Secondary air active
  - B\_dsls: Diagnosis secondary air active
  - B\_ftedab: Diagnosis purge control system
  - B\_dllra: Condition for request close PCV by idle controller diagnosis
  - B\_fraoan: With not learned adaptation in FRAO region
  - B\_dldpte: Condition for request close PCV by diagnostic function leak diagnosis pump
  - B\_lamsdef: Active diagnosis Lambda sensor operates. If the bit B\_lamsdef is set due to catalyst deoxidation, the PCV is not controlled close during normal running.
  - E\_teve: Fault diagnosis PCV output stage, if B\_ldpi = False and LDP output stage fault
  - E\_dk: Fault throttle valve sensor
  - E\_ldpe: Fault output stage LDP, if B\_ldpi = False and no AAV exists
  - B\_m8te: Mode 8 active

### Description of the Partial Function TEBNL (Enabling of Purge Control, Limp-home Purge Control):

B\_ten is only TRUE if the purge control is principally enabled and if the following conditions are fulfilled:

- Neither sensor bank 1 nor sensor bank 2 is ready for operation!(B\_sbbvk V B\_sbbvk), or if no Lambda control (bank1 or bank2) is active and if the purge control phase is active and lamsons\_w is unequal to 1.0, or if an OBDII total fault is given, which prohibits the Lambda control (e.g. secondary air fault)
- Sufficient air mass was put through after fuel cut-off so that the Lambda control is activated again. Thereby it is prevented that e.g. during a purge control phase the PCV opens shortly after fuel cut-off.
- B\_lrssa(2): Activation condition of the Lambda controller after fuel cut-off with slow sensor
- The Lambda controller is blocked for an active diagnosis of Lambda sensor and a testing function is started. In this case LIMP-HOME purge control is to be prohibited.
- B\_eobdlr: OBDII total fault Lambda controller is blocked
- B\_lamsdef = FALSE: Thereby it is prevented that e.g. the purge rate is strongly reduced at controlled catalyst deoxidation
- The bit B\_ten is set in the master even if the bit B\_tenc has been set.



## APP TEBEB 6.20 Application hint

Engine temperature - activation threshold: TMTE

- \* the lower, the earlier the TEB becomes active, the more purging can be performed
  - \* the higher, the less are the exhaust-gas influences of the TEB at cold catalyst
- => Compromise: TMTE about 40 - 50 degrees

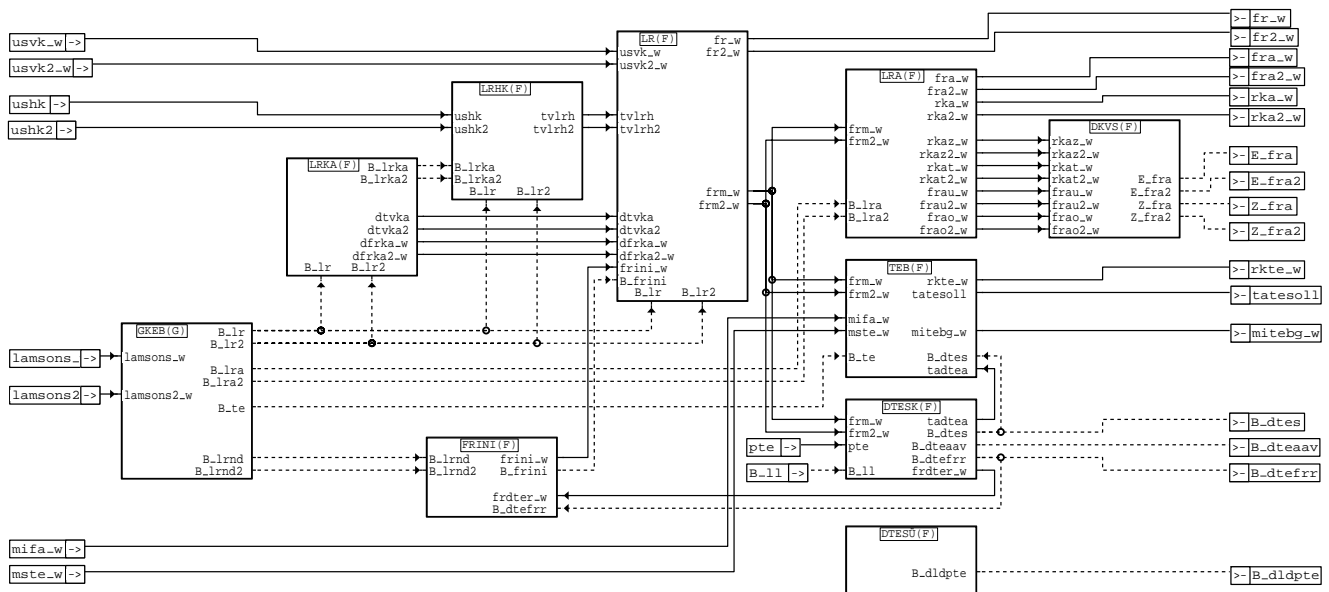
Off-time for purge control after start: TTEAUS

- \* Reason: During a hot start the pre-control may at first be too lean, fr must enrich so that the saturation ftead does not unlearn itself the purge control is not enabled immediately after start.
- => Guidance value: TTEAUS about 10s - 20s

## GKRA 3.0 Mixture control and adaptive pilot control

### FDEF GKRA 3.0 Function definition

Overview Mixture Control and Adaptation:



### gkra-gkra

### ABK GKRA 3.0 Abbreviations

Variable	Source	Type	Description
B_DLDPTE	GKRA	AUS	request from evap system monitoring to shut down PCV
B_DTEAAV	GKRA	AUS	canister vent valve closed
B_DTEFRR	GKRA	AUS	condition of lambda controller reset
B_DTES	GKRA	AUS	Condition for active diagnosis of canister purge system
B_FRINI	GKRA	LOK	Condition control factor fr initialize
B_LL	MSF	EIN	Condition idle
B_LR	GKRA	LOK	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	GKRA	LOK	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRA	GKRA	LOK	condition for basic mixture adaptation enabled
B_LRA2	GKRA	LOK	condition for basic mixture adaption 2 enabled
B_LRKA	GKRA	LOK	condition for neutralization of catalyst oxygen storage
B_LRKA2	GKRA	LOK	condition for neutralization of catalyst oxygen storage, cylinder row 2
B_LRND	GKRA	LOK	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_LRND2	GKRA	LOK	set control bit LR activ; request for "NORMAL" or "DIAGNOSIS"
B_TE	GKRA	LOK	Condition canister purge active
DFRKA2_W	GKRA	LOK	delta-fr for open loop catalyst oxygen neutralization, bank 2
DFRKA_W	GKRA	LOK	delta-fr for open loop catalyst oxygen neutralization
DTVKA	GKRA	LOK	delta-tv for catalyst oxygen neutralization
DTVKA2	GKRA	LOK	delta-tv for catalyst oxygen neutralization for 2nd bank of stereo lambda contr.
E_FRA	GKRA	AUS	error flag: multiplicative mixture adaptation factor fra
E_FRA2	GKRA	AUS	error flag: multiplicative mixture adaption factor fra2
FR	GKRA	LOK	Lambda controller output
FR2_W	GKRA	AUS	Lambda controller output (word)
FRA	GKRA	LOK	multiplicative mixture adaptation factor
FRA2_W	GKRA	AUS	multiplicative correction of the mixture adaptation (word)
FRAO2_W	GKRA	LOK	multipl. mixture adaptation factor higher load bank 2 (Word)
FRAO_W	GKRA	LOK	multipl. mixture adaptation factor higher load (word)
FRAU2_W	GKRA	LOK	multipl. mixture adaptation factor of the lower mult. section of bank 2 (Word)
FRAU_W	GKRA	LOK	multipl. mixture adaptation factor of the lower mult. section (Word)



Variable	Source	Type	Description
FRA_W	GKRA	AUS	multiplicative correction of the mixture adaptation (word)
FRDTER_W	GKRA	LOK	lambda control factor as reference value for CPV diagnosis
FRINL_W	GKRA	LOK	Initialisation value for control factor lambda control
FRM2_W	GKRA	LOK	fast mean value of lambda control factor bank 2(word)
FRM_W	GKRA	LOK	fast mean value of lambda control factor (word)
FR_W	GKRA	AUS	Lambda controller output (word)
LAMSONS2_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location
MIFA_W	MSF	EIN	desired indicated engine torque
MITEBG_W	GKRA	AUS	torque value for minimum charge canister purge
MSTE_W	BGTEV	EIN	mass flow purge control into the manifold
PTE	GGDST	EIN	tank pressure (from ADC)
RKA2_W	GKRA	AUS	additive adaptive correction of the relative fuel amount bank 2
RKAT2_W	GKRA	LOK	additive correction (per time) of the mixture adaptation bank 2 (Word)
RKAT_W	GKRA	LOK	additive correction (per time) of the mixture adaptation (Word)
RKAZ2_W	GKRA	LOK	additive correction (per ignition) of the mixture adaptation Bank 2 (Word)
RKAZ_W	GKRA	LOK	additive correction (per ignition) of the mixture adaptation
RKA_W	GKRA	AUS	additive adaptive correction of the relative fuel amount
RKTE_W	GKRA	AUS	relative fuel part of the purge control
TADTEA	GKRA	LOK	TEV duty cycle from canister purge diagnosis
TATESOLL	GKRA	AUS	desired duty cycle of the PCV
TVLRH	GKRA	LOK	LRHK: correction value for delayed controller switch tv
TVLRH2	GKRA	LOK	LRHK: correction value for delayed controller switch tv 2
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
USVK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst
Z_FRA	GKRA	AUS	cycle flag of mixture adaption factor fra
Z_FRA2	GKRA	AUS	cycle flag: Lambda adaptation multiplicative (bank 2)

### FW GKRA 3.0 Fixed Values

Parameter	Value	Description
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### FB GKRA 3.0 Detailed description of function

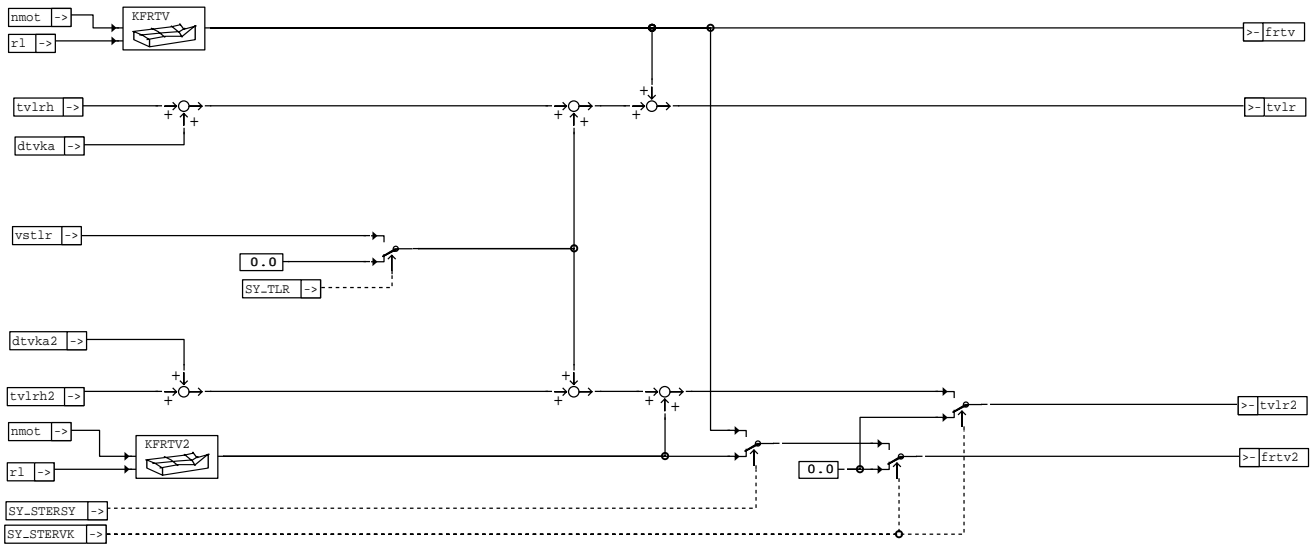
Only for 2-step Lambda control !!!

Overview of Lambda control, mixture adaptation, purge control, tank diagnosis including the activation conditions.  
Also contains the phase control mixture adaptation / purge control (%BBTEGA in %GKEB).



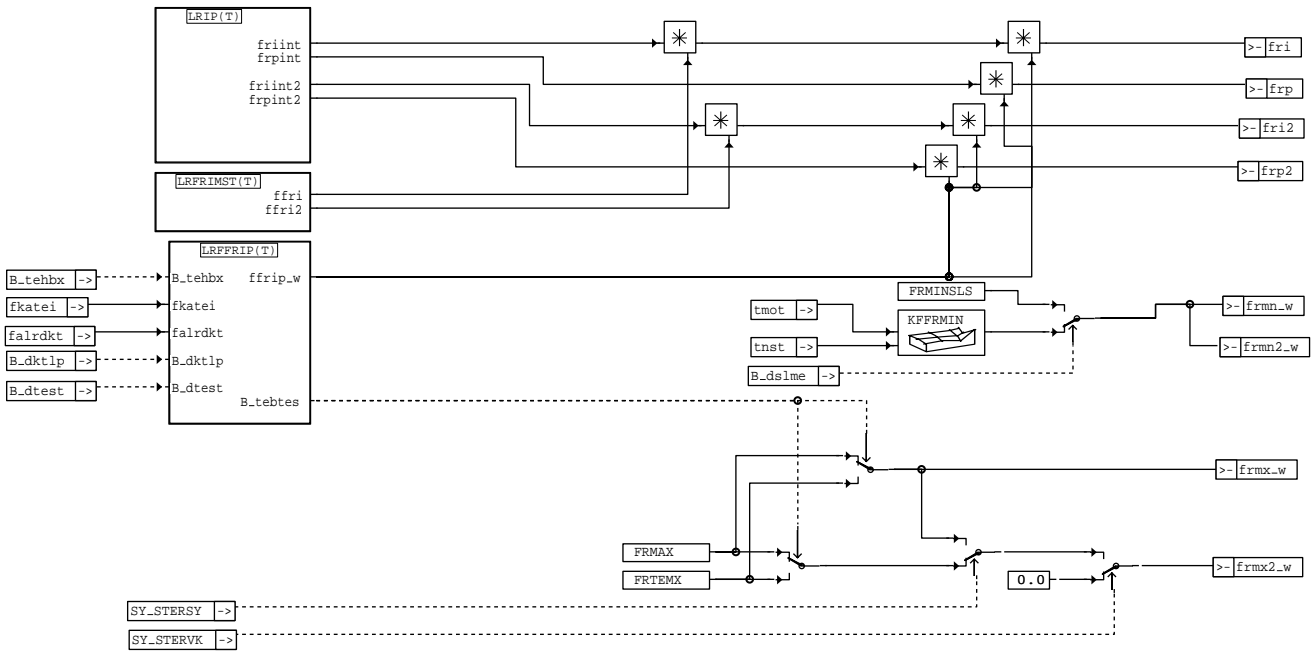


## 1.1 Lambdaregler Bildung Gesamt-tv-Zeit



### Ir-tvIr

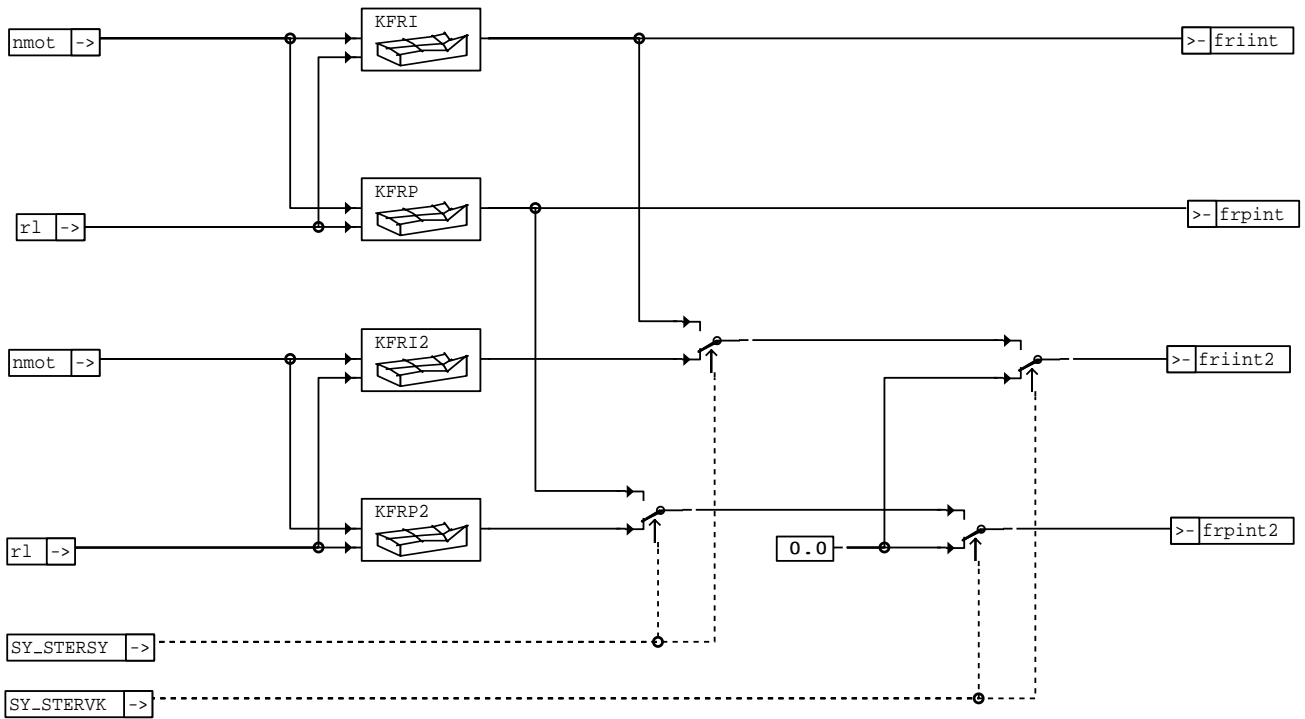
## 1.2 Lambdaregler Bildung funktionsspezifische Integratorsteigung, P-Sprungwert und fr-Begrenzung



### Ir-Irpxsel

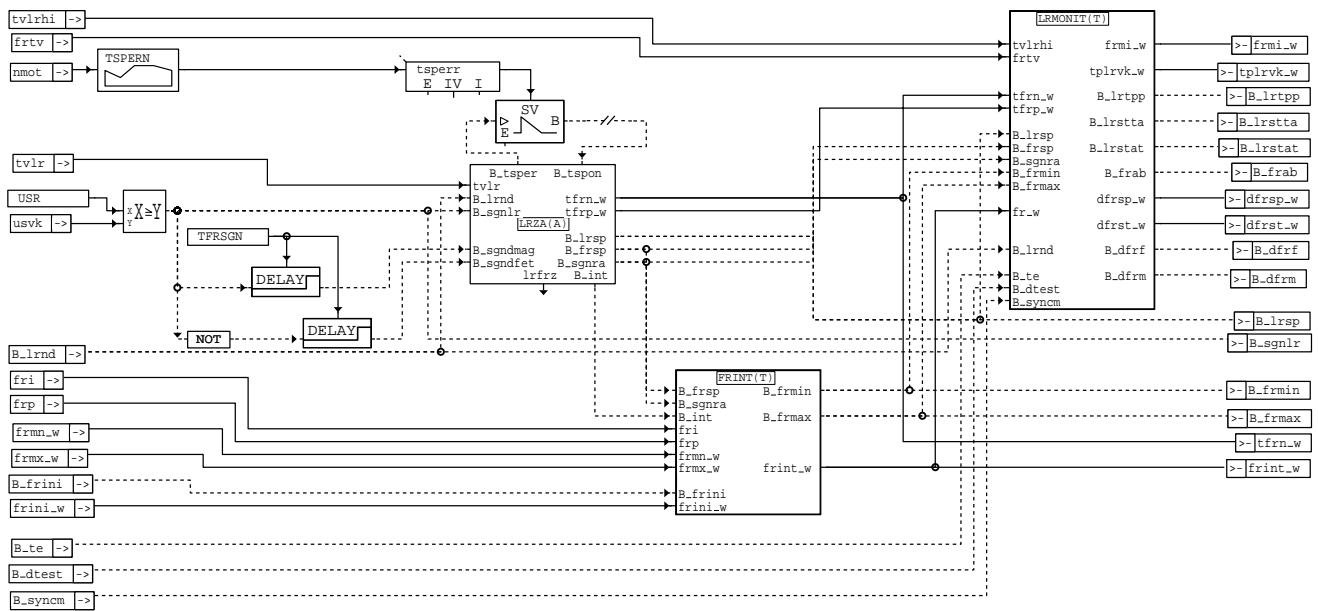


## 1.2.1 Lambdaregler Bildung bankspezifische Integratorsteigung, P-Sprungwert



Ir-Irip

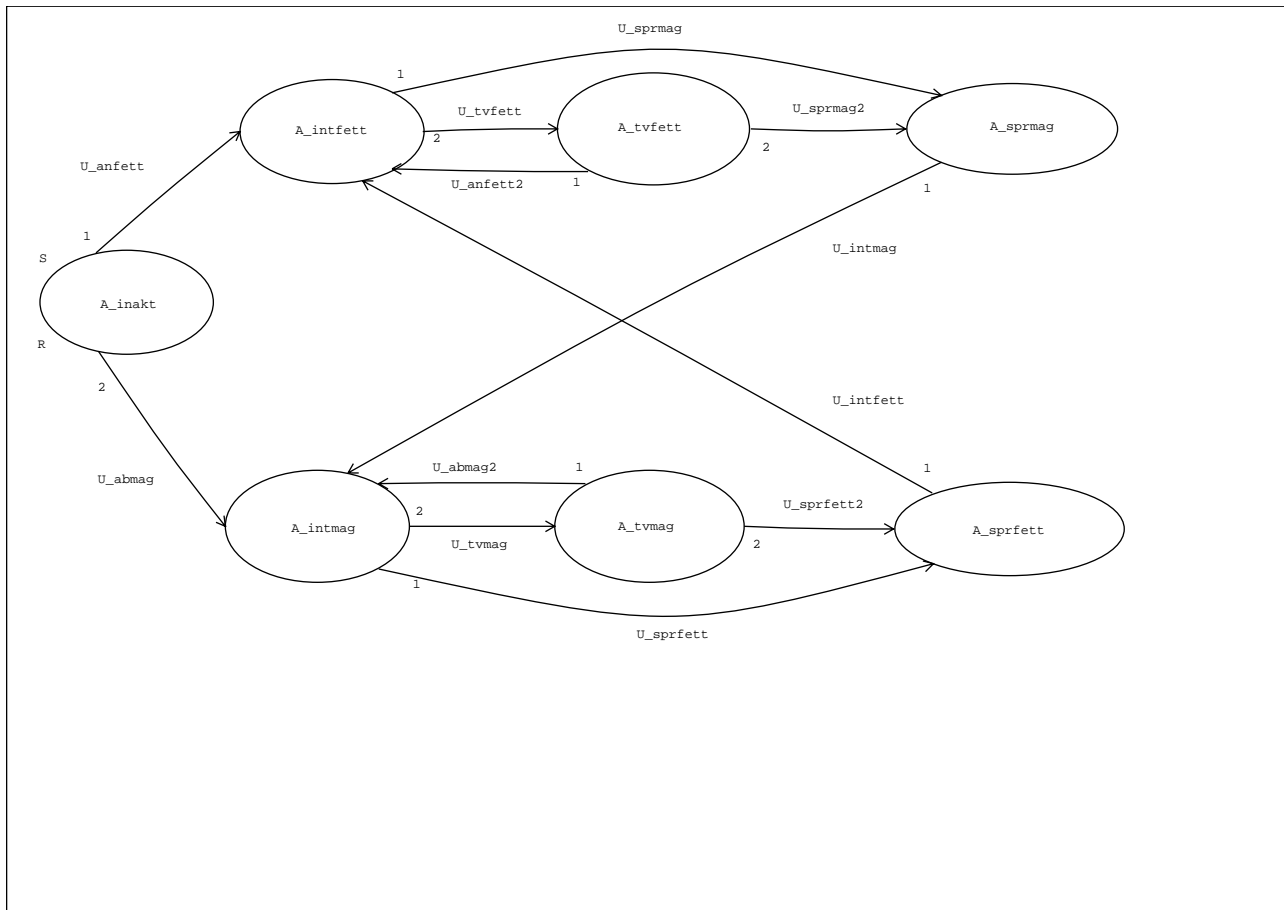
## 2. Lambdaregler Basisstruktur Bank 1



Ir-IrBank1



2.1 Lambdaregler Automat zur Steuerung von Integrieren, P-Sprung und tv-Zeit



lr-lrza

Zustand	Übergangsname	+ - Übergangsbedingung
V	V	V
	Aktionen	+ - Aktions-Code
V	V	V

```

A_inakt
Reset-Bedingung: B_lrnd = false
-- Dies ist der Reset-Zustand, er wird aus allen
Zuständen angesprungen, wenn die Reset-Bedingung
erfüllt ist.

Entry: lrfrz := 0;
Exit: tv := 0.0;
      B_sgnra := B_sgnlr;
      -- Initialisierung von Variablen,
      -- damit Division durch Null vermieden wird

      tfrnint_w := 1.0;
      tfrpint_w := 1.0;
      tfrn_w := 1.0;
      tfrp_w := 1.0;

U_anfett: -- Lambdaregelung freigegeben, Sonde erkennt mageres Gemisch
          B_lrnd and B_sgnlr
Action: -- Sondensprung bei Start
        B_lrsp := true;

U_abmag: -- Lambdaregelung freigegeben, Sonde erkennt fettes Gemisch
          B_lrnd and not B_sgnlr
Action: -- Sondensprung bei Start
        B_lrsp := true;

-----
A_intfett
Entry: -- Beginn des Integrierens
      B_int := true;
      -- Reset der positiven Integrierzeit
      tv := 0;

- Reset tv-Zeit
      tfrpint_w := 0;
      lrfrz := 1;
Action: -- Flag-Bit Sondensprung rücksetzen
      B_lrsp := false;
      -- Berechnung der Integrierzeit
    
```



```

tfrpint_w := tfrpint_w + dT;
Exit:
    B_int := false;
    tfrp_w := tfrpint_w;
    B_tsper := true;
    B_sgnalt := B_sgnlr;
U_sprmag:
    -- Signal fett, Sperrzeit abgelaufen, keine Fettverschiebung:
    (B_sgnlr = false) and (B_tspon = false) and (tvlr <= 0)
    Action:
        -- Sondensprung erkannt
    B_lrsp := true;
U_tvtfett:
    -- Signal fett, Fettverschiebung gewünscht:
    (B_sgnlr = false) and (B_tspon = false) and (tvlr > 0)
    Action:
        -- Sondensprung erkannt
        B_lrsp := true;
-----
A_tvtfett
Entry:
    tv := tvlr - dT;
    lrfrz := 2;
    Action:
        -- Flag-Bit Sondensprung rücksetzen
        B_lrsp := false;
        -- Abregelung der tv-Zeit:
        tv := tv - dT;
        -- Setzen der Sperrzeit, wenn Vorzeichenwechsel
        IF (B_sgnalt <> B_sgnlr) THEN
            B_tsper := true;
        ELSE
            B_tsper := false;
        ENDIF;
        B_sgnalt := B_sgnlr;
U_anfett2:
    -- Verzögerungszeit abgelaufen, aber Sonde sieht wieder mager
    (tv <= 0) and (B_sgnlr) or B_sgndmag
U_sprmag2:
    -- Verzögerungszeit abgelaufen:
    (tv <= 0)
    Action:
        B_lrsp := FALSE;
-----
A_sprmag
Entry:
    B_frsp := true;
    B_sgnra := false;
    lrfrz := 3;
    Action:
        -- fr-Sprung erlaubt
        -- Vorzeichen für Sprung und Integration setzen
Exit:
    B_frsp := false;
    B_lrsp := false;
    B_tsper := false;
    true
    Action:
        -- fr-Sprung durchgeführt
        -- Flag-Bit Sondensprung rücksetzen
        -- Bedingung Starten der Sperrzeit zurücksetzen
U_intmag:
    true
-----
A_intmag
Entry:
    B_int := true;
    tv := 0;
- Reset tv-Zeit
    tfrnint_w := 0;
    lrfrz := 4;
    Action:
        B_lrsp := false;
        -- Flag-Bit Sondensprung rücksetzen
Exit:
    tfrnint_w := tfrnint_w + dT;
    B_int := false;
    tfrn_w := tfrnint_w;
    B_tsper := true;
    B_sgnalt := B_sgnlr;
U_sprfett:
    -- Signal mager, Sperrzeit abgelaufen, keine Magerverschiebung:
    (B_sgnlr = true) and (B_tspon = false) and (tvlr >= 0)
    Action:
        -- Sondensprung erkannt
    B_lrsp := true;
U_tvvmag:
    -- Signal mager, Magerverschiebung gewünscht:
    (B_sgnlr = true) and (B_tspon = false) and (tvlr < 0)
    Action:
        -- Sondensprung erkannt
        B_lrsp := true;
-----
A_tvvmag
Entry:
    -- Setzen der Verzögerungszeit

```



```

tv := -(tvlr + dT);
lrfrz := 5;

Action:
    B_lrsp := false;
    tv := tv - dT;
    IF (B_sgnalt <> B_sgnlr) THEN
        B_tsper := true;
    ELSE
        B_tsper := false;
    ENDIF;
    B_sgnalt := B_sgnlr;
    -- Verzögerungszeit abgelaufen, aber Sonde sieht wieder fett
U_abmag2:
    (tv <= 0) and (not B_sgnlr) or B_sgndfet
U_sprfett2:
    -- Verzögerungszeit abgelaufen:
    (tv <= 0)

Action:
    B_lrsp := FALSE;
    
```

```

-----
A_sprfett
Entry:
    B_frsp := true;
    B_sgnra := true;
    lrfrz := 6;
    -- Sprung erlaubt
    -- Vorzeichen für Sprung und Integration setzen

Exit:
    B_frsp := false;
    B_lrsp := false;
    B_tsper := false;
    true
    -- Sprung durchgeführt
    -- Flag-Bit Sondensprung rücksetzen
    -- Bedingung Starten der Sperrzeit zurücksetzen
    
```

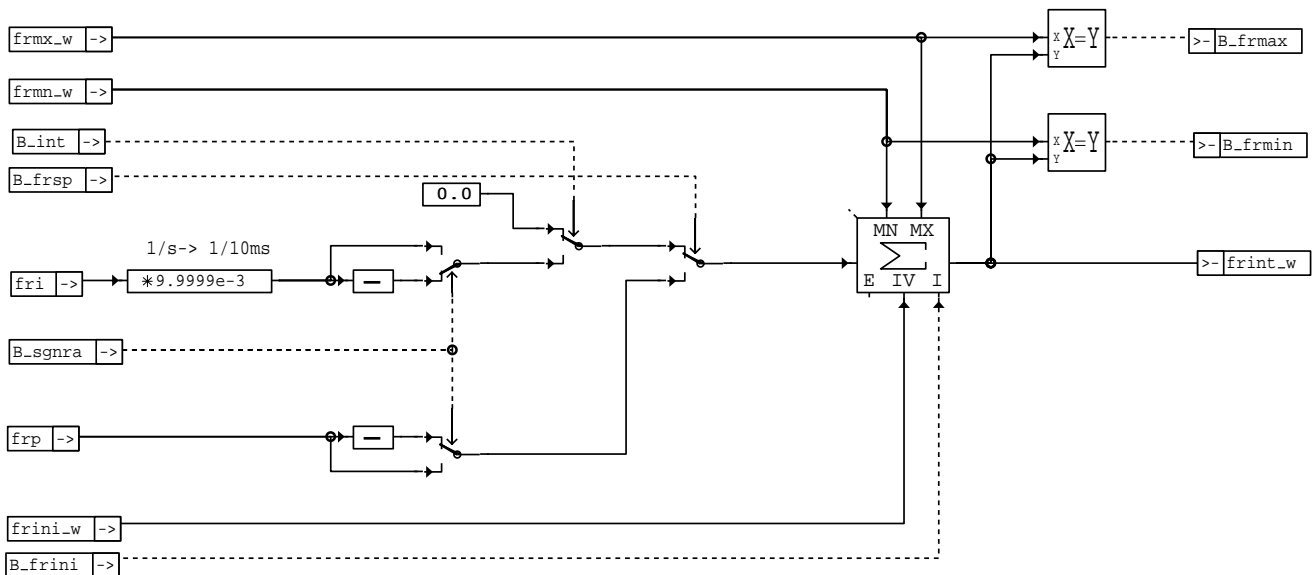
```

-----
Lokale Variablen:
Float tv := 0.0;      -- [s]
Float tfrpint_w := 0.0;

Float tfrnint_w := 0.0;

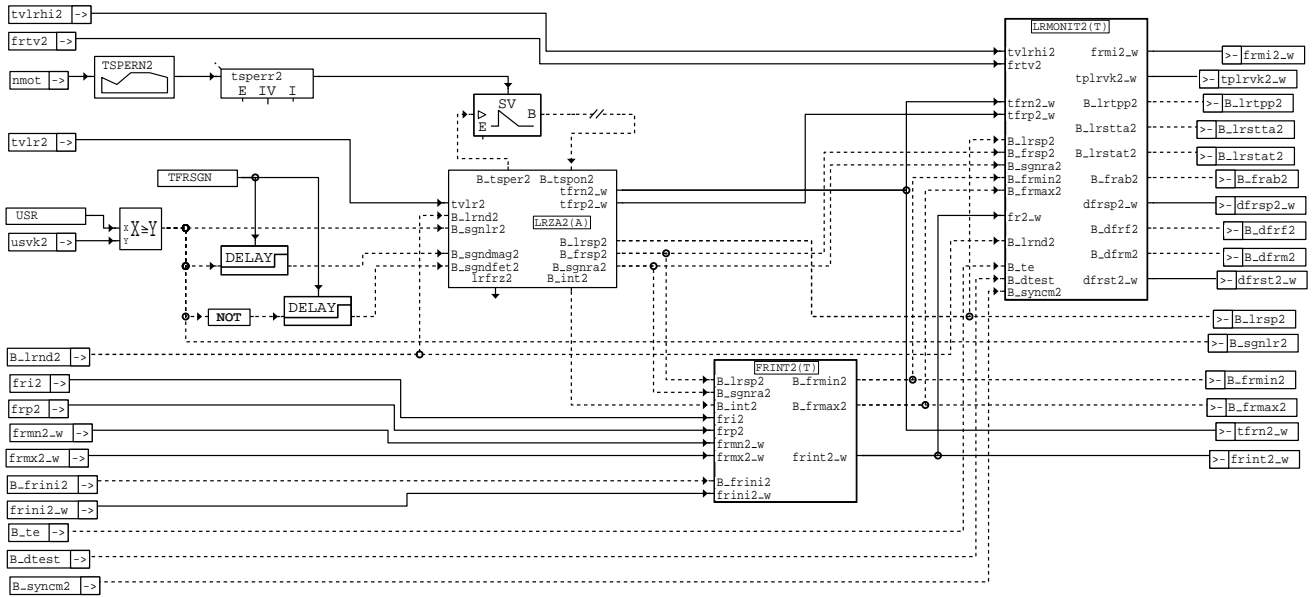
Bool B_sgnalt := false;
    
```

## 2.2 Lambdaregler Bildung des internen Reglerfaktors frint\_w



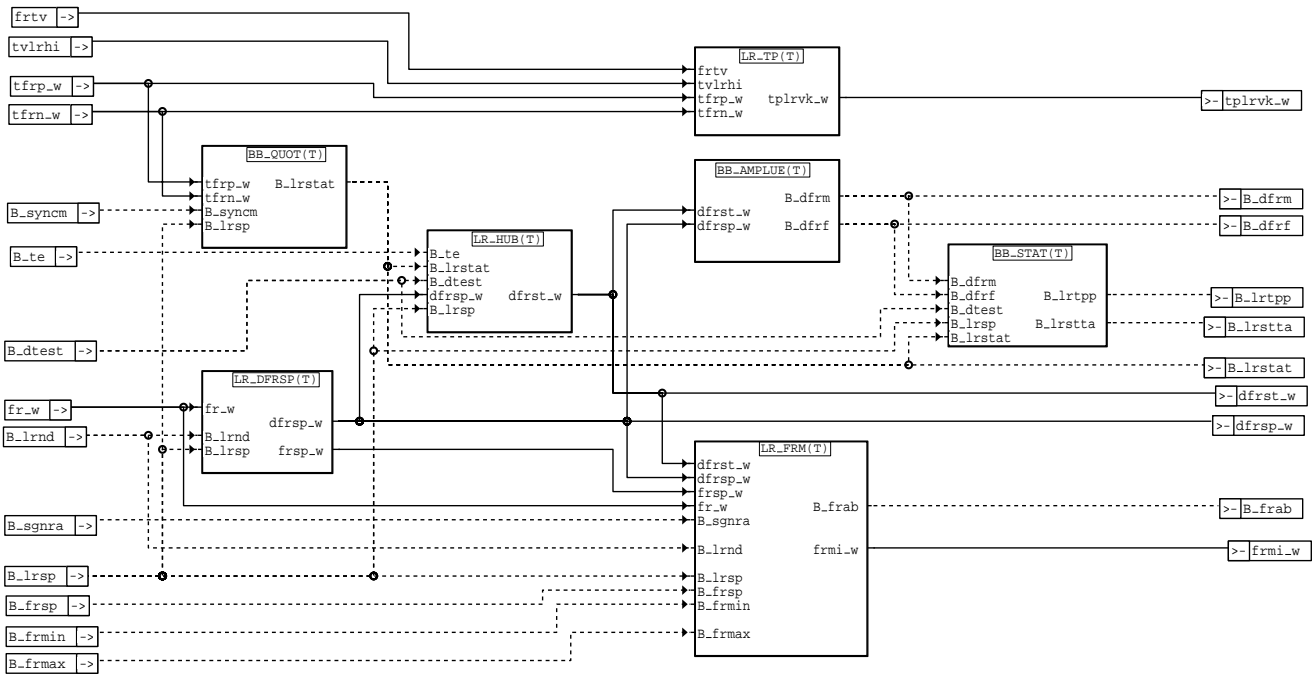
## Ir-frint

## 3. Lambdaregler Basisstruktur Bank 2



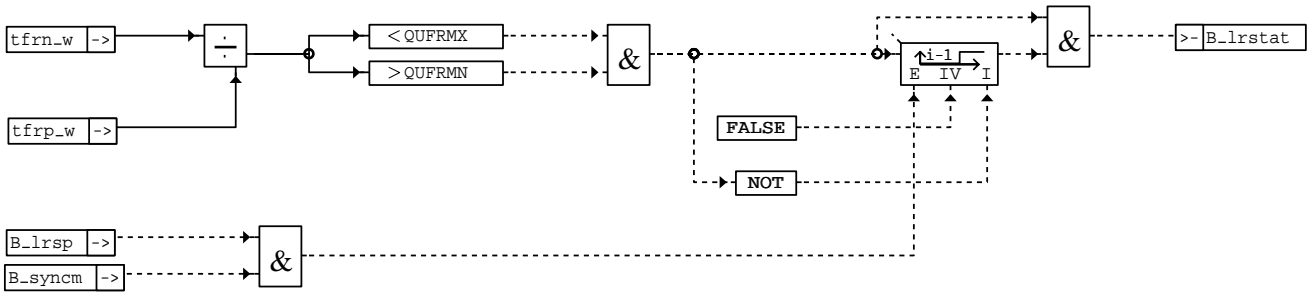
**Ir-Irbank2**

4. Lambdaregler Übersicht Basisblöcke zur Ermittlung Stationärbedingung, fr-Mittelwert fr<sub>w</sub> und Periodendauer



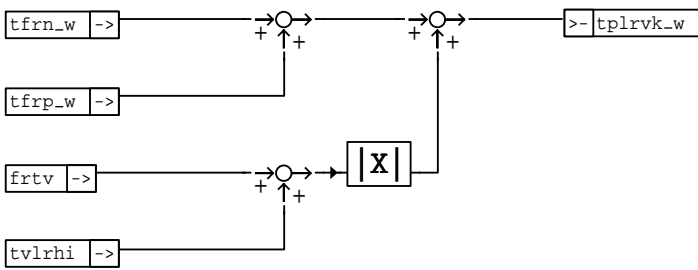
**Ir-Irmonit**

#### 4.1 Lambdaregler Ermittlung zeitbasierte Stationärbedingung



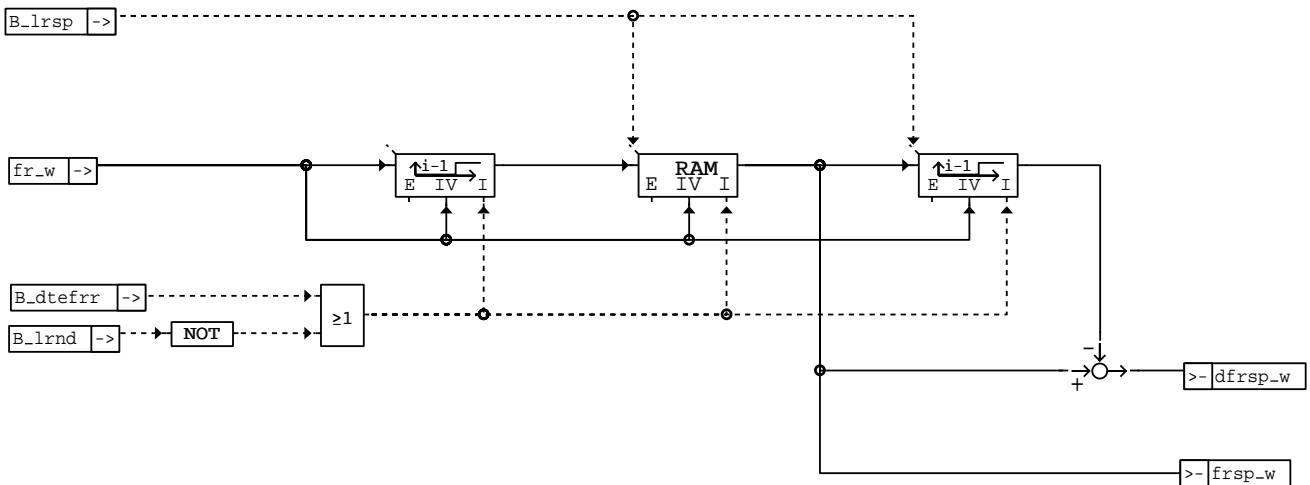
#### lr-bb-quot

#### 4.2 Lambdaregler Berechnung Periodendauer von fr



#### lr-lr-tp

#### 4.3 Lambdaregler Bildung aktueller Regelhub dfrps\_w

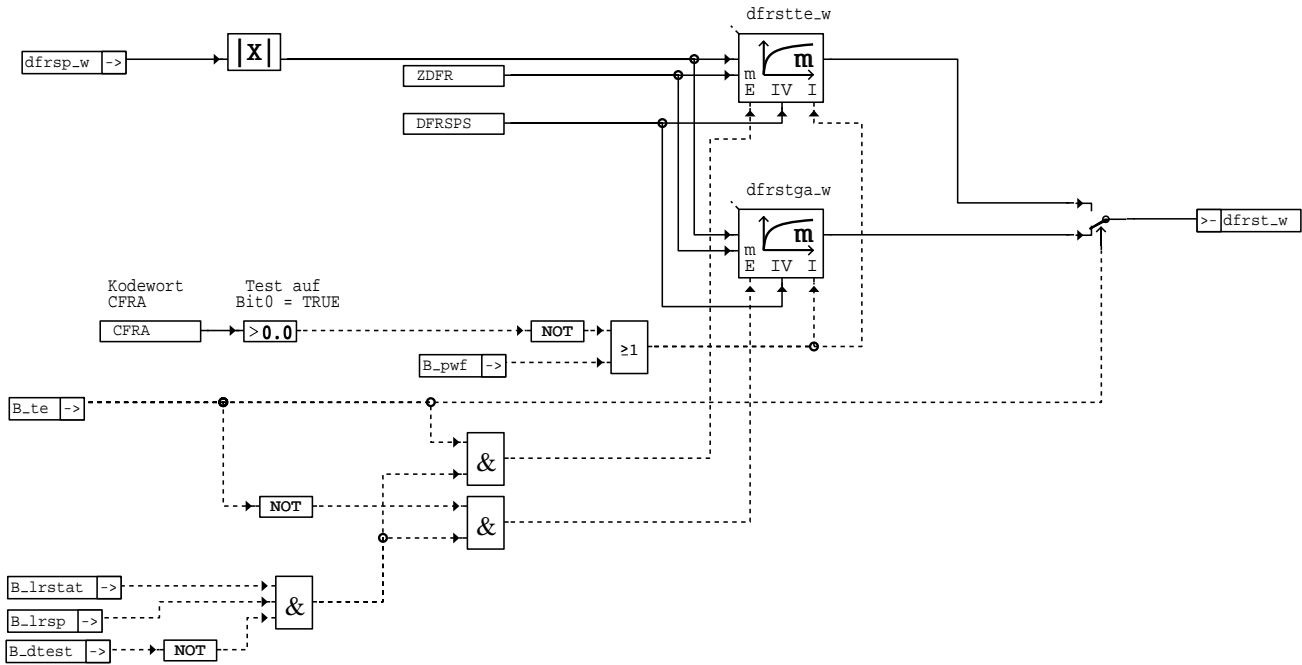


#### lr-lr-dfrsp



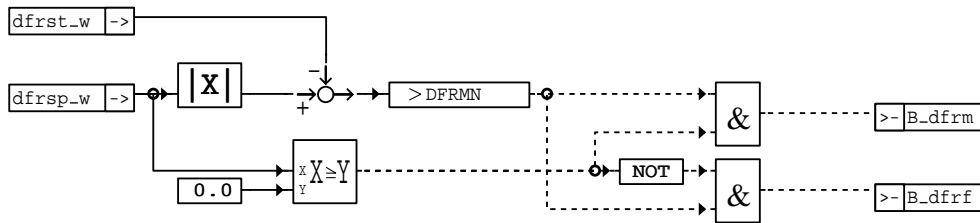


#### 4.5 Lambda regler Ermittlung amplitudenbasierte Stationärbedingung, Adaption Reglerhub



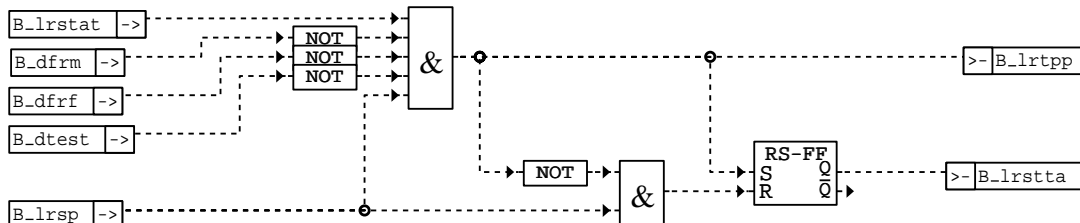
#### Ir-Ir-hub

#### 4.6 Lambda regler Erkennung Amplitudenüberschreitung



#### Ir-bb-amplue

#### 4.7 Lambda regler Ausgabe Status gültige Periodendauer und Stationärbedingung Zeit/Amplitude



#### Ir-bb-stat

#### ABK LR 89.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CFRA			FW	code word for adaptation of control amplitude
CWLRSYNC			FW	Code word: Selects bank1 or bank2 as master during fr-synchronization
DFRNM			FW	min. lambda deviation for steady state cond. and adaptation of transient contrl.
DFRSPS			FW	stroke of A/F ratio controller signal (standard value)
DLRPERIMN			FW	
DLRPERIMX			FW	



Parameter	Source-X	Source-Y	Type	Description
FFRITMS	TMST		KL	tmst dependent factor to modify I-dynamic of lambda control
FLRFKATE	FKATEI		KL	Rating of factor fkatei from %TEB to optimize the regulation parameter
FLRM	TMOT		KL	Engine temperature dependent factor to modify I-dynamic of lambda control
FRIPDSL1			FW	Factor adjustment of fri and frp during active phase 1 of DSLSLR
FRIPDSL4			FW	Factor adjustment of fri and frp during active phase 4 of DSLSLR
FRIPDTE5			FW	Factor adjustment of fri and frp during active DTEV
FRIPTE5			FW	Factor adjustment of fri and frp at fault "open TEV pinch"
FRMAX			FW	upper limit of control range
FRMINSL5			FW	lower control range limit during phas1 of secondary air system diagnosis
FRTEMX			FW	upper limit of control range on error "cannister purge valve open"
KFFRMIN	TMOT	TNST	KF	lower limit of control range
KFRI	NMOT	RL	KF	I characteristic map
KFRI2	NMOT	RL	KF	LR-I-Map for bank 2
KFRP	NMOT	RL	KF	P characteristic map
KFRP2	NMOT	RL	KF	LR-P MAP for bank 2
KFRTV	NMOT	RL	KF	delay time characteristic map
KFRTV2	NMOT	RL	KF	delay time characteristic map
KLRSYNIN	NMOT		KL	
KLRSYNPN	NMOT		KL	
QUFRMN			FW	lower limit for static condition of lambda controller
QUFRMX			FW	upper limit for static condition of lambda controller
TFRSGN			FW	
TSPERN	NMOT		KL	lock time for p-offset after lambda sensor voltage jump
TSPERN2	NMOT		KL	lock time for p-offset after lambda sensor voltage jump, bank 2
USR			FW	controller theshold for lambda control upstream catalyzt
ZDFR			FW	filter constant for calc. of A/F ratio contr. stroke mean value
ZLRFRI			FW	Time constant for ingreasing of tmst depending weighting factor FFRITMS

Variable	Source	Type	Description
B_ATMTPA	ATM	EIN	condition temperature upstream catalyzt exceeds dew-point
B_ATMTPA2	ATM	EIN	condition temperature upstream catalyzt exceeds dew-point2
B_DFRF	LR	AUS	rich deviation by %LR detected
B_DFRF2	LR	AUS	rich deviation by %LR detected, bank2
B_DFRM	LR	AUS	lean deviation by %LR detected
B_DFRM2	LR	AUS	lean deviation by %LR detected, bank2
B_DKTLP	DKAT	EIN	Request of parameter switch over in lambda control
B_DSL1		EIN	Diagnosis phase 1: secondary air mass
B_DSL4		EIN	Condition phase 4: secondary air mass adaptation/ add. diagnosis
B_DSLME		EIN	diagnosis secondary air mass, enable measurement
B_DTEFRFR	GKRA	EIN	condition of lambda controller reset
B_DTEST	DTEV	EIN	condition for start of TEV opening
B_FRAB	LR	AUS	condition fr outside adapted controller range
B_FRAB2	LR	AUS	condition fr outside adapted controller range, bank 2
B_FRINI	LRINI	EIN	Condition control factor fr initialize
B_FRINI2	LRINI	EIN	Condition control factor fr initialize, bank 2
B_FRMAX	LR	AUS	lambda control sets bit when lambda controller reaches its limit FRMAX
B_FRMAX2	LR	AUS	lambda control sets bit when lambda control reaches it limit FRMAX, bank2
B_FRMIN	LR	AUS	lambda control sets bit when lambda controller reaches its limit FRMIN
B_FRMIN2	LR	AUS	lambda control sets bit when lambda control reaches its limit FRMIN, bank2
B_FRMINI	LR	LOK	condition for initialize frm
B_FRMINI2	LR	LOK	condition for initialize frm bank 2
B_FRSP	LR	LOK	Flag controller factor fr is jumping
B_FRSP2	LR	LOK	Flag controller factor fr is jumping, Bank 2
B_JNIFRM	LR	LOK	Condition for the choixe of initial value of frm_w
B_JNIFRM2	LR	LOK	Condition for the choixe of initial value of frm_w , bank 2
B_JNT	LR	LOK	LR: Condition Intregation allowed
B_JNT2	LR	LOK	LR: Condition Intregation allowed , bank 2
B_LL	MSF	EIN	Condition idle
B_LRND	LREB	EIN	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_LRND2	LREB	EIN	set control bit LR activ; request for "NORMAL" or "DIAGNOSIS"
B_LRPERF	LR	LOK	Averaging of rich period terminated
B_LRPERM	LR	LOK	Averaging of lean period terminated
B_LRSP	LR	AUS	Flag 'O2 sensor voltage crosses threshold detected'
B_LRSP2	LR	AUS	condition for sensor signal bounce cylinderbench 2
B_LRSTAT	LR	AUS	static condition for lambda controller
B_LRSTAT2	LR	AUS	static condition for lambda controller, bank2
B_LRSTTA	LR	AUS	static condition for lambda controller, time and amplitude
B_LRSTTA2	LR	AUS	static condition for lambda controller, time and amplitude, bank2
B_LRSTTAMA	LR	LOK	static condition for lambda controller master, time and amplitude
B_LRSYINH	LR	AUS	Condition fr_b1-/fr_b2-synchronization due to min/max limiter disabled
B_LRSYNB1	LR	LOK	Condition fr_b1-/fr_b2-synchronization active, bank 1 is master
B_LRSYNC	DKAT	EIN	Condition fr_b1-/fr_b2-synchronization requested
B_LRSYNI	LR	LOK	Condition fr_b1-/fr_b2-synchronization active, local
B_LRTPP	LR	AUS	Periodic time valid, static cond. for %LR (amplitude/periodic time) = TRUE
B_LRTPP2	LR	AUS	static condition for lambda controller (amplitude/periodic time) bank2
B_PWF		EIN	Condition for powerfail
B_SBBVK	DLSV	EIN	condition for lambda sensor upstream cat ready for operation
B_SBBVK2	DLSV	EIN	condition oxygen sensor upstream cat. bank2 ready for operation
B_SBBVKSL	LR	LOK	condition for lambda sensor upstream cat ready for operation, slave bank
B_SGNALT	LR	LOK	Indication of rich / lean mixture pre cat, 1 slot retarded
B_SGNALT2	LR	LOK	Indication of rich / lean mixture pre cat, 1 slot retarded



Variable	Source	Type	Description
B_SGNDFET	LR	LOK	
B_SGNDFET2	LR	LOK	
B_SGNDMAG	LR	LOK	
B_SGNDMAG2	LR	LOK	
B_SGNLR	LR	AUS	calculation sign for mixture upsteam cat (Bool)
B_SGNLR2	LR	AUS	calculation sign for mixture upsteam cat (Bool), bank 2
B_SGNRA	LR	LOK	Indication of rich / lean mixture pre cat due to delay time control
B_SGNRA2	LR	LOK	Indication of rich / lean mixture pre cat due to delay time control bank2
B_SYNCM	LR	AUS	Condition fr_w/fr2_w-synchronization active, fr_w is used as master
B_SYNCM2	LR	AUS	Condition fr-synchronization active,bank 2 is used as master
B_TE	TEBEB	EIN	Condition canister purge active
B_TEBTES	LR	LOK	Dynamic manipulation of i and p part activated by B_tehbx or B_dtes
B_TEBHX	TEB	EIN	Condition load integrator ftead at max. limit
B_TSPER	LR	LOK	LR: Condition Start of delay time
B_TSPER2	LR	LOK	LR: Condition Start of delay time, bank 2
B_TSPON	LR	LOK	Condition of start of delay time in LR for signal interference elimination
B_TSPON2	LR	LOK	Condition of start of delay time in LR for signal interference elimination,bank2
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DFRSP2_W	LR	AUS	delta peak value lambda control factor frsp bank 2
DFRSP_W	LR	AUS	delta peak value lambda control factor frsp
DFRST2_W	LR	AUS	A/F ratio controller output stroke in steady-state condition (cylinderbench 2)
DFRSTGA2_W	LR	DOK	controller output stroke in steady-state condition (basic adaptation), bank 2
DFRSTGA_W	LR	DOK	controller output stroke in steady-state condition (basic adaptation)
DFRSTTE2_W	LR	DOK	controller output stroke in steady-state condition (canister purge), bank 2
DFRSTTE_W	LR	DOK	controller output stroke in steady-state condition (canister purge)
DFRST_W	LR	AUS	A/F ratio controller output stroke (steady-state condition)
DLRPERI_W	LR	LOK	
DLRPERP_W	LR	LOK	
DLRPER_W	LR	LOK	
DPERMF_W	LR	LOK	
DTVKA	LRKA	EIN	delta-tv for catalyst oxygen neutralization
DTVKA2	LRKA	EIN	delta-tv for catalyst oxygen neutralization for 2nd bank of stereo lambda contr.
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
FALRDKT	DKAT	EIN	Request form cat monitoring: modify lambda controller amplitude
FFRI	LR	LOK	LR with integrator stop: weighing factor I-Slope to compensate slow sensor
FFRI2	LR	LOK	LR with integrator stop: weighing factor I-Slope to compensate slow sensor,bank2
FFRIP_W	LR	LOK	LR with integrator stop: weighing factor I-Slope to compensate slow sensor
FKATEI	TEB	EIN	factor fuel part purge control (actuel value)
FR2_W	LR	AUS	Lambda controller output (word)
FRBAND2_W	LR	LOK	Close loop regulation frm calculation local variable Bank2
FRBAND_W	LR	LOK	Close loop regulation frm calculation local variable Bank2
FRI	LR	LOK	LR with integrator stop: gradient from KFR(n,tL) or corresp. to DSLS
FRI2	LR	LOK	bank2: LR with integrator stop: gradient from KFR(n,tL) or corresp. to DSLS
FRIBAND2_W	LR	LOK	Close loop regulation frm calculation local variable Bank2
FRIBAND_W	LR	LOK	Close loop regulation frm calculation local variable
FRIINT	LR	LOK	gradient from KFRI(nmot,rL) or corresp. to DSLS, local use
FRIINT2	LR	LOK	gradient from KFRI(nmot,rL) or corresp. to DSLS, local use, bank 2
FRINI2_W	LRINI	EIN	Initialisation value for control factor lambda control, bank 2
FRINI_W	LRINI	EIN	Initialisation value for control factor lambda control
FRINT2_W	LR	LOK	Close loop lambda coltrol regulation factor Bank 2 Integrator value
FRINT_W	LR	LOK	Close loop lambda coltrol regulation factor bank 2(word)
FRM2_W	LR	AUS	fast mean value of lambda control factor bank 2(word)
FRMA_W	LR	LOK	Lambda controller output (word), master during synchronisation
FRMI2_W	LR	LOK	Bypass: fast mean value of lambda control factor bank 2(word)
FRMI_W	LR	LOK	Bypass: fast mean value of lambda control factor (word)
FRMMA_W	LR	LOK	fast mean value of lambda control factor (word), master during synchronisation
FRMN2_W	LR	AUS	lambda regulator output min., bank 2
FRMN_W	LR	AUS	lambda regulator output min.
FRMSL_W	LR	LOK	fast mean value of lambda contr. factor (word), for slave during synchronisation
FRMX2_W	LR	AUS	LR bank 2: Maximum limit. of integrator fr;FRMAX increased by DSLS
FRMX_W	LR	AUS	LR with integrator stop:Maximum limit. of integrator fr;FRMAX increased by DSLS
FRM_W	LR	AUS	fast mean value of lambda control factor (word)
FRP	LR	LOK	LR with integrator stop; P-jump from KFRP(n,tL), or DSLS enabled
FRP2	LR	LOK	bank2: LR with integrator stop; P-jump from KFRP(n,tL), or DSLS enabled
FRPINT	LR	LOK	P-part from KFRP(nmot,rL) or corresp. to DSLS, local use
FRPINT2	LR	LOK	P-part from KFRP(nmot,rL) or corresp. to DSLS, local use, bank 2
FRSL_W	LR	LOK	Lambda controller output (word), slave during synchronisation
FRSP2_W	LR	LOK	Lambda close loop control: Regulation factor fr before p-jump bank2/min-value)
FRSP_W	LR	LOK	Lambda close loop control: Regulation factor fr before p-jump
FRTV	LR	LOK	integrator stop from KFRTV(nmot,rL) or corresp. to DSLS
FRTV2	LR	LOK	integrator stop from KFRTV(nmot,rL) or corresp. to DSLS, bank 2
FR_W	LR	AUS	Lambda controller output (word)
LRFRMZ	LR	LOK	Condition byte, Ccreation of fr-mean value frm_w
LRFRMZ2	LR	LOK	Condition byte of calculation Fr-meam value frm_w, Bank2
LRFRZ	LR	LOK	Condition byte of LR-machine
LRFRZ2	LR	LOK	Condition byte of LR-machine , bank2
NMOT	SWADAP	EIN	engine speed
PERMFMA_W	LR	LOK	
PERMFSL_W	LR	LOK	
RL	SWADAP	EIN	relative air charge
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyzt
SY_STERSY	PROKON	EIN	system constant condition stereo lambda control symmetrical



Variable	Source	Type	Description
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
SY_TLR	PROKON	EIN	system constant service device intervention LR, modif. of integrator stop time
TFETTIF_W	LR	LOK	
TFETTIMA_W	LR	LOK	
TFETTIM_W	LR	LOK	
TFETTMA_W	LR	LOK	
TFETTSL_W	LR	LOK	
TFRN2_W	LR	AUS	time duration lambda controller negativ slope, bank 2
TFRNINT2_W	LR	LOK	counter to measure time duration lambda controller negativ slope, bank 2
TFRNINT_W	LR	LOK	counter to measure time duration lambda controller negativ slope
TFRN_W	LR	AUS	time duration lambda controller negativ slope
TFRP2_W	LR	LOK	time duration lambda controller positiv slope, bank 2
TFRPINT2_W	LR	LOK	counter to measure the time duration lambda controller positiv slope, bank 2
TFRPINT_W	LR	LOK	counter to measure the time duration lambda controller positiv slope
TFRP_W	LR	LOK	time duration lambda controller positiv slope
TMAGERMA_W	LR	LOK	
TMAGERSL_W	LR	LOK	
TMAGRIF_W	LR	LOK	
TMAGRIMA_W	LR	LOK	
TMAGRIM_W	LR	LOK	
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
TNST		EIN	time after end of start
TPLRVK2_W	LR	AUS	cycle duration of sensor upstream cat, calculated by %LR, bank 2
TPLRVK_W	LR	AUS	cycle duration of sensor upstream cat, calculated by %LR
TSPERR	LR	LOK	Stop time for lambda close loop system
TSPERR2	LR	LOK	Stop time for lambda close loop system, bank2
TV	LR	LOK	LR: counter for delayed controller switch tv / ES: supply of voltage correction
TV2	LR	LOK	LR bank2: count. for delayed contr. switch tv / ES: supply of voltage correction
TVLR	LR	LOK	LR: total value for delayed controller switch tv
TVLR2	LR	LOK	LR: total value for delayed controller switch tv 2
TVLRH	LRHK	EIN	LRHK: correction value for delayed controller switch tv
TVLRH2	LRHK	EIN	LRHK: correction value for delayed controller switch tv 2
TVLRHI	LRHK	EIN	weighted I-part for delayed controller switching tv
TVLRHI2	LRHK	EIN	Bank2: weighted I-part for delayed controller switching tv
USVK	GGLSV	EIN	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyst 2
USVK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst 2
USVKMA_W	LR	LOK	output voltage master oxygen sensor upstream catalyst
USVKSL_W	LR	LOK	output voltage slave oxygen sensor upstream catalyst
USVK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) upstream catalyst
VSTLR		EIN	adjustment integrator stop time tv (service device interface)

### FW LR 89.20 Fixed Values

Parameter	Value	Description
CFRA		code word for adaptation of control amplitude
CWLRSYNC		Code word: Selects bank1 or bank2 as master during fr-synchronization
DFRMN		min. lambda deviation for steady state cond. and adaptation of transient contrl.
DFRSPS		stroke of A/F ratio controller signal (standard value)
DLRPERIMN		
DLRPERIMX		
FRIPDSL1		Factor adjustment of fri and frp during active phase 1 of DSLSLR
FRIPDSL4		Factor adjustment of fri and frp during active phase 4 of DSLSLR
FRIPDTE		Factor adjustment of fri and frp during active DTEV
FRIPTES		Factor adjustment of fri and frp at fault "open TEV pinch"
FRMAX		upper limit of control range
FRMINSLS		lower control range limit during phas1 of secondary air system diagnosis
FRTEMX		upper limit of control range on error "cannister purge valve open"
QUFRMN		lower limit for static condition of lambda controller
QUFRMX		upper limit for static condition of lambda controller
TFRSGN		
USR		controller theshold for lambda control upstream catalyst
ZDFR		filter constant for calc. of A/F ratio contr. stroke mean value
ZLRFRI		Time constant for ingreasing of tmst depending weighting factor FFRITMS

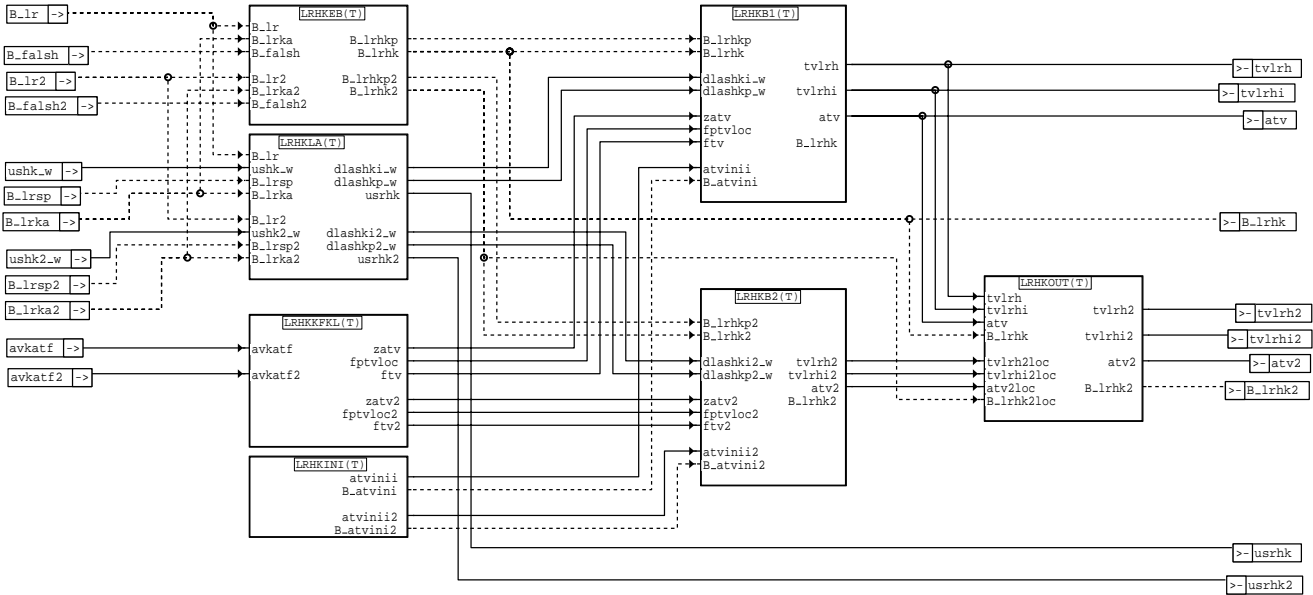
## FB LR 89.20 Detailed description of function

### APP LR 89.20 Application hint

## LRHK 33.70 Lambda closed loop control downstream catalyst (OBDII)

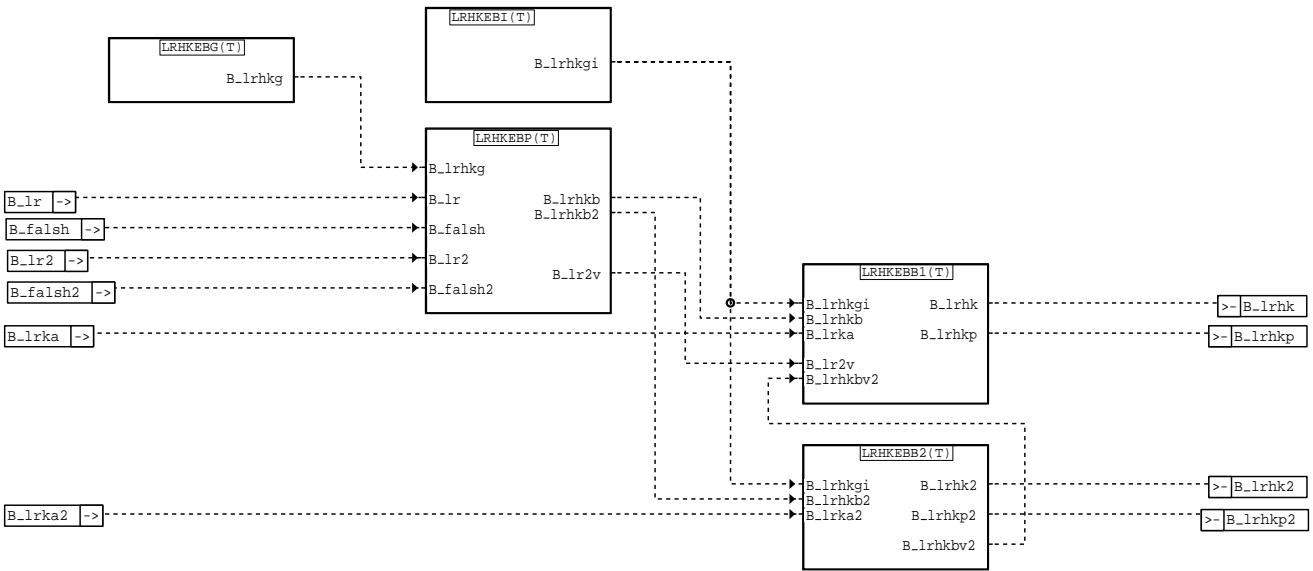
### FDEF LRHK 33.70 Function definition

Function LRHK: Overview of control downstream of the catalyzer with the sub-blocks



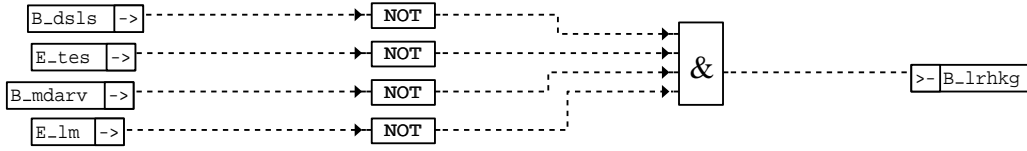
### lrhk-lrhk

Subfunction LRHKEB: Turn-on conditions for control downstream of the catalyzer



### lrhk-lrhkeb

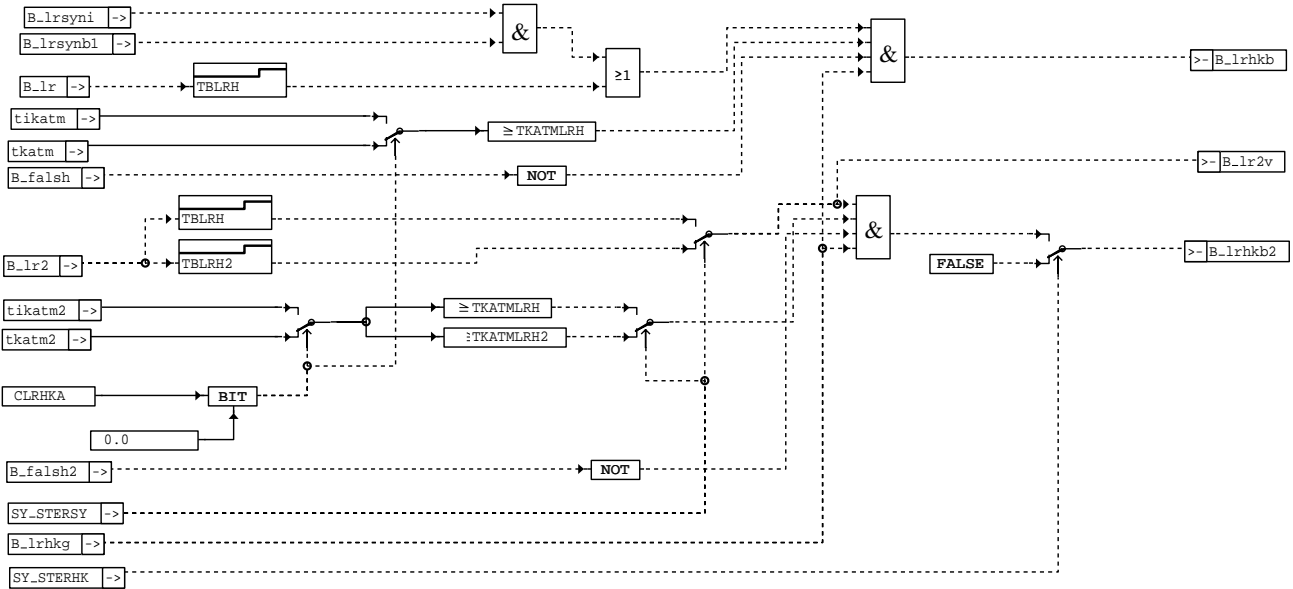
Subfunction LRHKEBG: Global turn-on conditions for control downstream of the catalyzer



lrhk-lrhkebg

### lrhk-lrhkebg

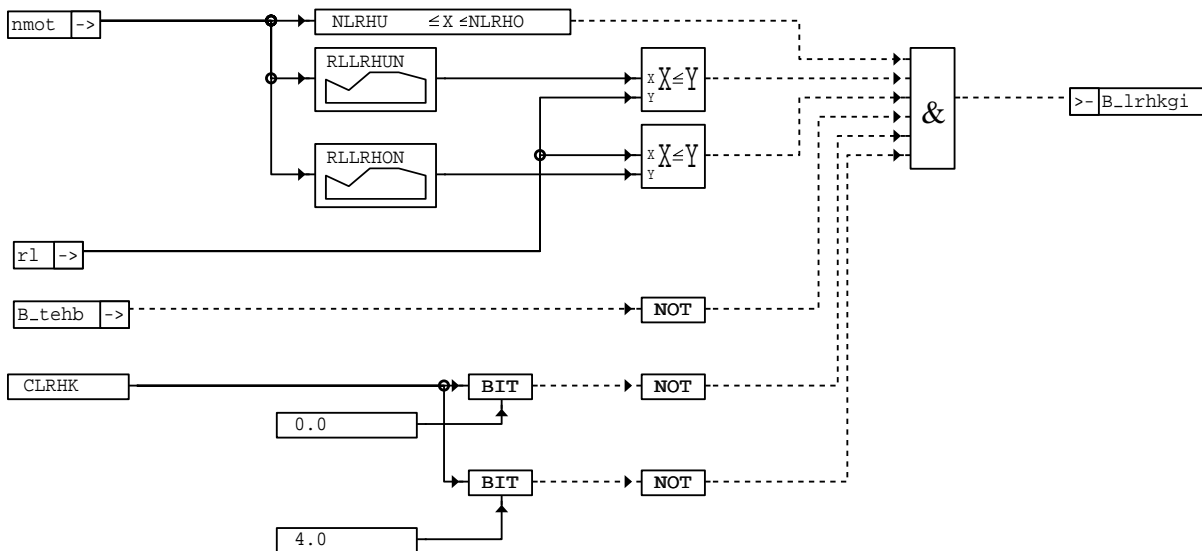
Subfunction LRHKEBP: Parameterizable turn-on conditions for control downstream of the catalyzer for bank 1 and bank 2



lrhk-lrhkebp

### lrhk-lrhkebp

Subfunction LRHKEBI: Turn-on conditions for I-component of the downstream control

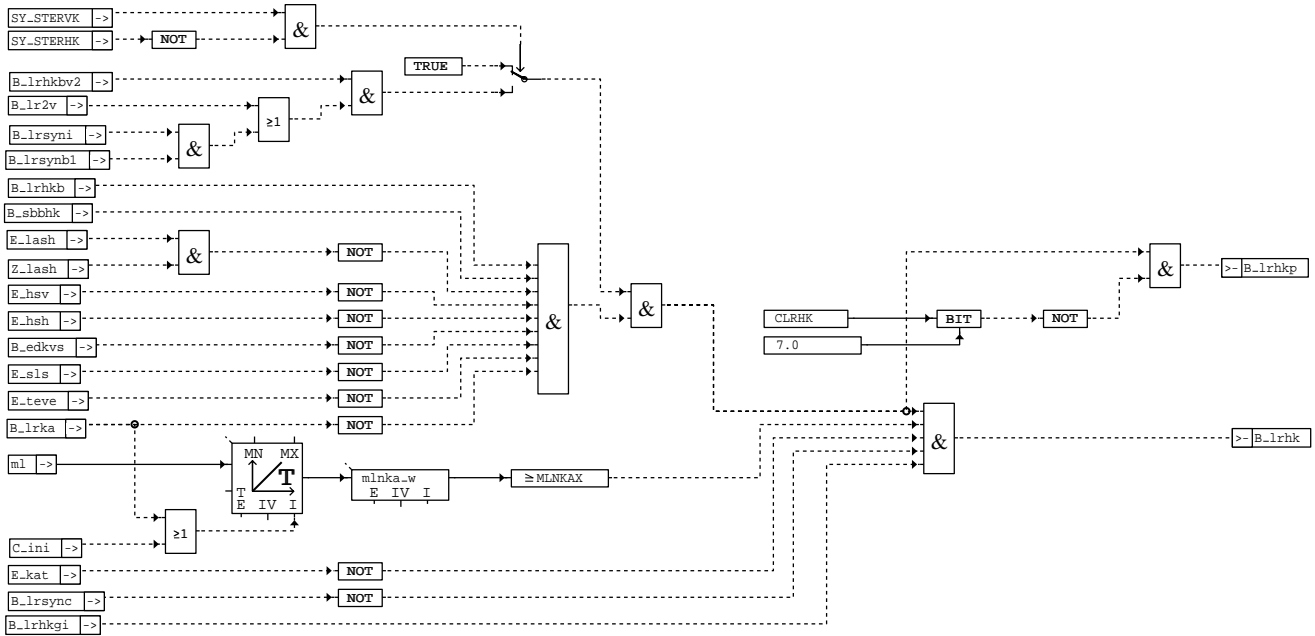


lrhk-lrhkebi

### lrhk-lrhkebi

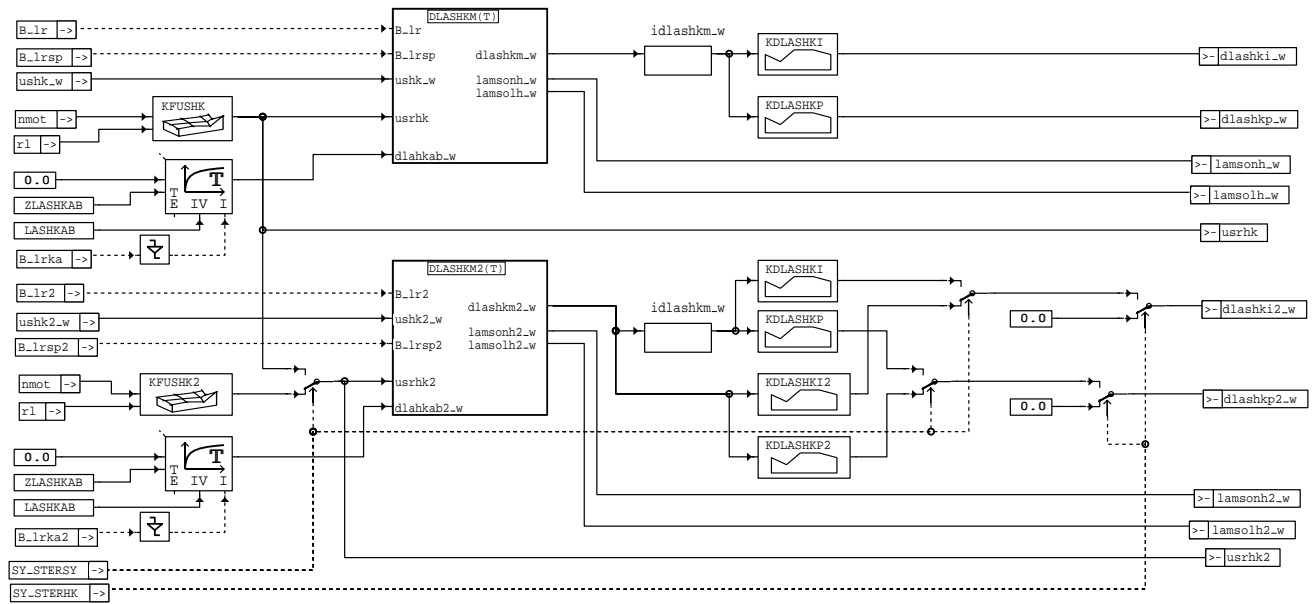


Subfunction LRHKEBB1: bank-specific turn-on conditions for control downstream of the catalyzer, bank 1



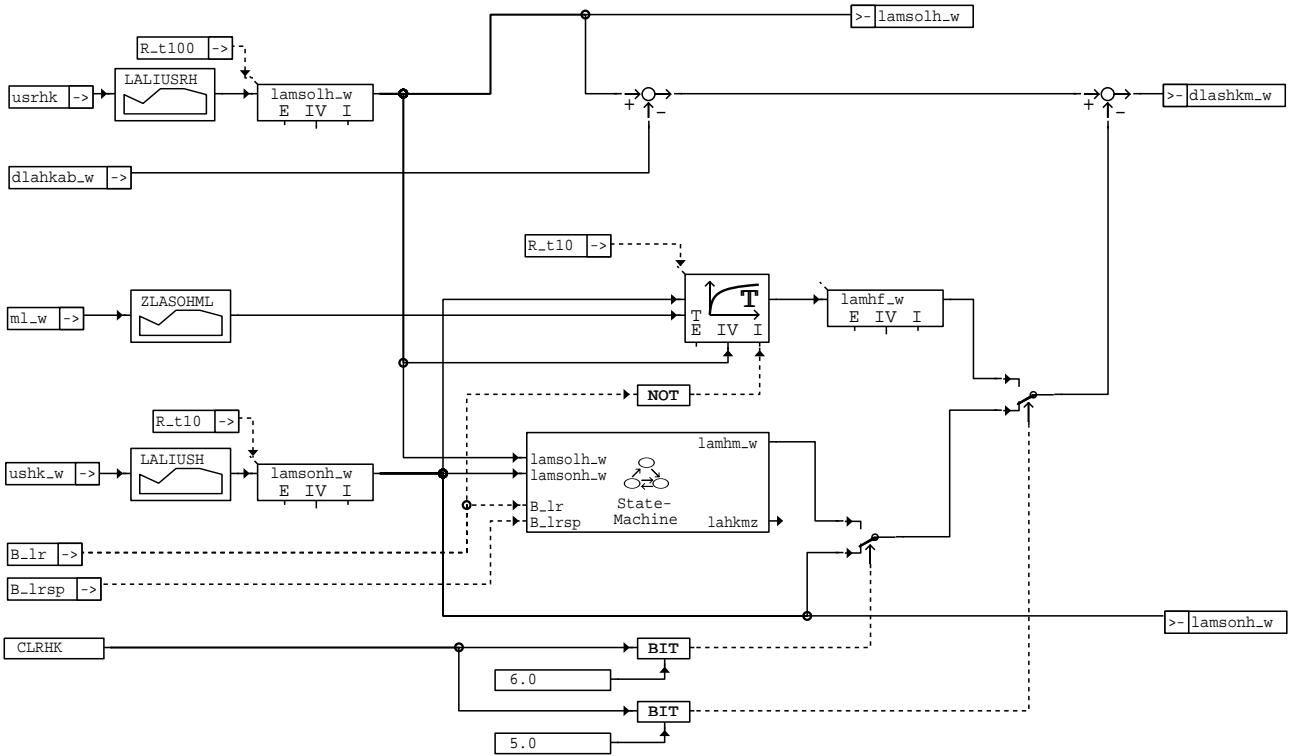
### lrhk-lrhkebb1

Subfunction LRHKLA: Evaluation of the sensor voltage



### lrhk-lrhkla

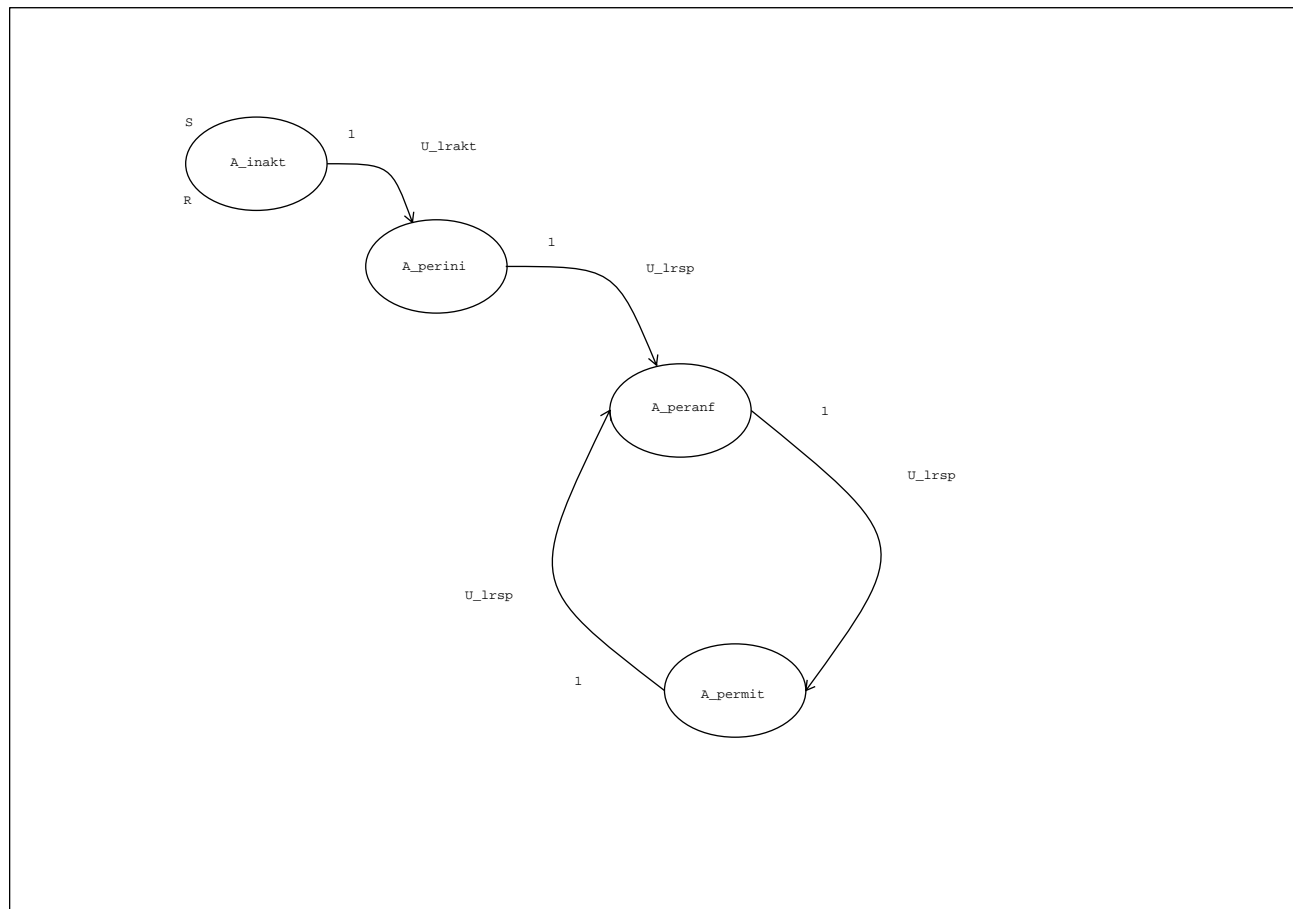
Subfunction DLASHKM: Pseudo-linearization of the sensor downstream of the catalyzer, Block of mean values formed DLASHKM and determination of the nominal value



lrhk-dlashkm

### lrhk-dlashkm

Subfunction LRHKMA: State machine for forming a fr-synchronous mean value for pseudo-lambda downstream of the catalyzer



lrhk-lahkma

### lrhk-lahkma





State machine code LAHKMAR: Formation of a fr-synchronous mean value for pseudo-lambda downstream of the catalyzer

State

Transition name	+/-	Transition condition
Action	+/-	Action code
V	V	V

```

A_inakt          Reset condition: NOT B_lr          -- This is reset state and is initiated from all
                                                         states when the reset condition
                                                         is fulfilled.

Entry:           lahkms := 0;

Action:          lamhm_w := lamsonh_w;
                 percent_w := 0;
                 lahksum_l := 0.0;

U_lrakt:         B_lr
    
```

```

A_perini

Entry:           lahkms := 1;

U_lrsp:          B_lrsp
    
```

```

A_peranf

Entry:           lahkms := 2;
                 percent_w := percent_w + 1;
                 lahksum_l := lahksum_l + lamsonh_w;
                 lamhm_w := lahksum_l/percent_w;
                 percent_w := 0;
                 lahksum_l := 0;

Action:          percent_w := percent_w + 1;
                 lahksum_l := lahksum_l + lamsonh_w;

U_lrsp:          B_lrsp
    
```

```

A_permit

Entry:           lahkms := 3;
                 percent_w := percent_w + 1;
                 lahksum_l := lahksum_l + lamsonh_w;

Action:          percent_w := percent_w + 1;
                 lahksum_l := lahksum_l + lamsonh_w;

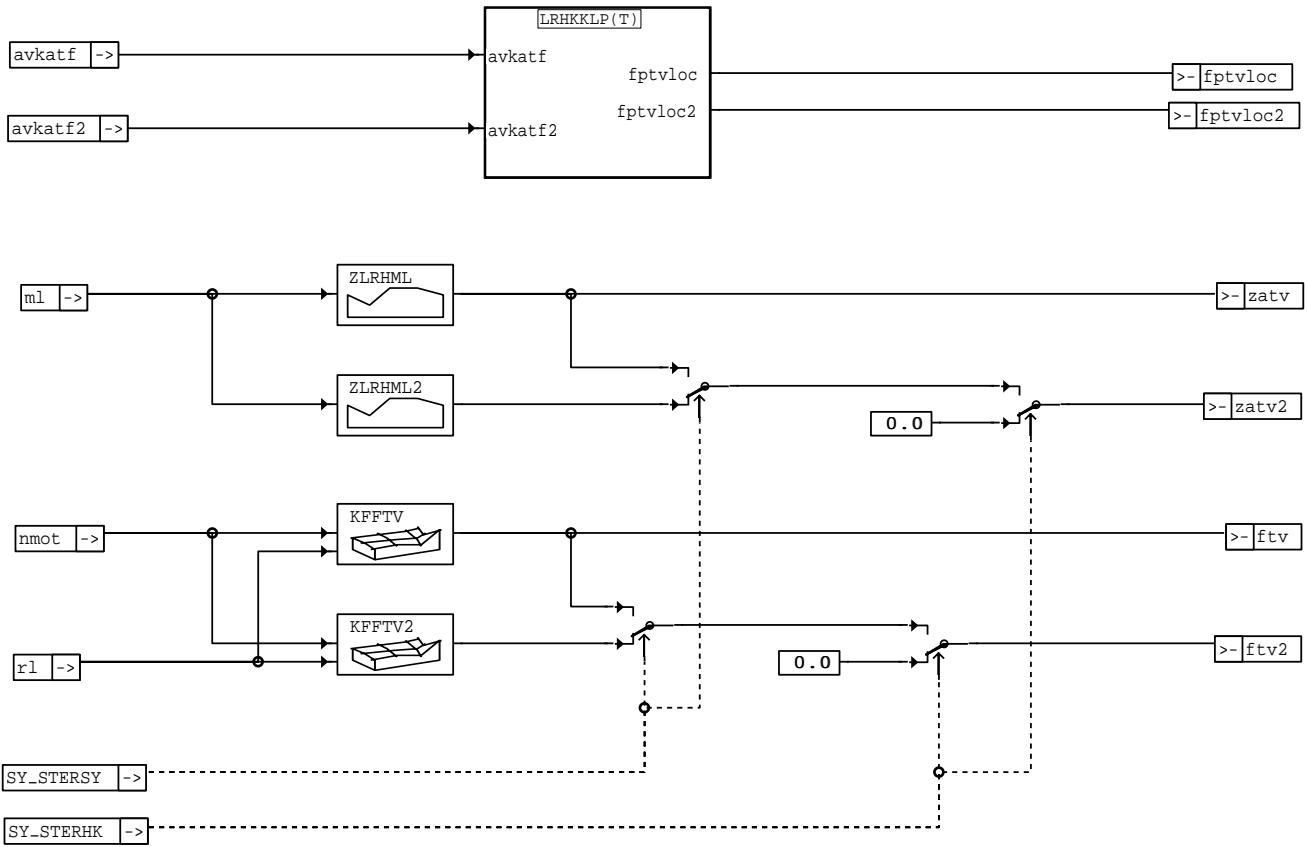
U_lrsp:          B_lrsp
    
```

Local variables:

```

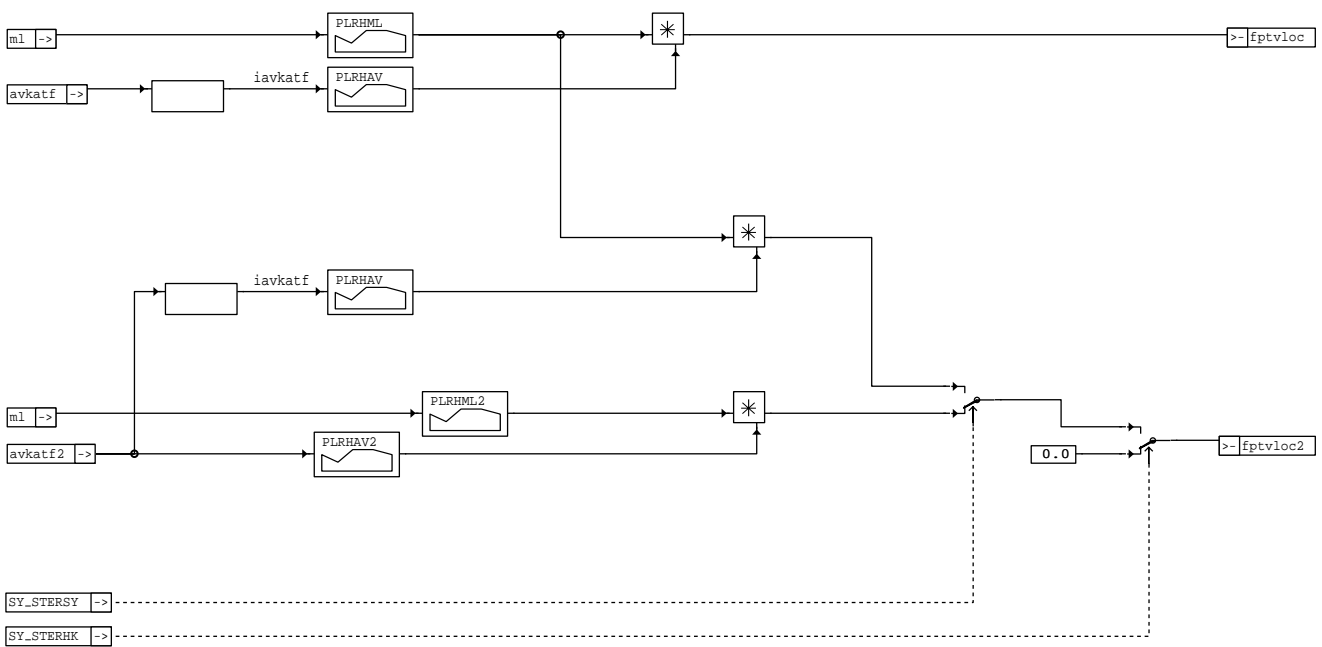
Float percent_w;
Float lahksum_l;
    
```

Subfunction LRHKFKL: Parameter selection for bank 1 and bank 2  
=====



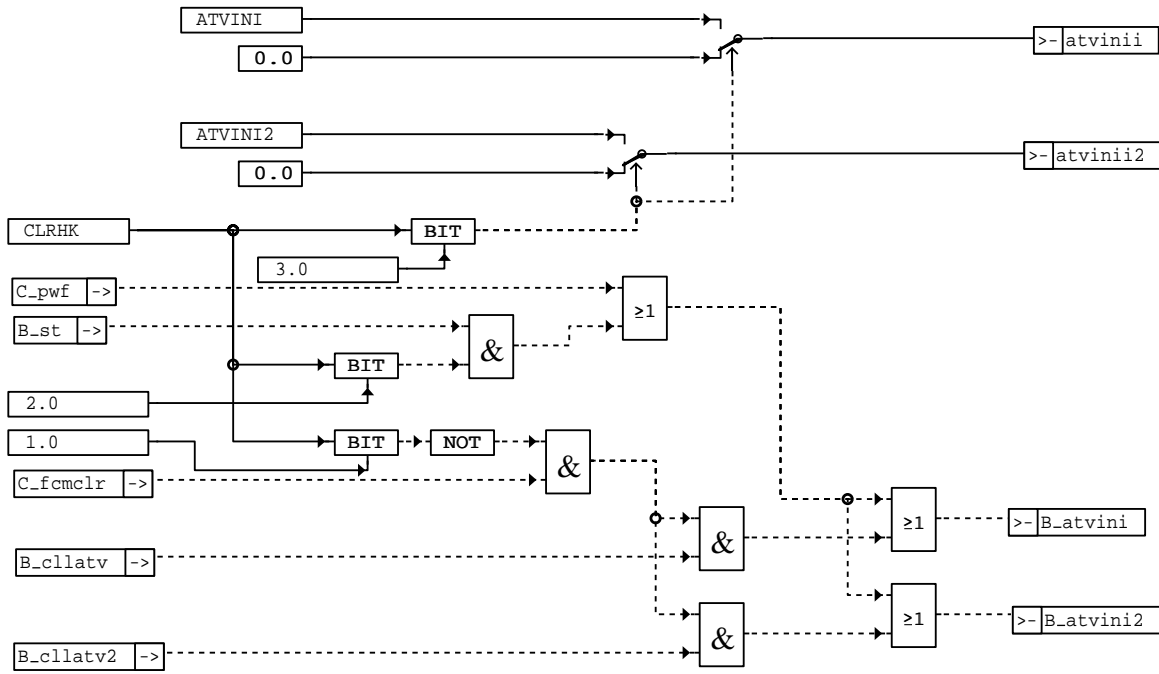
**lrhk-lrhkfkfkl**

Subfunction LRHKFKL: Parameter selection P-component for bank 1 and bank 2  
=====



**lrhk-lrhkklp**

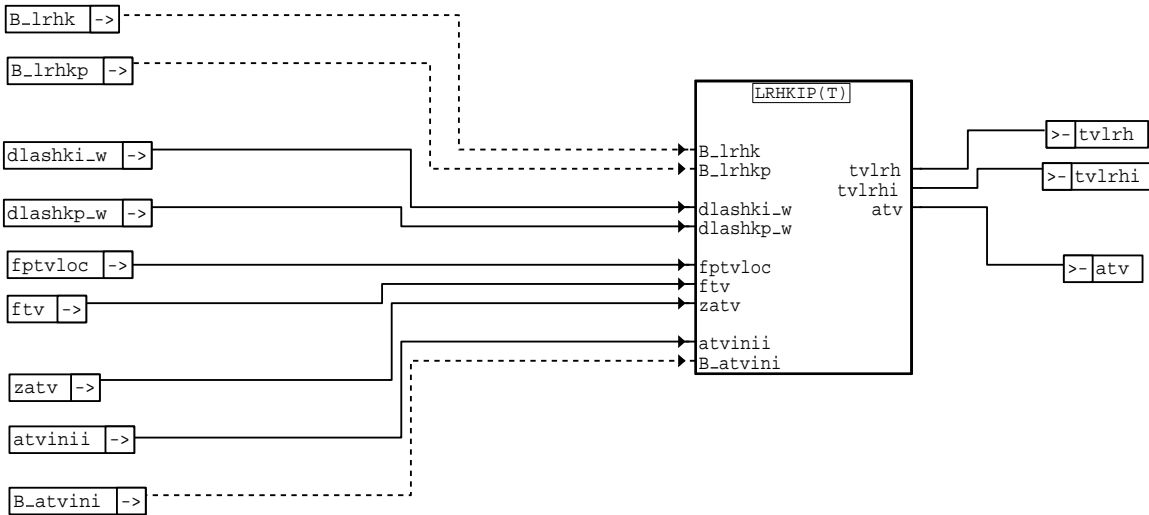
Subfunction LRHKINI: Initialization condition and Initialization value for LRHK integrators



lrhk:lrhki

**lrhk-lrhk1**

Subfunction LRHKB1: Control downstream of the catalyzer, bank 1  
turn-on conditions LRHKEB and the actual control I and P-component LRHKIP

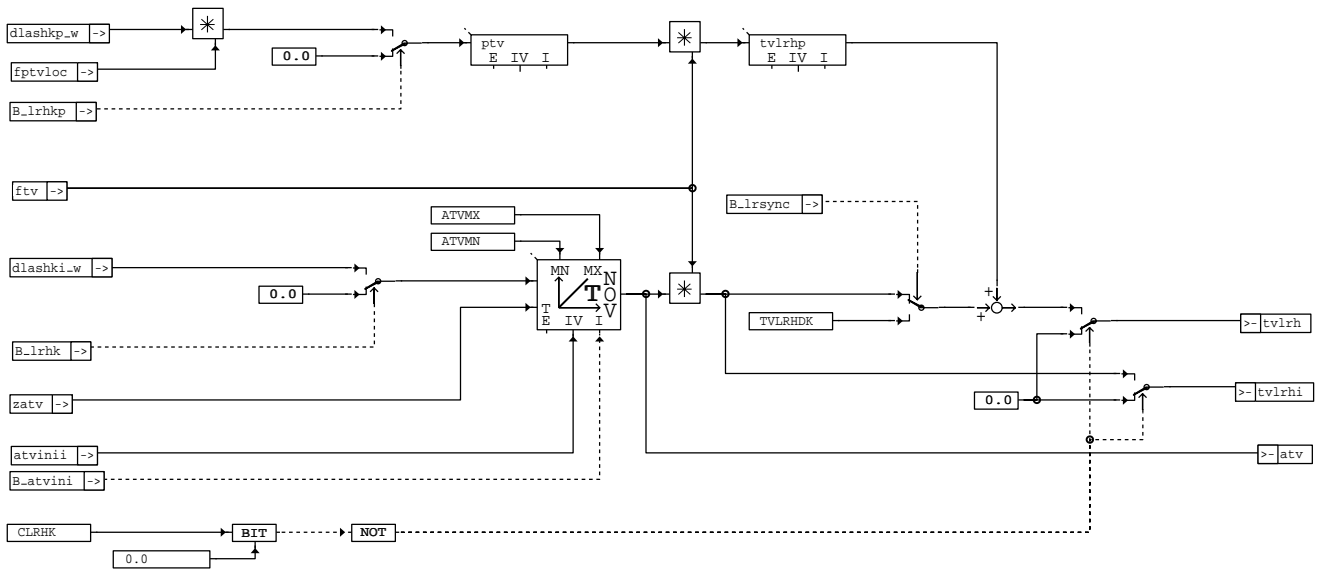


lrhk:lrhkb1

**lrhk-lrhkb1**

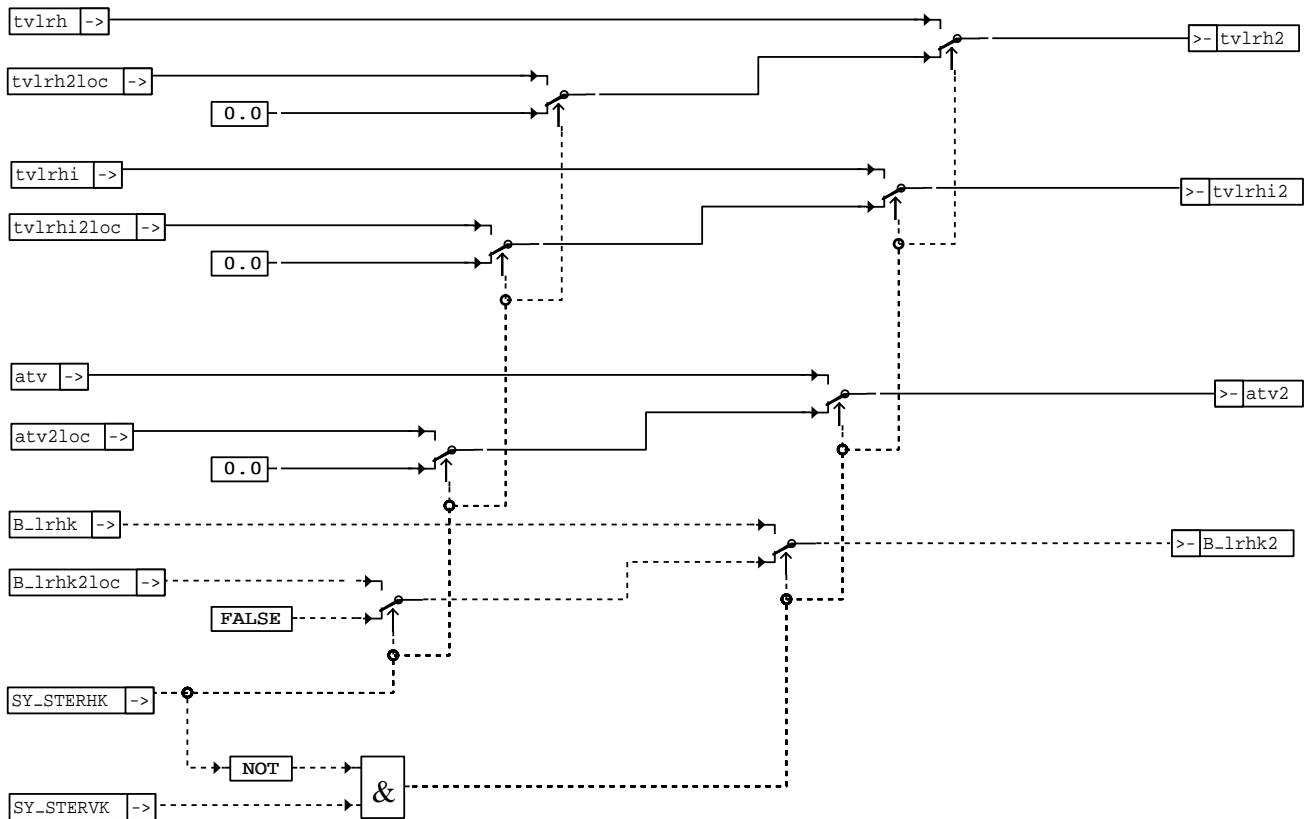


Subfunction block LRHKIP: Control downstream of the catalyzer - controller structure with I/P-component



### lrhk-lrhip

Subfunction block LRHKOUT: Output for bank 2 according to stereo/mono/symmetry



### lrhk-lrhhout

The labels to be carried twice for stereo-lambda control are identified accordingly. Defining the lower control limits by NLRHU and the characteristic RLRHUN. The upper control limits are to be established by NLRHO and the characteristic RLRHON.



## ABK LRHK 33.70 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ATVINI			FW	Initial value for control factor atv, set according to code word NOATV
ATVINI2			FW	Initial value for control factor atv, bank 2, set according to code word NOATV
ATVMN			FW	lower limit of control range of factor atv
ATVMX			FW	upper limit of control range of factor atv
CLRHK			FW	code word for lambda closed-loop control downstream catalyst on/off
CLRHKA			FW	code word for lambda closed-loop control downstream catalyst
KDLASHKI	IDLASHKM_W		KL	evaluation factor of I-part of LRHK, f(dlashkm)
KDLASHKI2	DLASHKM2_W		KL	evaluation factor of I-part of LRHK, f(dlashkm), bank 2
KDLASHKP	IDLASHKM_W		KL	evaluation factor of P-part of LRHK, f(dlashkm)
KDLASHKP2	DLASHKM2_W		KL	evaluation factor of P-part of LRHK, f(dlashkm), bank 2
KFFT	NMOT	RL	KF	weighting map for TVLRH
KFFT2	NMOT	RL	KF	weighting map for TVLRH bank 2
KFUSHK	NMOT	RL	KF	lambda sensor reference value for lambda control downstream of catalyst
KFUSHK2	NMOT	RL	KF	lambda sensor reference value for lambda control downstream of catalyst bank2
LALIUSH	USHK_W		KL	lambda linearization, sensor behind catalyst
LALIUSH2	USHK2_W		KL	lambda linearization, sensor behind catalyst, bank 2
LALIUSRH	USRHK		KL	lambda linearization, sensor behind catalyst
LALIUSRH2	USRHK2		KL	lambda linearization, sensor behind catalyst
LASHKAB			FW	initial value for dynamic increase of desired value (lamsolh) in the LRHK
MLNKAX			FW	air mass threshold for activation readiness LRSHK I-part
NLRHO			FW	upper engine speed threshold for lambda control downstream cat
NLRHU			FW	lower engine speed threshold for lambda control downstream cat
PLRHAV	IAVKATF		KL	Weighting factor of P-part LRHK depending on catalyst age
PLRHAV2	AVKATF2		KL	Weighting factor of P-part LRHK depending on catalyst age range 2
PLRHML	ML		KL	p-part of LRHK, f(dushk)
PLRHML2	ML		KL	Partie p. dans LRHK, agit avec la difference de tension de sonde aval cata banc2
RLLRHON	NMOT		KL	char. line on nmot, upper rl control threshold for downstream lambda control
RLLRHUN	NMOT		KL	char. line on nmot, lower control threshold rl for downstream lambda control
TBLRH			FW	lock per. f. c.-loop contr.downstr.cat after rel.by c.-loop contr.upstr.cat
TBLRH2			FW	lock per. f. c.-loop contr.downstr.cat after rel.by c.-loop contr.upstr.cat b2
TKATMLRH			FW	lower catalyst temperature threshold for lambda control downstream cat
TKATMLRH2			FW	lower catalyst temperature threshold for lambda control downstream cat, bank 2
TVLRHDK			FW	delay time used while catalyst diagnosis is active
ZLASHKAB			FW	time const.for decrease of the dynamic set point increase (dlasohkab)in the LRHK
ZLASOHL	ML_W		KL	time constant for PT1-filter of the pseude lambda behind catalyst
ZLASOHL2	ML_W		KL	Time constant for PT1-filter of pseudo lambda post cat, bank 2
ZLRHML	ML		KL	time constant of lambda control integrator downstream catalyst
ZLRHML2	ML		KL	time constant of lambda control integrator downstream catalyst bank 2

Variable	Source	Type	Description
ATV	LRHK	AUS	current integrator value of lambda control downstream cat
ATV2	LRHK	AUS	current integrator value of lambda control downstream cat 2
ATVINI	LRHK	LOK	Initialisation value for integrator atv
ATVINI2	LRHK	LOK	Initialisation value for integrator atv, bank 2
AVKATF	DKAT	EIN	amplitude ratio laafh/laafv strained
AVKATF2	DKAT	EIN	amplitude ratio laafh/laafv strained bank2
B_ATVINI	LRHK	LOK	Condition integrator atv be initialized
B_ATVINI2	LRHK	LOK	Condition integrator atv be initialized, Bank 2
B_CLLATV		EIN	Clear fault path in DLSA.
B_CLLATV2		EIN	Clear fault path in DLSA. Bank2
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_EDKVS	DKVS	EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS	EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_FALSH		EIN	condition function request downstream oxygen sensor diagnosis
B_FALSH2		EIN	condition function request downstream oxygen sensor diagnosis bank2
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LR2V	LRHK	LOK	condition for lambda closed loop control upstr. cat. delayed by TBLRH(2); bank 2
B_LRHK	LRHK	AUS	condition for lambda closed loop control downstream cat
B_LRHK2	LRHK	AUS	condition for lambda closed loop control downstream cat (bank 2)
B_LRHKB	LRHK	LOK	LRHK: condition lambda control behind catalyst, bank-specific parameter bank 1
B_LRHKB2	LRHK	LOK	LRHK: condition lambda control behind catalyst, bank-specific parameter bank 2
B_LRHKV2	LRHK	LOK	Bank 2 related condition based on lambda control upstream catalyst
B_LRHKG	LRHK	LOK	LRHK: bank-independent condition lambda control behind catalyst
B_LRHKG1	LRHK	LOK	LRHK: bank-independent condition I-part lambda control behind catalyst
B_LRHKP	LRHK	LOK	LRHK: condition for P-part lambda closed loop control downstream cat (bank 1)
B_LRHKP2	LRHK	LOK	LRHK bank2: condition for P-part lambda closed loop control downstream cat
B_LRKA	LRKA	EIN	condition for neutralization of catalyst oxygen storage
B_LRKA2	LRKA	EIN	condition for neutralization of catalyst oxygen storage, cylinder row 2
B_LRSP	LR	EIN	Flag 'O2 sensor voltage crosses threshold detected'
B_LRSP2	LR	EIN	condition for sensor signal bounce cylinderbench 2
B_LRSYNB1		EIN	Condition fr_b1-/fr_b2-synchronization active, bank 1 is master
B_LRSYNC	DKAT	EIN	Condition fr_b1-/fr_b2-synchronization requested
B_LRSYNI		EIN	Condition fr_b1-/fr_b2-synchronization active, local
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_ST	SWADAP	EIN	condition for start
B_TEB	TEB	EIN	condition for canister purge system with high canister load
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for initialisation



Variable	Source	Type	Description
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DLAHKAB2_W	LRHK	LOK	dynamic overshoot of the pseudo lambda set point value behind catalyst, bank2
DLAHKAB_W	LRHK	LOK	dynamic overshoot of the pseudo lambda set point value behind catalyst
DLASHK12_W	LRHK	LOK	delta lambda weighted for I-component LRSHK, bank2
DLASHK1_W	LRHK	LOK	delta lambda weighted for I-component LRSHK
DLASHKM2_W	LRHK	LOK	delta lambda of lambda contr.behind cat.(actual value averaged fr-synchr.),bank2
DLASHKM_W	LRHK	LOK	delta lambda of lambda contr.behind cat.(actual value averaged fr-synchr.)
DLASHKP2_W	LRHK	LOK	delta lambda weighted for P-component LRSHK5.30, Bank2
DLASHKP_W	LRHK	LOK	delta lambda weighted for P-component LRSHK5.30
E_HSH	DHLSHK	EIN	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK	EIN	error flag: lambda sensor heating downstream cat on the right
E_HSV	DHLSVK	EIN	error flag: lambda sensor heating upstream cat
E_HSV2	DHLSVK	EIN	error flag: lambda sensor heating upstream cat on the right
E_KAT	DKAT	EIN	error flag: catalyst conversion
E_KAT2	DKAT	EIN	error flag: catalyst conversion (cylinder row 2)
E_LASH	DLSAHK	EIN	error flag: lambda sensor aging downstream cat
E_LASH2	DLSAHK	EIN	error flag: lambda sensor aging downstream cat (cylinder row 2)
E_LM	EGFE	EIN	Error flag: main load sensor
E_SLS		EIN	error flag: secondary air system
E_SLS2		EIN	error flag: secondary air system, cylinder row 2
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_TEVE2		EIN	error flag: canister purge valve power stage
FTV	LRHK	LOK	factor weighting tv-correction of downstream lambda control
FTV2	LRHK	LOK	factor weighting tv-correction of downstream lambda control, bank 2
IAVKATF	LRHK	DOK	Char. Line source: amplitude relatio of catalyst downstream/upstream
IDLASHKM_W	LRHK	DOK	KL-Source: Delta-lambda from close loop regulation post cat.(actuall value of fr status byte of the machine: avera.of pseudo-lambda beh.cat. fr-synchr.
LAHKMZ	LRHK	LOK	status byte of the machine: avera.of pseudo-lambda beh.cat. fr-synchr.; bank 2
LAHKMZ2	LRHK	LOK	status byte of the machine: avera.of pseudo-lambda beh.cat. fr-synchr.; bank 2
LAMHF2_W	LRHK	LOK	pseudo-linearized lambda downstream, filtered by PT1, bank2
LAMHF_W	LRHK	LOK	pseudo-linearized lambda downstream, filtered with PT1
LAMHM2_W	LRHK	LOK	fr-synchronized mean-value of pseudo-lambda downstream, bank2
LAMHM_W	LRHK	LOK	fr-synchronized mean-value of pseudo-lambda downstream
LAMSOLH2_W	LRHK	AUS	pseudo lambda set point behind catalyst, bank2
LAMSOLH_W	LRHK	AUS	pseudo lambda set point behind catalyst
LAMSONH2_W	LRHK	AUS	pseudo-lambda, measured with Nernst-sensor downstream
LAMSONH_W	LRHK	AUS	pseudo-lambda,measured with Nernst-sensor downstream
ML	SWADAP	EIN	air mass flow
MLNKA2_W	LRHK	LOK	air mass after catalyst oxygen neutralization, bank 2
MLNKA_W	LRHK	LOK	air mass after catalyst oxygen neutralization
ML_W	EGFE	EIN	air mass flow filtered (Word)
NMOT	SWADAP	EIN	engine speed
PERCNT2_W	LRHK	LOK	counter 10-ms-steps for fr-synchronous lamsolh averaging, bank 2
PERCNT_W	LRHK	LOK	counter 10-ms-steps for fr-synchronous lamsolh averaging
PTV	LRHK	LOK	LRHK: unweighted p-part for delayed controller switching tv
PTV2	LRHK	LOK	Bank2: unweighted p-part for delayed controller switching tv
RL	SWADAP	EIN	relative air charge
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
SY_2SLS		EIN	System constant fault E_sls2 is defined and evaluated
SY_2TEV		EIN	System constant fault E_2teve2 is defined and evaluated
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERSY	PROKON	EIN	system constant condition stereo lambda control symmetrical
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TIKATM	ATM	EIN	exhaust gas temperature in catalyst (modelled)
TIKATM2	ATM	EIN	exhaust gas temperature in catalyst (modelled) bank2
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TVLRH	LRHK	AUS	LRHK: correction value for delayed controller switch tv
TVLRH2	LRHK	AUS	LRHK: correction value for delayed controller switching tv 2
TVLRHI	LRHK	AUS	weighted I-part for delayed controller switching tv
TVLRHI2	LRHK	AUS	Bank2: weighted I-part for delayed controller switching tv
TVLRHP	LRHK	LOK	weighted P-part for delayed controller switching tv
TVLRHP2	LRHK	LOK	Bank2: weighted p-part for delayed controller switching tv
USHK2_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst 2
USHK_W	SWADAP	EIN	output voltage oxygen sensor (4.88mV/LSB) downstream catalyst
USRHK	LRHK	AUS	momentary control threshold for downstream lambda control
USRHK2	LRHK	AUS	momentary control threshold for downstream lambda control, bank2
ZATV	LRHK	LOK	Integration speed I-part, close loop regulation post cat.
ZATV2	LRHK	LOK	Integration speed I-part, close loop regulation post cat, Bank2
Z_LASH	DLSAHK	EIN	cycle flag of lambda sensor aging downstream cat
Z_LASH2	DLSAHK	EIN	cycle flag of lambda sensor aging downstream cat, cylinder row 2

### FW LRHK 33.70 Fixed Values

Parameter	Value	Description
ATVINI		Initial value for control factor atv, set according to code word NOATV
ATVINI2		Initial value for control factor atv, bank 2, set according to code word NOATV
ATVMN		lower limit of control range of factor atv
ATVMX		upper limit of control range of factor atv
CLRHK		code word for lambda closed-loop control downstream catalyst on/off



Parameter	Value	Description
CLRHKA		code word for lambda closed-loop control downstream catalyst
LASHKAB		initial value for dynamic increase of desired value (lamsolh) in the LRHK
MLNKAX		air mass threshold for activation readiness LRSHK I-part
NLRHO		upper engine speed threshold for lambda control downstream cat
NLRHU		lower engine speed threshold for lambda control downstream cat
TBLRH		lock per. f. c.-loop contr.downstr.cat after rel.by c.-loop contr.upstr.cat
TBLRH2		lock per. f. c.-loop contr.downstr.cat after rel.by c.-loop contr.upstr.cat b2
TKATMLRH		lower catalyst temperature threshold for lambda control downstream cat
TKATMLRH2		lower catalyst temperature threshold for lambda control downstream cat, bank 2
TVLRHDK		delay time used while catalyst diagnosis is active
ZLASHKAB		time const.for decrease of the dynamic set point increase (dlasohkab)in the LRHK

## FB LRHK 33.70 Detailed description of function

The control by the sensor downstream of the catalyzer is superimposed on the lambda control with the sensor upstream of the catalyzer.

The only control intervention in the control upstream of the catalyzer is by the tv correction variable tvlrh.

Control downstream of the catalyzer:

-----  
Set bit 0 to shutdown in code word CLRHK to 1 (TRUE).

P/I control action  
=====

The control downstream of the catalyzer, as described in this FDEF, is a slow-acting two-point control with I characteristics.

The purely I-control used in previous versions for catalytic converters with a small to medium-size O2 storage capacity has been an adequate function. The larger O2 storage capacity of the new types of catalytic converters led to a greater tendency to errors by the integrator atv due to the function because following a change in the sensor voltage downstream of the catalyzer from rich to lean or from lean to rich, the integrator had first to learn back the excessively learned value before it could act correctly according to the sign. By the P-component and because it "has no memory", enrichment or enleanment is immediate following a change in the sensor voltage by the tv penetration.

The LRKH is in the position by the I-component of the control downstream of the catalyzer to largely compensate for deteriorations in the exhaust emissions that are accentuated by a shift in the static sensor characteristic attributable to non-symmetrical extensions in the response time of the front control sensor.

The P-component and I-component of the control downstream of the catalyzer is formed by an evaluation of the difference of the current voltage threshold depending on the operating point from the map KFUSHK and the sensor voltage. Prior to formation of the control difference, the output usrhk of the map KFUSHK is converted by the characteristic LALIUSRH to the pseudo-lambda nominal value lamsolh\_w. The sensor voltage downstream of the catalyzer ushk is converted by the characteristic LALIUSH into a pseudo-lambda nominal value lamsonh\_w. Because the control oscillation of the upstream control affects the course of the sensor voltage downstream of the catalyzer for older types of catalytic converters, an unchanged P-part would lead to oscillations in the control downstream of the catalyzer. Thus lamsonsh\_w in the 10-ms time frame is determined in synchronization to the control oscillations and the state machine LRHKMA is responsible for this averaging. In the state machine, lamsonsh\_w is determined from one sensor jump of a control period to the next-but-one sensor jump. The difference in control, dlashkm\_w, is formed by subtracting the pseudo-lambda actual value lamsonsh\_w from the control threshold lamsolh\_w. The weighting factor dlashki is then determined by means of the characteristic KDLASHKI = f(dlashkm\_w). The factor is then used for weighting the input of the atv integrator by multiplication. The weighting factor dlashkp\_w for den P-component is determined by means of the characteristic KDLASHKP = f(dlashkm\_w) and hence the P-component PLRHML=f(ml) is applied by multiplication. This means that both the P-component as well as the integrator rate are proportional to the difference dlashkm\_w determined above, and hence also tend towards zero for a difference in the control close to 0.

Because for older types of catalytic converters, the control oscillation of the pre-catalyzer control penetrates through to the course of the sensor voltage downstream of the catalyzer, an unchanged P-penetration would lead to oscillations in the control downstream of the catalyzer. It is for this reason that the P-component of the rear control is cancelled for older catalytic converters in a further multiplication with the evaluation factor from the characteristic PLRHAV = f(avkatf). In addition to this for older types of catalytic converters that are associated with a lower oxygen storage capacity, the necessity for a P-component in the control downstream of the catalyzer is of lesser importance.

Effect of the LRHK on the sensor diagnostic routine  
=====

The control downstream of the catalyzer intervenes solely by an additional tv shift (tvlrh = tvlrhi + tvlrhp) in the front control. The magnitude of the intervention is a measure for the aging of the sensor and is needed in the diagnostic routine for the upstream lambda-sensor aging. A symmetrical increase of the sensor-response time cannot be detected via tvlrh.

Compensation for the influence of the control frequency on the effects of tv  
=====

The current integrator value for control downstream of the catalyzer (atv) and the proportional component PLRHML = f(ml) are generally weighted with a factor from the map KFFTV and this thus gives the effective tv shift tvlrh.

The weighting map KFFTV was introduced in order to be able to describe the influence of the period duration TP of the control upstream of the catalyzer on the effect of the integrator stop time tv in delta lambda. This effect can be described - for the condition that P-jump is identical to the control amplitude - that is given according to the application procedure, by the following equation:

$$\text{Amplitude} * \text{Delta tv}$$



Delta lambda = -----  
Period duration

According to this, delta lambda is proportional to the amplitude, to delta-tv and to 1/period duration.  
A load / speed-dependent weighting of the controller correction is thus possible in the entire load-speed range by multiplication of the integrator value with the weighting factor from the map KFFTV.  
The product (tvlrhi) from the integrator content and the KFFTV value totaled with the product (tvlrhp) from the P-component and KFFTV value gives the tv correction variable for the control downstream of the catalyzer (tvlrh). This is then added in the lambda control %LR to each value from the tv precontrol map KFRTV.

Control threshold from map KFUSHK  
=====

If the sensor downstream of the catalyzer, signals e.g. a mixture that is too lean, then the integrator value increases and by this the entire tv shift as well, and the mixture is enriched until the actual value lamsons\_w and hence ushk, surpasses the control threshold downstream of the catalyzer again.  
Unlike control upstream of the catalyzer, a map is foreseen for the control threshold downstream of the catalyzer. A minor load-dependent shift in lambda can be attained by the selection made for the threshold.  
The limitations shall be observed thereby, that are given by the specification for the sensor (temperature dependency of the enrichment branch).

LRHK control dynamics  
=====

The superimposed control is to be applied considerably slower than for a control upstream of the catalyzer. Since the voltage downstream of the catalyzer has, as a rule, a more irregular course for a lower air-mass throughput (lower load-speed point) and hence oscillations following lower sensor voltages should not be evaluated to the same extent here, the time constant for the rear control shall be chosen to be independent of the air-mass throughput rate ml - (characteristic ZLRHML). The integrator rate can, as a rule, be selected to be higher for a higher air flow.

Turn-on conditions  
=====

If the control downstream of the catalyzer LRHK is disabled, then the output of the controller downstream of the catalyzer is still the integrator value atv learned up to that point in time, except that it is frozen.  
The evaluation of atv depending on the operating point continues however to be active because of the map KFFTV. This means that the output tvlrhi = atv \* KFFTV(nmot,rl) will indicate this dependency even for a control downstream of the catalyzer that is disabled.

The turn-on conditions for the P and the I-components are defined differently and are indicated by the bits B\_lrhkp and B\_lrhk.  
The following conditions apply for the P-component:

If the readiness for control upstream of the catalyzer(B\_lr = 1) is detected, then the LRHK is enabled after elapse of the delay time TBLRH.  
The control downstream of the catalyzer is only to be activated above a certain temperature of the catalytic converter threshold (tkatm > TKATMLRH) and for a detected readiness for operation by the sensor downstream of the catalyzer (B\_sbbhk).

In addition to this, a number of faults in the diagnostic routine disables the control downstream of the catalyzer.

Remark: Provided there is secondary air, B\_lrhk must be disabled during the secondary-air diagnostic routine (B\_dsls = 1). In addition to this, B\_lrhk is disabled by B\_lr = 0 (section LREB) for an active secondary air system (B\_sls = 1).

The following additional conditions apply for the I-component:

Thus the integrator is only disabled in the nmot-rl range (NLRHU <= nmot <= NLRHO and RLRHUN(nmot) <= rl <= RLRHON(nmot)). The characteristics RLRHUN and RLRHON make the selection possible of the rl limits of the control range as a dependency of the speed. By this, the control range that in earlier FDEF versions formed a rectangle in the rl-/nmot area, can be defined such that the operating range can be limited that lead to an incorrect adaptation of the control downstream of the catalyzer. This can for example occur for operating points where the air-mass throughputs are too low.

The catalytic converter is saturated with oxygen following trailing-throttle fuel cutoff. The sensor voltage downstream of the catalyzer remains at small "lean" values for a certain length of time.

In this phase, the section LRKA disables the control downstream of the catalyzer by the bit B\_lrka.  
Following completion of clearing O2 out of the catalyzer, the control downstream of the catalyzer is prohibited for such a time until the air mass MLLRH has flowed through the catalytic converter.

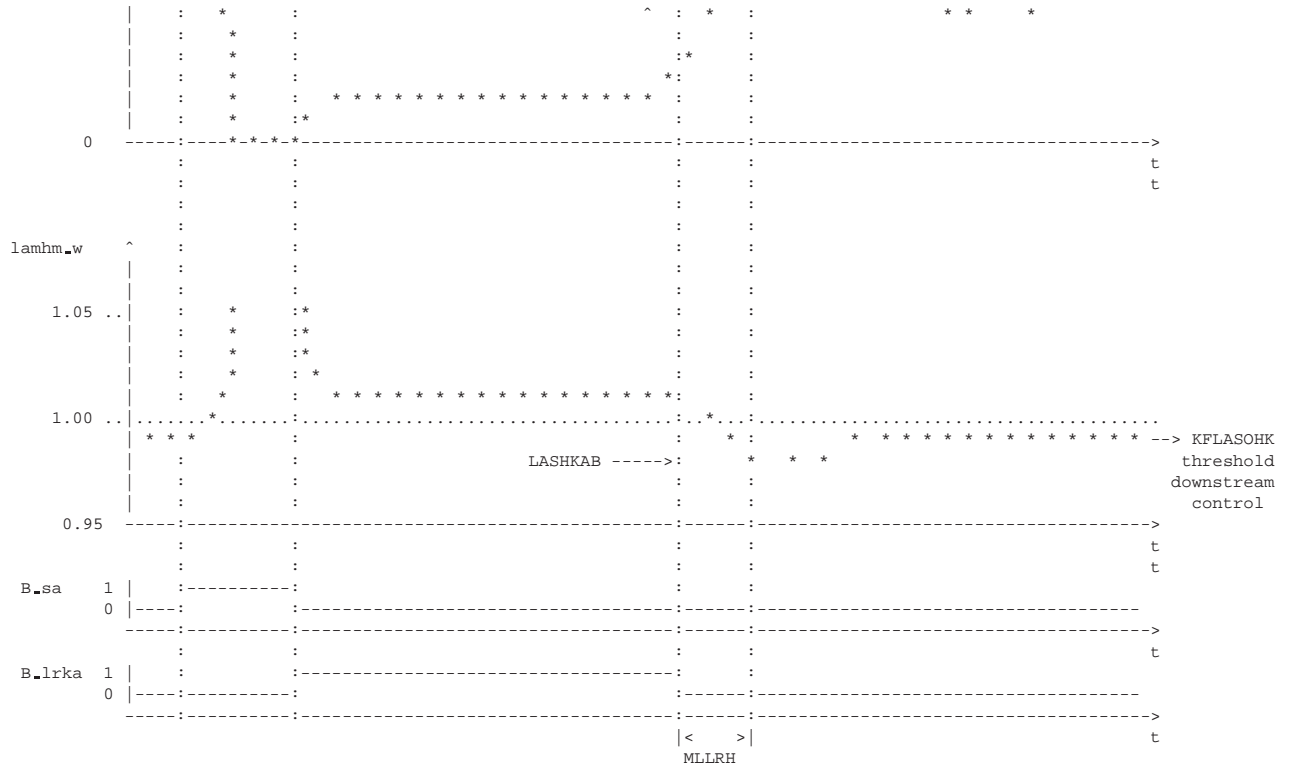
If the bit B\_tehb, "purge canister high load" is set, then the I-component of the LRHK is disabled since the integrator would otherwise learn incorrectly here. The P-component remains active in this case because this helps to reduce problems with exhaust emissions.

Dynamics increase in the control threshold following clearing out of the catalytic converter  
=====

Following completion of clearing O2 out of the catalytic converter, the sensor downstream of the catalyzer oscillates for typically 5 to 30 s above the threshold value of 600 mV. The sensor voltage thereby reaches values of between 750 and 800 mV. The overshoot depends on the characteristics of the catalytic converter.  
The increase can be disabled for those types of catalytic converters that do not exhibit this behavior.

ushk	^			v	
mV		:	:	---	: * * * *
				USHKAB:	* : * * *
600	..	.*.*.*.....	.....	.....	.....*.*.*..*.*.*.*.....





The course of the sensor voltage ushk, the pseudo-lambda lahm\_w and the status bits B\_sa (trailing-throttle cutoff) and B\_lrka (clear-out catalyzer) is shown schematically in the diagram given above. In order that "Time" (air mass MLLRH), in which the control downstream of the catalyzer is prohibited, can be kept as short a possible, the response of the sensor voltage following clearing out of the catalyzer is described over the time by dynamically raising the nominal value. To do this, the input of a PTL filter is occupied for a short period by LASHKAB and gradually decreased to 0 with the time constant ZLASHKAB. The time constant is derived from the course determined for the sensor voltage. It is possible by means of this function in those cases where clearing out O2 was not successful or where the control position upstream of the catalyzer leads to a more lean sensor voltage downstream of the catalyzer, to raise the sensor voltage downstream of the catalyzer by the LRHK.

## APP LRHK 33.70 Application hint

Method of proceeding for application of the %LRHK:

Code word CLRHK

The code word CLRHK has been introduced in order to be able to influence the handling of the adaptation value atv during the application.

The significance of the individual control bits in CLRHK is described under Remarks.

Meaningful combinations - presented in decimal - are listed in the following:

CLRHK = 0	Normal course for the function
CLRHK = 1	LRHK disabled I and P-component disabled
CLRHK = 2	atv is not reset for delete error memory
CLRHK = 4	atv is reset for engine start-up
CLRHK = 8	atv is reset with the value ATVINI for delete error memory
CLRHK = 12	atv is reset with the value ATVINI for engine start-up

LRHK parameters

- The application of the %LR must be completed
  - Select the datapoints KFPTV exactly as for the datapoints KFRI (7\*nmot, 6\*r1), provisionally set all values KFPTV = 1. It is found that a weighting is necessary outside of the control range, then this can be performed with the map KFPTV. If values other than 1 are selected, the integration rate varies for the downstream controller.
  - 4 \* 4 datapoints are foreseen for the map KFUSHK:  
 Proposal: nmot: 1000, 1800, 2400, 3000 / min  
 rL: 20 35 45 60 / %
  - Lower control limit e.g. NLRHU = 1200/min  
 characteristic RLRHUN dependent on n
  - Upper control limit e.g. NLRHO = 3000/min  
 characteristic RLRHON dependent on n
- The characteristics RLRHUN and RLRHON depend greatly on the project. A characteristic with 4 datapoints lying between NLRHU and NLRHO should however suffice.
- Select TKATMLRH such that control is at a catalyzer temperature > 300 ° C. There is a catalyzer-temperature model (%ATM), by which the catalyzer temperature tkatm is formed.



- TBLRH is dependent on the characteristics of the catalytic converter should be selected as a minimum to be 1 s. The time is defined by this label that elapse until the control upstream of the catalyzer correlates with the sensor signal downstream of the catalyzer after the lambda control has switched on.
- ZLRHML characteristic that describes the integration rate via the air mass in ms/s.  
Datapoints for an engine with ml full load for example: 450 kg/h  
ml: 9.6 28.8 86.4 200 400 kg/h  
ZLRHML: 0.6 1.2 1.8 2.4 3.0 ms/s

Application of the P-component in the LRHK:  
-----

The effective action of the P-component on the control downstream of the catalyzer is calculated as follows. The following conditions thereby apply:

A numerical range of  $\pm 1.0$  is permissible for `dlashkp_w`.  
The pseudo-difference in lambda is transformed into a dimensionless factor by the maps `KDLASHKI/KDLASHKP`, and is standardized such that it can take values between -2 and 2. The value from the characteristic `PLRHML = f(ml)` is then multiplied by this factor. `PLRHML` has the dimension of seconds as is quantized with 0.01 s/incr., like the tv time. With a further factor from the characteristic `PLRHAV`, the influence of the age of the catalytic converter is included in the calculation by multiplication (RAM cell `ptv`), as described above.  
`PLRHAV` is occupied with 1.0 for a new catalytic converter (`avkatf` at 0.0). `PLRHAV` is returned to 0.0 for an increasing amplitude ratio (the catalytic converter has aged).  
The result is then weighted with the output of the map `KFFTV` that describes the influence of the control frequency of the control upstream of the catalyzer on the lambda implementation by `atv` and `ptv tvlrh`.

The following formula for the calculation is thus given:

$$tvlrhp = dlashkp\_w * PLRHML * PLRHAV(avkatf) * KFFTV(nmot,rl)$$

where

$$\begin{aligned} usrhk &= KFUSHK(nmot,rl) \\ dlashkm\_w &= LALIUSRH(usrhk) - LALIUSH(ushk) \\ dlashkp\_w &= f(dlashkm\_w) = KDLASHKP(dlashkm\_w) \end{aligned}$$

The effect of the difference in sensor voltage on the I / P component can be weighted by the characteristics `KDLASHKI` and `KDLASHKP`.

The characteristic is normally defined such that for a decreasing difference in the voltage, the amplification of the I / P-component is also reduced.

`KDLASHK` could be applied for example as follows:

`KDUSHKP` Characteristic via `dlashkm_w`  
Evaluation factor for I/P-component in the LRHK  
-----

	<code>dlashkm_w</code>	<code>KDLASHKI/KDLASHKP</code>
0 !	-0.297	1.000
1 !	-0.198	0.500
2 !	-.0991	0.500
3 !	0.000	0.00
4 !	0.198	-1.000
5 !	0.402	-1.000
6 !	0.495	-1.500
7 !	0.600	-1.703

The selection of parameters is essentially determined by the characteristics of the catalytic converter. In the event of queries, please inquire the application at the department developing the function.

Application of the parameter `MLLRH`:  
-----

The overshoot of the sensor voltage following completion of the function `LRKA` after clearing out O2 converter is a phenomenon specific to the project that disturbs the LRHK.  
It is for this reason that the LRHK shall be disabled for such a time until the air mass `MLLRH` has been put through. Since there is no experience available (above all with the new types of catalytic converters), those responsible for the `LRKA` or `LRSKA` should be consulted when specifying the parameter.

Application of the parameters `ZLRHML`:  
-----

For the application of the map `KFRTV` in the lambda control LR, the integration rate for control downstream of the catalyzer should be adjusted using the characteristic `ZLRHML` such that a control excursion of the integrator `atv` of between  $\pm 0.03$  to  $\pm 0.04$  s is given for the measurement at a datapoint.  
The air mass at each operating point is noted during the measurement.  
Following completion of the application of the map `KFRTV`, the values set from `ZLRHML` are plotted versus the air mass. A cloud of points above the air mass is thus obtained in the plot by this. The actual characteristic `ZLRHML` in the LRHK is obtained by averaging the cloud of points.



## LRKA 15.20 Two Sensor Lambda Control: Oxygen Clear Out Function

### FDEF LRKA 15.20 Function definition

No text for FDEF available!

### ABK LRKA 15.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CLRKA			FW	code word for catalyst O2 purge funktion
DTVKAML	ML		KL	delta-tv for cat oxygen neutralization (air mass dependent)
DTVKAML2	ML		KL	delta-tv for cat oxygen neutralization (air mass dependent) bank2
FFWEKA			FW	Weighting factor for inclusion of resumption factor fwe in calc.of enriched area
FKAXAVKAT	AVKATF		KL	weighting factor for oxygen capacity depending on avkatf
FLMLKAMA			FW	Factor for evaluation of threshold of richness to interrupt cat evacuation
FLMLKAPR			FW	Factor for weighing of the measured stored oxygen
FMLKAMA			FW	factor for threshold correc. of integrated air mass for stop of cat clear out
ILMLKAXTK	TKATM_W		KL	Threshold of richness area of O2 purging after fuel cut off, funct. of cat-temp
ILMLKAXTK2	TKATM2_W		KL	Thresh. of richness area of O2 purging after fuel cut off, funct. of cat-temp.
IMLKAMN			FW	integrated air mass threshold for minimum duration of cat oxygen neutralization
IMLKAMN2			FW	integrated air mass threshold for minimum duration of cat oxygen neutralization2
IMLKAXTK	TKATM_W		KL	integr. air mass threshold f(tkatm) for cancelation of cat oxygen neutralization
IMLKAXTK2	TKATM2_W		KL	integr. air mass threshold f(tkatm2) for cancelation of cat oxygen neutral.
LAMKAML	ML		KL	lambda setpoint for catalyyst deoxidation (dependent on air mass)
LAMKAML2	ML		KL	lambdasetpoint for catalyst deoxidation (air mass dependent), bank 2
NLRKA			FW	Speed threshold for suppression of controlling emptying of the catalyzer
TDFRKAD			FW	Control-down time for controlled emptying of the catalyzer
TDFRKAU			FW	Control-up time for controlled emptying of the catalyzer
TSAKAMN			FW	minimum duration of fuel cut-off for catalyst oxygen neutralization
USHKAMN			FW	downstream sensor voltage for detection of cat has compl. stored oxygen
USHKAMX			FW	downstream sensor voltage for cancelation of cat oxygen neutralization
USVKAMX			FW	upstream sensor voltage for detection of lean cond. of cat oxygen neutralization

Variable	Source	Type	Description
AVKATF	DKAT	EIN	amplitude ratio laafh/laafv strained
B_BEVAB	BGEVAB	EIN	condition: Inj. valve cut off on Bank/Bank1
B_BEVAB2	BGEVAB2	EIN	condition: Inj. valve cut off on Bank2
B_BLRKA	LRKA	LOK	Condition controlled oxygen purging of catalyzer requested
B_BLRKA2	LRKA	LOK	Condition controlled oxygen purging of catalyzer requested, bank 2
B_ILMLKAT	LRKA	AUS	Condition: valid measurement of oxygen storage
B_ILMLKAT2	LRKA	AUS	Condition: valid measurement of oxygen storage, bank 2
B_KAWE	LRKA	LOK	Factor fwe active during catalyzer clear-out, Bank 1
B_KAWE2	LRKA	LOK	Factor fwe active during catalyzer clear-out, Bank 2
B_LRKA	LRKA	AUS	condition for neutralization of catalyst oxygen storage
B_LRKA2	LRKA	AUS	condition for neutralization of catalyst oxygen storage, cylinder row 2
B_LRKAA	LRKA	LOK	condition for turning on/ turning off the neutralization of cat. oxygen storage
B_LRKAA2	LRKA	LOK	condition for turning on/off the neutralization of cat. oxygen storage, bank 2
B_LRKAE	LRKA	LOK	Condition open loop oxygen purging of catalyst possible
B_LRKAE2	LRKA	LOK	Condition open loop oxygen purging of catalyst possible
B_LRKAEI	LRKA	LOK	Condition open loop oxygen purging of catalyst possible (ALRKAGST)
B_LRKAEI2	LRKA	LOK	Condition open loop oxygen purging of catalyst possible (ALRKAGST2), bank 2
B_LRKAON	LRKA	LOK	status catalyst clearing stopped due to new trigger of function
B_LRKARG	LRKA	LOK	condition for neutralization of catalyst oxygen storage, closed loop
B_LRKARG2	LRKA	LOK	condition for neutralization of catalyst oxygen storage, closed loop, bank 2
B_LRKAST	LRKA	LOK	condition for neutralization of catalyst oxygen storage, open loop
B_LRKAST2	LRKA	LOK	condition for neutralization of catalyst oxygen storage, open loop, bank 2
B_SA	MDRED	EIN	Condition fuel cut-off
B_SBBHK	DLSH	EIN	condition for lambda sensor downstream cat ready for operation
B_SBBHK2	DLSH	EIN	condition for lambda sensor downstream cat ready for operation bank2
B_SLS	AK	EIN	Condition for active secondary air
C_JNI	SWADAP	EIN	ECU-condition for intialisation
DTVKA	LRKA	AUS	delta-tv for catalyst oxygen neutralization
DTVKA2	LRKA	AUS	delta-tv for catalyst oxygen neutralization for 2nd bank of stereo lambda contr.
DTVKAI	LRKA	LOK	delta-tv for catalyst oxygen neutralization, internal use
DTVKAI2	LRKA	LOK	delta-tv for catalyst oxygen neutralization, internal use, bank 2
FAVKATMX	LRKA	LOK	Evaluation factor for oxigen capacity of avkatf
FWE	ESWE	EIN	reinjection factor
ILMLKA2_W	LRKA	LOK	(air mass times delta fr)-integrator for cat oxygen neutralization, bank 2
ILMLKAH2_W	LRKA	LOK	Integrator, rich area for catalyyst purging of main cat, bank 2
ILMLKAH_W	LRKA	LOK	Integrator, rich area for catalyyst purging of main cat,
ILMLKAM_W	LRKA	LOK	weighted integrator of oxygen input in main catalyyst
ILMLKAT2_W	LRKA	AUS	Valid value of oxygen storage, bank 2
ILMLKAT_W	LRKA	AUS	Valid value of oxygen storage
ILMLKAV2_W	LRKA	LOK	Integrator, rich area after catalyyst purge pre cat, Bank2
ILMLKAV_W	LRKA	LOK	Integrator, rich area after catalyyst purge pre cat,
ILMLKAX2_W	LRKA	LOK	Rich area limit for controlled catalyyst purge f(tkatm2), bank 2
ILMLKAX_W	LRKA	LOK	Rich area limit for controlled catalyyst purge f(tkatm2), bank 1
ILMLKA_W	LRKA	LOK	(air mass times delta fr)-integrator for cat oxygen neutralization
IMLKA2_W	LRKA	LOK	air mass integrator for cat oxygen neutralization for 2nd bank of stereo control
IMLKAV2_W	LRKA	LOK	weighted integrator air-mass at end of deoxidation of precatalyyst, bank2
IMLKAV_W	LRKA	LOK	weighted integrator air-mass at end of deoxidation of precatalyyst
IMLKAX2_W	LRKA	LOK	Air mass threshold for regulated (KAT ausräumen) f(tkatm2), bank 2
IMLKAX_W	LRKA	LOK	Air mass threshold for regulated (KAT ausräumen) f(tkatm), bank 1
IMLKA_W	LRKA	LOK	air mass integrator for cat oxygen neutralization



Variable	Source	Type	Description
LAMKA2_W	LRKA	AUS	Lambdasetpoint catalyst clean out, bank2
LAMKAI2_W	LRKA	LOK	Lambdasetpoint catalyst O2 purge function, bank 2
LAMKAI12_W	LRKA	LOK	Lambdasetpoint catalyst o2 purge function, local intermediate value, bank 2
LAMKAI1_W	LRKA	LOK	Lambdasetpoint catalyst o2 purge function, local intermediate value
LAMKA_W	LRKA	AUS	Lambdasetpoint catalyst O2 purge function
LAMSNKA2_W	LRKA	LOK	Lambdasetpoint catalyst o2 purge function
LAMSNKA_W	LRKA	LOK	required lambda for internal use by function LRKA, bank 2
LAMSONS2_W	LAMSOLL	EIN	required lambda for internal use by function LRKA
LAMSONS_W	LAMSOLL	EIN	required lambda referred to lambda sensor fitting location bank2
LRKAZ	LRKA	LOK	required lambda referred to lambda sensor fitting location
LRKAZ2	LRKA	LOK	flagbyte of the catalyst oxygen neutralization
ML	SWADAP	EIN	status byte of the cat O2 neutralization for 2nd bank of stereo lambda control
ML_W	EGFE	EIN	air mass flow
NMOT	SWADAP	EIN	air mass flow filtered (Word)
SY_STERHK	PROKON	EIN	engine speed
SY_STERSY	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERVK	PROKON	EIN	system constant condition stereo lambda control symmetrical
TKATM2_W	ATM	EIN	system constant condition: stereo exhaust system upstream of cat
TKATM_W	ATM	EIN	catalyst temperature modelled (word) bank2
TSAKA	LRKA	LOK	catalyst temperature modelled (word)
TSAKA2	LRKA	LOK	timer fuel cut-off duration for cat oxygen neutralization
USHK	GGLSH	EIN	timer fuel cut-off duration for cat O2 neutralization 2nd bank stereo control
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USVK	GGLSV	EIN	output voltage oxygen sensor downstream catalyst 2
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyzt
			output voltage oxygen sensor upstream catalyzt 2

### FW LRKA 15.20 Fixed Values

Parameter	Value	Description
CLRKA		code word for catalyst O2 purge funktion
FFWEKA		Weighting factor for inclusion of resumption factor five in calc.of enriched area
FLMLKAMA		Factor for evaluation of threshold of richness to interrupt cat evacuation
FLMLKAPR		Factor for weighing of the measured stored oxygen
FMLKAMA		factor for threshold correc. of integrated air mass for stop of cat clear out
IMLKAMN		integrated air mass threshold for minimum duration of cat oxygen neutralization
IMLKAMN2		integrated air mass threshold for minimum duration of cat oxygen neutralization2
NLRKA		Speed threshold for suppression of controlling emptying of the catalyzer
TDFRKAD		Control-down time for controlled emptying of the catalyzer
TDFRKAU		Control-up time for controlled emptying of the catalyzer
TSAKAMN		minimum duration of fuel cut-off for catalyst oxygen neutralization
USHKAMN		downstream sensor voltage for detection of cat has compl. stored oxygen
USHKAMX		downstream sensor voltage for cancelation of cat oxygen neutralization
USVKAMX		upstream sensor voltage for detection of lean cond. of cat oxygen neutralization



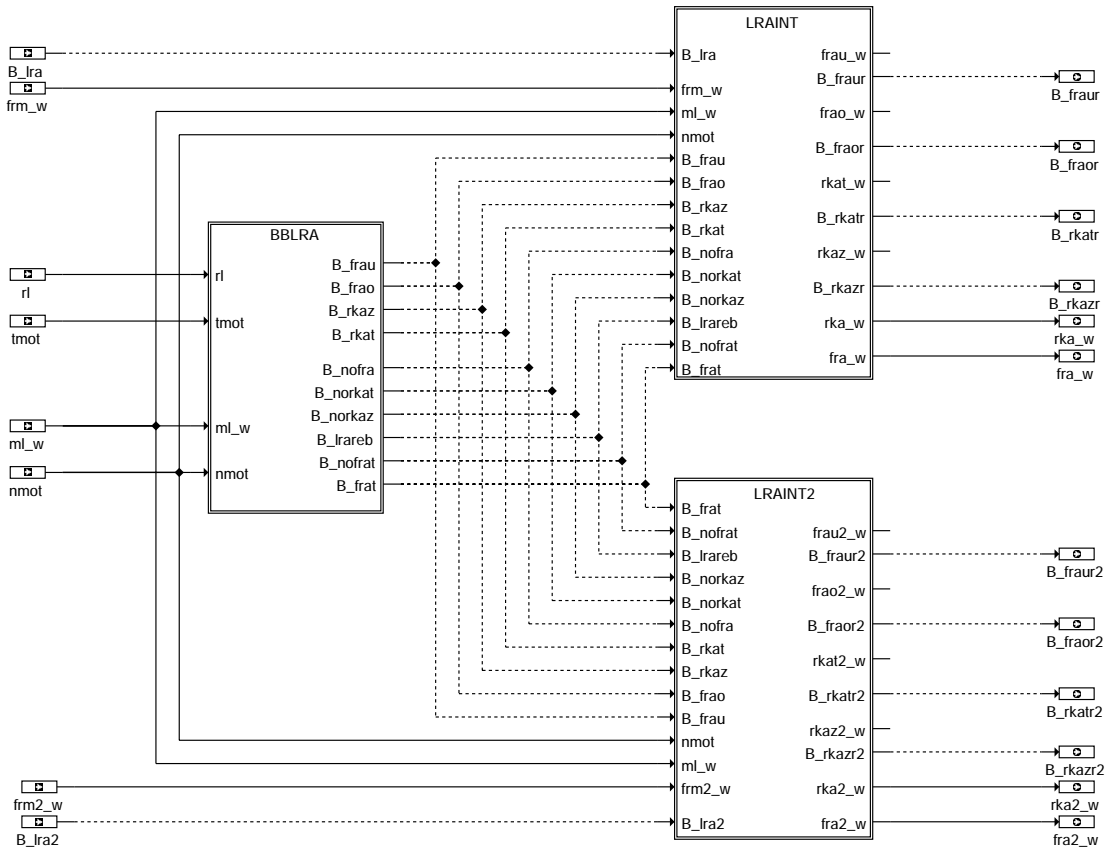
## FB LRKA 15.20 Detailed description of function

### APP LRKA 15.20 Application hint

## LRA 93.60 Lambda closed loop control; Adaptive pilot control

### FDEF LRA 93.60 Function definition

LRA : calculation of adaptation variables and their reset-, deactivation conditions (Bank 1 und 2)

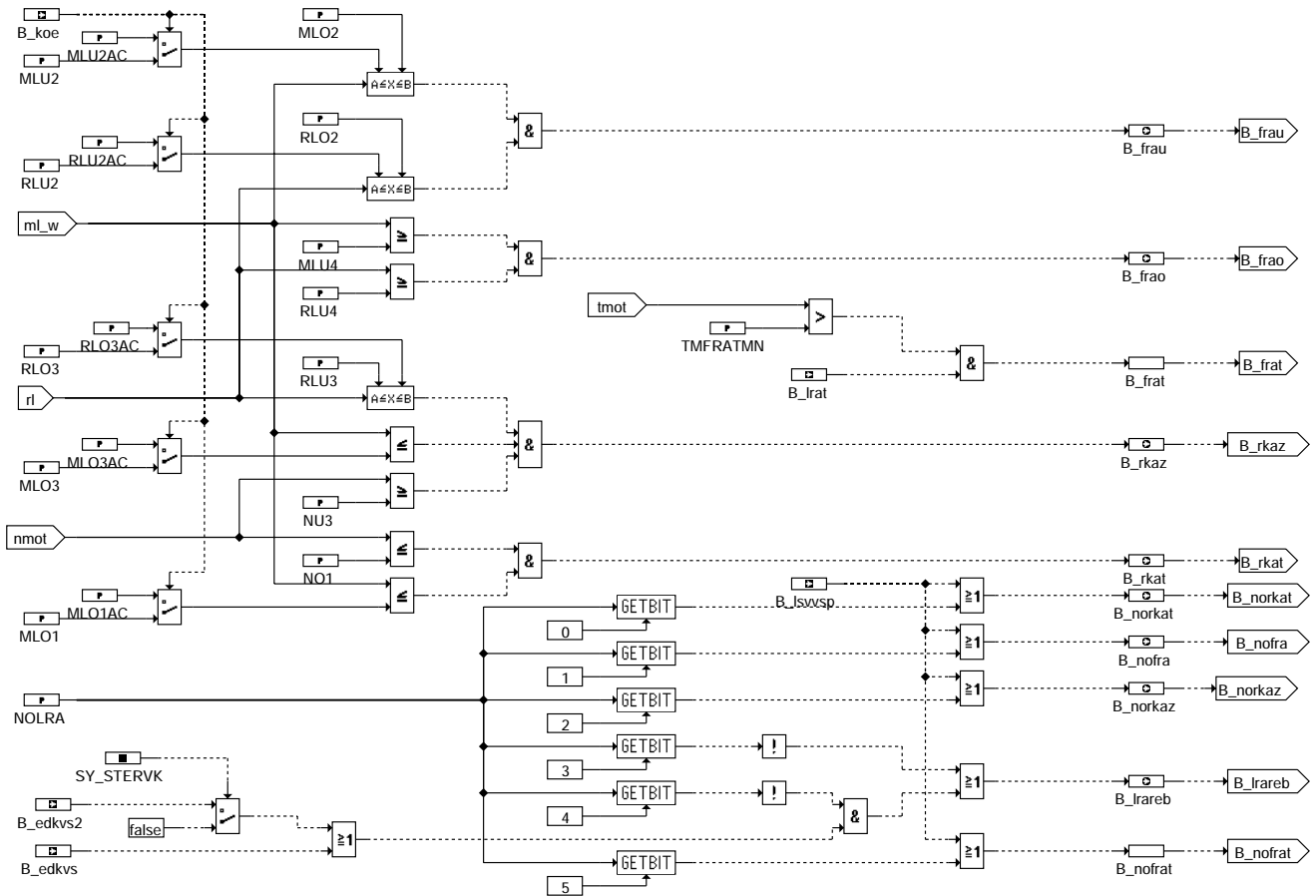


lra-main

lra-main



BBLRA : commitment of learning ranges, calculation of reset and deaktivation conditions

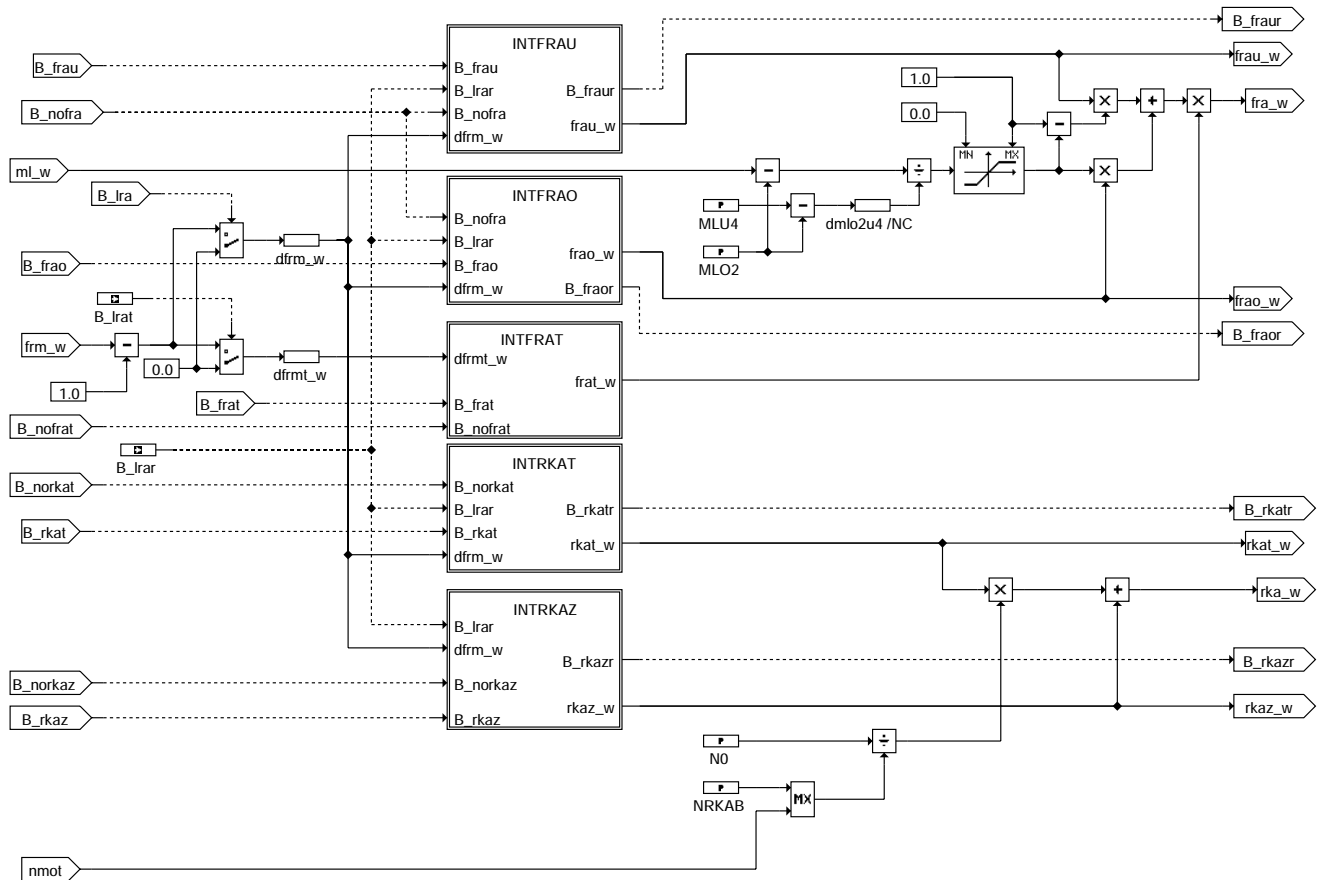


lra-bblra

lra-bblra

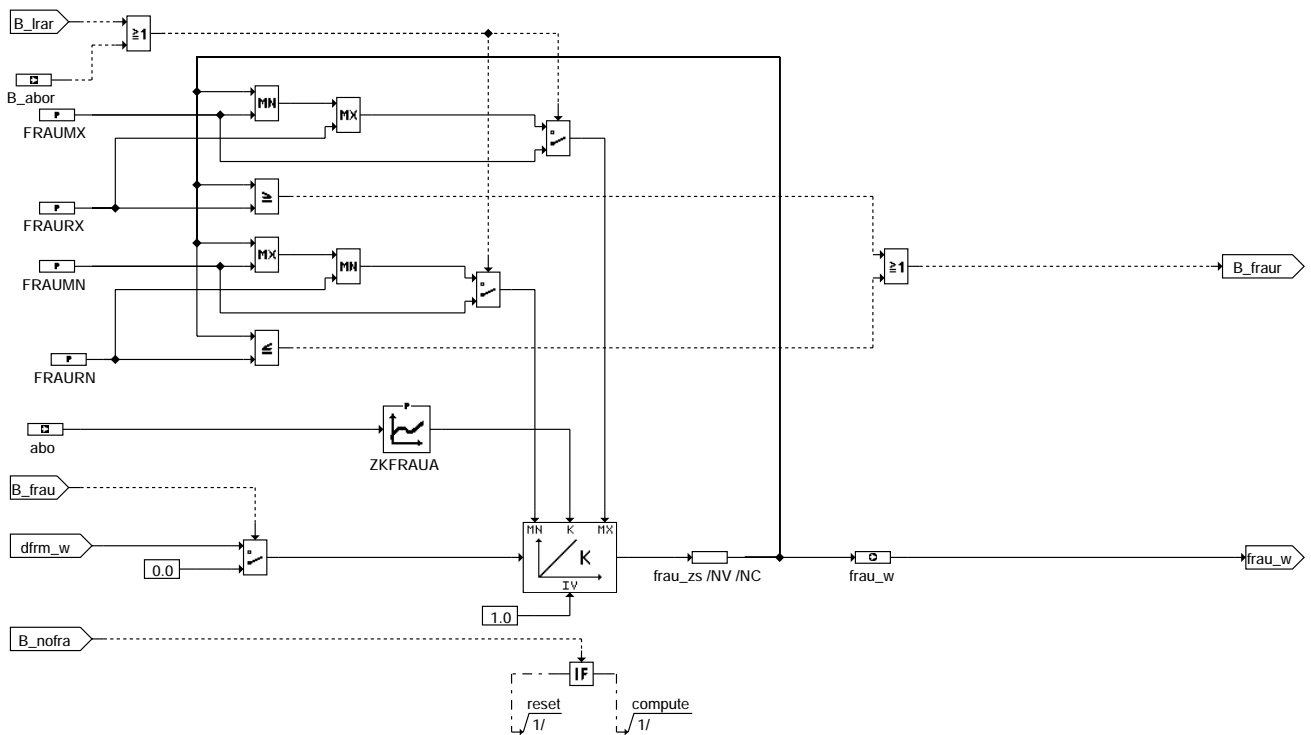
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LRAINT : calculation of adaptation variables frao\_w, frau\_w, rkat\_w und rkaz\_w



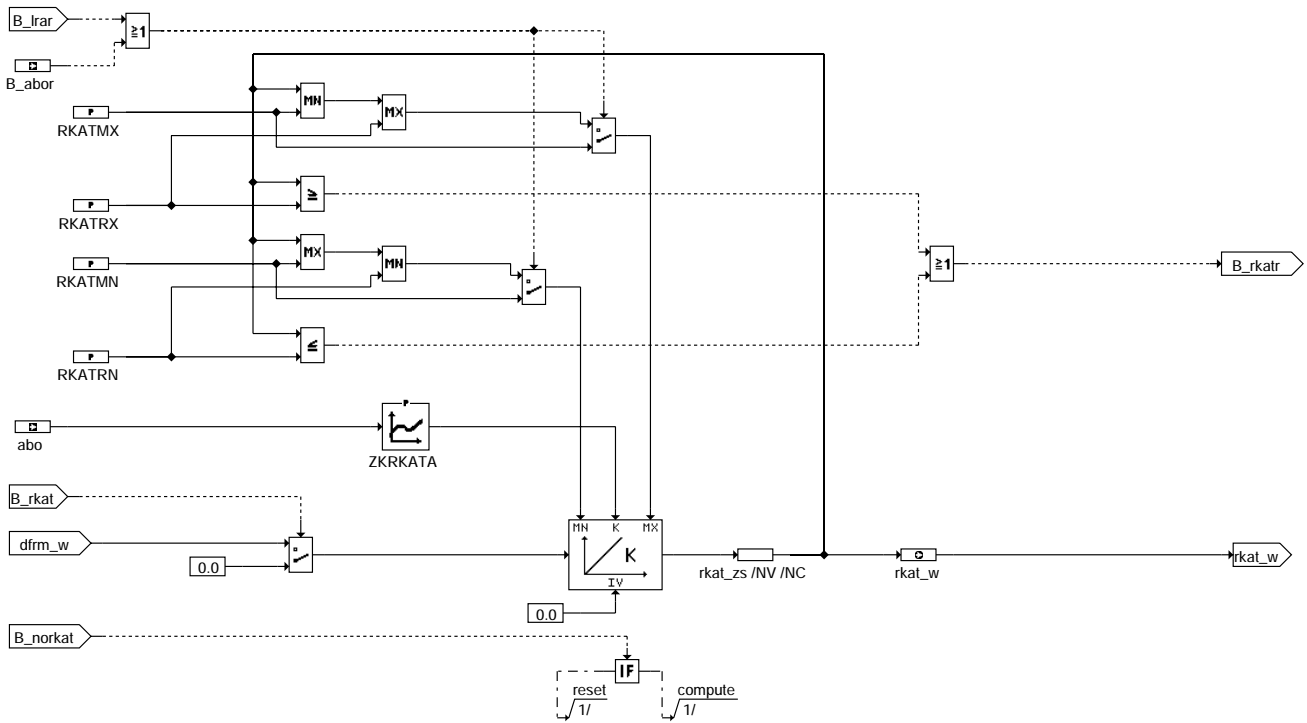
### Ira-Iraint

INTFRAU : calculation of lower multiplicative adaptation variable frau.w



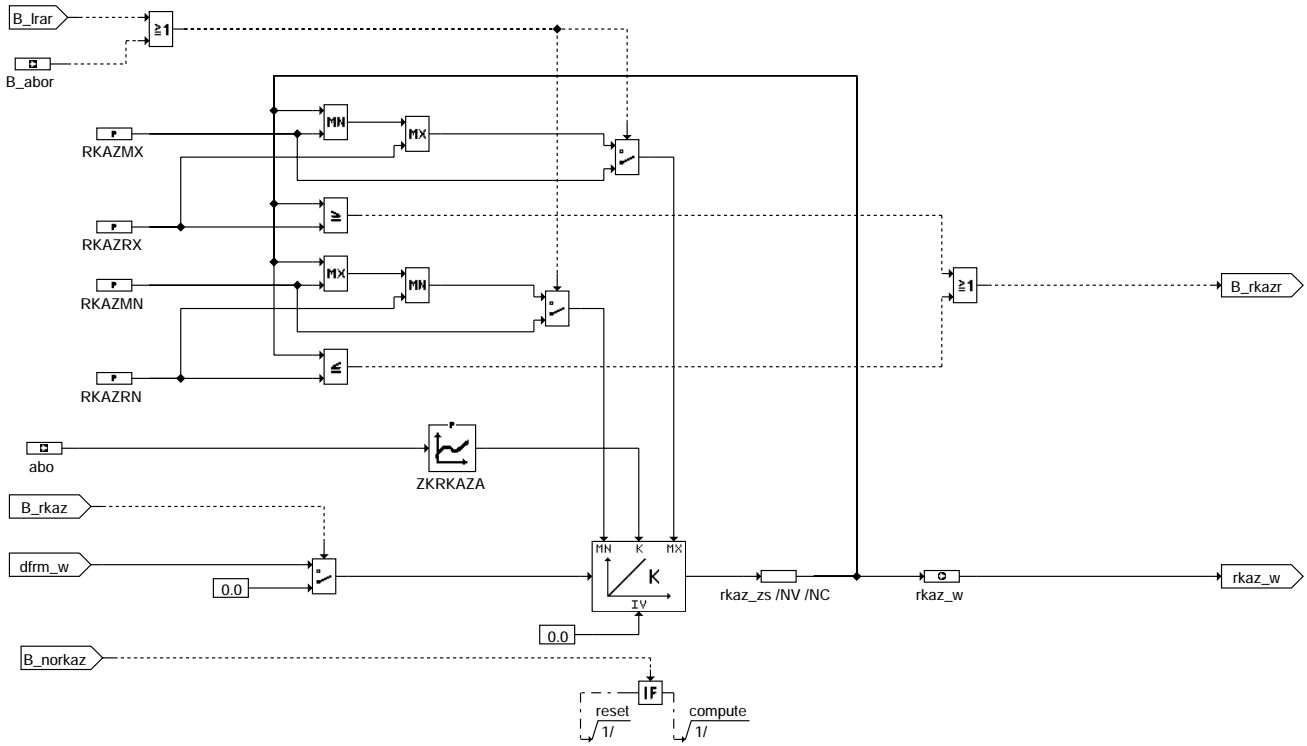
### Ira-intfrau

INTRKAT : calculation of additive adaptation variable per time unit rkat\_w



### Ira-intrkat

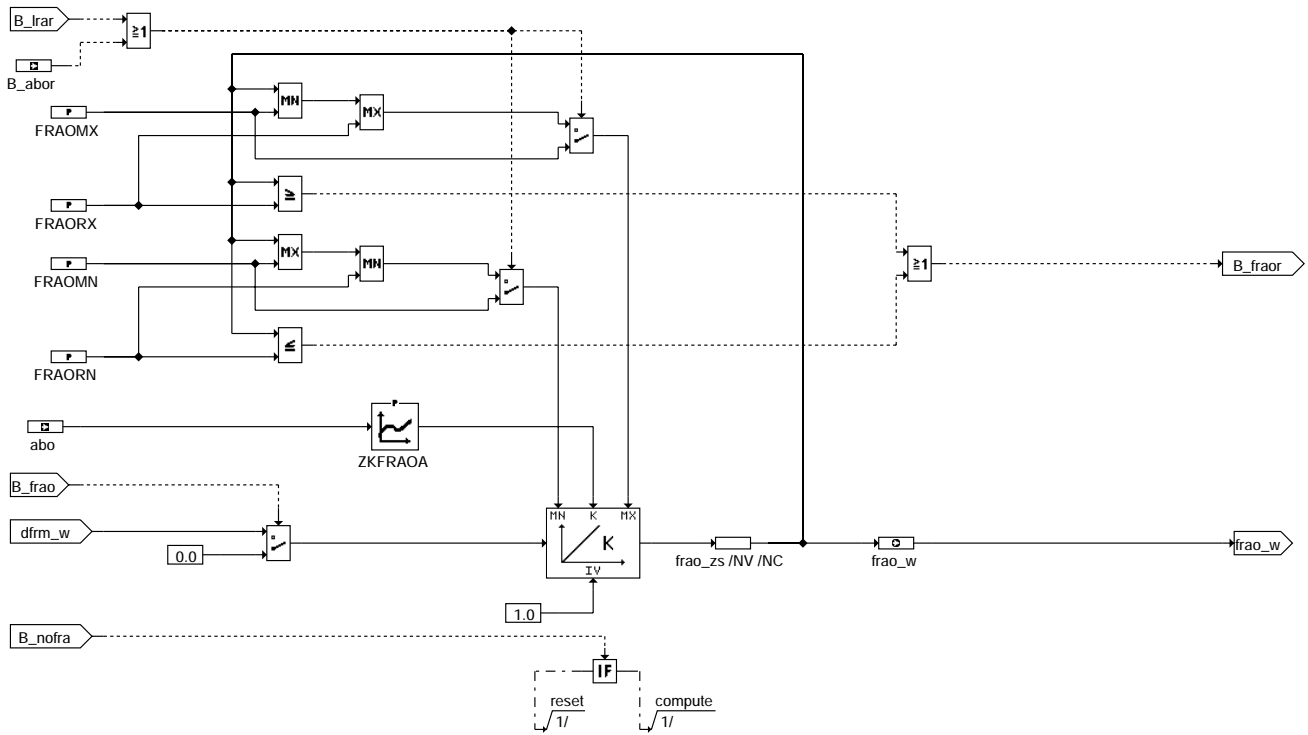
INTRKAZ : calculation of additive adaptation variable per ignition rkaz\_w



### Ira-intrkaz



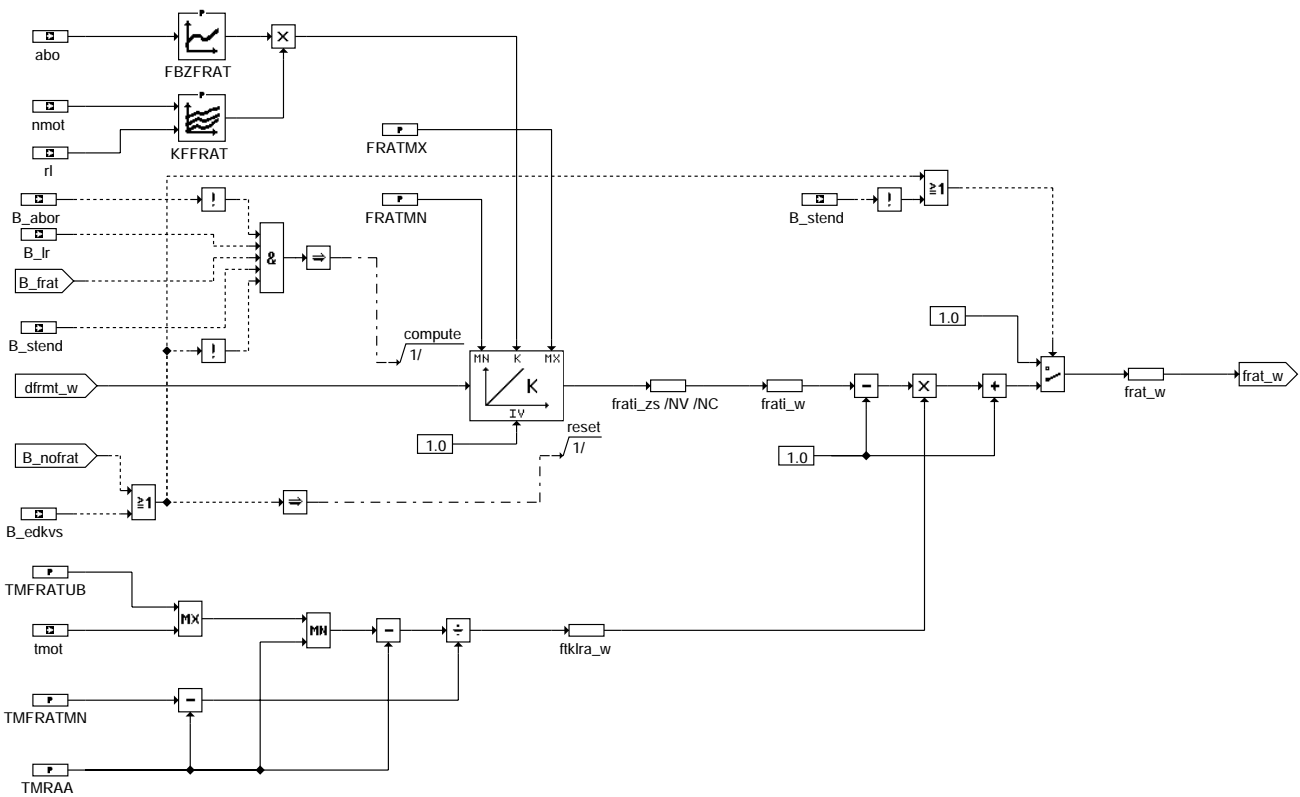
INTFRAO : calculation of upper multiplicative adaptation variable frao\_w



ira-intfrao

### ira-intfrao

INTFRAT : calculation of temperature dependent adaptation variable frat\_w



ira-intfrat

### ira-intfrat



## ABK LRA 93.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FBZFRAT	ABO		KL	weighting factor for integration speed KFFRAT as f(ab0)
FRAOMN			FW	lower limit of correction factor frao
FRAOMX			FW	upper limit of correction factor frao
FRAORN			FW	reduced lower threshold for frao correction
FRAORX			FW	reduced upper threshold for tra0 correction
FRATMN			FW	lower limit of correction factor frat
FRATMX			FW	upper limit of correction factor frat
FRAUMN			FW	lower limit of correction factor frau
FRAUMX			FW	upper limit of correction factor frau
FRAURN			FW	reduced lower threshold for frau correction
FRAURX			FW	reduced upper threshold for frau correction
KFFRAT	NMOT	RL	KF	load and speed dependent gradient of FRAT integrator
MLO1			FW	upper air-quantity threshold range 1
MLO1AC			FW	upper air-quantity threshold range 1 with compressor
MLO2			FW	upper air-quantity threshold range 2
MLO3			FW	upper air-quantity threshold range 3
MLO3AC			FW	upper air-quantity threshold range 3 with compressor
MLU2			FW	lower air-quantity threshold range 2
MLU2AC			FW	lower air-quantity threshold range 2 with compressor
MLU4			FW	lower air-quantity threshold range 4
NO			FW	conversion constant for calculation the mixture correction rkat
NO1			FW	upper engine-speed threshold range 1
NOLRA			FW	codeword for release of adaptation
NRKAB			FW	minumum engine speed for limitation rkat correction
NU3			FW	lower engine-speed threshold range 3
RKATMN			FW	lower threshold of additive correction per time
RKATMX			FW	upper threshold of additive correction per time
RKATRN			FW	reduced lower threshold of additive correction per time
RKATRX			FW	reduced upper threshold of additive correction per time
RKAZMN			FW	lower threshold of additive correction per ignition
RKAZMX			FW	upper threshold of additive correction per ignition
RKAZRN			FW	reduced lower threshold of additive correction per ignition
RKAZRX			FW	reduced upper threshold of additive correction per ignition
RLO2			FW	upper load threshold of range 2
RLO3			FW	upper load-signal threshold range 3
RLO3AC			FW	upper load-signal threshold range 3 with compressor
RLU2			FW	lower load-signal threshold range 2
RLU2AC			FW	lower load-signal threshold range 2 with compressor
RLU3			FW	lower load-signal threshold range 3
RLU4			FW	lower load threshold of the upper multiplicative section
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TMFRATMN			FW	minimum temperature at it ftklra_w is one
TMFRATUB			FW	upper temperature threshold at it ftklra_w is constant
TMRAA			FW	cut-in temperature adaptive precontrol for lambda closed-loop control
ZKFRAOA	ABO		KL	time constant for frao-integrator, f(number of starts with fuel in oil)
ZKFRAUA	ABO		KL	time constant for frau-integrator, f(number of starts with
ZKRKATA	ABO		KL	integration speed integrator rkat, f(ab0)
ZKRKAZA	ABO		KL	integration speed integrator rkaz, f(ab0)
Variable	Source		Type	Description
ABO	BBBO		EIN	numbers of starts with fuel in oil
B_ABOR	BBBO		EIN	condition numbers of starts with fuel in oil for reduced adaptive lambda control
B_CLFRAO			EIN	condition clear failure path FRAO (upper multipl. section)
B_CLFRAO2			EIN	condition clear failure path FRAO2 (stereo)
B_CLFRAU			EIN	condition clear failure path FRAU (lower multipl. section)
B_CLFRAU2			EIN	condition clear failure path FRAU2 (stereo)
B_CLRKAT			EIN	condition clear failure path RKAT (add. per time)
B_CLRKAT2			EIN	condition clear failure RKAT2 (stereo)
B_CLRKAZ			EIN	condition clear failure RKATZ (add. per ignition)
B_CLRKAZ2			EIN	condition clear failure path RKAZ2 (stereo)
B_EDKVS	DKVS		EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS		EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_FA			EIN	condition general function request
B_FAKVS			EIN	condition function request diagnoses fuel supply system
B_FRAO	LRA		AUS	condition for enabling adaption of frao
B_FRAOR	LRA		AUS	condition frao-integrator outside reduced thresholds
B_FRAOR2	LRA		AUS	condition frao2-integrator outside reduced thresholds
B_FRAT	LRA		LOK	condition enable adaptation of frat
B_FRAU	LRA		AUS	condition enable adaptation of frau
B_FRAUR	LRA		AUS	condition frau-integrator outside reduced thresholds
B_FRAUR2	LRA		AUS	condition frau2-integrator outside reduced thresholds
B_KOE	KOS		EIN	Condition for AC-compressor ON
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRA	LRAEB		EIN	condition for basic mixture adaptation enabled
B_LRA2	LRAEB		EIN	condition for basic mixture adaption 2 enabled
B_LRAR	TEB		EIN	condition for reduced correction ranges at LRA
B_LRARE	LRA		AUS	condition reset of mixture adaptation
B_LRARE2	LRA		AUS	condition reset of mixture adaptation bank 2
B_LRAREB	LRA		AUS	condition reset readiness of mixture adaptation
B_LRAT	LRAEB		EIN	condition for basic mixture adaptation temperature dependet enabled



Variable	Source	Type	Description
B_LSVVSP		EIN	condition for exchange lambda sensor; lambda control stopped
B_NOFRA	LRA	AUS	condition no fra adaptation active
B_NOFRAT	LRA	LOK	condition no frat adaptation active
B_NORKAT	LRA	AUS	condition additive correction of the mixture adaptation switched off
B_NORKAZ	LRA	AUS	condition additive correction of the mixture adaptation switched off
B_PWF		EIN	Condition for powerfail
B_RKAT	LRA	AUS	condition adaptation area rkat active
B_RKATR	LRA	AUS	condition rkat-integrator outside reduced thresholds
B_RKATR2	LRA	AUS	condition rkat2-integrator outside reduced thresholds
B_RKAZ	LRA	AUS	condition adaptation area rkaz active
B_RKAZR	LRA	AUS	condition rkaz-integrator outside reduced thresholds
B_RKAZR2	LRA	AUS	condition rkaz2-integrator outside reduced thresholds
B_STEND	BBSTT	EIN	condition end of start
DFP_DPL	LRA	DOK	ECU int. fault path no.: power fail
DFP_FRAO	LRA	DOK	internal failure path number mixture adaptation FRAO
DFP_FRAO2	LRA	DOK	internal failure path number mixture adaptation FRAO bank 2
DFP_FRAU	LRA	DOK	ECU int. fault path no.: upper multiplicative mixture adaptation factor
DFP_FRAU2	LRA	DOK	internal failure path number mixture adaptation FRAU bank 2
DFP_RKAT	LRA	DOK	internal failure path number mixture adaptation RKAT
DFP_RKAT2	LRA	DOK	internal failure path number mixture adaptation RKAT bank 2
DFP_RKAZ	LRA	DOK	internal failure path number mixture adaptation RKAZ
DFP_RKAZ2	LRA	DOK	internal failure path number mixture adaptation RKAZ bank 2
DFRM2_W	LRA	LOK	deviation of fast lambda controller mean value from 1.0 (Word), bank 2
DFRMT2_W	LRA	LOK	deviation of fast lambda controller mean value from 1.0 (Word), bank 2
DFRMT_W	LRA	LOK	deviation of fast lambda controller mean value from 1.0 (Word)
DFRM_W	LRA	LOK	deviation of fast lambda controller mean value from 1.0 (Word)
E_DPL		EIN	error condition: power fail
FRA2_W	LRA	AUS	multiplicative correction of the mixture adaptation (word)
FRAO2_W	LRA	AUS	multipl. mixture adaptation factor higher load bank 2 (Word)
FRAO_W	LRA	AUS	multipl. mixture adaptation factor higher load (word)
FRAT2_W	LRA	LOK	temperature dependent mixture adaptation factor (2. bank)
FRAT12_W	LRA	LOK	temperature dependent mixture adaptation factor integral value (2. bank)
FRAT1_W	LRA	LOK	temperature dependent mixture adaptation factor integral value
FRAT_W	LRA	LOK	temperature dependent mixture adaptation factor
FRAU2_W	LRA	AUS	multipl. mixture adaptation factor of the lower mult. section of bank 2 (Word)
FRAU_W	LRA	AUS	multipl. mixture adaptation factor of the lower mult. section (Word)
FRA_W	LRA	AUS	multiplicative correction of the mixture adaptation (word)
FRM2_W	LR	EIN	fast mean value of lambda control factor bank 2(word)
FRM_W	LR	EIN	fast mean value of lambda control factor (word)
FTKLRA_W	LRA	LOK	correction factor for temperature dependent adaptation factor
ML_W	EGFE	EIN	air mass flow filtered (Word)
NMOT	SWADAP	EIN	engine speed
RKA2_W	LRA	AUS	additive adaptive correction of the relative fuel amount bank 2
RKAT2_W	LRA	AUS	additive correction (per time) of the mixture adaptation bank 2 (Word)
RKAT_W	LRA	AUS	additive correction (per time) of the mixture adaptation (Word)
RKAZ2_W	LRA	AUS	additive correction (per ignition) of the mixture adaptation Bank 2 (Word)
RKAZ_W	LRA	AUS	additive correction (per ignition) of the mixture adaptation
RKA_W	LRA	AUS	additive adaptive correction of the relative fuel amount
RL	SWADAP	EIN	relative air charge
TMOT	SWADAP	EIN	Engine temperature

### FW LRA 93.60 Fixed Values

Parameter	Value	Description
FRAOMN		lower limit of correction factor frao
FRAOMX		upper limit of correction factor frao
FRAORN		reduced lower threshold for frao correction
FRAORX		reduced upper threshold for frao correction
FRATMN		lower limit of correction factor frat
FRATMX		upper limit of correction factor frat
FRAUMN		lower limit of correction factor frau
FRAUMX		upper limit of correction factor frau
FRAURN		reduced lower threshold for frau correction
FRAURX		reduced upper threshold for frau correction
MLO1		upper air-quantity threshold range 1
MLO1AC		upper air-quantity threshold range 1 with compressor
MLO2		upper air-quantity threshold range 2
MLO3		upper air-quantity threshold range 3
MLO3AC		upper air-quantity threshold range 3 with compressor
MLU2		lower air-quantity threshold range 2
MLU2AC		lower air-quantity threshold range 2 with compressor
MLU4		lower air-quantity threshold range 4
NO		conversion constant for calculation the mixture correction rkat
NO1		upper engine-speed threshold range 1
NOLRA		codeword for release of adaptation
NRKAB		minumum engine speed for limitation rkat correction
NU3		lower engine-speed threshold range 3
RKATMN		lower threshold of additive correction per time
RKATMX		upper threshold of additive correction per time
RKATRN		reduced lower threshold of additive correction per time
RKATRX		reduced upper threshold of additive correction per time
RKAZMN		lower threshold of additive correction per ignition



Parameter	Value	Description
RKAZMX		upper threshold of additive correction per ignition
RKAZRN		reduced lower threshold of additive correction per ignition
RKAZRX		reduced upper threshold of additive correction per ignition
RLO2		upper load threshold of range 2
RLO3		upper load-signal threshold range 3
RLO3AC		upper load-signal threshold range 3 with compressor
RLU2		lower load-signal threshold range 2
RLU2AC		lower load-signal threshold range 2 with compressor
RLU3		lower load-signal threshold range 3
RLU4		lower load threshold of the upper multiplicative section
TMFRATMN		minimum temperature at it ftklra_w is one
TMFRATUB		upper temperature threshold at it ftklra_w is constant
TMRAA		cut-in temperature adaptive precontrol for lambda closed-loop control

## FB LRA 93.60 Detailed description of function

### Principle:

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The fuel pilot control is adjusted by the mixture adaptation multiplicative and additive such that the Lambda controller corrections become minimal and that the desired Lambda is also obtained during open-loop controlled operation (e.g. B\_vl = 1 or tmot < activation temperature threshold of the Lambda control). The correction variables multiplicative (fra\_w) and additive (rka\_w) are included in the calculation on the mixture side, i.e. the load signal rl is not corrected (see %GK).

The method of the LRA is based on the following assumptions:

1. Due to the service life and by manufacturing tolerances mainly three fault types occur: multiplicative faults, additive faults per time unit (leakage air) and additive faults per injection (injector pickup delay).
  2. During idling the leakage air fault dominates (low air throughput, low engine speed), with high air throughput the multiplicative fault dominates and at high engine speed and low load the injector fault dominates.
  3. An arbitrary fault combination of multiplicative and additive kind is correctly compensated if a correction variable each is adapted in its corresponding dominating range. Precondition is a repeated switching from one range to another during the driving cycle.
- Learning ranges are defined for individual adaptation variables. Only during engine operation within a learning range is the corresponding integrator activated. The adaptation variables are however included global in the calculation according to their physical effect (fra\_w multiplicative - everywhere equally strong, rkat\_w additive per time decreases according to the engine speed nmot).

Remark: In addition to the above-mentioned fault types the mixture adaptation should also correct characteristic deviations of the HFM. In order to adapt "a curved HFM fault characteristic" the multiplicative range was subdivided into two ranges (FRAU and FRAO).

### Remarks regarding Stereo Lambda control:

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- This FDEF is designed for a system with stereo Lambda control.
- The stereo variables are distinguished by attaching a (2) (fra\_w(2) means fra\_w for bank 1 and fra2\_w for Bank 2).
- The FDEF is, however, also completely suitable for a mono-system. In this case B\_lra2 = FALSE. Additionally B\_lrare2 = TRUE (reset of the integrators), so that the integrators of bank 2 are set to their neutral values.
- In so far as they exist in duplicate the ASCET pictures only show the function of bank 1.

### Description of the overview representation:

=====

The LRA is part of the %GKRA (mixture check, controls, adaptations). It makes available the multiplicative and additive adaptation variables of the DKVS (for the diagnosis of the fuel supply system) and the mixture check GK (for the ti calculation).

The LRA contains the following subfunctions:

- BBLRA (determination of the learning ranges of the adaptation variables and calculation of the reset and deactivation conditions for the integrators)

Remark: The learning ranges (over nmot, rl and ml) of the two banks are identical.

- LRAINT (calculation of the adaptation variables for bank 1 resp mono Lambda control)
- LRAINT2 (calculation of the adaptation variables for bank 2 with stereo Lambda control)

a) Description of the subfunction BBLRA:  
-----

Four learning ranges are defined, in each of which a learning integrator is active.

1. FRAU : lower multiplicative learning range for the adaptation of multiplicative faults and HFM deviations with mean air masses
2. FRAO : upper multiplicative learning range for the adaptation of multiplicative faults and HFM deviations with large air masses
3. RKAZ : additive adaptation variable for the learning of faults additive per ignition
4. RKAT : additive adaptation variable for the learning of faults additive per time

The learning ranges should each time be counted such that the effect of the assigned fault is at its maximum.  
Die temperaturabhängige Gmischadaption FRAT wird unabhängig von der Last, Drehzahl sondern von einem Temperaturbereich nämlich  $TMFRATMN \leq tmot \leq TMRAA$  aktiviert.

## Limitation of the ranges:

The lower multiplicative learning range is limited by a lower air mass threshold ( $m1 \geq MLU2$ ) and a lower relative load threshold ( $r1 \geq RLU2$ ) as well as by an upper air mass threshold ( $m1 \leq MLO2$ ) and an upper load threshold ( $r1 \leq RLO2$ ) (range 2).

The upper multiplicative learning range (range 4) is limited by a lower air mass threshold ( $m1 \geq MLU4$ ) and a lower relative load threshold ( $r1 \geq RLU4$ ).

The learning range for additive adaptation correction per injection (range 3) is limited by the air mass  $m1 \leq MLO3$ , by the engine speed  $nmot \geq NU3$  and by the relative load between  $RLU3$  and  $RLO3$ .

The learning range for the additive adaptation variable per time unit (range 1) is limited by the engine speed  $nmot \leq NO1$  and by the air mass  $m1 \leq MLO1$ .

Remark: If the throttle valve is completely open (HFM pulsations) learning must be prohibited: -> see threshold WDKARN in %LRAEB.  
The general activation condition  $B\_lra(2)$  is reset here. The above-mentioned learning conditions remain unchanged from this.

## Calculation of the reset conditions for the integrators in LRAINT(2):

There are several conditions, for which the adaptation integrators should be set to neutral values.

They are furthermore generally reset:

- a) After detected powerfail (C\_pwf)  
If the voltage supply is interrupted, then this is detected by a powerfail test. (A stored test word then no longer corresponds to the value, which is also stored in the EPROM). In this case the adaptation is started with neutral values.
- b) During the initialization C\_ini = TRUE,
  1. If one of the integrator values (frau\_w, frao2\_w or frao\_w, frao2\_w) is outside of the absolute limit
  2. With detected fault E\_dpl

## Deactivation of individual integrators:

The status byte NOLRA is a simple possibility to deactivate individual adaptation ranges.

This should also then happen if the respective range is not entered.

- |  |          |
|--|----------|
| a) Bit 0 in NOLRA resets the RKAT-integrator in LRAINT(2)              | B_norkat |
| b) Bit 1 in NOLRA resets the FRAU and the FRAO-integrator in LRAINT(2) | B_nofra  |
| c) Bit 2 in NOLRA resets the RKAZ-integrator in LRAINT(2)              | B_norkaz |
| d) Bit 5 in NOLRA resets the FRAT-integrator in LRAINT(2)              | B_nofrat |

Remark: It is not useful to only deactivate one of the two multiplicative integrators. Therefore a separate reset of FRAO and FRAU was abstained from.

For the clearing of the individual fault path the bit reset readiness B\_lrareb is made available. The bit B\_lrareb is set to TRUE,

- a) if bit 3 of NOLRA = FALSE or
- b) if bit 4 of NOLRA = FALSE and B\_edkvs or B\_edkvs2 = TRUE.

B\_edkvs(2) is set as soon as a fault threshold of the DKVS is exceeded. If bit 3 was set to TRUE and bit 4 was set to FALSE then the individual adaptation variables are only reset in case of clear fault path if a fault of the DKVS occurred.

## Attention:

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In the series production version the adaptation must at least then be reset with clear fault memory if a fault of the DKVS occurred.

A general resetting is, however, recommended.

==> NOLRA bit 4 must be FALSE in any case, it is also recommendable to set NOLRA bit 3 to FALSE.

NOLRA bit 3 and NOLRA bit 4 may only both be TRUE during the application phase.

If SY\_STERVK = FALSE all integrators in LRAINT2 are reset (B\_lrare2 = TRUE). Thus all integrators of the LRAINT2 are at their neutral values with a mono-system. In the software bank 2 is not processed and no program codes are generated.

b) Description of the subfunctions LRAINT(2):  
-----

Since the two subfunctions LRAINT and LRAINT2 (for 2. bank) are designed similarly, the description of LRAINT2 is abstained from here.

Wherever no stereo labels exists, this will be mentioned explicitly (e.g. frm\_w(2) means frm\_w for bank 1 and frm2\_w for bank 2).

## LRAINT(2) consists of:

- Calculation of dfrm\_w(2): The frm\_w(2) (mean value of the Lambda controller from continuous or 2-step Lambda control) serves as input value
- Calculation of fra\_w: Interpolation between frau\_w(2) and frao\_w(2) over the air mass ml\_w
- Calculation of rka\_w(2) from rkat\_w(2), rkaz\_w(2) and nmot
- The following subfunctions:
  - INTFRAU(2): Integrating of the frm\_w(2) deviation for the lower multiplicative fault correction and for the calculation of the condition "frau\_w(2) outside the reduced range" B\_fraur(2)
  - INTFRAO(2): Integrating of the frm\_w(2) deviation for the upper multiplicative fault correction and for the calculation of the condition "frao\_w(2) outside the reduced range" B\_fraor(2)
  - INTRKAT(2): Integrating of the frm\_w(2) deviation for the additive fault correction per time and for the calculation of the condition "rkat\_w(2) outside the reduced range" B\_rkatr(2)
  - INTRKAZ(2): Integrating of the frm\_w(2) deviation for the additive fault correction per ignition and for the calculation of the condition "rkaz\_w(2) outside the reduced range" B\_rkazr(2)

Calculation of fra\_w(2): Interpolation between frau\_w(2) and frao\_w(2) over the air mass ml\_w  
-----

Between the learning ranges a linear interpolation over ml\_w from frau\_w(2) and frao\_w(2) is to be performed for the multiplicative correction variable. If ml\_w has a value within one of the learning ranges FRAU resp. FRAO, then fra\_w(2) to frau\_w(2) resp. frao\_w(2) shall be chosen.

The interpolation takes place as follows:

- Formation of the difference from the current ml and the upper threshold of the lower multiplicative range (MLO2).
- Formation of the difference from the lower ML threshold of the upper multiplicative range (MLU4) and of the upper ml threshold multiplicative range (MLO2)
- Formation of the ratio of both values calculated above ->  $Norm\_Wert\_ml = (ml - MLO2) / (MLU4 - MLO2)$   
thus a normalized value between 0 and 1 is obtained for the current air mass ml\_w. For air masses less than MLO2 an extrapolation to frau\_w is performed and for air masses greater than MLU4 an extrapolation to frao\_w is performed. For air masses between MLO2 and MLU4 a linear interpolation between frau\_w and frao\_w is performed.

$$fra\_w = frau\_w * (1 - Norm\_Wert\_ml) + frao\_w * Norm\_Wert\_ml = Norm\_Wert\_ml * (frao\_w - frau\_w) + frau\_w$$

Calculation of rka\_w(2):  
-----

The additive correction per time rkat\_w(2) calculated by the subfunction INTRKAT(2) is multiplied by the factor N0/nmot (value N0=640 rpm) and added to the additive correction per injection calculated by the subfunction INTRKAZ(2) and then it is passed on to the injection calculation (see mixture check %GK) as additive correction rka\_w(2).

By a maximum selection of nmot with NRKAB it is ensured that the additive correction per time, which was included in the calculation does not become too large in case of very low engine speeds (stalling).



Description of the subfunctions INTFRAU(2), INTFRAO(2), INTRKAT(2) and INTRKAZ(2)

Subfunction INTFRAU(2):

The lower multiplicative adaptation factor frau\_w(2) is adjusted with the integration speed ZKFRAU, if the condition B\_frau(2) is fulfilled. If this condition is not fulfilled, then the integration input is set to zero.

The integrator is initialized with the value 1.0, if one of the following conditions is fulfilled: B\_nofra (deactivate FRA range by bit 1 in NOLRA = TRUE), B\_lrare(2) (reset mixture adaptation during the initialization phase) or clear fault path FRAU (if B\_lrareb=TRUE reset readiness). The output of the integrator is set to 1.0, if the functional request is signalized to be equal to TRUE by B\_fa and B\_fakvs. The output of the integrator is limited by the absolute threshold FRAUMX resp. FRAUMN, which may by no means be exceeded. In order to rule out the incorrect messages of the DKVS (see diagnosis; fuel supply system) due to hot gasoline problems, additionally the reduced threshold FRAURX resp. FRAURN were introduced. The reduced thresholds apply, if the condition B\_lrar was set to TRUE by the subfunction HOHE BEL. (high charge in TEB). In case the integrator value is already outside of the reduced thresholds with B\_lrar = TRUE, only a reversed integral-action to the neutral position is still possible otherwise the integrator will be held at the present value. This comportment is forced by MINi-, MAXi-operators (resp. MAXi, MINi with lower limit), which are connected in series.

If frau\_w(2) is greater than or equal to FRAURX or less than or equal to FRAURN, the condition B\_fraur(2) = TRUE is set. B\_fraur(2) is needed in the DKVS to prevent an erroneous setting of the bit B\_gaefra(2) (multiplicative adaptation factor stabilized) and of B\_gaeing(2) (mixture adaptation bank 1 resp. bank 2 stabilized).

Subfunction INTFRAO(2) :

The facts mentioned regarding INTFRAU(2) apply analogous with the following differences:

- The thresholds can be adjusted separately (labels FRAOMX, FRAOMN, FRAORX, FRAORN)
- The time constant can be adjusted separately ZKFRAO
- B\_fraor(2) is not needed for the formation of B\_gaefra(2)
- The FRAO integrator is reset to the neutral value by clear fault path FRAO (if reset readiness is given).

Subfunction INTFRAT(2) :

The adaptation value dependent on temperature will be active at temperature which is lower then switch on temperature of mixture adaptation TMRAA. The feul density is dependent on temperature and at high common rail temperature learns the fra\_w (frau\_w resp. frao\_w) the mixture fault which describes the density of feul. Since the adaptation values is calculated at every temperature in mixture control, the adaptation values are not right at low temperature anymore. The frat\_w learns this faults und corrects the fra\_w so that the mixture is exacaty again. If the engine temperature converges against the switch on temperature of mixture adaptation (TMRAA), the frat\_w converges against one and thus it is not relevant anymore. With the factor TMFRATMN can be varies the gradient of temerature dependent correction frat\_w so that integrator FRAT learns not too much. With FRATMX and FRATMN the integrator FRAT can be limited. The geradiient of Integrator FRAT is dependent on load and speed. This isnecessray, because at low temperature the frm\_w deviation, which e.g. are caused by transient control, do not interpret as density fault. The correction factor ftklra\_w is limited down by TMFRATUB. In start and by mixture fault the adaptation corrcction is neutral.

Subfunction INTRKAT(2):

The additive adaptation variable per time rkat\_w(2) is adjusted with the integration speed ZKRKAT, if the condition B\_rkat(2) is fulfilled.

The integrator is initialized with the value 0.0, if one of the following conditions is fulfilled: B\_norkat (bit no. 0 in NOLRA), B\_lrare(2) or clear fault path RKAT. The output of the integrator is set to 0.0 if the functional request is signalized to be equal to TRUE by B\_fa and B\_fakvs. The integrator is limited by the absolute thresholds (RKATMX, RKATMN).

Analogous to the FRAU and the FRAO integrator there are also reduced thresholds (RKATRn and RKATRX). These thresholds apply as soon as B\_lrar(2) is set. If, however, rkat\_w(2) has exceeded or undershot these thresholds then only a reversed integral-action resp. a hold at instantaneous value is possible.

If rkat\_w(2) is outside of the reduced thresholds, then the condition B\_rkatr(2) = TRUE is set. B\_rkatr(2) is needed in the DKVS to prevent an erroneous setting of the bit B\_gaeing(2) (mixture adaptation bank 1 resp. bank 2 stabilized).

Subfunction INTRKAZ(2):

The additive adaptation factor per ignition rkaz\_w(2) is adjusted with the integration speed ZKRKAZ, if the condition B\_rkaz(2) is fulfilled. If this condition is not fulfilled, then the integration input is set to zero. The integrator is initialized with the value 0.0, if one of the following conditions is fulfilled: B\_norkaz (bit no. 2 in NOLRA), B\_lrare(2) or clear fault path RKAZ. The output of the integrator is set to 0.0 if the functional request is signalized to be equal to TRUE by B\_fa and B\_fakvs. The integrator is limited by the absolute thresholds RKAZMX resp. RKAZMN.

Analogous to the RKAT integrator there are also reduced thresholds(RKAZRN and RKAZRX). These thresholds apply as soon as B\_lrar is set. If, however, rkaz\_w(2) has exceeded or undershot these thresholds then only a reversed integral-action resp. a hold at instantaneous value is possible.

If rkaz\_w(2) is outside of the reduced thresholds, then the condition B\_rkazr(2) = TRUE is set. B\_rkazr(2) is needed in the DKVS to prevent an erroneous setting of the bit B\_gaeing(2) (mixture adaptation bank 1 resp. bank 2 stabilized).

It must be taken into account that only one of the two integrators RKAT resp. RKAZ is checked for stabilization in the DKVS (see %DKVS code word CPLRA). It is recommendable, here, to stop that integrator, which is not needed via the code word NORLA.

Remark:

The adaptive corrections are included in the injection calculation during all operating states outside of the start and they are stored in the RAM with permanent voltage supply (permanent RAM), so that they are not lost when the engine is turned off.







Application of the subfunction INTFRAU and INTFRAO:  
-----

A p p l i c a t i o n   v a r i a b l e s

FRAUMX	upper limitation of the correction factor FRAU	[1,2...1,25...1,3]
FRAUMN	lower limitation of the correction factor FRAU	[0,7...0,75...0,8]
FRAURX	upper reduced limitation of the correction factor FRAU	[1,2...1,25...1,3]
FRAURN	lower reduced limitation of the correction factor FRAU	[0,7...0,75...0,8]
FRAOMX	upper limitation of the correction factor FRAO	[1,2...1,25...1,3]
FRAOMN	lower limitation of the correction factor FRAO	[0,7...0,75...0,8]
FRAORX	upper reduced limitation of the correction factor FRAO	[1,2...1,25...1,3]
FRAORN	lower reduced limitation of the correction factor FRAO	[0,7...0,75...0,8]

ZKFRAUA	Integration speed Integrator FRAU	[0,025..0,025..0,0125] 1/Sec	3 * abo
abo	0            3            8		
-----			
ZKFRAUA [1/Sec]	0,02        0,02        0,015		

ZKFRAOA	Integrations speed Integrator FRAO	[0,025..0,025..0,0125] 1/Sec	3 * abo
abo	0            3            8		
-----			
ZKFRAOA [1/Sec]	0,15        0,075        0,03		

The values indicated in the middle are reference values.

Time constants, which result with feedback (via engine and Lambda control):

Time constant for FRAU/FRAO integrator : 40 to 80 s        (integration gradient ZKFRAU: 0.025/s to 0.0125/s)

Example for fra integration gradient ZKFRAU:

A firm deviation of 0.1 (step change from 1.0 to 1.1) causes a ti increase of 10 percent. The output of the integrator must therefore increase from 1.0 to 1.1, so that the frm will fall back to 1.0. If the integrator output shall reach the value 1.1 after 40 s, the integration gradient then has the value ZKFRAU = 1/40s = 0.025/s .

Adaptation limits: FRAURX = FRAORX = FRAUMX; no reduction of the fra range, so that DKVS is successful also with high charge (restricted)  
FRAURN = FRAORN = FRAUMN; no reduction of the fra range

Application of the subfunction INTFRAT:  
-----

A p p l i c a t i o n   v a r i a b l e s

FRATMX	upper limitation of the correction factor FRAT	[1,0...1,05...1,07]
FRATMN	lower limitation of the correction factor FRAT	[0,93...0,95...1,0]
TMFRATMN	lower temperature, at this ftklra = 1	[-48...20..< TMRAA] °C
TMFRATUB	lower temperature, at this ftklra = constant	[-48...0,0..< TMRAA] °C

KFFRAT [0,01...0,2] 1/sec

nmot[1/min]	600	1000	2000	4000
-----				
rl [%]				
0	0.1	0.1	0.02	0.0125
20	0.1	0.05	0.02	0.0125
60	0.02	0.02	0.02	0.0125
100	0.0125	0.0125	0.0125	0.0125

FBZFRAT [0,0...0,99]

abo	0            1            3            5            8
-----	
FBZFRAT	0,99        0,99        0,5        0,0        0,0

The values indicated in the middle are reference values.

The fault should be learnt in Ca. 10 Second. On the one hand this is dependent on the gradient of intergrator and on the other hand on the lower temperature threshold, at this the factor ftklra is equal one. If the lower temperature threshold is chosen very low, the integrator gradient can be made faster.

Let have learnt the mixture adaption so that the precontrol is at 100% all right at the temperature greater then TMRAA. TMFRATMN set to 20 ° C. At tmtot = 20 ° C and with switched on lambda control let have learnt the FRAT correction until the the precontrol is all right again.



Application of the subfunction INTRKAT and INTRKAZ:

Application variables

RKATMX	upper limitation of the correction factor RKAT	[7,0...9,0...11,0] %
RKATMN	lower limitation of the correction factor RKAT	[-11,0...-9,0...-7,0] %
RKATRX	upper reduced limitation of the correction factor RKAT	[7,0...9,0...11,0] %
RKATRN	lower reduced limitation of the correction factor RKAT	[-9,0...-7,0...-5,0] %
RKAZMX	upper limitation of the correction factor RKAZ	[7,0...9,0...11,0] %
RKAZMN	lower limitation of the correction factor RKAZ	[-11,0...-9,0...-7,0] %
RKAZRX	upper reduced limitation of the correction factor RKAZ	[7,0...9,0...11,0] %
RKAZRN	lower reduced limitation of the correction factor RKAZ	[-11,0...-9,0...-7,0] %
ZKRKATA	Integrationsgeschwindigkeit Integrator RKAT	[0,1...0,5...0,5] %/Sec
abo	0                      3                      8	
-----		
ZKRKATA [1/Sec]	0,38                      0,38                      0,293	
ZKRKAZA	Integrationsgeschwindigkeit Integrator RKAZ	[0,1...0,5...0,5] %/Sec
abo	0                      3                      8	
-----		
ZKRKAZA [1/Sec]	0,38                      0,38                      0,293	

The values indicated in the middle are reference values.

Background of the above values -> a rl of 30% was assumed during idling.  
 Choose RKATMX such that during idling 25% to 30% rk-correction is possible  
 Choose RKATMN such that during idling -25% to -30% rk-correction is possible  
 (Choose RKAZMX such that with typ. rl in range three +25% rk- correction is possible  
 Choose RKAZMN such that with typ. rl in range three -25% rk- correction is possible)

RKATRX =RKATMX; no upward reduction of the rkat  
 RKATRN : about 2% to 3% (related to idle rl) above diagnostic threshold RKATDN  
 Remark: For OBDII with running losses no reduction at all RKATRX = RKATMX  
 (RKAZRX : about 2% to 3% (related to typ. rl in RKAZ range) below diagnostic threshold RKAZDX  
 RKAZRN : about 2% to 3% (related to typ. rl in rkaz range) above diagnostic threshold RKAZDN)

Time constants, which result with feedback (via engine and Lambda control):

Time constant for RKAT integrator : 40 to 80 s (ZKRKAT 0.5 %/s to 0.25 %/s) Att.: oscillation tendency with frm!!  
 Time constant for RKAZ integrator : 40 to 80 s (ZKRKAZ 0.5 %/s to 0.25 %/s)

Example for rkat integration gradient ZKRKAT:

A frm deviation of 0.1 causes a ti increase of 10 percent. This constitutes a 2% rl change as related to rl = 20%.  
 The engine speed is to be 800 rpm during idling. If these 2% have to be controlled within 50s, so that the frm reaches the value 1.0, then the integration gradient for RKAT integrator is the same ZKRKAT = (800 rpm \* 2%)/(640 rpm \* 0.1 \* 50 s) = 0.5 %/s .

Example for rkaz integration gradient ZKRKAZ:

A frm deviation of 0.1 causes a ti increase of 10 percent. This constitutes a 2% rl change as related to rl = 20%.  
 If these 2% have to be controlled within 40s, so that the frm deviation of one becomes zero again, then the integration gradient is the same  
 ZKRKAZ = 2% / (40 s \* 0.1 ) = 0.5 %/s .

An oscillation tendency of the LRA with the frm is definitely to be ruled out during the application of the time constants. The most critical case is given here during idling without consumers. The integrator gradient of the frm is at its lowest here. The integration speed of the rkat must be chosen distinctly slower than that speed, at which an oscillation tendency could be provoked. Otherwise the system will oscillate after excitation (large frm deviations).

Application of the subfunction LRAINT:

Application variables

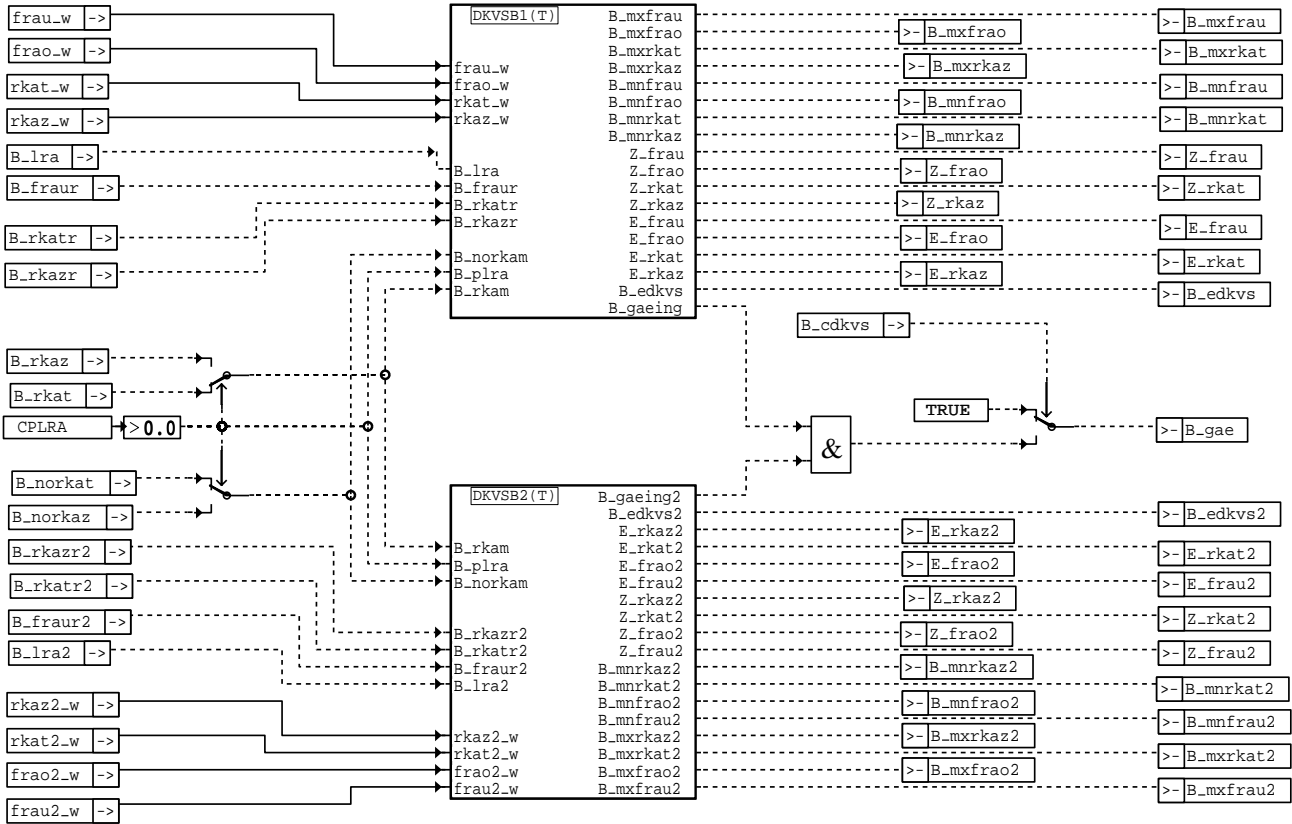
NRKEB	minimum engine speed for limitation control action rkat	[400...400...500] rpm
NO	conversion constant for inclusion mixture correction rkat	[640...640...800] rpm

The values indicated in the middle are reference values.

## DKVS 17.60 Diagnosis; plausibility test fuel supply system

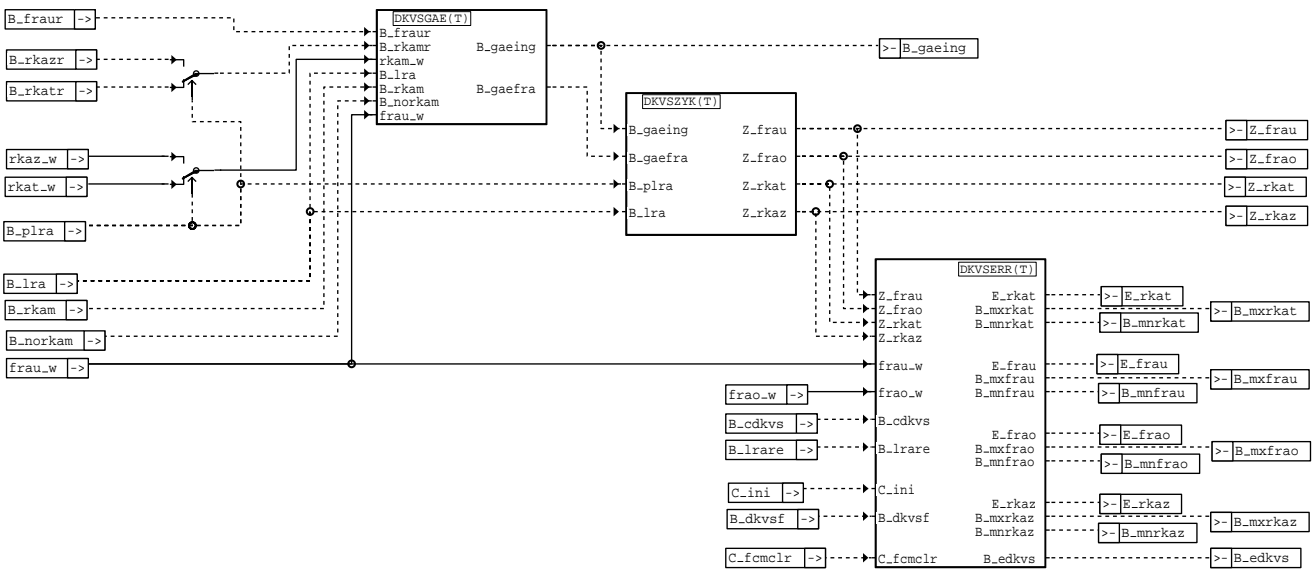
### FDEF DKVS 17.60 Function definition

DKVS : Plausibility test fuel supply systems



### dkvs-dkvs1

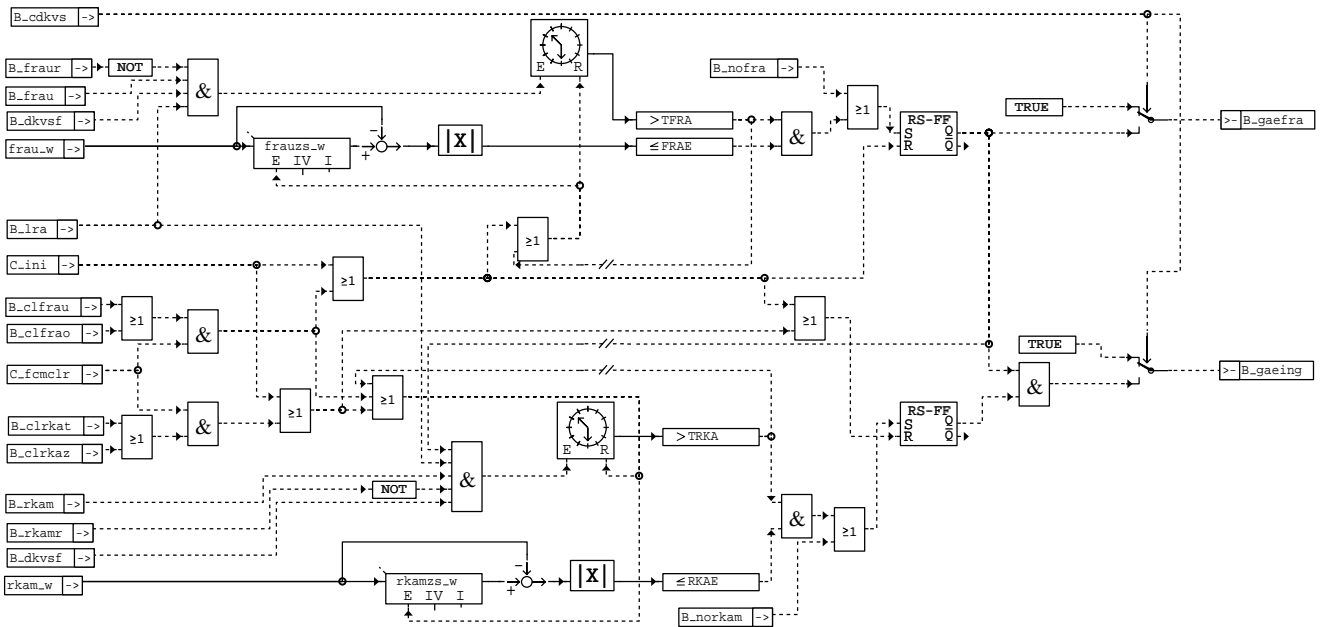
DKVSB1 : Formation of the cycle and error flags and checking on whether the basic adaptation stabilizes



### dkvs-dkvsb1

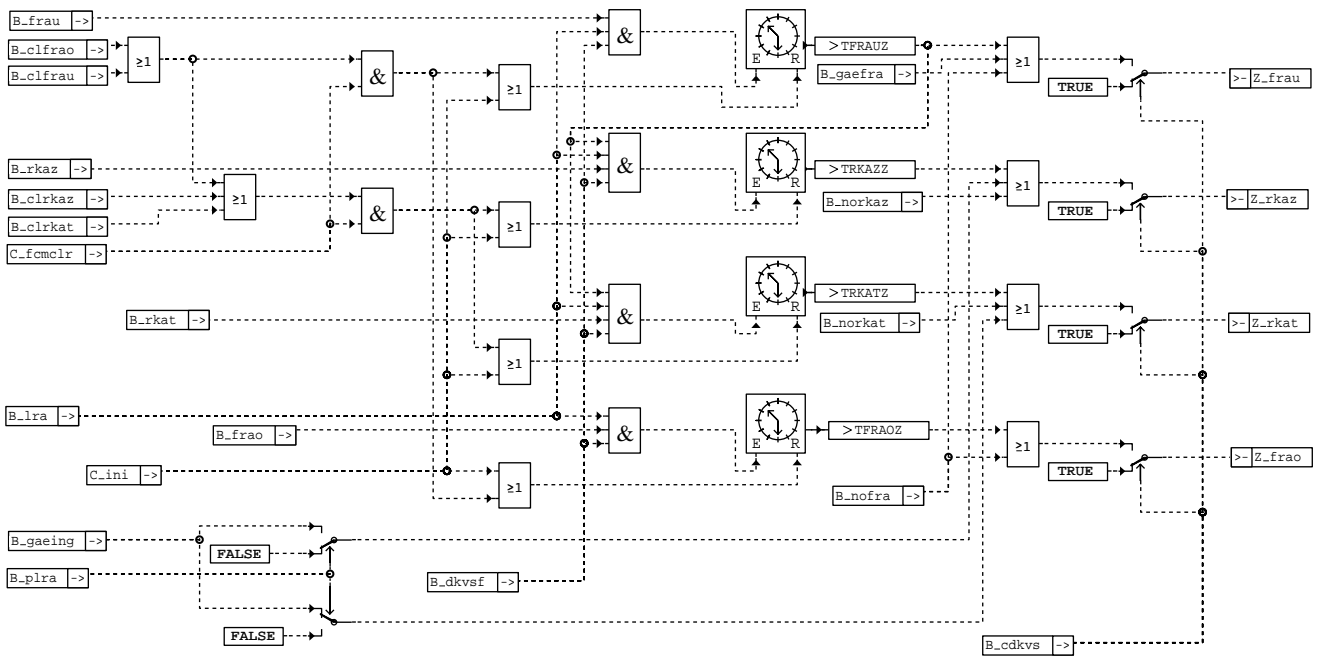


DKVSGAE :Checking on whether the basic adaptation stabilizes



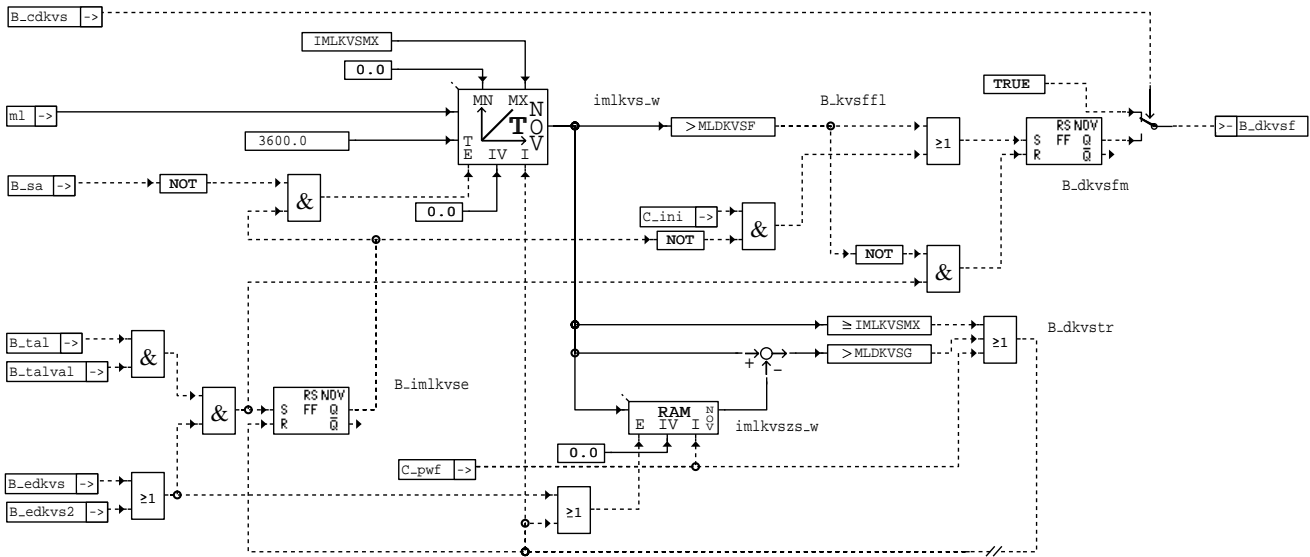
### dkvs-dkvsgae

DKVSYK : Setting of the cycle flag and checking on whether it is active for a minimum time



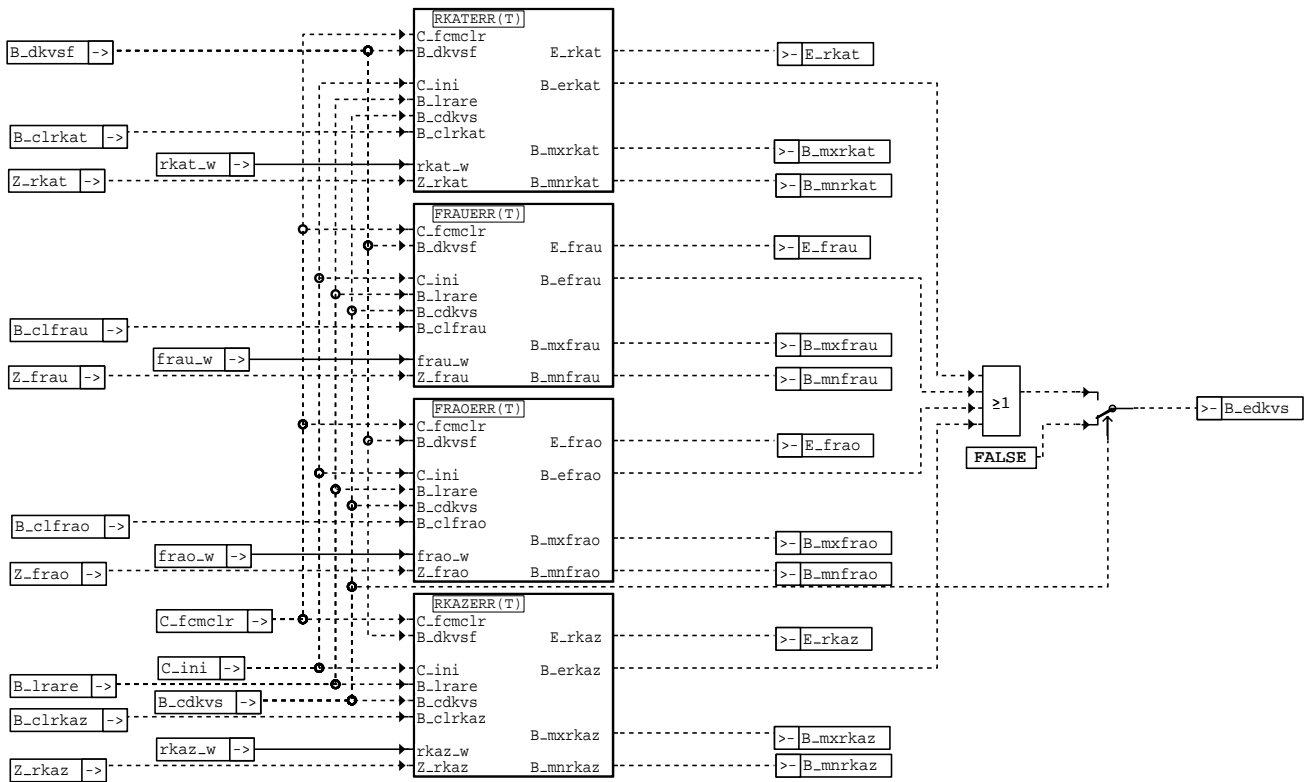
### dkvs-dkvszyk

DKVSES : By tank empty error disable



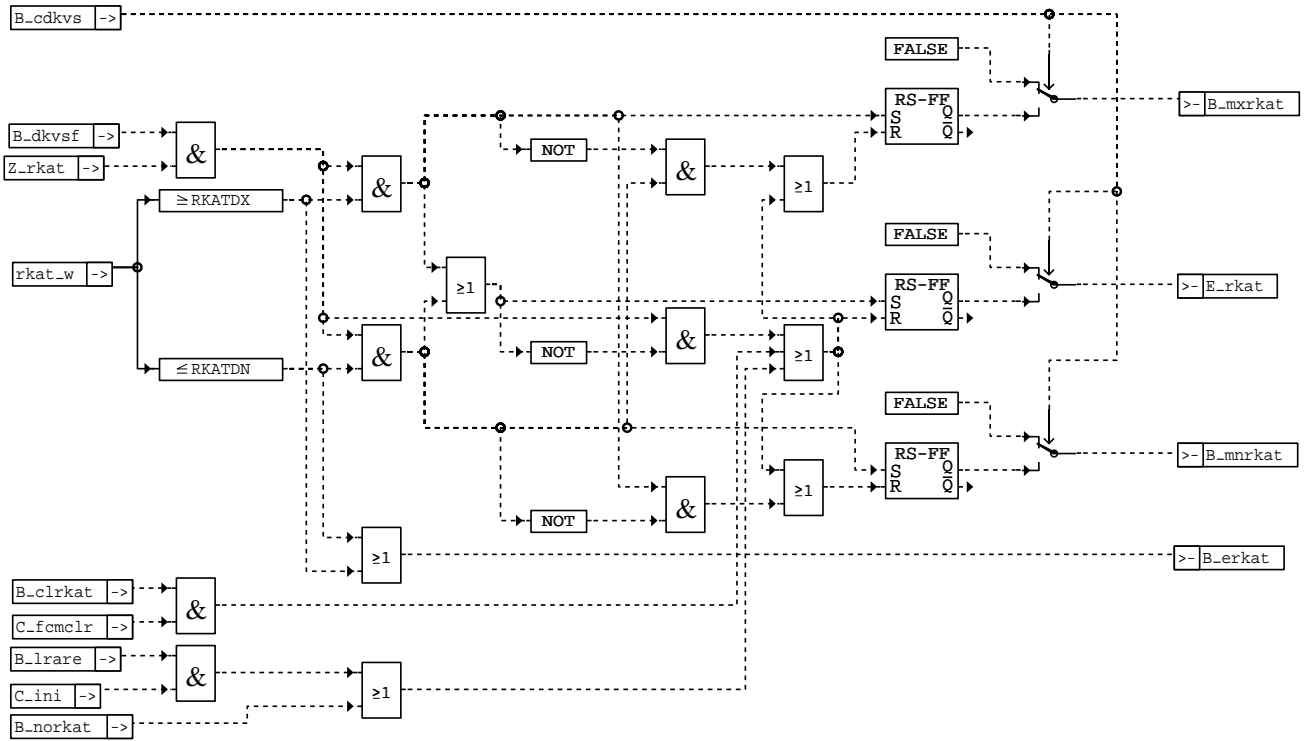
### dkvs-dkvses

DKVSERR :Formation of the error flag for FRAO, FRAO, RKAT and RKAZ



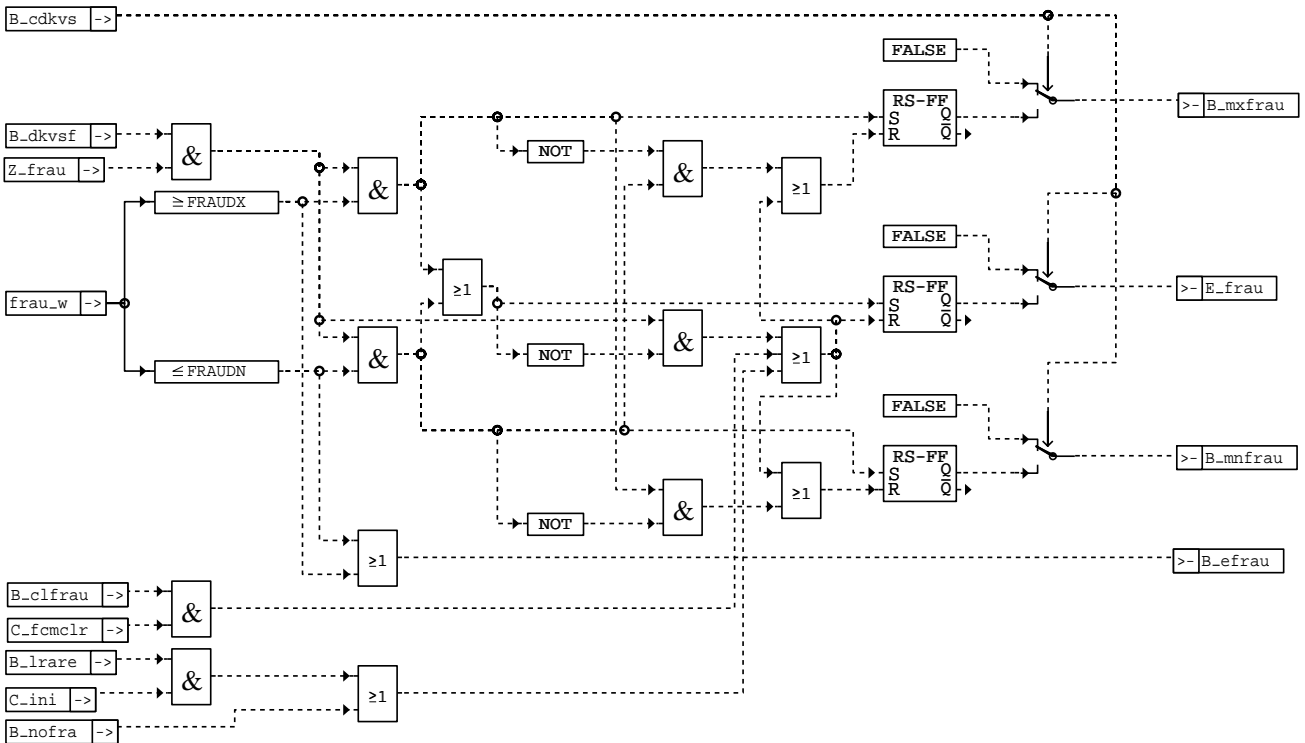
### dkvs-dkvserr

RKATERR : Checking of the additive adaptation correction per time RKAT for error



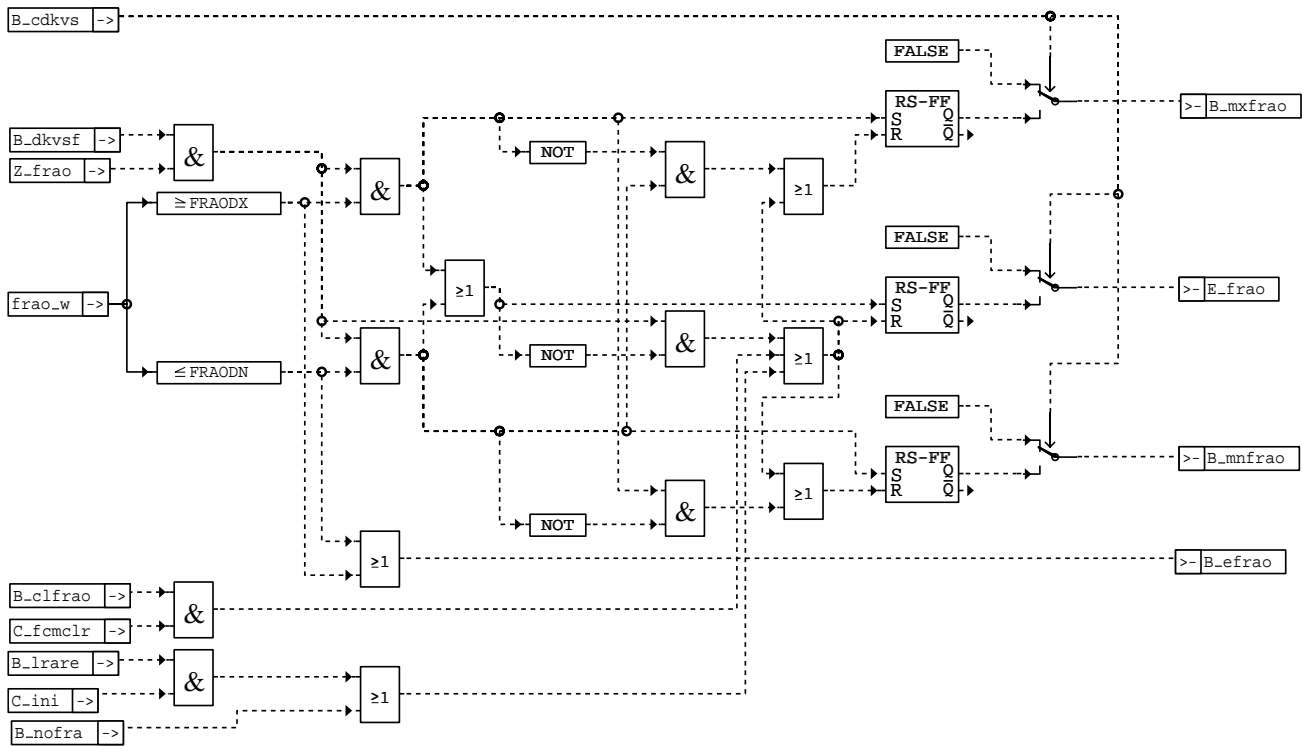
**dkvs-rkaterr**

FRAUERR : Checking of the lower multiplicative adaptation correction FRAU for error



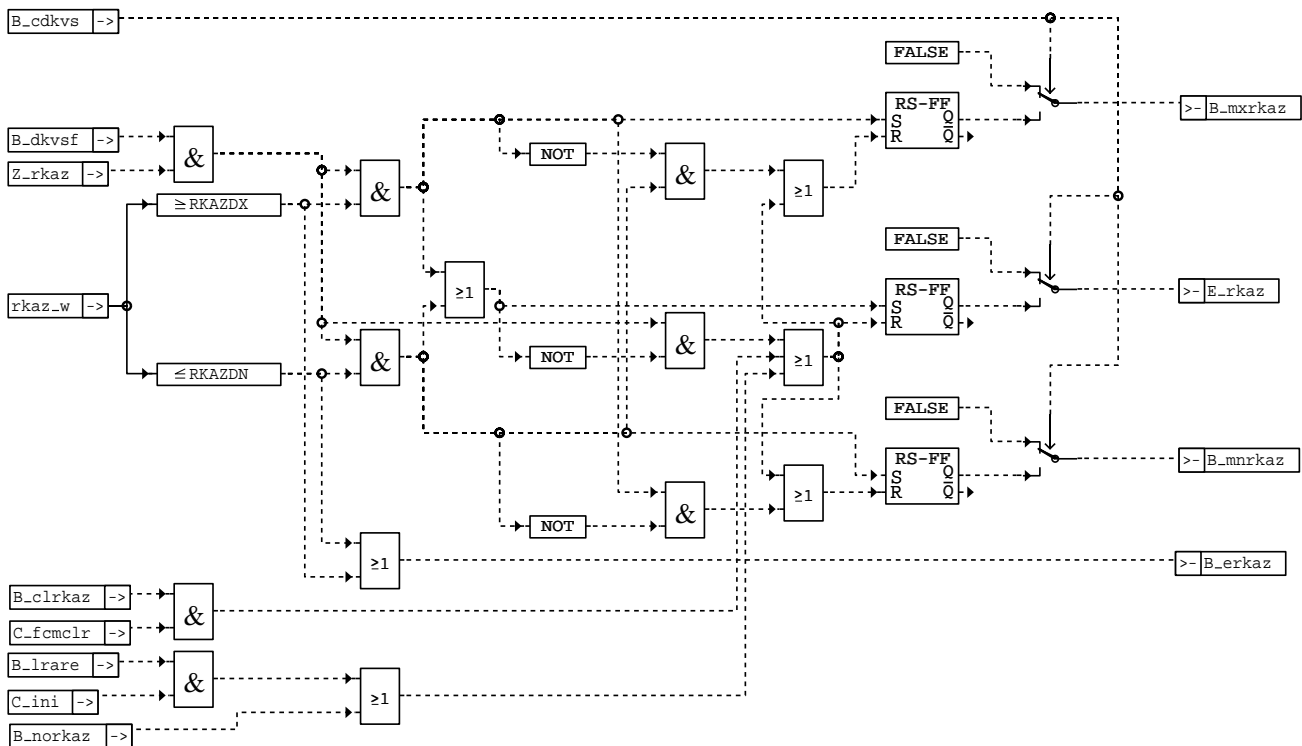
**dkvs-frauerr**

FRAOERR : Checking of the upper multiplicative adaptation correction FRAO for error



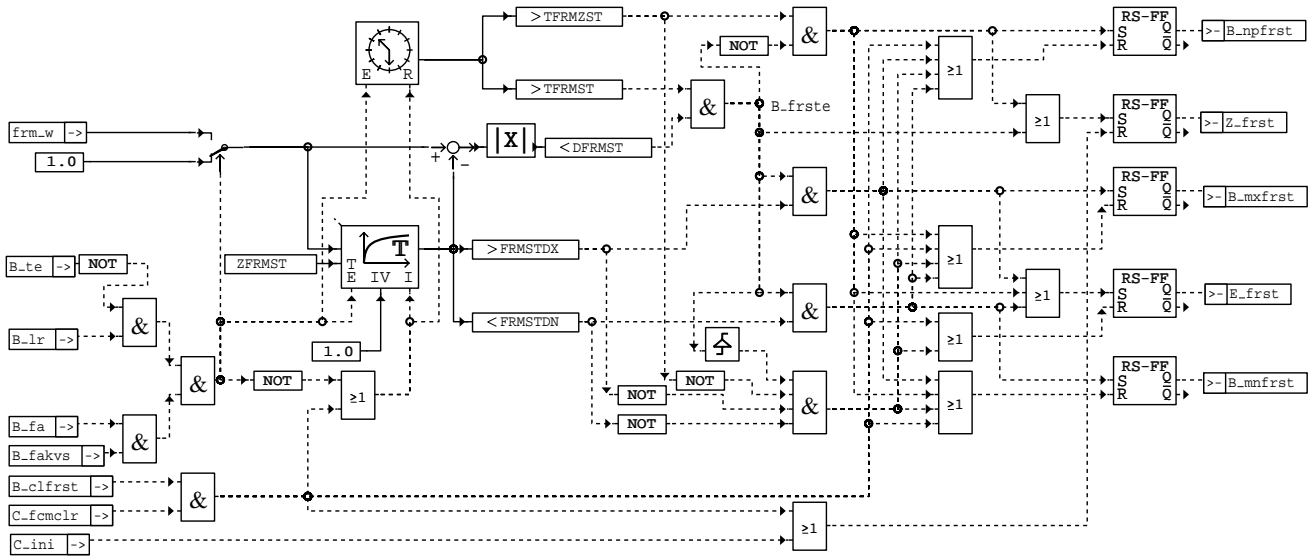
**dkvs-fraoerr**

RKAZERR : Checking of the additive adaptation correction per ignition RKAZ for error



**dkvs-rkazerr**

DKVSST : Short Test



### dkvs-dkvsst

In block diagrams error type informations as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the error path xyz back into the central diagnosis management DPFM. The bits E\_xyz, Z\_xyz, B\_mxyz etc. are contents of this status word. For error and cycle flags of external error paths which occur as inputs access methods are available which read these informations directly from the error path status managed in the DPFM.

For each error path xyz of this diagnosis function the following values are defined:

Status error path xyz	sfpxyz
Error flag xyz :	E_xyz
Cycle flag xyz :	Z_xyz
Error type xyz :	TYP_xyz : (B_mxyz, B_nxyz, B_sxyz, B_pxyz)
Delete error path:	B_clxyz
Substitution value active :	B_bkxyz (optional)
Error path code xyz:	CDTxyz
Error class xyz:	CLAxz
Error intensity xyz:	TSFxyz
CARB code xyz:	CDCxyz
Table of environm. cond.xyz:	FFTxyz

In this function definition (FDEF) the following error paths xyz are treated:

Error path name	used abbreviation (substitutes ,,xyz``)
upper multiplicative correction FRAO	frao
upper multiplicative correction FRAO2	frao2
lower multiplicative correction FRAU	frau
lower multiplicative correction FRAU2	frau2
additive correction per time RKAT	rkat
additive correction per time RKAT2	rkat2
additive correction per ignition RKAZ	rkaz
additive correction per ignition RKAZ2	rkaz2
Error path name for short test	used abbreviation (substitutes ,,xyz``)
short test Lambda control deviation	frst
short test Lambda control deviation	frst2

### ABK DKVS 17.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCFRAO	BLOKNR		KL	code word CARB: mixture adaptation factor frao
CDCFRAO2	BLOKNR		KL	code word CARB: mixture adaptation factor frao bank 2
CDCFRAU	BLOKNR		KL	code word CARB: mixture adaptation factor frau
CDCFRAU2	BLOKNR		KL	code word CARB: mixture adaptation factor frau bank 2
CDCFRST	BLOKNR		KL	code word CARB: deviation of lambda closed loop control
CDCFRST2	BLOKNR		KL	code word CARB : deviation of lambda closed loop control bank 2
CDCRKAT	BLOKNR		KL	code word CARB: additive adaptive mixture correction rkat
CDCRKAT2	BLOKNR		KL	code word CARB: additive adaptive mixture correction rkat bank 2
CDCRKAZ	BLOKNR		KL	code word CARB: additive adaptive mixture correction rkaz
CDCRKAZ2	BLOKNR		KL	code word CARB: additive adaptive mixture correction rkaz bank 2
CDLFRAO	BLOKNR		KL	code word lamp : LR-Adaptation multiplicative upper threshold
CDLFRAO2	BLOKNR		KL	code word lamp : LR-Adaptation multiplicative upper threshold bank 2





Parameter	Source-X	Source-Y	Type	Description
CDLFRAU	BLOKNR		KL	code word lamp: LR-Adaptation multiplicative lower threshold
CDLFRAU2	BLOKNR		KL	code word lamp: LR-Adaptation multiplicative lower threshold bank 2
CDLFRST	BLOKNR		KL	code word lamp: feul supply system short test
CDLFRST2	BLOKNR		KL	code word lamp: feul supply system short test bank 2
CDLRKAT	BLOKNR		KL	code word lamp : LR-Adaptation additive per time
CDLRKAT2	BLOKNR		KL	code word lamp : LR-Adaptation additive per time bank 2
CDLRKAZ	BLOKNR		KL	code word lamp : LR-Adaptation additive per ignition
CDLRKAZ2	BLOKNR		KL	code word lamp : LR-Adaptation additive per ignition bank 2
CPLRA			FW	Code word for switching DKVS from HFM- to pressure controlled system
DFRMST			FW	delta frm threshold for detection of successful basic mixt. adaptation
FRAE			FW	delta-fra-threshold for detection of successful basic mixture adaptation
FRAODN			FW	lower diagnostic threshold of frao correction
FRAODX			FW	upper diagnostic threshold of frao correction
FRAUDN			FW	lower diagnostic threshold of correction frau
FRAUDX			FW	upper diagnostic threshold of correction frau
FRMSTDN			FW	lower threshold for diagnosis (short test)
FRMSTDX			FW	upper threshold for diagnosis (short test)
IMLKVSMX			FW	maximum integration threshold for error enabled in DKVS (empty tank)
MLDKVSF			FW	Air mass threshold for error enable in DKVS (empty tank)
MLDKVSG			FW	air mass threshold for error enable empty tank
RKAE			FW	delta rkat- rkaz threshold for detection of successful basic mixt. adaptation
RKATDN			FW	lower threshold for diagnosis of additive correction per time
RKATDX			FW	upper threshold for diagnosis of additive correction per time
RKAZDN			FW	lower threshold for diagnosis of additive correction per ignition
RKAZDX			FW	upper threshold for diagnosis of additive correction per ignition
TFRA			FW	monitoring duration FRA
TFRAOZ			FW	duration of stay in FRAO for cycle flag with not successful adaptation
TFRAUZ			FW	duration of stay in FRAU for cycle flag with not successful adaptation
TFRMST			FW	monitoring duration frm sufficient
TFRMZST			FW	duration of stay for unplausable frm-signal (short test)
TRKA			FW	monitoring duration rkat, rkaz sufficient
TRKATZ			FW	activation duration rkat for setting the cycle-flag if B_gae = FALSE
TRKAZZ			FW	activation duration rkaz for setting the cycle-flag if B_gae = FALSE
ZFRMST			FW	time constant for frm-filter (short test)
Variable	Source		Type	Description
B_CDKVS	PROKON		EIN	function active per codeword CDKVS
B_CLFRAO			EIN	condition clear failure path FRAO (upper multipl. section)
B_CLFRAO2			EIN	condition clear failure path FRAO2 (stereo)
B_CLFRAU			EIN	condition clear failure path FRAU (lower multipl. section)
B_CLFRAU2			EIN	condition clear failure path FRAU2 (stereo)
B_CLFRST			EIN	condition clear failure path FRST (short test)
B_CLFRST2			EIN	condition clear failure path FRST (short test bank 2)
B_CLRKAT			EIN	condition clear failure path RKAT (add. per time)
B_CLRKAT2			EIN	condition clear failure RKAT2 (stereo)
B_CLRKAZ			EIN	condition clear failure RKATZ (add. per ignition)
B_CLRKAZ2			EIN	condition clear failure path RKAZ2 (stereo)
B_DKVSF	DKVS		AUS	condition: enabled of error
B_DKVSFM	DKVS		LOK	condition: enabled of error (flipflop output)
B_DKVSTR	DKVS		AUS	condition: integrator reset by tank empty
B_EDKVS	DKVS		AUS	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS		AUS	condition for adaption fault thresholds bank 2 momentarily exceeded
B_EFRAO	DKVS		LOK	Condition: diagnostic thresholds of upper multipl. correction actually exceeded
B_EFRAO2	DKVS		LOK	Condition: diagnostic thresholds (bank 2) of upper multipl. correction exceeded
B_EFRAU	DKVS		LOK	Condition diagnostic thresholds of lower multipl. correction actually exceeded
B_EFRAU2	DKVS		LOK	Condition diagnostic thresholds (bank 2) of lower multipl. correction exceeded
B_ERKAT	DKVS		LOK	Condition diagnostic thresholds of additive correction per time actually exceeded
B_ERKAT2	DKVS		LOK	Condition diagnostic thresholds (bank2) of additive correction per time exceeded
B_ERKAZ	DKVS		LOK	Condition: diagnostic thresholds of add. correction per inj. actually exceeded
B_ERKAZ2	DKVS		LOK	Condition: diagnostic thresholds (bank2) of add. correction per inj. exceeded
B_FA			EIN	condition general function request
B_FAKVS			EIN	condition function request diagnoses fuel supply system
B_FRAO	LRA		EIN	condition for enabling adaption of frao
B_FRAU	LRA		EIN	condition enable adaptation of frau
B_FRAUR	LRA		EIN	condition frau-integrator outside reduced thresholds
B_FRAUR2	LRA		EIN	condition frau2-integrator outside reduced thresholds
B_FRSTE	DKVS		LOK	condition frm stabilized (short test)
B_FRSTE2	DKVS		LOK	condition frm2.w stabilized (short test 2. bank)
B_GAE	DKVS		AUS	condition for adaptive Lambda pilot control successful
B_GAEFRA	DKVS		AUS	condition for fra portion of adaptive Lambda pilot control successful
B_GAEFRA2	DKVS		AUS	condition for fra2 portion of adaptive lambda pilot control successful
B_GAEING	DKVS		LOK	condition basic adaption Bank 1 steady state
B_GAEING2	DKVS		LOK	condition for adaptive lambda pilot control 2 successful
B_JMLKVSE	DKVS		LOK	condition air mass integrator reset
B_KVSFFL	DKVS		LOK	condition: enable of error in spite of empty tank
B_LR	LREB		EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB		EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRA	LRAEB		EIN	condition for basic mixture adaptation enabled
B_LRA2	LRAEB		EIN	condition for basic mixture adaption 2 enabled
B_LRARE	LRA		EIN	condition reset of mixture adaptation
B_LRARE2	LRA		EIN	condition reset of mixture adaptation bank 2



Variable	Source	Type	Description
B_MNFRAO	DKVS	LOK	condition below low plausibility threshold (upper multipl. section)
B_MNFRAO2	DKVS	LOK	condition below low plausibility threshold (stereo)
B_MNFRAU	DKVS	LOK	condition below low plausibility threshold (lower multipl. section)
B_MNFRAU2	DKVS	LOK	condition below low plausibility threshold (stereo)
B_MNFRST	DKVS	LOK	condition below low plausibility threshold (short test)
B_MNFRST2	DKVS	LOK	condition below low plausibility threshold (short test stereo)
B_MNRKAT	DKVS	LOK	condition below low plausibility threshold (add. per time)
B_MNRKAT2	DKVS	LOK	condition below low plausibility threshold (stereo)
B_MNRKAZ	DKVS	LOK	condition below low plausibility threshold (add. per ignition)
B_MNRKAZ2	DKVS	LOK	condition below low plausibility threshold (stereo)
B_MXFRAO	DKVS	LOK	Condition: upper plausible value exceeded (frao)
B_MXFRAO2	DKVS	LOK	Condition: upper plausible value exceeded (bank 2) (frao2)
B_MXFRAU	DKVS	LOK	Condition: upper plausible value exceeded (frau)
B_MXFRAU2	DKVS	LOK	Condition: upper plausible value exceeded (multiplicative 2. bank )
B_MXFRST	DKVS	LOK	Condition: upper plausible value exceeded (short test)
B_MXFRST2	DKVS	LOK	Condition: upper plausible value exceeded (short test stereo)
B_MXRKAT	DKVS	LOK	Condition: upper plausible value exceeded (rkat)
B_MXRKAT2	DKVS	LOK	Condition: upper plausible value exceeded (Bank 2) (rkat2)
B_MXRKAZ	DKVS	LOK	Condition: upper plausible value exceeded (rkaz)
B_MXRKAZ2	DKVS	LOK	Condition: upper plausible value exceeded (bank 2) (rkaz)
B_NOFRA	LRA	EIN	condition no fra adaptation active
B_NORKAM	DKVS	LOK	condition additive correction of the mixture adaptation switched off
B_NORKAT	LRA	EIN	condition additive correction of the mixture adaptation switched off
B_NORKAZ	LRA	EIN	condition additive correction of the mixture adaptation switched off
B_NPFRST	DKVS	LOK	condition for fault type "unplausible signal" detected (DKVS short test)
B_NPFRST2	DKVS	LOK	condition for fault type "unplausible signal" detected (DKVS short test bank 2)
B_PLRA	DKVS	LOK	Condition: Switch over from HFM to pressure controlled system
B_RKAM	DKVS	LOK	Condition: One of both additive LRA sections is active
B_RKAMR	DKVS	LOK	Condition: rkaz or rkat has exceeded it's thresholds
B_RKAMR2	DKVS	LOK	Condition: rkaz2 or rkat2 has exceeded it's thresholds
B_RKAT	LRA	EIN	condition adaptation area rkat active
B_RKATR	LRA	EIN	condition rkat-integrator outside reduced thresholds
B_RKATR2	LRA	EIN	condition rkat2-integrator outside reduced thresholds
B_RKAZ	LRA	EIN	condition adaptation area rkaz active
B_RKAZR	LRA	EIN	condition rkaz-integrator outside reduced thresholds
B_RKAZR2	LRA	EIN	condition rkaz2-integrator outside reduced thresholds
B_SA	MDRED	EIN	Condition fuel cut-off
B_TAL	GGFST	EIN	Condition tank empty or reserve
B_TALVAL	GGFST	EIN	condition ; bit empty tank valid
B_TE	TEBEB	EIN	Condition canister purge active
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_FRAO	DKVS	AUS	error flag: upper multiplicative mixture adaption factor frao
E_FRAO2	DKVS	AUS	error flag: upper multiplicative mixture adaption factor frao2
E_FRAU	DKVS	AUS	error flag: lower multiplicative mixture adaption factor frao
E_FRAU2	DKVS	AUS	error flag: lower multiplicative mixture adaption factor frao2
E_FRST	DKVS	AUS	error flag: fuel supply system (short test)
E_FRST2	DKVS	AUS	error flag: fuel supply system (short test bank 2)
E_RKAT	DKVS	AUS	error flag DKVS (additive correction per unit of time)
E_RKAT2	DKVS	AUS	error flag DKVS (additive correction per unit of time, bank 2)
E_RKAZ	DKVS	AUS	error flag DKVS (additive correction per ignition)
E_RKAZ2	DKVS	AUS	error flag DKVS (additive correction per ignition, bank 2)
FRAO2_W	LRA	EIN	multipl. mixture adaptation factor higher load bank 2 (Word)
FRAO_W	LRA	EIN	multipl. mixture adaptation factor higher load (word)
FRAU2_W	LRA	EIN	multipl. mixture adaptation factor of the lower mult. section of bank 2 (Word)
FRAUZS2_W	DKVS	LOK	multipl. mixture adaptation factor of the lower mult. section (stereo)
FRAUZS_W	DKVS	LOK	multipl. mixture adaptation factor of the lower section (old value)
FRAU_W	LRA	EIN	multipl. mixture adaptation factor of the lower mult. section (Word)
FRM2_W	LR	EIN	fast mean value of lambda control factor bank 2(word)
FRM_W	LR	EIN	fast mean value of lambda control factor (word)
IMLKVSZS_W	DKVS	LOK	stored value:air mass after DKVS fault with empty fuel tank
IMLKVS_W	DKVS	LOK	air mass after DKVS fault with empty fuel tank
ML	SWADAP	EIN	air mass flow
RKAM2_W	DKVS	LOK	Selection of additive correction of the mixture adaptation for calc. of B_gae2
RKAMZS2_W	DKVS	LOK	correction additive (per time or ignition) bank 2 ( old value)
RKAMZS_W	DKVS	LOK	correction additive (per time or ignition); old value
RKAM_W	DKVS	LOK	Selection of additive correction of the mixture adaptation for calc. of B_gae
RKAT2_W	LRA	EIN	additive correction (per time) of the mixture adaptation bank 2 (Word)
RKAT_W	LRA	EIN	additive correction (per time) of the mixture adaptation (Word)
RKAZ2_W	LRA	EIN	additive correction (per ignition) of the mixture adaptatition Bank 2 (Word)
RKAZ_W	LRA	EIN	additive correction (per ignition) of the mixture adaptation
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
Z_FRAO	DKVS	AUS	cycle flag of mixture adaption factor frao
Z_FRAO2	DKVS	AUS	cycle flag of mixture adaption factor frao2 (bank 2)
Z_FRAU	DKVS	AUS	cycle flag of mixture adaption factor frau
Z_FRAU2	DKVS	AUS	cycle flag of mixture adaption factor frau2 (bank 2)
Z_FRST	DKVS	AUS	cycle flag: fuel supply system (short test)
Z_FRST2	DKVS	AUS	cycle flag: fuel supply system (short test bank 2)
Z_RKAT	DKVS	AUS	cycle flag of additive adaptive mixture correction per time
Z_RKAT2	DKVS	AUS	cycle flag of additive adaptive mixture correction per time (bank 2)



Variable	Source	Type	Description
Z_RKAZ	DKVS	AUS	cycle flag of additive adaptive mixture correction rkaz
Z_RKAZ2	DKVS	AUS	cycle flag of additive adaptive mixture correction rkaz (bank 2)

### FW DKVS 17.60 Fixed Values

Parameter	Value	Description
CPLRA		Code word for switching DKVS from HFM- to pressure controlled system
DFRMST		delta frm threshold for detection of successful basic mixt. adaptation
FRAE		delta-fra-threshold for detection of successful basic mixture adaptation
FRAODN		lower diagnostic threshold of frao correction
FRAODX		upper diagnostic threshold of frao correction
FRAUDN		lower diagnostic threshold of correction frau
FRAUDX		upper diagnostic threshold of correction frau
FRMSTDN		lower threshold for diagnosis (short test)
FRMSTDX		upper threshold for diagnosis (short test)
IMLKVSMX		maximum integration threshold for error enabled in DKVS (empty tank)
MLDKVSF		Air mass threshold for error enable in DKVS (empty tank)
MLDKVSG		air mass threshold for error enable empty tank
RKAE		delta rkat- rkaz threshold for detection of successful basic mixt. adaptation
RKATDN		lower threshold for diagnosis of additive correction per time
RKATDX		upper threshold for diagnosis of additive correction per time
RKAZDN		lower threshold for diagnosis of additive correction per ignition
RKAZDX		upper threshold for diagnosis of additive correction per ignition
TFRA		monitoring duration FRA
TFRAOZ		duration of stay in FRAO for cycle flag with not successful adaptation
TFRAUZ		duration of stay in FRAU for cycle flag with not successful adaptation
TFRMST		monitoring duration frm sufficient
TFRMZST		duration of stay for unplausable frm-signal (short test)
TRKA		monitoring duration rkat, rkaz sufficient
TRKATZ		activation duration rkat for setting the cycle-flag if B_gae = FALSE
TRKAZZ		activation duration rkaz for setting the cycle-flag if B_gae = FALSE
ZFRMST		time constant for frm-filter (short test)

**FB DKVS 17.60 Detailed description of function**

## Introduction:

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The OBD II legislation requires monitoring of the fuel supply system. A defective fuel supply system leads to deviations in the pilot mixture control. As a result, the average control factor (frm) will deviate from factor 1.0.

The mixture adaptation (LRA) will try to "learn" such errors in order to correct the error even during dynamic engine operation in the best possible way. The best result is obtained for errors with a specifically assigned LRA integrator. Examples are:

- rkat in case of an additive error per time (leakage air)
- frau, frao in case of a multiplicative error (pressure controller tolerance or fluctuating fuel density)
- rkaz in case of an additive error per ignition (injection valve-delay time TVUB wrong)

Within certain limits (+/- 25% multiplicative and +/- 25% additive) the mixture adaptation is capable of correcting such an error with only little impact on emissions. Errors, however, which deviate from the above-mentioned characteristics cause continuously activated integrators. In this case only part of the error can be compensated and a residual error remains which must constantly be compensated by the Lambda controller dependent on the load and engine speed point. In this case the legal emission limits may be exceeded by factor 1.5 even in case of small deviations of the LRA integrators from the neutral value. This must be taken into consideration when selecting the diagnosis thresholds.

The diagnosis thresholds of the LRA adaptation values are to be determined such that the emissions do not exceed the defined limits with respect to the factor 1.5 (see block APP).

The DKVS is closely connected to the mixture adaptation (LRA) and it evaluates the following integrators of the mixture adaptation:

- RKAT...: additive error per time (e.g. leakage air)
- FRAU...: multiplicative error (at average air masses - lower multiplicative range)
- FRAO...: multiplicative error (at high air masses - upper multiplicative range)
- RKAZ...: additive error per ignition (e.g. wrongly adjusted valve delay time TVUB)

Apart from the error flags (E\_xyz) and the corresponding cycle flags (Z\_xyz) the DKVS also provides the information "basic adaptation stabilized" (B\_gae). Once the adaptation has stabilized an early switch-over to long canister purge phases can be performed (see phase control %BBTEGA).

Apart from the integrator values (rkat\_w, frau\_w, frao\_w and rkaz\_w) and the conditions B\_rkat, B\_frau, B\_rkaz and B\_frao, the DKVS also needs the information from the mixture adaptation whether the corresponding integrator has reached resp. exceeded one of the reduced thresholds.

- B\_rkatr: a reduced threshold of rkat reached resp. exceeded
- B\_fraur: a reduced threshold of frau reached resp. exceeded
- B\_fraor: is not needed since frao is not checked for stabilization
- B\_rkazr: a reduced threshold of rkaz reached resp. exceeded

As soon as the reduced thresholds are reached resp. exceeded the bit "mixture adaptation stabilized" (B\_gae) can no longer be set.

The reduced thresholds were introduced in order to avoid possible error messages which mistakenly occur under certain conditions (e.g. high charge of the activated carbon filter).

The banks 1 and 2 have the same structure. Where bank-specific signals occur an index (2) is given for the second bank. Example: frau\_w(2) means frau\_w for bank 1 and frau2\_w for bank 2.



The diagnosis fuel supply systems (DKVS) consists of the following partial functions :

Partial function block DKVSGAE(2) :

In this partial function it is checked whether the basic adaptation has stabilized (B\_gaeing(2) = TRUE). It only monitors the adaptation stabilization of 2 LRA integrators. One of these integrators is the FRAU. The other is either the RKAT (HFM-systems) or the RKAZ (P-load acquisition). The switch-over is performed outside of this partial function via the code word CPLRA. If CPLRA > 0 then the RKAZ (adaptive correction per ignition) is monitored for stabilization and if CPLRA = 0 the RKAT (adaptive correction per time) is monitored. It is recommendable to always deactivate the integrator not needed in the LRA (B\_norkaz = TRUE with HFM load acquisition or B\_norkat = TRUE with P-load acquisition) => see %LRA - partial function BBLRA.

If frau, frao ist stopped by B\_nofra, B\_gaefra is set.  
If rkat ist stopped by B\_norkat and CPLRA = 0 the Flip-Flop for B\_gaeing is set.  
If rkaz ist stopped by B\_norkaz and CPLRA = 1 the Flip-Flop for B\_gaeing is set.  
With this method "B\_gae can be set TRUE" also if one range is stopped!

The bit "basic adaptation stabilized" is needed:

- for a quick switch-over to long canister purge phases (TTE -> TTEAE) in the function %BBTEGA
- for a quick setting of the cycle flags of the DKVS (Z\_rkat(2), Z\_frau(2), Z\_frao(2) and Z\_rkaz(2)).
- as an information for other diagnosis functions

Generally it can be assumed that an integrator of the LRA has stabilized if the corresponding integrator changed only little during the time in which it was active.

However, if only a fixed load / engine speed point (e.g. idle speed) is entered an intergrator (e.g. RKAT) may stabilize even though it falsely learned a mixture error (e.g. multiplicative error) which does not belong in this range. In order to avoid a too early setting of the bit B\_gaeing(2) the check on stabilization in the additive range (RKAM = RKAT resp. RKAZ) is only performed after FRAU has stabilized (B\_gaefra(2) = TRUE). The basic adaptation stabilizes only once both monitored integrators have stabilized (B\_gaeing(2) = TRUE).

The check in detail:

At the beginning of the check (e.g. from start for FRAU, resp. after FRAU has stabilized for RKAM) the adaptation value frau\_w is temporarily stored in frau\_w resp. rkam\_w in rkamz\_w. Then the time during which the condition for the adaptation of the variables FRAU resp. RKAM were fulfilled is measured starting from the beginning.

The time counter is only active if frau\_w (rkam\_w) has not already reached or undershot resp. exceeded one of the reduced thresholds FRAURX resp. FRAURN(RKATRX resp. RKATRN or RKAZRX resp. RKAZRN) and the Bit B\_dkvsf is set to TRUE.

Reason: A forced limitation on the reduced threshold may not be interpreted as stabilized state.

After the time TFRA (TRKA) has passed an inquiry is made whether the adaption has deviated by more than FRAE (RKAE) from the starting value. If this is not so then the FRAU- resp. the RKAM-adaptation has stabilized and the flags B\_gaefra(2) and B\_gaeing(2) are set.

The flags B\_gaefra(2) and B\_gaeing(2) are set to FALSE under the following conditions :

- in case of start (C\_ini = TRUE)
- reset of all integrators of the LRA during the initialization phase (B\_lrare(2) = TRUE, this bit is formed in %LRA)
- individual error path deletion:
  - deleting of the error path FRAO(2) or FRAU(2) i.e.. B\_clfrao(2) or B\_clfrau(2) equal TRUE and C\_fmclr = TRUE  
=> B\_gaefra(2) and B\_gaeing(2) = FALSE
  - deleting of the error path RKAT(2) or RKAZ(2) => o n l y B\_gaeing(2) = FALSE is set.
- the additive corrections of the mixture adaptation RKAT or RKAZ are switched off with B\_norkat resp. B\_norkaz (selecting via codeword CPLRA => B\_norkam = TRUE)

B\_gaefra(2) and B\_gaeing(2) are set to TRUE if B\_cdkvs was set to FALSE by the bit no. ZERO of the code word CDKVS (in %PROKON). In this case this block is not calculated. They are also set TRUE, if the range, that is needed for a TRUE is stopped by B\_noxxx.

On the stereo version the adaptation has stabilized once both banks have stabilized (B\_gaeing and B\_gaeing2 equal TRUE).



Partial function block DKVSZYK(2) :  
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The task of this partial function is the formation of the cycle flags (Z\_rkat(2), Z\_rkaz(2), Z\_frau(2) and Z\_frao(2)).

- The cycle flag Z\_frau(2) is set if
  - a) the accompanying integrator has stabilized in LRA. The stabilization of the FRAU(2)-integrators is signaled by the bit B\_gaeFra(2) from the partial function DKVSGAE.
  - b) the time during which the adaptation is active in the FRAU range is larger than a defined threshold (TFRAUZ).  
This setting of the cycle flag is described as "forced setting".
- The cycle flag Z\_frao(2) is set if the passed time during active Lambda control in the FRAO range is larger than the adjustable threshold TFRAOZ.
- The cycle flag Z\_rkaz(2) is set if
  - a) in case of the set bit B\_plra the accompanying integrator RKAZ(2) has stabilized in the LRA. The stabilization of the RKAZ(2) integrator is signaled by the bit B\_gaeing(2) = TRUE from the partial function DKVSGAE.
  - b) in case of the not set bit B\_plra the time during which the adaptation is active in the RKAZ range is larger than TKRAZZ.  
In this case the cycle flag Z\_frau must be set beforehand.
- The cycle flag Z\_rkat(2) is set if
  - a) in case of the not set bit B\_plra the accompanying integrator has stabilized in the LRA. The stabilization of the RKAT(2) integrator is signaled by the bit B\_gaeing(2) = TRUE from the partial function DKVSGAE.
  - b) in case of the set bit B\_plra the time during which the adaptation is active in the RKAT range is larger than TKRATZ.  
In this case the cycle flag Z\_frau must be set beforehand.

The cycle flags Z\_frau(2), Z\_frao(2), Z\_rkaz(2) and Z\_rkat(2) are set to TRUE if B\_cdkvs = FALSE. In this case the function is not calculated. They are also set TRUE, if the range is stopped by B\_noxxx.

The timers and thus the cycle flags are reset under the following conditions:

- a) in case of start (C\_ini = TRUE)
- b) in case of delete error path FRAO(2) or delete FRAU(2)
- c) in case of delete error path RKAT(2) or RKAZ(2) only the cycle flags Z\_rkat(2) and Z\_rkaz(2) are set to FALSE by the resetting of the accompanying timers.

The resetting of all cycle flags in case of condition b) is necessary because the stabilization of the integrators RKAZ resp. RKAT is only checked for after the FRAU integrator has stabilized. The condition c) is permitted because after the RKAT resp. the RKAZ integrators were deleted only the stabilization behaviour of the RKAT resp. the RKAZ integrator is observed for the setting of the bit B\_gaeing(2).

## Partial function block DKVSES :

In order to avoid an error diagnosis in DKVS ( fuel supply system) due to an empty tank, the sitting of error flag is prohibited for a definite time (if one of the threshold diagnosis is exceeded or undershot). Because for the reason the air mass throughput is integrated so much that, the threshold MLDKVSF is exceeded. In fuel cut off the integrator is stopped. The Integrator is initialized with the value Zero and then stopped, if after enable in next driving,

a) the air mass integrator is integrated at least MLDKVSG (imlksv - imlksvzs > MLDKVSG)  
b) The integrator has reached his maximum. Remark: The integrator is limited to maximal value IMLKVSXM.

The bit B\_dkvsf by the make ones debut of error with an empty tank is set to FALSE und as a result, the DKVS is deactivated against the error diagnosis.

The bit B\_dkvsf is set to TRUE und so error identify is enabled, if

- a) the integrator is exceeded the value MLDKVSF(B\_kvsffl=TRUE).  
b) in case of start (C\_ini=TRUE) if the bit B\_imlkvse is set to FALSE

## Partial function block DKVSERR(2) :

This partial function consists of four further partial functions (RKATERR(2), FRAUERR(2), FRAOERR(2), RKAZERR(2)). The task of each partial function is the formation of the error bit E\_xyz(2) and the formation of the flag error type (B\_mnxyz(2), B\_mxyz(2)). Since these partial functions all show the same structure here only the partial function FRAUERR is described.

Description of the partial function FRAUERR:

- Formation of the flags E\_frau, B\_mxfrau and B\_mnfrau

If in case of set cycle flag the adaptation value frau\_w reaches resp. exceeds the upper diagnosis threshold FRAUDX resp. the lower diagnosis threshold FRAUDN and the bit tank empty is enabled then E\_frau is set to TRUE. When the cycle flag Z\_frau is set the error type B\_mxfrau is detected if frau\_w is greater than or equal to the diagnosis threshold FRAUDX and the errors B\_mnfrau are detected if the adaptation value frau\_w is less than or equal to the diagnosis threshold FRAUDN.

In addition to the error flag E\_frau a quick error message for the blocking of other diagnosis functions in case of an error is needed. In this case the error bit B\_efrau is set to TRUE when an error threshold is exceeded. The bit B\_efrau is not directly available to other diagnosis functions but the bit B\_edkvs(2) is formed by an OR operation of the four error bits B\_efrau(2), B\_efrao(2), B\_erkat(2) and B\_erkaz(2).

The error flag is again reset during a drive while the cycle flag is set if frau\_w is in the permitted diagnosis range. This means that the error flag can be set and again reset as often as desired during a drive.

The error flag (E\_xyz) and the fault type (B\_mnxyz, B\_mxyz) are set to FALSE with B\_noxyz = TRUE.

## Partial function block DKVSST(2) :

This subfunction is needed for a short test. If low pass filtered frm\_w(2)-signal has stabilized, the error flags E\_frst(2), B\_mxfrst(2) (max. permissible frm\_w(2)-value) oder B\_mnfrst(2) (min permissible frm\_w(2)-value) are set in relatet of diagnosis thershold FRMSTDx resp. FRMSTDN.

The frm\_w(2) signal has stabilized, if the time TFRMST is passed and the change of frm\_w(2) is less then DFRMST. If the time TFRMZST is passed and the change of frm\_w(2) ist not less then DFRMST, the error flags E\_frst(2), B\_npfrst(2) (für unplaussible signal) and the cycle flag Z\_frst are set of TRUE.

The time counter and the low pass filter are enabled, if

- canister purge is not active (B\_te = FALSE).
- lambda closed loop control is active (B\_lr(2) = TRUE).
- the function request will be actived by the tester (B\_fa and B\_fakvs are TRUE).
- condition clear failure path FRST (B\_clfrst(2) = TRUE and C\_fmclr) are not set

With cancel of the function request the cycle flag, the error flag, und the error type flags are unchanged (Z\_frst(2), E\_frst(2), B\_mxfrst(2), B\_mnfrst(2) and B\_npfrst(2) ). A reset of the cycle flag is done at engine start (C\_ini).

If there is no error detected a Reset of the error flag is possible if the thresholds are not exceeded while the positive slope of B\_frste is detected.

**APP DKVS 17.60 Application hint**

## Application process :

It is sensible to start the application of the DKVS only once the application of the Lambda controller, of the transient control, of the charge acquisition, of the torque management and of the idle speed control has been terminated. In the mixture adaptation especially adaptation speeds (ZKFRAU,...) and the adaptation ranges (MLU2,...) shall be determined. In the LRA reduced thresholds shall be set to maximum thresholds ( FRAURX = FRAUMX, FRAURN = FRAUMN, RKATRX = RKATMX, RKAZRN = RKAZMN, a.s.o.).

An exception is RKATRN.

Application of the partial function DKVSGAE :

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## Application values

TFRA	Detection time for stabilized basic adaptation of FRAU	[8..10..12] sec
TRKA	Detection time for stabilized basic adaptation of RKAT or RKAZ	[4..6..8] sec
FRAE	Delta-FRAU for detection of the stabilized adaptation value FRAU	[0,01..0,03..0,05]
RKAE	Delta-RKAT resp. RKAZ for detection of the stabilized adaptation value RKAT resp. RKAZ	[0,2..0,6..1,0] %

The values indicated in the middle are reference values

By means of the partial function DKVSGAE the adaptation values FRAU and alternative RKAT (HFM system) or RKAZ (P-load acquisition) are checked for stabilization.

Frau\_w is the lower multiplicative adaptation correction. A multiplicative error only differs significantly from an additive error if air masses >> idle speed air mass. For this reason the application values TFRA and FRAE should be chosen such that the bit B\_gaeFra can be set in the FTP75 in the large hill.

The choice of the value FRAE is directly dependent on the adaptation speed ZKFRAU. It should be chosen such that in case of a frm\_w deviation from the neutral value 1.0 by 3% to 7% B\_gaeFra(2) is just not set. A multiplicative error can be simulated e.g. by an adjustable pressure controller. It should be possible to adjust the pressure between 1 and 6 bar so that a delta Lambda of +- 25 % can be adjusted. In future the CARB also allows an error simulation by manipulation of the ECU (e.g. multiplication of the injection time by a factor).

RKAZ resp. RKAT are the additive adaptation correction values and they act significantly in the low load range respectively load / engine speed range. The application values TRKA and RKAE should be chosen such that the bit B\_gaeing(2) can be set in the FTP75 during idling after the big hill. Here again the value RKAE depends on the adaptation speed ZKRKAZ resp. ZKRKAT. It should be chosen in such a way that in case of a frm deviation by more than 3% - 7% no stabilization is detected. Via the code word CPLRA it is possible to switch from the detection of RKAT having stabilized to RKAZ having stabilized. It is recommendable to deactivate the integrator in %LRA which was not checked for stabilization via the code word NOLRA. An additive error can be simulated by a leakage after the HFM in the intake manifold. A leakage of 3-4 mm diameter proved itself useful for a certification on a 2.4 l engine. With lager holes it may happen that the engine no longer starts. Leakage air can also be simulated by a drop-off of the crankcase purge pipe (if there is one).





Application of the partial function DKVSZYK :  
-----

A p p l i c a t i o n   v a l u e s

TFRAUZ	Waiting time for the forced setting of the adaption correction FRAU	[20..30..50] sec
TFRAOZ	Waiting time for the forced setting of the adaption correction FRAO	[20..30..50] sec
TRKATZ	Waiting time for the forced setting of the adaption correction RKAT	[20..30..50] sec
TRKAZZ	Waiting time for the forced setting of the adaption correction RKAZ	[20..30..50] sec

The values indicated in the middle are reference values

By means of the partial function DKVSZYK the cycle flags for all adaptation ranges are set. The cycle flag is either set by the bit B\_gaefra for FRAU and B\_gaeing for RKAT resp. RKAZ or after an adjustable time has passed.

The cycle flags Z\_rkat and Z\_rkaz may only be set during a drive once a mixture error can reliably be detected by the integrator (RKAT resp. RKAZ) assigned to it. It must for example be definitely ruled out that a multiplicative error after engine start and long idling leads to an error message in the additive range.

Such false messages can be ruled out if the demand is made that the adaptation first must be active in the frau range for a certain time (TFRAUZ) before it then is active for another time in the RKAT resp. RKAZ range (TRKATZ,TRKAZZ).

For the FTP-72 test without error in the fuel supply system the times TRKATZ and TFRAUZ are too long. A quicker setting is necessary. For this the information basic adaptation stabilized (B\_gaefra resp. B\_gaeing) can be used.

Application of block DKVS enable:  
-----

A p p l i c a t i o n   v a l u e s :

MLDKVSF : Air mass threshold for fault enable [8...10...15] Kg  
MLDKVSF is to choose greater than the air mass value, which could be sucked in only after first low fuel e.g. by not straight standing auto until finally auto standstill by e.g. straight auto position.

MLDKVSG : air mass threshold for integrator to set of zero [10...20...30] Kg  
MLDKVSG is the air mass, which must flow in motor for verification of fill up. After this the DKVS is free for closing by repeated fault with empty tank. MLDKVSG must be not too less, so that by a real error DKVS with togglebehavior of bit B\_edkvs it does not occur an erroneously closing.

IMLKVSMX: air mass threshold for integrator to set of zero [50...80...100] Kg  
IMLKVSMX is introduced, with them a reset of integrator occurs anyway. IMLKVSMX is to choose higher than air mass, which in 2 FTP75 tests could be sucked in.

Remark : The Values indicated in the middle are recommend reference values.

Application of the partial function DKVSERR :  
-----

A p p l i c a t i o n   v a l u e s

FRAUDX	upper diagnosis threshold FRAU	[1,2...1,23...1,25]
FRAUDN	lower diagnosis threshold FRAU	[0,75..0,77...0,80]
FRAODX	upper diagnosis threshold FRAO	[1,2...1,23...1,25]
FRAODN	lower diagnosis threshold FRAO	[0,75..0,77...0,80]
RKATDX	upper diagnosis threshold RKAT	[7...8,5...10,0] %
RKATDN	lower diagnosis threshold RKAT	[-10..-8,5...-7,0] %
RKAZDX	upper diagnosis threshold RKAZ	[7...8,5...10,0] %
RKAZDN	lower diagnosis threshold RKAZ	[-10..-8,5...-7,0] %

The values indicated in the middle are reference values.

The diagnosis thresholds must be entered into the permissible adaptation range (limit). The thresholds are to be determined such that an error fitted in the fuel supply system which results in the emission limit being exceeded by more than factor 1.5 definitely causes the error threshold to be reached in the FTP72 test. The diagnosis threshold should be adjusted in such a way that if the crankcase purge pipe drops off a leakage air error is detected (new CARB requirement).

In order to avoid undesired error messages under certain conditions (hot fuel, very high intake air temperature) reduced adaptation limits were introduced in the LRA, of which, however, only RKATRN shall be used.

These adaptation limits are to be adjusted to the determined diagnosis thresholds. The following conditions shall apply:

set FRAURX = FRAUMX and FRAURN = FRAUMN; i.e. no reduced threshold for FRAU  
set FRAORX = FRAOMX and FRAORN = FRAOMN; i.e. no reduced threshold for FRAO

set RKATRX = RKATMX.

RKATRN approx. 2% - 3% Delta Lambda (related to  $\lambda$  during idling) above diagnosis threshold RKATDN



The 2% - 3% Delta Lambda must be maintained, so that "further adaptation into the wrong direction" for a short time after the next cranking (where the extended correction thresholds are again released) cannot lead to an error message.

set RKAZRX = RKAZMX and RKAZRN = RKAZMN; i.e. no reduced threshold for RKAZ

Maximum resp. minimum limits (FRAUMX,...,FRAUMN,...) should lie approx. 2% - 3% Delta-Lambda above resp. below the diagnosis thresholds.

```

----- FRAUMX = FRAURX (upper adaptation limit)
----- FRAUDX (upper diagnosis threshold)

-.-.-.-.- FRAUDN (lower diagnosis threshold)
-.-.-.-.- FRAUMN = FRAURN (lower adaptation limit)
    
```

Application of the partial function DKVSST :

**A p p l i c a t i o n v a l u e s**

ZFRMST	Low pass time constant für frm_w(2)-signal	[3,0...5,0...10,0] sec
TFRMST	Detection time for stabilized of frm_w(2)-signal	[3,0...15,0...30,0] sec
TFRMZST	Waiting time for the unplausible frm_w(2)-signal	[20,0...50,0...50,0] sec
DFRMST	Delta-frm for detection of the stabilized frm_w(2)-signal	[0,01...0,03...0,05]
FRMSTDX	upper diagnosis threshold for frm_w(2)-signal short test	[1,2...1,23...1,25]
FRMSTDN	lower diagnosis threshold for frm_w(2)-signal short test	[0,75...0,77...0,80]

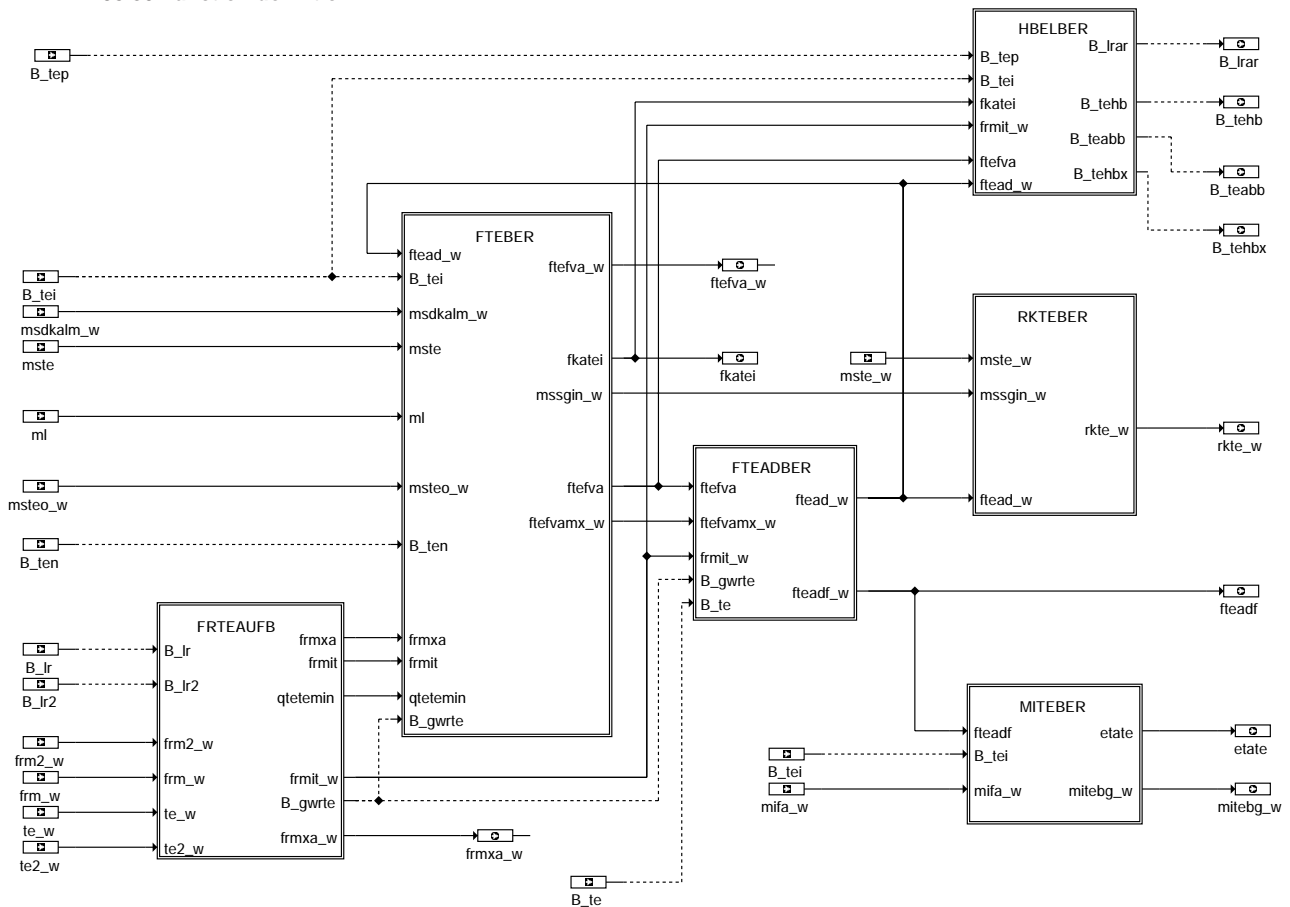
The values indicated in the middle are reference values.

The detection time for stabilized frm\_w(2)-signal TFRMST should be chosen laset 3 time of low pass time constans.

The diagnostic thresholds (FRMSTDX and FRMSTDN) must be entered into the permissible control range (lift) and less then diagnostic threshold of FRAU. The thresholds are so to define, such that a fitted error in the fuel supply system, which in stationary state exceeds the error threshold of FRAU, with certainty reaches the error threshold (FRMSTDX resp. FRMSTDN). The time threshold TFRMZST should be greater then time threshold TFRMST.

## TEB 95.80 Purge canister function

### FDEF TEB 95.80 Function definition

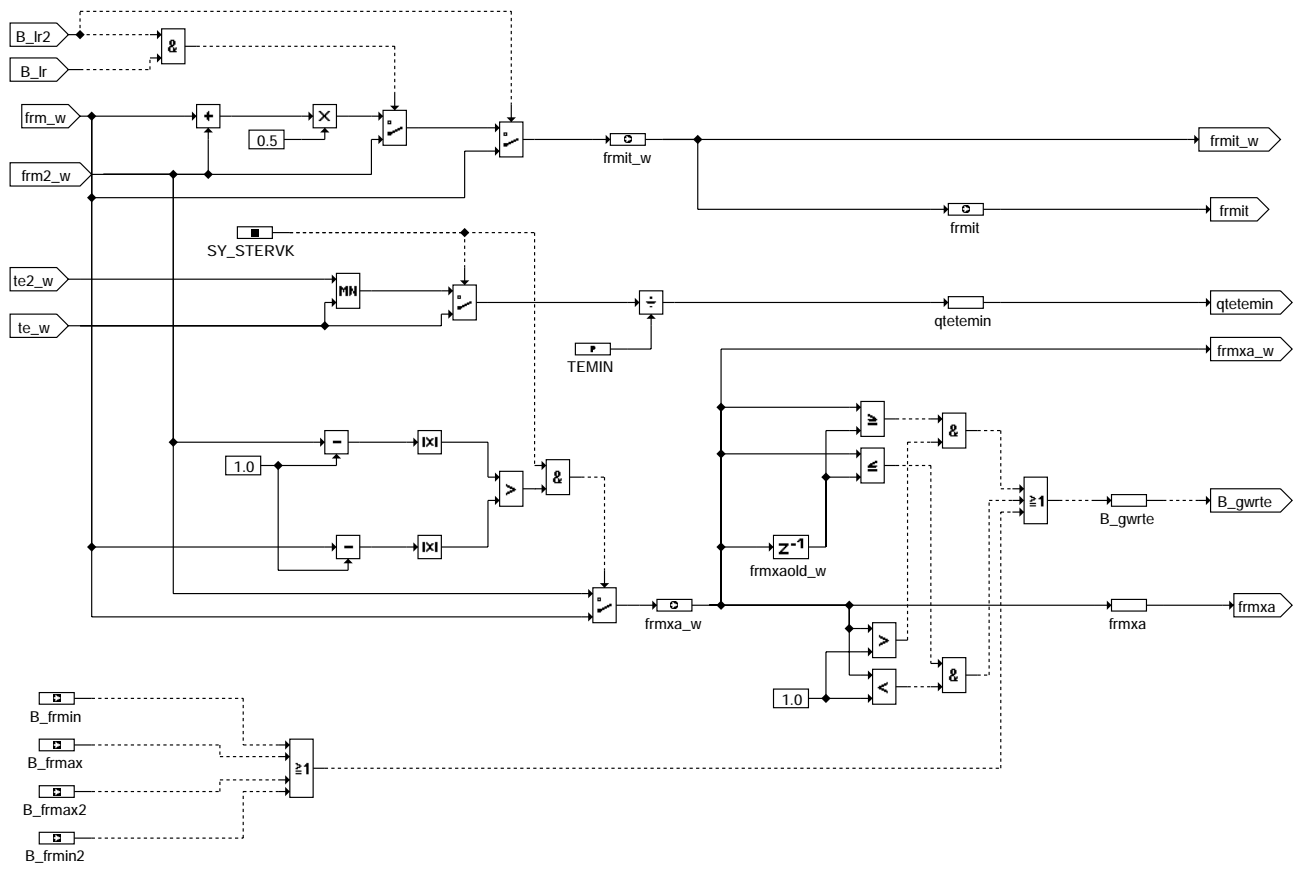


teb-main

teb-main



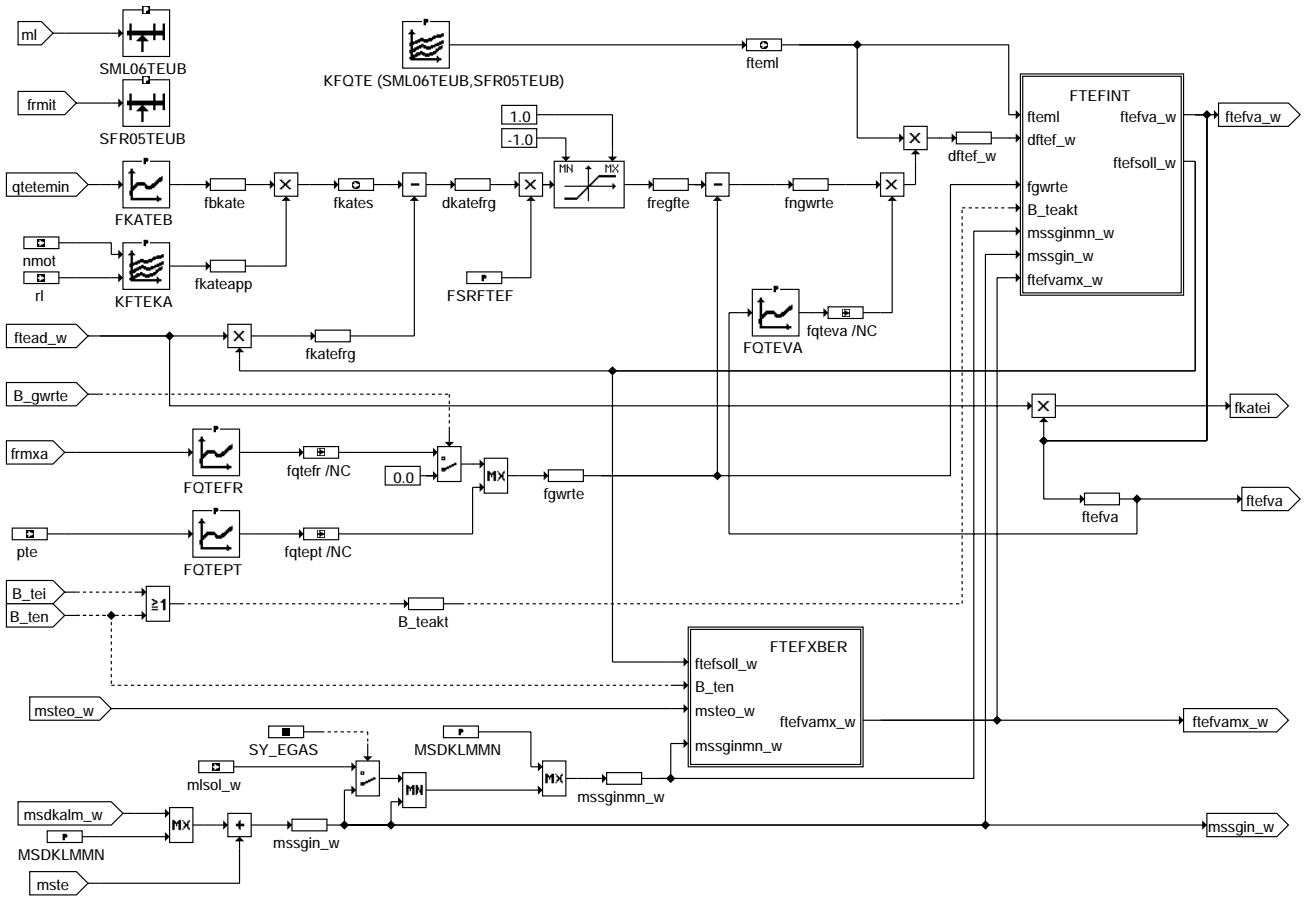
Calculation of Lambda control signals (frmx<sub>a</sub>, frmit<sub>w</sub> and B<sub>gwrt<sub>e</sub></sub>) and of the quotient: qtetemin = MIN(te<sub>w</sub>, te2<sub>w</sub>) / TEMIN:



teb-frteaufb

abb-frteaufb

Calculation of the desired value of purge mass flow (mstesoll\_w) and of the purge rate (ftefva\_w):

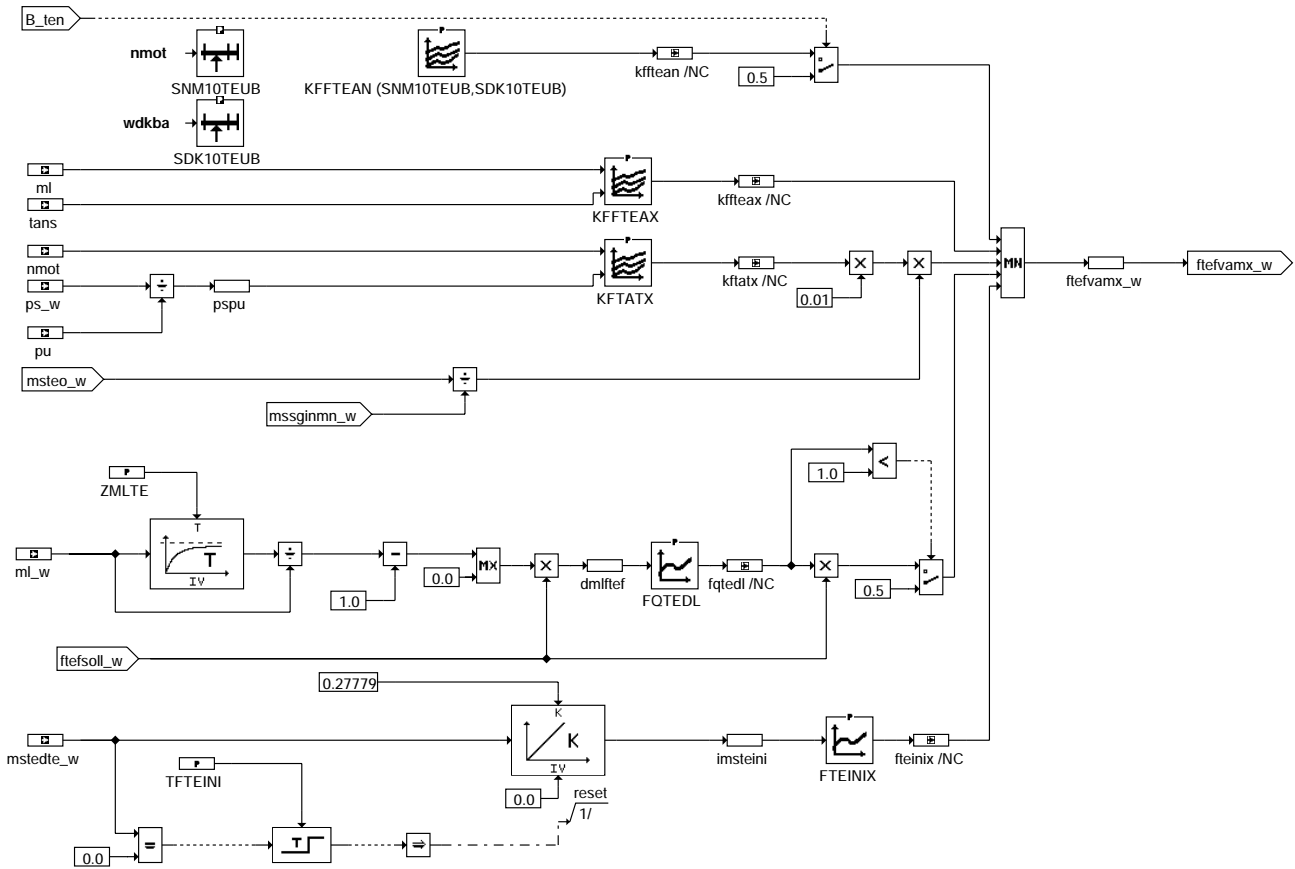


teb-fteber

teb-fteber



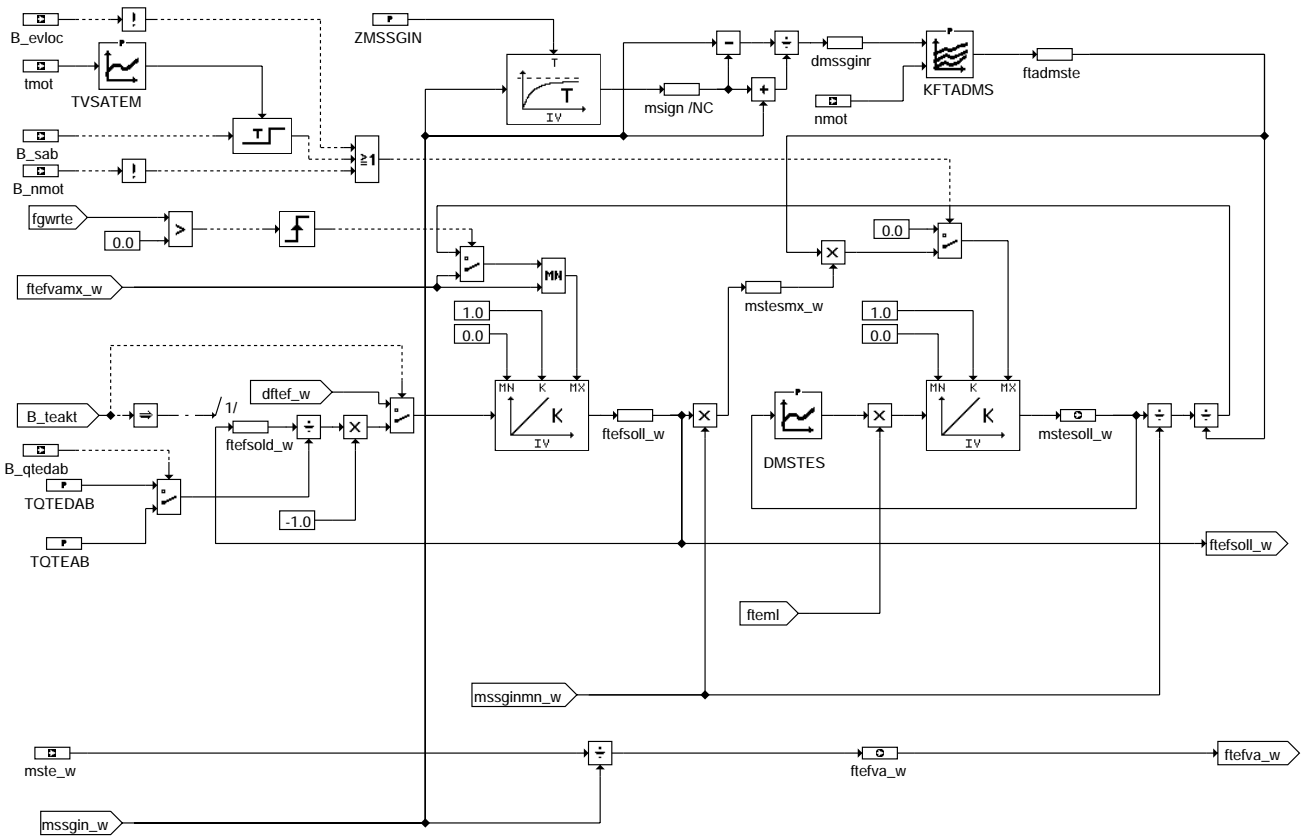
Limitation of the purge rate (signal ftefvamx\_w):



teb-ftefxber

teb-ftefxber

The two integrators: ftefsoll\_w and mstesoll\_w:

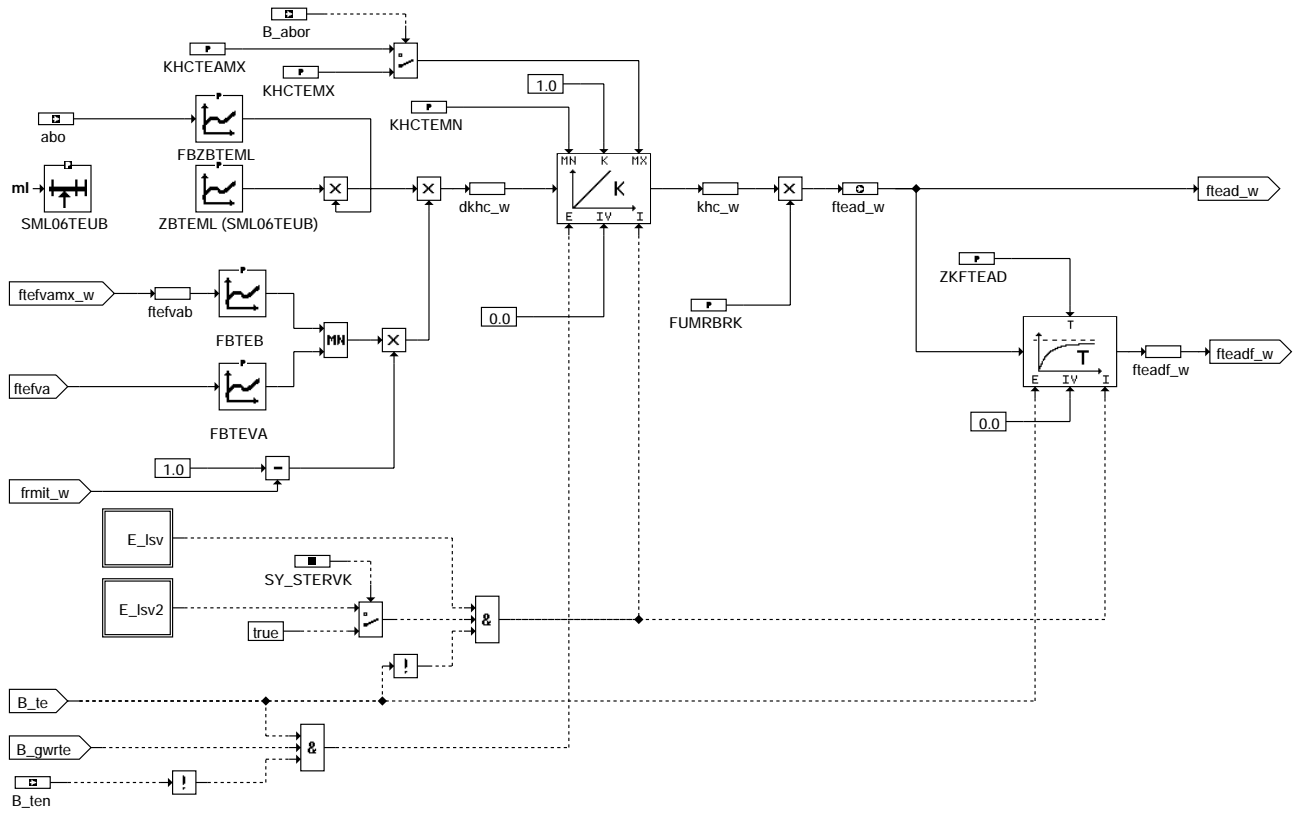


teb-ftefint

teb-ftefint

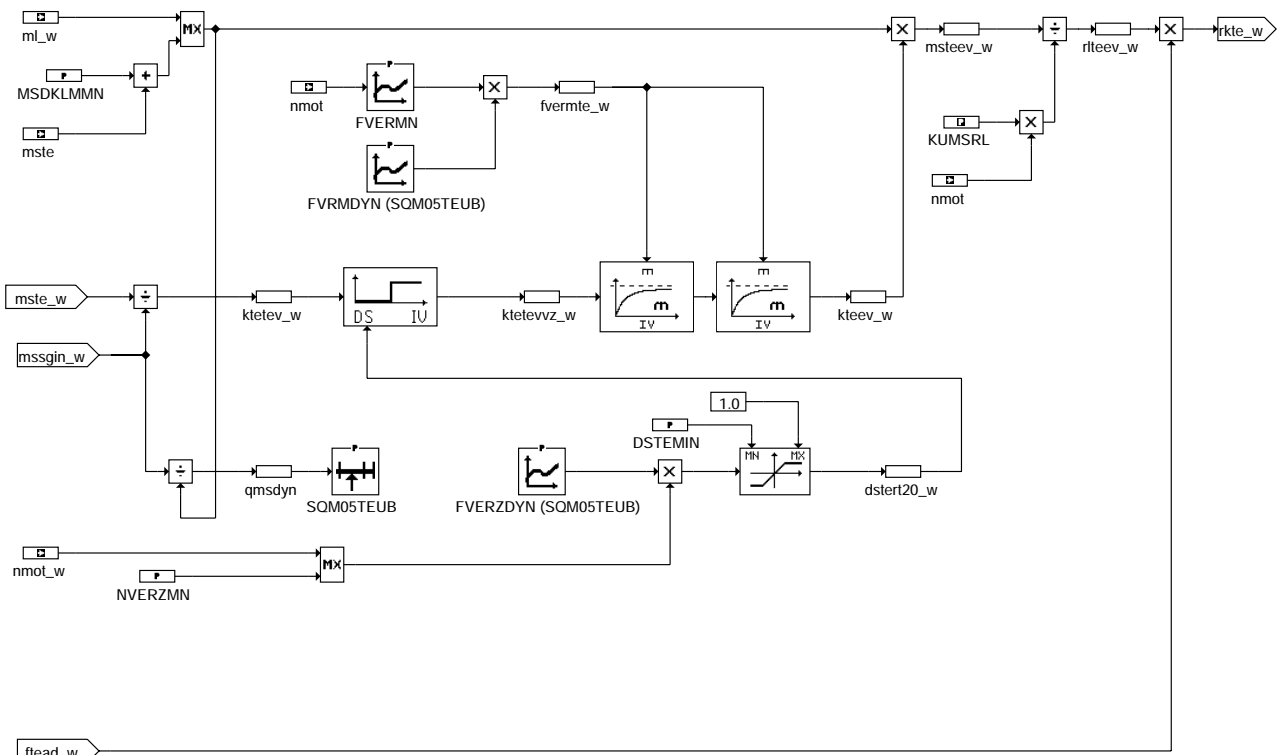


Adaptation of the HC-concentration of the purge flow:



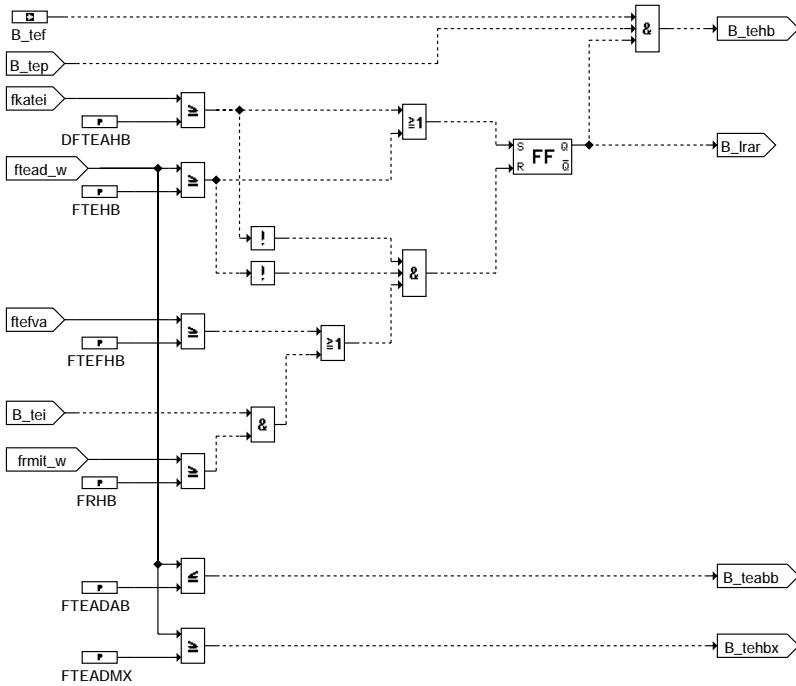
**teb-fteadber**

Calculation of the mixture correction signal "rkte\_w":



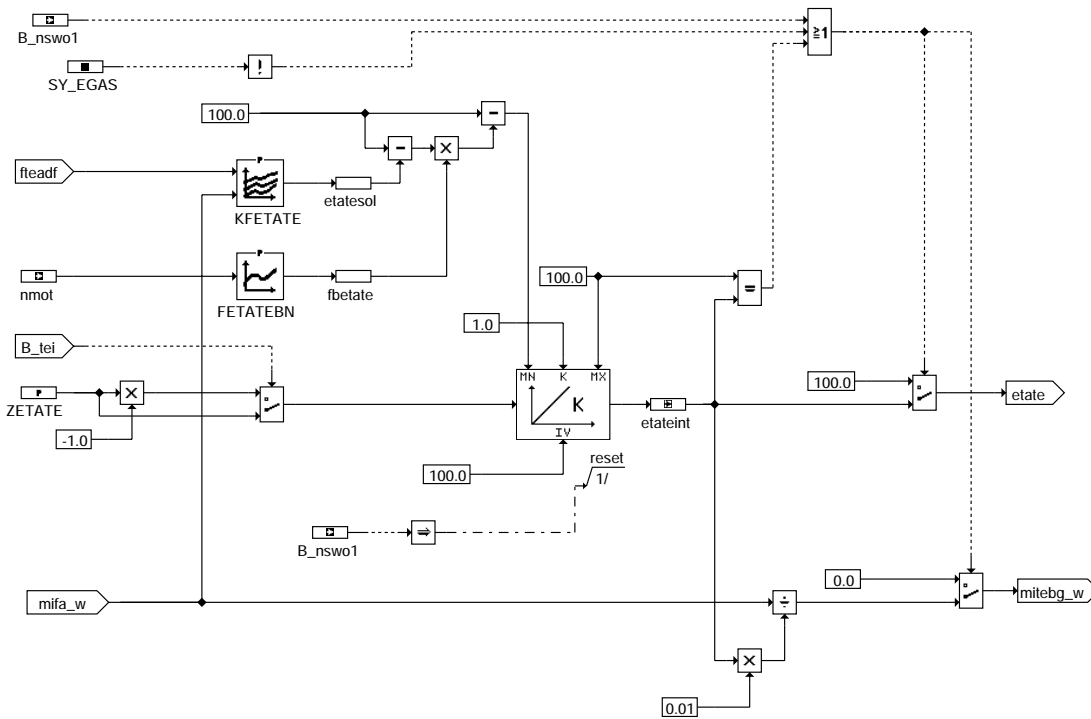
**teb-rkteber**

Calculation of the Bits derived from "Canister Charge - ftead\_w":



**teb-hbelber**

Interaction on engine torque:



**teb-miteber**

**ABK TEB 95.80 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
DFTEAHB			FW	threshold fuel rate for switching the bit B_tehb to TRUE
DMSTES	MSTESOLL_W		KL	characteristic line maximum increase of purge mass flow
DSTEMIN			FW	minimum value for transportation distance in delay-time block
FBTEB	FTEFVAB		KL	factor ftefvab-depending limitation of the canister charge adaptation speed
FBTEVA	FTEFVA		KL	factor ftefva-depending canister charge adaptation speed





Parameter	Source-X	Source-Y	Type	Description
FBZBTEML	ABO		KL	Weighting factor integration speed for canister charge adaptation
FETATEBN	NMOT		KL	characteristic line: reduction of engine efficiency as f(nmot)
FKATEB	QTETEMIN		KL	Characteristic line fuel portion depending on te / TEMIN
FQTEDL	DMLFTEF		KL	Factor for exponential decrease of flow rate
FQTEFR	FRMXA		KL	characteristic line: purge rate reduction with big frm-deviation
FQTEPT	PTE		KL	characteristic line: for fuel-tank underpressure limitation
FQTEVA	FTEFVA		KL	progression of purge rate controller
FRHB			FW	limit for lambda controller to reset Bit "High HC-canister charge"
FSRFTEF			FW	factor: control speed of purge rate controller
FTEADAB			FW	Canister charge threshold for interruption of the purge phase
FTEADMX			FW	Maximum value of the canister charge (flead)
FTEFHB			FW	Limit for flow rate of purge system to detect high concentration
FTEHB			FW	Limit for purge factor to detect high concentration
FTEINIX	IMSTEINI		KL	characteristic line for max. purge rate = F(integral purge flow after TE-Stop)
FUMRBRK			FW	factor calculation of canister charge (flead) from HC-concentration
FVERMN	NMOT		KL	characteristic line: filter factor for purge flow in the manifold with fresh air
FVERZDYN	QMSDYN		KL	dynamic factor delay of purge flow in the manifold
FVRMDYN	QMSDYN		KL	dynamic factor for purge flow in the manifold with fresh air
KFETATE	FTEADF_W	MIFA_W	KF	characteristic map for efficiency at active purging when te is near TEMIN
KFFTEAN	NMOT	WDKBA	KF	characteristic map for limitation of the purge rate with no Lambda control
KFFTEAX	ML	TANS	KF	Characteristic map for limitation of the purge rate
KFQTE	ML	FRMIT	KF	Map for purge rate increase / decrease
KFTADMS	DMSSGINR	NMOT	KF	dynamic evaluation factor for close off of PCV
KFTATX	NMOT	PSPU	KF	map for max. duty cycle
KFTEKA	NMOT	RL	KF	characteristic map of desired fuel portion purge control
KHCTEAMX			FW	maximum value of HC concentration in purge flow (by B_abor)
KHCTEMN			FW	minimum value of HC concentration in purge flow
KHCTEMX			FW	maximum value of HC concentration in purge flow
KUMSRL			FW (REF)	conversion constant from mass flow to relative air charge
MSDKLMMN			FW	minimum mass flow over throttle in canister purge control
NVERZMN			FW	minimal engine speed for dealy time
SDK10TEUB	WDKBA		SV (REF)	wdkba dependet basic point (number 10)
SFR05TEUB	FRMIT		SV (REF)	frmit dependet basic point (number 5)
SML06TEUB	ML		SV (REF)	ml dependet basic point (number 6)
SNM10TEUB	NMOT		SV (REF)	nmot dependet basic point (number 10)
SQM05TEUB	QMSDYN		SV	air mass quotient dependet basic point (number =5)
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TEMIN			FW	minimum effective injection time
TFTEINI			FW	Time for detection of purge stop
TQTEAB			FW	time for decrementation of the purge rate
TQTEDAB			FW	time for fast decrementation of the purge rate
TVSATEM	TMOT		KL	delay time for closing of the PCV after readiness for fuel cut off
ZBTEML	ML		KL	integration speed for canister charge adaptation
ZETATE			FW	changing speed of engine efficiency because of purge control
ZKFTEAD			FW	time constant filtered factor load scavenging air at tank ventilation
ZMLTE			FW	Time constant for ml-filter
ZMSSGIN			FW	filter time constant for calculation of relative evaluation mssgin_w

Variable	Source	Type	Description
ABO	BBBO	EIN	numbers of starts with fuel in oil
B_ABOR	BBBO	EIN	condition numbers of starts with fuel in oil for reduced adaptive lambda control
B_EVLOC	BGEVAB	EIN	Status: all injection valves are activated
B_FRMAX	LR	EIN	lambda control sets bit when lambda controller reaches its limit FRMAX
B_FRMAX2	LR	EIN	lambda control sets bit when lambda control reaches it limit FRMAX, bank2
B_FRMIN	LR	EIN	lambda control sets bit when lambda controller reaches its limit FRMIN
B_FRMIN2	LR	EIN	lambda control sets bit when lambda control reaches its limit FRMIN,bank2
B_GWRTE	TEB	LOK	condition: purge rate reduction because of fr-controller deviations
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_LRAR	TEB	AUS	condition for reduced correction ranges at LRA
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_QTEDAB	TEBEB	EIN	condition fast decrementation of purge rate
B_SAB	MSF	EIN	Condition fuel cut-off requested
B_TE	TEBEB	EIN	Condition canister purge active
B_TEABB	TEB	AUS	Condition purge canister function ready to finish
B_TEAKT	TEB	LOK	condition purge control active (open loop or closed loop)
B_TEF	TEBEB	EIN	Condition canister purge function principally released
B_TEHB	TEB	AUS	condition for canister purge system with high canister load
B_TEHBX	TEB	AUS	Condition load integrator ftead at max. limit
B_TEI	TEBEB	EIN	Internal condition: canister purge function active
B_TEN	TEBEB	EIN	condition open loop purging
B_TEP	GKEB	EIN	Condition canister purge phase active
DFP_LSV	TEB	DOK	ECU int. fault path no.: electrical diagnosis for lambda sensor upstream cat.
DFP_LSV2	TEB	DOK	ECU int. fault path no.: electr. diagnos. for lambda sensor upstream cat. bank 2
DFTEF_W	TEB	LOK	input purge rate integrator
DKATEFRG	TEB	LOK	deviation actual fuel rate purge control from desired value
DKHC_W	TEB	LOK	input integrator for learning HC-concentration of purge control
DMLFTEF	TEB	LOK	product of percentual air flow change with purge rate
DMSSGINR	TEB	LOK	relative variation of mass flow mssgin_w



Variable	Source	Type	Description
DSTERT20_W	TEB	LOK	normalised transportation amount of purge flow in the manifold
ETATE	TEB	AUS	engine efficiency when purging with high vapour concentration
ETATEINT	TEB	LOK	integrator engine efficiency while purging
ETATESOL	TEB	LOK	desired engine efficiency when purging (depending on HC-vapor concentration)
E_LSV	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_LSV2	DLSV	EIN	error flag: lambda sensor upstream catalyst
FBETATE	TEB	LOK	desired engine efficiency as f(nmot) at purge control to avoid te/TEMIN<=1
FBKATE	TEB	LOK	factor fuel portion of purge flow depending on te / TEMIN
FGWRTE	TEB	LOK	value: purge rate reduction because of fr-controller deviations
FKATEAPP	TEB	LOK	factor calibrated fuel portion of purge flow
FKATEFRG	TEB	LOK	factor fuel rate purge control at desired purge rate
FKATEI	TEB	AUS	factor fuel part purge control (actual value)
FKATES	TEB	AUS	factor fuel part purge control (desired value)
FNGWRTE	TEB	LOK	factor purge rate control after fr-controller reduction
FREGFTE	TEB	LOK	factor purge rate control before fr-controller reduction
FRM2_W	LR	EIN	fast mean value of lambda control factor bank 2(word)
FRMIT	TEB	AUS	Mean value of fr and fr2
FRMIT_W	TEB	AUS	mean value of fr and fr2 (16 bit)
FRMXA	TEB	LOK	fr value (out of fr and fr2) which is the farrest away from 1.0
FRMXA_W	TEB	AUS	fr value (out of fr and fr2) wich is the farrest away from 1 (16bit)
FRM_W	LR	EIN	fast mean value of lambda control factor (word)
FTADMSTE	TEB	LOK	evaluation factor for close off of PCV when dynamic case
FTEADF	TEB	AUS	filtered factor load scavening air at tank ventilation
FTEADF_W	TEB	LOK	filtered factor load scavening air at tank ventilation (16 bit)
FTEAD_W	TEB	AUS	charcoal canister charge
FTEFSOLD_W	TEB	LOK	last desired canister purge rate before closing the PCV
FTEFSOLL_W	TEB	LOK	desired canister purge rate
FTEFVA	TEB	LOK	canister purge rate
FTEFVAB	TEB	LOK	actual limit of the purge rate
FTEFVAMX_W	TEB	LOK	max. purge rate (16 bit value)
FTEFVA_W	TEB	AUS	purge rate of the purge control function
FTEML	TEB	AUS	input purge rate integrator
FVERMTE_W	TEB	LOK	factor filtering purge low in the manifold
IMSTEINI	TEB	LOK	integral of purge mass flow after a longer purge stop
KHC_W	TEB	LOK	adapted HC-concentration of the purge flow
KTEEV_W	TEB	LOK	concentration purge flow in the manifold at the injection valve
KTETEUVZ_W	TEB	LOK	concentration purge flow in the manifold (with delay)
KTETEUV_W	TEB	LOK	concentration purge flow in the manifold at the PCV
MIFA_W	MSF	EIN	desired indicated engine torque
MITEBG_W	TEB	AUS	torque value for minimum charge canister purge
ML	SWADAP	EIN	air mass flow
MLSOL_W	FUEDK	EIN	set air mass flow
ML_W	EGFE	EIN	air mass flow filtered (Word)
MSDKALM_W	BGMSZS	EIN	Mass flow over throttle (balance with HFM signal)
MSSGINMN_W	TEB	LOK	mimum of mass flow into manifold (through throttle and PCV)
MSSGIN_W	TEB	LOK	mass flow into manifold (through throttle and PCV)
MSTE	BGTEV	EIN	mass flow purge control into the manifold
MSTEDTE_W	BGTEV	EIN	purge mass flow for DTEV (word)
MSTEEV_W	TEB	LOK	purge mass flow at the injection valve
MSTEO_W	BGTEV	EIN	Mass flow the 100 % opened TEV
MSTESMX_W	TEB	LOK	max. possible desired purge mass flow
MSTESOLL_W	TEB	AUS	desired purge mass flow
MSTE_W	BGTEV	EIN	mass flow purge control into the manifold
NMOT	SWADAP	EIN	engine speed
NMOT_W	SWADAP	EIN	engine speed
PSPU	TEB	LOK	quotient: manifold pressure / ambient pressure
PS_W	EGFE	EIN	intake manifold pressure (absolute) (Word)
PTE	GGDST	EIN	tank pressure (from ADC)
PU	BGPU	EIN	Ambient pressure
QMSDYN	TEB	LOK	quotient from mLw und mmssgin_w
QTETEMIN	TEB	LOK	quotient: te / TEMIN for BDE teh_w/teminh_w resp. tes_w/temins_w
RKTE_W	TEB	AUS	relative fuel part of the purge control
RL	SWADAP	EIN	relative air charge
RLTEEV_W	TEB	LOK	relative cylinder air amount because of purging
TANS	SWADAP	EIN	Intake air temperature
TE2_W		EIN	effective injection time bank 2 (word)
TE_W		EIN	effective injection time (word)
TMOT	SWADAP	EIN	Engine temperature

### FW TEB 95.80 Fixed Values

Parameter	Value	Description
DFTEAHB		threshold fuel rate for switching the bit B_tebh to TRUE
DSTEMIN		minimum value for transportation distance in delay-time block
FRHB		limit for lambda controller to reset Bit "High HC-canister charge"
FSRFTEF		factor: control speed of purge rate controller
FTEADAB		Canister charge threshold for interruption of the purge phase
FTEADMX		Maximum value of the canister charge (ftead)
FTEFHB		Limit for flow rate of purge system to detect high concentration
FTEHB		Limit for purge factor to detect high concentration
FUMRBRK		factor calculation of canister charge (ftead) from HC-concentration



Parameter	Value	Description
KHCTEAMX		maximum value of HC concentration in purge flow (by B_abor)
KHCTEMN		minimum value of HC concentration in purge flow
KHCTEMX		maximum value of HC concentration in purge flow
MSDKLMMN		minimum mass flow over throttle in canister purge control
NVERZMN		minimal engine speed for dealy time
TEMIN		minimum effective injection time
TFTEINI		Time for detection of purge stop
TQTEAB		time for decrementation of the purge rate
TQTEDAB		time for fast decrementation of the purge rate
ZETATE		changing speed of engine efficiency because of purge control
ZKFTEAD		time constant filtered factor load scavenging air at tank ventilation
ZMLTE		Time constant for ml-filter
ZMSSGIN		filter time constant for calculation of relative evaluation mssgin_w

## FB TEB 95.80 Detailed description of function

### Introduction:

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The new "loading-dependent purge control" is subdivided into several functions:

- > %TEB - core of the function
- > %TEBEB - activation conditions
- > %ATEV - output of the duty cycle to the PCV
- > %BGTEV - calculation of the mass flows PCV (separate functions for aspirating engines and for turbo charger engines)

### Short description of the function purge control:

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- > A desired mass flow scavenge gas is determined (mstesoll\_w)
- > From this the pulse duty cycle PCV is calculated (tateout)
- > The actual scavenging flow purge control into intake manifold is calculated (mste\_w)
- > The concentration of scavenge gas in the intake manifold at the level of the PCV is calculated (ktetev\_w)
- > The transport and mixing through the intake manifold are taken into consideration (ktetev\_w -> kteev\_w)
- > The mass flow of scavenge gas at the level of the intake valve of the engine (msteev\_w) is calculated
- > The relative charge in the cylinder due to scavenge gas (rlteev\_w) is calculated.
- > From the deviations of the Lambda controller from 1.0 the HC concentration directly upstream the PCV (khc\_w) is adapted and directly from this the variable loading (ftead\_w) is calculated.
- > The needed relative fuel correction is calculated (rkte\_w = relative charge \* loading).

Remark: All mass flows (so also scavenging flows) refer to pure air. A possible "loading" with hydrocarbons (HC) is only taken into consideration during the mixture correction (rkte\_w).  
The system constant SY\_EGAS distinguishes the system-specific versions with/without electronic accelerator (EGAS)

### List of the most important values for purge control (turbo charge engine + aspirating engine):

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#### Mass flows:

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- > Air masses flowing into and out of the intake manifold (msdkalm\_w, ml\_w)
- > Scavenge gas masses flowing into and out of the intake manifold (mste\_w, msteev\_w)
- => thus resulting scavenge gas concentrations (ktetev\_w - at the level of throttle valve, kteev\_w)

#### Physical values (only for description):

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- > HC concentrations (mass of HC particles / mass of air particles) in the monitored gas flow
  - khc\_tev: directly upstream PCV  
(no motronic value, however, adapted value "HC conc. upstream PCV" exists in motronic: khc\_w )
  - khc\_einl.: at the level of the intake valve of the engine (no motronic value)

#### Special motronic values for PCV triggering and mixture correction:

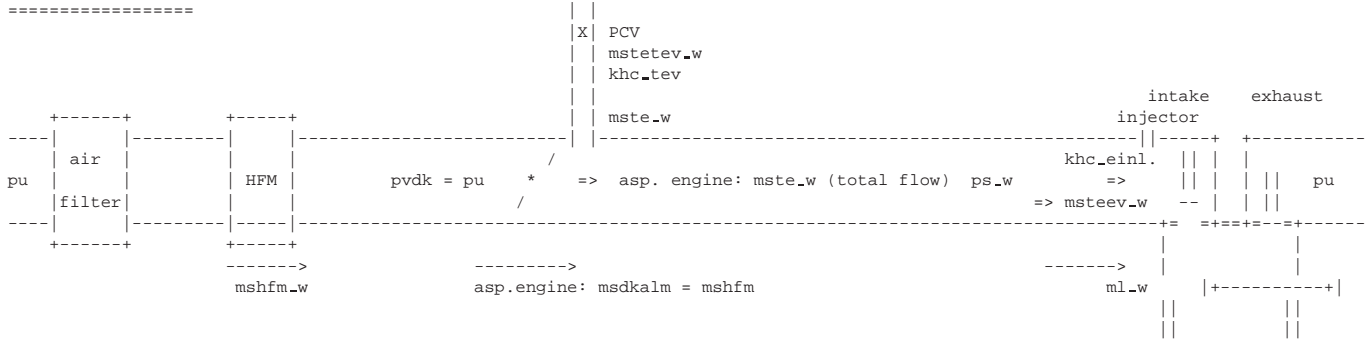
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- > tateout : Output duty cycle PCV (contains pickup delay PCV)
- > rkte\_w : Mixture correction for injection (is subtracted from the injection volume needed without purge control)
- > khc\_w : Adapted HC concentration of the scavenge gas flow directly upstream the PCV
- > rlteev\_w : Relative charge in the cylinder due to scavenge gas
- > ftead\_w : Value obtained from khc\_w only by conversion (re-normalization) (rkte\_w = ftead\_w \* rlteev\_w)



Intake manifold models (separate for aspirating engines and turbo charger engines), complete list of all values:

Aspirating engine:



Mass flows:

- mshfm\_w.....: Mass flow of air flowing through HFM
- msdkalm\_w.....: Mass flow through throttle valve equalized with air mass meter signal  
(on the aspirating engine msdkalm\_w = mshfm\_w, on the turbo charger engine the balance air mass turbo charger is added)
- mstetev\_w.....: On the aspirating engine: mass flow PCV (intake downstream throttle valve)
- mste\_w.....: Total flow purge control ("currently flowing at the level of the throttle valve")
- msteev\_w.....: Total (compared to throttle valve) timewise delayed and "smoothed out mass flow purge control"  
msteev\_w is only used for the mixture correction (the charge sensing calculates with mste).
- mssgin\_w.....: mssgin\_w = msdkalm\_w + mste\_w: total gas mass flow flowing into intake manifold  
(air throttle valve + TE scavenge gas). EGR is not taken into consideration
- ml\_w.....: Total air mass flow siphoned from the engine (in ml\_w also scavenge gas is contained)

Pressures:

- ps\_w.....: Manifold pressure in hPa
- pu.....: Ambient pressure in hPa
- pvdk.....: Pressure upstream throttle valve

HC concentrations:

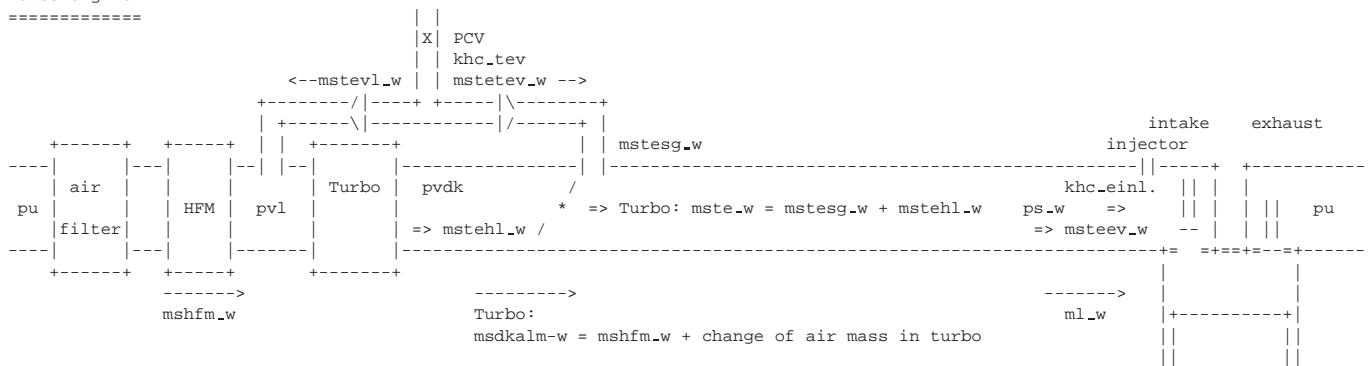
- khc\_tev.....: Concentration HC at PCV
- khc\_einl.....: Concentration HC at the level of the intake valves

Concentrations of scavenge gas in air, which is taken in through the throttle valve (not illustrated in above diagrams) :

- ktetev.....: Concentration of scavenge gas in the intake manifold immediately after scavenge gas has mixed with air
  - kteev.....: Concentration of scavenge gas at intake valve
- Remark: Conc. of scavenge gas is not equal to concentration of HC but only indicates how many gas particles from the TE-system have currently mixed with the gas particles of the air.
- ktetev = mste / (msdkalm + mste) ktete
  - kteev = msteev / ml



Turbo engine:  
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**Mass flows:**

- mshfm\_w.....: Air mass flow flowing through HFM
- msdkalm\_w.....: Mass flow through throttle valve equalized by air mass meter signal  
(on the aspirating engine msdkalm\_w = mshfm\_w, on the turbo charger engine the balance air mass turbo charger is added)
- mstevl\_w.....: Only turbo engine: portion of mass flow PCV which is led in upstream of the turbo charger
- mstehw\_w.....: Only turbo engine: mass flow purge control currently flowing into the intake manifold from the turbo charger
- mstesg\_w.....: Only turbo engine: the mass flow purge control currently flowing into the manifold via the intake position of the manifold
- mstetev\_w.....: On the turbo engine: the mass flow PCV which is led in upstream throttle valve
- mste\_w.....: Total flow purge control ("currently flowing at the level of the throttle valve")
- msteew\_w.....: Total (compared to throttle valve) timewise delayed and "smoothed out mass flow purge control"  
msteew\_w is only used for the mixture correction (the charge sensing calculates with mste).
- mssgin\_w.....: mssgin\_w = msdkalm\_w + mste\_w: total gas mass flow flowing into intake manifold  
(air throttle valve + TE scavenge gas). EGR is not taken into consideration
- ml\_w.....: Total air mass flow siphoned from the engine (in ml\_w also scavenge gas is contained)

**Pressures:**

- ps\_w.....: Manifold pressure in hPa
- pu.....: Ambient pressure in hPa
- pvl.....: Only turbo engine: Pressure upstream the turbo charger (little below external pressure due to flow resistance)
- pvdw.....: Pressure upstream throttle valve

**HC concentrations:**

- khc\_tev.....: Concentration HC at PCV
- khc\_einl.....: Concentration HC at the level of the intake valves

Concentrations of scavenge gas in air, which is sucked in through the throttle valve (not illustrated in above diagrams) :

- ktetev.....: Concentration of scavenge gas in the intake manifold immediately after scavenge gas has mixed with air
  - kteev.....: Concentration of scavenge gas at intake valve
- Remark: Conc. of scavenge gas is not equal to concentration of HC but only indicates how many gas particles from the TE-system have currently mixed with the gas particles of the air.
- $$\text{ktetev} = \text{mste} / (\text{msdkalm} + \text{mste}) \quad \text{ktete}$$

$$\text{kteev} = \text{msteew} / \text{ml}$$



Statements and physical regularities:  
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- > For the purge control at first the entire mass flow of scavenge gas which flows in at the level of the throttle valve is of interest (mste\_w). On the aspirating engine there is only one intake downstream throttle valve. Due to the intake manifold vacuum, regenerating gas flows into the intake manifold. On the turbo charger two intake positions are to be provided (1. downstream throttle valve, 2. upstream the turbo charger) In case of low manifold pressure the scavenging flow will flow in downstream throttle valve. In the charging area the flow resistance of the air filter causes a minor vacuum upstream the turbo charger. Then the scavenge gas will flow upstream the turbo charger. A check valve prevents that air from the intake manifold will flow upstream the turbo charger.
  - > On the aspirating engine and also on the turbo charger engine the entire purge flow at throttle valve is calculated (mste\_w) - important common intermediate value.  
=> Mste\_w is thus then the input value for %TEB. Mste\_w calculation for aspirating engines and for turbo engines, however, in separate versions %BGTEV  
Remarks: Mste\_w at first does not take into consideration that also HC particles are contained in the flow. Additionally also a HC concentration must be learned (adapted) (khc\_w resp. ftead\_w). Mste\_w is related to pure air !  
Storage effects in the pipe PCV-intake manifold and in the turbo charger can (in later versions) be taken into consideration in mste\_w. For this the values mstetev\_w (aspirating engine, turbo engine) and mstevl\_w, mstehl\_w (additionally only for turbo engine) were introduced.
  - > The HC flow led in at the PCV needs a certain time until it reaches the intake valve (position of the intake valve).
  - > Steep edges of concentration differences at the position of the PCV are smoothed by diffusion in the intake manifold. Generally it can be said that the longer a gas particle is in the intake manifold the more diffused become the concentration jumps. A concentration progress in form of a rectangle (0->1 jump) smoothes out and results in a concentration progress in form of a -S- at the intake valve of the engine.
  - > The time spend by a particle in the intake manifold is approx. inversely proportional to the engine speed during steady-state engine operation.
  - > If the PCV does not open resp. close at exactly the same time or to exactly the same degree as the throttle valve then load changes cause strong HC concentration changes in the intake manifold. For example in case of a constantly open PCV the opening of the throttle valve will result in a temporarily very low scavenge gas concentration (air shoots into the intake manifold, PCV flow remains the same or reduces).
  - > However, if the PCV is opened resp. closed at exactly the same time as the throttle valve then the scavenge gas concentration in the intake manifold remains at a constant level. Unfortunately this mode of operation is not possible. As a rule the PCV timer enables the closing of the PCV only 50 ms after the throttle valve has closed. A throttle valve synchronous opening is also only to be passed on to the PCV delayed by the same time.  
In order to obtain an as constant as possible HC concentration of the scavenge gas flow it is furthermore recommendable to open the PCV only slowly also in case of quick positive load changes (e.g. double the opening within 5 s to 10 s). This prohibits a throttle valve synchronous activation of the PCV.
- => With load changes the dilution of the scavenge gas flow in the intake manifold changes very quickly with the inflowing air. This must be taken into consideration for the injection correction.

Advantages of the new charge sensing for the purge control function:  
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- > The new charge sensing performs a "particle balance" in the intake manifold. All gas particles flowing in are determined and from this the outflowing particles are calculated. Thus an exact knowledge of the manifold pressure is obtained. By means of the manifold pressure and of the external pressure the gas particles flowing in can then again be calculated in the next step. The only factors which must be known are the opening areas (resp. the mass flow led off from them in the over-critical under standard conditions) to the intake manifold.
- > The consequences for the purge control are:  
  
The following values are known:  
  
a) Aspirating engine (see e.g. BGTEV1.20):  
- one intake position downstream throttle valve  
ps\_w - manifold pressure  
pu\_w - ambient pressure  
=> from this the current mass flow through the PCV (mste\_w = KLAFFE(ps\_w/pu\_w))  
and the mass flow with open PCV (msteo\_w) can be derived.  
Remark: Additional characteristic KLAFFE (and not KLAF) to take into consideration the flow resistance of the pipe ACF-PCV or the flow characteristic of a Laval PCV changed with regard to the throttle valve.  
  
Exceptions: close to full load and full load. Here a map value (KFAFFE = f(nmot, wdka)) instead of the HFM-signal is used due to steady-state accuracy reasons.
- b) Turbo engine (see e.g. BGTEV2.10):  
- as shown above as a rule two intake positions are provided here  
- The quotient ps\_w/pu is taken from the charge sensin for the intake downstream throttle valve.  
- For the intake upstream the turbo charger the characteristic DPVMS (pressure drop upstream turbo charger due to air filter) is used.  
- Also an own outflow characteristic is defined (KLAFFE). Deviations from the normal characteristic may be necessary in order to:  
a) take into consideration the flow resistance of a long pipe ACF-PCV.  
b) take into consideration another PCV characteristic (Laval nozzle)





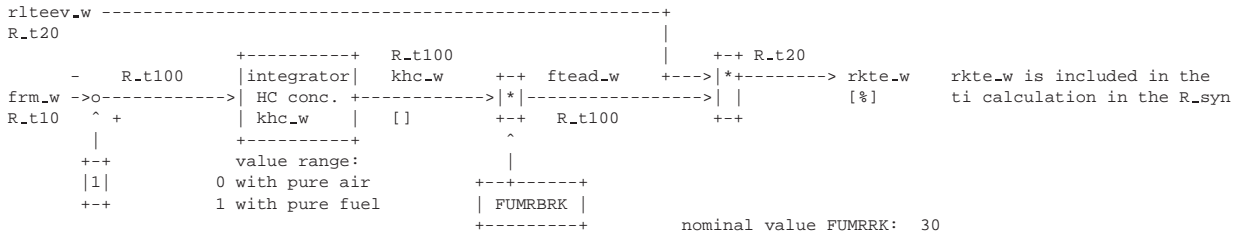
Several other statements and calculations follow, some of which were also valid for the previous TEB:

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- > Dependent on the total air mass currently flowing into the intake manifold and on the HC concentration of the gas flow (also called loading in the following) the purge control valve is triggered by the activated carbon filter. The aim is to obtain a certain fuel portion from the purge control.
  - > For the calculation of the pulse duty cycle it is important to know the maximum possible air mass flow through the PCV (msteo\_w). It can be calculated from the corresponding load state of the engine and from ambient conditions (pressure, temperature).  
Remark: msteo\_w is the gas mass flowing into the intake manifold at fully opened PCV provided pure air is coming.  
In case of an air-fuel mixture the actual gas mass flow is greater (since fuel vapor is denser), the air mass flow, however, is less, since the HC particles reduce the cross section of the valve, which is effective for air.
  - > Mste\_w is the gas mass flow PCV currently flowing into the intake manifold (related to air). In mste (calculated in %BGTEV) the delay of the PCV timer is already taken into consideration.
  - > The quotient from: "gas mass flow PCV (related to air) / total air mass flowing into the intake manifold" is called purge rate.  
Remark: In the purge rate control a distinction is made between desired purge rate (ftefsoll\_w) and the currently realized purge rate ftefva\_w. Reason for the splitting-up into two values: It must be possible to limit the change of the desired volume flow through the PCV (mstesoll).
  - > The purge control function adapts the HC concentration of the scavenge gas flow (khc\_w) flowing through the PCV. This concentration is multiplied by FUMRBK and the value loading ftead\_w is obtained. By this conversion it is achieved that khc\_w has the plausible value range [0..1].
  - > The additive mixture correction (ti-correction with rkte\_w) is obtained from the relative charge with scavenge gas particles currently flowing into the cylinders (rlteev\_w) multiplied by the loading ftead\_w. Rlteev\_w is a value related to pure air. Transport and mixing in the intake manifold are already taken into consideration in rlteev\_w.
  - > For the calculation of rlteev\_w at first the desired pulse duty cycle, by which the PCV power stage is activated, is transferred to a simulation of the PCV timer. Here a pulse duty cycle course is calculated which comes quite close to the actual mechanical pulse duty cycle by which the PCV adjusts (as delay of the PCV timer approx. half of the current cycle duration is assumed).
  - > With the pulse duty cycle "tateist" calculated from this, the mass flow (mste\_w) currently flowing through the PCV into the intake manifold is calculated without temporal cycle offset (important!!!) from the actual pulse duty cycle, from the ambient temperature, from the ambient pressure as well as from the manifold pressure. This is done in %BGTEV. Mste\_w is the mass flow, provided pure air would come from the PCV.
  - > In the TEB the transport time and the mixing in the intake manifold to which the scavenge gas particles are subject to is then taken into consideration. The mass flow scavenge gas msteev\_w currently being siphoned from the intake manifold is obtained (still provided pure air is coming). Finally the relative charge purge control rlteev\_w, i.e. the relative charge in the cylinder which was caused by regenerating gas is obtained by a division by nmot\_w and by a re-normalization (KUMSRL).
  - > With rlteev\_w on its own no mixture correction can be performed. The needed mixture correction is dependent on the HC concentration in the scavenging flow. In case of pure air the mixture correction is zero since the mass flow flowing through the PCV is already included in the calculation in the charge sensing.  
The necessary mixture correction rkte\_w is obtained from the product of the loading (ftead\_w) by rlteev\_w.  
The loading ftead\_w is calculated from the HC concentration khc\_w which in turn is continuously learned from the deviations of the mean value of the Lambda controller. The re-normalization factor khc\_w  
-> ftead\_w is calculated related to 20,7 = 14,7 \* 1.4142 :  
\* 14,7.....: stoichiometric ratio "air mass / fuel mass"  
\* 1.4142....: = root (roh\_fuel / roh\_air) assuming that fuel vapor is double as dense as air
- It was neglected that the maximum of the flow rate function PSI for HC gas is slightly different to the maximum of air.  
Remark: Law for mass flow flowing through restrictor dependent on ambient temperature and ambient pressure:  
$$mp(rohu, pu) = mp = u * Aa * PSI * SQRT(2 * pu * rohu)$$
  
In practice a factor 30 results!! => FUMRBK = 30 !







Formulas:  
-----

Volume flow and mass flow through the PCV in dependency on ambient pressure and temperature:  
Siphoned volume flow (thus with  $p_u$  and  $T_u$ )  
 $vp = u * A_a * PSI * \sqrt{2 * p_u / \rho_{ohu}}$

Siphoned mass flow:  
 $mp = u * A_a * PSI * \sqrt{2 * p_u * \rho_{ohu}}$

Ratio mass / volume:  
 $mp = vp * \rho_{ohu}$

Normalization to temperature  $T_o$  and pressure  $p_o$ :  
 $\rho_{ohu} = \rho_{oh_o} * p_u / p_o * T_o / T_u$

$\Rightarrow vp = vp_o * PSI * \sqrt{T_u / T_o}$   
 $\Rightarrow mp = mp_o * PSI + p_u / p_o * \sqrt{T_o / T_u}$

Fuel mass flow through a PCV (pure fuel vapor provided) at known mass flow air:  
 $mktev = mltev * \sqrt{\rho_{oh\_Kraftst.} / \rho_{oh\_Luft}} = mltev * 1.4142$

Through a PCV the 1.4142-fold fuel mass passes referred to air !!!  
Reason: Stoichiometric ratio mass portions air / mass portions fuel = 14.7  
Density fuel / density air = 2 (assumed to be constant for the sake of simplification)  
Mass flow through PCV, however, only  $\sqrt{2}$  times that of air

$\Rightarrow$  If the PCV is open so wide that in ml 1% air flow through PCV is contained this PCV opening at the same load-/engine speed point would cause a Lambda deviation of 20.7% with fuel vapor.

This value is independent of the altitude and the temperature since  $mste_w$  is supplied density- and altitude-corrected from %BGTEV.

Description of the ASCET block diagram of the function %TEB:  
=====

The function is subdivided into the following subfunctions:

- > FRTEAUFB - Processing of the Lambda controller values and formation of quotient  $qtetemin$
  - > FTEBER - Calculation purge rate and desired mass flow
  - > FTEFXBER - Subfunction for the calculation of the maximum of the purge rate
  - > FTEFINT - Integrator purge rate and integrator mass flow purge control valve
  - > FTEADBER - Calculation of HC concentration of the scavenge gas flow, of the loading and of a filtered value of the loading
  - > RKTEBER - Calculation of the relative fuel portion purge control
  - > HBELBER - Calculation of the bit  $B_{lrar}$  at high loading and of other bits
  - > MITEBER - Calculation of requested minimum torque purge control
- > FRTEAUFB - Formation quotient:  $qtetemin$  and processing of the Lambda controller values  
-----
- > Formation of the quotient  $qtetemin$ 
    - The minimum value of  $te_w$  and  $te2_w$  is used
    - With mono Lambda control ( $SY\_STERVK = FALSE$ ) automatically  $te_w$  is used.
    - After division by  $TEMIN$  the variable  $qtetemin$  is formed. It indicates how far the smallest  $te$  is still away from the minimum value  $TEMIN$ .  $Qtetemin$  is needed in the purge rate control FTEBER.
  - > Formation of  $frmxa_w$  ( $frmxa$ ) (maximum deflection of  $fr_w$  and  $fr2_w$ )
    - the absolute value of the deviation of  $frm_w$  and  $frm2_w$  from 1.0 is formed.
    - via a transfer switch  $frmxa_w$  is determined with respect to the value  $frm_w$  or  $frm2_w$ , which has the greater absolute value of the deviation from 1.0
    - For mono Lambda control ( $SY\_STERVK = FALSE$ ) automatically  $frmxa_w = frm_w$ .
  - > Formation of  $frmit_w$  (mean value related to  $fr_w$  and  $fr2_w$ )
    - if  $B_{lr}$  and  $B_{lr2} = TRUE$  the mean value  $frmit_w$  is formed with respect to  $(frm_w + frm2_w) / 2$
    - if only  $B_{lr2} = FALSE$  the  $frm_w$  is used for the mean value  $frmit_w$
    - if only  $B_{lr} = TRUE$ , but  $B_{lr} = FALSE$  the  $frm2_w$  is used for the mean value





Description of the subfunction FTEBER:

- The purge rate (ftefsoll\_w) is controlled such that a fuel portion defined in KFTEKA should be reached. The fuel portion is calculated with respect to: fthead\_w \* ftefsoll\_w. However, if the injection time te lies close to TEMIN only a small fuel portion can be realized.
- Via the controller amplification FSRFTEF the control behaviour at fthead\_w \* ftefsoll\_w can be adjusted approx. equal to KFTEKA. The smaller FSRFTEF, the "softer" the control characteristic.
- Via the limiting value action (FQTEFR (frmx) as well as FQTEPT (pte)) the purge rate is controlled down in case of large fr-deviations and in case of an unpermissibly high canister vacuum.
- Via the characteristic FQTEVA the increasing control can be made increasingly quicker with increasing purge rate.
- The speed of the increasing control is given in the map KFQTE dependent on ml and on the deviation of the frmit from 1.
- Subfunction FTEFXBER:
  - The max. purge rate is limited by a number of characteristics / maps:
    - FQTEDL: Decrease of purge rate if a negative load gradient is detected
    - KFFTEAN: Purge rate in case of TEB without Lambda control (limp-home purge rate)
    - KFFTEAX: Limitation of purge rate in dependency on ml and tans
    - KFTATX: Max. PCV volume flow reduced by map in percent to the maximum flow rate through the open PCV
    - FTEINIX: Characteristic purge rate limitation dependent on the integral mass flow PCV after purge break

Remarks to the initial limitation of the purge rate (FTEINIX):

On vehicles on which the ACF is "engine distant" the pipe ACF-PCV often has a length of over 3 m. If now, e.g. in case of a fully loaded ACF, the purge rate is activated after a long deactivation phase at first pure air flows through the PCV into the intake manifold. Only once this air has completely been siphoned the HC concentration suddenly increases immensely. So that the purge rate cannot increase too much until then and so that no too strong enrichment occurs the purge rate can be limited dependent on the integral of the air taken in after a purge break. Only once more scavenge gas was taken in than can remain in the the pipe ACF-PCV, shall the purge rate be able to increase to higher values.

Remarks to the limitation at a neg. load gradient (FQTEDL):

- unbuffered charcoal canisters can cause fast HC-concentration change
- the desired purge rate should then be decreased
- For this mlsol\_w is low pass filtered (PT1). The filtered signal is divided through mlsol\_w. One ist subtracted. You get the procentual load change. The value ist positive, if a negative load change is detected.
- This procentual load change is multiplied with the desired purge rate. You get dmlftf.
- Dmlftf is source for FQTEDL. FQTEDL contains factors in the Range [0 ... 1.0]. This factor is a degree for purge rate decrease.
- The decrease is realised by a limitation of the purge rate: Limit = Factor \* Old desired Purge rate
- This causes an exponential decrease of ftefsoll\_w.

Example for FQTEDL:

0	0.01	0.02	0.05	0.1
1	1	0.9	0.9	0.5

- Start purge rate = 0.05
- procentual load change = 10 = const.

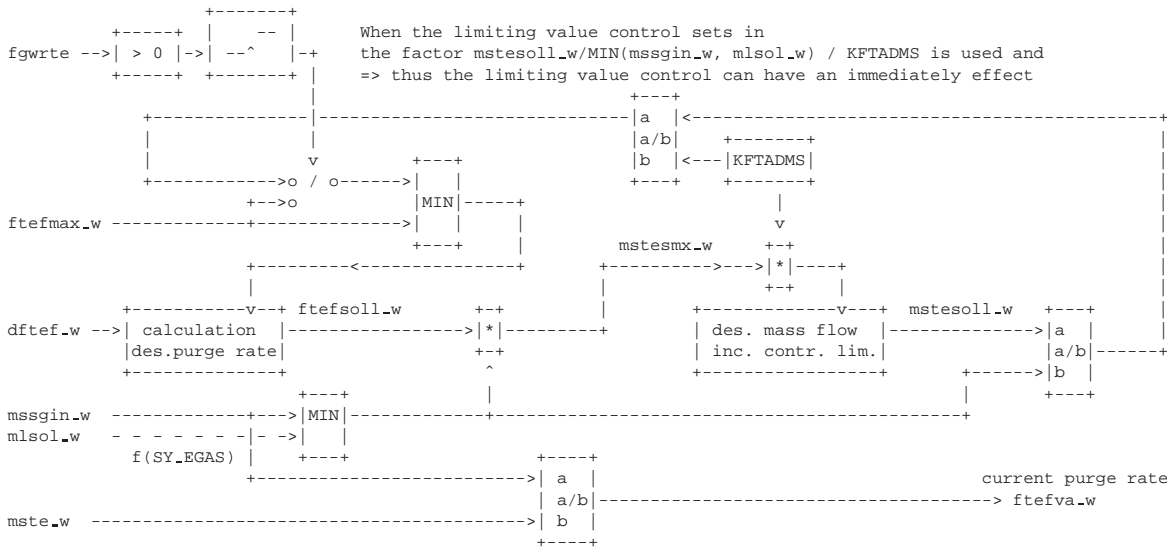
0.05 \* 10 => 0.5 => \* 0.5  
 0.025 \* 10 => 0.25 => \* 0.5  
 0.0125 \* 10 => 0.125 => \* 0.5  
 0.00625 \* 10 => 0.0625 => \* 0.8  
 0.005 \* 10 => 0.05 => \* 0.9

Start	ftefsoll_w = 0.05
=> after 20 ms	ftefsoll_w = 0.025
=> after 40 ms	ftefsoll_w = 0.0125
=> after 60 ms	ftefsoll_w = 0.00625
=> after 80 ms	ftefsoll_w = 0.005
=> after 100 ms	ftefsoll_w = 0.0045

and so on. The purge rate ist first fast, then slower decreased.



The following principle diagram is for the understanding of the purge rate and desired mass flow calculation by means of the subfunction FTEFINT:



The integrators for desired purge rate and for desired air mass are in the subfunction FTEFINT. This separation was made in order to be able to adjust a maximum increase of the mass flow PCV separately from the purge rate control. Via DMSTES the mass flow increase can be chosen dependent on the current mass flow purge control. Choosing the minimum ( $mssgin\_w / mlsol\_w * fafteptk\_w$ ) has the effect that just before the throttle valve is closed already the new smaller pulse duty cycle is passed on to the PCV timer. This prevents mixture faults in case of neg. load changes. The system constant SY\_EGAS decides whether  $mlsol\_w$  is to be used for the comparison or whether  $mssgin\_w$  is used directly. A quickly closing of CPV for diagnosis function can be made with  $B\_qtedab = TRUE$ . In this case is switched of closing time  $TQTEDAB$ . With  $KFTADMS$  it is possible to reduce the PCV mass flow at dynamic engine conditions. With  $KFTADMS$  it is possible to reduce Lambda deviations at load changes.

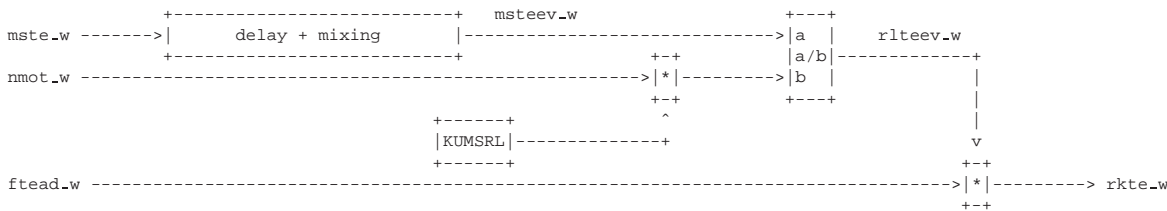
> FTEADBER - Calculation of the HC concentration of the scavenge gas flow (loading) and of a filtered value of the loading

- The HC concentration is calculated from the integral of the deviation of the  $frmit\_w$  (mean value from  $frm$  and  $frm2$ ) if  $B\_te = TRUE$ .
- Apart from depending on  $ml$  (ZBTEML) the integration speed also depends on a value from the characteristics  $FBTEB$  and  $FBTEVA$  determined by the chosen minimum.
  - $FBTEB$  serves for the reduction of the integration speed in case of a limitation to very small purge rates.
  - $FBTEVA$  serves to avoid an oscillation tendency  $fr$  (resp.  $frm$ ) towards  $rkte$ .
- From the HC concentration the loading  $fthead\_w$  is calculated (multiplication by  $FUMBRK = 30$ )
- The TEB also provides a filtered value of the loading ( $ftheadf$ ). The low pass filter is necessary so that short-termed oscillations of  $fthead\_w$  are not taken into account. This value is needed e.g. to reduce the engine performance in case of long-termed high loading (see below) and so as to increase the idle speed.



> RKTEBER - Calculation of the relative fuel portion purge control

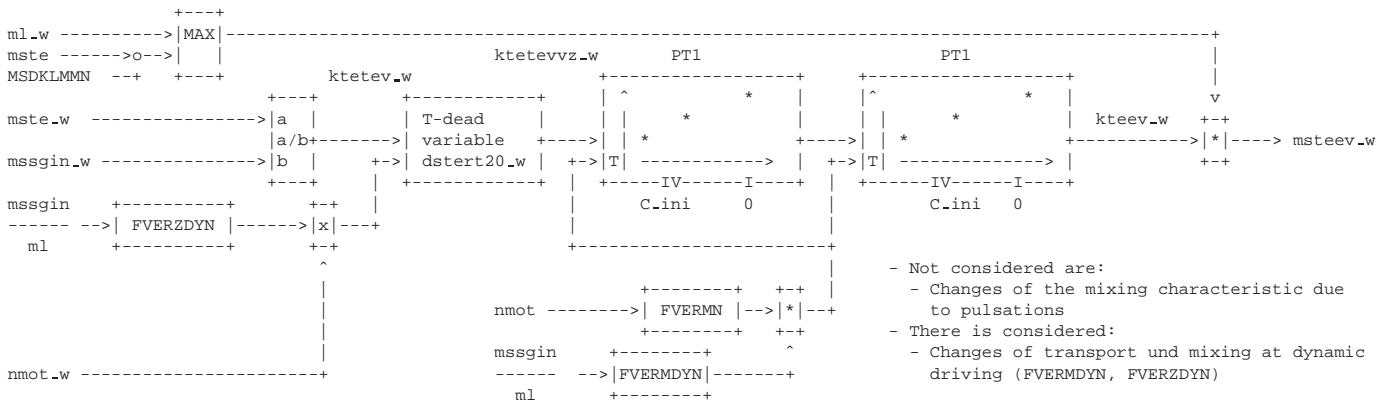
This subfunction at first calculates the mass flow purge control (msteev.w) flowing to the combustion chamber from the mass flow purge control (mste.w) which flows into the intake manifold at the level of the throttle valve. After a division by nmot.w and by the conversion constant KUMSRL the relative charge purge control at the level of the intake valve (rlteev.w) is obtained. After a multiplication by the loading ftead.w the relative fuel portion purge control rkte.w is obtained. In order to maintain the injection time at the intake valve, rkte.w is subtracted from the value rk.w without purge control during the injection calculation => "additive action in the TEB" .



So in the subfunction RKTEBER the transport and the mixing in the intake manifold are also described.  
> The mass flow mste.w led in at the PCV is at first converted to a concentration "scavenge gas purge control in air" (ktetev.w).

> After delay (variable lag element) and after mixing (filtering 2 \* PT1 with the same time constant) the concentration of scavenge gas purge control at the intake valve (kteev.w) is calculated.

> By a multiplication by ml.w the mass flow purge control at the intake valve of the engine (msteev.w) is obtained.  
Attention: msteev.w refers to pure air as scavenge gas !



- Not considered are:
- Changes of the mixing characteristic due to pulsations
- There is considered:
- Changes of transport und mixing at dynamic driving (FVERMDYN, FVERZDYN)

Calculation of delay and mixing in the intake manifold

> HBELBER - Calculation of the bit B\_lrar "mixture adaptation reduced range" at high loading

as well as of the bit loading at maximum limit stop (B\_tehbx).

- > In case of a high fuel concentration in the scavenging flow the Lambda controller frequency may possibly change due to an uneven distribution of the scavenge gas to the individual cylinders. OBDII functions which evaluate the Lambda controller (DLSA, DKAT) must be blocked. - A high loading is an indication for hot fuel. There is a risk of vapor blisters occurring in the intake valve. The diagnostic fuel supply system evaluates the adaptation factors of the LRA. They are limited via B\_lrar to a lift lower than the fault thresholds.
- > In case of C\_ini the flip-flop is always set: If the purge rate exceeds the value FTEHB or if the frmit.w exceeds the threshold FRHB (if B\_tei = 1) and if at the same time the loading is less or greater than FTEHB, then the flip-flop is reset. If ftead.w rises above FTEHB or if ftea falls below FTEAHB, then the flip-flop is set again.
- > If the loading undershoots the value FTEADAB an error in the fuel supply system is assumed and the flag " canister purge control ready for abort" (B.teabb) is set.
- > An indication for a pilot control fault (pilot control too rich) or for a leaking PCV is the dead stop of the loading integrator at the maximum value FTEADMX. The bit B\_tehbx can be used e.g. for the switch-over of the controller speed of the fr and of the maximum fr-lift.



> MITEBER - Calculation of the demanded minimum torque purge control  
-----

Calculation of a minimum torque (mitebg) for the torque management for the increase of the purge rate at high loading.

From the filtered value of the loading fteadf (see above) and from the driver's request torque mifa\_w a desired engine performance for engine operation with purge control is derived, which is corrected by an engine speed dependent evaluation factor fbetate.

It is e.g. possible to increase the air charge of the engine with long-lasting high loading and with a low induced driver's request torque, so as to increase the purged quantity. The torque coordination ensures that the driver will not notice this while at the same time the ignition angle is retarded and thus the engine performance is worsened.

For the determination of the torque mifafu\_w (torque driver's request for charge) the value mitebg is included in a maximum selection.

- etate is the desired engine performance with purge control. A desired low engine performance is only reached if mitebg\_w is not high-limited to zero by etate = 100%.
- mifa is the torque requested by the driver. The charge resulting from it assumes an engine performance of 100%.

The calculation of etate:

- > The desired engine performance is stored in the map KFETATE dependent on fteadf and on mifa\_w.  
By means of this map very small injection times te with high fuel portions purge control can be avoided.  
By reducing the engine performance the small te-values are no longer reached.
- > In the characteristic FETATEBN an evaluation factor is stored dependent on nmot, which corrects the etatesoll change of 100%.
- > The core of this subfunction is an integrator whose output gives the currently desired engine performance. At the beginning of the purge control phase the input value is adjusted to - ZETATE, so that the integrator integrates down to 0 starting from 100%.  
Once the integrator reaches its minimum, it is stopped.
- > For non E-Gas systems the performance etate is set to 100% by means of the system constant SY\_EGAS.

## APP TEB 95.80 Application hint

Instruction for the application of the entire purge control:  
=====

Concerns sections: TEBEB, BGTEV, ATEV, TEB, (BBTEGA)

Preliminary remark: Apart from this APP. hint also a detailed APP. standard with measurement reports and diagrams exists. This APP. hint can be obtained until the end of 1996 only directly from Mr. Mallebrein, dep. K3/ESY4. Later on (approx. from beginning of 1997) it will also be available in the APS. In case of differences the data should be taken from the detailed APP. hint. If necessary call Tel.: 811/8432

The following must be dealt with prior to an application:

- > Throttle valve activation (%FUEDK): The throttle valve may have no considerable over-, undershoot, it may not flutter.
- > The charge sensing must have been adjusted (adjustment of the pilot control (rl) to +/- 3%-4%, so that the adaptation of the HC concentration is not performed incorrectly, adjustment of ps\_w on the turbo charger stationary as exact as possible).
- > Application of all time constants of the charge sensing, of all temperature models especially on the turbo charger so that the intermediate value manifold pressure (ps\_w) is sufficiently accurate. The manifold pressure is needed in BGTEV for the turbo charger in order to calculate the mass flow PCV.
- > Application of the engine warm-up so that the HC-concentration does not stop learning itself there.
- > The transient control must be adjusted in order to be reliably able to learn a HC-concentration from the fr-course and so as to avoid the limiting value control being erroneously activated.
- > Application of the Lambda control (incl. all activation conditions). If no exhaust gas test has yet been performed the control downstream catalyst must not necessarily be adjusted (resp. active).

Application of the BBTEGA and of the TEBEB:

- > In BBTEGA the time for the purge control can be adjusted. Make TTEINI, TTE, TTEAE as long as possible, make TTEGAI, TTEGA as short as possible (only for application phase, for FTP-test see values in BBTEGA).
- > Adjust TEBEB according to specifications in the section

Application of the sections BGTEV, ATEV:

- > The main work of a purge control application will have to be done in BGTEV (turbo resp. aspirating engine version) !!!  
BGTEV must definitely be adjusted prior to a test on the engine test bench reps. chassis test bench ! See in BGTEV !
- > ATEV is also to be adjusted according to the suggestion in the section ATEV.

Actual core function TEB:

- > Most of the data are general and not vehicle-specific !! - The values shown below are to be used.
- > However, KFQTE, ZBTEML, KFTATX, FVERZTE, FVERMN and DMSTES are engine-specific ! For the initial entering of data the data given below can be used.
  - KFQTE, ZBTEML depend on the delay time of the Lambda control - the larger the delay time the smaller the values.
  - KFTATX must especially be adjusted on the turbo engine, so that in the range where the turbo charger sets in (ps\_w/pu around 1.0) the PCV is opened less especially at low engine speeds.
  - FVERZTE and FVERMN depend on the design of the intake manifold, on the PCV intake position and on the ratio of intake manifold volume to lift volume. The variables are to be determined by performing jumps while scavenge gas is taken in.
  - DMSTES is to be determined after the application of KFQTE and ZBTEML. For a not buffered ACF the increasing control speed (PCV mass flow increase) must be distinctly smaller than for a buffered ACF.
  - With KFTADMS Lambda deviations can be reduced. Output values smaller than one reduce the purge mass flow at dynamic driving.

The data, which follow now, are for an initial entry. Depending on the engine size possibly ml base points need to be shifted a little. The data are only guidance values and were thought up by the function developer without having been tested on the vehicle. They do not represent an application state on an actually existing vehicle.



Data for the initial entry of all parameters of the TEB:

Subfunction FRTEAUFB:

> TEMIN: see injection calculation

Subfunction FTEBER:

FQTEPT: Limiting value control for the limitation of canister vacuum                      unit [-]  
 -----  
 - 32.00   -28.00   -25.00   -20.00   -15.00   0   pte [hPa]  
 -----  
 15.75   4   2   1   0   0   factor

FQTEFR: Limiting value control to avoid uncontrolled Lambda controller deviations                      unit [-]  
 -----  
 0.75   0.80   0.86   0.92   1.08   1.14   1.20   1.25   fr  
 -----  
 12   4   2   0   0   2   4   12   factor

KFFTEAN: Map maximum purge rate for limp-home purge control                      unit purge rate [-]  
 -----  
 nmot[rpm]                      600   800   1000   1400   1800   2400   3000   3500   4000   5000  
 -----  
 wdkba[%]  
 4   |   0.005   0.005   0.006   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 10   |   0.005   0.005   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 16   |   0.005   0.006   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 24   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 34   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 45   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 55   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 65   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 80   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007  
 100   |   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007   0.007

FQTEDL: Purge rate decrease factor at neg. load change  
 -----  
 0   0.01   0.02   0.05   0.1  
 -----  
 1   1   0.9   0.9   0.5

ZMLTE: 1 s

KFFTEAX : Map maximum purge rate for normal operating                      unit purge rate [-]  
 -----  
 ml [kg/h]                      10   20   50   100   500  
 -----  
 tans [°C]  
 -30   |   0.02   0.02   0.03   0.03   0.03  
 0   |   0.04   0.04   0.06   0.06   0.08  
 20   |   0.10   0.10   0.10   0.10   0.10  
 80   |   0.10   0.10   0.10   0.10   0.10





KFTATX: Map maximum pulse duty cycle unit pulse duty cycle [%]  
(Recommendation for turbo engine - pspu around 1.0 the pulse duty cycle is reduced especially at low engine speeds - on an aspirating engine here no reduction needs to be performed)

nmot [rpm]	600	800	1000	1400	1800	2400	3000	3500	4000	5000
pspu										
0.30	60.00	60.00	70.00	80.00	80.00	99.61	99.61	99.61	99.61	99.61
0.90	60.00	60.00	70.00	80.00	80.00	99.61	99.61	99.61	99.61	99.61
0.95	10.00	15.00	20.00	25.00	30.00	40.00	50.00	65.00	80.00	99.61
1.05	10.00	15.00	20.00	25.00	30.00	40.00	50.00	65.00	80.00	99.61
1.10	80.00	80.00	80.00	90.00	99.61	99.61	99.61	99.61	99.61	99.61
1.70	99.61	99.61	99.61	99.61	99.61	99.61	99.61	99.61	99.61	99.61

KFTEKA : Map maximum fuel portion purge control unit fuel portion [-]

nmot [l/min]	800	1400	2000	3000	5000
rl [%]					
20	0.4	0.45	0.5	0.5	0.5
50	0.5	0.5	0.5	0.5	0.5
70	0.5	0.5	0.5	0.5	0.5
90	0.5	0.5	0.5	0.5	0.5
120	0.5	0.5	0.5	0.5	0.5

Please note that te\_w each time remains greater than TEMIN.

FKATEB : Characteristic evaluation factor for fuel portion in dependency on qtemin

qtetemin [l]	1.0	1.1	1.2	1.5	2
fbkate	0.0	0.5	1.0	1.0	1.0

FTEINIX : Characteristic maximum purge rate in dependency on the integral air mass after purge break unit purge rate [-]

The example data apply for a pipe ACF-PCV of 4 m length with an internal diameter of 6 mm.

$$V = 4 \text{ m} * \text{Pi} * 0.006 \text{ m} * 0.006 \text{ m} / 4 = 113 \text{ E-6 m}^3 = 113 \text{ cm}^3 \Rightarrow 150 \text{ E-6 kg}$$

Application recommendation: At first (for small values of imsteini) the purge rate may rise to high values. However, after exactly that mass scavenge gas was taken in, which was in the pipe as a precaution the purge rate is at first reduced to 0.01. Then it can be increased to 0.1.

For application data: Let the purge rate at low values for a longer time (until e.g. 1g).

imsteini [g]	0.1	0.20	0.5	1.0	2.0
Output	0.02	0.02	0.01	0.02	0.1

TFTEINI [s]: Time for detection of purge break: 30 s (in any case shorter than TTEGA)

KFQTE: Increasing control speed desired purge rate unit [l/s]

ml [kg/h]	10	20	50	100	200	500
frmit						
0.7	0.0006	0.0010	0.0020	0.0040	0.0060	0.0100
0.9	0.0002	0.0003	0.0005	0.0010	0.0016	0.0026
1.0	0.0006	0.0010	0.0020	0.0040	0.0060	0.0100
1.1	0.0002	0.0003	0.0005	0.0010	0.0016	0.0026
1.3	0.0006	0.0010	0.0020	0.0040	0.0060	0.0100

FSRFTEF: Factor steepness purge rate controller 20 [-]

FQTEVA: Increasing control progression desired purge rate unit [-]

0.002	0.006	0.012	0.020	0.040	0.100	ftefva [-]
1.00	2.00	3.00	4.00	6.00	8.00	factor progression [-]

TVSATEM: Delay time for PCV closed after fuel cut-off readiness unit [s]

-30	-10	20	40	70	90	tmot [°C]
3	2	1.5	1.0	0.8	0.8	delay time [s]



TQTEAB: Decreasing control time PCV at the end of a purge control phase TQTEAB: 10 s

TQTEDAB: Quickly decreasing control time PCV at the end of a purge control phase TQTEDAB: 2 s

DMSTES: Increase of mass flow PCV

0.005	0.02	0.08	0.32	1.28	5.12	mstesoll_w [kg/h]
25.6	51.2	204.8	819.2	2048	5120	output DMSTES [kg/h]

ZMSSGIN: Filter time constant for mssgin\_w: 0.6 s

KFTADMS: Map for reduction of the purge mass flow at dynamic engine driving

dmssginr	-1	-0.4	0	0,4	1
nmot					
600	0.4	0.6	1.03	0.6	0.4
1000	0.5	0.7	1.03	0.7	0.5
2000	0.7	0.8	1.03	0.8	0.7
5000	1.0	1.0	1.03	1.0	1.0

MSDKLMN: Lower limit of msdkalm\_w: max. 75% of the air mass flow at idle: 8 kg/h  
MSDKLMN prevents too high values of ktetev\_w if mshfm is near zero at neg. load change !!!

Subfunction FTEABER:

ZBTEML: Learning speed loading unit [1/s]

10	20	50	100	200	500	ml [kg/h]
0.30	0.50	0.80	1.2	2.0	3.0	learning speed [1/s]

FBTEB: Unlearning brake loading with limitation to small purge rates unit [-]

0.00024	0.00061	0.00122	0.00244	0.00610	0.0122	ftefvab [-]
0	0.0	0.1	0.2	0.5	0.9961	factor learning speed [-]

FBTEVA: Purge rate dependent learning speed of the loading unit [-]

0.000	0.005	0.01	0.020	0.050	0.100	ftefva [-]
0.4	0.9961	0.9961	0.5	0.2	0.1	factor learning speed [-]

KHCTEMX: Maximum fuel concentration scavenge gas: 1.25 [-]

KHCTEMN: Minimum fuel concentration scavenge gas: -0.25 [-]

FUMRBRK: Factor conversion loading / HC conc.: 30 [-]

ZKFTBAD: Time constant filtering of the loading: 100 [s]



Subfunction RKTEBER:

FVERZDYN: Factor delay time scavenge gas in the intake manifold: 1.6.E-4 [min]  
=> continued transport at 1000 rpm: 1000 rpm \* 1.6E-4 min = 0.160 => delay = 20 ms / 0.16 = 125 ms

0	0.4	1	2	10	qmsdyn
0.0001	0.00014	0.00016	0.0003	0.0005	Faktor transportation / time slot [-]

FVERMN: Characteristic factor mixing in the intake manifold []

800	1200	1800	2600	3600	5000	nmot [1/min]
0.25	0.30	0.35	0.40	0.45	0.50	Faktor Vermischung [-]

FVERMDYN: characteristic line dynamic part gas mixing in manifold []

0	0.4	1	2	10	qmsdyn
1.5	1.2	1	1.4	2.5	Faktor dyn. part in mixing [-]

NVERZMN: 800/min (idle speed)

KUMSRL: see charge sensing: V\_Hub [1] / 2578

DSTEMIN 0.01 []

Subfunction MITEBER:

KFETATE : Map desired performance with te close to TEMIN unit performance [%]

mifa [%]	8	16	32	60	100
ftheadf					
12	90	100	100	100	100
20	80	90	95	100	100
30	70	80	90	95	100

FETATEBN: Characteristic evaluation factor for desired engine performance dependent on the engine speed

600	1200	2000	3000	5000	nmot [rpm]
1	1	0.5	0	0	evaluation factor

ZETATE: Ramp steepness change of engine performance 1 [%/s]

Subfunction HBELBER:

DFTEAHB: Fuel portion detection high loading: 0.3 [-]

FTEHB: Loading threshold for detection high loading: 5 [-]

FTEPHB: Minimum purge rate for resetting high loading: 0.01 [-]

FRHB: fr threshold to prevent resetting high loading 1.24 [-]

FTEADAB: Threshold for setting B\_teabb -4 [-]

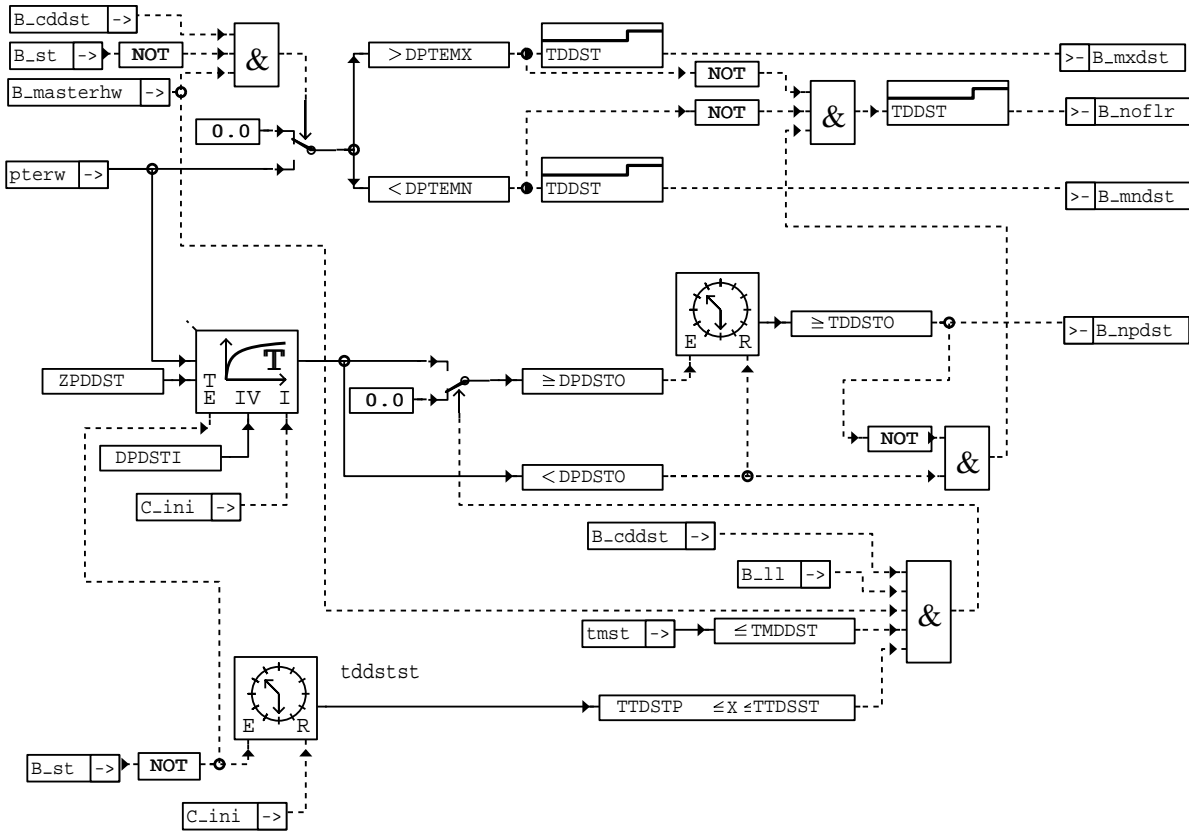
FTEADMX: Threshold for setting B\_tebhx 37.5 = KHCTEMX \* FUMBRK [-]

## DDST 7.30 diagnosis of tank pressure sensor

### FDEF DDST 7.30 Function definition

The tank pressure sensor provides information on the tank differential pressure to the ambient. The tank pressure sensor is required for the diagnosis of the purge control system (leakage detection).

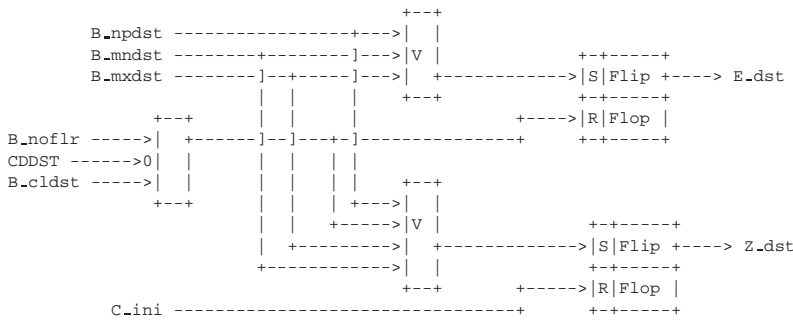
The sensor signal is monitored concerning electronic plausibility (B\_mndst, B\_mxdst) as well as functional plausibility (B\_npdst).



**ddst-ddst**

Interaction with other modules:

In fault management module:



Fault code storage with: CDDST ; LDDST ; FLCDDST ; HLCDDST ; U1DST ; U2DST ; B\_mndst \ B\_npdst \ B\_noflr  
U1= ; U2=

**ABK DDST 7.30 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
DPDSTI			FW	Initialization pressure for low pass filtered tank pressure
DPDSTO			FW	upper pressure threshold for detection of press.sensor. error
DPTEMN			FW	min. plausible differential pressure
DPTEMX			FW	max. plausible differential pressure
TDDST			FW	debouncing time for fault detection tank pressure sensor
TDDSTO			FW	delay time for press. sensor rationality error
TMDST			FW	eng. temp. thrshreshold for pressure sensor rationality check
TTDSST			FW	time period after start for enabled press. sensor rationality check
TTDSTP			FW	time period for stabilization of low pass
ZPDDST			FW	time constant for tank pressure sensor rationality check
Variable	Source		Type	Description
B_CDDST	PROKON		EIN	function active per codeword CDDST
B_LL	MSF		EIN	Condition idle
B_MASTERHW			EIN	Condition Master-SG corresponding with code-pin (plausible)
B_MNDST	DDST		AUS	condition fault type "minimum value" detected: tank pressure sensor



Variable	Source	Type	Description
B_MXDST	DDST	AUS	condition fault type "maximum value" detected: tank pressure sensor
B_NOFLR	DDST	AUS	Condition diagnosis finished with o.k. report
B_NPDST	DDST	AUS	condition for fault type "unplausible DS-T signal"
B_ST	SWADAP	EIN	condition for start
C_INI	SWADAP	EIN	ECU-condition for intialisation
PTERW	GGDST	EIN	tank pressure rough value (8 bit)
TDDSTST	DDST	DOK	time after start for press. sensor rationality check
TMST	GGTFM	EIN	engine temperature at start

### FB DDST 7.30 Detailed description of function

Plausibility check of the tank pressure sensor

This check is permanently performed, independently on the regeneration function or the purge control system diagnosis.

The pressure signal may be falsified, caused by wiring interruption or short circuit.

The pressure signal is limited to its minimum and maximum value by the sensor itself.

If the sensor signal exceeds or falls short of the limits DPTEMX (DPTEMN), then a wiring fault has occurred.

Functional plausibility check of the tank pressure sensor.

In case of the sensor providing a constant overpressure signal, the leakage diagnosis (%DTES) will be disabled.

Hence this case must be checked. It will be done at idle condition and after a cold start of the engine. If the lowpass filtered pressure "ptedstp" exceeds DPDSTO for a period longer than TDDSTO, a defective pressure sensor will be notified (B\_npdst).

2 SG: Durch B.masterhw wird beim 2SG-System die Diagnose im Slave-Steuergerät abgeschaltet.

### APP DDST 7.30 Application hint

#### 1. Characteristic values

DPTEMX 29.5 hPa (RB pressure sensor DS-T1 and DS-T2)  
DPTEMN -28.2 hPa (RB pressure sensor DS-T1 and DS-T2)  
TDDST 3...5 s

Functional plausibility check

TDDST: Max. engine temp. threshold for detection of a cold start (35 °C) (Not to be exceeded in an FTP)

TTDSST: Max. time after start for conducting of the funktional plausibility check (10 s)

TTDSTP: Time after initialisation for stabilization of the low pass

ZPDDST: time constant for low pass filter. It must be assured that low pass ZPDDST is stabilized lon gbefore TDDST has elapsed, else B\_noflr will irrationally be set before B\_plaus is set.

DPDSTI: Initialisation value of tank pressure low pass (0 hPa)

DPDSTO: pressure threshold for detection of implausibel sensor

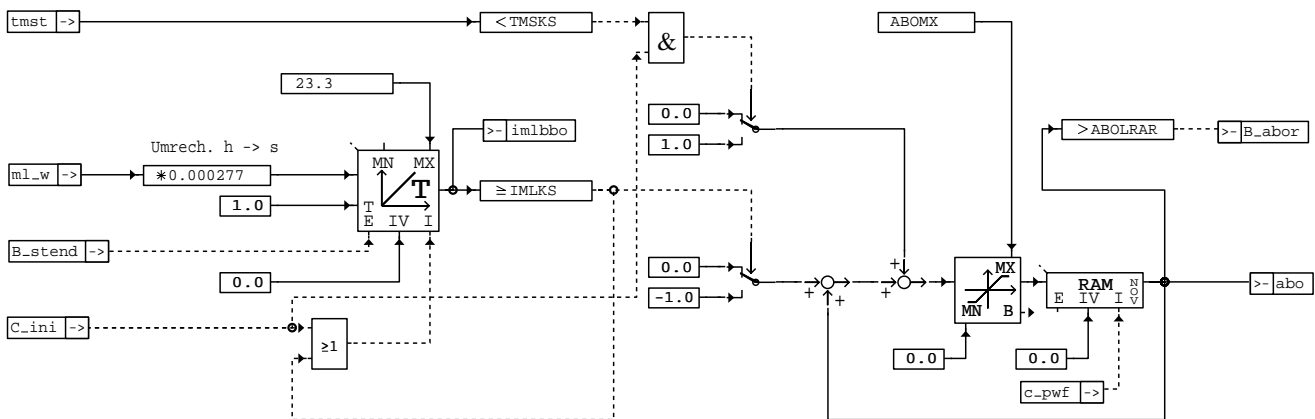
This threshold to be applied identically as DPTEBO (in %DTES) only if the vehicle has no excessive tank overpressures during plausibility check. Otherwise the check can be disabled by setting DPDSTO = max. value.

In any case DPDSTO to be significantly higher than the specified sensor offset.

TDDSTO: Delay time for notification of B\_plaus-error. (3 s)

### BBBO 2.10 Start operating range with fuel in oil

#### FDEF BBBO 2.10 Function definition



bbbo-bbbo

bbbo-bbbo



## ABK BBBO 2.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ABOLRAR			FW	threshold numbers of starts with fuel in oil for reduction LRA
ABOMX			FW	max. numbers of starts for recognition of fuel in oil
IMLKS			FW	threshold integrated air mass for detection fuel in oil
TMSKS			FW	engine temperature threshold for detection fuel in oil

Variable	Source	Type	Description
ABO	BBBO	AUS	numbers of starts with fuel in oil
B_ABOR	BBBO	AUS	condition numbers of starts with fuel in oil for reduced adaptive lambda control
B_STEND	BBSTT	EIN	condition end of start
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
IMLBBO	BBBO	AUS	integration air mass for recognizing fuel in oil
ML_W	EGFE	EIN	air mass flow filtered (Word)
TMST	GGTFM	EIN	engine temperature at start

## FW BBBO 2.10 Fixed Values

Parameter	Value	Description
ABOLRAR		threshold numbers of starts with fuel in oil for reduction LRA
ABOMX		max. numbers of starts for recognition of fuel in oil
IMLKS		threshold integrated air mass for detection fuel in oil
TMSKS		engine temperature threshold for detection fuel in oil

## FB BBBO 2.10 Detailed description of function

Fuel can get into the engine oil during cold start. The engine oil gets warm during continued driving. The fuel evaporates. The fuel vapor is delivered to the combustion via the crankcase ventilation. The mixture deviation occurring in the process can amount to up to 30% at idle. The Lambda control corrects this. The mixture adaptation stores this correction as long-term effect. If the values of the mixture adaptation exceed certain values, the error lamp may be triggered. Furthermore the subsequent start may fail, since the starting mixture has become too lean, however, during the start no degassing of the fuel in the oil takes place.

By means of a counter abo the feeding of fuel into oil is simulated. The counter is incremented by one if a start below the temperature threshold TMSKS takes place. This can be the engine and or the intake or the transmission oil temperature of the vehicle.

The counter is decremented if it is ensured that the oil temperature has remained above a threshold for long enough. Then it is ensured that the fuel has degassed again. The air mass flow integrated during a drive or the transmission oil temperature can serve as measure for high oil temperature. When this variable exceeds a threshold the counter is decremented again. In the process zero may not be undershot.

Realization: The air mass ml is integrated in imlbbo. If the integrator value imlbbo is greater than IMLKS the counter abo is decremented and the integrator value imlbbo is reset. Thereby the counter can be decremented several times during an engine run. The counter abo is stored in the permanent RAM.

By the count of the counter abo, which can be limited to a maximum value, the learning speed of the mixture adaptation is varied.

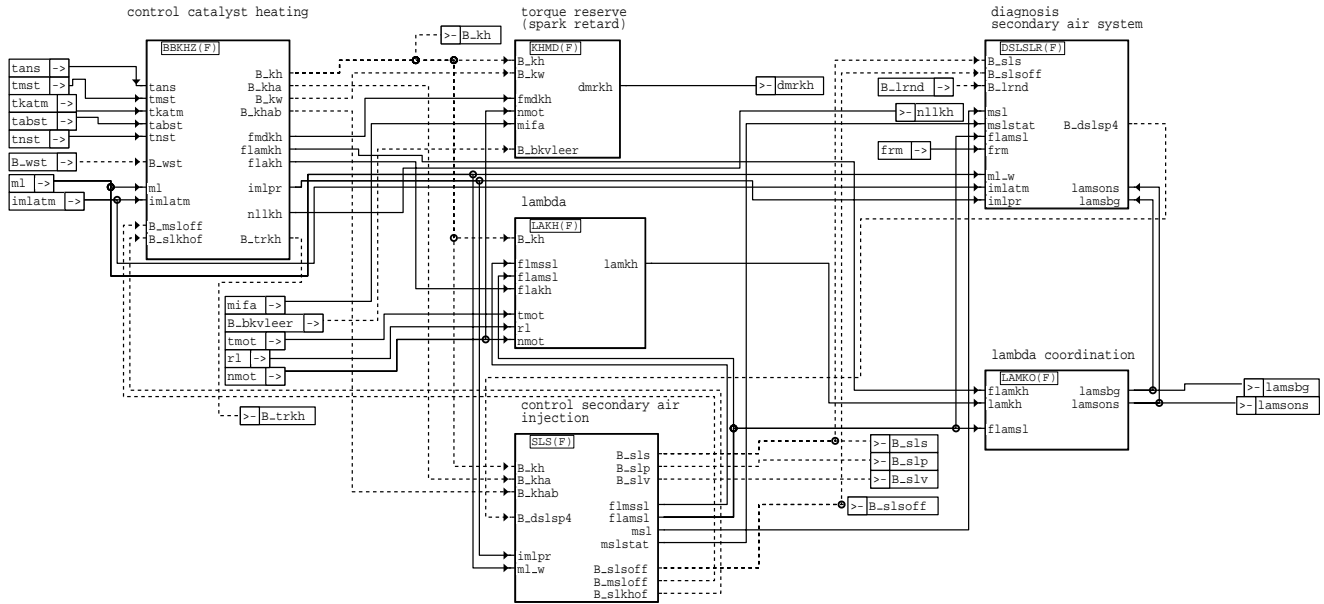
If the counter is greater than the threshold ABOLRAR the condition B\_abor is set, which enables the reduced adaptation ranges in the function %LRA.



APP BBBO 2.10 Application hint

## AK 1.20 Overview Emission reduction / catalyst

### DDEF AK 1.20 Function definition



ak-ak

### ABK AK 1.20 Abbreviations

Variable	Source	Type	Description
B_BKVLLEER	AK	EIN	condition brake booster without enough vacuum
B_DSLSP4	AK	LOK	Condition: Request start of SAI for adaptation/additional diagnosis
B_KH	AK	AUS	condition catalyst heating activated
B_KHA	AK	LOK	request of activated catalyst heating
B_KHAB	AK	LOK	condition catalyst heating terminating
B_KW	AK	LOK	Condition catalyst warming
B_LRND	LREB	EIN	set control bit LR active; request for "NORMAL" or "DIAGNOSIS"
B_MSLOFF	AK	LOK	Condition secondary air mass flow removed after switch off
B_SLKHOF	AK	LOK	condition shut down secondary air pump caused by imlpr threshold
B_SLP	AK	AUS	condition for secondary air pump
B_SLS	AK	AUS	Condition for active secondary air
B_SLSOFF	AK	AUS	Condition end of secondary air after removing secondary air
B_SLV	AK	AUS	condition for secondary air valve
B_TRKH	AK	AUS	Flag for catalyst fast heating
B_WST	ESSTT	EIN	condition for re-start
DMRKH	AK	AUS	torque reserve for catalyzer heating
FLAKH	AK	LOK	Factor control lambda at catalyst heating
FLAMKH	AK	LOK	factor setting up lambda engine nominal at catalyst heating
FLAMSL	AK	LOK	Factor lambda change by secondary air
FLMSSL	AK	LOK	Factor lambda engine by secondary air
FMDKH	AK	LOK	Weighting factor torque reserve for catalyst heating
FRM		EIN	mean value of lambda control factor
IMLATM	ATM	EIN	integrated air mass flow from engine start to maximum value
IMLPR	AK	LOK	relative amount of integrated air mass flow at catalyst heating
LAMKH	AK	LOK	Weighted lambda nominal for catalyzer heating
LAMSBG	AK	AUS	Desired Lambda limitation
LAMSONS	AK	AUS	lambda setpoint value w.r.t. to location of lambda-sensor installation
MIFA	MDFAW	EIN	desired indicated engine torque
ML	SWADAP	EIN	air mass flow
ML_W	AK	LOK	air mass flow filtered (Word)
MSL	AK	LOK	secondary air mass flow
MSLSTAT	AK	LOK	static secondary air mass flow
NLLKH	AK	AUS	Idling speed for catalyzer heating
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
TABST		EIN	Soak Time
TANS	SWADAP	EIN	Intake air temperature
TKATM	ATM	EIN	catalyst temperature (model)
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
TNST		EIN	time after end of start



## FW AK 1.20 Fixed Values

Parameter	Value	Description
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## FB AK 1.20 Detailed description of function

Caused by emission legislations the engine has to be controlled after cold start to reach accelerated catalyst light off.

The required heating energy is mainly provided by thermal exhaust power (exhaust temperature and exhaust mass flow), running the engine with maximum spark retard and increased idle speed. To reduce engine out emissions it is possibly necessary to run the engine lean ( $\lambda = 0,95 \dots 1,05$ ).

Another catalyst heating source uses chemical exhaust energy ("rich warming up") by running the engine rich ( $\lambda = 0,6 \dots 0,95$ ). In combination with secondary air injection the rich exhaust gas reacts inside exhaust manifold or catalyst. The heat of this oxidation process heats the catalyst and reduces simultaneously HC- and CO- emissions.

The catalyst heating function %BBKHZ coordinates the sub-functions:

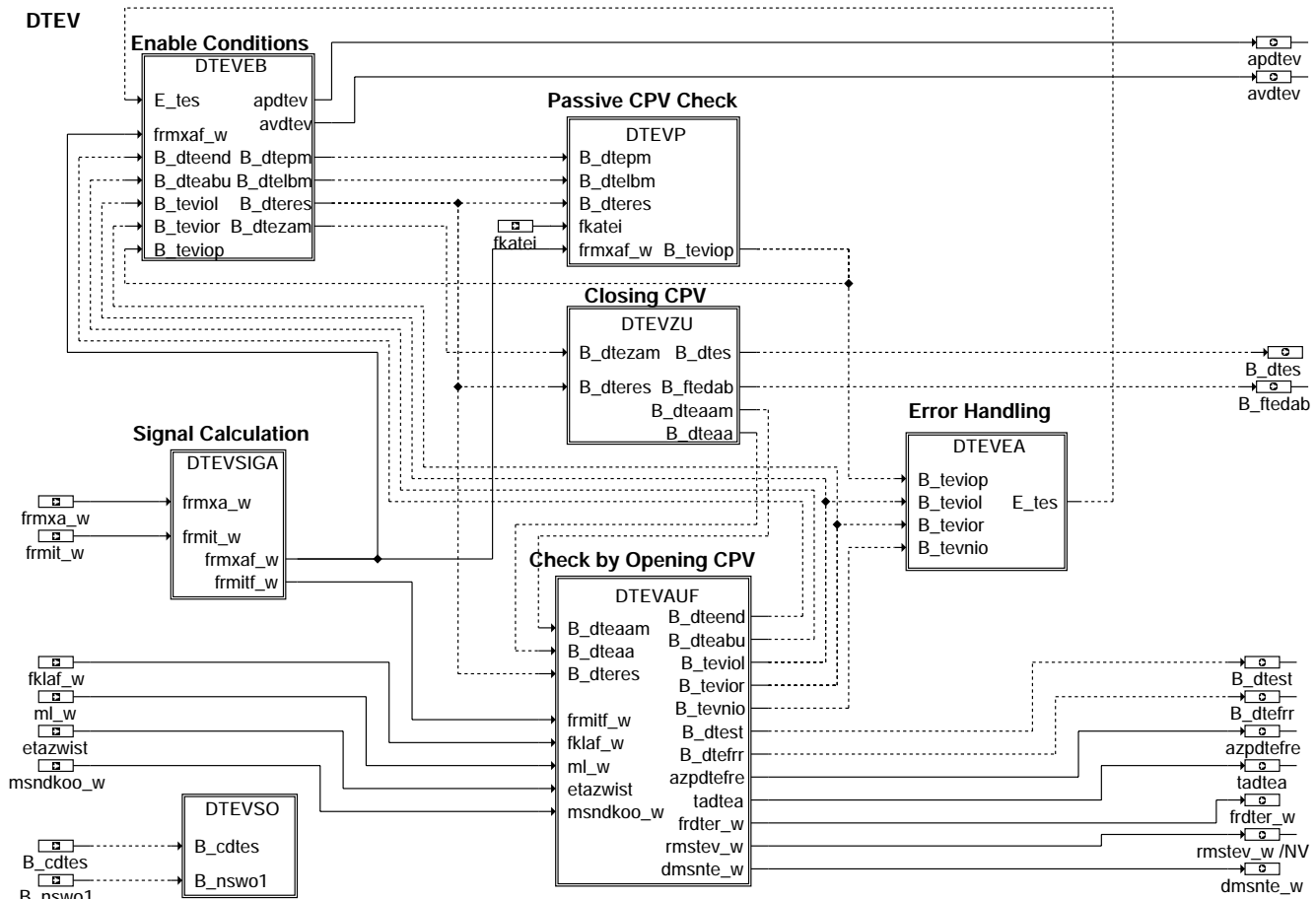
- \* nominal idle speed at catalyst heating inside %BBKHZ,
- \* torque reserve to increase the exhaust temperature by spark retard, combined with increased load inside %KHMD,
- \* mixture control at catalyst heating and lambda - limitation for driveability inside %LAKH and %LAMKO,
- \* secondary air control inside %SLS and OBDII- diagnosis inside %DSLSLR with conventional lambda - control or %DSLSLRS with continuous lambda - control.

For detailed information, see description in each sub-function.

## APP AK 1.20 Application hint

## DTEV 32.90 Diagnosis; canister purge valve (OBDII)

### FDEF DTEV 32.90 Function definition



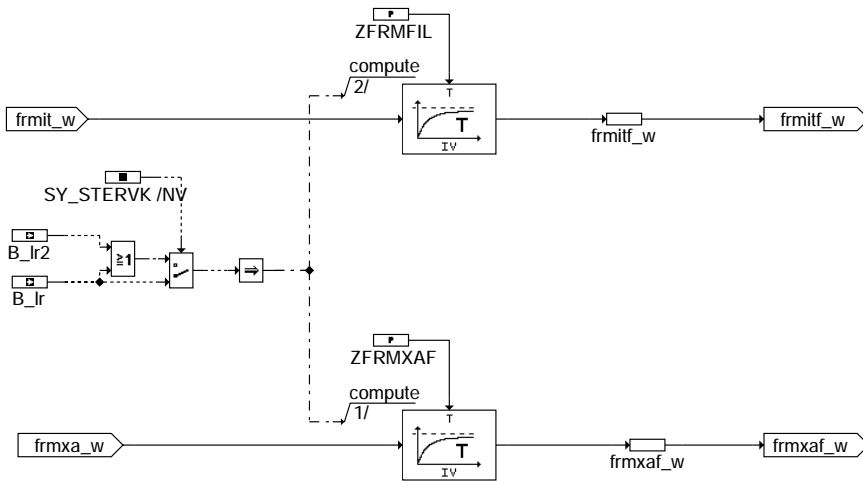
dtev-main

dtev-main



DTEVSIGA: Signal Calculation

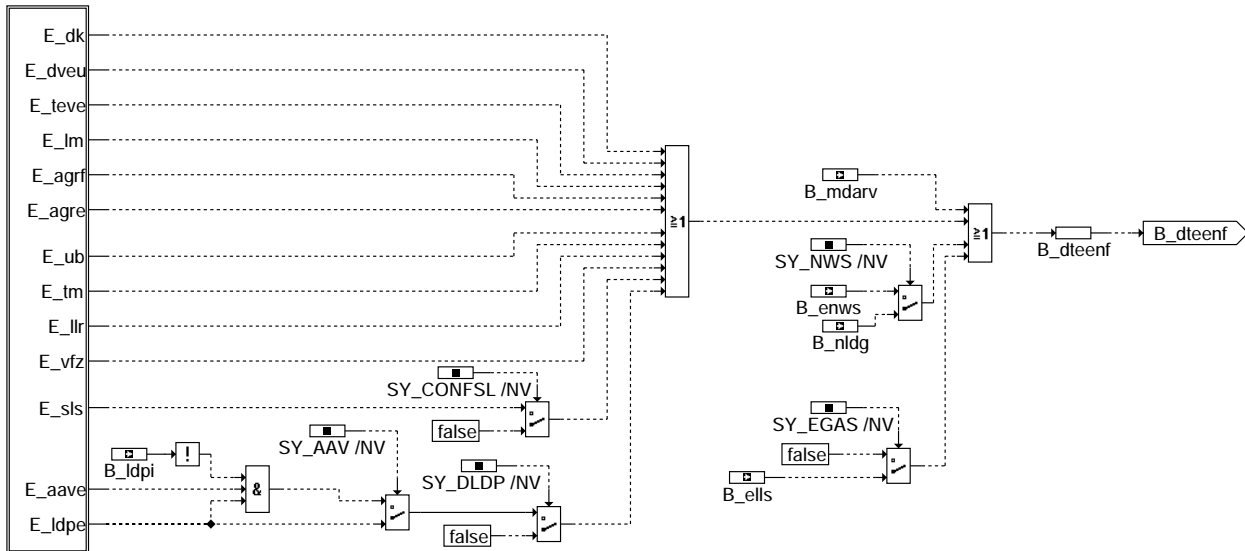
**DTEVSIGA: Signal Calculation**



**dtev-dtevsiga**

DTEVEB: Enable Conditions

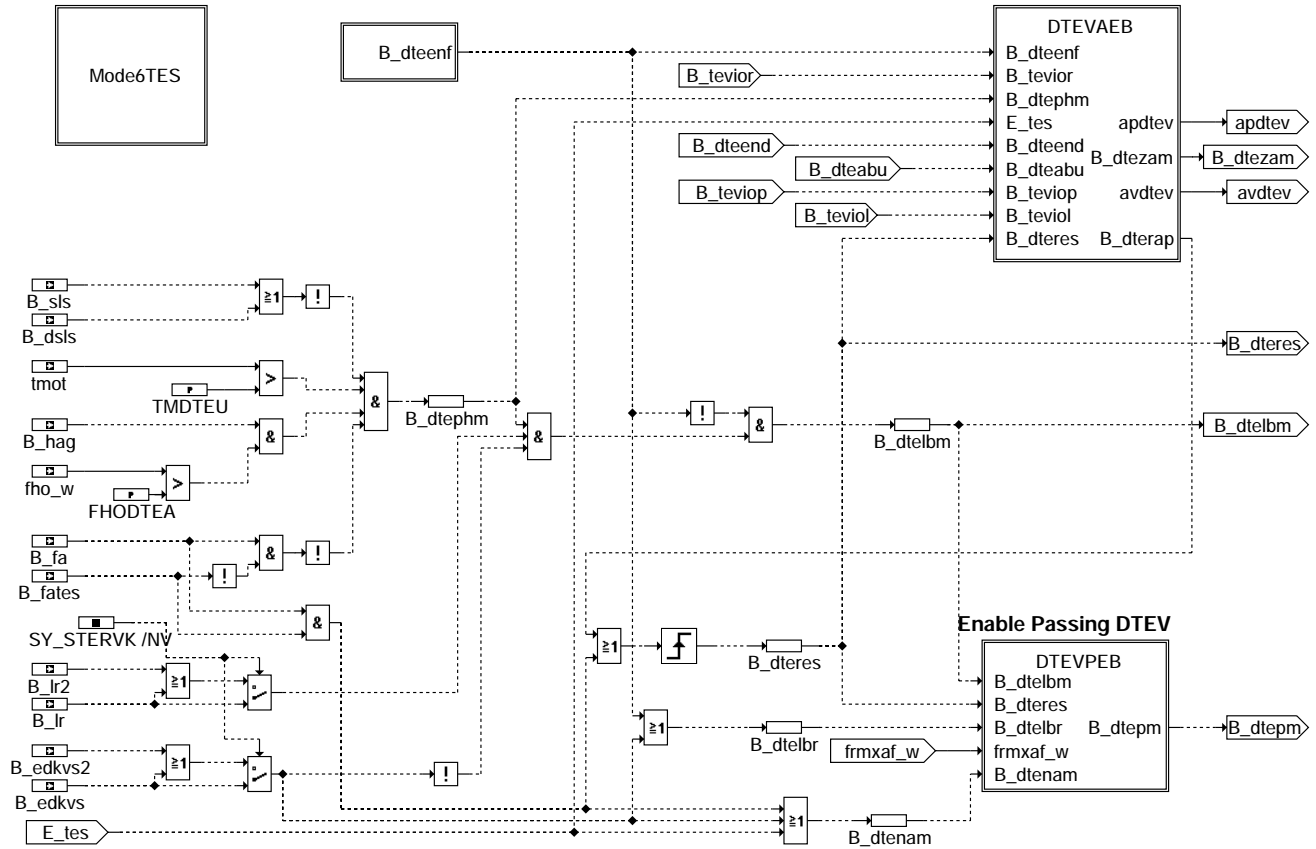
**Reading Errorflags**



**dtev-dtev-e**

**DTEVEB: Enable Conditions**

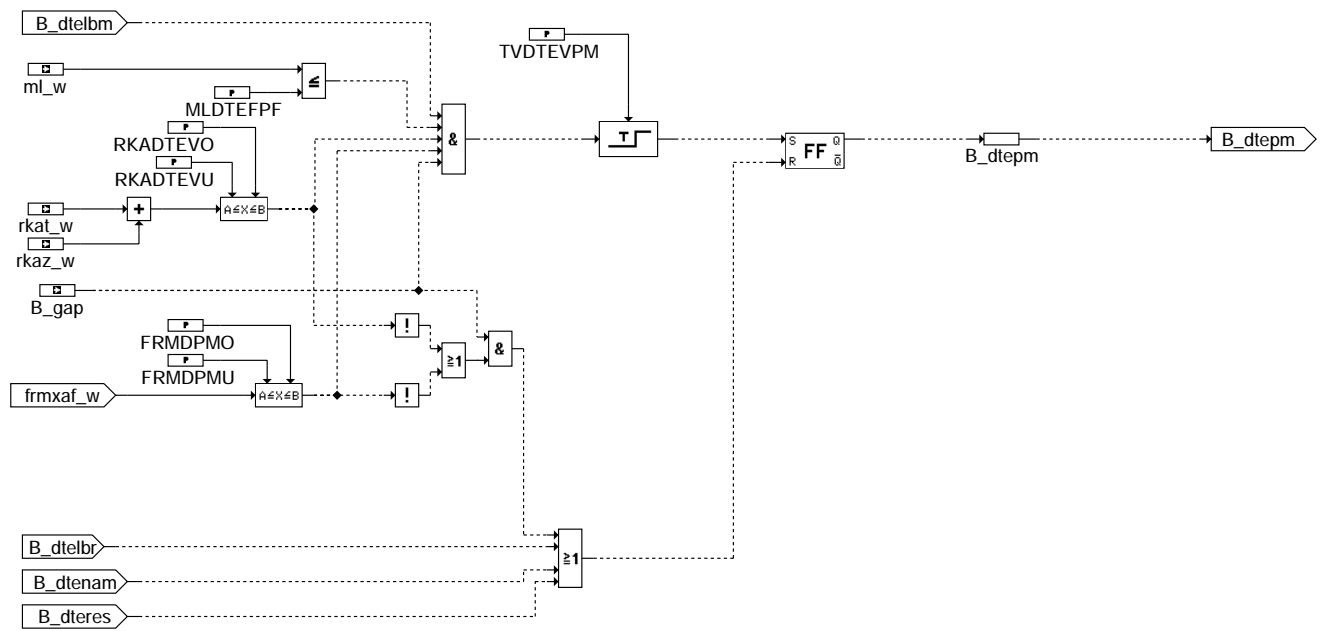
**Enable Active DTEV**



dtev-dteveb

DTEVPB: Enable Conditions of Passive Check

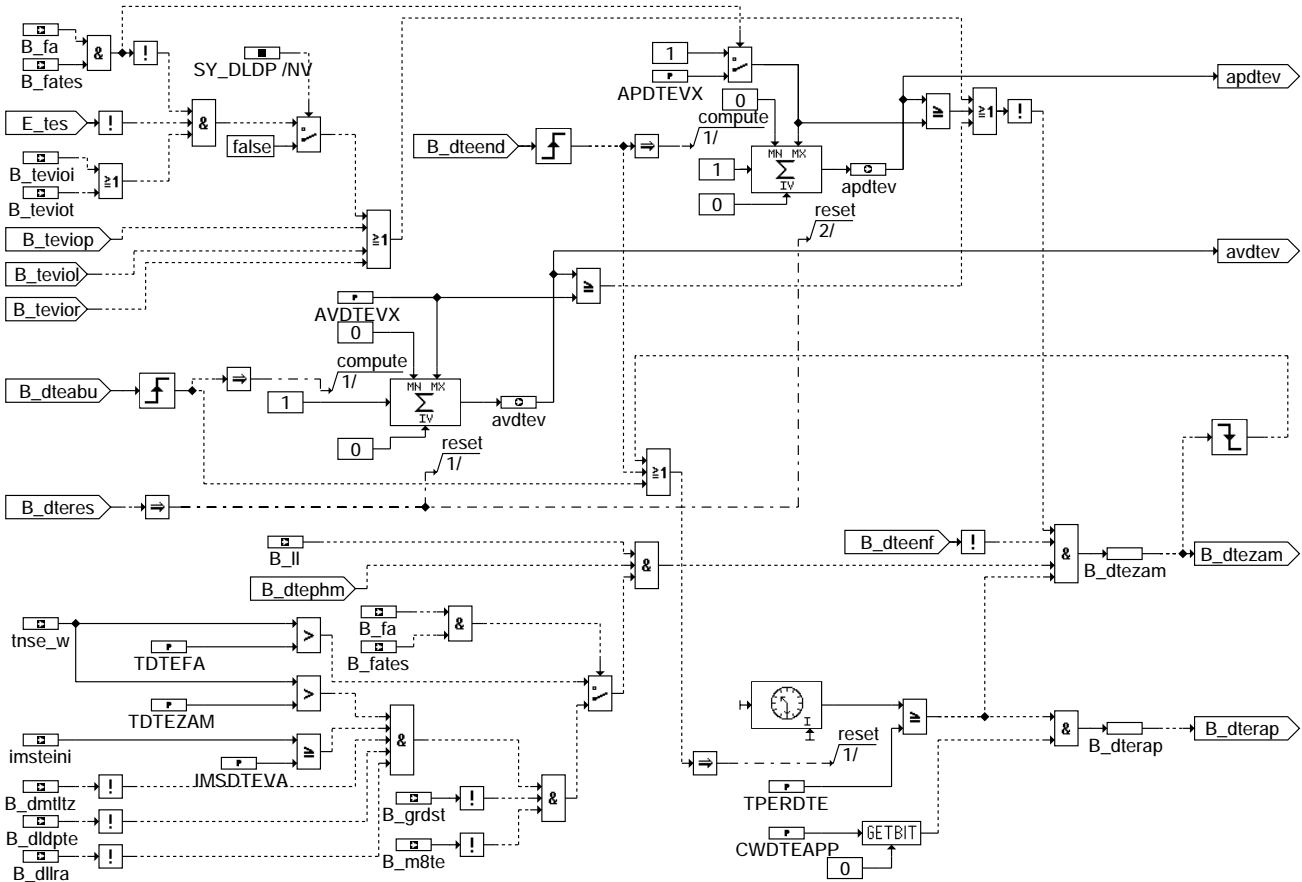
**DTEVPB: Enable Conditions of Passive Check**



dtev-dtevpb

DTEVAEB: Enable Conditions of Active Check

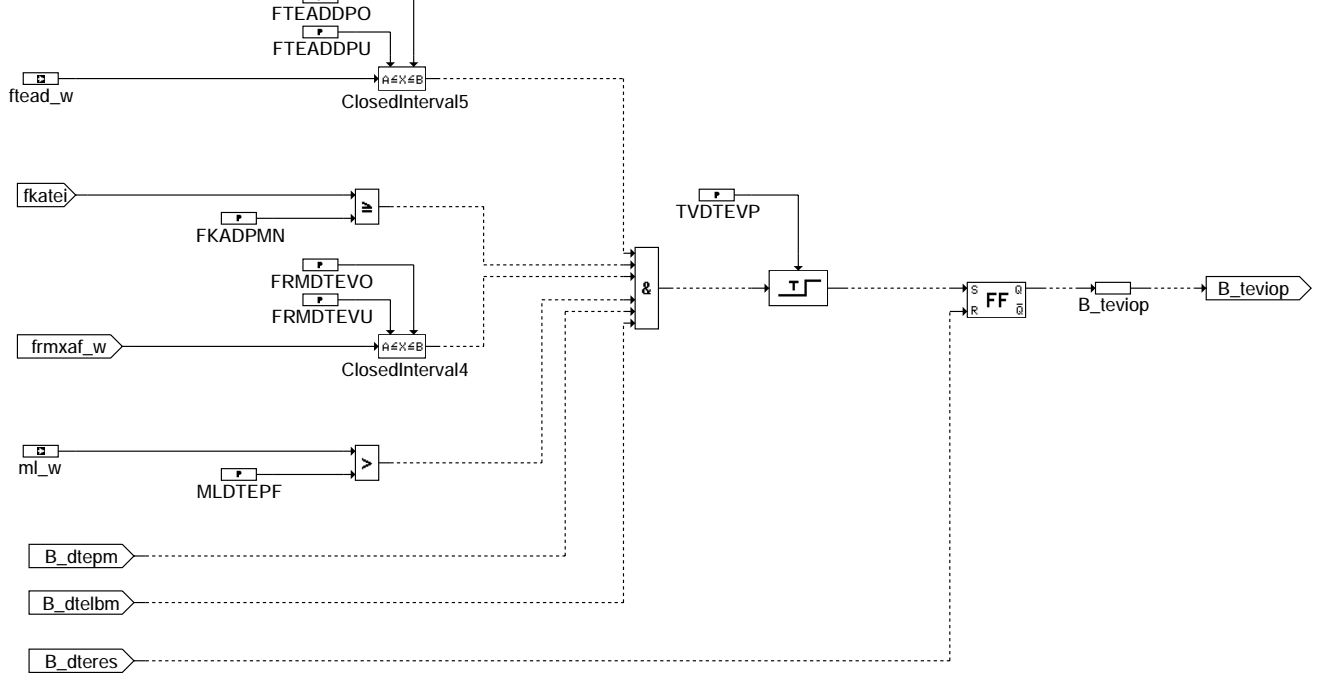
**DTEVAEB: Enable Condition of Active Check**



dtev-dtevaeb

DTEVP: Passive Check

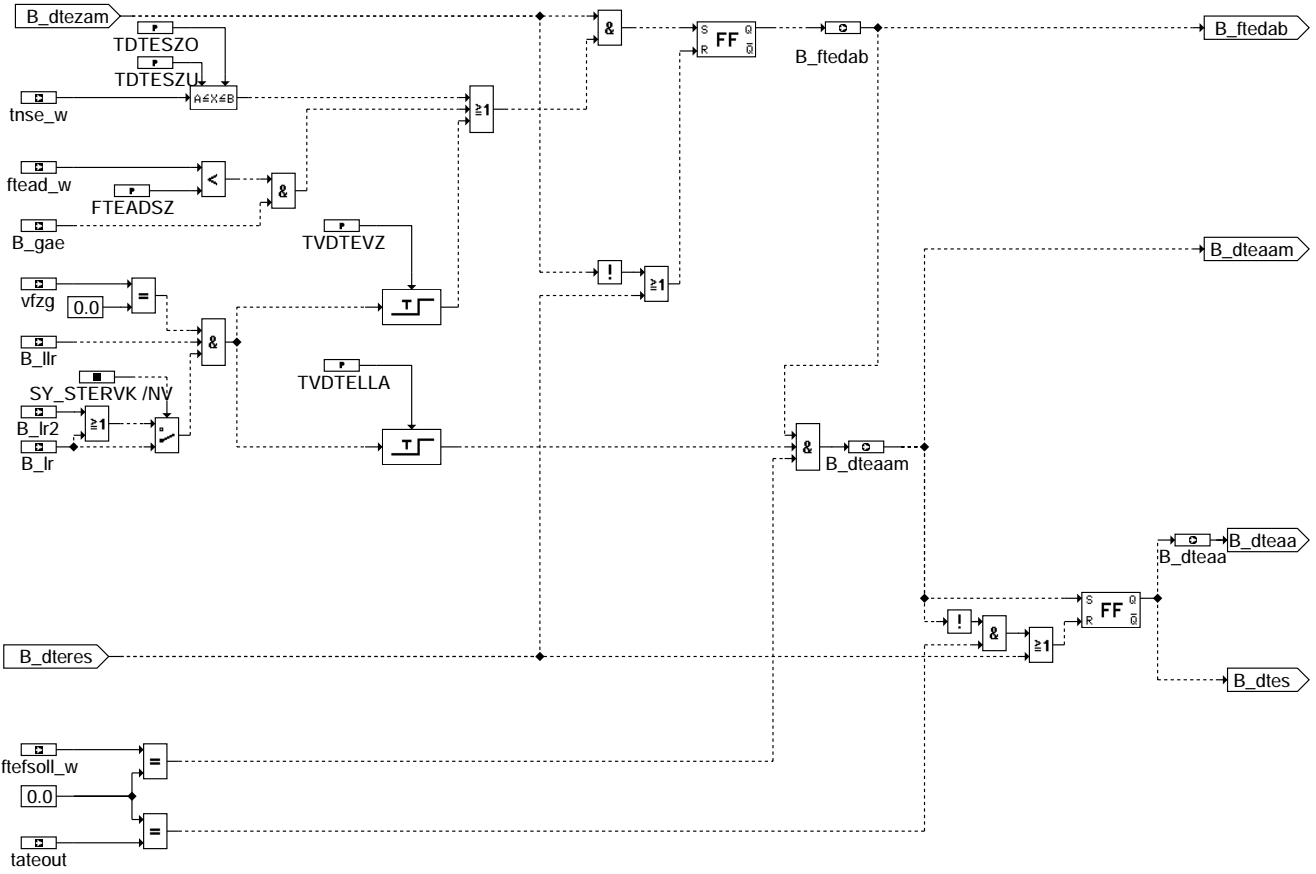
**DTEVP: Passive Check**



dtev-dtevp

DTEVZU: Closing the Canister Purge Valve (CPV)

### DTEVZU: Closing the Canister Purge Valve (CPV)



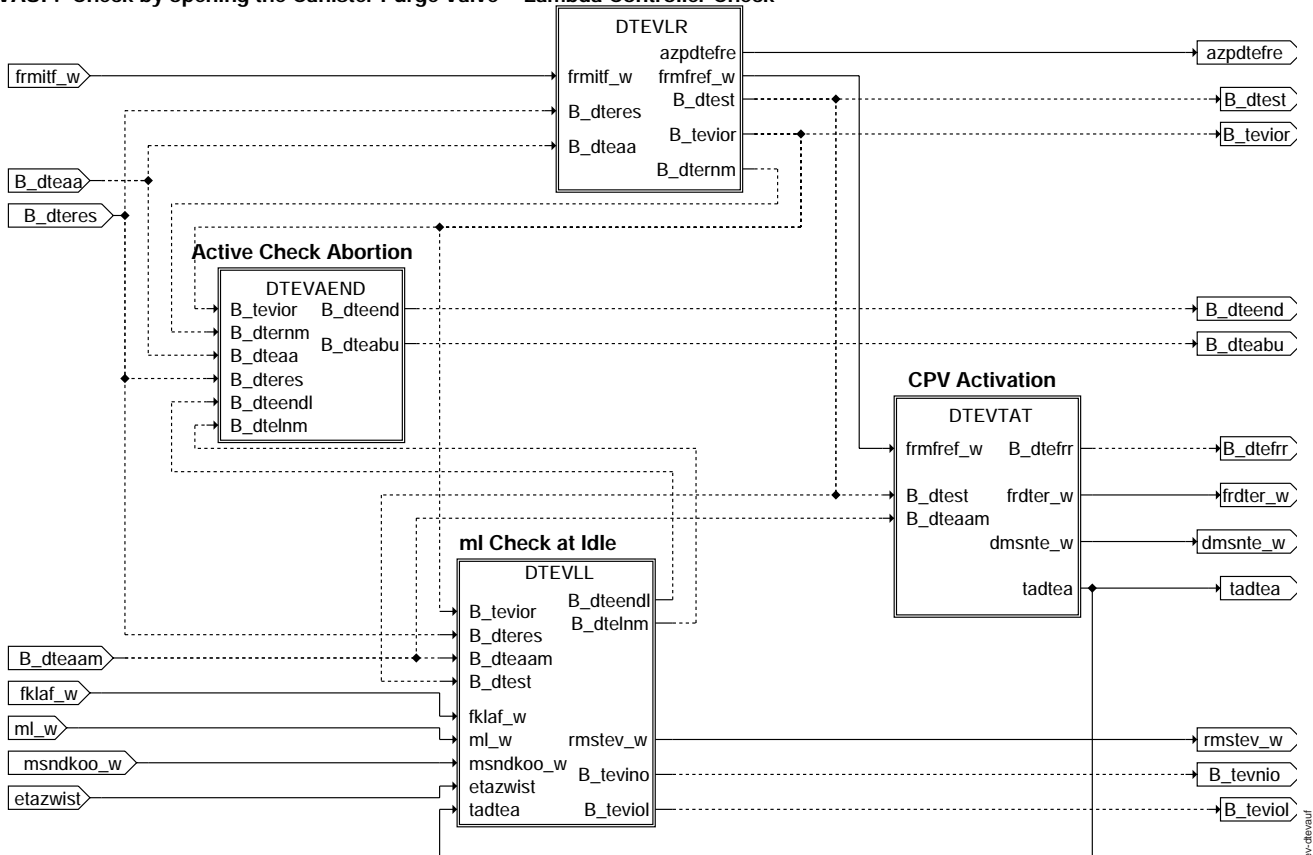
dteV-dteVZU

dteV-dteVZU



DTEVAUF: Check by opening the Canister Purge Valve

### DTEVAUF: Check by opening the Canister Purge Valve Lambda Controller Check



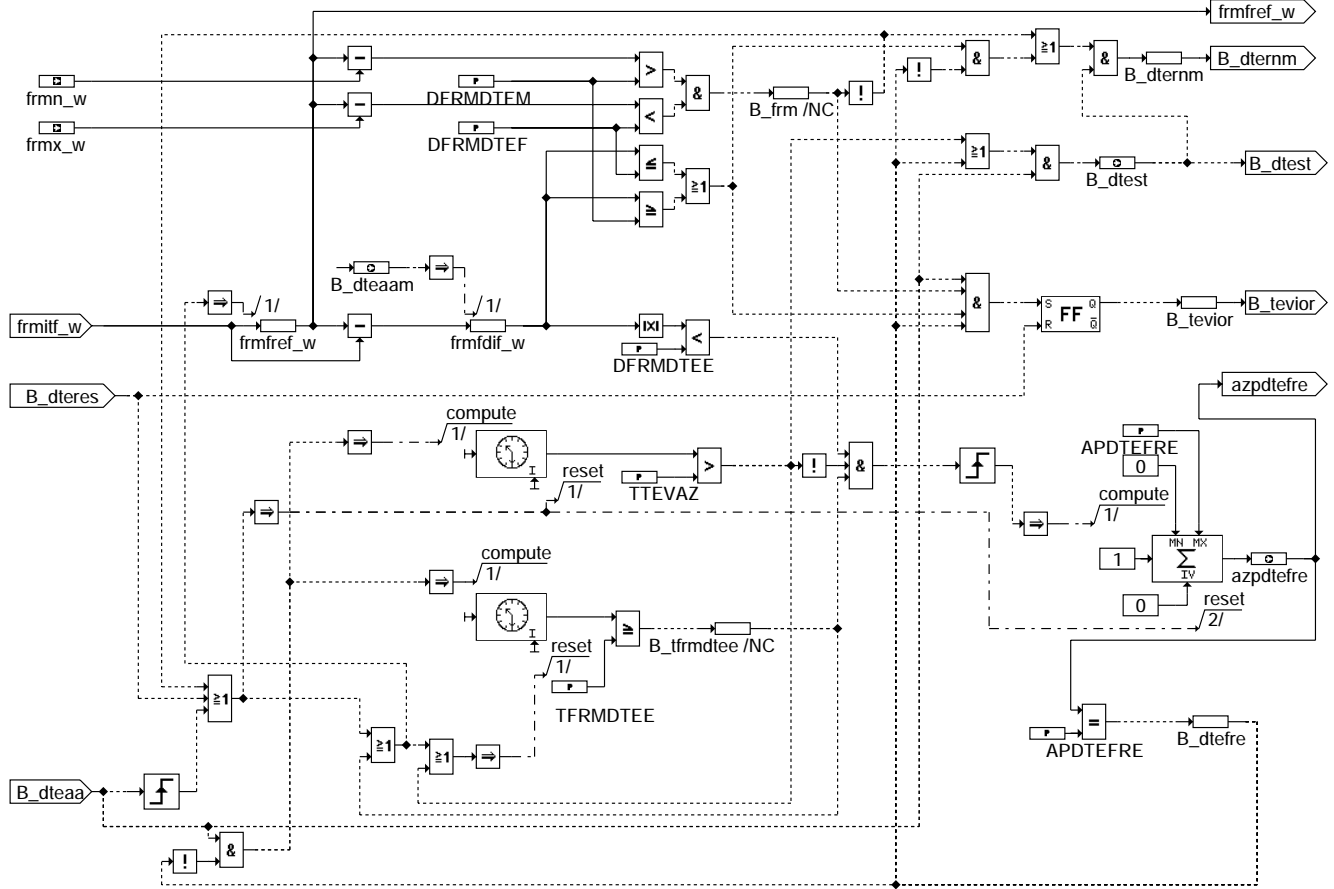
dtevd-dtevauf

dtevd-dtevauf



DTEVLR: Lambda Controller Check

### DTEVLR: Lambda Controller Check



dtev-dtevlr

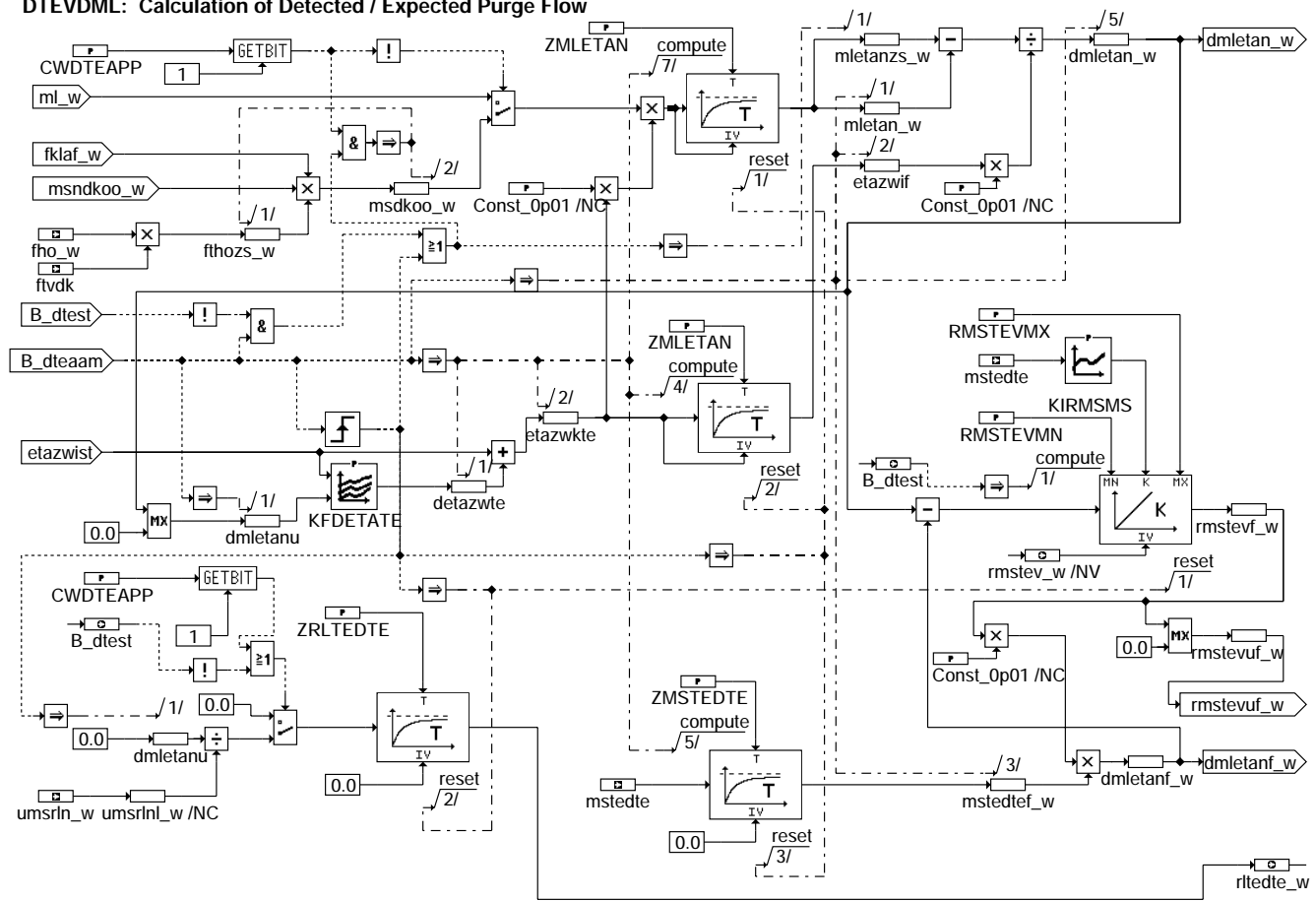
dtev-dtevlr





DTEVDML: Calculation of Detected / Expected Purge Flow

### DTEVDML: Calculation of Detected / Expected Purge Flow



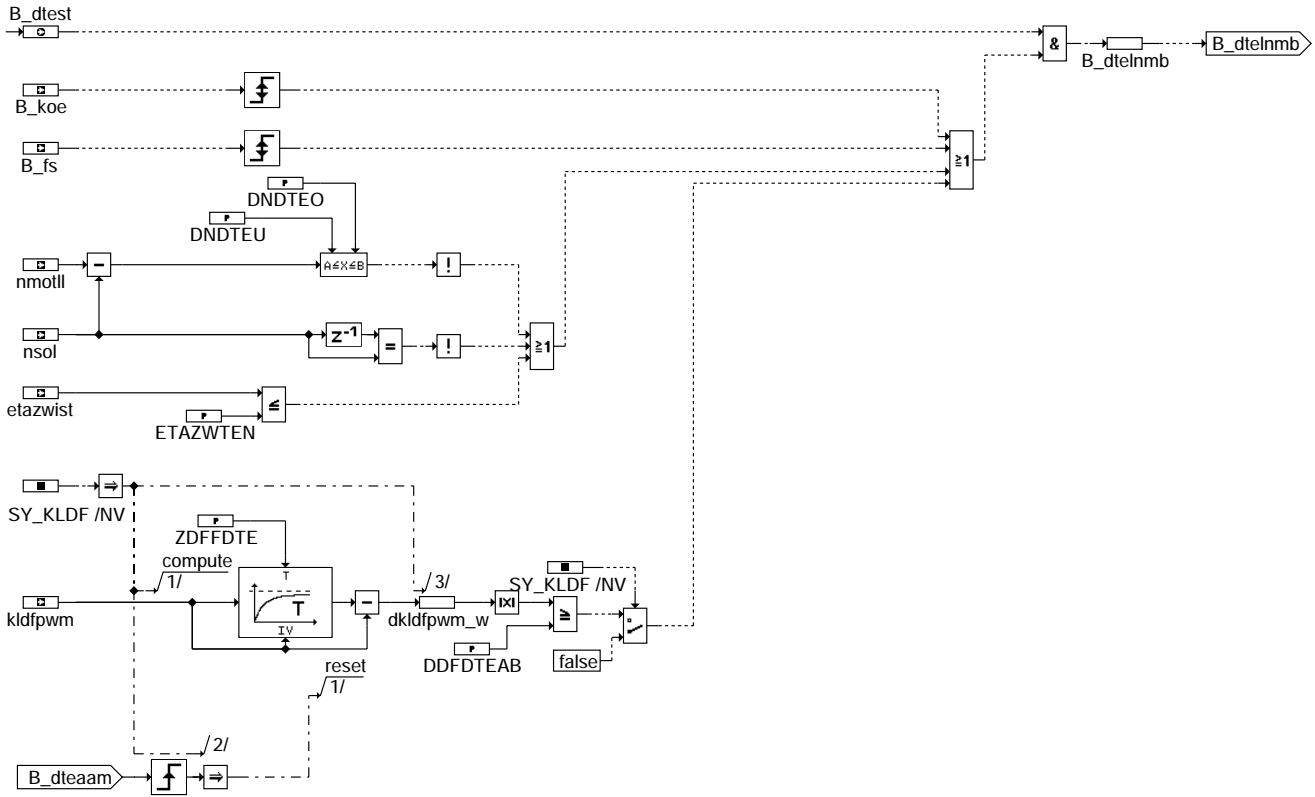
dtev-dtevdml

dtev-dtevdml



DTEVLAB : Bearing out of Abort

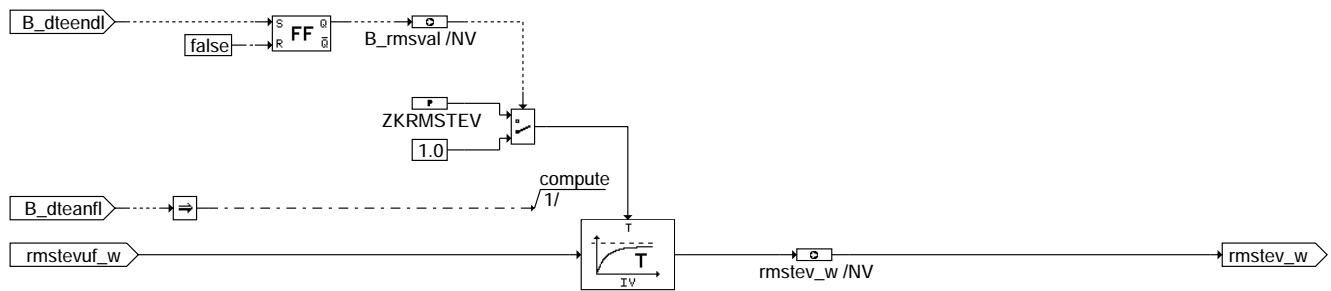
### DTEVLAB: bearing out of abort



### dtev-dtevlab

DTEVRQ: Quality value

### DTEVRQ: Quality Value

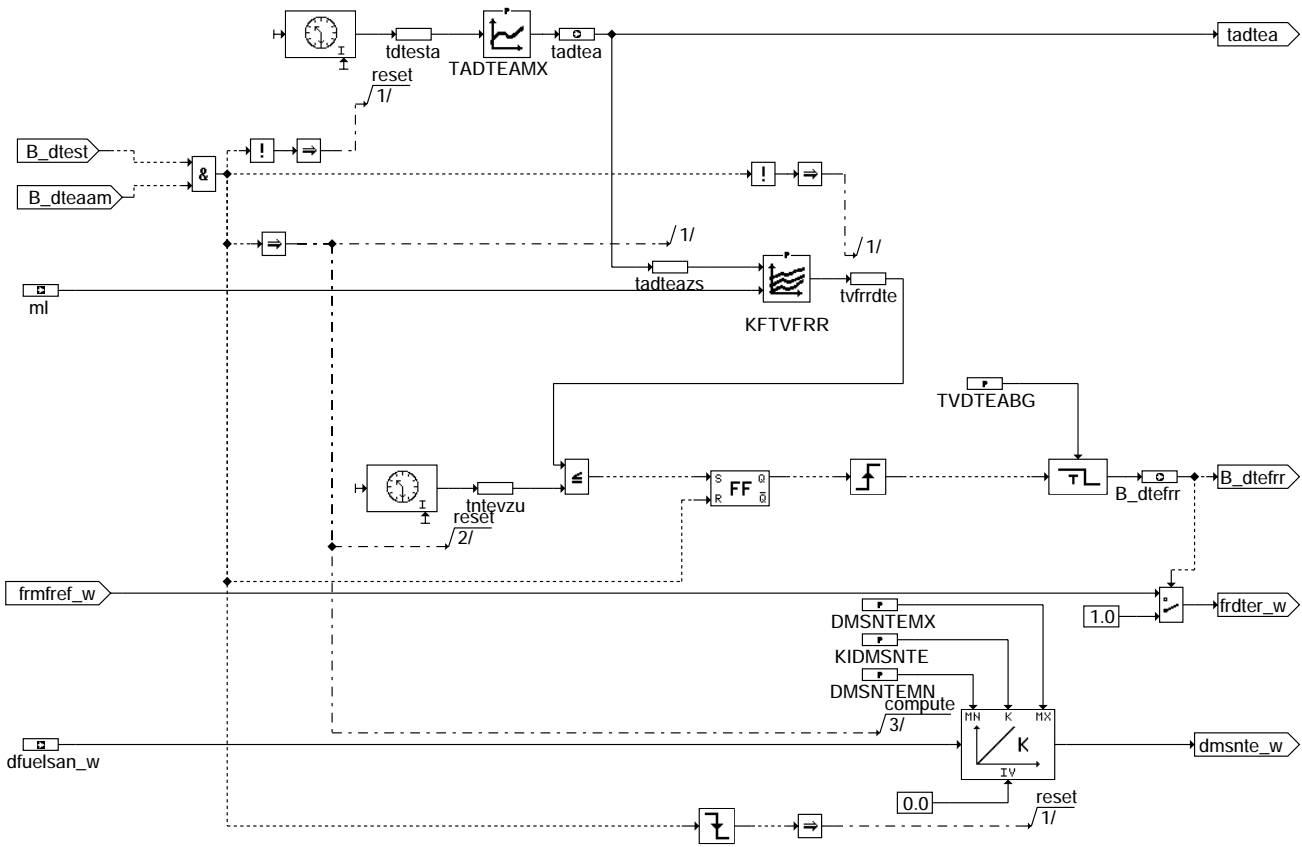


### dtev-dtevrq



DTEVTAT: Canister Purge Valve Activation, Lambda Controller Reset, Learning Purge Valve Air Flow for %BGMSZS

### DTEVTAT: Canister Purge Valve Activation, Lambda Controller Reset, Learning Purge Valve Air Flow for %BGMSZS

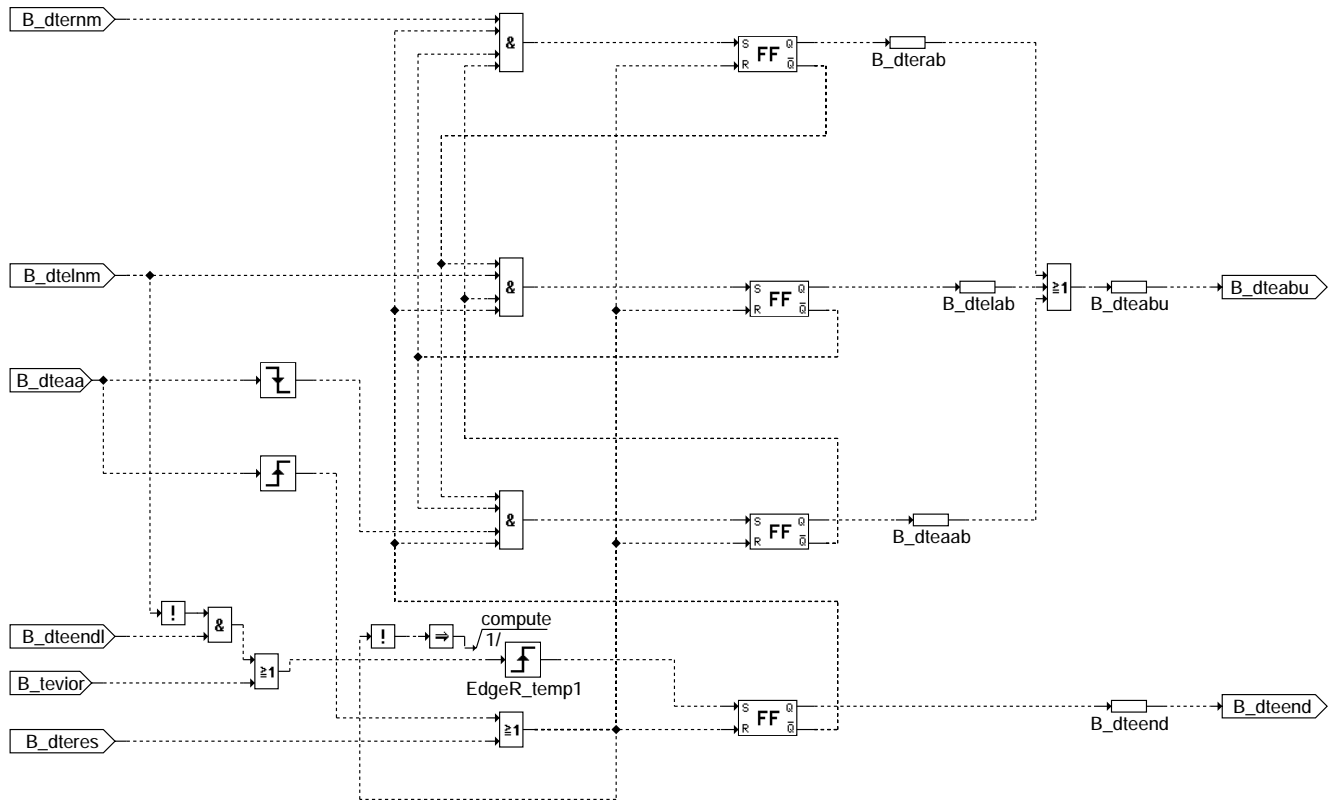


dtev-dtevtat

dtev-dtevtat

DTEVAEND: Active Check Abortion

### DTEVAEND: Active Check Abortion

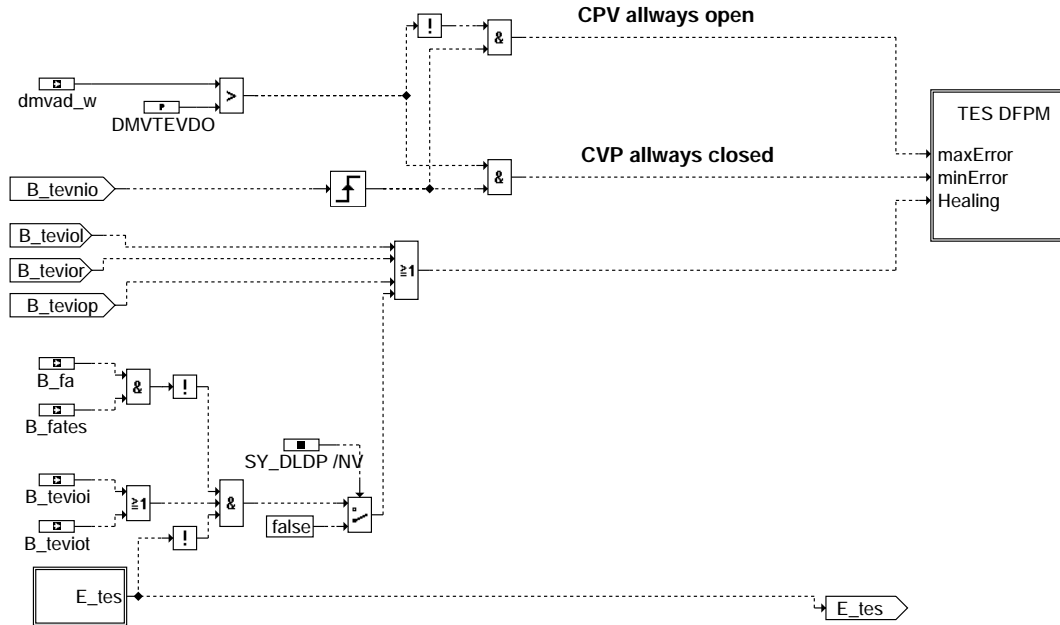


dtev-dtevaend

dtev-dtevaend

DTEVEA: Error Handling

**DTEVEA: Error Handling**



**Action Table for fault path \* in DFPM:**

	E_*	Z_*	B_mx*	B_mn*	B_si*	B_np*
maxError:	S	S	S	R	R	R
minError:	S	S	R	S	R	R
sigError:	S	S	R	R	S	R
nplError:	S	S	R	R	R	S
Healing:	R	S	R	R	R	R

S: set R: reset \* = tes

**dtev-dtevea**

In block diagrams fault type information as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the fault path xyz back into the central diagnostic management DFPM. The bits E-xyz, Z-xyz, B-mnxyz etc. are contents of this status word. For error and cycle flags of external fault paths which occur as inputs, access methods are available which read these information directly from the fault path status managed in the DFPM.

The following values are defined for the fault path of this diagnostic function:

Status fault path DTEV	sfptes
Error flag DTEV :	E_tes
Cycle flag DTEV :	Z_tes
Fault type DTEV :	TYP_tes :(B_mxtes, B_mntes, B_sites, B_nptes)
Clear fault path:	B_cltes
Default value active:	B_bktes (optional)
Fault path code DTEV:	CDTTES
Fault class DTEV:	CLATES
Fault severity DTEV:	TSFTES
CARB Code DTEV:	CDCTES
Table of ambient cond. DTEV:	FPTTES

Fault path entry with: LDTES; FLCTES; HLCTES; ULTES= nmot\_w; U2abc=ml\_w

**ABK DTEV 32.90 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
APDTEFRE			FW	number of tests to set flag fr stabilized for DTEV
APDTEVX			FW	maximum number of checks at detected fault
AVDTEVX			FW	maximum number of DTEV checks
CDCTES	BLOKNR		KL	code word CARB: canister purge system
CDKTES			FW	code word customer: canister purge system
CDTTES			FW	code word tester: canister purge system
CLATES			FW	fault class: evap system monitoring, PCV stuck open
CWDTEAPP			FW	Application code word for DTEV always active and swithing between HFM and P-sys.
DDFDTEAB			FW	Threshold for abort of diagnosis because change of generator signale is high
DFRMDTEE			FW	delta-frm-threshold for detection of successful mixture correction
DFRMDTEF			FW	delta Fr threshold 'rich correction' for check o.k.
DFRMDTEM			FW	delta Fr threshold 'lean correction' for check o.k.
DMLDTEFN			FW	Threshold air mass flow not plausible for detection fault in DTEV
DMLDTEFX			FW	Air mass threshold for detection PCV defective no longer necessary



Parameter	Source-X	Source-Y	Type	Description
DMLDTEMN			FW	Lower threshold for detection air mass flow not plausible for evaluation in DTEV
DMLDTEMX			FW	Upper threshold for detection air mass flow not plausible for evaluation in DTEV
DMSNTEMN			FW	Minimum standardized mass flow change PCV
DMSNTEMX			FW	Maximum standardized mass flow change PCV
DMVTEVDO			FW	Threshold loss adaptation to distinguish min, max faults in DTEV
DNDTEO			FW	upper Nsoll-Nist threshold for abortion diagnosis CPV
DNDTEU			FW	lower Nsoll-Nist threshold for abortion diagnosis CPV
ETAZWTEEN			FW	minimum threshold of ignition angle efficiency for diagnosis of PCV
FFTTES	BLOKNR		KL	freeze frame table: canister purge valve
FHODTEA			FW	lower altitude threshold for diagnosis CPV active
FKADPMN			FW	minimum fuel part via CPV for passive O.K. testing.
FRMDPMO			FW	upper frn threshold for passive switch on condition of diagnosis CPV
FRMDPMU			FW	lower frn threshold for passive switch on condition of diagnosis CPV
FRMDTEVO			FW	upper frn threshold for passive O.K. testing of diagnosis CPV
FRMDTEVU			FW	lower frn threshold for passive O.K. testing of diagnosis CPV
FTEADDP0			FW	upper load threshold for passive O.K. testing.
FTEADDP1			FW	lower load threshold for passive O.K. testing.
FTEADSZ			FW	threshold for immediate closing of CPV from DTEV
IMSDTEVA			FW	threshold for integral of purge mass flow after a long purge stop
KFDETEATE	ETAZWIST	DMLETANU	KF	correction of ignition angle effectiveness for diagnosis of PCV
KFTVFRR	TADTEAZS	ML	KF	Map: Lambda control after this time reset at reference value
KIDMSNTE			FW	Integration speed for the calculation of the mass flow change PCV
KIRMSMS	MSTEDTE		KL	Integration speed matching of mass flow PCV with calculated mass flow
MLDTEFFP			FW	threshold ml for possible Check passive diagnosis DTEV possible
MLDTEFP			FW	threshold ml for possible Check passive diagnosis DTEV
RKADTEVO			FW	upper rka threshold for passive switch on condition of diagnosis CPV
RKADTEVU			FW	lower rka threshold for passive switch on condition of diagnosis CPV
RMSTEVI0			FW	Threshold relative mass flow for O.K. detection
RMSTEVMN			FW	Minimum value relative mass flow PCV
RMSTEVMX			FW	Maximum value relative mass flow PCV
SY_CONFSL			SYS (REF)	System constant: secondary air present vorhanden
SY_DLDP			SYS	SY_DLDP = 1 there ist a DLDP in system
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_KLDF			SYS	system constant for generator DF-signale
SY_NWS			SYS (REF)	system constant camshaft control: none, 2 point, continuous
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
TADTEAMX	TDTESTA		KL	characteristic line for max. duty cycle = F(integral purge flow after TE-Stop)
TADTEMX			FW	duty cycle threshold for active testing
TC6TECI			FW	mode 6 code word for O.K. check of CPV form DLDP
TC6TECL			FW	mode 6 code word for O.K. check of CPV from air-test
TC6TECNL			FW	mode 6 code word for NOT O.K. check of CPV from air-test
TC6TECP			FW	mode 6 code word for passive O.K. check of CPV
TC6TECRF			FW	mode 6 code word for O.K. check of CPV from FR-deviation direction rich
TC6TECRM			FW	mode 6 code word for O.K. check of CPV from FR-deviation direction lean
TC6TECT			FW	mode 6 code word for O.K. check of CPV form DLDP
TDTEFA			FW	Time for blocking of DTEV as of start with tester request
TDTESZO			FW	time after start for desactivation fast purge rate decrease DTEV at B_JI= TRUE
TDTESZU			FW	time after start for activation purge rate decrease DTEV at B_JI= TRUE
TDTEZAM			FW	time after engine start for possible activation of active DTEV
TFRMDTEE			FW	monitoring duration frn
TMDTEU			FW	lowest engine temperature threshold for diagnose
TPERDTE			FW	time for repeating DTEV at non stop idle
TSFTES			FW	fault active time: canister purge system
TTEVAZ			FW	duration of stay for CPV opening with not successful frn
TVDTEABG			FW	delay time between engine and Lambda- sensor
TVDTEB			FW	delay time for statement TEV o.k./defect in diagnosis DTEV
TVDTEE			FW	Duration as of PCV open for checking of DTEV
TVDTELLA			FW	min. time for activation conditions DTEV at idle fulfilled
TVDTEVP			FW	delay time for setting of the flip flop "Passive Diagnosis CPV o.k."
TVDTEVPM			FW	delay time for setting of the flip flop "Diagnosis passive possible"
TVDTEVZ			FW	delay time for closing CPV for active DTEV
ZDFFDTE			FW	Time constant for highpas filter of generator signale
ZFRMFIL			FW	filter timeconstant for lambda controller
ZFRMXAF			FW	filter time constant for frmx_a_w signal
ZKRMSTEV			FW	time constant low pass filter for mode 6 DTEV
ZMLETAN			FW	Time cons. for filtering for the calc. of the energy needed for idling for DTEV
ZMSTEDTE			FW	Time constant for filtering of the calculated mass flow PCV
ZRLTEDTE			FW	Time constant for filtering of the calculated charge PCV

Variable	Source	Type	Description
APDTEV	DTEV	AUS	Number of DTEV Tests with success
AVDTEV	DTEV	AUS	Number of DTEV Tests without success
AZPDTEFRE	DTEV	AUS	number of tests for lambda controller stabilized
BLOKNR		EIN	DAMOS source for block number
B_BETES	DTEV	AUS	condition leak detection request
B_BKTES	DTEV	AUS	condition backup value evap system monitoring, PCV stuck open
B_CDTES	PROKON	EIN	function active per codeword CDTES
B_CLTES		EIN	condition: clear error "evaporation control system open"
B_DLDPTE	GKRA	EIN	request from evap system monitoring to shut down PCV
B_DLLRA	DLLR	EIN	Condition DLLR request
B_DMLTZ		EIN	Condition TEV should be closed



Variable	Source	Type	Description
B_DSLS		EIN	condition for active diagnosis of secondary air system
B_DTEAA	DTEV	AUS	Condition diagnosis CPV by opening the CPV active
B_DTEAAB	DTEV	LOK	condition DTEV abortion because of activation conditions no more fulfilled
B_DTEAAM	DTEV	AUS	Condition diagnosis CPV by opening the CPV active possible
B_DTEABU	DTEV	LOK	Condition interruption of TE diagnosis without result
B_DTEANFL	DTEV	LOK	terminated time from this the CPV duty-cycle over threshold
B_DTEEND	DTEV	LOK	Condition TEV check was successful
B_DTEENDL	DTEV	LOK	Condition TEV check was successful by idle speed air check
B_DTEENF	DTEV	LOK	Condition CPV diagnosis not allowed because of an error of the system
B_DTEFRE	DTEV	LOK	Condition fr for diagnosis CPV stabilized.
B_DTEFRR	DTEV	AUS	condition of lambda controller reset
B_DTELAB	DTEV	LOK	condition DTEV abortion because of destorption idle speed air check
B_DTELBM	DTEV	LOK	Condition detection of Lambda controller possible for diagnosis CPV
B_DTELBR	DTEV	LOK	condition reset of flip flop "Passive DTEV" possible
B_DTELNM	DTEV	LOK	Condition diagnosis CPV not possible
B_DTELNMB	DTEV	LOK	bear out : Condition diagnosis CPV not possible
B_DTELNMV	DTEV	LOK	Reservation: Condition diagnosis CPV not possible
B_DTENAM	DTEV	LOK	Condition diagnosis CPV only possible by opening the CPV
B_DTEPHM	DTEV	LOK	condition physical enable of DTEV
B_DTEPM	DTEV	LOK	Condition passive CPV diagnosis possible
B_DTERAB	DTEV	LOK	condition DTEV abortion because of too much fr deviation
B_DTERAP	DTEV	LOK	condition DTEV reset by application
B_DTERES	DTEV	LOK	Condition reset for CPV diagnosis
B_DTERNM	DTEV	LOK	Condition no fr-lift for diagnosis CPV available
B_DTES	DTEV	AUS	Condition for active diagnosis of canister purge system
B_DTEST	DTEV	AUS	condition for start of TEV opening
B_DTEZAM	DTEV	LOK	Condition Diagnosis CPV is released for active test (CPV - close/open)
B_EDKVS	DKVS	EIN	condition for adaption fault thresholds momentarily exceeded
B_EDKVS2	DKVS	EIN	condition for adaption fault thresholds bank 2 momentarily exceeded
B_ELLS		EIN	Condition: error idle speed actuator
B_ENWS	DNWS	EIN	condition error camshaft control
B_FA		EIN	condition general function request
B_FATES		EIN	condition leak detection request
B_FS	BBGANG	EIN	Condition driving state (automatic gear box)
B_FTEDAB	DTEV	AUS	Condition decrease purge rate for diagnosis CPV
B_FTTES	DTEV	AUS	Condition fault entry by tester for TEV
B_GAE	DKVS	EIN	condition for adaptive Lambda pilot control successful
B_GAP	GKEB	EIN	condition mixture adaptation phase active
B_GRDST		EIN	condition basic attitude
B_HAG	BGPU	EIN	condition altitude adaptation valid
B_KOE	KOS	EIN	Condition for AC-compressor ON
B_LDPI		EIN	condition reed contact leakage diagnosis pump
B_LL	MSF	EIN	Condition idle
B_LLR	LLRBB	EIN	condition idle speed control
B_LR	LREB	EIN	LREB: condition for Lambda closed loop control upstream catalyst; bank 1
B_LR2	LREB	EIN	LREB: condition for lambda closed loop control upstream catalyst; bank 2
B_M8TE	TC8MOD	EIN	condition to enable function evap system by SAE J1879 Mode 8 TID \$01
B_MDARV	DMDMIL	EIN	critical misfire rate detected
B_MNTES	DTEV	AUS	condition for fault type "minimum value" detected
B_MXTES	DTEV	AUS	condition for fault type "maximum value" detected (tank vent valve)
B_NLDG		EIN	condition limp-home function speed sensor
B_NPTES	DTEV	AUS	condition for fault type "unplausible signal" detected (PCV stuck open)
B_NSWO1	PROKON	EIN	condition engine speed > NSWO1
B_PWF		EIN	Condition for powerfail
B_RMSVAL	DTEV	AUS	Condition relative mass flow PCV valid
B_SITES	DTEV	AUS	error type: PCV stuck open
B_SLS	AK	EIN	Condition for active secondary air
B_TEVIOI		EIN	Condition CPV detected as o.k. by DLDP check (initial purge)
B_TEVIOL	DTEV	LOK	Condition CPV detected o.k. from idle speed control
B_TEVIOLM	DTEV	LOK	condition CPV o.k. test by idle speed air consumption possible
B_TEVIOP	DTEV	LOK	Condition CPV in passive test detected as o.k.
B_TEVIOR	DTEV	LOK	Condition CPV from fr-deviation detected as o.k.
B_TEVIOT		EIN	Condition CPV detected as o.k. by DLDP check (increase of period)
B_TEVNIO	DTEV	LOK	Condition CPV in active test detected as defect
B_TEVNIOIOM	DTEV	LOK	condition CPV o.k. test by idke speed air consumption not possible
DETAZWTE	DTEV	LOK	correction factor of ignition angle effectiveness for diagnosis of PCV
DFP_AAVE	DTEV	DOK	ECU int. fault path no.: diagnosis AAVE valve power stage
DFP_AGRE	DTEV	DOK	ECU int. fault path no.: EKR power stage
DFP_AGRF	DTEV	DOK	ECU int. fault path no.: partial pressure EGR
DFP_DK	DTEV	DOK	ECU int. fault path no.: clear error throttle potentiometer
DFP_DVEU	DTEV	DOK	ECU-internal fault-path no.: DV-E failure during UMA learning
DFP_LDPE	DTEV	DOK	ECU int. fault path no.: leakage detection pump power stage
DFP_LLR	DTEV	DOK	ECU int. fault path no.: idle speed control
DFP_LM	DTEV	DOK	ECU-internal fault path no.: main-load sensor
DFP_SLS	DTEV	DOK	Internal fault path number: secondary air-system
DFP_TES	DTEV	DOK	Internal error path number evap system monitoring, pcv Struck open
DFP_TEVE	DTEV	DOK	Internal fault path number: canister purge valve power stage
DFP_TM	DTEV	DOK	Internal fault path number: engine temperature
DFP_JUB	DTEV	DOK	Internal fault path number: ambient conditions
DFP_VFZ	DTEV	DOK	ECU int. fault path no.: vehicle speed signal
DFUELSAN_W	BGMSZS	EIN	Delta charge sensor to alpha/n-systems
DKLDFPWM_W	DTEV	LOK	variation of generator signale as PWM-signale



Variable	Source	Type	Description
DMLETANF_W	DTEV	LOK	Filtered value for deviation energy needed for idling during DTEV
DMLETANU	DTEV	LOK	Delta: airflow * ignition efficiency at DTEV unsigned
DMLETAN_W	DTEV	LOK	Delta: airflow * ignition efficiency at DTEV 16 bit
DMSNTE_W	DTEV	AUS	Standardized mass flow change through PCV
DMVAD_W	MDVERAD	EIN	Delta resistant torque from resistant torque adaptation
ETAZWIF	DTEV	LOK	value of ignition efficiency: filtered value for DTEV
ETAZWIST	MDIST	EIN	actual ignition angle effectiveness
ETAZWKTE	DTEV	LOK	correction ignition angle effectiveness for diagnosis of PCV
E_AAVE		EIN	error flag: canister ventilation valve (power stage)
E_AGRE		EIN	error flag: EGR power stage monitoring
E_AGRF		EIN	error flag: EGR flow monitoring
E_DK	DDVE	EIN	Error flag: throttle position sensor
E_DVEU	DDVE	EIN	Error flag: DV-E cause of failure: UMA-learning
E_LDPE		EIN	error flag: leakage detection pump power stage
E_LLR	DLLR	EIN	Error flag: idle speed control
E_LM	EGFE	EIN	Error flag: main load sensor
E_SLS		EIN	error flag: secondary air system
E_TES	DTEV	AUS	error flag: canister purge system diagnosis
E_TEVE	DTEVE	EIN	error flag: canister purge valve power stage
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
E_UB	GGUB	EIN	error flag: power supply voltage UB
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
FHO_W	BGPU	EIN	correction factor: altitude
FKATEI	TEB	EIN	factor fuel part purge control (actual value)
FKLAF_W	BGMSZS	EIN	Factor saint venant (KLAF)
FRDTER_W	DTEV	AUS	lambda control factor as reference value for CPV diagnosis
FRMFDIF_W	DTEV	LOK	difference value between trail value and momentary value
FRMFREF_W	DTEV	LOK	filtered reference value of fr for DTEV active check
FRMITF_W	DTEV	LOK	filtered value of fr for DTEV
FRMIT_W	TEB	EIN	mean value of fr and fr2 (16 bit)
FRMN_W	LR	EIN	lambda regulator output min.
FRMXAF_W	DTEV	LOK	fr value (out of fr or fr2) which is the farrest away from 1 (filtered)
FRMXA_W	TEB	EIN	fr value (out of fr and fr2) wich is the farrest away from 1 (16bit)
FRMX_W	LR	EIN	LR with integrator stop:Maximum limit. of integrator fr;FRMAX increased by DSL8
FTEAD_W	TEB	EIN	charcoal canister charge
FTEFSOLL_W		EIN	desired canister purge rate
FTHOZS_W	DTEV	LOK	factor temperature and altitude depending correction of mass flow
FTVDK	SWADAP	EIN	correction factor for temperature upstream of throttle valve
IMSTEINI		EIN	integral of purge mass flow after a longer purge stop
KLDFPWM		EIN	generator signale as PWM-signale filtrated
ML	SWADAP	EIN	air mass flow
MLETANZS_W	DTEV	LOK	safed value: at ignition efficiency = 100% normalised air amount
MLETAN_W	DTEV	LOK	At ignition efficiency = 100% normalised air amount
ML_W	EGFE	EIN	air mass flow filtered (Word)
MSDKOO_W	DTEV	LOK	Mass flow throttle valve without offset
MSNDKOO_W	BGMSZS	EIN	Normalized mass flow over throttle without offset (word)
MSTEDTE	BGTEV	EIN	purge mass flow for DTEV
MSTEDTEF_W	DTEV	LOK	purge massflow für DTEV (filtered value)
NMOTLL	BGNMOT	EIN	engine speed
NSOL	LLRNS	EIN	idle reference speed
RKAT_W	LRA	EIN	additive correction (per time) of the mixture adaptation (Word)
RKAZ_W	LRA	EIN	additive correction (per ignition) of the mixture adaptation
RLTEDTE_W	DTEV	AUS	from DTEV calculated relative charge through the purge control valve
RMSTEVF_W	DTEV	LOK	Current measured value for relative PCV quality
RMSTEVUF_W	DTEV	LOK	Current, unsigned measured value for relative PCV quality
RMSTEV_W	DTEV	AUS	Long-time stored measured value for value of relative PCV quality
SFPTES	DTEV	AUS	status fault path: evap system monitoring, PCV defective open
SY_AAV	DTEV	DOK	system constant condition : shut-off-valve available
TADTEA	DTEV	AUS	TEV duty cycle from canister purge diagnosis
TADTEAZS	DTEV	LOK	last duty cycle value from canister purge diagnosis
TATEOUT	ATEV	EIN	output duty cycle for canister purge valve
TC6TESC	DTEV	AUS	Output code SCAN tool mode 6 from purge control diagnosis
TC6TESS	DTEV	AUS	Output threshold SCAN tool mode 6 from purge control diagnosis
TC6TESW	DTEV	AUS	Output check value SCAN tool mode 6 from purge control diagnosis
TDTESTA	DTEV	LOK	time for DTEV check by CPV opening active
TDTETEVO	DTEV	LOK	time for CPV duty-cyle over threshold
TISPLDPX_W		EIN	Threshold for time for initial purging until LDP switch switches
TISPLDP_W		EIN	time for initial purging until LDP switch switches
TMOT	SWADAP	EIN	Engine temperature
TNSE_W	BBSTT	EIN	time counter at end of start (16 bit)
TNTEVZU	DTEV	LOK	time after PCV closing
TPLDPTCX_W		EIN	threshold time until LDP switch switches if CVP is open
TPLDPTC_W		EIN	time until LDP switch switches if CVP is open
TVFRDTE	DTEV	LOK	delay time for Lambda controll reset after PCV closing
UMSRLN_W	BGMSZS	EIN	calculation factor load to mass flow
VFZG	SWADAP	EIN	vehicle speed (km/h)
Z_TES	DTEV	AUS	cycle flag of canister purge system



## FW DTEV 32.90 Fixed Values

Parameter	Value	Description
APDTEFRE		number of tests to set flag fr stabilized for DTEV
APDTEVX		maximum number of checks at detected fault
AVDTEVX		maximum number of DTEV checks
CDKTES		code word customer: canister purge system
CDTTES		code word tester: canister purge system
CLATES		fault class: evap system monitoring, PCV stuck open
CWDTEAPP		Application code word for DTEV always active and swiching between HFM and P-sys.
DDFDTEAB		Threshold for abort of diagnosis because change of generator signale is high
DFRMDTEE		delta-frm-threshold for detection of successful mixture correction
DFRMDTEF		delta Fr threshold 'rich correction' for check o.k.
DFRMDTEM		delta Fr threshold 'lean correction' for check o.k.
DMLDTEFN		Threshold air mass flow not plausible for detection fault in DTEV
DMLDTEFX		Air mass threshold for detection PCV defective no longer necessary
DMLDTEMN		Lower threshold for detection air mass flow not plausible for evaluation in DTEV
DMLDTEMX		Upper threshold for detection air mass flow not plausible for evaluation in DTEV
DMSNTEMN		Minimum standardized mass flow change PCV
DMSNTEMX		Maximum standardized mass flow change PCV
DMVTEVDO		Threshold loss adaptation to distinguish min. max faults in DTEV
DNDTEO		upper Nsoll-Nist threshold for abortion diagnosis CPV
DNDTEU		lower Nsoll-Nist threshold for abortion diagnosis CPV
ETAZWTEEN		minimum threschold of ignition angle efficiency for diagnosis of PCV
FHODTEA		lower altitude threshold for diagnosis CPV active
FKADPMN		minimum feul part via CPV for passive O.K. testing.
FRMDPMO		upper frm threshold for passive switch on condition of diagnosis CPV
FRMDPMU		lower frm threshold for passive switch on condition of diagnosis CPV
FRMDTEVO		upper frm threshold for passive O.K. testing of diagnosis CPV
FRMDTEVU		lower frm threshold for passive O.K. testing of diagnosis CPV
FTEADDPO		upper load threshold for passive O.K. testing.
FTEADDPU		lower load threshold for passive O.K. testing.
FTEADSZ		threshold for immediate closing of CPV from DTEV
IMSDTEVA		thershold for integral of purge mass flow after a long purge stop
KIDMSNTE		Integration speed for the calculation of the mass flow change PCV
MLDTEFPF		threshold ml for possible Check passive diagnosis DTEV possible
MLDTEPF		threshold ml for possible Check passive diagnosis DTEV
RKADTEVO		upper rka threshold for passive switch on condition of diagnosis CPV
RKADTEVU		lower rka threshold for passive switch on condition of diagnosis CPV
RMSTEVIO		Threshold relative mass flow for O.K. detection
RMSTEVMN		Minimum value relative mass flow PCV
RMSTEVMX		Maximum value relative mass flow PCV
TADTEMX		duty cycle threshold for active testing
TC6TECI		mode 6 code word for O.K. check of CPV form DLDP
TC6TECL		mode 6 code word for O.K. check of CPV from air-test
TC6TECNL		mode 6 code word for NOT O.K. check of CPV from air-test
TC6TECP		mode 6 code word for passive O.K. check of CPV
TC6TECRF		mode 6 code word for O.K. check of CPV from FR-deviation dircetion rich
TC6TECRM		mode 6 code word for O.K. check of CPV from FR-deviation dircetion lean
TC6TECT		mode 6 code word for O.K. check of CPV form DLDP
TDTEFA		Time for blocking of DTEV as of start with tester request
TDTESZO		time after start for desactivation fast purge rate decrease DTEV at B <sub>JL</sub> = TRUE
TDTESZU		time after start for activation purge rate decrease DTEV at B <sub>JL</sub> = TRUE
TDTEZAM		time after engine start for possible activation of active DTEV
TFRMDTEE		monitoring duration frm
TMDTEU		lowest engine temperature threshold for diagnose
TPERDTE		time for repeating DTEV at non stop idle
TSFTES		fault active time: canister purge system
TTEVAZ		duration of stay for CPV opening with not successful frm
TVDTEABG		delay time between engine and Lambda- sensor
TVDTEB		delay time for statement TEV o.k./defect in diagnosis DTEV
TVDTEE		Duration as of PCV open for checking of DTEV
TVDTELLA		min. time for activation conditions DTEV at idle fulfilled
TVDTEVP		delay time for setting of the flip flop "Passive Diagnosis CPV o.k."
TVDTEVPM		delay time for setting of the flip flop "Diagnosis passive possible"
TVDTEVZ		delay time for closing CPV for active DTEV
ZDFFDTE		Time constant for highpas filter of generator signale
ZFRMFIL		filter timeconstant for lambda controller
ZFRMXAF		filter time constant for frmxa_w signal
ZKRMSTEV		time constante low pass filter for mode 6 DTEV
ZMLETAN		Time cons. for filtering for the calc. of the energy needed for idling for DTEV
ZMSTEDTE		Time constant for filtering of the calculated mass flow PCV
ZRLTEDTE		Time constant for filtering of the calculated charge PCV





## FB DTEV 32.90 Detailed description of function

Essentials of the DTEV for quick readers and crash course beginners

"- Task of: Check of the PCV with regard to controllability of the flow rate => permanently open as well as permanently closed" the DTEV PCV is detected.

"- Checking principle: 5 possibilities for O.K. - check "

- 1.) O.K.: DLDP reports PCV being O.K. from initial purging - only on projects with according DLDP
- 2.) O.K.: DLDP reports PCV being O.K. from compulsory purging after canister pressure check - only on projects with according DLDP
- 3.) O.K.: From passive check. In a purge control phase high saturation is detected, which can only be caused by an O.K. PCV. No previous problems of the mixture control => PCV can be controlled thus is O.K.
- 4.) O.K.: From active check at idle. A deviation of the Lambda controller from its value prior to opening the PCV indicates that the PCV can be controlled. => PCV O.K.
- 5.) O.K.: If a stoichiometric mixture is coming there is no deviation of the Lambda controller  
=> Only the reaction of the idle control, which closes the throttle valve can be evaluated  
=> Indication for an O.K. check is the decrease of the air mass flowing through the throttle valve  
=> If the valve cannot close any further the ignition angle efficiency is worsened. This is also detected.

1 possibility for defective PCV check

- 1.) defective: If neither a reaction of the Lambda controller nor of the idle controller can be observed during the active check by controlling the PCV open, then the PCV can no longer be controlled (jammed at closed or open position) => defective

"- Preconditions: Precondition is a reasonably satisfactory application of the labels in %BGTEV and %ATEV especially at" idle. => MSNTATE, KLAFT !

- Equally important is an application of the idle control incl. torque margin (KFMRES). If the parameters of the idle control are changed later on, this may affect the result of the DTEV.
- An adequately adjusted mixture pilot control and Lambda control is also a precondition for the DTEV.

"- Application: - Now we can get started:"

- Set important codes and customer-specific labels correctly!!!
- CWDTEAPP: Via Bit 0 a "continuous operation" of the DTEV can be activated, so that one open-control check after the other results without the result being considered => very recommendable !  
By means of the time TPERDTE it can be determined how fast the DTEVs follow one another!  
Do not set TPERDTE to zero !!!
- CWDTEAPP: By means of Bit 1 a distinction between a system with HFM and a system with P-charge sensing can be made. On a P-system bit 1 is set => CWDTEAPP = 2 or 3!!!  
On an HFM-system bit 1 of CWDTEAPP = FALSE => CWDTEAPP = 0 or 1!!!  
In any case, please make sure that this bit is set correctly!!!
- AVDTEVX: Number of trials per driving cycle, until the DTEV "retreats unsatisfied"  
Depends on the customer's request! AVDTEVX: minimal 5
- APDTEVX: After a terminated check with negative result (E\_tes = TRUE) the authorities only allow for one repeated check within the same driving cycle. => APDTEVX = 2 !!!
- TDTEZAM: Time after the start as from when the DTEV tries an active check for the first time.  
In the application phase the time can (should) be lowered to e.g. 10 s, otherwise it is to be set to 590s for the FTP. Values for the Euro-Test are not yet known.
- After this introduction of the most important labels for the initial start-up the DTEV should start acting at idle (CWDTEAPP Bit 0 = TRUE, TDTEZAM = 10 s).

"- For more details refer to the following function description or to the block APP hint!"

Contents:

- Essentials of the DTEV for quick readers (see above)
- Task and environment of the DTEV
- Features of the PCV check
- Comparison of the DTEV in ME7 in contrast to M4- and M5-systems
- Functional principle, functional sequence, sequential control (timing in the exhaust test and in the field)
- Connection of the DTEV to other functions
- Detailed description of the FDEF figures and explanation of the bits and RAM-cells



Task, efficiency and environment of the DTEV:

- The task of the DTEV is to detect a defective purge control valve. It is used in addition to the electrical diagnosis." Provided the electrical diagnosis (%DTEVE) has already detected a fault, the DTEV remains inactive. If the electrical diagnosis should not yet have detected a fault it will be detected by the DTEV.
- Provided a leak diagnosis pump (LDP) is mounted in the system a PCV can also be checked for being O.K. by means of the" diagnostic function DLDP. The DTEV obtains the input signals (B\_tevioi and B\_teviot) from the DLDP. The active check DTEV is then switched off and the cycle flag is set. If no O.K. is obtained from the DLDP or if no LDP is mounted then the DTEV will perform the check.
- The DTEV, however, at long last only gives a defect-statement by a comparison of"
  - a) through throttle valve (DK) "flowing performance" of the engine at idle (air mass DK\* ignition angle efficiency) at closed PCV
  - b) through throttle valve (DK) "flowing performance" of the engine at idle (air mass DK\* ign. angle efficiency) at 100% open PCV
 If the PCV opens the performance flowing in through the throttle valve must decrease. The performance also decreases if the PCV as from a certain opening will distinctly open even further. Therefore a PCV leak up to about 40% of the maximum flow rate cannot definitely be detected, since the flow increases by 60% of the maximum flow rate when opening completely. When the activated carbon filter is highly saturated, such a leakage, however, will trigger a fault in the diagnosis of the fuel supply (rkat or rkaz at the min. limit stop) and in the DLDP it will in any case produce a fault message "canister leaks". A reduced maximum quantity through the PCV (lesser blockage) is also not definitely detected.
  - a) During the saturation test a PCV with about half of the maximum flow rate can already be tested as being O.K.
  - a) During the test by means of detection of an fr-deviation at idle already 10% of the maximum flow rate suffices if the activated carbon filter is highly saturated to arrive at an O.K. message.
  - b) During the air test on the other hand a PCV is only tested as being O.K. if the flow rate is higher than 50% - 60% of the nominal flow rate, otherwise an abort without result takes place. A defect-check will only be successful with a PCV with less than about 40% of the nominal flow rate.
- The DTEV is suitable for Mono and Stereo Lambda control with continuous as well as two-step Lambda control."
- '- The DTEV needs the "saturation-dependent purge control" (TEB) as well as the functions BGTEV (calculation of mass flow TEV) and' ATEV (output pulse duty cycle).
- The DTEV is suitable for P-charge sensing (B\_hfmv=FALSE) as well as for HFM-charge sensing."
  - With the P-charge sensing the air mass flow through the throttle valve is derived from the throttle valve angle
  - With the HFM-charge sensing this flow is obtained from the signal ml\_w based on the HFM-signal.
  - Via the code word CWDEAPP (Bit 1) this can be coded.

Features of the PCV Check

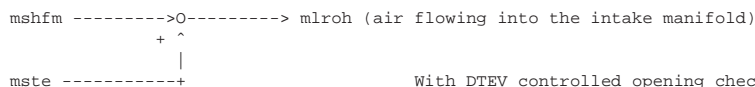
\* 2-stage Check:

- 1) In a mixture adaptation phase it must be detected that there is no fault of the pilot control and that the factor Lambda control fluctuates stable round 1.0. If now - in a successive purge control phase - a high degree of saturation of the activated carbon filter is detected and regenerated by means of a high fuel rate, then this is an obvious sign that the PCV is okay (O.K.).
- 2) The following test only needs to be performed if up to the time TDTEZAM after engine start no O.K. detection via high fuel rate from purge control (or via the DLDP) exists:
  - Progressive opening control of the PCV (comparable to DTEV on M4, M5).
  - O.K. check, if a deviation of the Lambda controller (toward rich or lean) or a distinct reaction of the idle control (negative torque action) is observed.
  - Defect-check, if no considerable Lambda controller deviation can be observed and if also the idle controller does not perform any considerable action (explanation see section: Comparison of DTEV in ME7 in contrast to M4, M5).

Comparison of the DTEV in ME7 in contrast to M4- and M5-systems / Differences between HFM-charge sensing / P-charge sensing:

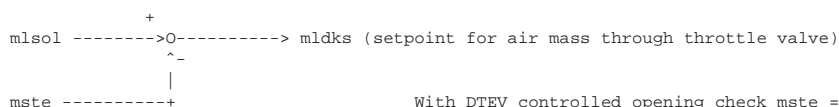
Especially for the opening check mste = 0 is set, although the PCV is controlled open. Thus the relations in the system change at a few places in contrast to normal operation with purge control (TEB) as defined in ME7:

- 1) The air mass flow through the purge control valve is taken into consideration in the charge sensing. The mass flow PCV (mste) is taken into consideration in the function %EGFE => rl\_w comprises mste !



With DTEV controlled opening check mste = 0 is set !!  
=> this switches off the consideration of the PCV air in the charge sensing !  
Remark for P-system: The P-sensor also measures the charge rate of the PCV !!!  
Thus it is always taken into consideration in ml\_w and rl\_w (also with DTEV) !!!

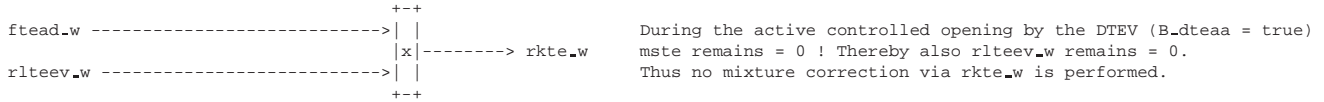
- 2) During the calculation of the desired throttle valve angle mste is taken into consideration => at open PCV the throttle valve opens accordingly less !



With DTEV controlled opening check mste = 0 is set !!  
=> thereby the position of the throttle valve will at first not change when the PCV is opened.  
Only if the idle control and mifa\_w decrease, is the throttle valve e.g. closed.



3) The mixture correction of the purge control takes place additive in the ME7 (rkte\_w instead of ftea on M4 and M5).  
The relative fuel rate is calculated from: Degree of saturation (ftead\_w) \* relative charge purge control (rlte\_w)



**Conclusion:**

- When the PCV is opened by the DTEV (controlled opening check) all above-mentioned actions are switched off (mste\_w = 0).
- Thereby the relations of the M4 and M5 are re-established.
- One of the features of an O.K. PCV is that either the Lambda control or the idle control shows a reaction.
- Only if both control types show no reactions is the PCV defective (either incorrectly open or incorrectly connected).

Further exceptional features of the ME7 as compared to M4 and M5:

- A further difference of the ME7 is the torque-based idle control.
- Actions of the idle control take place on basis of the torque (dmllr...) and not as in M4, M5 on basis of air only (qsol)!
- The idle control takes action via the throttle valve as well as via the ignition angle.

Special features of HFM charge sensing as compared to P charge sensing:

- The ignition angle efficiency effective at active DTEV (PCV open) is not etazwist, since the additional charge through the PCV is not taken into consideration on the HFM-system when the optimum ignition angle KFZWOB (nmot, rl) is calculated. The actual efficiency is usually greater since the charge is greater and thus zwopt is less advanced.
- => Correction map KFDEETATE. With the P charge sensing the PCV air mass flow is in any case contained in rl\_w.
- Since rl\_w becomes very small on the HFM-system during DTEV and in the process does not correspond to the actual charge it could happen that the lower rl threshold RLMNN would be reached. So that this will not happen the threshold is lowered by the amount of the already detected rl\_w decrease (rltedte\_w).
- During HFM charge sensing the Lambda controller will show no reaction when the PCV is opened, only in case of stoichiometric mixture. During P charge sensing this will be the case with pure air since here the additional PCV charge is measured in rl\_w.
- During the HFM charge sensing the charge sensor (HFM) only sees that air, which flows through the throttle valve. Provided over-critical pressure ratios exist the equalizing HFM / Alfa-n (msndko\_w, fkmsdk\_w) is not influenced when the PCV is opened by DTEV.
- During the P charge sensing the charge sensor (P-sensor) sees the PCV air, the Alpha-n system does not see this mass flow. This leads to a mismatch and to adaptation demand with msndko\_w. This Delta (dmsnte\_w) is learned in the DTEV and transferred to the BGMSZS. When the PCV is abruptly closed at the end of the DTEV, dmsnte\_w is reset to zero.

4) There is an ME7 for the continuous as well as for the two-step Lambda control. Therefore the PCV check should work with both Lambda controls. The fast mean value of the Lambda controller (frm\_w) serves as input value for the DTEV. On Stereo-systems either the mean value from both banks (frmit\_w) calculated in the TEB or that frm\_w, which is further away from the neutral value 1.0 (frmx\_a) is used. By means of a low-pass filtering (of frmxf\_w) it is in addition possible to achieve an approximately equal dynamics for continuous or two-step control. Thereby the DTEV is suitable for both controls. Frmitf\_w should be filtered with a distinctly smaller time constant.



Functional principle, functional sequence, sequential control (timing in the exhaust test and in the field):

By means of the 2-stage check (passive, active) the DTEV tries to come to a diagnostic result as soon as possible after the engine start.

a) Passive check (can only be terminated if the PCV is O.K.):

- During a mixture adaptation phase with low engine air mass flow it is determined whether the pilot control is O.K. An indication for this is: Mixture adaptation needs to perform minor corrections only, the Lambda controller is not far off the neutral value. The flip-flop "diagnosis passive possible" (B\_dtepm) is set. The passive diagnosis is only enabled if a fault was not already detected (E\_tes = TRUE). Thereby a healing at detected fault is only possible via the controlled opening check.
- In one of the successive purge control phases the O.K. check can already take place with medium to high but plausible degrees of saturation of the activated carbon filter. As soon as it is discovered that purging is performed at high fuel rate at an air mass greater than a threshold and that in the process the Lambda controller fluctuates relatively stable round 1.0, an O.K. detection is triggered (B\_teviop). The PCV check is terminated for this driving cycle.

Remark: In the US FTP75 Test - during the actual exhaust test with saturated activated carbon filter - this check will in all probability be successfully terminated already on the 3rd or 4th hill if the PCV is O.K.

b) Active check (check by means of active PCV opening control by the DTEV):

- Enabling of the active diagnosis:
  - After the time TDTEZAM has elapsed (e.g. TDTEZAM = 590s in the FTP75 prior to long idling at 600 s) the active check is permitted (B\_dtezam), if so far no other check was completed with O.K. and if in addition the integral of the currently purged air mass (imsteini) has exceeded the threshold IMSDTEVA. Other diagnostic functions can furthermore block the DTEV (DDMTL, DLLDP, DLLR).
  - The active check is only attempted for a limited number of times per driving cycle. In case of an abort (diagnosis can make neither an O.K. nor a defective statement), the counter is increased by "number of trials DTEV" (avdtev). If it reaches the value AVDTEVX then the active DTEV is no longer activated during this driving cycle.
  - After a defect-check (no O.K. but B\_dteend = TRUE) only one repeated test is possible (APDTEVX=2) - CARB requirement! During the quick test (B\_fa, B\_fates) no repeated test is possible.
- Decreasing control of the purge rate in TEB (B\_ftedab)
  - As soon as the flag B\_ll is set (driver steps off the accelerator) a decision is made on whether the decreasing control shall be effected immediately or only once idling is stable. The following is achieved by means of this distinction:
    - a) An immediate decreasing control in case of "snap off throttle" (B\_ll = TRUE) in order to be able to use the limited time during the exhaust test at idling solely for the controlled opening of the PCV. No valuable idle time shall be wasted for a controlled decrease of the PCV from a purging phase. A decreasing control is then performed during fuel cut-off on overrun (manual transmission) or already prior to the stopping of the vehicle (automatic transmission). This quick decreasing control of the purge rate (B\_ftedab) reduces the necessity of an adaptation phase prior to the DTEV as compared to the M4 or the M5.
    - b) With high saturation it would not be sensible to each time request a quick decreasing control of the purge rate whenever the driver steps off the accelerator (B\_ll = TRUE). The purge quantity would be distinctly reduced. The decreasing control is only activated here if the vehicle is at rest for a certain time (delay time: TVDTEVZ) during idle (vfzg = 0).
- Request of the active check:
  - The partial function DTEVZU checks the performed decreasing control of the purge rate by an inquiry of ftefsoll\_w = 0 ! If ftefsoll\_w = 0, the bits "active check active" (B\_dteaam and B\_dteaa) are set. B\_dteaa switches mste\_w and mste = 0 in BGTEV!! B\_dteaam is reset one calculation cycle earlier than B\_dteaa and is needed as function-internal control bit.
  - Simultaneously the "global bit" B\_dtes is set, which indicates in the motronic system that the DTEV now actively opens the PCV. B\_dtes and B\_dteaa remain set in case of an abort of the DTEV or when the DTEV has terminated until the PCV is truly closed (tateout = 0)! Only then is the flip-flop reset. Thus this bit constitutes "the bracket" round the active PCV opening control by DTEV.
- Mode of operation of the active check:
  - The inclusion of the mass flow PCV is switched off in the motronic system (B\_dteaa = TRUE => mste\_w = 0).
  - The PCV is controlled open progressively (at first slowly then increasingly faster).
  - The deviation of the Lambda control factor is watched. A deviation of more than 5% - 10% suggests an O.K. PCV.
  - Apart from the Lambda controller also the needed air mass is evaluated with the current ignition angle efficiency (so to speak the performance flowing through the throttle valve needed at idle) is watched. If this performance drops as expected when the PCV is opened then it can be assumed that the PCV is O.K.; if it drops less than expected then the PCV is partially blocked (the PCV quality is less); if the performance flowing through the throttle valve remains constant then the PCV is defective.



c) Interaction of the DTEV with the canister diagnosis DLDP (if existing)

- The canister diagnosis DLDP can have the PCV checked as being O.K. already prior to the passive or active check (B\_tevioi or B\_teviot is set). The active check of the DTEV then no longer needs to be performed, the passive check (B\_tevio), however, is not blocked. B\_tevio being set then, however, has no effect on the fault memory since Z\_tes = TRUE and E\_tes = FALSE were already set prior to the DLDP.

- In DLDP there is a code word, which distinguish here

1) LDP without external AAV (LDP is near the charcoal canister (AKF)). The LDP ist the only connection between tank system and ambient air. The membrane e.g. is closed by the shor circuit to mass and the tank system is not aerated.

2) LDP with extrenal AAV ( LDP is near the engine, at chacole canister is a electiric shut-off-valve). The tank is not aerated, if the electric shut-off-valve can not open and the DLDP membrane is closed too.

SY\_AAV =

TRUE: AAV is installed ==> DTEV stop only, if E\_aave&E\_ldpe&!B\_ldpi  
FALSE: without AAV ==> DTEV stop only, if E\_ldpe = TRUE

Summary Timing: DLDP-PCV-Check / Passive check / Active check / immediate and delayed decreasing control of the purge rate in TEB for active check:

- In the first mixture adaptation phase the DLPD (about: Second 200 - 350 after start) can become active, if its input conditions are fulfilled. With O.K. system (PCV O.K., canister O.K., LDP O.K.) either B\_tevioi or B\_teviot is set. The active check of the DTEV will in this case be switched off otherwise, or if a fault PCV is already given (E\_tes = TRUE) the DTEV will check itself. If no DLDP exists B\_tevioi and B\_teviot remain set to FALSE.
- For a certain time as from engine start at first only the passive check is possible (TDTEZAM). Provided it cannot be terminated successfully by then the active check becomes possible (B\_dtezam). As from second 590 in the FTP.
- A quick decreasing control of the purge rate was defined for the DTEV in TEB and TEBEB. With the bit B\_ftedab it is possible to control the purge rate down within e.g. 2 seconds. Thus a preliminary mixture adaptation phase is not necessarily needed in the exhaust test.
- This decreasing control usually only becomes active at considerable saturation if all conditions for the DTEV are given for a certain time (vehicle at rest during idle, idle control active ...).
- With low saturation and if the time after start lies within a time window (e.g. for long idling in the FTP75: 990 s - 1030 s), the quick decreasing control is already started with B\_ll = TRUE. By this the DTEV has a guaranteed maximum of checking time in this idle phase.

Connection of the DTEV to other functions:

- a) Charge sensing and calculation of ignition angle efficiency => provision of a variable for the energy demand of the engine
- The charge sensing supplies the air flowing through the throttle valve:
    - i) HFM-charge sensing: Air mass flow ml\_w (does not include the PCV air mass flow mste\_w since mste\_w = 0 !)
    - The DTEV evaluates the air mass flow with the accuracy of the HFM !
    - ii) P-charge sensing: msndkoo\_w \* fho\_w \* ftvdk\_w \* fklaf\_w (msndkoo\_w => standardized air mass DK (characteristic MSNWDK))
    - Attention: The application of MSNWDK is relevant for DTEV !!! Do not change after the application of DTEV !!!
  - With the P-system a learning of the PCV leakage air is necessary: dfuelsan\_w => dmsnte\_w (inclusion in BGMSZS in msndko\_w).
  - The ignition angle efficiency is etazwist ! Provided the ignition angle does not correspond to the optimum ignition angle it becomes less than 100%. Attention: The ignition angle efficiency is only accurate if the charge rl\_w is correct. This is not the case for an open PCV on an HFM-system!! => refer to application correction map KFDETATE !
- b) Lambda Control:
- Input values from the Lambda control:
    - From frm\_w and frm2\_w the variables frmxa\_w and frmit\_w are formed in %TEB. Refer to TEB.
    - B\_lr, B\_lr2 indicate, that the Lambda control of the respective bank is active. For DTEV it is sufficient only if one bank operates.
  - Output values for the Lambda control:
    - B\_dtefr: Condition setting of the control factors to the value frdter\_w
    - frdter\_w: Value for control factors for B\_dtefr
- c) Idle Control
- B\_llr : Idle control active
  - > although the idle control is decisive for the DTEV, no analogous variable of the idle control is directly inquired upon. The following variables, however, are evaluated indirectly:
    - ml\_w: measured HFM air mass flow, which indicates the air mass flow through the throttle valve
    - etazwist: current ignition angle efficiency. This value is influenced by the idle control.
  - Remark: The product from air mass flow ml\_w and ignition angle efficiency is a variable, which corresponds to the needed and measured performance of the engine during idling. If the PCV now opens the measured performance becomes less since the PCV introduces "not measured" performance (air mass PCV \* ignition angle efficiency at open PCV). At constant idling the measured performance needs to drop with an O.K. PCV.
  - Actions taken by the DTEV in the idle control and in the demand adaptation are:
    - at active DTEV the demand adaptation is blocked
    - the I component of the idle controller is expanded
    - at the end of the DTEV the I component is reset by that absolute value, which it has "learned down" during the check. Thereby it is possible to prevent a drop of the idle speed.



d) Purge Control (TEB):

- Input values from TEB:
  - Desired purge rate (ftefsoll\_w): The desired purge rate is the output of an integrator in the TEB.
  - Currently learned ACF saturation (ftead\_w): The saturation is no longer learned during DTEV
  - Current fuel rate purge control (fkatei): The fuel rate is calculated from fteva\_w \* ftead\_w
  - Max-deviation of the Lambda controllers (frmxa\_w): Serves as a measure for a system without mixture fault
  - Mean value of the Lambda controllers (frmit\_w):
  - Integral of just purged mass flow (imsteini): Enables the active check
- Output values for TEB:
  - B\_ftedab: Condition quick decreasing control of purge rate: controls ftefsoll\_w down to zero within a short time and holds the purge rate at zero during the DTEV controlled opening check.
- Output values for TEBEB:
  - B\_dtes: Disables the TEB

e) Decrease of the RL-Min-limitation in MDFUE => Variable from DTEV: rltedte\_w:

Only significant on HFM-systems. Here, the variable rl\_w does not contain the charge flowing through the PCV into the intake manifold. Thus the limit RLMIN would be reached in many cases and the throttle valve would thereby be stopped against further closing. However, since the actual charge at open PCV is higher, the MIN-threshold for rl\_w can be decreased by that absolute value, as was already detected as decrease of the air flowing through the throttle valve into the intake manifold (dmletan\_w resp. dmletanu).

f) Calculation of mass flow PCV (BGTEV):

- BGTEV supplies that mass flow mstedte\_w, which is also calculated if the DTEV is active.
- The bit B\_dteaa is also included in BGTEV and it switches the mass flow mste and mste\_w to zero for the other motronic functions (charge sensing, throttle valve triggering) when B\_dteaa = TRUE.

g) Switch on condition mixture adaptation (LRAEB): The LRA is only blocked once the DTEV truly performs an opening control of the PCV (B\_dtest = TRUE).

h) Sequential control (BBTEGA):

- B\_dtes forces the decreasing control of the purge rate and triggers a mixture adaptation phase. The LRA is active until B\_dtest is set. (refer to point f)

i) Diagnosis canister leak with pressure pump (DLDP):

- B\_tevioi (PCV detected as O.K. by DLDP-PCV-Check by means of initial purging)
- B\_teviot (PCV detected as O.K. by DLDP-PCV-Check by means of a decrease of the dropout time after leak test)
- For Mode 6: tispdp\_w and tispdp\_x\_w from DLDP for B\_tevioi
- For Mode 6: tpldptc\_w, tpldptcx\_w from DLDP for B\_teviot

j) Diagnosis idle control

- The DLLR must be able to block the active check of the DTEV: B\_dllra blocks B\_dtezam
- Thereby priority can be given to the DLLR (=> see DLLR).

k) Other input values:

- Vehicle speed: vfzg
- Factor altitude: fho\_w
- Condition factor altitude is valid: B\_hag
- Detection driving position engaged/disengaged: B\_fs
- Detection air conditioner on/off: B\_koe
- Deactivation due to fault:
- Deactivation in case of SLS and DSLS
- nsol, nmotll: to check on whether a constant idle speed is maintained and for the abort in case of engine speed increase
- B\_dldpte: Diagnosis DLDP can block DTEV
- B\_dmtltz: Diagnosis leak diagnosis pump can block DTEV
- kldfpwm: PWM-signal of the generator excitation

l) Tester interface

- B\_fa
- B\_fates
- The DTEV switches off as soon as another function is to be tested
- The opening control check is activated by B\_fa & B\_fates. Prior to that quick decreasing control DTEV. Other blocks (B\_dllra, tnse\_w < TTEZAM) are canceled.
- When the quick trip is activated a DTEV internal reset is triggered, so that the check will be performed in any case. The fault memory, however, is not cleared. At the end of the quick trip the result is maintained!



Detailed description of the FDEF figures and explanation of the bits and RAM-cells:

The function is subdivided into 6 partial functions:

- 1) Creating of some signals (DTEV SIGA)
- 2) General switch-on conditions (DTEVEB) / subdivided into partial functions: DTEVPEB and DTEVAEB
- 3) Passive check PCV (DTEVP)
- 4) Request of quick closing control (DTEVZU)
- 5) PCV check by active opening control (DTEVAUF) / subdivided into partial functions: DTEVLR, DTEVLL, DTEVTAT, DTEVAEND
  - 5.1) Partial function DTEVAUF / DTEVLR:
  - 5.2) Partial functions DTEVAUF / DTEVLL and DTEVAUF / DTEVLL / DTEVDML:
  - 5.3) Partial function DTEVAUF / DTEVLL / DTEVRQ:
  - 5.4) Partial function DTEVAUF / DTEVTAT:
- 6) Formation of the signals for the fault management (DTEVEA - "Error-treatment")

1) Partial function DTEV SIGA:

The signals of the Lambda control (frmit\_w and frmxa\_w - conditioned in %TEB) are filtered in this partial function. Varying time constants should be chosen.

2) Partial function DTEVEB:

General switch-on conditions - The partial function DTEVEB has the subfunctions DTEVAEB (switch-on conditions for DTEV active check) and DTEVPEB (switch-on conditions for DTEV passive check).

Local bits from DTEVEB:

- B\_dteenf: all functional parts of DTEV blocked, since other error was detected, which interacts with DTEV
  - blocks the active check by an opening control of the PCV (B\_dtezam)
  - blocks the Lambda evaluation at any one check (B\_dtelbm)
  - resets the flip-flop: Passive check possible (B\_dtepm)
- B\_dtelbr: resets the flip-flop: Passive check possible (B\_dtepm)
- B\_dtephm: DTEV checks are physically possible (exception: the readiness of the Lambda control, this is executed separately). Important here: Altitude deactivation via fho\_w and switch-off if engine temperature < threshold.
- B\_dtenam: Diagnosis only possible by an opening control of the PCV !
  - PCV already detected as defective (E\_tes)
  - fault in the fuel supply system assumed
  - DTEV is activated by the tester
- B\_dterap: Reset after aborted or successful check in the application phase so that another check can be enabled. This continuous periodically returning reset is activated via the code word: CWDTEAPP (Bit 0)

Output values of the partial function DTEVEB:

- B\_dtezam: Diagnosis by an opening control possible
  - Conditions for B\_dtezam = TRUE:
    - PCV not already checked as being O.K. by the passive check
    - PCV not already checked as being O.K. by the idle control
    - PCV not already checked as being O.K. by the Lambda control
    - PCV not already checked as being O.K. from the DLDLP (B\_tevioi or B\_teviot) if error bit E\_tes = FALSE and no function demand DTEV (B\_fates)
    - Max. number of trials by active action (avdtev) not yet reached
    - Max. number of checks with detection of a fault (apdtev) not yet reached
    - no other fault blocks the DTEV
    - bit idling (B\_ll) is set
    - active checks of the DTEV are physically possible (B\_dtephm)
    - time as from start has exceeded the value TDTEZAM (time for DTEV closing/opening check elapsed) (For FTP-Test: TDTEZAM: 590 s) or with function demand (B\_fates) time TDTEFA exceeded.
    - counter for cyclic repeat (CWDTEAPP Bit0=TRUE) has reached the value TPERDTE.
    - B\_dldpte, B\_dmtltz and B\_dllra, B\_grdst and B\_m8te can block the active check
    - imsteini must be greater or equal to a threshold: Thereby the DTEV active check is only started if a purging phase was performed immediately beforehand.
- B\_dtelbm: Lambda evaluation possible: Diagnosis via fr evaluation possible, system O.K.
- B\_dtepm: flip-flop - condition passive diagnosis possible
  - Setting conditions for B\_dtepm (must be given for longer than TVDTEVPM for the flip-flop to be set):
    - a) B\_dtelbm = TRUE (Lambda evaluation possible)
    - b) additive correction (rkat\_w + rkaz\_w) of the mixture adaptation small
    - c) air mass less than threshold (ml < MLDTFPPF), so that a PCV jamming at the open position does not lead to B\_dtepm being set erroneously.
    - d) filtered Lambda controller frmxf\_w in range round 1.0
    - e) an adaptation phase must be active (B\_gap = TRUE)
  - Reset conditions for B\_dtepm:
    - a) additive correction of the mixture adaptation during an adaptation phase large
    - b) filtered Lambda controller outside of range round 1.0 during an adaptation phase
    - c) fault, which blocks the diagnosis or fault in the fuel supply system detected
    - d) only active check possible (B\_dtenam = TRUE)
    - e) Reset DTEV desired (B\_dteres = TRUE)
- B\_dteres: Condition reset diagnosis DTEV: resets all memories of the function to initial values (also error and cycle flags).



### 3) Partial function DTEVP:

Passive check - O.K. detection with reliably detected high degree of saturation of the activated carbon filter while simultaneously there is a high fuel rate from the purge control during purge control operation.

- saturation medium or high, however, plausible: FTEADDPU <= ftead.w <= FTEADDPO
- fuel rate purge control high: fktei = ftead.w \* ftefva.w > FKADPMN
- filtered Lambda controller within the range round 1.0: FRMDTEVU <= frmxaf.w <= FRMDTEVO
- engine air mass greater than threshold: ml.w > MLDEPF (so that PCV with only minor throughput is not erroneously detected as being O.K.)
- in partial function DTEVEB it was determined that the diagnosis passive is possible: B\_dtepm = TRUE.
- Lambda evaluation for diagnosis DTEV is possible (B\_dtelbm)

=> All conditions must be fulfilled for a minimum time (TVDEVP), only then will the flip-flop B\_teviop be set.

### 4) Partial function DTEVZU:

Request of a quick decreasing control of the purge rate, activation of the opening control check

As soon as the bit B\_dtezam (active check possible) is set a decreasing control of the purge rate is either immediately effected or it is still waited until the activation condition of the DTEV are stable (B\_llr, vfzg = 0, at least the Lambda control on one bank is active for longer than TVDEVZ). The bit B\_ftedab goes to the TEB and demands a quick decreasing control of ftefsoll.w there.

Immediate decreasing control:

- in case degree of saturation (ftead.w) is less than threshold (FTEADSZ) or
- time as from end of start within window: TDTEVZU <= tnse.w <= TDTEVZO.

The opening control of the PCV can be enabled (B\_dteeam = TRUE) as soon as the purge rate was controlled down and at the earliest once the time TVDELLA after stable idling has elapsed.

The bits B\_dtes and B\_dteaa inform the motronic that the PCV may be open due to the opening control from the DTEV. These bits are only reset once tateout = 0. Two bits are necessary so that in the same system also a DTESK can be used (B\_dteaa sets in BTEV mste and mste.w = 0; mste.w is to be calculated in case of DTESK) !

### 5) Partial function DTEVAUF:

Check by means of an opening control of the PCV during idling

The opening control check is only activated, if so far no O.K. detection is given: The test is performed by a progressive PCV opening control (comparable to DTEV with M4, M5).

An O.K. check takes place if a deviation of the Lambda controller is observed or if the idle actuator performs a considerable action (product from air through throttle valve \* ignition angle efficiency decreases)!

A defect-check takes place if no considerable Lambda controller deviation can be observed and if in addition the idle controller does not need to perform any considerable action. (Explanation also refer to section: Changes of ME7 as compared to M4, M5).

The opening control check is again subdivided into 4 further partial functions

- DTEVLR: Check of PCV by an evaluation of the factor Lambda control
- DTEVLL: Check of PCV by an evaluation of the determined power demand
- DTEVTAT: Calculation of the pulse duty cycle tadtea, as well as of the resetting value and of the reset condition for the Lambda controller in case of end or abort of the opening control check DTEV
- DTEVAEND: Combination of all abort and end conditions of the opening control check DTEV

#### 5.1) Partial function DTEVAUF / DTEVLR:

The partial function (DTEVLR) evaluates the filtered mean value of the Lambda controller (frmitf.w) and forms the bit for the start of the PCV opening control (B\_dtest).

Start of the PCV opening control:

- i) If frmitf.w has changed only little (change < DFRMDTEE) for several times in succession (no. of times: APDTEFRE) within a predefined time (TFRMDTEE) then the bit "frmitf.w stabilized" is set (B\_dtere = TRUE). Now an opening control is possible and the Lambda controller can be evaluated.
- ii) If the time as from the beginning of the enabling (B\_dteaa) has exceeded the value TTEVAZ, an opening control is also performed. Without the detection "frmitf.w stabilized", however, the O.K. detection via the evaluation of the Lambda controller is refrained from.

Remark: If the frmitf.w is close to the limits frmn.w resp. frmx.w, then neither the PCV is controlled open nor is the DTEV terminated until either idling is exited or until the mixture adaptation has learned the deviation.

The RAM-cell frmfref.w is updated each time a "sample" of frmitf.w is taken.

frmfref.w is also continuously updated if frmitf.w lies close to the lift limits of the Lambda control (frmn.w, frmx.w). frmfref.w serves as reset value for the Lambda controller after the end resp. in case of an abort of the DTEV.

The function is successfully terminated (B\_tevior - O.K. detection via the factor Lambda control):

- if B\_dteaa is set
- if frmitf.w was detected as having stabilized
- if frmitf.w was still far enough away from the control limit stop
- if frmitf.w rose by more than DFRMDTEF after the beginning of the PCV opening control or if it dropped by more than DFRMDTEM

Remark: A successful termination via B\_tevior also leads to a resetting of the bit B\_dtezam, which in turn resets the active bit B\_dteeam. Thus tadtea = 0 results (partial function DTEVTAT), which in turn resets B\_dteaa, B\_dtes and B\_dtest in the partial functions DTEVZU and DTEVLR.





The function is aborted (B\_dterm):

- if B\_dteaa is reset, because e.g. idling is stopped. Then also B\_dtes and B\_dtest are reset.
- if the control limits (frmn\_w resp. frmw\_w are narrowed during the diagnosis and therefore not enough control lift remains for an O.K. diagnosis.
- if with "not stabilized" Lambda controller - B\_dtefre = FALSE

Prior to the opening of the PCV the function waits for a stabilization of the mixture adaptation (rkat\_w) if frmitf\_w has no sufficient distance to the control limits.

The evaluation of the measured engine performance (air mass flow throttle valve \* ignition angle efficiency) is performed simultaneously for as long as the function was neither successfully terminated with B\_tevior nor that it was aborted.

=> see partial function DTEVLL:

### 5.2) Partial functions DTEVAUF / DTEVLL and DTEVAUF / DTEVLL / DTEVDML:

This part of the check evaluates the "performance flowing in through the throttle valve". If the O.K. PCV is opened then the engine speed and thus the idle engine performance is kept constant by means of the idle control; ignition angle efficiency and /or air mass flow through the throttle valve are reduced by that absolute value of unmeasured performance, which the PCV brings in (mass flow PCV \* ignition angle efficiency), provided the Lambda control corrects the mixture to Lambda = 1.

On the HFM charge sensing the signal "ml\_w" is used as airflow through the throttle valve!

On the P charge sensing this airflow can be calculated from the characteristic MSNWDK as well as from the KLAF and the altitude and temperature correction. Since the intake air temperature (especially with a sensor in the intake manifold) can change fho\_w \* ftdk is "held" during the check.

On HFM-systems, however, the following problem results:

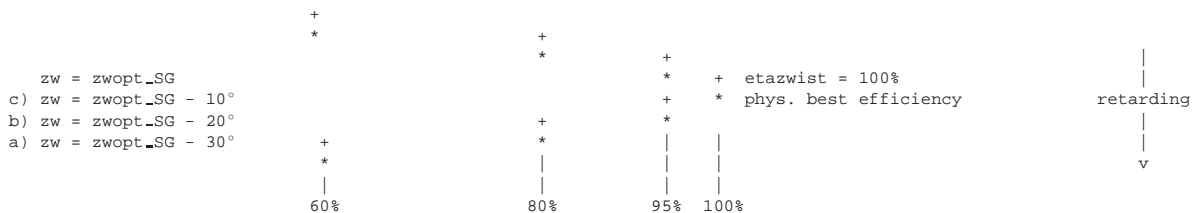
- By a feed-in of not measured additional charge through the PCV the source rl of the map KFZWOP becomes incorrect. A smaller value is for example outputted for zwopt (more advance ignition angle) than the actual current physically correct value at completely open PCV (e.g. zwopt = 35° (rl = 12%) although the actual charge is 17% and zwopt would be 30° for this).
- If zwist lies in the region of zwopt, this is not dramatic. This only becomes a problem if simultaneously a considerable torque margin (resp. ignition angle timing of the idle control) is active.

The dependency of the engine torque on an incorrect optimal ignition angle is then high. The ECU value etazwist is then extremely incorrect.

The following diagram shows two ignition angle efficiency parabolas next to each other:

- 1) +++ engine efficiency calculated in the ECU (calculation is performed with etazwist)
- 2) \*\*\* current physically acting engine efficiency

Characteristic ETADZW:



CONCLUSION: The angle for the physically best efficiency lies by 10° later than the angle assumed in the ECU. Thus the following faults result:

- a) Control Unit (ECU) shows etazwist = 60% => due to a higher charge, however, the engine runs with 80% efficiency! 20% error
- b) Control Unit (ECU) shows etazwist = 80% => due to a higher charge, however, the engine runs with 95% efficiency! 15% error
- c) Control Unit (ECU) shows etazwist = 95% => due to a higher charge, however, the engine runs with 100% efficiency! 5% error

This must be taken into consideration in DTEV ! => Formation of etazwkte in DTEV for the performance balance.

The above representation shows: The smaller etazwist, the larger is the fault between the value of the ignition angle efficiency in the ECU (etazwist: curve with +) and the physical efficiency acting in the engine (curve with \*).

Solution: etazwist is increased by detazwte. Detazwte is again output of the map KFDEETATE (etazwist, dmletanu) Thereby - dependent on the current ignition angle efficiency (etazwist) and on the already detected decrease of the HFM mass flow at idling (dmletan) - it is possible to add a delta efficiency to etazwist in order to obtain the actual engine efficiency. Application of KFDEETATE refer to APP.

Remark: The charge rl\_w is always correctly sensed with the P charge sensing => KFDEETATE = 0 !



Calculation of the detected PCV air mass flow (mste\_ber = dmletan\_w):

The PCV air mass mste\_ber calculated from the decrease of the "performance flow through the throttle valve" is:

$$mste\_ber = dmletan\_w\ddot{a}h = \frac{(msdk\_vor * etazwkte\_vor) - (msdk\_w\ddot{a}h * etazwkte\_w\ddot{a}h)}{etazwkte\_w\ddot{a}h}$$

**Abbreviations:**

mste\_ber: calculated effect of the air mass flow PCV  
 dmletan\_w\ddot{a}h: decrease of the measured engine performance / ignition angle efficiency during the check  
 msdk\_vor: air mass flow throttle valve prior to the check  
     - from ml\_w with an HFM-system  
     - from MSNDK, fklaf\_w and fho\_w and ftvdk with a P-system  
 etazwkte\_vor: ignition angle efficiency prior to the check  
 msdk\_w\ddot{a}h: air mass flow throttle valve during the check (calculation of msdk\_w see above)  
 etazwkte\_w\ddot{a}h: ignition angle efficiency during the check

The RL-fault of the HFM-system necessitates a further connection:

DTEV -> MDFUE. The RL-Min-limitation must be lowered in MDFUE => variable from DTEV: rltedte\_w:  
 Otherwise the limit RLMN would be reached in many cases and the throttle valve would thereby be held against further closing. The MIN-threshold for rl\_w can be lowered by that absolute value, which was detected as decrease of the air flowing into the intake manifold through the throttle valve, since the actual charge at open PCV is higher.

Check of the idle energy demand:

Preliminary remark: Since this check at long last decides on "defective", O.K. or function abort it is the most important and "unfortunately" also the most complicated part of the DTEV. For the basic understanding, here are a few important statements to start with:

- Quite a few "disturbances known or not known to the motronic" influence the check.
- For one the air conditioner must be mentioned. Its energy demand distorts the balance extremely. As a rule at least one switch on / off is known (edge of B\_koe). In this case an immediate abort is performed.
- The same applies to the driving position switch on the automatic transmission (B\_fs)
- The generator excitation (kldfpwm) is known for some projects. A change leads to an abort.
- Unknown large disturbance variables are power steering and slipping clutch!!
- Just as, it is possible that electric consumers can but must not have a disturbing effect. A switch-on and off only disturbs, if the energy absorbed by the generator changes. If it was already at "its end" prior to the current output, then the supply voltage will break down, the engine is not put under more stress.
- Further effects are surely also the engine friction, which can change immediately after engine start or after a high-load phase during idling.

If now - with an O.K. PCV - an unknown consumer "sets in" while the PCV opens then this leads to a minor decrease of the "performance flow through the throttle valve". There is a risk of an erroneous defect-detection. Analogous the reversed case (defective PCV and O.K. detection) is possible.

Conclusion: - An as reliable as possible detection of such disturbances must be realized.

Solution: - The basic idea of the solution is as follows.  
     - The temporal course of the expected decrease of the air mass flow through the throttle valve is known (mstedtef\_w)  
     - The currently "measured" value of this decrease is dmletan\_w. In case of an e.g. partially blocked PCV this decrease is only a percentage of the expected value. This percentage will be described as PCV quality in the following description. This percentage can also be greater than 100% with a MAX-PCV.  
     - This percentage can be determined in a control loop directly from mstedtef\_w and dmletan\_w (integrator for PCV quality rmstevf\_w). For that the product from the determined PCV quality rmstevf\_w is multiplied by mstedtef\_w and subtracted from dmletan\_w and the result is passed on to the input of the integrator.

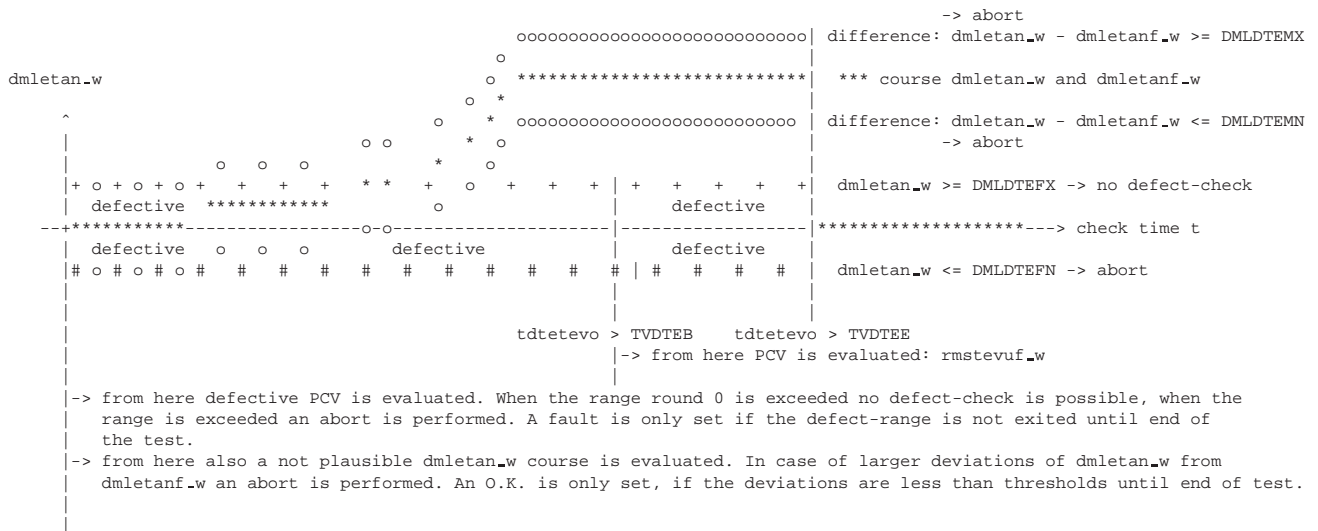
After this introduction for the basic understanding, now further details of the function:

- The current value of mletan\_w (ml\_w \* etazwkte) is stored temporarily in the RAM-cell mletanzs\_w when the PCV is opened for the opening control check.
- From then on the deviation between the current and the temporarily stored value is formed.
- This difference is divided by the current, filtered ignition angle efficiency etazwif. The calculation value for the PCV air mass flow "dmletan\_w" of the currently mounted PCV is thus obtained.
- This calculated value must approximately correspond to the expected value mstedte with an O.K. PCV. With a defective PCV, dmletan\_w hardly changes. With a partially blocked PCV the value is only a percentage of mstedte.
- The respective input values are filtered by the three low-pass filters "mletan\_w, etazwif and mstedtef\_w", so that very short-termed fluctuations (especially of etazwif) do not disturb the diagnosis. Just like the measuring signals also the reference signal (mstedte) needs to be filtered. Here it is possible to choose a different time constant (ZMSTEDTE) in order to straight away take the delayed stabilization of the idle control, which after all causes a delay at dmletan\_w, into consideration.
- The integration speed of the PCV quality integrator can be chosen dependent on mstedte (KIRMSMS). If e.g. a high integration speed with small mstedte and a low integration speed with large mstedte values is chosen then it is possible to keep the difference "dmletan\_w - dmletanf\_w" largely independent of mstedte in case of disturbances.  
=> constant disturbance deactivation.
- The "unsigned" variable of the PCV quality is rmstevuf\_w. Provided the PCV was already open for a certain time (B\_dteanf) rmstevuf\_w approximately corresponds to the quotient: Air mass flow of currently mounted PCV/air mass flow of standard PCV \* 100%.



- The formation of the bits B\_teviol (O.K. detection by "air check") and B\_tevnio (PCV defective) is described in the partial function DTEVAUF / DTEVLL.
- An O.K. detection is only possible, if rmstevuf\_w is constantly greater than RMSTEVI0 after B\_dteanf\_l was set.
- A defect-detection is only possible, if rmstevuf\_w is constantly less than RMSTEVI0 after B\_dteanf\_l was set.
- If rmstevuf\_w fluctuates round RMSTEVI0 the check is terminated (B\_dteand\_l), however, B\_teviol and B\_tevnio cannot be set.
- The function is capable of two ways of abort:
  - immediate abort
  - delayed abort (the fr-evaluation should still have a chance to perform the "good" check). An evaluation of the decrease of the performance demand at idling is no longer possible.
- The immediate abort is performed in case of engine speed fluctuations > threshold, switch-on and off of known consumers, changes of the desired engine speed and when a minimum ignition angle efficiency (ETAZWTEEN) is undershot.
- The delayed abort is triggered in case of a not plausible course of the air mass decrease  $|dmletan\_w - dmletanf\_w| > threshold$  or if  $mletan\_w \leq threshold$ . The delay has the advantage that a possible good-check is still possible via the control factor.

The following diagram shows the thresholds for an O.K. check, for the defect-check and for an abort of the evaluation of the air:



### 5.3) Partial function DTEVAUF / DTEVLL / DTEVRQ:

Calculation of a value for the relative PCV quality (rmstev\_w):

- The variable rmstevuf\_w is low-pass filtered. Thus a reliable value for the PCV quality is obtained after several checks.
- During the first check after a reset or power-fail the time constant is reduced to 2s. The value initialized with 100% can thereby stabilize quickly. The time constant can otherwise be chosen as desired.
- The setting of the bit B\_dteanf\_l (start of air check) activates the low-pass filtering.
- Initialize with 100% for C\_pwf and C\_fcmlr & B\_cltes
- The RAM-cell rmstev\_w is a permanent RAM. Thereby a once stored value is preserved for reading.

### 5.4) Partial function DTEVAUF / DTEVTAT:

- The PCV is triggered via the characteristic TADTEAMX. The PCV is abruptly controlled closed once the check has ended (B\_dtest & B\_dteaam are no longer fulfilled).
- The Lambda control factor must be reset to the reference value by the delay time of the purge gas in the intake manifold (tvfrdrte) time-variant after the closing of the PCV (bit: B\_dtefrr, value: frdter\_w). The delay time can be stored in the map KFTVFRR (tadteazu, ml).
- Via the dependency of tadteazs (max. pulse duty cycle at abort) it can be taken into consideration that dependent on the HC concentration a different delay time is necessary.
- Via the dependency of ml it can be taken into consideration that the time will strongly reduce itself when starting to drive. The reset signal is given for the time TVDTEABG. Thus it is possible to take into consideration the run-time engine -> sensor.
- The deviation "P charge / Alpha-n - system" must be learned on a P-system. dfuelsan\_w (deviation), output: dmsnte\_w. The output is added to the learned throttle valve leakage air in BGMSZS. The sum is msndko\_w !

### 6) Partial function DTEVEA:

- Formation of the signals for the fault management (DTEVEA - "error treatment")  
The error and cycle flags B\_mntes and B\_mxtes are set here.  
Deactivation and purposeful setting of the flip-flops in case of B.cdtes.  
The flip-flops B\_mntes, B\_mxtes and E\_tes are in the permanent RAM.  
A Min-fault exists if during the fault detection  $dmvad\_w > DMVTEVDO$  (does not work on the P-system)  
A Max-fault exists if during the fault detection  $dmvad\_w \leq DMVTEVDO$  "  
The bits B\_tevioi and B\_teviot are ignored in case a quick test or a fault (E\_tes) is given.

**APP DTEV 32.90 Application hint**

## Introduction:

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The DTEV is a diagnostic function demanded by the legislator, which can trigger the error lamp. Erroneous fault messages as well as not detected faults need to be classified as being critical.

The most important points (very critical) to be checked are:

- Avoiding of an erroneous fault detection in case of an O.K. PCV under all practically conceivable driving situations and ambient conditions
- Reliable detection of faults during the certification test (no abort of the function so that cycle flag is set, no O.K. message in case of a defective PCV).

Aims of "secondary order" (not quite as critical) are:

- An as frequent as possible setting of the cycle flag (Z-tes) during normal driving operation in the field
- No O.K. message in case of a defective PCV under all practically conceivable driving situations and ambient conditions

What is a defective PCV?

- A PCV, which is completely closed or which is blocked
- A PCV, which is jammed while fully open and which allows for no or only a minimum controllability of the flow rate
- A PCV with an increased leakage (e.g. also up to 40% of the max. flow rate) is not reliably detected.
- A PCV, which shows a minor to medium blockage (open quantity only 60% of the max-value), is not reliably detected.

\* Certification possibilities at the authority: 1) PCV totally blocked resp. defective 2) PCV continuously fully open (jammed at open position)

The DTEV requires very intensive testing. The application requires a very good knowledge of the vehicle (especially knowledge of the "disturbing factors of the performance demand at idling"), of the purge control system and of the idle control.

The application phase will most probably at least take one man week. During all tests the DTEV should be "one topic". During the certification the DTEV should be watched in the exhaust test (fault simulation with open or blocked PCV). Is the setting of the cycle flag guaranteed in all cases?

## Preconditions for a DTEV application:

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Later changes of one of the mentioned functions can have an effect on the application of the DTEV!!!

- Charge sensing, idle control, torque structure, Lambda control and adaptation and all other important basic functions of the engine.
- Especially: Purge control function (%TEB) with the partial functions %BGTEV and %ATEV
- The canister system must be final (with possibly canister pressure valve, PCV, pipes...)
- Sequential control of the diagnostic functions (BBTEGA)

## Important cross-couplings to other functions:

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- DLDP: Input into DTEV are the bits B\_tevioi and B\_teviot (see DLDP)
- Idle control: The limits LIMNDTES and LIMN (LIMNV) and the time constant ZLIBG and the integration speed (IVDN resp. IVDNV), torque margin (KFMRES) !!!, resetting of the integrator dmlri\_w !!
- BGTEV: Entire function
- ATEV: Entire function
- TEB: Max. fuel rate, quick opening control time for DTEV
- On P-system: Characteristic MSNWDK, WDKMSN (or comparable maps) as well as interaction with BGMSZS dfuelsan\_w => dmsnte\_w
- On systems without ambient pressure sensor: Altitude adaptation fho\_w
- With Lambda control 2-step: The control parameters (P and I component of the Lambda control can be increased at active DTEV)



Timing around the DTEV:  
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The DTEV possesses a passive part and an active part

"- The passive part is again subdivided into the parts:"

- a) Determination of mixture pilot control with closed PCV O.K. (during a mixture adaptation phase at idling) => B\_dtepm
- b) Check whether purge control purges with high fuel rate outside of idling (in one of the successive purge control phases)

=> Condition DTEV passive possible during first mixture adaptation phase (TTEGAINI)  
=> Condition PCV O.K. passive in successive purge control phase, once the ACF has a certain HC charge.

- The active part is blocked for the time TDTEZAM (typical value for FTP = 590 s) after start.  
The active check is furthermore only allowed if sufficient purging was performed immediately before the DTEV (imsteini > threshold). This is necessary since it must be ensured that there is always a continuous HC concentration in the pipe PCV-ACF when the PCV is controlled open. Other diagnostic functions can also block the opening control check (DLDP, DDMTL, DLLR).
- When the active check is enabled (B\_dtezam) at first an idle phase is waited for. Only once the vehicle is at rest while idling for longer than TVDTEVZ (e.g. 2 s) is the quick PCV closing control requested.
- The request for the opening control check (B\_dteaa) starts only once the vehicle is at rest during idling for longer than the time TVDTELLA (e.g. 2 s). With a low degree of saturation and if e.g. a typically long idle phase lies in the exhaust test (TDTESZU <= time after start <= TDTESZO) the purge rate is immediately controlled down with "snap off throttle". Then no valuable time is lost for the PCV closing control.  
Remark: In M4, M5 systems an additional mixture adaptation phase was necessary prior to the DTEV, this no longer applies here.
- The actual PCV opening control only takes place once it is detected that the idle control has stabilized or once a maximum time has elapsed (TTEVAZ).
- So as to be able to make an O.K. or defect-statement also in case of stoichiometric mixture, the PCV check needs at least 12 s - 15 s. Together with waiting time at idling and stabilization time of the controller the total check needs an idle phase of 15 s - 20 s ! Due to the reduced control speed in the two-step control the opening control can be performed slower only. The control parameters (P and I component of the Lambda control) can be increased here at active DTEV => %LR.

The individual labels separated according to partial functions:  
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A detailed description is attached to the data suggestion for critical labels and for labels to be adjusted project-specifically. Where no additional remarks are mentioned the suggestion should only be deviated from after querying.

Always three values are mentioned:

[sensible lower value .... value recommended according to current level of knowledge ... sensible upper value]

"- Partial function DTEVSIGA: Signal conditioning"

- Filter time constant for frmit\_w: Variable: ZFRMFIL [0.2s ... 0.5s ... 1s] continuous Lambda control
  - Filter time constant for frmit\_w: Variable: ZFRMFIL [0.4s ... 0.8s ... 1.5s] 2-step Lambda control
  - Filter time constant for frmxa\_w: Variable: ZFRMXAF [5s ... 8s ... 10s] continuous Lambda control
  - Filter time constant for frmxa\_w: Variable: ZFRMXAF [4s ... 6s ... 8s] 2-step Lambda control
- ZFRMXAF is not much larger than TVDTEVPM, but not too small so that a short-termed frm deviation does not cause a resetting of B\_dtepm. Also adjust in connection with thresholds FRMDPMU, FRMDPMO.

"- Partial function DTEVEB: Switch-on conditions"

- TMDTEU: Engine temperature threshold DTEV: [60°C ... 70°C ... 80°C]  
Activation during warm-up is not permitted since the engine friction steadily decreases here. It would impede the detection of a defective PCV or it would lead to an erroneous O.K. message. This threshold also applies during the quick test !!!
- Introduction of a threshold for engine start temperature was refrained from! During cold tests it must be ensured that when activating the DTEV as from TDTEZAM after engine start a PCV, which was possibly at first iced, has "defrosted" by means of current input during TEB operation !!!
- FHODTEA: Deactivation threshold when driving at high altitude: [0.70 ... 0.72 ... 0.74]: With mounted altitude sensor (diagnosis must work reliably at 2440 m above sea-level!!!) [0.65 ... 0.68 ... 0.70]: At altitudes above altitude adaptation tolerance!!!

"- Partial function DTEVEB: Passive check switch-on condition"

- Lower rkat-threshold for enabling of passive diagnosis possible: RKADTEVU [RKATR ... -5% ... -3%] remark: RKATR comes from %LRA
- Upper rkat-threshold for enabling of passive diagnosis possible: RKADTEVO [3% ... 5% ... -RKATMX] remark: RKATMX comes from %LRA
- Air mass threshold for enabling of diagnosis passive possible: MLDTEFPF [15 kg/h ... 30 kg/h ... 40 kg/h]  
Basic idea: The check should be performed at idling with all possible consumers.  
The expansion of the check to the "range close to idle" => MLDTEFPF up to max. 60 kg/h is in principle also conceivable.  
Here, however, it is quite possible that a PCV jamming at the open position is erroneously detected as being O.K. when the ACF is at first not saturated but then becomes increasingly saturated!  
Attention: Threshold should in any case be higher than the highest idle air demand !!! Otherwise there is no passive O.K. !!!
- Lower frm-threshold for enabling of diagnosis passive possible: FRMDPMU [0.85 ... 0.88 ... 0.93]
- Upper frm-threshold for enabling of diagnosis passive possible: FRMDPMO [1.07 ... 1.12 ... 1.15]
- Debounce time for setting of flip-flop B\_dtepm: TVDTEVPM [ 5 s ... 8 s ... 10 s]



"- Partial function DTEVAEB: Active check switch-on condition"

- \* Important label for application phase / Series production: CWDTEAPP [Bit 0] - Code word for permanent DTEV  
In the series production bit 0 of CWDTEAPP must be = FALSE !!!!!!!  
In the application phase it is possible to request a continuously repeated activation of the DTEV: Bit 0 = TRUE  
Thereby the system is immediately active again after an O.K. check, without the engine having to be turned off!!!
- Time from engine start, as from when the opening control check DTEV can become active for the first time: TDTEZAM:  
For FTP 75: [590s]  
For ECE: [?]  
For application phase: [5s ... 10s] so that DTEV can become active immediately after engine start.
- Time from engine start for diagnosis active with quick trip: TDTEFA [30s... 45s...60s]:  
Attention: Set TDTEFA to that value, where the course of ml\_w is stable after an engine start. It can be observed that the air mass at first decreases also after a warm start.
- Cycle duration for repeated operation: TPERDTE: [2s ... 5s .... 25.5s]: Only important for application phase !!
- Number of terminated opening control checks DTEV: APDTEVX [2]  
Remark: By the law max. 2 trials for series production, for application purposes it can be chosen much greater. When mounting a defective PCV it can be checked, whether erroneous O.K. detections occur and how often !!! => then APDTEVX = 255 !
- Number of aborted opening control checks DTEV: AVDTEVX: [3 ...5...20]  
The number of trials are limited so that with according driving (only very short idle phases) the mixture adaptation or the purge control is not interrupted "for ages". During the application phase much larger values are possible.
- Threshold integral purge flow for enabling of (IMSDEVA): On systems with a short pipe ACF-PCV it can be adjusted to zero. On systems where the pipe ACF-PCV is longer than 70 cm a purging phase should take place immediately before the DTEV. The variable imsteini (integral purge mass flow since last purge break) is scanned from the TEB for this. Only once this integral has exceeded a certain value (e.g. volume of the pipe ACF-PCV) may the active check DTEV be started.  
Reason: An HC front could just be reaching the PCV after a longer purge break when it is completely opened by the DTEV.  
Suggestion IMSDEVA: [0.5g < 1 g < 4g]

"- Partial function DTEVP: Passive DTEV"

- Lower ftead-threshold for passive diagnosis: FTEADDP: [3 ... 5 ... 7]
- Upper ftead-threshold for passive diagnosis: FTEADDP: [30 ... 32 ... 35]  
The scanning of an upper threshold shall prevent that a PCV jamming at the open position can cause an O.K. A PCV jamming at the open position leads as from certain saturation and at low and medium air masses to a MAX limit stop of the saturation [37.5].
- Fuel rate purge control for passive diagnosis: FKADPMN: [0.15 ... 0.20 ... 0.25] : 0.15 only if MLDTEPF > idle air mass
- Lower frm-threshold for passive diagnosis: FRMDTEVU [0.9 ... 0.92 ... 0.94]
- Upper frm-threshold for passive diagnosis: FRMDTEVO [1.06 ... 1.08 ... 1.10]  
By these fr-thresholds all those cases are excluded, during which the PCV is not controllable (e.g. because it jams at the open position), so that a fr-course round 1.0 will practically not occur for a certain time at high saturation.
- Air mass threshold for diagnosis passive: MLDTEPF [30 kg/h ... 40 kg/h ...50 kg/h]  
A higher air mass flow than idle air mass is in principle demanded for O.K. detection.  
The expansion of the check to idling (MLDTEPF = 5 kg/h) is in principle also possible. Then, however, FKADPMN > 0.20 should be chosen. There is, however, a larger possibility that at activated O.K. detection during idling, a PCV jamming at the open position is erroneously detected as being O.K. with lesser saturated ACF.

"- Partial function DTEVZU: Closing control PCV for active diagnosis"

- Time from end of start for start of time window for immediate closing of PCV when B\_ll = TRUE: TDTEZSU: [990s] for FTP
- Time from end of start for end of time window for immediate closing of PCV when B\_ll = TRUE: TDTEZSO: [1050s] for FTP
- ECE-window: 650 s - 850 s (2 DTEV trials) or if no DLLR: 570s - 850 s (3 trials DTEV)
- Threshold saturation for immediate closing of PCV when B\_ll = TRUE, if B.gae = TRUE: FTEADSZ: [1...3...5]
- Delay time for closing of PCV as from idle at stand-still active: TVDTEVZ: [3s...5s...10s]
- Delay time for earliest start of active DTEV after idle at stand-still: TVDTELLA: [2 s... 3s ... 5s]

"- Partial function DTEVLR: Check of PCV via the Lambda control"

- Threshold fr-deviation toward lean for O.K. detection: DFRMDTEM: [0.06 ...0.07... 0.10]
- Threshold fr-deviation toward rich for O.K. detection: DFRMDTEF: [-0.10 ...-0.07... -0.06]
- Delta fr-threshold for detection "fr - stabilized": DFRMDTEE: [0.004 ...0.005...0.01]
- Time for check "fr - stabilized": TFRMDTEE: [0.3 s ...0.4 s .... 1s]
- Number of checks for stabilized: APDTEFRE: [3...5...8]
- Time for "compulsory stabilization": TTEVAZ: [4... 5...8]  
=> defined such that DTEV can definitely be successful via the "air check" during the longest idle phase of the test also if fr does not stabilize !



"- Partial functions DTEVLL and DTEVDML together: Check of PCV via the performance balance"

- Code word for switch-over HFM-system / P-system: CWDTEAPP Bit 1
- Bit1 = 0 => HFM-system !!! Pay attention, an incorrect application is not necessarily noticed !!!
- Bit1 = 1 => P-system

Remark: The evaluation can also take place via the throttle valve on an HFM-system (bit 1 = 1). This, however, is by no means recommended for the series production. Except maybe for the "trying out during the start-up". The tolerance with throttle valve evaluation (msndkoo\_w, fklaf\_w, fho\_w, and ftdvk) is distinctly higher !!!

- Threshold pulse duty cycle as from which the open-time of the PCV is counted. Simultaneously threshold for abort possible: TADTEMX: [30%..... 80% ....98%]
- Time threshold for the start of the evaluation of the performance balance: TVDTEB [1s ... 3s ...5s]
- Time threshold for the end of the evaluation of the performance balance: TVDTEE [TVDTEB + 1 s ... 5s ....8s]  
=> Checking time should at least be one second!!!
- Threshold ignition angle efficiency for abort DTEV: ETAZWTEN: [40% .. 50% ..60%]  
=> definitely lower than each etazwist measured under normal conditions during DTEV!!  
=> no abort during test !!
- Lower engine speed deviation for abort: DNDTEU [-100 rpm... -80 rpm... -50 rpm]: The more stable the idle, the narrower
- Upper engine speed deviation for abort: DNDTEO [50 rpm... 80 rpm... 100 rpm]: The more stable the idle, the narrower
- Abort when the generator excitation is changed: High-pass filter time constant ZDFDTE: [1 s... 1.5 s... 3s]  
Delta % for abort DDFDTEAB: [5%...10%...20%]
- RMSTEVIO: Diagnostic threshold for defective / O.K.
- To be adjusted together with DMLDTEFX (threshold for defect-check no longer possible) !  
The following facts result:  
Setting of B\_tevnio is no longer possible in case of an air mass decrease through the throttle valve by more than DMLDTEFX (e.g. 0.8 kg/h). Simultaneously RMSTEVIO decides on defective or O.K. RMSTEVIO is a relative value, so e.g. independent of altitude and temperature.  
A "dead range" between good and bad check develops. RMSTEVIO and DMLDTEFX should be matched to one another, in order to prevent this dead range from becoming wider than a certain width. This is to be calculated at standard pressure and temperature conditions.

"- Partial functions DTEVLL and DTEVDML together: Check of PCV via the performance balance"

Example: Small PCV: PCV max. flow rate 3.2 kg/h [at 1013 mbar and 0 °C]  
Threshold for defect-check: 0.8 kg/h => that means no defect above 25.00 %  
Threshold RMSTEVIO: 35% => no O.K below 35%  
=> Dead range: from 25.00% to 35.00%  
At 3000 m altitude: => Maximum flow rate: 2.24 kg/h  
Defect-detection only possible within 35.7% = 100% \* 0.8 / 2.24  
O.K. detection via RMSTEVIO as from 35%  
=> No more dead range !!

Large PCV: PCV max. flow rate 4.8 kg/h [at 1013 mbar and 0 °C]  
Threshold for defect-check: 1.0 kg/h => that means no defect above 20.08 %  
Threshold RMSTEVIO: 35% => no O.K below 35%  
=> Dead range: from 20.08% to 35%  
At 3000 m altitude: => Maximum flow rate: 3.36 kg/h  
Defect-detection only possible below 29.76% = 100% \* 1.0 / 3.36  
O.K. detection via RMSTEVIO as from 35%  
=> Dead range now only 5.24 % wide so between 29.76% and 35%

OBD-durability test: If a durability test is made for this test RMSTEVIO can be set to higher values to receive information about "tests with a low rmstevf result". Proposal: RMSTEVIO 45% - 55%

"- Map for correction of ignition angle efficiency: Default values map KFDETEATE: "

Important: To be adjusted only on an HFM-system ! The PCV air is measured in any case on a P-system !  
=> no fault with etazwist on P-system !!! => fill map with zero on P-system !!!

etazwist	0%	50%	75%	100%	
dmletanu	0.0 kg/h	0	0	0	0
	1.5 kg/h	0	0	0	0
	3.0 kg/h	30%	20%	10%	0
	4.5 kg/h	40%	25%	13%	0
	6.0 kg/h	45%	30%	16%	0
	7.5 kg/h	50%	35%	20%	0

Values for HFM-system !!!

"- Time constant for rltedte\_w formation: Default value ZRLTEDETE = 1s "



"- Partial functions DTEVLL and DTEVDML together: Check of PCV via performance balance"

- Application of the map KFDTEATE:

- Stage I
  - The map KFMRES is at first to be set to zero (no torque margin).
  - So that the throttle valve does not bottom at least one large as constant as possible consumer is to be activated (e.g. drive with automatic transmission). For the manual transmission this can possibly be the A/C.
  - The time TVDTEE is to be set to a high value (e.g. 25s), so that the PCV stays open for a long time.
  - Small quantities of HC are to be led from a butane bottle into a well-buffered ACF (if not given in the project, find a foreign ACF), so that at the output of the ACF a roughly stoichiometric mixture is obtained!
  - In this way it can be achieved that no O.K. is obtained via the fr. To support this ZFRMFIL can be set to a high value ( > 20 s).
  - The DTEV is to be switched to permanently active. An O.K. standard PCV is to be mounted. Monitor rmstevf\_w. Is a PCV quality of about 100% reached during the individual checks, (which after all take a long time now)?
  - Etazwist should at first be about 100% during the entire measuring period.
  - If rmstevf\_w considerably deviates from 100%, TATEMSN and MSNTATE are to be adjusted accordingly.
- => Target of this first stage: During each measurement rmstevf\_w reliably reaches about 100% +/- 15% !!!
- Stage II
  - Now a torque margin KFMRES is set, which results in an efficiency etazwist of about 75% (e.g. 3% - 4% in KFMRES).
  - Consumers should be maintained (Drive still engaged)
  - The DTEV is again activated. How large is rmstevf\_w ? Are 100% still reached, is it more or less? If less, decrease the values in the third column of above-mentioned map. If more than 100% is indicated, the values must be increased accordingly.
  - The same needs to be performed for the higher torque margin (etazwist = 50%). The lowest base point of the source etazwist is to be extrapolated!
  - Repetition for "partially blocked PCV": The values for dmletan\_u = 3.0 kg/h can be repeated with a small PCV (e.g. 3.0 kg/h instead of e.g. 4.8 kg/h) for a very exact application. Now e.g. 62% rmstevf\_w must be reached consistently.
- Stage III
  - Checking: Now all consumers are to be switched off and the usual torque margin is to be adjusted.
  - The checking time DTEV is still to be kept high (25 s PCV completely open)
  - If 100% are still reached with O.K. PCV, then the application is correct. The above measurements should be repeated in case of deviations of more than 20%. A 3 kg/h PCV should now too come to about rmstevf\_w = 62%.

- Filter time constants: ZMSTEDTE and ZMLETAN:

- ZMSTEDTE should be chosen slightly greater than ZMLETAN, so that the time delay of the "answer" of the idle control is more or less taken into consideration in the filtered expectation value "mstedtef\_w".
- ZMLETAN [1 s.....1.5 s.....3 s]
- ZMSTEDTE [1.5 s...2.0 s....4 s]

- Upper threshold relative PCV quality: RMSTEVXM: [150% ... 170% .... 199%]

- Lower threshold relative PCV quality: RMSTEVNM [-80% ... -50% .... -30%]

This expansion beyond the plausible value range [0... 120%] is necessary, so that the deactivation of disturbances will also work with small values of mstedtef. If the range is too narrow, an abort will frequently terminate the function!!!

- DTEVLL and DTEVDML together: Check of PCV via the performance balance

The air mass thresholds for "defect-check no longer possible" and for "abort" should now be adjusted in form of a package together with the integrator speed KIRMSMS:

- Threshold for defect-check no longer possible: DMLDTEFX: [0.5 kg/h ...0.7 kg/h ...0.8 kg/h]
- Threshold for defect-check no longer possible => abort: DMLDTEFN: [-0.8 kg/h ...-0.7 kg/h ...-0.5 kg/h]
- Upper threshold for abort due to disturbing factors: DMLDTEMX: [0.4 kg/h ...0.6 kg/h ...1.0 kg/h]
- Lower threshold for abort due to disturbing factors: DMLDTEFN: [-1.0 kg/h ...-0.6 kg/h ...-0.4 kg/h]

- Integrator speed for re-adjustment rmstevf\_w : Default values characteristic KIRMSMS:

mstedte	0	0.5 kg/h	2 kg/h	5 kg/h	
Value	1000	200	60	30	%/ [kg/h*s]

=> The following applies here:

- The faster the integrator, the smaller the deviations of dmletan\_w and dmletanf\_w and thus the lower the abort tendency of the DTEV (also with small disturbing factors)
- The higher the absolute value of the thresholds, the lower the abort tendency but also the lower the protection against disturbing factors.

=> Intensive testing by simulation of all possible disturbing factors is demanded!

- Abort with disturbing factors, which influence the PCV quality by more than +/- 25% -> +/- 30 %
- Reliable passing of the exhaust test ! No abort allowed without "self-inflicted" disturbing factors (e.g. power steering, power-window control)!!!

"- Partial function DTEVRQ: Calculation of PCV quality"

- Time constant for filtering of PCV quality: [10 s... 20 s....40s]

The higher, the better is the PCV quality filtered and less noticeable do deviations become. Since, however, only a few checks are successful via an evaluation of the performance balance, this value should not be set too high.





"- Partial function DTEVTAT: Output of pulse duty cycle and reset of Lambda controller"  
Default values characteristic TADTEAMX:

- This is dependent on whether a continuous or a two-step Lambda control exists. The opening control characteristic TADTEAMX is to be adjusted correspondingly faster or slower. In the process the highest ACF saturation must be taken as orientation. The Lambda deviation should not exceed more than 15%!
- Very important, however, is that the entire checking time of the DTEV does not exceed the time available in the exhaust test!  
FTP: approx. 24 s  
ECE: approx. 20 s  
It must be assumed that "only" stoichiometric mixture comes. Also the detection of a defective PCV needs the longest time.  
=> Application of TVDTEE !!
- Suggestion for continuous control:

tdtesta	0	1	2	3	4	5	6	7	8	9	10	12	18	25.5	s
TADTEAMX	0	3	4	5	10	15	25	40	65	100	100	100	100	100	%

Default values map KFTVFRR: Delay for fr reset!

tadteazs		10%	30%	60%	100%
ml	12 kg/h	1.0	0.9	0.8	0.7 Sec
	20 kg/h	0.9	0.8	0.7	0.5 Sec
	60 kg/h	0.4	0.3	0.2	0.1 Sec

- => If the PCV could be opened up to higher pulse duty cycles without this process being terminated by fr, then the saturation was not high. It has shown that the fr-reset then needs to be delayed less.  
If the PCV closes already at small pulse duty cycles a high saturation existed, the fr must then only be reset later.
- => The reset is distinctly shortened with high air masses, since the throttle valve was opened, this resulting in the intake manifold being free of HC more quickly.

TVDTEABG: Period for fr-reset !

=> The fr can be held at its reset value for some 100 ms [100 ms ... 300 ms ... 600 ms]

=> Checking of the reset delay and of the reset duration with Lambda measurement! Target being to keep Lambda deviations low at all degrees of saturation.

KIDMSNTE: Integration speed for output variable dmsnte\_w from dfuelsan\_w = (1 - rlmod\_w/rl\_w):  
[0.5kg/h / s ... 2kg/h / s ... 4 kg/h / s]

The PCV air mass flow should be learned fast enough when the PCV is controlled open.

DMSNTEMX: Maximum value for adapted PCV air mass flow: for Bosch PCV2 [5 kg/h ... 6 kg/h...8 kg/h]

DMSNTEMN: Minimum value for adapted PCV air mass flow: for Bosch PCV2 [-3 kg/h ... -2 kg/h...-1 kg/h]

Negative values are permissible since even with a defective PCV a residual adaptation of the throttle valve leakage must still be possible.

"- Partial function DTEVAEND: Setting of the abort flag DTEV"

-> no label

"- Partial function DTEVEA: Fault treatment of DTEV"

- Threshold for detection defective open /defective closed: DMVTEVDO: [- 5% ... - 3% ...-2%]

The current value of the loss adaptation is taken as indication, whether

A) the PCV defectively jams at the open position

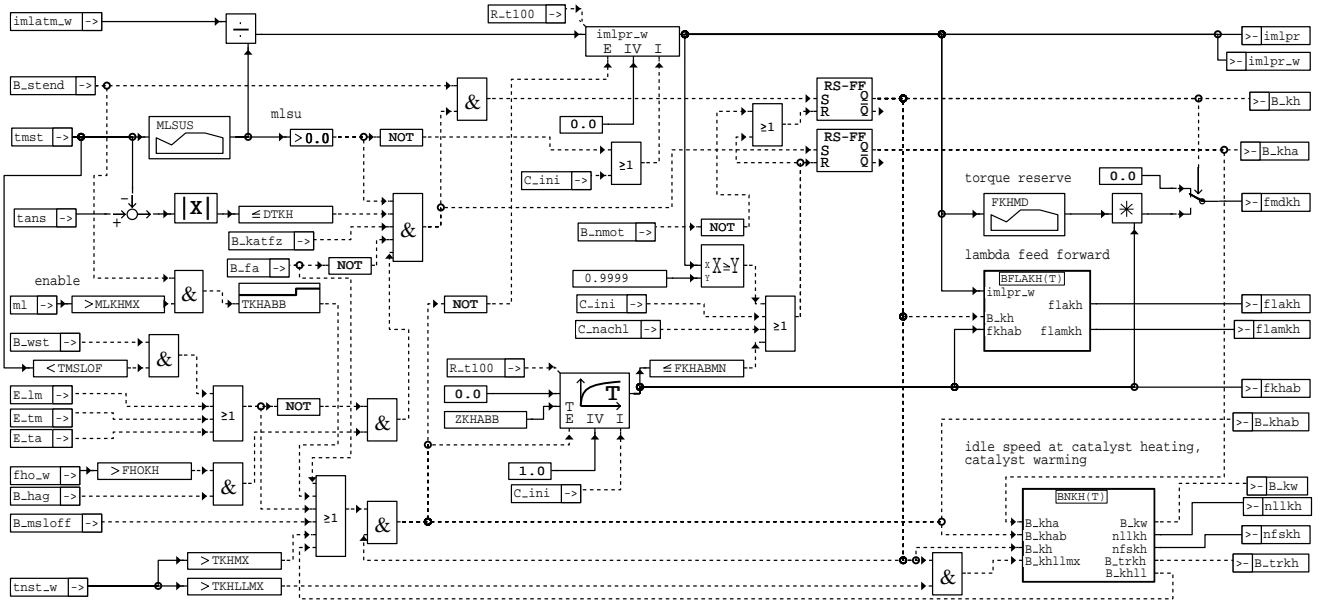
B) the PCV defectively jams at the closed position

With a PCV jamming at the open position the loss adaptation has learned the PCV leakage; dmvad\_w then has a distinctly negative value. This distinction does not work on a P-system, since dmvad\_w basically does not react if the PCV jams at the open position. The information can be found in msndko\_w on a P-system.

Remark: Also on an HFM-system it must be accepted that the information max-fault / min-fault is not very reliable in case of a torque loss pilot control that was not adjusted optimal.

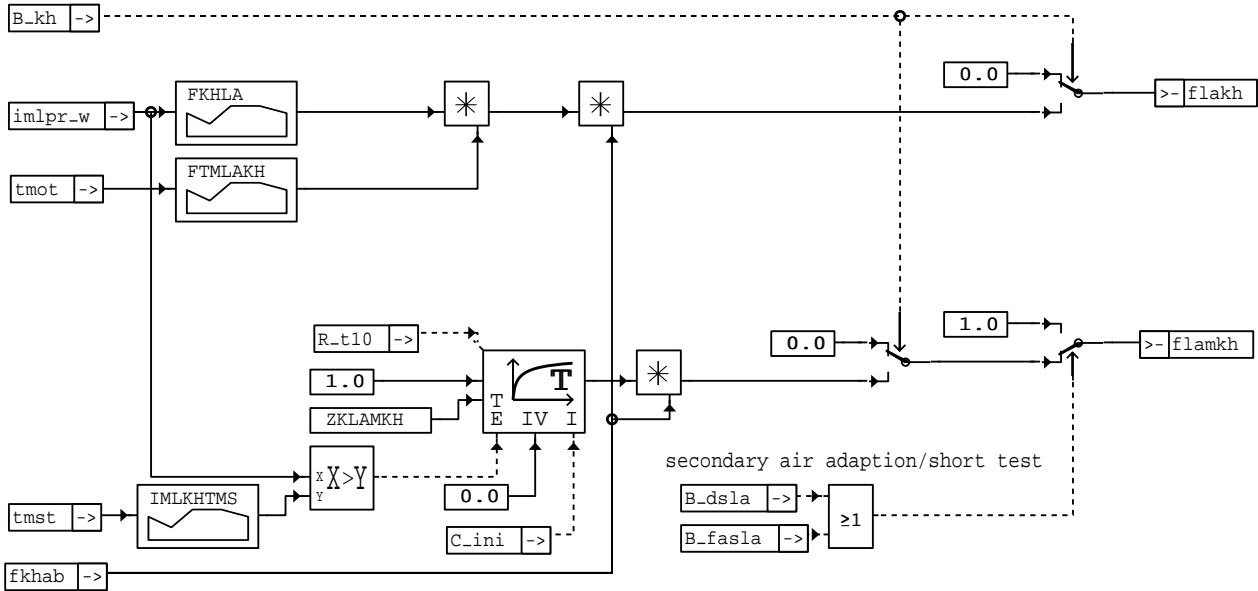
## BBKHZ 11.130 Control of catalyst heating

### FDEF BBKHZ 11.130 Function definition



#### bbkhz-bbkhz

BFLAKH: Calculation Lambda control



#### bbkhz-bflakh

BNKH: Calculation idle speed and keeping the catalyst warm





Variable	Source	Type	Description
B_SLSFZ	PROKON	EIN	condition: SLS fitted in vehicle
B_STEND	BBSTT	EIN	condition end of start
B_TRKH	BBKHZ	AUS	Flag for catalyst fast heating
B_WST	ESSTT	EIN	condition for re-start
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_NACHL		EIN	ECU condition for ECU switch off delay
E_LM	EGFE	EIN	Error flag: main load sensor
E_TA	GGTFA	EIN	error flag: TANS
E_TM	GGTFM	EIN	Error flag: engine temperature tmot
FHO_W	BGPU	EIN	correction factor: altitude
FKHAB	BBKHZ	AUS	terminating factor catalyst heating
FLAKH	BBKHZ	AUS	Factor control lambda at catalyst heating
FLAMKH	BBKHZ	AUS	factor setting up lambda engine nominal at catalyst heating
FMDKH	BBKHZ	AUS	Weighting factor torque reserve for catalyst heating
IMLATM_W	ATM	EIN	integrated air mass flow from engine start to max. value (word)
IMLPR	BBKHZ	AUS	relative amount of integrated air mass flow at catalyst heating
IMLPR_W	BBKHZ	AUS	relative amount of integrated air mass at catalyst heating (word)
ML	SWADAP	EIN	air mass flow
MLSU	BBKHZ	LOK	nominal air mass for catalyst heating
NFSKH	BBKHZ	AUS	Idling speed driving level for catalyzer heating
NLLKH	BBKHZ	AUS	Idling speed for catalyzer heating
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
TANS	SWADAP	EIN	Intake air temperature
TKATM	ATM	EIN	catalyst temperature (model)
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
TNST_W	BBSTT	EIN	time after end of start

### FW BBKHZ 11.130 Fixed Values

Parameter	Value	Description
CWKHZ		code word for catalyzer heating control
DNKH		
DTKATMN		Hysteresis catalyst temperature control threshold for catalyst warming
DTKH		absolute value difference (tans -tmst) for catalyst heating
FHOKH		minimum altitude threshold to enable catalyst heating
FKHABMN		threshold terminating factor catalyst heating
MLKHMx		max. air flow for catalyst heating
NLLKT		Nominal idle speed at short test of SAI-system
TKATMN		Catalyst temperature control threshold for catalyst warming
TKATW		Catalyst temperature threshold for catalyst warming
TKHABB		delay time switching off catalyst heating
TKHFSAB		delay time switching to idle speed at drive at catalyst heating
TKHLL		cancelling time catalyst heating idle speed
TKHLLAB		delay time switching off increased idle speed at catalyst heating
TKHLLMX		Maximum time for increased catalyst heating idle speed
TKHMX		maximum time for active catalyst heating
TMSLOF		threshold of engine temperature for disabled secondary air
ZKHABB		Time constant for abort low-pass catalyzer heating
ZKLAMKH		time constant lambda engine nominal at catalyst heating



## FB BBKHZ 11.130 Detailed description of function

The catalyst heating function coordinates the actions:

- \* KHMD: Torque margin for the specific increase of the exhaust gas temperature by retarded ignition,
- \* LAKH, LAMKO: mixture control,
- \* desired idle speed and
- \* SLS: Secondary air injection

for the faster heating of the catalyst after start.

Switch-on, switch-off condition:

The catalyst heating function is only released by the condition  $B\_katfz = 1$  from %Prokon and activated by default selection of the desired intake air mass  $mlsu > 0$  dependent on the engine temperature at start  $tmst$  as from end of start ( $B\_kh = 1$ ). Here the intake air mass describes the quantity of heat in the exhaust pipe, which is necessary to warm up the catalyst.

The control is performed by the heating progress in percent  $imlpr$  by relating the air mass put through since end of start ( $B\_stend$ )  $imlatm\_w$  to the desired air mass  $mlsu$  from the characteristic  $MLSUS = f(tmst)$ .

Additionally the intake air temperature  $tans$  must lie close to the engine temperature at start due to  $(tmst - tans) < DTKH$ .

The quantity of heat necessary for the warming-up of the catalyst is reached if the desired air mass was put through the engine and if  $imlpr = 0.9999$  is reached.

In case of repeated start ( $B\_wst = 1$ ) at an engine temperature at start  $tmst < TMLOF$  catalyst heating is blocked, in order to avoid an undesired switching on of the possibly still frozen secondary air system.

Catalyst heating is only activated if the altitude factor  $fho\_w$  exceeds the threshold  $FHOKH$  and if the altitude information ( $B\_hag = 1$ ) is valid.

Torque margin:

Dependent on  $imlpr$  the torque margin is assessed by  $fmdkh$  from the characteristic line  $FKHMD$ . The increasing control from 0 to 0.9961 is performed dependent on  $imlpr$ . By a delayed decreasing control of the torque margin after end of start by means of a suitable definition of the  $imlpr$  base points and of the assessment factor it is possible to ensure that a sufficient vacuum of the vacuum system, the power brake unit is obtained. The decreasing control is performed by an assessment by the value 0 at the base point  $imlpr = 0.9999$ .

Mixture control:

The mixture control takes place by the assessment factor  $flakh$  from the characteristic line  $FKHLA$  by an increasing control from 0 -> 0.9961 and a decreasing control to 0 dependent on  $imlpr$ , analogous to the torque margin. Additionally it is possible to assess the Lambda catalyst heating weight  $flakh$   $tmot$ -dependent by  $FTMLAKH$ . The filtered increasing control with the time constant  $ZKLMKH$  to  $lamkh$  takes place in %LAMKO by the factor  $flamkh$  after the  $imlpr$  threshold value from  $IMLKHTMS$ , which is dependent on  $tmst$  (without interpolation!), so as to achieve a coupling to the after-start mixture control. An abort of the catalyst heating leads back to the Lambda after-start warm-up input  $lamnswl$ .

Desired idle speed:

The desired idle speed is obtained by an entry into the  $tmot$ -dependent characteristic lines  $NLLKHM$  and  $NFSKHM$  when the automatic gear box is in gear. For comfort reasons an irreversible switch-over to the input from  $NFSKHM$  is performed by shifting into gear. In addition the increased catalyst heating speed after start and after the time  $TKHLLMX$  was exceeded can be terminated by means of the code word  $CWKHZ.0$ .

Secondary air control:

The secondary air control is performed by the evaluation of  $imlpr$  in the separate secondary air control. By means of the bit  $B\_kha$  the secondary air can, dependent on the electrical system, be activated already during start, as is described in the secondary air control. An abort of the secondary air  $B\_slpoff = 1$  also leads to an abort of the catalyst heating. The abort can optionally be stopped by  $B\_lpoff = 1$  by the setting of  $CWKHZ.6$ .

Abort of catalyst heating:

The abort of the catalyst heating ( $B\_khab = 1$ ) is performed by a debounced exceeding of the max. intake air mass  $MLKHMx$  in case of an error of the main load signal  $E\_lm$ , in case of an error of the engine or intake air temperature sensor  $E\_tm$ ,  $E\_ta$ , or if the permitted catalyst heating time  $TKHMx$  is exceeded. (On secondary air systems this complies to the permitted switch-on duration of the secondary air pump). The abort condition  $B\_slpoff = 1$  from %SLS also aborts the catalyst heating (optional: dependent on  $CWKHZ.6$ ). With abort of catalyst heating the heating progress in percent  $imlpr$  is frozen. The catalyst heating actions are controlled down with the time constant  $ZKHABB$  by the decreasing control factor  $fkhhab$ . The catalyst heating function is stopped ( $B\_kh = 0$ ) once the threshold  $FKHABMN$  is reached. With uninterrupted idling since engine start the catalyst heating is also stopped after the time  $TKHLL$  was reached.

Keeping the catalyst warm:

With a warm catalyst it is possible to adjust the mode "keep catalyst warm, temporary" ( $B\_kw = 1$ ) dependent on the catalyst temperature  $tkatm$  after the temperature threshold  $TKATW$  was exceeded once. For this the desired engine speed  $nllkh$  from  $NLLKHM$  is increased between  $TKATMN$  and  $TKATMN + DTKATMN$  also in case of higher engine temperatures. The increase in engine speed, when the vehicle is in gear  $nfskh$ , is determined by the characteristic line  $NFSKHM$ . (Attention: On vehicles with automatic gear box the increase in engine speed in  $NFSKHM$  must be adjusted carefully in order to avoid an undesired rolling away of the vehicle, e.g. with insufficient operating of the parking brake.) To increase the performance loss in the exhaust pipe additionally an own torque margin can be activated from  $KFKWTMP$ .

Secondary air adaptation/quicktrip:

By  $B\_dsla$  from the secondary air diagnosis or by  $B\_fasla$  from %SLS the secondary air adaptation phase resp. the quicktest is requested. In the Lambda input selection  $BFLAKH$  the evaluation factor  $flamkh$  is then switched to 1, i.e. Lambda catalyst heating input  $lamkh$  in %LAKH. By  $B\_fasla$  from the tester request the engine speed input  $NLLKT$  is additionally activated.

Note:

The bit  $B\_khlll$  is also generated outside of catalyst heating, however, it is only of significance during catalyst heating ( $B\_kh = 1$ ). The bit  $B\_trkh$  serves to request the accelerated Lambda sensor heating. Dependent on the sensor mounting position and on the amount of condensate it is possible to couple the bit  $B\_trkh$  to catalyst heating by  $CWKHZ.0$ , otherwise a reset will be performed when idling is left, when the drive is shifted to and so on.





## ABK KHMD 1.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWKHMD			FW	code word for torque reserve in catalyzer heating
FMDKHFH	FHO_W		KL	altitude correction of torque reserve for catalyst heating
FMDKHTM	TMOT		KL	tmot-correction of torque reserve for catalyst heating
KFKWTMP	NMOT_W	MIFAKH_W	KF	Characteristic torque reserve for keeping catalyst warm, temporary
KFMDDSLA	NMOT_W	MIFAKH_W	KF	Map torque reserve at tester demand of SAI-diagnosis short test
KFMDKH	NMOT_W	MIFAKH_W	KF	Characteristic torque reserve for catalyst heating

Variable	Source	Type	Description
B_FASLA		EIN	Condition: external request of SAI system aktiv
B_KH	BBKHZ	EIN	condition catalyst heating activated
B_KW	BBKHZ	EIN	Condition catalyst warming
DMLLRI_W	LLRRM	EIN	desired torque change from the idle speed control (I-)
DMRDSL_W	KHMD	AUS	Torque reserve for SAI- diagnosis
DMRKH	KHMD	AUS	torque reserve for catalyzer heating
DMRKH_Z_W	KHMD	LOK	Torque reserve for catalyst heating
DMRKH_W	KHMD	AUS	Torque reserve for catalyst heating
DRKWTMP_W	KHMD	LOK	Torque for keeping catalyst warm, temporary
FHO_W	BGPU	EIN	correction factor: altitude
FMDKH	BBKHZ	EIN	Weighting factor torque reserve for catalyst heating
FMKHFHO_W	KHMD	LOK	Altitude correction of torque reserve at catalyst heating
FMKHTM	KHMD	LOK	tmot-correction of torque reserve at catalyst heating
MIFAKH_W	KHMD	LOK	desired indicated engine torque at catalyst heating
MIFA_W	MSF	EIN	desired indicated engine torque
NMOT_W	SWADAP	EIN	engine speed
TMOT	SWADAP	EIN	Engine temperature

## FW KHMD 1.50 Fixed Values

Parameter	Value	Description
CWKHMD		code word for torque reserve in catalyzer heating

## FB KHMD 1.50 Detailed description of function

So as to heat up the catalyst quicker resp. to keep it warm, the engine performance is deliberately reduced and therewith the exhaust-gas temperature is increased.  
For this, the torque margin dmrkh is taken into account in the function %MDKOL, which causes the charge to be increased and the ignition angle to be retarded.

A distinction is made between "catalyst heating" dmrkhz and "keeping catalyst warm, temporarily" drkwtmp:

### Catalyst heating:

The torque margin dmrkhz only has an effect while catalyst heating (B\_kh = 1) is active. The control is performed from %BBKHZ by fmdkh. In order to ensure the performance at altitudes and the build-up of a vacuum for the brake, the torque margin can be evaluated altitude-dependent (FMDKHFH). The build-up of a vacuum when starting the engine is to be ensured by an increasing control of fmdkh 0 -> 1 in %BBKHZ. So as to expand the catalyst heating range, a tmot-dependent evaluation of the torque margin is possible.

### Keeping the catalyst warm:

A temporary "keeping catalyst warm, temporarily" (B\_kw) can be realized by the temporary torque margin drkwtmp from the map KFKWTMP dependent on the catalyst temperature tkatm from %ATM.

The resulting torque margin dmrkh\_w is obtained by a max-selection from dmrkhz\_w and drkwtmp.

By the code word CWKHMD, bit 0 it is possible to optionally deactivate the idle intervention dmlri\_w in the addressing of the torque margin by mifakh\_w = (mifa\_w - dmlri\_w), e.g. in case of steep gradients in KFMDKH in the idling region.

### Quick-trip for the secondary air diagnosis:

By an input selection of the torque margin KFMDDSLA at tester intervention (B\_fasla), it is possible to adjust the desired intake air mass for the secondary air diagnosis. (Also refer to %SLS.) For this, the necessary torque margin dmrdsls\_w is transferred to %MDTRIP from the map KFMDDSLA.

## APP KHMD 1.50 Application hint

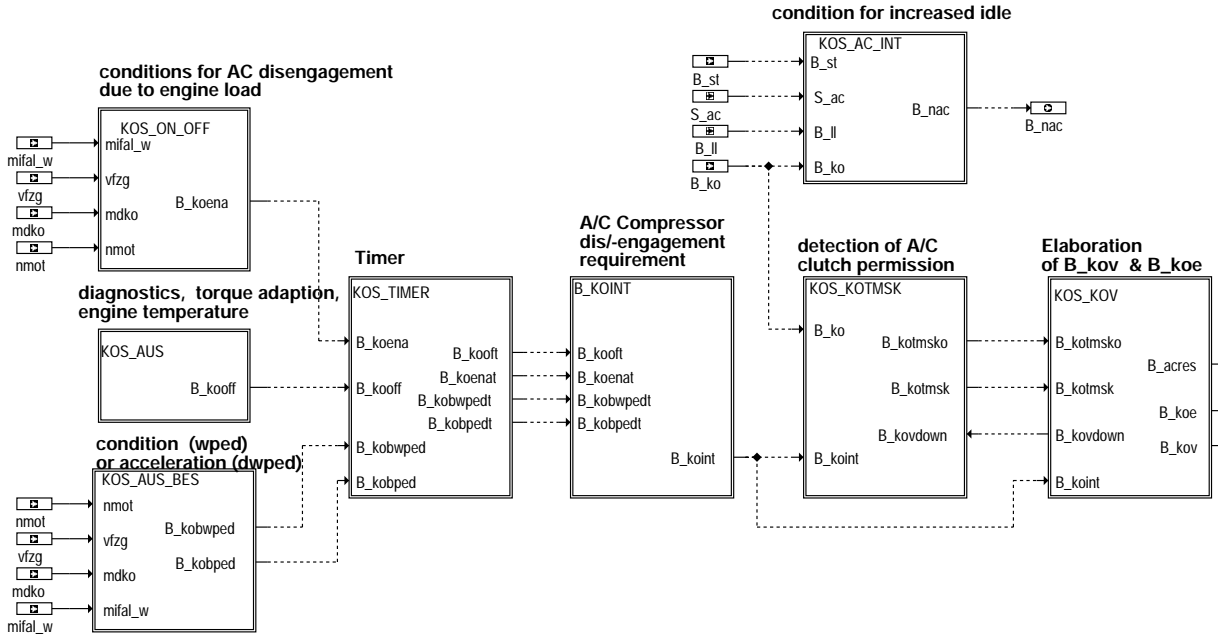
Preconditions: Application of torque margin coordination (%MDUE)

Suggestion for presetting:

- KFMDKH: Base point distribution for intended catalyst heating operating range, decreasing control of the torque margin with increasing driver's request mifa to start from rest most efficiently. Preset with 0, application of the torque margin e.g. from the necessary performance loss for catalyst heating.
- FMDKHFH: Altitude-dependent evaluation of the torque margin, preset with 1.0
- FMDKHTM: tmot- dependent evaluation of the torque margin, preset with 1.0
- KFKWTMP: Base point distribution for idle and for operating ranges close to idle, in which the catalyst cools down when being in these ranges for longer. Preset with 0.
- KFMDDSLA: Base point distribution for secondary air diagnosis at tester intervention. Preset with 0.
- CWKHMD: 0

## KOS 113.140 Control of A/C compressor

### FDEF KOS 113.140 Function definition



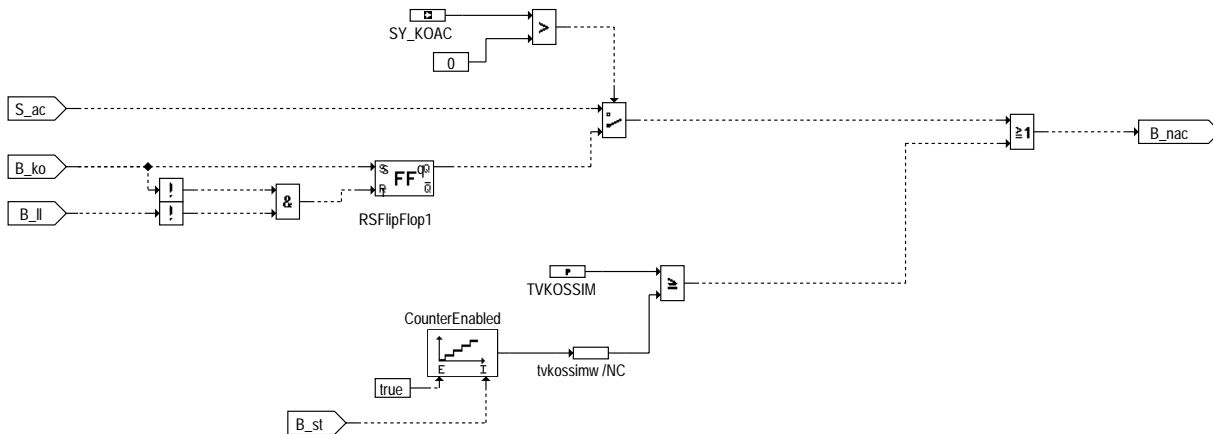
kos-kos

General view of the AC-compressor control

The AC-compressor control is divided into four parts. These parts are:

- KOS.AC.INTERF : Software interface between the external signals from the AC-control and the Motronic
- KOS.ON.OFF : Conditions for swiching the compressor on or off depending of the engine operating conditions
- KOS.TIMER : Scheduler for the swiching-on and -off times of the compressor
- KOS.MANAGER : Controller for the compressor, decides if the compressor has to be swiched on or off in dependence of the informations from the above listed functions

### Condition for increased idle-speed



kos-kos-ac-int



Software interface between the external signals of the AC-control and the Motronic:

(This subfunction is specific for each project)

The AC-control delivers two informations in the form of an on/off-signal:

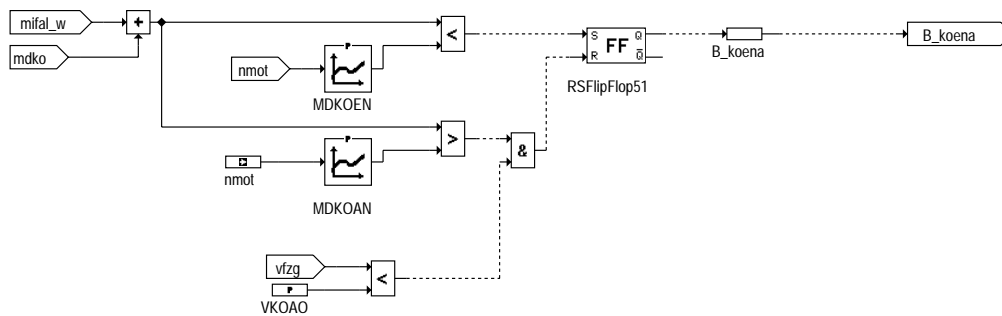
Inputs from the AC-control:

- S<sub>ac</sub> : Swich AC-stand-by, is equal to the wish of an accelerated idling
- S<sub>ko</sub> : Swich AC-compressor, is equal to the wish of having the compressor on

Outputs of the interface:

- B<sub>nac</sub> : Condition for an accelerated idling, see %LLRNS
- B<sub>ko</sub> : Condition AC needs the compressor

### A/C Clutch disengagement due to torque



### kos-kos-on-off

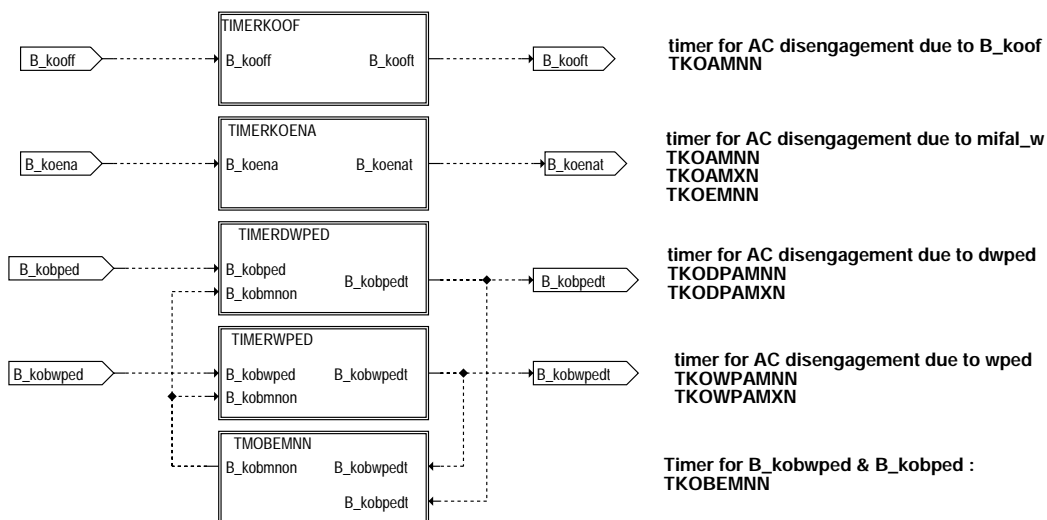
Engine dependant conditions to swich the AC-compressor on or off:

The compressor remains in any way swiched off for the time TNSTKO after engine start. In normal use the compressor is disabled or swiched off only if he is the reason for an insuffisant torque at the clutch. This is the case if the sum of the desired torque by the driver mifal and the compressor load-torque mdko is geather than the maximal torque that the engine can deliver. This limit sum is stored into the caracteristic line MDKOAN. The compressor is enabled again if the sum mifal+mdko becomes less than the limit MDKOEEN.

If the engine coolant temperature exceeds the limit TMKOAO or is less than TMKOAU, the compressor is swiched off. The output B.kooff disables the compressor time independantly.

For several diagnostic functions it is important that the compressor state remains unchanged for the time this functions are active because they need the reactions of the torque controller. Therefore torque jumps have to be avoided. The output B.kosta freezes the actual compressor state. It is actually unused and therefore set to false.

### Timer for for B\_kooff, B\_koena, B\_kopped & B\_kobwped



### kos-kos-timer



Sheduling the minimal an maximal compressor state times:  
-----

In dependance of the engine speed, the following compressor state times can be determined:

- "- TKOAMNN : Minimal compressor off time; the compressor remains swiched off at least for this time before he could be swiched" on again.
- "- TKOEMNN : Minimal compressor on time; the compressor remains swiched on at least for this time before he could be swiched" off again.
- "- TKOAMXN : Maximal compressor off time; the compressor is swiched on again if he has been swiched off for a time greather" then TKOAMXN

The times TKOAMNN and TKOEMNN are used to prevent the compressor cluch from to often changing the swich state.  
The time TKOAMXN avoids a permanent swich off of the compressor if the engine ist permanently used in an point where the compressor is disabled. It assures that the AC could work.  
If the time TKOAMXN is set above the limit LIMTKOA, the compressor will never be swiched on by the time scheduler.

Compressor-control - manager of the different informations:  
-----

The manager decides in dependance of the input signals if the compressor will be swiched on or off.  
Additionally the manager controles the swiching on and off of the compressor.  
The condition B\_ko has the highest priority. The compressor control enables or disables the compressor.  
The compressor is enabled if the engine allows the compressor load (B\_koena = 1) or the compressor has been swiched off for a too long time (B\_komxoff = 1) and an minimal off time has elapsed (B\_komnoff = 1)  
The compressor is disabled if if the engine doesn't allow the compressor (B\_koena = 0) and the compressor is operating since at least a minimal time (B\_komnon = 1).

The input B\_kooff swiches the compressor allways off independly of minimal or maximal on or off times.

The input B\_kosta freezes the actual compressor state.

The compressor is swiched on in two steps:

first step: B\_acres = 1, B\_koe = 0: the compressor remains still swiched off, the engine torque reserve is increased.

after the time TKOE:

second step: B\_acres = 0, B\_koe = 1: the compressor is swiched on, the torque reserve is reduced to the normal lower value.

The compressor is swiched off in one step:

B\_acres = 0 and B\_koe = 0: the compressor is swiched off.

Paralelly to the swiching on and off of the compressor the load torque is increased or decreased.

## ABK KOS 113.140 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDWGANG			FW	Gear detection for compressor shutdown at full throttle
CDWGANGB			FW	Gear detection during acceleration
CDWKOB			FW	Code word: Selection for gear detection for compr. shutdown (gangi or nmot/vfzw)
CWKOGANG			FW	configuration for transmission
DWPEDKOB			FW	gradient of the standardized accelerator pedal for the compressor
FHOKOB			FW	altitude threshold to enable the compressor
MDKOAB	NMOT		KL	Torque threshold to shut down the compressor during acceleration
MDKOAN	NMOT		KL	Torque threshold to switch the AC-compressor off
MDKOEN	NMOT		KL	Torque threshold to switch the AC-compressor on
SNM08K0UB	NMOT		SV	Datapoint distribution for air-conditioner compressor control 8 nmot
SY_GGGTS			SYS	system constant: sensor variable exact temperature signal
SY_KOBIDIR			SYS	AC- with bidirect. connection
TANSKOB			FW	Intake-air temperature threshold for compressor shutdown
TKOAMAD			FW	Inhibition time for AC compressor during adaptation of requirement
TKOAMNN	NMOT		KL	minimum shutdown time for air-conditioning compressor
TKOAMXN	NMOT		KL	maximum shutdown time for air-conditioning compressor
TKOBEMNN	NMOT		KL	Minimum switch-on time for compres. after triggering by B_kobped or B_kobwped
TKODPAMNN	NMOT		KL	Minimum cut-out time of the air-conditioner compressors during acceleration (dwp)
TKODPAMXN	NMOT		KL	Maximum cut-out time for compressor cut-out by dwped
TKOEMNN	NMOT		KL	minimal time of air-condition compressor beeing swiched on
TKOMBKOA			FW	Engine temperature thresholt from panel board for switching the compressor off
TKOMBKOE			FW	Engine temperature threshold from panel board for switching on the compressor
TKOVKO			FW	Monitoring time for air-cond. key detection after reset of B_kov (bidirect. inte
TKOWPAMNN	NMOT		KL	Minimum cut-out time at full load (by wped)
TKOWPAMXN	NMOT		KL	Maximum cut-out time at full load (by wped)
TMKOA0			FW	Upper coolant temperature for swiching off the AC-compressor
TMKOAU			FW	Lower coolant temperature for swiching off the AC-compressor
TMSTMAD			FW	Threshold for engine temperature at start for adaptation of requirement
TNSTKO			FW	AC OFF time after engine start



Parameter	Source-X	Source-Y	Type	Description
TVKOE1			FW	delay time for compressor ON
TVKOEV			FW	delay time for compressor ON
TVKOSSIM			FW	Delay time for simulation of an air conditioner switched-on during start-up
VKO			FW	vehicle speed threshold for AC-control
VKOA0			FW	Upper vehicle speed threshold to inhibit the AC-compressor
VKOB			FW	Speed threshold for compr. control during acceleration
VNVKO			FW	Gear detection threshold for compr. shutdown at full load
VNVKOB			FW	Gear detection threshold for compr. shutdown at full load
WPEDKO	NMOT		KL	Accelerator position treshold for the A/C cut off
Variable	Source		Type	Description
B_ACRES	KOS		AUS	Condition for increasing the torque reserve by AC-stand-by
B_AUTGET	PROKON		EIN	condition automatic gearbox
B_DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP		EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_GEOA			EIN	Condition for switching off the compressor due to transmission actions
B_GRDST			EIN	condition basic attitude
B_GSCH			EIN	Condition gear-shift in process
B_GWHS	BBGANG		EIN	Condition gear change on manual transmission vehicle
B_KO			EIN	condition AC compressor authorised
B_KOA	KOS		LOK	Condition for AC-compressor OFF
B_KOBAUS	KOS		LOK	Condition for compressor during acceleration or at load
B_KOBMNON	KOS		LOK	Minimum Switch-on time after switching off during acceleration or full load
B_KOBPED	KOS		LOK	Condition for compressor off during acceleration by dwped
B_KOBPEDT	KOS		LOK	Condition for compressor switch-off by dwped acc. to timer
B_KOBWPEDT	KOS		LOK	Condition: A/C cut off over wped after timer
B_KOE	KOS		AUS	Condition for AC-compressor ON
B_KOENA	KOS		LOK	Condition AC-compressor is enabled
B_KOENAT	KOS		LOK	Condition AC-compressor is enabled after timer
B_KOINT	KOS		LOK	Condition for compressor switch-off from engine management
B_KOMNOFF	KOS		LOK	Condition AC-compressor is swiched off for more mor than an minimal time
B_KOMNON	KOS		LOK	Condition AC-compressor is swiched on for more mor than an minimal time
B_KOMXOFF	KOS		LOK	Condition AC-compressor is swiched off for more than a maximal time
B_KOOFF	KOS		LOK	Condition for immediate swiching off the AC-compressor
B_KOOFFT	KOS		LOK	Condition for immediate swiching off the AC-compressor after timer
B_KOTMSK	KOS		LOK	Condition for air-conditioning switch-on
B_KOTMSKO	KOS		LOK	Condition for air-conditioning switch-on acc. to timer
B_KOV	KOS		AUS	Condition AC compressor forbidden
B_KOVDOWN	KOS		LOK	Monitoring time of B_ko after reset B_kov to B_kotmsko (bidirect. interface)
B_KOWPED	KOS		LOK	condition for A/C compressor cut off over wped
B_KUPPL	SWADAP		EIN	EGAS Condition clutch is disengaged
B_LL	MSF		EIN	Condition idle
B_MADFK			EIN	condition for torque adaptation AT in drive and AC compressor on
B_MADFS			EIN	condition for torque adaptation AT in drive
B_MADKO			EIN	condition for torque adaptation AC-compressor on
B_MADLL			EIN	condition for torque adaptation loadless
B_NAC	KOS		AUS	condition for increased idle-speed at AC
B_SA	MDRED		EIN	Condition fuel cut-off
B_ST	SWADAP		EIN	condition for start
B_STEND	BBSTT		EIN	condition end of start
DWPED	GGPED		EIN	gradient of the standardized accelerator pedal angle
FHO	BGPU		EIN	Correction factor altitude
GANGI	SWADAP		EIN	Engaged gear
MDKO	MDVERB		EIN	torque needed for air condition
MIFAL_W	MSF		EIN	Indicated driver's wish torque for torque coordination cylinder filling
NMOT	SWADAP		EIN	engine speed
SY_KOAC			EIN	system constant : commutation for S_ko and S_ac
S_AC			EIN	A/C stand-by position
TANS	SWADAP		EIN	Intake air temperature
TMKI			EIN	Coolant temperature of instrument panel
TMOT	SWADAP		EIN	Engine temperature
TMST	GGTFM		EIN	engine temperature at start
VFZG	SWADAP		EIN	vehicle speed (km/h)
WPED	GGPED		EIN	Standardized accelerator pedal angle

### FW KOS 113.140 Fixed Values

Parameter	Value	Description
CDWGANG		Gear detection for compressor shutdown at full throttle
CDWGANGB		Gear detection during acceleration
CDWKOB		Code word: Selection for gear detection for compr. shutdown (gangi or nmot/vfzw)
CWKOANG		configuration for transmission
DWPEDKOB		gradient of the standardized accelerator pedal for the compressor
FHOKOB		altitude threshold to enable the compressor
TANSKOB		Intake-air temperature threshold for compressor shutdown
TKOAMAD		Inhibition time for AC compressor during adaptation of requirement
TKOMBKOA		Engine temperature thresholt from panel board for switching the compressor off
TKOMBKOE		Engine temperature threshold from panel board for switching on the compressor
TKOVKO		Monitoring time for air-cond. key detection after reset of B_kov (bidirect. inte
TMKOA0		Upper coolant temperature for swiching off the AC-compressor
TMKOAU		Lower coolant temperature for swiching off the AC-compressor



Parameter	Value	Description
TMSTMAD		Threshold for engine temperature at start for adaptation of requirement
TNSTKO		AC OFF time after engine start
TVKOE1		delay time for compressor ON
TVKOEV		delay time for compressor ON
TVKOSSIM		Delay time for simulation of an air conditioner switched-on during start-up
VKO		vehicle speed threshold for AC-control
VKOA0		Upper vehicle speed threshold to inhibit the AC-compressor
VKOB		Speed threshold for compr. control during acceleration
VNVKO		Gear detection threshold for compr. shutdown at full load
VNVKOB		Gear detection threshold for compr. shutdown at full load

## FB KOS 113.140 Detailed description of function

### APP KOS 113.140 Application hint

The following picture shows an example of calibration for the AC-compressor control parameters:

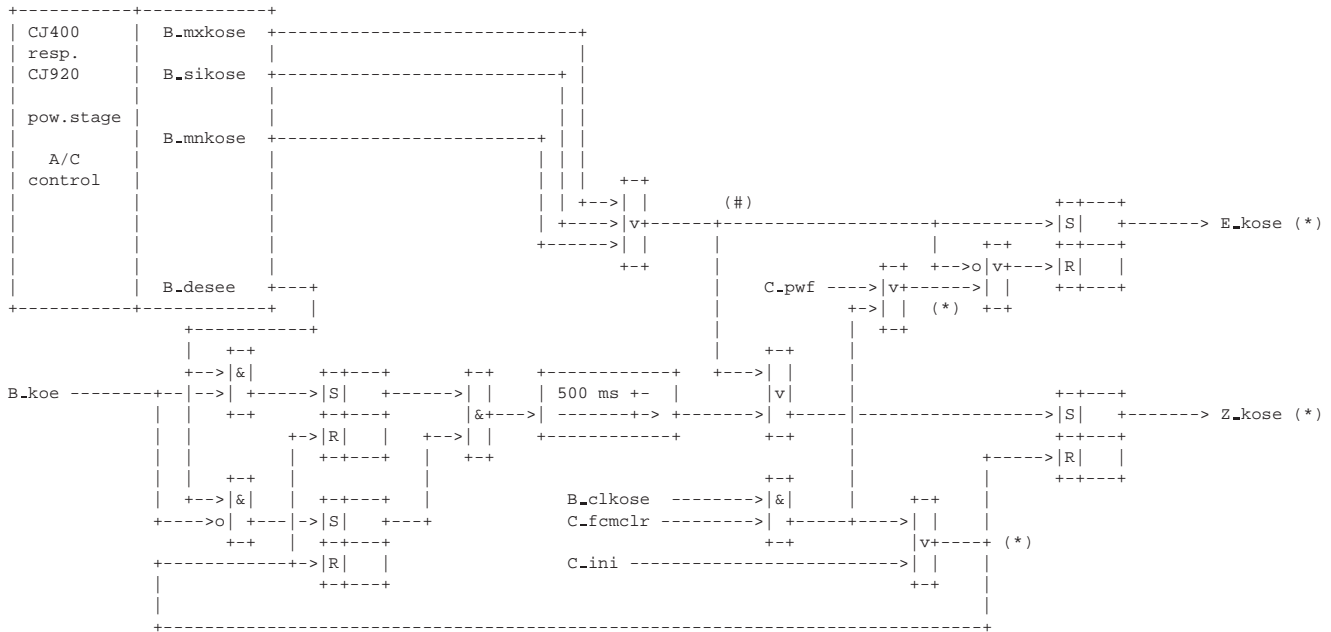
Switching off threshold MDKOAN:	Far under the idle speed the threshold is equal to zero. Immediately if the engine speed drops into this speed region, the compressor is switched off to avoid engine stalling. The time TKOEMNN is set to zero to permit always the immediate switching off. The time TKOAMXN is greater than LIMTKOA to avoid a switching on as long as the engine remains in this speed region.
	For normal engine speeds the switch-off threshold is nearly equal to the maximum of engine torque. The disponibility of the compressor becomes here maximal. For very high engine speeds it could be necessary for preventing the compressor from damage to switch him off. Therefore the threshold MDKOANN is here again set to zero. Here the same time conditions are used as for very low engine speeds.
Switching on threshold MDKOEN:	The switching on threshold is typically lower than the switching off threshold. At constant engine speed there is a torque hysteresis for the switching of the compressor.  For high engine speeds the two thresholds MDKOEN and MDKOAN are speed shifted to each other. So a speed hysteresis for the compressor switching can be obtained.
Minimal on time TKOEMNN:	For low and high engine speed, the minimal on time is set to zero to permit an immediate switching of of the compressor an any time. Between this speed limits the car manufacturer decides of the minimal on time.
Minimal off time TKOAMNN:	The minimal off time is not important for the compressor control. This time is only a request of the manufacturer of the compressor-clutch.
Maximal off time TKOAMXN:	The maximal off time must be greater than LIMTKOA for low and high engine speeds to avoid a a compressor switching on in this engine speed regions. Between this speed limits the maximal off time is determined by the car manufacturer depending of the requested AC disponibility.



## DKOSE 5.10 Diagnosis of power stage for AC compressor

### FDEF DKOSE 5.10 Function definition

Diagnosis CJ400, resp. CJ 920 see %DECJ



(\*) deviant from the description this path is served in the module %DFPM resp. the flags are managed in %DFPM;  
 (#) deviant from the description this path is served in the module %DECJ;

Substitution measures: non

Error memory management:

```

Status error path kose:      SFPKOSE
Error flag :                 E_kose
Cycle flag :                 Z_kose
Error type :                 B_mnkose
                             B_mxkose
                             B_sikose
Delete error path:          C_fcmlr & B_clkose
Error path :                 CDTKOSE
Error class :                CLAKOSE
Error intensity :            TSPKOSE
Carb code :                  CDCKOSE
Environmental conditions :    FFTKOSE
  
```

### ABK DKOSE 5.10 Abbreviations

Variable	Source	Type	Description
B_CLKOSE		EIN	condition: clear fault path A/C power stage
B_DESEE	DKOSE	AUS	Diagnosis power stage: entry conditions fulfilled
B_KOE	KOS	EIN	Condition for AC-compressor ON
B_MNKOSE	DKOSE	AUS	Error type: short circuit to ground air cond. power stage
B_MXKOSE	DKOSE	AUS	error type: short circuit to Ubat A/C power stage
B_SIKOSE	DKOSE	AUS	error type: cable disconnection of A/C power stage
C_FCMLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_KOSE	DKOSE	AUS	Error flag: AC compressor activation , power stage
Z_KOSE	DKOSE	AUS	Cycle flag: AC compressor activation, power stage





Variable	Source	Type	Description
E_HSV2	DHLSVKE	AUS	error flag: lambda sensor heating upstream cat on the right (Endstufe)
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
Z_HSV2	DHLSVKE	AUS	cycle flag of lambda sensor heating upstream cat (Endstufe)
Z_HSV2	DHLSVKE	AUS	cycle flag of lambda sensor heating upstream cat, cylinder row 2 (Endstufe)

### FW DHLSVKE 2.20 Fixed Values

Parameter	Value	Description
CDTHSV2		code word tester: oxygen sensor heater upstream catalyst power stage
CDTHSV2		code word tester: power stage oxygen sensor heater2 upstream catalyst
CLAHSV2		fault class: O2 Sensor Heater power stage bank 1
CLAHSV2		fault class: O2 Sensor Heater power stage bank 2
TSFHSV2		fault active time: lambda sensor heating catalyst upstream (driver stage)
TSFHSV2		fault active time: power stage lambda sensor heating catalyst upstream, bank 2

### FB DHLSVKE 2.20 Detailed description of function

The precondition for the diagnosis "power stage heating Lambda sensor" is the use of a power stage of the type CJ400/CJ920. The detection of a non-plausible state at the power stage and the reading of the fault type from the IC is described in the section %DECJ.

The fault types from the CJ400 diagnosis are combined according to their effect on the HLS for the further processing in other ECU functions. Short-circuit to UBat or wiring interruption lead to the Lambda sensor not being heated. In case of a short-circuit to ground the sensor is heated with maximum performance.

The cycle flag is set by the CJ400 diagnosis in case of detected power stage fault. The cycle flag is also set, if via the condition B\_dese it is indicated that a CJ400 diagnosis can be performed and if the heater power stage was switched on and off once without fault.

### APP DHLSVKE 2.20 Application hint

## AS 5.0 Output signal adaption

### FDEF AS 5.0 Function definition

Responsible:

### ABK AS 5.0 Abbreviations

### FW AS 5.0 Fixed Values

Parameter	Value	Description
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### FB AS 5.0 Detailed description of function

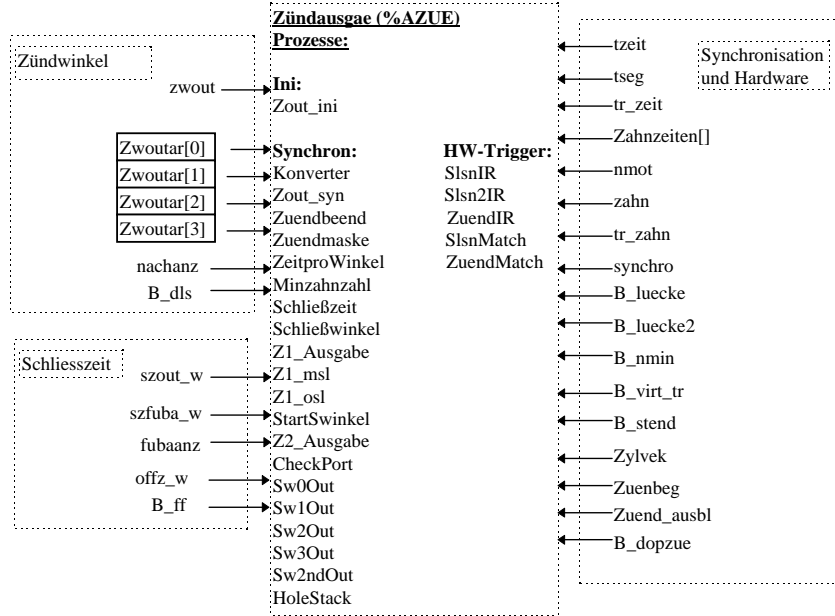
Description is missing !!!!

Responsible:

## APP AS 5.0 Application hint

## AZUE 5.40 Output ignition

### FDEF AZUE 5.40 Function definition



#### azue-syn

Fig. 1.0 Overview interfaces %AZUE:

### ABK AZUE 5.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CW_AZUE			FW	configuration code word ignition output
SY_DLS			SYS (REF)	system constant digital idle speed control
SY_DOPZW			SYS (REF)	System constant doubled ignition output included
SY_FFZ			SYS (REF)	system constant interval ignition
SY_FREQ_CP			SYS (REF)	system constant cpu frequency
SY_GAP			SYS (REF)	system constant: number of missing teeth in the gap
SY_GRNDWRT			SYS (REF)	system constant basis angle ref. tr-mark
SY_NACH			SYS (REF)	System constant ignition output after KL15 off included
SY_JNZUEB			SYS (REF)	system constant engine speed threshold for switching between ignition modes 1+2
SY_TEETH			SYS (REF)	system constant: number of teeth at the crankshaft wheel (gapteeth included)
SY_WMIN			SYS (REF)	System constant latest ignition timing that can be outputted
SY_ZNDAUS			SYS (REF)	System constant ignition timing output (single or double fir.), 1: single,2: d.
SY_ZYLZA			SYS (REF)	system constant number of cylinders
TMZUB2MX			FW	temperature limit for angular priority during cold-start
ZWFUBAMN			FW	end angle of multiple strike ignition if configured

Variable	Source	Type	Description
B_LUECKE	GGDPG	EIN	current segment covers the reference gap
B_LUECKE2		EIN	condition tooth gap at odd number of cylinders in the center of the segment
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_SLSN2	AZUE	AUS	Condition overlapping dwell-time after cylinderspecific ignition-timing retard
B_STEND	BBSTT	EIN	condition end of start
B_SW0	AZUE	AUS	Condition no overlapping of dwell-time
B_SW1	AZUE	AUS	Condition overlapping of dwell-time
B_VIRT_TR		EIN	Condition virtual calculation of tr marking is active
B_Z1	AZUE	AUS	Condition ignition section 1 is active
B_ZESYNC	AZUE	AUS	Condition ignition synchronized
B_ZWS0	AZUE	AUS	Condition change to single dwell-time overlapping - dwell time is outputted
MINZAHN	AZUE	AUS	Minimum number of teeth for earliest ignition event
NMOT	SWADAP	EIN	engine speed
OVLCTR	AZUE	AUS	Overlap counter dwell-event
SLSNINKR	AZUE	AUS	Rest of dwell-begin angle in 0.75 degree quantisation
SLSNINKR2	AZUE	AUS	Rest of dwell-begin angle in 0.75 degree quantisation overlapping after knocking
SLSNZAHN	AZUE	AUS	Dwell-begin angle in tooth quantisation 6 degree
SLSNZAHN2	AZUE	AUS	Dwell-begin angle in tooth quantisation 6 degree
SNZZKVEK	AZUE	AUS	Next ignition circuit to close for 2nd event





Variable	Source	Type	Description
SNZKVEK	AZUE	AUS	Next ignition circuit to close
SWOUT	AZUE	AUS	dwel angle
SZOUT_W	ZUESZ	EIN	dwel time
TINKR	AZUE	AUS	time per ignition angle incrementation
TR_ZAHN		EIN	teeth counter
TR_ZEIT		EIN	Timer-value at TR-event
TSEG_W	BGNMOT	EIN	segment cycle time
TZND	AZUE	AUS	Real controlled dwell-time
WOUTA0	AZUE	AUS	Ignition angle array referring angle basis element 0
WOUTA1	AZUE	AUS	Ignition angle referring to TR event plus zylinderspecific correct. of foll. cyl
WOUTA2	AZUE	AUS	Ignition angle referring to TR event plus zylinderspec. correct. of act. cyl+ 2
WOUTA3	AZUE	AUS	Ignition angle referring to TR event plus zylinderspec. correct. of act. cyl+ 3
WOUTST0	AZUE	AUS	Lowest ram-cell of ignition angle stack
WOUTST1	AZUE	AUS	Ram-cell 1 of four element ignition angle stack
WOUTST2	AZUE	AUS	Ram-cell 2 of four element ignition angle stack
WOUTST3	AZUE	AUS	Ram-cell 3 of four element ignition angle stack
ZKVEK	AZUE	AUS	Shifting value for calculation of ignition mask
ZNZKVEK	AZUE	AUS	Next ignition circuit to fire
ZOUTTMX	AZUE	AUS	Max. time from TR event till end of AZUE
ZUENBEG		EIN	Value of cylinder counter at wich an injection has taken place
ZUENINKR	AZUE	AUS	Rest angle from last tooth till ignition
ZUENTMX	AZUE	AUS	Max. time from TR event till final calculation of ignition values
ZUENZAHN	AZUE	AUS	Ignition angle in tooth quantisation
ZWOUT	ZUE	EIN	Ignition angle output value
ZWOUTAR0		EIN	Ignition angle output array Element 0
ZWOUTAR1		EIN	Ignition angle output array Element 1
ZWOUTAR2		EIN	Ignition angle output array Element 2
ZWOUTAR3		EIN	Ignition angle output array Element 3
ZYLVEK		EIN	cylinder vector

### FW AZUE 5.40 Fixed Values

Parameter	Value	Description
CW_AZUE		configuration code word ignition output
TMZUB2MX		temperature limit for angular priority during cold-start
ZWFUBAMN		end angle of multiple strike ignition if configured

### FDEF AZUE 5.40 Function definition

#### 1. Ignition concept:

The ignition concept of the ME7 has been conceived for single spark and double spark coils. The coils are triggered by ignition power stages, which can either be located inside of the ECU or outside. The triggering of the ignition power stages is performed via port outputs of the processor. ASIC-concepts for the ignition output do not exist. Some of the power stages include a current limitation.

For external power stages diagnosis-capable small signal drivers (ex. CK110) can be integrated in the power stage diagnosis according to %DECJ. The state machine described in %DECJ is manipulated in such a way that a diagnosis logic according to %DZUEET is obtained.

For internal power stages, a diagnosis does not exist.

The task of the ignition is to reliably initiate a combustion. For this, it must be ensured, that a sufficiently high amount of energy is present at the ignition coils in all operating points of the engine. This means that the voltage at the spark plug must be sufficiently high and a minimum spark duration must not be undershot. This is realized by the control of the ignition coil dwell periods (szout). The coil dwell periods are stored in characteristic maps and are applied through ub and nmot (KFSZT) in such a manner that the coil current is situated within the range of the nominal current (see %ZUEZ) for all engine load points. Normal spark durations hover around 1 ms, which corresponds to an angle range of 18 degrees for 3000 rpm. The voltage at the plug is possibly applied to 30KV.

In order to optimize the combustion process (exhaust gas reduction, optimum torque), the dwell end (i.e. the ignition point) is controlled such that a spark beginning corresponds as exactly as possible to the preset ignition point zwout.

Angle information is available through the counting of teeth of the engine speed sensor. During an engine speed sensor limp-home, this information must be artificially generated. The remaining residual angle, which cannot be measured by referring to the teeth, is added as a waiting period to the last counted tooth. Time-controlled events, like e.g. the output of the dwell period during start, are realized via a special timer. It should be observed that the time interval output is not longer than one timer cycle. This is 52.4ms for a resolution of 800ns. The ignition event is limited to one synchro. The dwell event in ignition range 2 can be realized as an output for up to 3 synchronization rasters after the calculation of the event (return of the 3-fold overlap to an overlap-free operation).

#### 1.1 Block diagram:

=====

Assignment: engine speed signal (nBM), phase signal and ignition signal (Example 4-cyl.-engine, firing order 1 3 4 2):

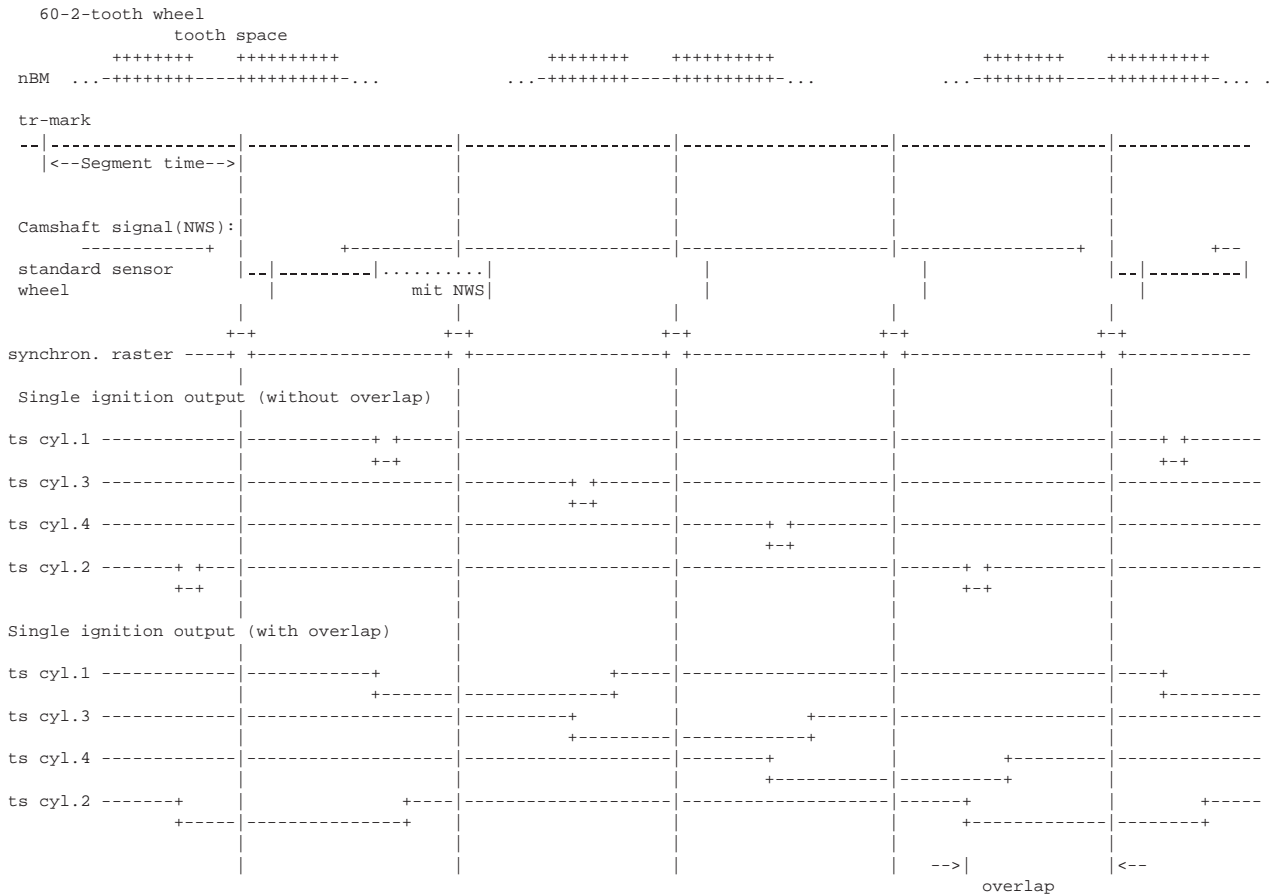


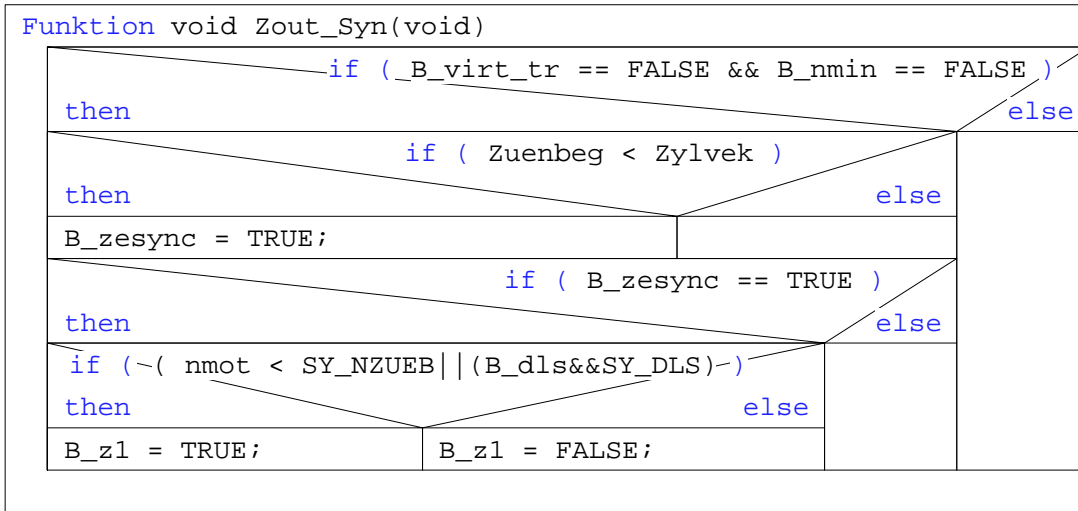
Figure 1.1 shows in principle the course of ignition signals at the controller. Via engine speed sensor and camshaft sensor the controller HW generates the synchronization raster by counting a determined number of teeth. The first synchronization raster is established immediately after the detection of the tooth space. By requesting the level of the camshaft sensor directly after the tooth space has been detected, the synchronization raster is assigned to the corresponding cylinders. At the beginning of the synchronization raster the segment time - i.e. the time between the tr-marks - is calculated. Afterwards the synchronous processes of the user SW (applicable SW) - containing among others the calculation of the output ignition angle  $zwout$  (see %ZUE) - are called. The dwell period  $szout$  (see %ZUESZ), the segment time  $tseg_w$  and the ignition angle  $zwout$  are used to calculate a dwell beginning angle ( $Slsnzahn, Slsninkr$ ). The dwell beginning is set by the controller HW by counting sensor teeth ( $Slsnzahn$ ) including a waiting period for the increment refinement ( $Slsninkr * Tinkr$ ).

The ME7 uses two different output methods, called ignition range 1 and 2 in the following. Basically, the ignition output is provided with the information about ignition angle and dwell period. The synchronisation SW transmits the segment time  $tseg$ . Via the segment time, the dwell period  $szout$  is converted into a dwell angle  $swout$ . Ignition angles of few dwell angles result in the dwell beginning angle. In both of the ignition ranges, the output of the dwell beginning angle is performed by counting sensor teeth plus added increment refinement. Is the dwell beginning angle reached, the dwell event is released. In ignition range 1, the dwell period is defined as a timer-comparative value at the release of the dwell event. This means, the ignition coil remains closed until the dwell period  $szout$  is reached with a max. timer precision (800ns for 20 Mhz). When the comparative value is reached, the controller HW opens the coil circuit, and an ignition is triggered. In ignition range 2, no further actions are started anymore in the release routine of the dwell event. In this operating mode, the output of dwell beginning angle and ignition angle is carried out parallelly and independently of each other. This means, the ignition angle in ignition range 2 is released in the same way as the dwell beginning angle (counting of sensor teeth plus increment refinement).

Principle of function: synchronisation and switch-over between the ignition ranges:



## Zout\_Syn



azue-umsch

### azue-umsch

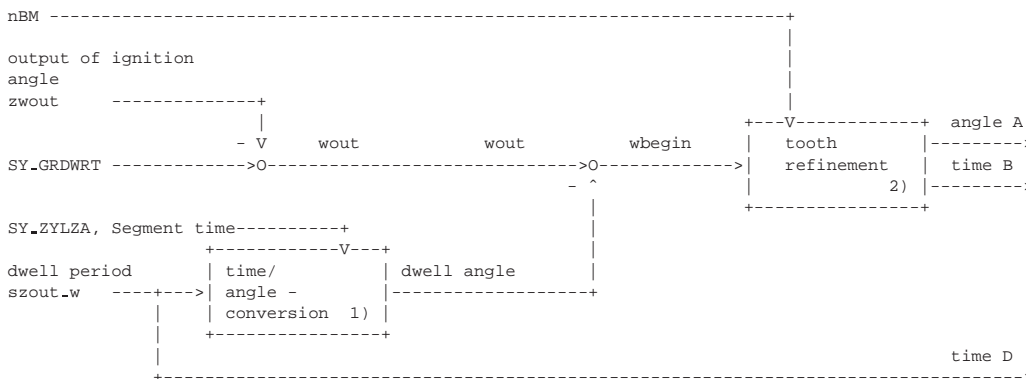
Figure AZUE-5-UMSCH-1 shows the synchronisation mechanism as well as the range switch-over in a structogram. It should be noticed that the structogram constitutes only an abstraction of the assembler SW in the ECU. The used names as well as the position of the request elements differs from the real SW. If the minimum engine speed exceeded (B\_nmin == FALSE), a real synchronisation has been carried out (B\_virt\_tr == FALSE). If the cylinder counter exceeds the cylinder value of the first injection (Zylvek > Zuenbeg), the ignition output routine is started. The synchronisation with the injection effects an ignition at a defined Motronic-mixture. That way, the asymmetries (jerk during start) are reduced.

The switch-over between the ignition ranges happens via the flag B\_Z1 (visible in the application system). Below the speed SY\_NZUEB B\_Z1 = TRUE is set, the ignition range 1 thus being activated. By means of a code word intervention, it is also possible to select another switch-over mechanism (see chapters later on). Above the threshold B\_Z1 = FALSE, i.e. ignition range 2 is activated. In some single projects a so-called "digital low idle stabilisation" is used, for which the output of dwell beginning and ignition event is performed by a timer-comparison. The DLS-function is utilized in VW-projects and requires various frame conditions for a correct functioning. If the DLS-functionality is integrated in the ECU via the system constant SY\_DLS, ignition range 1 is activated, in the case of an active DLS (B\_dls = TRUE).

### 1.2 Signal sequence in ignition range 1

=====

Overview : calculation of the dwell time:



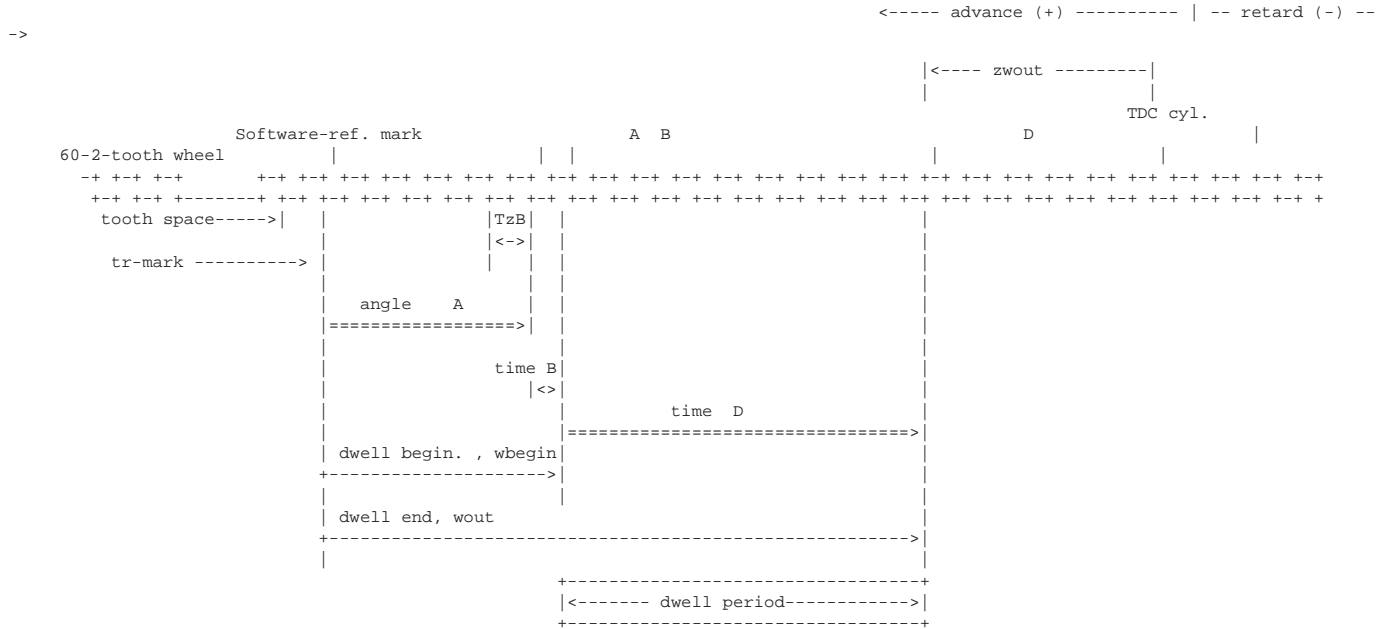
1) and 2) as for the "calculation of the dwell angle"

Calculation of dwell beginning and dwell end:  
Calculation of the dwell beginning and the dwell end:  
The dwell beginning is calculated, just like in the ignition range 2, with tooth refinement.  
The dwell end results directly from the dwell period szout.w. The exact output of the dwell period uninfluenced by the engine speed dynamics takes place.



Output: fixed dwell period (ignition range 1, B\_wz1 = 1):

Overview:

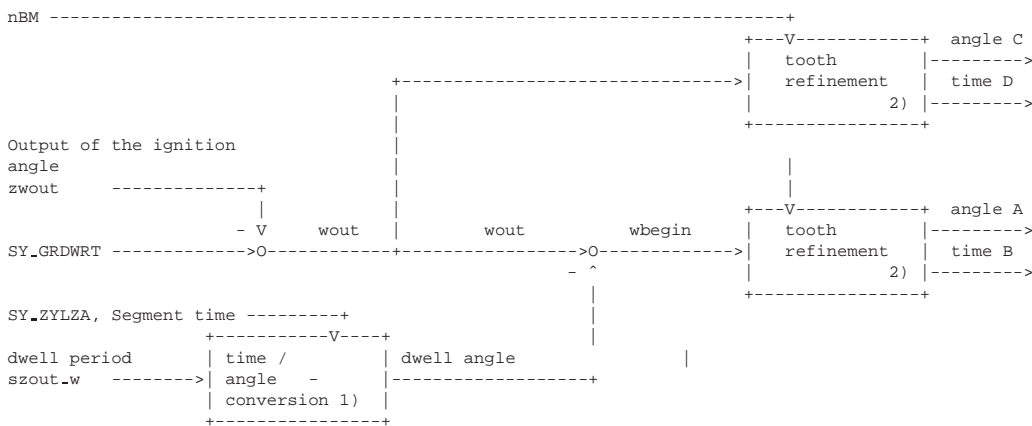


In ignition range 1, the dwell period szout is re-quantized after the triggering of the dwell beginning and is loaded into a comparative register of the ignition timer. That way, exactly (800ns) after the dwell period has elapsed, an ignition pulse is generated.

Ignition range 1 has only been conceived for lower engine speeds. An operation with overlapping dwell periods is not supported.

### 1.3 Signal sequence in ignition range 2

Overview: calculation of the dwell angle:





1):

$$\text{Dwell angle} = \frac{720^\circ / \text{SY\_ZYLZA}}{\text{segment time (tseg-w, tseghi)}} * \text{szout\_w}$$

2):

Tooth refinement:

$$\text{Factor tooth refinement} = \frac{\text{tooth angle}}{\text{angle increment}} = \frac{6^\circ}{0.75^\circ} = 8$$

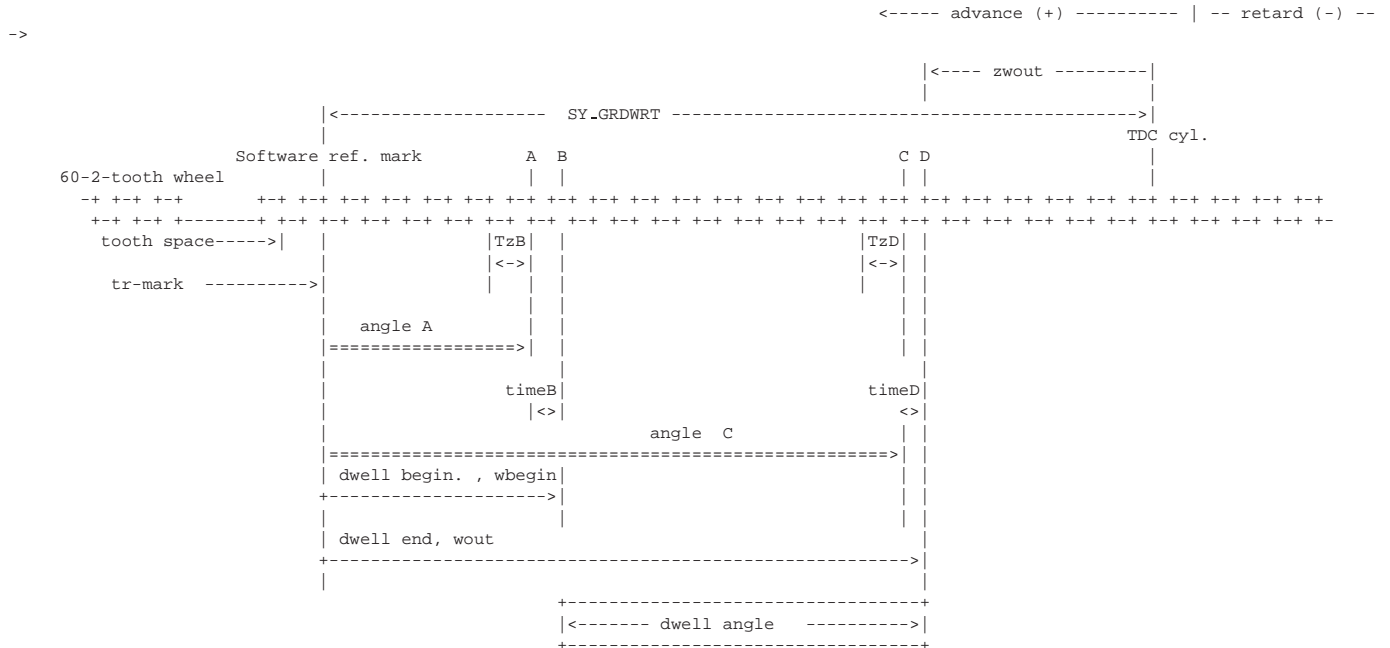
Sequence:

1. Determine angle A for 1. interrupt:  
Angle A [no. of teeth] = wbegin[°] / 6 ; with rest [no. of teeth]
2. Determine the last tooth time TzB
3. Residual angle [°] = rest[no. of teeth] \* 6°
4. No. of increments = residual angle[°] / 0.75
5. Determine timeB for 2. interrupt:  
TimeB = (TzB/8) \* no. of increments

;accordingly for the time D

Output: Fixed dwell angle (ignition range 2, B\_z1 = 0):

Overview:



In ignition range 2, dwell beginning angle and ignition angle are used independently of each other for the output of dwell beginning and dwell end by counting the angle values at the sensor wheel teeth.

Ignition range 2 permits dwell period overlaps. This means, that the dwell beginning of a charging time can be situated max. three segments before the ignition event. Since the charging times must be kept as exactly as possible, the ignition angle related to the dwell beginning in the segment of the dwell beginning is frozen, and the ignition angle calculated during the charging time is not taken into account anymore.



## 2. Ignition output methods

### 2.1 Ignition range 1

The ignition output is divided into two ignition methods between which a hard switch-over is performed during stationary operation at an engine speed of SY\_NZUEB, as soon as the start phase ends.

Summary of the advantages and the disadvantages of the two methods:

	Advantages:	Disadvantages:
Dwell period output (ZB1):	minor power dissipation, sufficient ignition energy also in case of dynamics (start, time output not influenced by dynamics)	engine speed dynamics causes a deviation of zwout compared to the real angle position of the ignition output pulse. The deviation strongly depends on the length of the dwell period.
dwell angle output(ZB2):	more accurate ignition angle	inaccurate ignition energy (too high: power dissipation, too low: misfire)

It should be noticed that at a stable engine speed no difference between the immediate output of the dwell periods and the angle accurate output of the dwell beginning and the ignition angle (ignition range 2) can be observed. The division into two ignition ranges has the major aim to avoid an affection of the dwell periods through pre-emptive dynamics during start. In the old Motronic-Systems a hyperbolically increasing dynamic value must be added to the dwell periods to obtain an angle accurate output of dwell beginning and ignition point. This is due to the fact, that the engine speed information in the synchro is only determined rather rarely, with the effect, that the extreme accelerations during start result into an extreme reduction of the real dwell period. In this case, a sufficiently high dynamic value must be considered during the application phase so that even at the highest acceleration within a segment the output of the charging time remains correct.

In practice, the charging times sometimes take on such high values, that coil/power stage are in danger during warm starts. For ignition systems with current limitation, it has been observed that the considered dynamic value at start is so high, that the primary current clearly reaches the current limitation range at normal dynamic influences.

This means that during normal operation the power dissipation increases with increasing dynamic value.

Since the dwell period application is optimized regarding power loss/plug wear, it is of a major importance to realize a dynamically correct output of the dwell period to ensure that an ignition spark is established. With increasing engine speed the frequency used for the detection of the speed signal in the ECU increases too. Thus dynamic changes can more easily be determined. Therefore it is advisable to realize an output of dwell periods at low engine speeds. The higher the engine speed, the higher the dynamic resolution. Due to this fact, it is no more necessary to proceed to an immediate output of the dwell periods from a particular engine speed threshold onwards. Since with increasing engine speed and load also the fuel management is improved, it becomes more and more probable that already at spark beginning a combustion is caused. The ignition angle resolution therefore increases.

In the current ignition no dynamic value must be applied during start. The disadvantage of the very exact control of the dwell periods is that the ignition angle deviates under dynamic influences from the applied ignition angle zwout. This deviation, however, only occurs for dynamic influences and decreases with reduced dwell periods. Since the output of the dwell period enables a very exact control, the dwell periods in ignition range 1 should be selected as small as possible.

### 2.2 Ignition range 2

Starting with the threshold SY\_NZUEB, dwell beginning and dwell end (ignition) are realized as an output via an angle comparison. This ignition mode is designated as ignition range 2.

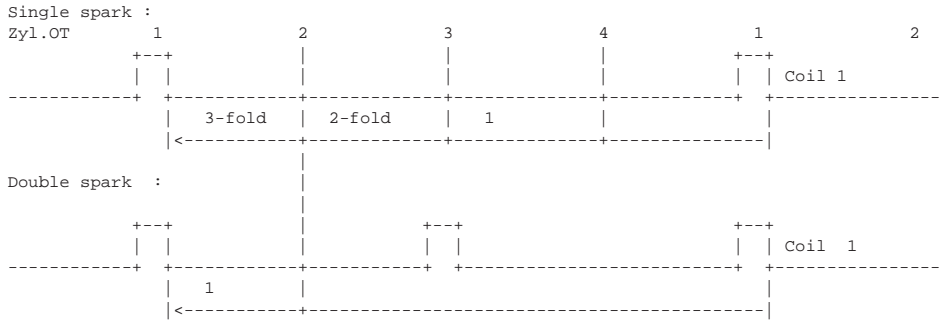
The output of the ignition related dwell beginning in ignition range 2 can be realized up to 3 segments in advance.

The output of the dwell beginning one or more segments before the ignition segment is called overlap. The overlap can comprise 3 segments at max..

In the case of double spark coils for cylinder numbers lower than 6 and in the case of single spark plugs for cylinder numbers lower than 3, the max. degree of the overlap is less than three segments.

Possible overlap in segment	Cylinder number	Used coil concept
3	8	single and double spark
3	6	single spark
2	6	double spark
3	5	single spark
3	4	single spark
1	4	double spark
2	3	single spark

E.g. single and double spark coils (4 cylinder)



One single coil can be closed for almost 4 segments, as long as the power dissipation permits it. This means, the dwell period can overlap for max. 3 segments. For ideal, loss-free components only a residual open time must be kept during the spark duration. The last possible ignition angle is in this case determined by the system variable SY-WMIN.

For the double spark plug, already 2 segments after the last ignition, the ignition of the complementary cylinder is carried out with the same coil. This means, the dwell beginning can be at max. one segment in advance of the ignition segment.

Dwell beginning angle and ignition angle in ignition range 2 define the dwell angle and thus the energy of the coil. If between dwell beginning and ignition angle a synchronization raster is active, the calculated new ignition angle has no effect on the current ignition, since otherwise the coil energy could change too gravely.

### 2.1.1 Overlap operation - ignition array/ignition angle stack =====

As described above, the dwell beginning is placed one or two segments before the ignition during the overlap operation. Since the calculation of the ignition events takes place in the general synchro-program, a possibility must be created to enable an access of the synchro-program to an ignition angle that is part of a dwell beginning resulting from several synchros in advance. For this, the SW uses a 4-element (0..3) deep ignition angle stack. If the SW is in overlap operation, the ignition angle is not taken directly from zwout, but from the 0-element of the ignition angle stack. If a 3-fold overlap is detected, zwout is written on the third element of the ignition angle stack and the dwell beginning angle belonging to zwout is realized as an output in the current synchro. At the end of this synchro, the elements of the ignition angle stack are shifted downwards by one element. As a result, the zwout written into the third element of the stack occurs 3 synchros later at the zero position of the stack. The output SW takes over the corresponding output ignition angle.

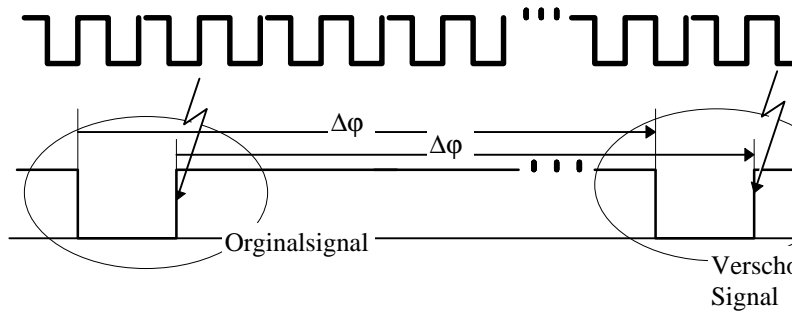
ZWOUTST3=ZWOUTAR3	ZWOUTST3= xx	ZWOUTST3= xx	ZWOUTST3= xx
ZWOUTST2= xx	ZWOUTST2=ZWOUTAR3	ZWOUTST2= xx	ZWOUTST2=xx
ZWOUTST1= xx	ZWOUTST1=xx	ZWOUTST1=ZWOUTAR3	ZWOUTST1=xx
ZWOUTST0= xx	ZWOUTST0=xx	ZWOUTST0= xx	ZWOUTST0=ZWOUTAR3
0 segment	1 st segment	2 nd segment	3 rd segment

The figure shows the principle of the ignition angle stack at a 3-fold overlap. In the zero segment, the dwell beginning of an ignition which should be triggered in the 3rd segment is started. For this, the output ignition angle is copied to the 3rd element of the ignition stack. It then moves one element downwards per synchro, so that it accesses the ignition output in the third segment at zero position.

The ignition angle written into the stack in the zero segment could belong to a knocking cylinder, whereas the cylinder which is fired in segment 0 does not knock. The ignition angle zwout is calculated in the synchro for the cylinder which should be fired in the current synchro. In the example, the firing of the cylinder has already been initialized 3 segments in advance. This means, the output ignition angle is also placed in the zero element of the ignition angle stack.

For the described ignition angle stack zwout can not be used. For this, an ignition angle array zwoutar[0..3] is defined in %ZUE. This array increases zwout in the zero element. In the elements 1 to 3 the same value is used, if no cylinder-individual offsets are added to the ignition angle. If a knocking occurs or if other cylinder-individual proportions are added to the basic ignition angle, zwoutar1..zwoutar3 contains that value, which would result for zwout in the following cylinder, and also the next two cylinders. This means, the ignition angle array includes the basic ignition angle of the current cylinder plus the cylinder-individual offset for the following cylinders, for the case that the ignition output must shift to the overlap mode, to realize after all the output of the applied dwell period. The ignition thus works during the overlap operation with the ignition angle of the previous segment (single overlap) or with the ignition angle of the third advanced segment (3-fold overlap).

### 2.2 Dual-spark ignition output (DZA) =====



**Doppelte Zündausgabe bei ungeradzahigen Zylinderzahlen:  
Schließ- und Zündereignis werden ein halbes Segment später nochmals  
ausgegeben**

azue-dza1

**azue-dza1**

The dual spark ignition output is activated, if no cylinder synchronisation of the segments is reached and the synchronisation SW requests this mode via the bit B\_dopzue.

At the DZA, the cylinders are always fired again after 360 degree. This means that each cylinder is fired at working TDC and gas exchange TDC. For even-numbered cylinders, a complementary cylinder is at gas exchange TDC, if the considered cylinder is at working TDC. The DZA for even-numbered cylinders and single coil systems can thus be realized by a corresponding masking of the output register. For ignition systems with double spark coils, a special DZA-operation is not required. For single coil ignition systems and uneven cylinder number, no complementary cylinder exists. However, it exists an offset of 1/2 segments between a cylinder at working TDC and the next cylinder which is heading for the gas exchange TDC. For this reason, two further interrupts are placed for the DZA-operation with uneven cylinder number. The two IR are added to the dwell event and the ignition event of an "original ignition" in a 1/2 segment-distance. This means, the thus activated ignition is independent of the synchro, new calculation results of the synchro-program cannot be taken into account in the mirrored event.

Attention ! The DZA could provoke an intake manifold explosion. The customer must be informed about these risks.

A single spark ignition during DZA-operation cannot be compared to a double spark ignition. A double spark ignition has two spark gaps in series, i.e. the working spark needing a high voltage quickly consumes the energy provided by the coil. For the secondary spark only a small amount of energy is available. The burning duration is equal to the burning duration of the working spark at a lower burning voltage. If the single spark coil is ignited during charge change, the burning durations are longer, since the voltage requirement at the plug and the burning voltage are much smaller than at working TDC.

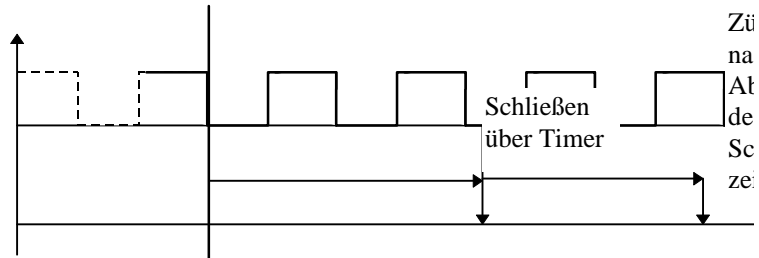
**2.3 Spark band ignition**  
=====

At the spark band ignition sparks derived from the original spark are added through a kind of mirror effect. The original spark is in this case conventionally defined over the ignition angle  $z_{wout}$  and the ignition angle array  $z_{woutar}[0..3]$  as well as the dwell period  $szout$ . The following ignitions are started after an open time (offzt) succeeding the last ignition. The dwell period of the following ignitions is described in  $szfuba$ . The number of added sparks is determined in  $fubaanz$ .

Via the code word ZWFUBAMN, the last permissible angle position of a recharge pulse of a partial spark of the spark band can be applied. In this case, the actual teeth number at the ignition of a partial spark is compared to the teeth number of the tr-mark. If the distance between the last released ignition spark and tr-mark is smaller than the value described by ZWFUBAMN, a further charge process is triggered, if the applied spark number has not been reached yet. If the last possible ignition angle coincides with a space, a distinction is made whether the end mark is situated behind or in front of the middle of the segment. If the last possible ignition angle is placed before the middle of the space, the preceding tooth is used as an end mark. If the ignition angle is placed behind the middle of the space, the following tooth is used as an end mark.

**2.4 Digital low-idle stabilisation (DLS-function)**  
=====





TR-Marke:  
Auswerten  
der Segmentzeit  
Umrechnen der Winkel-  
ereignisse in Zeitpunkte  
bzgl TR-Marke.  
Start des Zeitvergleichs.

azue-dls

azue-dls



The DLS-function can be classified as an extension of the ignition range 1. In ignition range 1, the dwell period is added to the dwell beginning angle, which is effected by counting of the sensor teeth. In contrast to ignition range 1, also the dwell beginning angle is controlled via a timer-comparison.

## 2.5 Ignition during after-run =====

In single systems, the ignition coil is permanently set to plus in the after-run phase via a relay in the ECU. For this, the ignition is also kept during the after-run. So that the motor stops after a definite time, the revolutions during the after-run are counted and after reaching the threshold nachanz, the ignition is suppressed.

## 2.6 Configuration word ignition output =====

At a high acceleration or for a drastic change of the dwell period, it can occur that it is detected in the synchro interrupt that the current supply to reach the desired primary current should have been already initialized in the past.

In such a case, the primary current will not reach the desired value, if the desired ignition angle zwoutar(overlap wheel) is kept. For this reason, the standard configuration of the ME7 ignition will move the ignition angle to 'retard', to ensure, that the desired primary current will still be reached.

If, however, long dwell periods are applied in a system, and do high dynamic influences occur, it can happen, that the retarded ignition angles are not permitted anymore.

In such cases, the ignition angle correction can be switched off via the code word CW\_AZUE on behalf of the dwell period. The Bit 0 code word is usually in the correction mode. If a correction should not be carried out, Bit 0 of CW\_AZUE must be set to 1.

## 2.7 Different switch-over mechanisms =====

By setting the Bit 1 of the code word CW\_AZUE, it can be switched between the conventional and the power loss contioned switch-over mechanism between the ignition ranges. This means, that for engine speeds below SY\_NZUEB it is not automatically switched over to time output and for engine speeds above SY\_NZUEB it is not automatically switched to angle output. If bit 1 of the code word is set, at  $t_{mot} < TMZUB2MX$  the angle output is activated an at  $t_{mot} > TMZUB2MX$ , the switch-over mechanism is activated via a fixed engine speed threshold (800Upm).

Tmot dependent range selection:

- 1. CW\_AZUE    xxxx xxlx    :    TMOT dependent activation of the time output
- 2.  $t_{mot} < TMZUB2MX$     :    angle output
- 3.  $t_{mot} > TMZUB2MX$     :    time output

## 2.8 Turn-back detection =====

At a detected turn-back, a service of the ignition output is called by the turn-back detection which directly causes an ignition and blocks the ignition interrupt.

The turn-back detection sets the Bit B\_motstop which is called at the beginning at the ignition output. The ignition event calculation is then no longer carried out, at the same time, the ignition is once more forcibly released and the IR-releases are taken back.

## 2.9 The actual ignition angle =====

If the ECU is in the overlap mode, the ignition angle of the current segment is taken over from a previous segment. This means, the ignition angle calculated in the current synchro does not occur as an output in the same segment. The ignition angle passed over to the output HW in the current synchro is described by the RAM-cell zwoutakt.

## 3. Detailed functions of the ignition output =====

Figure 1.0 shows an interface overview of the AZUE and the processes in which the model of the AZUE is split under ASCET-SD.

It should be noticed that the AZUE as a whole takes place in the HW of the ME7 and thus only occurs in the SW as an HW partial process. The process structure is first of all a logic representation of the functionalities occurring in the ignition output . Parts of the ASCET-SD processes are behaviour descriptions of HW functions which have been transferred to ASCET-SD for ignition timing simulation reasons. The processes are described in the programming language C. This representation is however not to be confused with the source code of the ME7. It is rather a model of the timing behaviour for the simulation environment ASCET-SD.

In the following table the functional principle of the logic function groups of the ME7-ignition is described by means of the ASCET-SD processes:

Process	Time shedule	Functional description
1. Zout_ini	Ini	Initialization of the control information of the ignition
2. Converter	Synchro	Re-quantisation and re-formatting of the values visible for the application into values which can be processed by the HW-components of the controller.



		e.g.. szout in 0,lms/Ink is restored in sztcalc_w (800ns/Ink -> Timer 1 quantisation).
3. Zout_syn	Synchro	Request for the start conditions of the ignition: - a first ignition has been triggered - a successful synchronisation of the SW with the camshaft and the crankshaft has taken place - the min. engine speed has been exceeded Adjustment of the ignition range : If nmot < SY_NZUEB then -> ignition range 1 active otherwise -> ignition range 2 active
4. Zuendbeend	Synchro	If the release of the ignition output SW to the timer-comparison unit of the last segment does still exist, for realizing an output of an ignition pulse at the actual comparative value, the release is taken back and an ignition is effected immediately.
5. Zuendmaske	Synchro	Calculation of the output mask for the ignition port preparation for actual ignition
6. ZeitProWinkel	Synchro	Time for the calculation of an angle increment
7. Minzahnzahl	Synchro	Min. tooth distance concerning the segment start at which an event can still be triggered. Depending on the engine speed, the SW calculation of the ignition events takes more or less time. This means, the output signals are only available for an angle that is not zero. It thus exists an earliest possible ignition angle set by the program running time and the engine speed.
8. Schliesszeit	Synchro	Re-storage of the dwell period in internal registers
9. Schliesswinkel	Synchro	Conversion of the dwell period via the angle time calculated in process 6 in a dwell angle.

-----  
Ignition range 1  
-----

10. Z1_Ausgabe	Synchro	Initialize Controller HW for dwell period output, check, if already a current flows through the coils (return from overlap operation in ignition range 2 to ignition range 1), depending on this, a dwell event or an ignition signal is initialized.
11. Z1_msl	Synchro	Calculation of a port mask for the dwell beginning release by the controller. Calculate dwell beginning angle out of ignition angle minus dwell angle. If the dwell beginning angle is negative, then switch-over of the controller from angle comparison to time comparison. Immediate switch on of the coil current. The charging time is limited in such a way, that a last possible ignition angle WMAX is not exceeded. If the dwell beginning angle is positive, then check, if it can still be realized as an output by a tooth count. If the dwell beginning angle is so early that it can still be triggered after the elapsed program-time by a tooth count, a switch over to time comparison is carried out. If the program has already passed the comparative point of the timer, at which the dwell beginning should have been released, a forced closure is provoked and the charging time up to the ignition has to be awaited, the charging time being limited to a last possible ignition angle WMAX. If the dwell beginning can be calculated by measuring the tooth distance, the output is effected according to the above sketch.
12. StartSwinkel	Synchro	Conversion of the dwell beginning angle in comparative values for the Timer/comparison unit of the controller. Check, if the angle event is situated in a space, if this is the case, missing teeth are subtracted from the comparison value and are added to the residual increment. If the angle event is situated behind the space, only the missing teeth must be subtracted.

-----  
Ignition range 2  
-----

13. Z2_Ausgabe	Synchro	In that way the dwell beginning has been treated in processes 10-12, the ignition angle is processed in this case. As for the dwell event, the ignition event is connected to an angle event (tooth interrupt). The ignition is not released by awaiting the end of a charging time
----------------	---------	---



		<p>after the dwell beginning. In this case dwell beginning and ignition are individual, independent events. The ignition angle in the overlap-free range is directly taken out of the synchronous zwout-calculation (s.%ZUE). In the overlap range, the ignition angle is taken from the ignition angle stack (zwoutst0...zwoutst3). The ignition angle stack contains always the ignition angle belonging to the dwell beginning of the coil of the actual segment, already flown through by a current. The number of the described stack element is equal to the degree of overlapping. At a 3-fold overlap, the dwell beginning is situated 3 segments in advance of the ignition. The currently calculated ignition angle is written to zwoutst3. In the following segment, the ignition angle shifts to zwoutst2, after that to zwoutst1, and finally to zwoutst0. At a signalized overlap, The process Z2-output takes over the the ignition angle of zwoutst0.</p>
14. CheckPort	Synchro	<p>Checking of the output port. If a current is flowing through all of the coils, a dwell beginning has been triggered in the past. The particular number of such coils defines the overlap degree. Depending on the detected overlap degree, the processes Sw0_out, Sw1_out, Sw2_out, Sw3_out are called for the dwell masks and dwell event calculation, for no overlap up to a 3-fold overlap.</p>
15. Sw0_out	Synchro	<p>Calculation of the port mask for the dwell event release 0 overlaps. Check, if Sw2nd_out must be called. Calculation of the dwell angle. If the dwell beginning angle is situated in the past, a forced closure is effected and the call of Sw1_out. Limp-home/emergency measures and plausibility checks, as well as the signal processing correspond to those of the dwell beginning output in ignition range 1.</p>
16. Sw1_out	Synchro	<p>Calculation of the port mask for the dwell event output 1-fold overlap. Check, if Sw2nd_out must be called. Calculation of the dwell angle. If the dwell beginning angle is situated in the past, a forced closure is effected and call of Sw2_out. Limp-home/emergency measures and plausibility checks, as well as the signal processing correspond to those of the dwell beginning output in ignition range 1.</p>
17. Sw2_out	Synchro	<p>Calculation of the port mask for the dwell event output 2-fold overlap. Check, if Sw2nd_out must be called. Calculation of the dwell angle. If the dwell beginning angle is situated in the past, a forced closure is effected and the call of Sw3_out. Limp-home/emergency measures and plausibility checks, as well as the signal processing correspond to those of the dwell beginning output in ignition range 1.</p>
18. Sw3_out	Synchro	<p>Calculation of the port mask for the dwell event output 3-fold overlap. No call of Sw2nd_out, since the max. overlap degree has been reached. Calculation of the dwell angle. If the dwell beginning angle is situated in the past, a forced closure is effected. Limp-home/emergency measures and plausibility checks and the signal processing correspond to those of the dwell beginning output in ignition range 1.</p>
19. Sw2nd_out	Synchro	<p>Calculation of the port mask for the dwell event output for the next higher degree of overlap, from which the function has been started. Calculation of the dwell angle. If the dwell beginning angle is situated in the past, a forced closure is effected. Limp-home/emergency measures and plausibility checks and the signal processing correspond to those of the dwell beginning output in ignition range 1. For the second dwell event a separate dwell interrupt is used which also writes on the ignition port. This has the result, that the conventional dwell event calculation detects a correspondingly higher overlap degree in the next synchro.</p>
20. SlsnIR	HW-Trigger	<p>Dwell beginning interrupt: is called for the first time by the timer-comparison unit, when the tooth is reached behind which according to the calculation in the synchro, the dwell event is situated. In this case the duration of the last tooth period is measured and the residual angle up to the dwell beginning is converted into a time value. Afterwards the timer-comparison unit is switched from tooth comparison to angle comparison and the residual time up to the dwell beginning is loaded into a register of the timer comparison unit. If the residual time has elapsed, the timer comparison unit carries out the same interrupt a second time. This time, the ignition output mask calculated in the synchro is written in the port latch of the ignition port and is available as an output of the controller-periphery. In ignition range 1 or at the transition between no overlap/single overlap in ignition range 2, the timer-comparison unit is additionally switched to time comparison, the coil dwell period is loaded into the comparison register of the ignition interrupt and the ignition interrupt is released.</p>

21. Slsn2IR	HW-Trigger	Interrupt of the second dwell event in the case of an overlap operation after knocking. Functional principle as SlsnIR without functionality for ignition range 1 with dwell time output.
22. ZuendIR	HW-Trigger	Ignition interrupt: Is effected by the timer-comparison unit, if the tooth counter and the tooth calculated by the synchro behind which the ignition should start are identical.
23. SlsnMatch		Auxiliary processes for the ASCET-SD Simulation
24. Slsn2Match		Auxiliary processes for the ASCET-SD Simulation
25. ZuenMatch		Auxiliary processes for the ASCET-SD Simulation
22. HoleStack	Synchro	Stack shifted downwards by one element

### APP AZUE 5.40 Application hint

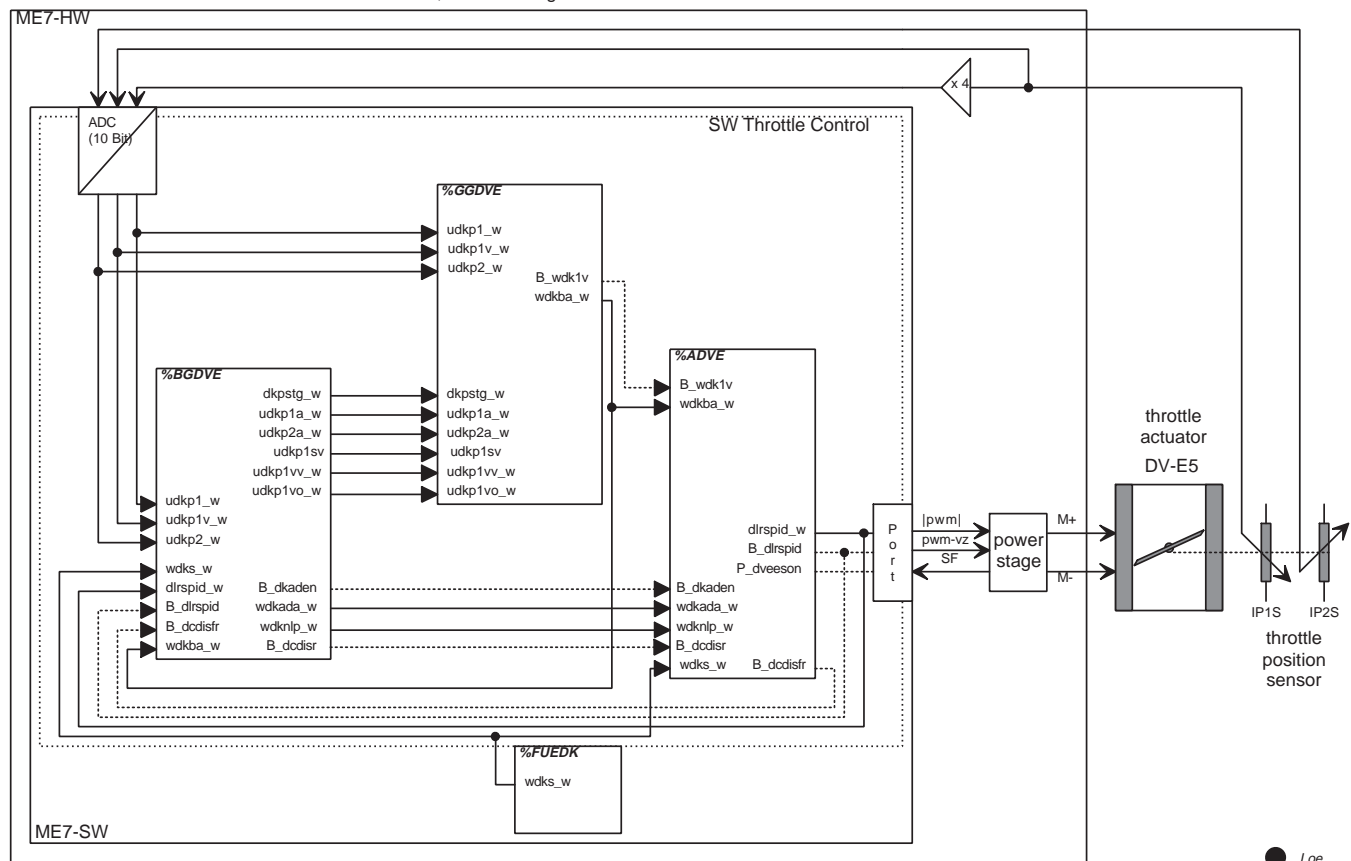
Switch-over of the ignition ranges by means of a program-constant:

NIST\_Z2 = 800/min

## DVEUE 1.0 Overview of DV-E-control

### FDEF DVEUE 1.0 Function definition

overview  
throttle control, command signals



dveue-dve-ans0

### ABK DVEUE 1.0 Abbreviations

### FW DVEUE 1.0 Fixed Values

Parameter	Value	Description
-----------	-------	-------------



## FB DVEUE 1.0 Detailed description of function

The trigger of the throttle adjustment device is sectionalized in following parts:

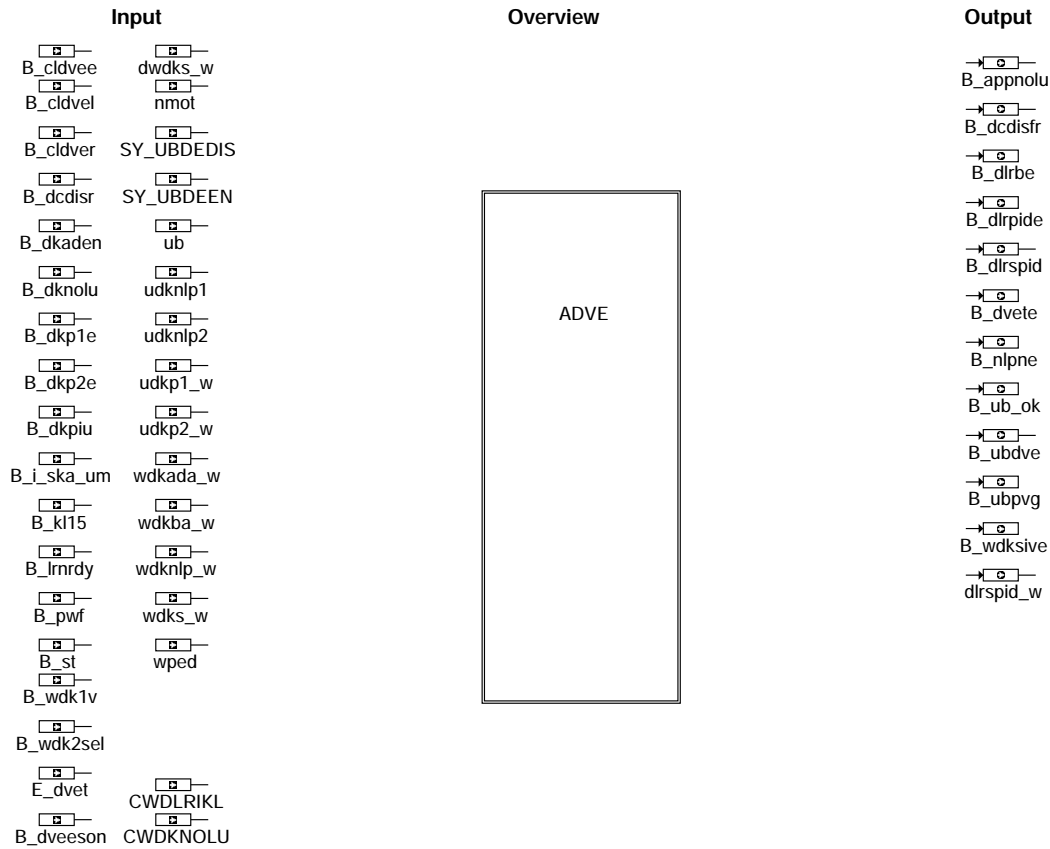
- block ADC: actual value with 10 Bit analog-digital converter
- FDEF GGDVE: standardization and check of actual value  
diagnosis
- FDEF BGDVE: learning of the lower mechanical DK limit stop (UMA learning)  
gain adjustment, offset and gradient  
learning and checking of the DV-E air at limphome position (NLP learning)  
DV-E return spring check  
diagnosis
- FDEF ADVE: digital position controller (DLR)  
coordination of the DV-E power stage release (disable/enable)  
monitoring of the DK position (DK at air in limphome position and DK setpoint/actual value)  
monitoring of the DLR setting range  
monitoring of battery voltage  
diagnosis

Parts of above-mentioned functions are implemented in the initialization or run after of the control device.

## APP DVEUE 1.0 Application hint

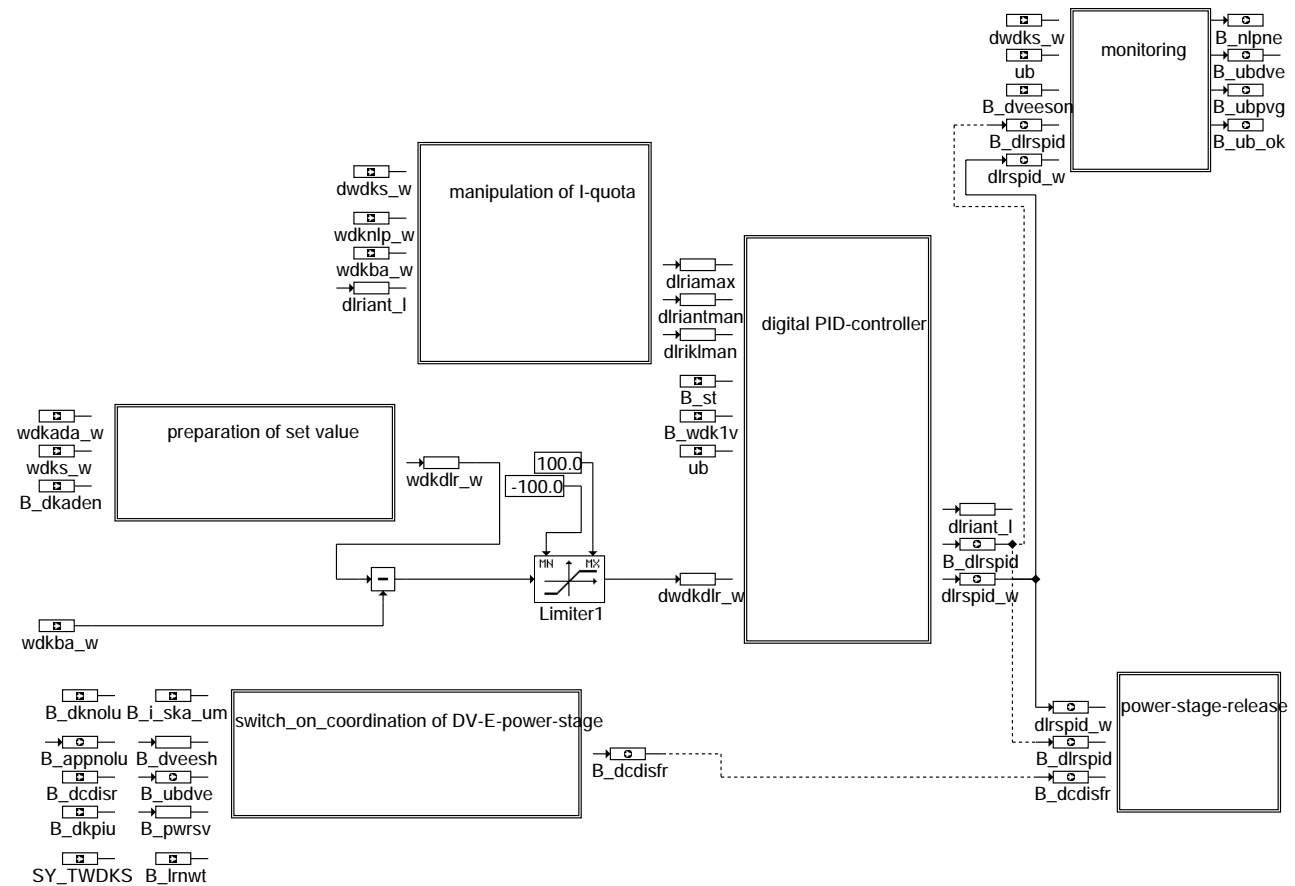
## ADVE 3.70 Activation of the DV-E by means of the DLR

### FDEF ADVE 3.70 Function definition

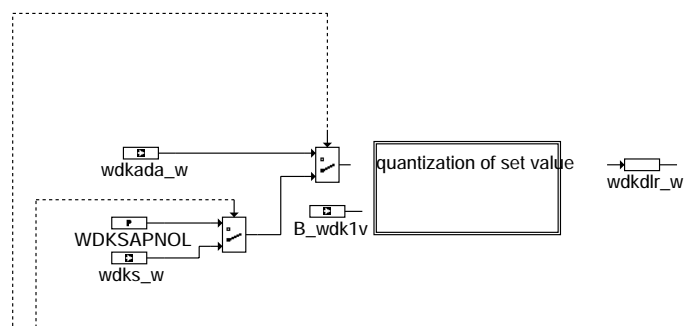


adve-main

adve-main



### adve-adve



### preparation of set value

### adve-preparation-of-set-value

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adve-adve

adve-preparation-of-set-value



Code of block DV-E powersave:

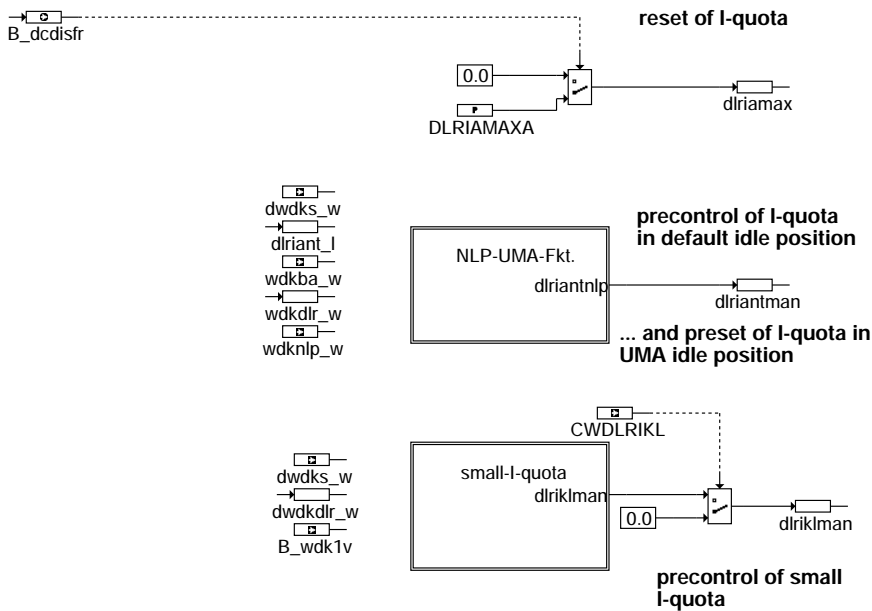
```

=====
-- task rate 10 ms

if ((( B_dkaden = false ) AND (wped = 0)
  AND (nmot = 0) #if (SY_TWDKS) then
  AND (B_cwdk = false) #endif))
then
  if ((dpwrsvc < TPWRSV))
  then
    -- Increment time counter for powersave
    dpwrsvc := dpwrsvc + 10 ms;
  else
    -- Demand DV-E power stage shutdown
    B_pwrsv := true;
  endif;
else
  -- Cancel time counter for powersave
  -- and DV-E power stage shutdown
  dpwrsvc := 0;
  B_pwrsv := false;
endif;

-- code of application help for DK limp-home operation
-- task rate 1000 ms

if (CWDKNOLU AND (nmot > 0))
then
  if (B_apnoluv = false)
  then
    B_apnoluv := true;
  endif;
else
  B_apnoluv := false;
endif;
  
```



**manipulation of I-quota**

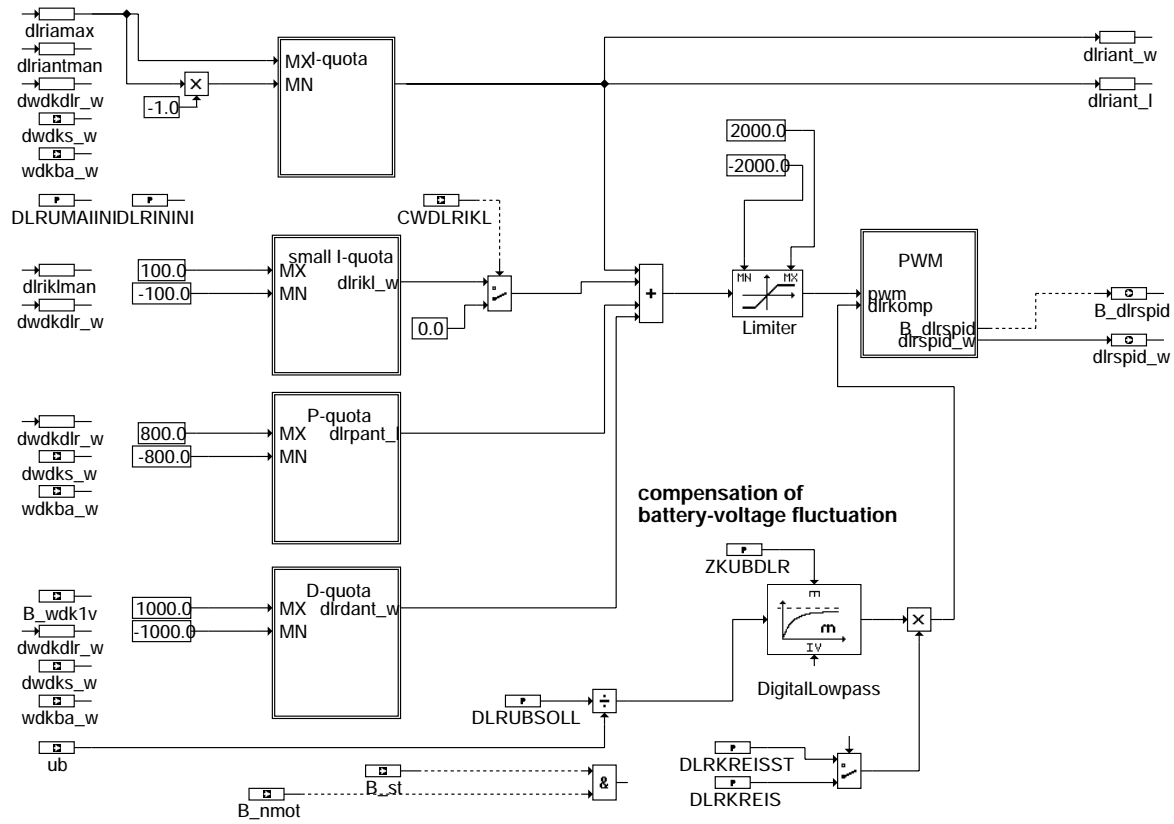
**please note: dlriantlp, dlrikman only serve for documentation purpose and do not exist as labels in ADVE 3.10**

adve-manipulation-of-i-quota

adve-manipulation-of-i-quota



## digital PID-controller

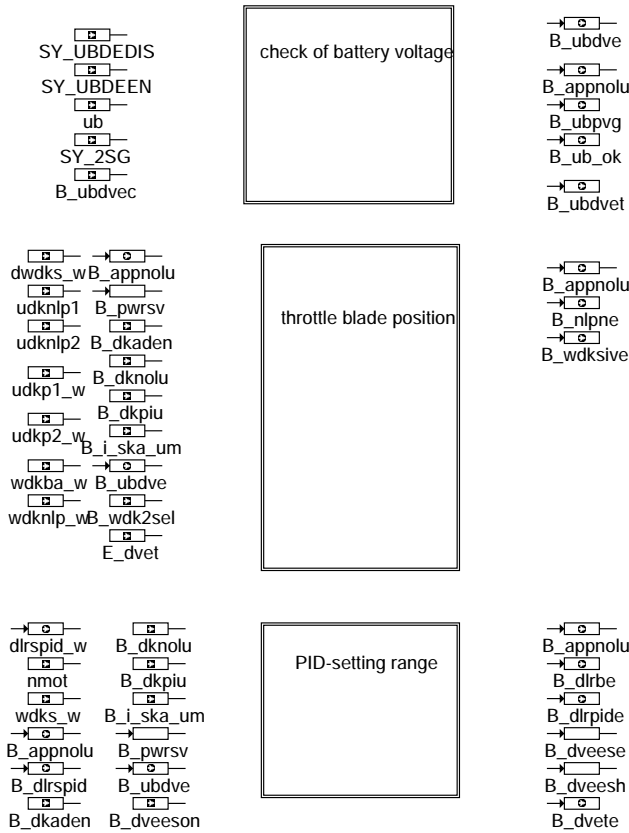


adve-digital-pid-controller

adve-digital-pid-controller



## monitoring



### adve-monitoring

Code of block throttle blade position:  
=====

```

-- monitoring of position from throttle blade
-- task rate: 20 ms
if ((B_dkpiu = false) AND (B_i_ska_um = false) AND B_ubdve
    # if (SY_2SG) then AND (B_dcdiscan = false) endif #)
then
    if ((B_dknolu) AND (B_appnolu = false))
    then
        -- monitoring DK-NLP during DK limp-home operation with application help
        if (E_dvet)
        then
            -- actuator replacement without adaptation, UMA not known, only the absolute
            -- potentiometer-voltage values at the limp-home can be monitored
            if (B_wdk2sel = false)
            then
                if ((udkp1_w > (udknlp1 + UDKNLPTOL))
                then
                    -- demand reversible SKA
                    B_nlpne := true;
                else
                    -- cancel reversible SKA
                    endif;
            else
                if ((udkp2_w < (udknlp2 - UDKNLPTOL))
                then
                    -- demand reversible SKA
                    B_nlpne := true;
                else
                    -- cancel reversible SKA
                    B_nlpne := false;
                endif;
            endif;
        else
            -- UMA known, relative NLP can be monitored
            if (wdkba_w > (wdknlp_w + WDKNLPTOL))
            then
                -- demand reversible SKA
                B_nlpne := true;
            else
                -- cancel reversible SKA
            endif;
        endif;
    endif;

```



```

        B_nlpne := false;
    endif;
endif;
else
-- monitoring DK tareget/actual values
if (B_dkaden = false)
then
-- transfer change in target value from FUEDK übernehmen and
-- form the absolute value.
-- ATTENTION: Range gwdk_w from -50 .. 0 .. +50 % DK
gwdk_kge := abs(gwkdldr_w);
-- determine permissble difference
-- determine the value from a table, without interpolation
dwkksimx := DWDKSBAMX(gwdk_kge);
if (abs(wdksfi_w - wdksba_w) > dwkksimx)
then
if (dklagerc > DKLAGERT)
then
-- fault-reaction time has elapsed, i.e.
-- set error flag to demand limp-home operation
-- without application help
B_appnolu := false;
B_wdksive := true;
else
-- increment fault counter
dklagerc := dklagerc + 20 ms;
endif;
else
-- decrement fault counter
dklagerc := dklagerc - TDKLAGDE;
-- and limit in the ECU to min 0
dklagerc := limit(0, dklagerc, DKLAGERT+20 ms);
endif;
-- filter DK target value with PT1 to predict
-- the DK actual value. Only use the filter value in the
-- next calculation schedule so that DK start-up
-- behavior will be considered (PT2)
wdksfi_w := wdksfi_w + (wdkdlr_w - wdksfi_w) * ZKWDKSPT1;
endif;
endif;
endif;

```

Code of block PID-setting range:  
=====

```

-- monitoring of PID-setting range
-- task rate: 10 ms
if ((B_dknolu = false) OR (B_dknolu AND B_appnolu)
# if (SY_2SG) then AND (B_dcdiscan = false) endif #)
AND (B_dkpiu = false)
AND (B_i_ska_um = false))
then
if (B_ubdve AND (B_dkaden = false)
AND (B_pwrsv = false))
then
if ((dlrspid_w > DLRPIDMAX) AND B_dlrspid)
then
-- range exceeded
FKT_DLRBER-Test();
else
if ((dlrspid_w > DLRPIDMIN) AND (B_dlrspid = false))
then
-- range exceeded
FKT_DLRBER-Test();
else
-- Cancel reversible SKA
B_dlrbe := false;
-- decrement fault counter
dlrpdc := dlrpdc - TDLRPIDDEC;
dlrpdc := limit (0, dlrpdc, DLRPID2T + 10 ms);
-- cancel debounce counter and shutdown demand
dveesc := 0;
B_dveesh := false;
endif;
endif;
endif;
else
-- decrement fault counter
dlrpdc := dlrpdc - TDLRPIDDEC;
dlrpdc := limit (0, dlrpdc, DLRPID2T + 10 ms);
-- reset debounce counter
dveesc := 0;
-- cancel extended actuator-exchange detection
B_dvete := 0;
endif;
endif;

```



```

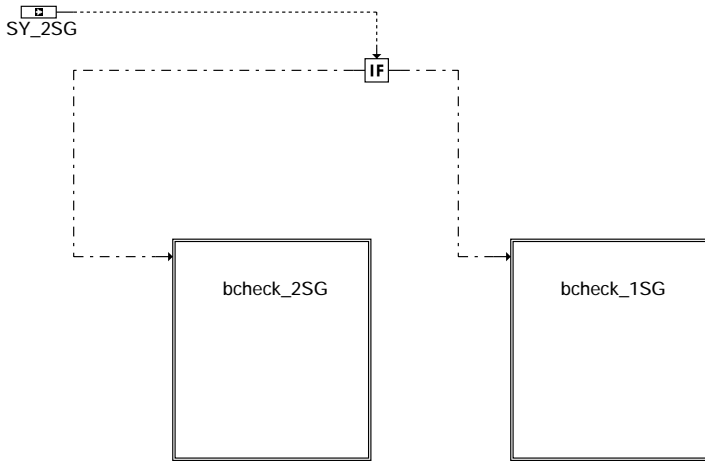
-- function FKT_DLRBER-Test()

if (dlrpidc > DLRPID2T)
then
  -- the HW port, B_dveeson, to be inquired
  -- in the following, constitutes the status
  -- flags for the DV-E power-stage port.
  -- e.g. status flag at P3.15,
  -- it applies for DV-E-ES CJ220 that status = ok,
  -- when the line is on 'high'.
  -- i.e. it applies that P_dveeson = P3.15
  if (B_dveeson = false)
  then
    -- set DV-E power-stage fault
    B_dveese := true;
  endif;
  -- set fault 'DLR control range at limit', and
  -- by this, signal DK limp-home operation without
  -- application help as the desired reaction
  B_dlrpidc := true;
  B_appnolu := false;
else
  if (dlrpidc > DLRPID1T)
  then
    -- demand reversible SKA
    B_dlrbe := true;
    B_appnolu := false;
  else
    if ((dlrpidc > DLRPID0T) AND (wdkdlr_w < WDKETE)
        AND (nmot = 0) AND (B_dlrspid = false) )
    then
      -- extended actuator-exchange detection
      B_dvete := true;
    endif;
  endif;
endif;

-- increment fault counter
dlrpidc := dlrpidc + 10 ms;
if (P_dveeson = false)
then
  -- DV-E power-stage restart test
  if (dveesc >= DVEEST)
  then
    -- cancel shutdown demand for DV-E power stage.
    -- A negative flank is generated by this. This
    -- flank can activate the power stage again.
    B_dveesh := false;
  else
    -- increment debounce counter
    dveesc := dveesc + 10 ms;
    if (dveesc >= DVEEST)
    then
      -- set shutdown demand for DV-E power stage,
      -- to be able to generate a negative flank
      -- for activating the power stage by subsequently
      -- canceling the demand for shutdown.
      B_dveesh := true;
    endif;
  endif;
else
  -- reset debounce counter
  dveesc := 0;
endif;
endif;

```

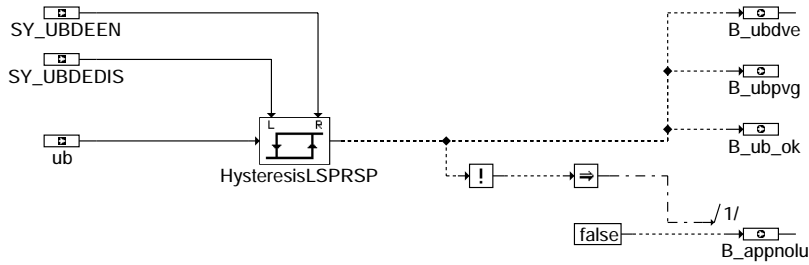
If a fault occurs it will be analyzed in the function SREAKT7.xx. Depending on what kind of fault has been detected SREAKT7.xx will switch the system to (DK limp-home operation, DK potentiometer limp-home, SKA ).



**check of battery voltage**

adve-check-of-battery-voltage

if (SY\_2SG = false) then

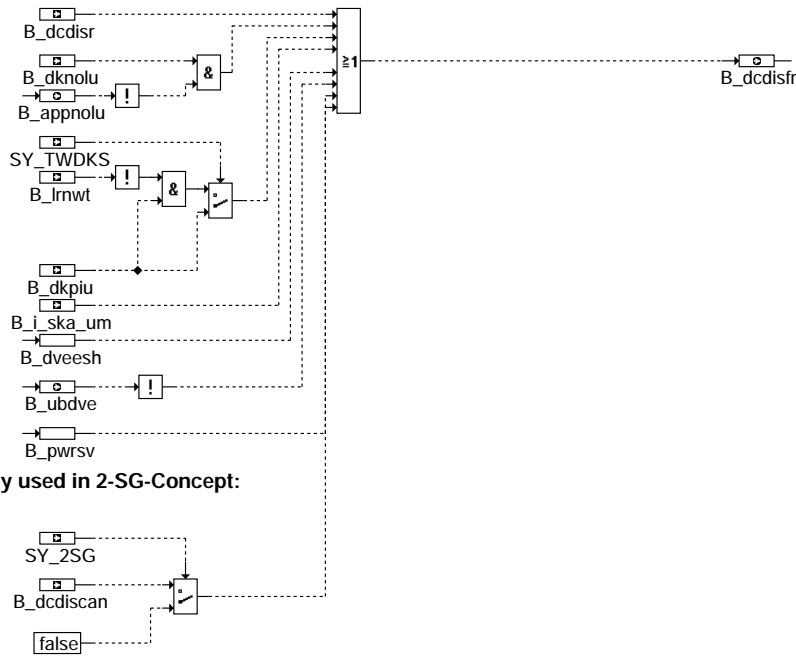


**check of battery-voltage in 1\_SG\_Concept**

adve-bcheck-1sg

adve-check-of-battery-voltage

adve-bcheck-1sg



switch on coordination of DV-E-power-stage

adve-switch-on-coordination-of-dv-e

### ABK ADVE 3.70 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DANTGESWNV			FW	Threshold for activation of D component (speed) in the non-amplified range
DANTGESWV			FW	Threshold for activation of D component (speed) in the amplified range
DANTSCHWNV			FW	Threshold for activation of D component (deviation) in the non-amplified range
DANTSCHWV			FW	Threshold for activation of D component (deviation) in the amplified range
DKLAGERT			FW	Permissible fault time for DK setpoint/actual comparison
DLRDWDKSS1			FW	DLR, upper limit for the parameter switch-over
DLRDWDKSS2			FW	DLR, lower limit for the parameter switch-over
DLRIAMAXA			FW	Maximum permissible I-component
DLRIKLPAR			FW	DLR, I small parameter
DLRINIINI			FW	I-component during init for ramp passing through NLP
DLRKDONLP0			FW	DLR, D parameter above NLP
DLRKDUNLP0			FW	DLR, D parameter below NLP (weak)
DLRKDUNLP1			FW	DLR, D parameter below NLP (medium)
DLRKDUNLP2			FW	DLR, D parameter below NLP (strong)
DLRKIONLP0	DWDKDLR_W		KL	I component as f(abs(dwkdldr.w)), above NLP
DLRKIUINLP0	DWDKDLR_W		KL	I component as f(abs(dwkdldr.w)), below NLP (weak)
DLRKIUINLP1	DWDKDLR_W		KL	I component as f(abs(dwkdldr.w)), below NLP (medium)
DLRKIUINLP2	DWDKDLR_W		KL	I component as f(abs(dwkdldr.w)), below NLP (strong)
DLRKPONLP0			FW	DLR, P parameter above NLP
DLRKUNLP0			FW	DLR, P parameter below NLP (weak)
DLRKUNLP1			FW	DLR, P parameter below NLP (medium)
DLRKUNLP2			FW	DLR, P parameter below NLP (strong)
DLRKREIS			FW	DLR, factor loop gain
DLRKREISSST			FW	DLR, factor loop gain at the time of the engine start
DLRNLPD			FW	Fuzzy range of DK in limphome air position
DLRPID0T			FW	Timecounter for extended DV-E-exchange detection
DLRPID1T			FW	Permissible fault time 1 for DLR setting range at the limit stop
DLRPID2T			FW	Permissible fault time 2 for DLR setting range at the limit stop
DLRPIDMAX			FW	Max. permissible PWM pulse duty factor for DLR
DLRPIDMIN			FW	Min. permissible PWM pulse duty factor for DLR
DLRUBSOLL			FW	DLR, battery standard voltage
DLRUMABAND			FW	Range of uncertainty during the step change out of the UMA range
DLRUMAIINI			FW	Default value of the I component during the step change out of the UMA range
DVEEST			FW	Time for the healing attempt of the DV-E-power stage
DWDKSIKLS			FW	Threshold for the activation of the I small component
KDLRIDDVE			FW	Identification of the DLR parameter block regarding DV-E type
TDKLAGDE			FW	Time delta for clearing of fault counter with DK setpoint/actual comparison
TDLRPIDC			FW	Timstep for decrementing of dlripdc
TPWRSV			FW	Waiting time before DV-E Powersave becomes active
UDKNLPTOL			FW	Tolerance of DK-potentiometer signal in limphome position
WDKBWS			FW	Threshold for the DK movement detection (I-small)
WDKETE			FW	Upper limit of DK-set value with DV-E extended exchange detection active
WDKNLPTOL			FW	Permissible DK angle tolerance of the NLP
WDKREIB			FW	Frictional component of the DK I small
WDKSAPNOL			FW	DK-set value used with application supply DK at air in limphome position
WDKSTFEIN			FW	Threshold for detection of steady-state (amplified range)



Parameter	Source-X	Source-Y	Type	Description
WDKSTGROB			FW	Threshold for detection of steady-state (non-amplified range)
ZKUBDLR			FW	DLR, time constant for filtering of Ubatt
ZKWDKSPT1			FW	Time constant for prediction of DK angle from setpoint
Variable	Source		Type	Description
B.APNOLUV	ADVE		LOK	Latch: Application supply DK at air in limphome position
B.APPNOLU	ADVE		AUS	Condition: Throttle limp-home air driving requested by application
B.CLDVEE			EIN	Flag for clearing measures: DV-E power stage
B.CLDVEL			EIN	Flag for clearing measures: DV-E position deviation
B.CLDVER			EIN	Flag for clearing measures: DV-E deviation
B.DCDISCAN	SREAKT		EIN	Condition: DV-E power-stage-switch-off because of CAN-ERROR
B.DCDISFR	ADVE		AUS	Condition: Disable DV-E power stage by means of the funct. processor
B.DCDISR	BGDVE		EIN	Condition: DV-E power stage deactivation is requested
B.DKADEN	BGDVE		EIN	Condition: Use DK setpoint from DK adaptation and DK check
B.DKBEW	ADVE		LOK	Condition: Throttle valve has moved
B.DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B.DKP1E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 1
B.DKP2E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 2
B.DKPIU	SREAKT		EIN	Condition: irreversible SKA
B.DLRBE	ADVE		AUS	Condition: DLR correction range exceeded
B.DLRIKLA	ADVE		LOK	Condition: DLR, I-small active
B.DLRIKLST	ADVE		LOK	Condition: First run of I-small after start
B.DLRPARC	ADVE		LOK	Condition: desired value step change is about to happen
B.DLRPIDE	ADVE		AUS	Condition: Fault, DLR correction range at limit
B.DLRSPID	ADVE		AUS	Condition: DLR, sign of sum of the PID-components, = 1: positiv, =0: negative
B.DLRUMZU	ADVE		LOK	Condition: NLP reloading is permitted
B.DVEESE	ADVE		LOK	Condition: DV-E power stage fault
B.DVEESH	ADVE		LOK	Condition: DV-E power stage healing
B.DVEESON			EIN	Condition: DV-E-poe-stage is switches on (= P.dveeson)
B.DVETE	ADVE		AUS	Condition: Extended DV-E-exchange detection
B.KLREST	ADVE		LOK	Condition: Re-triggering of I-small
B.KLSTAR	ADVE		LOK	Condition: I-small shall start
B.J_SKA_UM	UFREAC		EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B.KL15			EIN	condition ignition switch on
B.LRNRDY	BGDVE		EIN	learning complete
B.LRNWT			EIN	Condition: DV-E adaptions activated by tester at end of intake-module-production
B.NLPNE	ADVE		AUS	Condition: NLP not reached for DK standby trip
B.NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B.PWF			EIN	Condition for powerfail
B.PWRSV	ADVE		LOK	Condition: DV-E-powersave active
B.ST	SWADAP		EIN	condition for start
B.JBDVE	ADVE		AUS	Condition: Battery voltage for DV-E control OK
B.JBDVEC			EIN	CAN-Receive-Message: 2.SG has low voltage
B.JBDVET	ADVE		AUS	CAN-Send-Message:1.SG has low voltage and sends this information to 2.SG
B.JBPGV	ADVE		AUS	condition: battery voltage sufficient for 5-V potentiometer supply
B.JB_OK	ADVE		AUS	Battery voltage o.k.
B.WDK1V			EIN	Condition: amplified signal from potentiometer 1 used to calc. throttle angle
B.WDK2SEL	GGDVE		EIN	Condition: DV-E position control is performed with actual-value-poti 2
B.WDKSIVE	ADVE		AUS	Condition: Fault in comparing DK angle nominal value/actual value
CWDKNOLU			EIN	Codeword: Application supply DK at air in limphome position
CWDLRIKL			EIN	Codeword: DLR-small-I-quota is activ
DKLAGERC	ADVE		LOK	Fault counter DK position monitoring
DLRBATKP_W	ADVE		LOK	Compensation factor for fluctuation UBatt
DLRD	ADVE		LOK	DLR, D-parameter
DLRDANT_W	ADVE		LOK	D component
DLRDSV_W	ADVE		LOK	Threshold for activation of D component (speed)
DLRDSW_W	ADVE		LOK	Threshold for activation of D component (deviation)
DLRI	ADVE		LOK	DLR, I-parameter
DLRIAMAX	ADVE		LOK	DLR, maximum possible I-component
DLRIANTMAN	ADVE		LOK	For documentation only: precontrol of I-quota in default idle position
DLRIANT_I	ADVE		LOK	DLR, I component
DLRIANT_W	ADVE		LOK	DLR, I-component, high word of dlriant_I
DLRIKLMAN	ADVE		LOK	
DLRIKLST_W	ADVE		LOK	Input value i small component
DLRIKL_W	ADVE		LOK	DLR, I small component
DLRKOMP	ADVE		LOK	DLR, factor loop gain
DLRP	ADVE		LOK	DLR, P-parameter
DLRPANT_I	ADVE		LOK	DLR, P component
DLRPIDC	ADVE		LOK	Fault counter DLR setting range monitoring
DLRRAST	ADVE		LOK	DLR task counter
DLRSPID_W	ADVE		AUS	DLR for DV-E: Sum of the PID-components
DPWRSVC	ADVE		LOK	Timecounter for DV-E power stage
DWDKDLR_W	ADVE		LOK	Difference-DK-angle setpoint - act. value (wdkdlr_w - wdkba_w)
DWDKS_KGE	ADVE		LOK	Change of the throttle valve setpoint angle, absol.value for charact.line input
DWDKS_W	FUEDKSA		EIN	modification of desired throttle angle
E_DVET	DDVE		EIN	Errorflag: DV-E-exchange detection
NMOT	SWADAP		EIN	engine speed
SY_2SG	PROKON		EIN	system constant 2 motronic systems
SY_TWDKS			EIN	system constant: input of desired angle DVE via tester is possible
SY_UBDEDIS	PROKON		EIN	Ubatt threshold for disabling the DV-E output stage
SY_UBDEEN	PROKON		EIN	Ubatt threshold for enabling the DV-E output stage



Variable	Source	Type	Description
UB	SWADAP	EIN	battery voltage
UDKNLP1		EIN	Voltage DK-Poti 1 at the NLP
UDKNLP2		EIN	Voltage DK-Poti 2 at the NLP
UDKP1_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UDKP2_W		EIN	sensor voltage from throttle potentiometer 2 (word)
WDKADA_W	BGDVE	EIN	Setpoint DK-angle, from DV-E adaptation function and check function
WDKBAALT_W	ADVE	LOK	Old Throttle valve actual value to determine the D component
WDKBAS_W	ADVE	LOK	Throttle valve actual value for the movement detection for I-small
WDKBA_W	GGDVE	EIN	throttle angle with respect to lower mechanical stop
WDKDLR_W	ADVE	LOK	Setpoint DK-Angle in 12 Bit-Resolution
WDKNLP_W	BGDVE	EIN	throttle angle in the limphome air position
WDKSFL_W	ADVE	LOK	Predicted DK angle from wdks_w
WDKSSTSW_W	ADVE	LOK	Threshold for steady-state detection for I-small
WDKS_W	MSF	EIN	desired throttle angle w.r.t. to lower mechanical stop
WPED	GGPED	EIN	Standardized accelerator pedal angle

## FW ADVE 3.70 Fixed Values

Parameter	Value	Description
DANTGESWNV		Threshold for activation of D component (speed) in the non-amplified range
DANTGESWV		Threshold for activation of D component (speed) in the amplified range
DANTSCHWNV		Threshold for activation of D component (deviation) in the non-amplified range
DANTSCHWV		Threshold for activation of D component (deviation) in the amplified range
DKLAGERT		Permissible fault time for DK setpoint/actual comparison
DLRDWDKSS1		DLR, upper limit for the parameter switch-over
DLRDWDKSS2		DLR, lower limit for the parameter switch-over
DLRIAMAXA		Maximum permissible I-component
DLRIKLPAR		DLR, I small parameter
DLRINIINI		I-component during init for ramp passing through NLP
DLRKDONLP0		DLR, D parameter above NLP
DLRKDUNLP0		DLR, D parameter below NLP (weak)
DLRKDUNLP1		DLR, D parameter below NLP (medium)
DLRKDUNLP2		DLR, D parameter below NLP (strong)
DLRKPONLP0		DLR, P parameter above NLP
DLRKUNLP0		DLR, P parameter below NLP (weak)
DLRKUNLP1		DLR, P parameter below NLP (medium)
DLRKUNLP2		DLR, P parameter below NLP (strong)
DLRKREIS		DLR, factor loop gain
DLRKREISST		DLR, factor loop gain at the time of the engine start
DLRNLDP		Fuzzy range of DK in limphome air position
DLRPIDOT		Timecounter for extended DV-E-exchange detection
DLRPID1T		Permissible fault time 1 for DLR setting range at the limit stop
DLRPID2T		Permissible fault time 2 for DLR setting range at the limit stop
DLRPIDMAX		Max. permissible PWM pulse duty factor for DLR
DLRPIDMIN		Min. permissible PWM pulse duty factor for DLR
DLRUBSOLL		DLR, battery standard voltage
DLRUMABAND		Range of uncertainty during the step change out of the UMA range
DLRUMAIINI		Default value of the I component during the step change out of the UMA range
DVEEST		Time for the healing attempt of the DV-E-power stage
DWDKSIKLS		Threshold for the activation of the I small component
KDLRIDVE		Identification of the DLR parameter block regarding DV-E type
TDKLAGDE		Time delta for clearing of fault counter with DK setpoint/actual comparison
TDLRPIDC		Timestep for decrementing of dlrpidc
TPWRSV		Waiting time before DV-E Powersave becomes active
UDKNLPTOL		Tolerance of DK-potentiometer signal in limphome position
WDKBEWS		Threshold for the DK movement detection (I-small)
WDKETE		Upper limit of DK-set value with DV-E extended exchange detection active
WDKNLPTOL		Permissible DK angle tolerance of the NLP
WDKREIB		Frictional component of the DK I small
WDKSAPNOL		DK-set value used with application supply DK at air in limphome position
WDKSTFEIN		Threshold for detection of steady-state (amplified range)
WDKSTGROB		Threshold for detection of steady-state (non-amplified range)
ZKUBDLR		DLR, time constant for filtering of Ubatt
ZKWDSPT1		Time constant for prediction of DK angle from setpoint

## FB ADVE 3.70 Detailed description of function

### 0. Overview

=====

1. Introduction
2. Initialization
3. DK position control
  - 3.1 DK setpoint and DK actual value
  - 3.2 DV-E power-save
  - 3.3 Application supply 'DK at air in limphome position'
  - 3.4 Pre-control of the I component
  - 3.5 Compensating the battery voltage fluctuations
  - 3.6 Digital PID controller
4. DV-E power stage triggering
5. Coordination of the DV-E power stage release
6. Monitoring of battery voltage





- 7. Monitoring of the DK position
  - 7.1 Monitoring of the DK at air in limphome position
  - 7.2 Monitoring of the DK setpoint/actual value
- 8. Monitoring of the DLR setting range
- 9. Protection of DV-E power stage from overheating during hot idling
- 10. Diagnosis
  - 11. Function to suppress shutdown rattling

1. Introduction  
=====

The task of the function is to trigger the throttle adjustment device (DV-E) and to diagnose faults in the triggering circuit. The position of the throttle blade (DK) is controlled by a digital position controller (DLR), which transfers a PWM pulse duty factor and a directional bit to the DV-E power stage (DV-E-ES). The DV-E-ES is designed as an integrated H-bridge with internal current limitation. The input values are for one the DK setpoint (wdks\_w), which is generated in the function FUEDK and for the other the DK actual value (wdkba\_w), which is formed in the function GGDVE.

Furthermore the position control loop is monitored for non-permissible desired / actual deviations (wdks\_w to wdkba\_w), for the setting signal exceeding the range (dlrspid\_w with B\_dlrspid) and for the operating state of the DV-E-ES (B\_dveesson).

2. Initialization  
=====

During the initialization fixed values are written into the following RAM cells:

```

B_dlrparc := true
B_dlrsumzu := true
B_ubdve := true
B_ubpvg := true
B_ubok := true
dlrbatkp_w := 1.0
dlrkomp := DLRKREIS
dlrd := DLRKDONLPO
dlri := 1.0
dlrp := DLRKPONLPO
dlrhaftak := DLRHAFTMN/DLRKREIS
dlrini_w := DLRININI/DLRKREIS
    
```

Additionally in systems with main relay for supply of DV-E5 during SG-run after with K1.15 OFF (only if SY\_UBR = true) adaption of quantization:

```

ubdedis := SY_UBDEDIS * SY_UBSQ_W
ubdeen := SY_UBDEEN * SY_UBSQ_W
dlrbrsq := DLRUBSOLL * SY_UBSQ_W
    
```

3. DK position control  
=====

3.1 DK setpoint and DK actual value  
=====

The setpoint for the DK position control is supplied by the FUEDK as a 16 bit value (wdks\_w). Since the DK actual value (wdkba\_w) is given with a maximum resolution of 0,0244 %DK (100 %DK / (2<sup>e12</sup> - 1)) in the amplified and of 0,0978 %DK (100 %DK / (2<sup>e10</sup> - 1)) in the remaining (non-amplified) range, the setpoint must be matched to the actual value. At first the setpoint is shifted to the right by 4 bit positions, this complies with a resolution of 12 bit. For the non-amplified range (B\_wdklv = false) the setpoint is additionally combined by an AND with the bit mask 0x0FFCh so that the resolution is 10 bit.

During adaptation- and UMA-learning the set value for DK comes from function BGDVE, this is enabled by (B\_dkaden = true). If 'application supply DK in air limphome position is active' (B\_appnolu = true) set value can be adjusted via the Label WDKSAPNOLU.

If (B\_dksbeg = true) DK-Setvalue will be limited according to DKNOTBEGR(nmot).

The DK actual value wdkba\_w must have been updated by the GGDVE for the 1 ms - cycle of the DLR prior to the call-up of the DLR. The max. dead time between AD conversion and output of the DLR pulse duty factor may not exceed 0,2 ms. The shorter this dead time, the better it is for the control behaviour.

3.2 DV-E powersave  
=====

To avoid unnecessary load of the car-battery the DV-E power stage is switched off automatically after a waiting time TPWRSV. This is only done if the engine does not turn (nmot = 0) and if the driver does not move the accelerator (wped = 0). Then the bit B\_pwrsv := true is set to request a switch off of the DV-E powerstage. If the driver starts the engine (nmot != 0) or moves the accelerator B\_pwrsv will be reset and the DV-E power stage can be switched on immediately.

In OPEL-Projects powersave-function does not become active when test of



position system is performed when tester sends B\_cwdk = true. (only when SY\_TWDKS = 1).

### 3.3 Application supply DK at air in limphome position =====

This function shall support the application engineer when driving with DK at air in limphome position. Setting the codeword CWDKNOLU triggers the bit B\_appnolu and this bit activates driving with DK at air in limphome position in the function SREAKT (B\_dknolu is set in SREAKT). When triggered this way driving with DK at air in limphome position will not be done with DV-E powers stage switched off. DV-E powerstage remains switched on and set value for the DK can be adjusted via WDKSAPNOLU. Monitoring of the DK at air in limphome position (see 7.1) is not active. If an error occurs (B\_dkple OR B\_dkp2e OR B\_i\_ska\_um OR !B\_ubdve OR B\_wdksive OR B\_dlrpide OR B\_dlrbe) bit B\_appnolu will be reset immediately. This guarantees that a real error has priority. B\_appnolu can only be retriggered when C\_wdknolu is set true  
-- > false -- > true.

### 3.4 Reset iof the I-component in the static-friction case =====

If an untypically high static-friction component occurs during a DV-E at high temperatures below the NLP in addition to the torque from the opening spring, then the I-component will be drawn to an unnecessarily large value during control of the nominal-actual deviation. This is drawn to such an extent that the maximum permissible continuous current of the DV-E will be exceeded. The current I-component is reset in this case to the minimum I-component necessary with the help of the criteria listed in the following.

Code of block reduction of I-quota in case of static friction

```
-- task rate: 50 ms

if (B_dlrrien)
then
  if ((highword)dlriant_l < dlrhaftak) AND
    (abs(dwgks.w) <= DLRHAFTST)
  then
    if (dlrihaftc > TDLRHAFTMX)
    then
      (highword)dlriant_l := dlrhaftak;
      dlrihaftc := 0;
    else
      dlrihaftc := dlrihaftc + 50 ms;
    endif;
  else
    dlrihaftc := dlrihaftc - 50 ms;
    dlrihaftc := lilmit(0,dlrihaftc, TDLRHAFTMX);
  endif;
endif;
```

### 3.5 Pre-control of the I component =====

Due to the strongly non-linear control system the I component is manipulated by a pre-control in case of a DK movement through the limphome air point (NLP) and out of the UMA range.

If the DK is in the vicinity of the UMA then the I component will increase to large negative values due to the strongly increased friction. For this reason the I component is set to the smaller default value DLRUMAIINI, if the DK setpoint rises above the threshold DLRUMABAND and if the I component has increased to more than DLRUMAIINI.

In case of a movement of the DK through the NLP a torque step change with a reversal of direction of movement takes place there. This step change is compensated with a delta I component DLRININI. The sequence of this pre-control is described below:

Code of block pre-control of I component at air in the limphome position:

```
-- for closing direction
if (wdkdlr.w < (wdknlp.w - DLRNLPD) AND B_dlrsumzu)
then
  if (abs(wdkba.w - wdknlp.w) > DLRNLPD)
  then
    (highword)dlriant_l := (highword)dlriant_l - DLRININI
  endif
  -- turn reversal of movement of direction
  B_dlrsumzu = false
endif
-- for opening direction
if (wdkdlr.w > (wdknlp.w + DLRNLPD) AND (B_dlrsumzu = false))
then
  if (abs(wdkba.w - wdknlp.w) > DLRNLPD)
  then
    (highword)dlriant_l := (highword)dlriant_l + DLRININI
  endif
  -- turn reversal of movement of direction
```



```
B_dlrsumzu = true  
endif
```

The highword of `dlriant_l` is available in `dlriant_w` for measurements with the VS100.

### 3.6 Compensation of the battery voltage fluctuation =====

Since a fluctuation of the battery voltage has a direct proportional effect on the loop gain of the DLR, this effect was compensated via a function. The battery voltage `ub` is filtered via a PTL with the constant `ZKUBDLR`. The compensation, however, does have its limits in case of start. The starter can lower the battery voltage with a weak battery so far that in spite of compensation the DK can be stimulated to vibrate. In order to diffuse this case, a switch-over to an individual loop gain `DLRKREISST` is performed during the start (`B.st = true`). Therefore a little slower DK movement does not influence the starting behaviour.

### 3.7 Digital PID controller =====

The control structure consists of a PID controller, however, here the D component is only formed with the actual value. The non-linearities of the system are taken into consideration in the characteristic lines for the I component as well as in the range-dependent parameters. A moving of the DK through the NLP of the DV-E is supported by reloading the I component, see chapter 3.2.

The controller is processed in a 1 ms basic cycle and in a 1 ms cycle transposed 3 times (corresponds to a 3 ms cycle).

The control deviation `dwkdlr_w`, the D component, the sum of all control components (`dlriant_l`, `dlrikl_w`, `dlrpant_l` and `dlrdant_w`) and the PWM signal (absolute value `dlrspid_w` and sign `B_dlrspid`) are calculated in the 1 ms cycle (see picture DLR in the block `FDEF`). The D component is limited to  $\pm 1000 \% \text{PWM}$ . In addition the value (`dlrkomp`) resulting from the compensation and from the changed loop gain is included in the calculation prior to the PWM signal being made available. The PWM signal is limited to  $\pm 100 \% \text{PWM}$ .

In the 3 ms cycle the individual cycles are processed in the counting mode 2 1 0 2 1. In cycle 2 the I small component `dlrikl_w` is calculated. The I small component is used to tear away the DK from the static friction. This I small component is limited to  $\pm 100 \% \text{PWM}$ . In cycle 1 the control parameters in dependency on the DK position (above/below NLP with `wkba_w`) and below the NLP (`wkba_w < wdknlp_w`) in dependency on the steepness of the step change of the DK setpoint (`gwkdldr_w`) are determined. Furthermore, here the I component `dlriant_l` is calculated and limited to  $\pm \text{dlriamax}$ . In cycle 0 the P component is calculated and limited to  $\pm 1000 \% \text{PWM}$ .

The I small component can be switched off with codeword `CWDLRIKL = false`.

A separate set of parameters is available for operating the DV-E5 with a no-gain potentiometer (`B.wdklv = false`) below the NLP.

### 4. DV-E power stage triggering =====

The setting signal given by the DLR is converted into a PWM signal with absolute value (`dlrspid_w`) and direction signal (`B_dlrspid`) and transferred to the DV-E power stage (DV-E-ES) via the functional processor (FR). The PWM frequency is 2000 Hz.

### 5. Coordination of the DV-E power stage release =====

Here the deactivation requests from various functions are combined in a resulting bit `B_dcdisfr`. This bit supplies the port of the FR, which supplies the disable line of the DV-E-ES. Representation in the block `FDEF` in the overview diagram part coordination of the DV-E power stage release

### 6. Monitoring of the battery voltage =====

For a faultless operation of the DV-E with the DV-E-ES a minimum supply voltage is required. So that the DV-E-ES does not constantly switch ON / OFF in case of undervoltage, the ES is therefore switched by means of a hysteresis (`SY_UBDEEN` and `SY_UBDEDIS`) via the bit `B_ubdve`. Furthermore a bit `B_ubpv` is supplied with this undervoltage detection, which blocks resp. enables the plausibility check of the potentiometer actual values of the PWG and the DV-E. See picture check of battery voltage in the block `FDEF`.

The differentiation in battery-voltage monitoring is made for systems with an additional measuring path for the DV-E5 `ubrsq` supply voltage after the main relay only for conditional compiling (`SY_UBR = true`):  
Plausibility check of the DV-E5 voltage, `ubrsq`, by comparison with the hysteresis thresholds `ubdedis` and `ubdeen`. (Refer also to: 2nd initialization.)  
Plausibility check of the HFM and DV-E potentiometer supply voltage at terminal 15, `wub`, using the hysteresis thresholds `SY_UBDEDIS` and `SY_UBDEEN`.



## 7. Monitoring of DK position

=====

Representation in the block FDEF in the picture monitoring of position of throttle blade.

### 7.1 Monitoring of the DK with air at limphome position

=====

In case of the DK drive default function ( $B\_dknolu = 1$ ) it is checked whether the DK is not further above the DK-NLP than the range permits ( $wdkba\_w \leq (wdknlp\_w + WDKNLPOL)$ ). As long as the DK has not reached the DK-NLP during the transition from normal operating to the DK drive default function, reversible safety fuel deactivation (rev. SKA) is requested.

If 'application support DK with air at limphome position' is used ( $B\_appnolu = true$ ) monitoring of the DK with air at limphome position is not active.

### 7.2 Monitoring of DK setpoint and DK actual value

=====

During normal operating the deviation between DK setpoint and DK actual value is compared with a permissible deviation and if it is exceeded the DK drive default function is requested. The deviation is calculated from the difference between the DK setpoint filtered with a PTL and delayed by one calculation cycle ( $wdksfi\_w$ , rough prediction) and the DK actual value. The permissible deviation is given in a characteristic line (DWDKSBAMX) as a function of the DK setpoint gradient ( $gwdk\_kge$ ).

If the permissible deviation is violated a fault counter ( $dklagerc$ ) is incremented, which can be counted back again by TDKLAGDE in case of healing.

## 8. Monitoring of the DLR setting range

=====

In order to avoid overheating of the DV-E or of the DV-E-ES due to a tight DK the DLR setting range is monitored. Additionally an attempt is made to switch the ES on again, if the DV-E-ES has switched off automatically for hardware reasons. This switch-on attempt is performed via 2 cycles ( $2 \times 10$  ms).

In case of a fault the rev. SKA resp. the DK drive default function is requested.

Representation in the block FDEF in the picture monitoring of PID setting range and monitoring of DV-E power stage status.

## 9. Protection of DV-E power stage from overheating during hot idling (only when SY-ESTZ = 1)

=====

Provided certain prerequisites are fulfilled, the triggering duty cycle for the power stage is limited in the short term to protect the DV-E power stage from overheating during hot idling in extreme environmental conditions. This is to let the power stage cool down.

The conditions for this are: Stationary vehicle ( $vfzg < VFZERH$ ) and a high ambient temperature ( $tans > TANERH$ ). If the duty cycle  $dlrspid\_w$  then exceeds a threshold  $DLRPIDERH$  for a time  $terhc \geq TERHMX$ , then for a negative duty cycle at the controller output, limiting is to  $dlrspid\_w = PIDERHBEG$  and a negative sign ( $B\_dlrspid = false$ ). This limitation is maintained for the time  $terholc = TERHOL$  so that the power stage can cool down. The controller-output duty cycle is applied at the power stage again after elapse of this time.

If the driver operates the accelerator pedal during this protective measure ( $B\_ll = false$ ), the vehicle is set in motion, the actual value for flap starts to drift, the idle speed fluctuates by more than  $DNMOTERH$ , the engine speed,  $nmot$ , exceeds the threshold  $NMOTERH$  or the nominal-actual difference,  $dwdkdlr\_w > DWDKERH$ , then the duty-cycle limitation is aborted immediately and the controller output duty cycle is applied at the power stage again.

Refer to the function DVEUE for the criteria to use the system constant SY-ESTZ.

## 10. Diagnosis

=====

For the workshop and CARB diagnosis 3 fault paths were defined.

- Path 'DVEL': indicates that the DK of the DV-E will not reach the desired position any more
- Path 'DVEE': indicates that the DV-E power stage has switched off, e.g. due to too high temperature, too high current or too low voltage.
- Path 'DVER': indicates that the DLR lies outside the valid control range.

## 11. Function to suppress shutdown rattling

=====

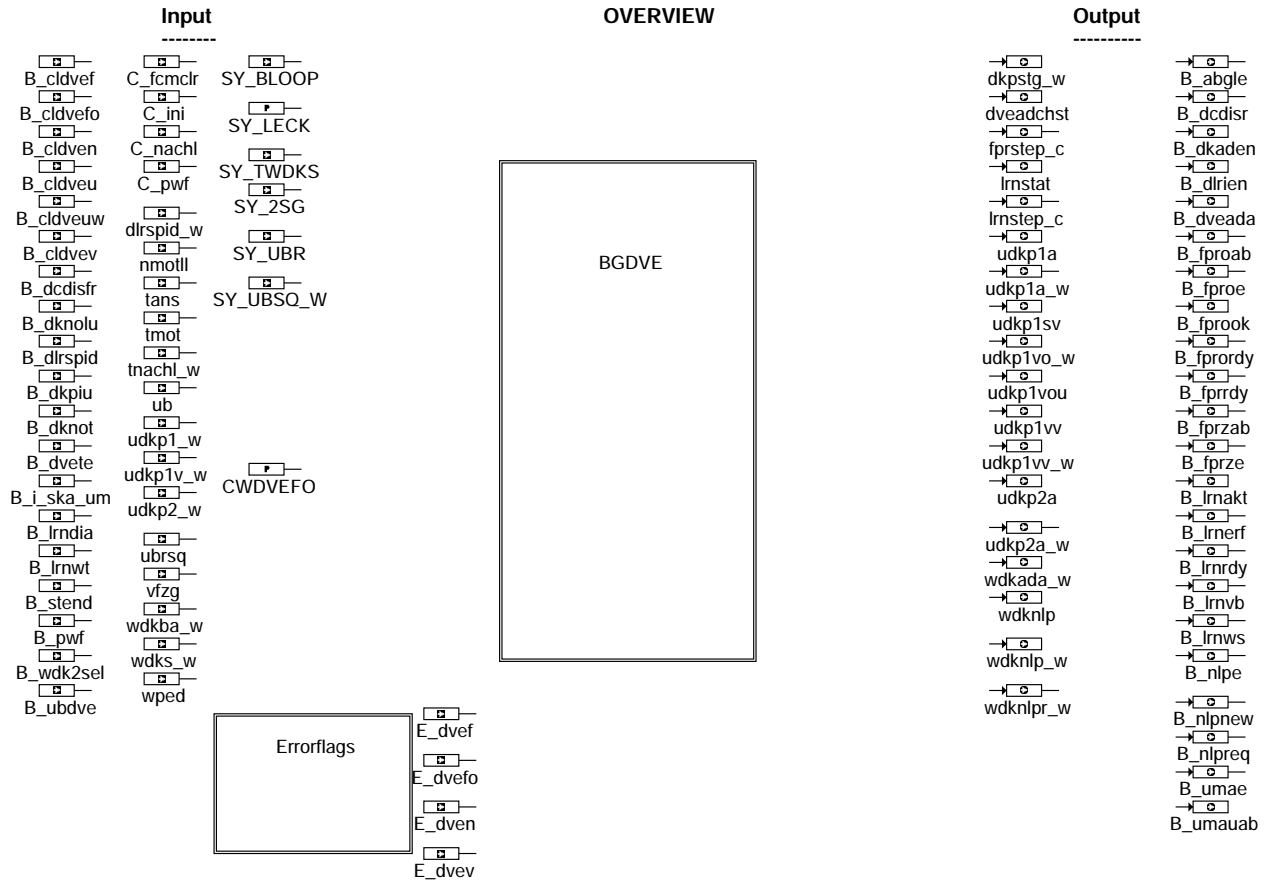
For projects with the possibility to supply the DV-E5 during after-run as well from a main relay after key OFF, position control also remains active during the after-run by conditional compiling ( $SY\_UBR = true$ ). The flap is driven to  $wdkba = 0$  by a speed-dependent DK nominal value from the function FUEDK. If the engine has stopped turning ( $B\_nmin = true$ ), then the DV-E5 is switched to currentless after elapse of the waiting time  $TWDKNL$ .





## BGDVE 3.110 Values for DV-E control from the learning and checking routines

### FDEF BGDVE 3.110 Function definition



bgdve-main

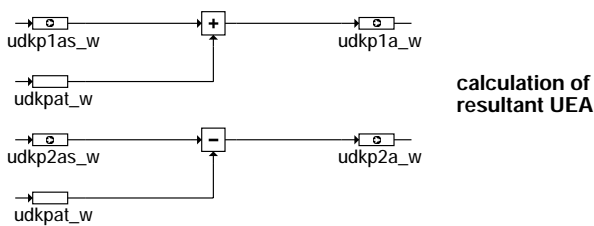
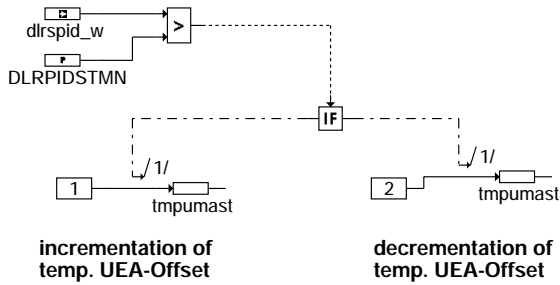
bgdve-main







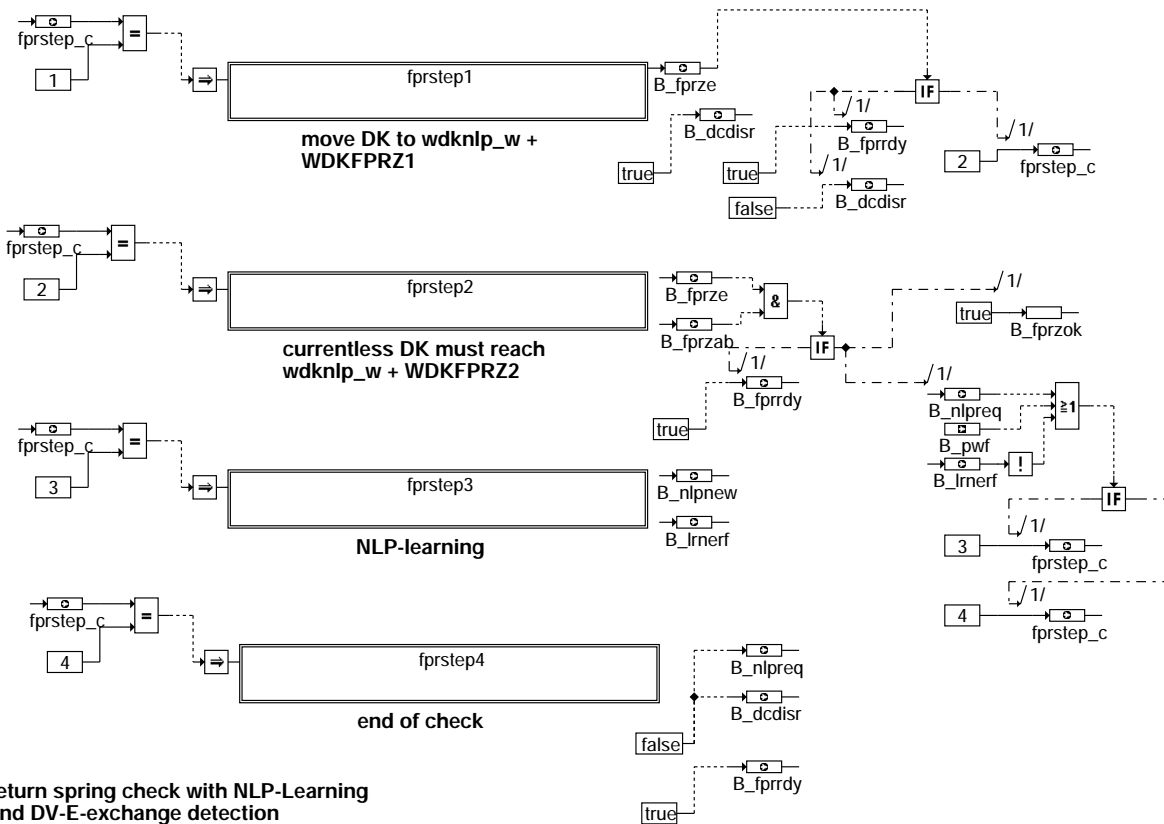
For more information read "Detailed description of function" chapter 5 "DV-E-adaption" part 5.2 "temporary part"



### temporary UMA-adaption

bgdve-tempuma

For more information read "Detailed description of function" chapter 4 "DV-E-spring check"



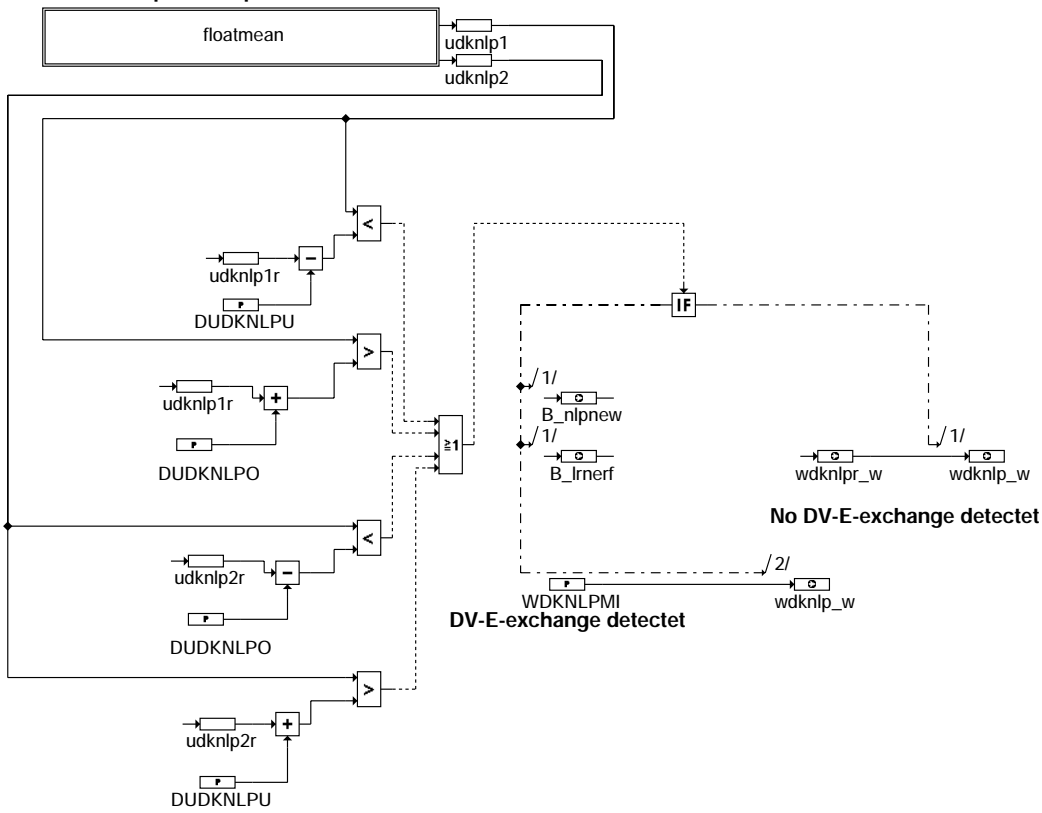
return spring check with NLP-Learning and DV-E-exchange detection

bgdve-retsprich

bgdve-tempuma

bgdve-retsprich

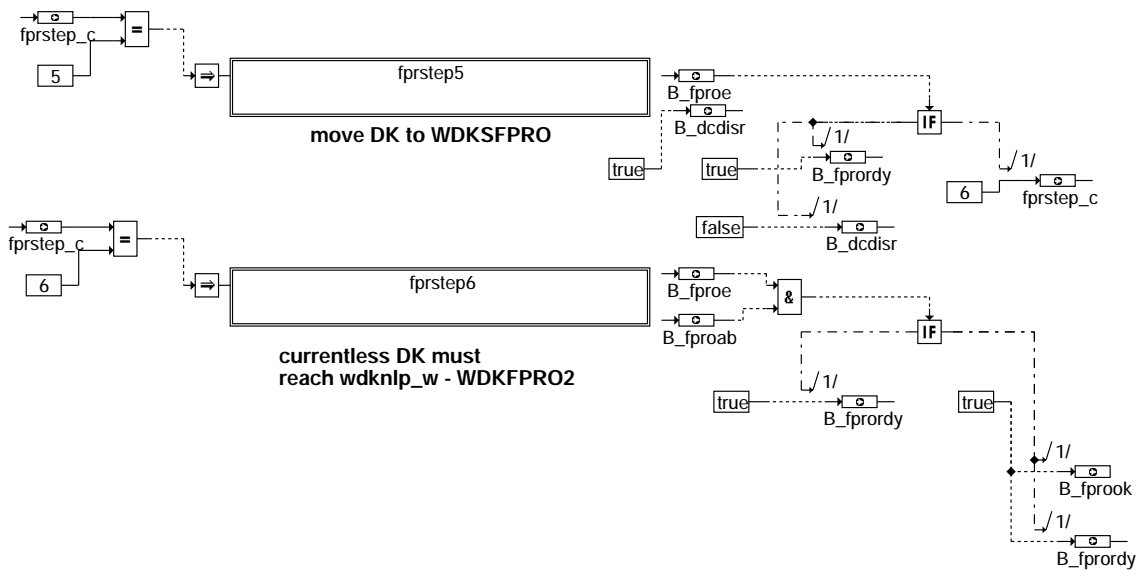
### floating mean value formation of udknlp1, udknlp2



### NLP-learning and DV-E-exchange detection

bgdve-fprstep3

For more information read "Detailed description of function"  
chapter 4 "DV-E-spring check"



### DV-E-Open spring check

bgdve-opsprich

bgdve-fprstep3

bgdve-opsprich



## ABK BGDVE 3.110 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWDVEFO			FW	Codeword DV-E opening spring-check
DKPSTGMIN			FW	Min. gradient of the DK poti for conversion abs. to rel. angle in the worst case
DLRPIDSTMN			FW	Min. threshold for PWM pulse duty factor of the DLR with temp. UMA adapt.
DUDKNLPO			FW	Tolerance range for NLP upward (incl. Rü)
DUDKNLPU			FW	Tolerance range for NLP downward
DUDKP1HY			FW	offset of hysteresis for switching to amplified throttle poti 1 signal
DUDKPTMP			FW	Delta of a ramp-step during the temp. UMA adaptation
FPRAT			FW	Inlet air temperature threshold for DV-E spring check
FPRMT			FW	Engine temperature threshold for DV-E spring check
FPRNMAX			FW	Engine speed threshold for DV-E spring check
FPRTIM1_T			FW	DV-E spring check, waiting time in check step 1
FPRTIM2_T			FW	DV-E spring check, waiting time in check step 2
FPRTIM3_T			FW	DV-E spring check, waiting time in check step 5
FPRTIM4_T			FW	DV-E spring check, waiting time in check step 6
LRNST1_T			FW	Waiting time during learning step 1
LRNST3_T			FW	Waiting time during learning step 3
LRNST7_T			FW	Waiting time during learning step 7
LRNST9_T			FW	Waiting time during learning step 9
LRNVB_T			FW	Time during which learning is forbidden for 'normal learning'
NLPST1T			FW	Waiting time 1 in the NLP learning
NLPST2T			FW	Waiting time 2 in the NLP learning
SY_LECK			FW	Leckluft im Steller
TCIDIS			FW	Max. time for CAN-Kommunikation to be stopped when B_stend
TDKNACH			FW	time during run after until zero current DK stabilizes in NLP
TDLRPIDMX			FW	Max. time for PWM pulse duty factor of the DLR at temp. UMA adapt.
TMSUTMUMA			FW	Lower Tmot threshold for temporary UMA adaptation
TTMUMASTA			FW	Time for steady-state during temp. UMA adaptation
UANAUF RP			FW	Step width for OPEN ramp
UANNMAX			FW	Engine speed threshold for the release of the UMA learning and gain adjustment
UANPEDMAX			FW	Pedal threshold for UMA learning allowed
UANPIDMIN			FW	Abort threshold PID-sum for CLOSE ramp
UANPIDMINA			FW	Abort threshold PID-sum for OPEN ramp
UANUATS			FW	Lower inlet air temperature threshold for release of learning
UANVFZG			FW	Car velocity threshold for DV-E check/adaption
UANZURP			FW	Step width for CLOSE ramp
UAN_OJMT			FW	upper engine temperature threshold for stop limit
UAN_STORE			FW	Threshold for storage of new learning values
UAN_UJMT			FW	lower engine temperature threshold for stop limit
UB_UANL			FW	Battery voltage threshold for release of learning
UDKNLP1N			FW	Nominal value voltage DK-Poti 1 in NLP-position
UDKNLP2N			FW	Nominal value voltage DK-Poti 2 in NLP-position
UDKP1AMAX			FW	Max. voltage DK-Poti 1 at lower DK limit stop
UDKP1AMIN			FW	Min. voltage DK-Poti 1 at lower DK limit stop
UDKP1AURI			FW	Voltage DK-poti 1 at the lower DK limit stop, initial. value
UDKP1DUS			FW	Nominal switch-over threshold for DK-Poti-1 switch-over
UDKP1NHUB			FW	Rated travel of the throttle valve in the DV-E, (poti 1)
UDKP1VID			FW	Nominal amplification for DK-Poti 1
UDKP1VOMA			FW	Max. offset error for DK-Poti-1-amplifier
UDKP1VOMI			FW	Min. offset error for DK-Poti-1-amplifier
UDKP1VOSC			FW	Lower limit for upper adjust.pt. DK-Poti 1
UDKP1VUSC			FW	Upper limit for lower adjust.pt. DK-Poti 1
UDKP1VVMA			FW	Upper value amplification error for amplifier
UDKP1VVMi			FW	Lower value amplification error for amplifier
UDKP2AMAX			FW	Max. voltage DK-Poti 2 at lower DK limit stop
UDKP2AMIN			FW	Min. voltage DK-Poti 2 at lower DK limit stop
UDKP2AURI			FW	Voltage DK-poti 2 at the lower DK limit stop, initial. value
UDKPALOS			FW	Voltage offset for detection of the breakaway
UDKPAOFF			FW	Voltage offset at lower limit stop
UDKPATMX			FW	Max. possible offset of the temp. UMA adaptation
UPVGNENN			FW	Nominal value for DV-E poti supply voltage
WDKFPRO1			FW	Shutdown actual throttle-valve value for opening DV-E spring check
WDKFPRO2			FW	Test threshold actual throttle-valve value for opening DV-E spring check
WDKFPRZ1			FW	Deactivation threshold DK actual value for DV-E return spring check
WDKFPRZ2			FW	Checking threshold DK actual value for DV-E return spring check
WDKNLPMA			FW	Upper allowed setpoint for NLP-position
WDKNLPMI			FW	Lower allowed setpoint for NLP-position
WDKNSTORE			FW	Threshold for storage of new learning values rel. limp home position
WDKSFFR			FW	DK setpoint for DV-E return spring check
WDKSFFPRO			FW	Nominal throttle-valve value for opening DV-E spring check
WDKSTMUMA			FW	DK angle threshold for temporary UMA adaptation
Variable	Source		Type	Description
B_2WART	BGDVE		LOK	condition: Wait for "injection enabled" from 2.ECU
B_ABGLE	BGDVE		AUS	Condition: Error during amplifier adjustment
B_CIDIS	BGDVE		LOK	condition: Stop of CAN-Kommunikation when B_stend
B_CLDVEF			EIN	Flag for clearance: DV-E cause of failure: spring check
B_CLDVEFO			EIN	Flag for detection: Fault in spring test "Open"
B_CLDVEN			EIN	Flag for clearance: DV-E cause of failure: limphome air position
B_CLDVEU			EIN	Flag for clearance: DV-E cause of failure: UMA-learning
B_CLDVEUW			EIN	Flag for deletion: Fault during UMA re-learning
B_CLDVEV			EIN	Flag for clearance: DV-E cause of failure: amplifier adjustment



Variable	Source	Type	Description
B_DCDISFR	ADVE	EIN	Condition: Disable DV-E power stage by means of the funct. processor
B_DCDISR	BGDVE	AUS	Condition: DV-E power stage deactivation is requested
B_DKADEN	BGDVE	AUS	Condition: Use DK setpoint from DK adaptation and DK check
B_DKNACH	BGDVE	LOK	Non-volatile RAM, Condition: DK currentless and in NLP in run after
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKNOT	SREAKT	EIN	condition: continued operation with a single remaining throttle actuator poti
B_DKP1E	GGDVE	EIN	condition: defect in throttle actuator potentiometer 1
B_DKP2E	BGDVE	EIN	condition: defect in throttle actuator potentiometer 2
B_DKPIU	SREAKT	EIN	Condition: irreversible SKA
B_DLRIEN	BGDVE	AUS	Condition: Perform no temp. limitation of I-component in the DLR
B_DLRSPID	ADVE	EIN	Condition: DLR, sign of sum of the PID-components, = 1: positiv, =0: negative
B_DVEADA	BGDVE	AUS	condition: disabling injection during DV-E-adaptation
B_DVEADAMC		EIN	CAN-Receive-Message: injection prohibited by master-ECU during DV-E-adaption
B_DVEADASC		EIN	CAN-Receive-Message: injection prohibited by slave-ECU during DV-E-adaption
B_DVEADAT	BGDVE	AUS	CAN-Send-Message: injection prohibits by slave- or master-ECU during DV-E-adapt
B_DVETE	ADVE	EIN	Condition: Extended DV-E-exchange detection
B_DVETV	BGDVE	LOK	Condition: Locking bit extended controller replacement detection
B_FPRAKT	BGDVE	LOK	Throttle return spring check active
B_FPROAB	BGDVE	AUS	Condition: Abort of DV-E open spring check, spring does not open
B_FPROE	BGDVE	AUS	Condition: Opening spring test fault
B_FPROOK	BGDVE	AUS	Condition: Opening spring test OK
B_FPRORDY	BGDVE	AUS	Condition: Opening spring test completed
B_FPROVB	BGDVE	LOK	Condition: Opening spring test prohibited
B_FPRRDY	BGDVE	AUS	throttle return spring check ended
B_FPRZAB	BGDVE	AUS	Condition: Abort of DV-E return spring check, spring does not close
B_FPRZE	BGDVE	AUS	Condition: Error in the DV-E return spring check
B_FPRZOK	BGDVE	LOK	Condition: DV-E return spring check o.k.
B_FPRZVB	BGDVE	LOK	Condition: DV-E return spring check forbidden
B_LSKAJUM	UFREAC	EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_LRNAKT	BGDVE	AUS	learning active bit
B_LRNDIA		EIN	Condition: DV-E adaptations and checks activated by means of diagnosis tester
B_LRNERF	BGDVE	AUS	learning success bit
B_LRNFG	BGDVE	LOK	learning enable bit
B_LRNRDY	BGDVE	AUS	learning complete
B_LRNTESA	BGDVE	LOK	Condition: UMA learning a.gain adj. activated due to tester request
B_LRNVB	BGDVE	AUS	learning prohibition bit
B_LRNWS	BGDVE	AUS	learned value save bit
B_LRNWT		EIN	Condition: DV-E adaption activated by tester at end of intake-module-production
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)
B_NLPE	BGDVE	AUS	Condition: Error in NLP-check and learning
B_NLPERF	BGDVE	AUS	Permanent RAM, condition: NLP acquisition successful
B_NLPNEW	BGDVE	AUS	Condition: NLP position not yet known
B_NLPREQ	BGDVE	AUS	Condition: Request NLP learning
B_PWF		EIN	Condition for powerfail
B_STEND	BBSTT	EIN	condition end of start
B_UBDVE	ADVE	EIN	Condition: Battery voltage for DV-E control OK
B_UMAE	BGDVE	AUS	Condition: Error during UMA learning
B_JMAUAB	BGDVE	AUS	Condition: UMA learning stopped during first initialization (SKA)
B_WDK2SEL	GGDVE	EIN	Condition: DV-E position control is performed with actual-value-poti 2
CIDISTIM	BGDVE	LOK	time-counter to stop CAN-Kommunikation after B_stend
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_NACHL		EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DKPSTG_W	BGDVE	AUS	slope of throttle potentiometer (% DK / V)
DLRMXT	BGDVE	LOK	Timer for DLR in the UMA within the limit
DLRSPID_W	ADVE	EIN	DLR for DV-E: Sum of the PID-components
DVEADCHST	BGDVE	AUS	DV-E adaptation: Status test conditions
E_DVEF	DDVE	EIN	Error flag: DV-E cause of failure: spring check
E_DVEFO	DDVE	EIN	error flag: DV-E cause of failure: spring check "open"
E_DVEN	DDVE	EIN	Error flag: DV-E cause of failure: limphome air position
E_DVEV	DDVE	EIN	Error flag: DV-E cause of failure: amplifier adjustment
FPRSTEP_C	BGDVE	AUS	step counter throttle return spring check
FPRTIM_C	BGDVE	LOK	time counter throttle return spring check
LRNSTAT	BGDVE	AUS	statusbyte DV-E-adaption routine for tester-communication
LRNSTEP_C	BGDVE	AUS	counter for learning time for a learning step
LRNTIM_C	BGDVE	LOK	Time counter for the waiting time in the learning steps
LRNVB_C	BGDVE	LOK	Learning prohibition counter (wait time)
NLP1TIM	BGDVE	LOK	Time counter for the waiting time 1 in the NLP learning
NMOTLL	BGNMOT	EIN	engine speed
SY_2SG	PROKON	EIN	system constant 2 motronic systems
SY_BLOOP		EIN	1=resetting of irrev. EGAS fault possible during clearing of FCM
SY_TWDKS		EIN	system constant: input of desired angle DVE via tester is possible
SY_UBR	PROKON	EIN	system constant onboard battery voltage scanned from main relay input
SY_UBSQ_W		EIN	System constant conversion factor UB resolution to standard quantization ubsq
TANS	SWADAP	EIN	Intake air temperature
TDKNACH_W	BGDVE	LOK	time counter during run after until curentless DK reaches NLP
TLOOP	BGDVE	LOK	Ring counter for time difference measurement
TMOT	SWADAP	EIN	Engine temperature
TMPUMAST	BGDVE	LOK	Status for temporary UMA adaptation
TNACHL_W	MOTAUS	EIN	time of ECU switch off delay
TTMUMAD	BGDVE	LOK	time difference for temporary UMA adaptation



Variable	Source	Type	Description
UB	SWADAP	EIN	battery voltage
UBRSQ		EIN	battery voltage via main relay, standard quantization
UBUANLR	BGDVE	LOK	min.voltage for UMA-Learning in Quantization of ubrsq
UDKNLP1	BGDVE	LOK	Voltage DK-Poti 1 at the NLP
UDKNLP1R	BGDVE	LOK	Permanent RAM: Voltage DK-Poti 1 at the NLP
UDKNLP2	BGDVE	LOK	Voltage DK-Poti 2 at the NLP
UDKNLP2R	BGDVE	LOK	Permanent RAM: Voltage DK-Poti 2 at the NLP
UDKP1A	BGDVE	AUS	sensor voltage poti 1 of throttle actuator at (lower) mechanical stop
UDKP1AALT	BGDVE	LOK	Temp. voltage DK-poti 1 at the lower DK limit stop
UDKP1ASR_W	BGDVE	LOK	Permanent RAM: Voltage DK-Poti 1 at lower DK limit stop, stationary value
UDKP1AS_W	BGDVE	AUS	Voltage DK-poti 1 at the lower limit stop, steady-state part
UDKP1A_W	BGDVE	AUS	sensor voltage poti 1 of throttle actuator at (lower) mechanical stop (word)
UDKP1ROB	BGDVE	LOK	Real DK-poti-1-value at the upper adjustment point
UDKP1RUN	BGDVE	LOK	Real DK-poti-1-value at the lower adjustment point
UDKP1SV	BGDVE	AUS	Max. DK potentiometer-1 value for using amplified signal
UDKP1VOR	BGDVE	LOK	Permanent RAM: Voltage offset at DK-Poti-1-amplification
UDKP1VOU	BGDVE	AUS	Diagnosis: 8 bit copy of udkp1vo_w as ambient value
UDKP1VO_W	BGDVE	AUS	voltage offset of DK potentiometer 1 amplification characteristic
UDKP1VROB	BGDVE	LOK	Real amplified DK-poti-1-value at the upper adjustment point
UDKP1VRUN	BGDVE	LOK	Real amplified DK-poti-1-value at the lower adjustment point
UDKP1VV	BGDVE	AUS	Diagnosis: 8 bit copy of udkp1vv_w as ambient value
UDKP1VVR	BGDVE	LOK	Permanent RAM: Amplification at DK-Poti-1-amplification
UDKP1VV_W	BGDVE	AUS	amplification of throttle potentiometer 1
UDKP1V_W		EIN	amplified sensor voltage throttle potentiometer 1
UDKP1_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UDKP2A	BGDVE	AUS	sensor voltage poti 2 of throttle actuator at (lower) mechanical stop
UDKP2AALT	BGDVE	LOK	Temp. voltage DK-poti 2 at the lower DK limit stop
UDKP2ASR_W	BGDVE	LOK	Permanent RAM: Voltage DK-Poti 2 at lower DK limit stop, stationary value
UDKP2AS_W	BGDVE	AUS	voltage DK-poti 2 at the lower limit stop, steady-state part
UDKP2A_W	BGDVE	AUS	sensor voltage throttle potentiometer 2 at (lower) mechanical stop
UDKP2_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UDKPATR_W	BGDVE	LOK	Static-RAM: temporary UEA offset of the DK-poti
UDKPAT_W	BGDVE	LOK	Temporary UEA offset of the DK-poti
VFZG	SWADAP	EIN	vehicle speed (km/h)
WDKADA_W	BGDVE	AUS	Setpoint DK-angle, from DV-E adaptation function and check function
WDKBA_W	GGDVE	EIN	throttle angle with respect to lower mechanical stop
WDKNLP	BGDVE	AUS	Diagnosis: 8 bit copy of wdknlp_w as ambient value
WDKNLPR	BGDVE	AUS	Diagnosis: 8 bit copy of wdknlpr_w as ambient value
WDKNLPR_W	BGDVE	AUS	Permanent RAM: Setpoint throttle angle in NLP-position, related to UMA
WDKNLP_W	BGDVE	AUS	throttle angle in the limphome air position
WDKS_W	MSF	EIN	desired throttle angle w.r.t. to lower mechanical stop
WDKVABOB	BGDVE	LOK	DK setpoint for upper adjustment point
WDKVABUB	BGDVE	LOK	DK setpoint for lower adjustment point
WPED	GGPED	EIN	Standardized accelerator pedal angle

## FW BGDVE 3.110 Fixed Values

Parameter	Value	Description
CWDVEFO		Codeword DV-E opening spring-check
DKPSTGMIN		Min. gradient of the DK poti for conversion abs. to rel. angle in the worst case
DLRPIDSTMN		Min. threshold for PWM pulse duty factor of the DLR with temp. UMA adapt.
DUDKNLPO		Tolerance range for NLP upward (incl. Rü)
DUDKNLPU		Tolerance range for NLP downward
DUDKP1HY		offset of hysteresis for switching to amplified throttle poti 1 signal
DUDKPTMP		Delta of a ramp-step during the temp. UMA adaptation
FPRAT		Inlet air temperature threshold for DV-E spring check
FPRMT		Engine temperature threshold for DV-E spring check
FPRNMAX		Engine speed threshold for DV-E spring check
FPRTIM1_T		DV-E spring check, waiting time in check step 1
FPRTIM2_T		DV-E spring check, waiting time in check step 2
FPRTIM3_T		DV-E spring check, waiting time in check step 5
FPRTIM4_T		DV-E spring check, waiting time in check step 6
LRNST1_T		Waiting time during learning step 1
LRNST3_T		Waiting time during learning step 3
LRNST7_T		Waiting time during learning step 7
LRNST9_T		Waiting time during learning step 9
LRNVB_T		Time during which learning is forbidden for 'normal learning'
NLPST1T		Waiting time 1 in the NLP learning
NLPST2T		Waiting time 2 in the NLP learning
SY_LECK		Leckluft im Steller
TCIDIS		Max. time for CAN-Kommunikation to be stopped when B_stend
TDKNACH		time during run after until zero current DK stabilizes in NLP
TDLRPIDMX		Max. time for PWM pulse duty factor of the DLR at temp. UMA adapt.
TMSUTMUMA		Lower Tmot threshold for temporary UMA adaptation
TTMUMASTA		Time for steady-state during temp. UMA adaptation
UANAUFPR		Step width for OPEN ramp
UANNMAX		Engine speed threshold for the release of the UMA learning and gain adjustment
UANPEDMAX		Pedal threshold for UMA learning allowed
UANPIDMIN		Abort threshold PID-sum for CLOSE ramp
UANPIDMINA		Abort threshold PID-sum for OPEN ramp
UANUATS		Lower inlet air temperature threshold for release of learning
UANVFZG		Car velocity threshold for DV-E check/adaption



Parameter	Value	Description
UANZURP		Step width for CLOSE ramp
UAN_OJMT		upper engine temperature threshold for stop limit
UAN_STORE		Threshold for storage of new learning values
UAN_UJMT		lower engine temperature threshold for stop limit
UB_UANL		Battery voltage threshold for release of learning
UDKNLP1N		Nominal value voltage DK-Poti 1 in NLP-position
UDKNLP2N		Nominal value voltage DK-Poti 2 in NLP-position
UDKP1AMAX		Max. voltage DK-Poti 1 at lower DK limit stop
UDKP1AMIN		Min. voltage DK-Poti 1 at lower DK limit stop
UDKP1AURI		Voltage DK-poti 1 at the lower DK limit stop, initial. value
UDKP1DUS		Nominal switch-over threshold for DK-Poti-1 switch-over
UDKP1NHUB		Rated travel of the throttle valve in the DV-E, (poti 1)
UDKP1VID		Nominal amplification for DK-Poti 1
UDKP1VOMA		Max. offset error for DK-Poti-1-amplifier
UDKP1VOMI		Min. offset error for DK-Poti-1-amplifier
UDKP1VOSC		Lower limit for upper adjust.pt. DK-Poti 1
UDKP1VUSC		Upper limit for lower adjust.pt. DK-Poti 1
UDKP1VVMA		Upper value amplification error for amplifier
UDKP1VVMI		Lower value amplification error for amplifier
UDKP2AMAX		Max. voltage DK-Poti 2 at lower DK limit stop
UDKP2AMIN		Min. voltage DK-Poti 2 at lower DK limit stop
UDKP2AURI		Voltage DK-poti 2 at the lower DK limit stop, initial. value
UDKPALOS		Voltage offset for detection of the breakaway
UDKPAOFF		Voltage offset at lower limit stop
UDKPATMX		Max. possible offset of the temp. UMA adaptation
UPVGNENN		Nominal value for DV-E poti supply voltage
WDKFPRO1		Shutdown actual throttle-valve value for opening DV-E spring check
WDKFPRO2		Test threshold actual throttle-valve value for opening DV-E spring check
WDKFPRZ1		Deactivation threshold DK actual value for DV-E return spring check
WDKFPRZ2		Checking threshold DK actual value for DV-E return spring check
WDKNLPM		Upper allowed setpoint for NLP-position
WDKNLPMI		Lower allowed setpoint for NLP-position
WDKNSTORE		Threshold for storage of new learning values rel. limp home position
WDKSFPR		DK setpoint for DV-E return spring check
WDKSFPRO		Nominal throttle-valve value for opening DV-E spring check
WDKSTMUMA		DK angle threshold for temporary UMA adaptation

## FB BGDVE 3.110 Detailed description of function

### 0. Overview

=====

1. Introduction
2. Initialization
3. NLP learning (DV-E exchange detection)
4. DV-E spring check
  - 4.1 Return spring check
    - 4.1.1 Overview
    - 4.1.2 Detailed order of events
  - 4.2 Open spring check
    - 4.2.1 Overview
    - 4.2.2 Detailed order of events
5. DV-E adaptation
  - 5.1 Steady-state part
    - 5.1.1 Overview
    - 5.1.2 Detailed order of events
  - 5.2 Temporary part
  - 5.3 Resulting part
6. Blocking of the injection
7. DV-E adaptation via tester request
8. Storage in permanent RAM and in EEPROM

### 1. Introduction

=====

Since there is no adjustment between the actual value acquisition by the potentiometer and the mechanical throttle valve position (DK) for the throttle adjustment device DV-E5, an adaptation needs to be performed in the ME. During the adaptation, the lower mechanical DK limit stop (UMA) and the air in the limp home position (NLP) of the DV-E5 are learned, and an adjustment of the actual value potentiometer gain is performed. The learned values are stored in the permanent RAM resp. in the EEPROM. In addition, the springs of the DV-E5 are checked. With ignition ON, this adaptation may under certain input conditions take place again.

Therefore, the following sub functions are realized in the BGDVE:

- Learning and checking of the DV-E air at limp home position (NLP learning) with DV-E exchange detection
- DV-E spring check (open spring, return spring)
- Learning of the lower mechanical DK limit stop (UMA learning)
- Gain adjustment, offset and gradient



A 'first initialization' was performed only, if all of the mentioned sub functions are successfully executed during an initial start. The variables must then be given the following values:

```
B_lrnws = 1, B_lrnerf = 1, B_fprzok = 1, (B_fprook = 1 only for CWDVEFO = 1)
and lrnstep_c = 11.
```

(B\_nlperf is not needed anymore for event control purposes from BGDVE3.110 onwards, thus being reduced to a Dummy - Function. B\_nlperf = 1 is cyclically refreshed and is of no importance anymore)

## 2. Initialization =====

The initialization phase consists of three parts.

```
"- Part 1: Copy EEPROM values into the permanent RAM"
  B_lrnerf, B_lrnws, udknlplr, udknlp2r, udkplasr_w,
  udkp2asr_w, udkplvor, udkplvvr and wdknlp_w
"- Part 2: Copy permanent RAM values into the RAM"
  udkplasr -> udkplas_w, udkplasr_w -> udkpla
  udkp2asr -> udkp2as_w, udkp2asr_w -> udkp2a
  udkpatr_w -> udkpat_w
  udkplvor -> udkplvo_w, udkplvvr -> udkplvv_w
  wdknlp_w -> wdknlp_w
"- Part 3: Calculate ini-values and write them into RAM"
  Poti gradient dkpstg_w := 100.0 %DK / UDKP1NHUB
  Switch-over threshold udkplsv := UPVGNENN / udkplvv_w - UDKP1DUS
```

If the EEPROM was cleared or if it is defective, fixed values are written into the permanent RAM in part 1. The assignment is as follows:

```
udkplasr_w := UDKP1AURI
udkp2asr_w := UDIP2AURI
udkplvor   := 0.0
udkplvvr   := UDKP1VID
B_lrnws    := false
B_lrnerf   := false
udknlplr   := UDKNLP1N
udknlp2r   := UDKNLP2N
wdknlp_w   := WDKNLPMA
```

Furthermore the following plausibility checks are performed in part 3:

```
if (udkplasr_w < UDKP1AMIN) OR (udkplasr_w > UDKP1AMAX + UDKPAOFF)
OR (udkp2asr_w < UDKP2AMIN - UDKPAOFF) OR (udkp2asr_w > UDKP2AMAX)
then
  B_lrnws := false
  B_lrnerf := false
  udkplasr_w := UDKP1AURI
  udkp2asr_w := UDKP2AURI
  udkplas_w := UDKP1AURI
  udkpla := UDKP1AURI
  udkp2as_w := UDKP2AURI
  udkp2a := UDKP2AURI
endif

if (udkplvo_w < UDKP1VOMI) OR (udkplvo_w > UDKP1VOMA) OR
(udkplvv_w < UDKP1VVM I) OR (udkplvv_w > UDKP1VVM A)
then
  B_lrnerf := false
  udkplvo_w := 0.0
  udkplvv_w := UDKP1VID
endif

if ((wdknlp_w < WDKNLPMI) OR (wdknlp_w > WDKNLPMA)
then
  B_lrnerf := false
  wdknlp_w := WDKNLPMA
endif
```

For projects with additional measurement path for the voltage ubrsq downstream the main relay (conditional compilation, SY\_UBR = true), a re-quantisation of the voltage threshold UB\_UANL to the resolution of ubrsq is required. In this case ubuanlr replaces the environmental condition UB\_UANL. (see 5.1.2 Detailed order of events/Starting conditions).

```
if (SY_UBR)
then
  ubuanlr := UB_UANL * SY_UBSQ_W
endif
```

## 3. NLP learning (DV-E exchange detection) =====

The NLP is needed for the digital position controller (DLR) and



for the detection of a DV-E adaptation need, e.g. in the case of an actuator exchange. At ignition ON, the NLP is read via the actual value potentiometers, as long as the DV-E is still at zero current (result in udknlp1 and udknlp2) and it is then checked for plausibility with the values stored in the memory (udknlp1r and udknlp2r). If the values differ, adaptation need is detected and after the return spring was checked in checking step 3 (fprstep\_c = 3), the NLP is learned. The NLP is made available to the DLR in the ADVE as wdknlp-w.

In order to avoid an incorrect DV-E exchange detection in the case of a quick change from ignition ON -> OFF -> ON the DV-E exchange detection is only permitted in the ECU initialization, if the DK in the previous ECU-after-run has been at zero current for at least a time tdknach\_w >= TDKNACH (then B\_dknach = true). Thus it is ensured that the DK can definitely stabilize into the NLP while it is at zero current.

In the case of an actuator exchange without adaption by service-tester, it might be possible that udknlp1 and udknlp2 are still inside of the tolerance limit. Therefore at first the exchange detection is not active and no adaption will be made. If the UMA of the new actuator is above UMA of the old one, it could be possible that with ignition ON and no operation of the accelerator the current limitation in the ADVE will become active. In this case, the extended DV-E exchange detection reacts with blocking of the injection and a DV-E adaption. The extended DV-E exchange detection is only active with nmot = 0, wdks\_w < (UDKPIAURI - udkplas\_w) \* dkpstg\_w und B\_stend = false. After the start, the extended DV-E exchange detection is stopped with B\_dvetv = true and can only become active again when the ignition was turned OFF --> ON again.

Also see chapter 6, blocking of the injection.

4. DV-E spring check  
=====

4.1 Return spring check  
=====

4.1.1 Overview  
=====

By an opening of the DK from the NLP into the direction DK OPEN and by a subsequent switch-off of the DV-E power stage (DV-E-ES), the return motion forced by the return spring is checked. In the case of a fault, the DK drive default function (previously driving with DK limp home air) is requested via B\_fprzab = 1. The course of events can be observed by means of the checking step counter fprstep\_c. The check is only performed once by it being locked via the check ready bit B\_fprrdy.

The check is performed only if the following preconditions are fulfilled - if not, the check will be prohibited (B\_fprzvb = true) and the counter dveadchst will be set. dveadchst indicates which precondition was not fulfilled.

Counter dveadchst:  
=====

((B_dkpiu = 0) AND (B_dknolu = 0) AND (B_i_ska_um = 0) AND (vfgz < UANVFZG) AND (nmotll <= FPRNMAX) AND (B_wdk2sel = false) AND (B_ubdve = true) AND (tmot >= FPRMT) AND (tans >= FPRAT)	AND	I	
		I	
		I	1
		I	
		I	5
		I	6
		I	4
		I	9
		I	7
		I	8

In the case of a conditional compilation with SY\_TWDKS = 1, in the intake manifold module test at the end of line of test request B\_lrnwt = 1, the environmental conditions 5,6,7,8 are left out, and in condition 1 B\_dkpiu = 0 is replaced by B\_dkunb = 0. (B\_lrnwt = 1 only exists for SY\_TWDKS = 1).

4.1.2 Detailed order of events  
=====

Spring check step 0 (B\_fprakt = 0 -> 1 AND fprstep\_c = 0):

Entry of the desired angle WDKSFPR for original position, starting of the spring check timer fprtim\_c and switching over of the DV-E triggering to 'setpoint selection by adaptation' (B\_dkaden = 1).

Spring check step 1 (fprstep\_c = 1):

If the actual DK angle reaches the threshold of the original position (wdkba\_w >= (wdknlp\_w + WDKFPRZ1)) within a max. time (fprtim\_c <= FPRTIM1\_T), a DV-E power stage switch-off is requested by B\_dcdisr = 1. If the max. time is exceeded or if the check threshold is not reached, then the internal check fault B\_fprze = 1 is set and the DV-E return spring check is aborted.

Spring check step 2 (fprstep\_c = 2):





As a result of the DV-E power stage switch-off, the DK returns into the direction NLP due to the return spring. If the actual DK angle reaches the threshold of the original position ( $wdkba\_w \leq (wdknlp\_w + WDKFPRZ2)$ ) within a max. time ( $fprt\_c \leq FPRTIM2\_T$ ), the check is detected to be O.K., the check bit  $B\_fprzok = 1$  is set and 'spring check active' is reset ( $B\_fprakt = 0$ ). If the max. time is exceeded or if the lower check threshold is not reached, it means that the return spring has not set the DK back within the necessary time or that the return spring can no longer perform a return. In case this fault occurs, the DK drive default function (previously driving with DK limphome air) is requested via  $B\_fprzab = 1$ . Furthermore it is checked whether a learning of the NLP was requested ( $B\_nlpreq = 1$ ). In the case of  $B\_nlpreq = B\_nlperft$  and no power fail, the check step counter is set to 4, otherwise the check step counter is set to 3.

Spring check step 3 ( $fprstep\_c = 3$ ):

Learning of the DK-NLP while the DK is in a zero current state. After a waiting time ( $nlpltim > NLPST1T$ ), during which the DK has stabilized into the NLP, both actual DK value potentiometers  $udkp1\_w$  and  $udkp2\_w$  are read until a certain time  $nlpltim \geq (NLPST1T + NLPST2T)$  has elapsed. During this measuring time the absolute NLP of the DK ( $udknlp1$  and  $udknlp2$ ) is determined by means of a floating mean value formation.

Spring check step 4 ( $fprstep\_c = 4$ ):

Check is terminated; request of the DV-E power stage switch-off is taken back ( $B\_dcds = 0$ ), check terminated is set ( $B\_fprdy = 1$ ) and DV-E triggering is enabled for the normal operation ( $B\_dkaden = 0$ ).

## 4.2 Open spring check

=====

### 4.1.1 Overview

=====

By closing the DK from the NLP into the direction DK CLOSE and by a subsequent switch-off of the DV-E power stage (DV-E-ES), the open motion forced by the open spring is checked. In case of a fault, the DK drive default function (previously driving with DK limphome air) is requested. The course of events can be observed by means of the checking step counter  $fprstep\_c$ . The check is only performed once by it being locked via the check ready bit  $B\_fprdy$ .

The check is performed only if the following preconditions are fulfilled, if not the check will be prohibited ( $B\_fprov = true$ ) and the counter  $dveadchst$  will be set.  $dveadchst$  indicates which precondition was not fulfilled.

The open spring check can be shut-off with the code word  $CWDVEFO = 0$

Counter  $dveadchst$ :

=====

$(B\_dkpiu = 0)$	AND	I	
$(B\_dknolu = 0)$	AND	I	
$(B\_i\_ska\_um = 0)$	AND	I	
$(B\_wdk2sel = 0)$	AND	I	40
$(vfg < UANVFZG)$	AND	I	44
$(nmotll \leq FPRNMAX)$	AND	I	45
$(tmot \geq FPRMT)$	AND	I	46
$(tans \geq FPRAT)$		I	47

In the case of a conditional compilation with  $SY\_TWDKS = 1$ , in the intake manifold module test at the end of line of test request  $B\_lrnwt = 1$ , the environmental conditions 44-47 are left out, and in condition 40  $B\_dkpiu = 0$  is replaced by  $B\_dkunb = 0$ . ( $B\_lrnwt = 1$  only exists for  $SY\_TWDKS = 1$ ).

### 4.1.2 Detailed order of events

=====

Spring check step 4 ( $B\_fprakt = 0 \rightarrow 1$  AND  $fprstep\_c = 4$ ):

Entry of the desired angle  $WDKAPPRO$  for original position, starting of the spring check timer  $fprt\_c$  and switching over of the DV-E triggering to 'setpoint selection by adaptation' ( $B\_dkaden = 1$ ).

Spring check step 5 ( $fprstep\_c = 5$ ):

If the actual DK angle reaches the threshold of the original position ( $wdkba\_w \leq WDKFPRO1$ ) within a max. time ( $fprt\_c \leq FPRTIM3\_T$ ) a DV-E power stage switch-off is requested by  $B\_dcds = 1$ . If the max. time is exceeded or if the check threshold is not reached, then the internal check fault  $B\_fproe = 1$  is set and the DV-E return spring check is aborted.

Spring check step 6 ( $fprstep\_c = 6$ ):

As a result of the DV-E power stage switch-off, the DK returns into the direction NLP due to the open spring. If the actual DK angle reaches the threshold of the original position ( $wdkba\_w \geq (wdknlp\_w - WDKFPRO2)$ ) within a max. time ( $fprt\_c \leq$



FPRTIM4.T), the check is detected to be O.K., the check bit B\_fproof = 1 is set and 'spring check active' is reset (B\_fprakt = 0), the request of the DV-E power stage switch-off is taken back (B\_dcdisr = 0) and end of check is set ((B\_fprordy = 1)..

If the max. time is exceeded or if the check threshold is not reached, it means that the open spring has not set the DK back within the necessary time or that the open spring can no longer perform a return. In case this fault occurs, the DK drive default function (previously driving with DK limp home air) is requested via B\_fproab = 1 and check error B\_fproe = 1 is set.

## 5. DV-E adaptation

### 5.1 Steady-state part

#### 5.1.1 Overview

The steady-state part of the DV-E adaptation includes the UMA learning and the adjustment of the actual value potentiometer gain. In principle the steady-state part only needs to be performed once during the start-up of a new control unit resp. when exchanging a DV-E. The possibility of a renewed adaptation at ignition ON can be controlled by means of the prohibition time for learning LRNVB.T. The shorter this time is, the more likely it becomes that the adaptation is performed once more.

During the learning of the UMA the DK is moved in steps from the max. possible UMA to the UMA. By monitoring the actual value potentiometer it is detected, that the DK no longer moves. The corresponding value is read and increased by an offset UDKPAOFF, it is checked for plausibility as lower electrical DK limit stop (UEA) and stored in the permanent RAM resp. EEPROM. The UEA udkplas\_w and udkp2as\_w are made available to the function GGDVE. When adjusting the gain, the offset and the gains of the OP loop are determined by taking up two measuring positions with the DK. The calculated values udkplvo\_w and udkplvv\_w are made available to the function GGDVE. The adjustment is performed after the UMA learning.

If a fault occurs during the first initialization resp. with not set learning value memory bit (B\_lrnws = 0), an irreversible safety fuel deactivation (SKA) is requested via B\_umaub = 1. The course of the adaptation can be observed by means of the learning step counter lrnstep\_c.

The adaptation can also be started by a tester. See chapter 7.

In adaptation step 0 ... 4 the UMA is learned  
5 the rel. NLP is calculated  
6 ... 9 the gain is adjusted

#### 5.1.2 Detailed order of events

##### Starting conditions:

The adaptation will only take place, if the return spring check has been terminated (B\_fprordy = 1) and if the following input conditions are fulfilled, if not the learning will be prohibited (B\_lrnvb = true) and the counter dveadchst will be set. dveadchst indicates which input condition was not fulfilled.

Counter dveadchst:  
=====

((B_dkpiu = 0)	AND	I	
(B_i_ska_um = 0)	AND	I	
(B_dknolu = 0)	AND	I	
(B_dknot = 0))	AND	I	20
(nmotll <= UANNMAX)	AND	I	24
*)		I	
(vfzg <= UANVFZG)	AND	I	25
(wped < UANPEDMAX)	AND	I	26
(ub > UB_UANL)	AND	I	27
((tmot >= UAN_U-MT)	AND	I	
(tmot <= UAN_O-MT))	AND	I	28
(tans >= UANUATS)		I	30

\*) : The conditions to follow are only tested, if  
(lrnvb\_c > LRNVB\_T) OR  
(B\_pwf = 1) OR  
(B\_lrnws = 0) OR  
(B\_lrnerf = 0)

When the engine is turning lrnvb\_c is stopped.

In the case of a conditional compilation with SY\_TWDKS = 1, in the intake manifold module test at the end of line of test request B\_lrnwt = 1 the environmental conditions 24-26,28,30 are left out, and in condition 20 B\_dkpiu = 0 is replaced by B\_dkunb = 0.  
(B\_lrnwt = 1 only exists for SY\_TWDKS = 1).

For projects with additional measurement path for the voltage ubrsq downstream the main relay



(conditional compilation, SY\_UBR = true), a re-quantisation of the voltage threshold UB\_UANL to the resolution of ubrsq is required. In this case ubuanlr replaces the environmental condition UB\_UANL. (see 5.1.2 Detailed order of events/Starting conditions).

In the case that all input condtions are fulfilled, the adaption is enabled (B\_lrng = 1), if not, the adaption is prohibited (B\_lrnvb = 1).

Adaptation step 0 (B\_lrng = 0 -> 1 AND lrnstep\_c = 0):

Initialization of the DV-E adaptation. Switch-over of the DV-E triggering to 'setpoint of the BGDVE' (B\_dkaden = 1) and entering the worst case values into the UMA values (udkplas\_w = UDKP1AMAX and udkp2as\_w = UDKP2AMIN).

Adaptation step 1 (lrnstep\_c = 1):

The DK is made to approach the UMA via a ramp by reducing udkplas\_w (step width UAN\_ZURP). As soon as the position controller output undershoots a min-threshold (condition: B\_dlrspid = 0 AND dlrspid\_w > UANPIDMIN) a waiting time counter (lrntim\_c) is started. During this time, the learning value is formed by means of a floating mean value formation in udkplaalt and udkp2aalt. After the waiting time (lrntim\_c >= LRNST1\_T), the determined values udkplas\_w and udkp2as\_w are checked for the permitted value range (UDKP1AMIN and UDKP2AMAX). In case of a fault, the learning fault is set (B\_umae = 1) and the UMA abort function is executed.

Adaptation step 2 (lrnstep\_c = 2):

The learned UMA, stored in the previous step in udkplas\_w and udkp2as\_w, is increased by the offset (UDKPAOFF) and it thus becomes UEA. The UEA values are subsequently checked for the permitted value range (UDKP1AMAX and UDKP2AMIN). In case of a fault, the learning fault is set (B\_umae = 1) and the UMA abort function is executed.

Adaptation step 3 (lrnstep\_c = 3):

In this step, a ramp with the step width UANAUFRRP is passed to the DK via the setpoint wdkada\_w until the position controller output again exceeds the min-threshold (condition: B\_dlrspid = 0 AND dlrspid\_w <= UANPIDMIN). As soon as the threshold was exceeded, it is checked - after a waiting time (lrntim\_c >= LRNST3\_T) - whether the DK has detached from the UMA (udkpl\_w > udkplaalt) resp. whether it is not more than one delta away from UEA (udkpl\_w <= udkplas\_w + UDKPALOS). In case of a fault, the learning fault is set (B\_umae = 1) and the UMA abort function is executed.

Adaptation step 4 (lrnstep\_c = 4):

Part 1 of the adaptation, the UMA learning has successfully been terminated; the bit learning value storage is set (B\_lrng = 1). If the following conditions are fulfilled, the currently learned UEA are entered into the permanent RAM (udkplasr\_w and udkp2asr\_w).

Conditions:

( udkplas_w - udkplasr_w  > UAN_STORE)	OR
(B_pwf = 1)	OR
(B_lrnerf = 0)	OR
(B_lrntesa = 1)	

Adaptation step 5 (lrnstep\_c = 5):

The value for the absolute NLP determined during the spring check is converted to a relative value (wdknlp\_w). The calculated value is checked for plausibility with the NLP tolerance range permitted for the DV-E (WDKNLPMI and WDKNLPMA). If the tolerance range is adhered to, NLP-new is reset (B\_nlpnew = 0). If the value is not within the tolerance range, the NLP-abort function is executed and NLP-fault (B\_nlpe = 1) is set. The correct NLP values are also passed on to the permanent RAM (udknlplr, udknlp2r and wdknlpr\_w), if the following conditions are fulfilled:

( udknlp1 - udknlplr  > UANSTORE)	OR
( wdknlp_w - wdknlpr_w  > WDKN_STORE)	OR
B_pwf = 1	OR
(B_lrnerf = false)	OR
B_lrntesa	

Adaptation step 6 (lrnstep\_c = 6):

Initialization for the gain adjustment (gain adj.). Calculation of the adjustment points (wdkvabub and wdkvabob), change control to non-amplified poti (udkplsv = 0) and enter setpoint for upper adjustment point (wdkada\_w = wdkvabob).

Adaptation step 7 (lrnstep\_c = 7):

After a waiting time (lrntim\_c >= LRNST7\_T), the actual values are read in the upper adjustment point (udkplrob and udkplvrob). The amplified actual value is checked for plausibility (UDKP1VOSC). In case of a fault the gain adj. abort function is executed.

Adaptation step 8 (lrnstep\_c = 8):

Enter setpoint for lower adjustment point (wdkada\_w = wdkvabub).

Adaptation step 9 (lrnstep\_c = 9):



After a waiting time ( $lrntim\_c \geq LRNST9\_T$ ) the actual values are read in the lower adjustment point ( $udkplrun$  and  $udkplvrn$ ). The amplified actual value is checked for plausibility ( $UDKP1VUSC$ ). Thereafter, the gain and the offset are calculated ( $udkplvo\_w$  and  $udkplvv\_w$ ) and checked for plausibility ( $UDKP1VOMI$ ,  $UDKP1VOMA$ ,  $UDKP1VVM I$  and  $UDKP1V VMA$ ). To finish off, the switch-over threshold was updated ( $udkplsv$ ), gain and offset were written into the permanent RAM ( $udkplvor$  and  $ukdplvvr$ ) and the learning success was set. In case of a fault the gain adj. abort function is executed.

Adaptation step 10 ( $lrnstep\_c = 10$ ):

In  $lrnstep\_c = 10$ , the adapted values are stored in the EEPROM. If the storage has been successful  $lrnstep\_c = 11$  is set. Has the storage not been successful, the DV-E-Adaption is stopped with  $lrnstep\_c = 10$  and the adapted values are then written in the EEPROM during the ECU-after-run. The DV-E-drive is enabled for normal operation ( $B\_dkaden = 0$ ), the injection is enabled ( $B\_dveada = 0$ ) and end of learning is set ( $B\_lrrndy = 1$  und  $B\_lrrnakt = 0$ ).

Adaptation step ( $lrnstep\_c = 11$ ):

The storage of the adapted values in the EEPROM has been successful. The DV-E-drive is enabled for normal operation ( $B\_dkaden = 0$ ), the injection is enabled ( $B\_dveada = 0$ ) and end of learning is set ( $B\_lrrndy = 1$  und  $B\_lrrnakt = 0$ ).

UMA abort function:

If no 'initial adaptation' has yet been performed ( $B\_lrrnws = 0$ ), irreversible SKA is realized as an output ( $B\_umauab = 1$ ). If an initial adaptation was performed, a basic initialization is performed ( $udkplasr\_w = UDKP1AURI$ ,  $udkp2asr\_w = UDKP2AURI$  and  $dkpstg\_w = DKPSTGMIN$ ) in the case of a detected actuator exchange ( $B\_nlpnw = 1$ ) and  $B\_lrrnerf = false$  is set. The permanent RAM values are continued to be transferred to the RAM ( $udkplasr\_w$  and  $ukdp2ar\_w$ ) and the settings for the adaptation are reset ( $B\_dkaden$ ,  $B\_dveada$ ,  $B\_lrrndy$  and  $B\_lrrnakt$ ).

NLP-abort function:

Setting of the NLP-fault ( $B\_nlpe = 1$ ) and settings of adaption reset ( $B\_dkaden$ ,  $B\_dveada$ ,  $B\_lrrndy$  und  $B\_lrrnakt$ ).

Gain adj. abort function:

Setting of the adjustment fault ( $B\_abgle = 1$ ), prohibit operation with amplified poti signal ( $udkplsv = 0$ ) and reset the settings for the adaptation ( $B\_dkaden$ ,  $B\_dveada$ ,  $B\_lrrndy$  und  $B\_lrrnakt$ ).

## 5.2 Temporary part =====

On the DV-E on which the DK enters the bore, the UMA is influenced by the temperature. That means that in case of a setpoint entry  $<< 1 \text{ } \text{DK}$  the DK can reach the UMA and that it can therefore be switched to zero current via the DLR range monitoring of the DV-E and the idle control (LLR) can no longer control the idling speed. For this reason, the UMA is increased in steps resp. decreased again to the learned value.

The offset formation is only permitted, if the engine temperature ( $t_{mot}$ ) has exceeded a threshold  $TMSUTMUMA$  and if the setpoint entry ( $w_{dks\_w}$ ) has undershot a threshold  $WDKSTMUMA$ .

A temp. offset is built up, if the DLR output ( $dlrspid\_w$  with  $B\_dlrspid$ ) exceeds the value  $DLRPIDSTMN$  for a time ( $dlrmxt \geq TDLRPIDMX$ ). The offset ( $udkpat\_w$ ) is increased by a delta ( $DUDKPTMP$ ) in each calculation cycle (50 ms). The offset is stored in the permanent RAM ( $udkpatr\_w$ ). The maximum possible offset is  $UDKPATMX$ . As soon as the offset is so large that the DLR is no longer at the limit stop ( $DLRPIDSTMN$ ), a time difference measurement is started ( $ttmumad$ ).

If the offset is no longer built up for at least a time ( $TTMUMASTA$ ), the temporary offset is reduced again. The delta per calculation cycle is  $DUDKPTMP/4$ .

As soon as the temp. offset is  $> 0$ , the gradient of the actual value potentiometer ( $dkpstg\_w$ ) is corrected, in order to avoid the DK from reaching the upper mechanical limit stop (OMA) when entering a setpoint of  $100 \text{ } \text{DK}$ . The maximum position the DK reaches, is the upper electrical DK limit stop (OEA).

The state of the temp. offset is indicated in  $tmpumast$ .

- $tmpumast = 0$ : no offset formation, resp. offset ( $udkpat\_w$ ) = 0
- 1: offset for UEA is increased, resp. is  $> 0$
- 2: offset for UEA is decreased

## 5.3 Resulting part =====

The resulting UEA is formed from the steady-state UEA and the temporary UEA offset.



The following applies:

```

udkp1a_w := ukdplas_w + udkpat_w
udkp2a_w := udkp2as_w - udkpat_w
udkp1a   := udkp1a_w
udkp2a   := udkp2a_w
    
```

## 6. Blocking of the injection

=====

By means of the system constant SY\_DVEADA, it is possible to adjust whether the injection in case of an adaptation need can be blocked or not by the BGDVE. If blocking is desired, then B\_dveada = 1. Via the blocking request (B\_dveada = 1) it can be ensured that an adaptation requested via the DV-E exchange detection can definitely be performed by the system in spite of a starting attempt.

## 7. DV-E adaptation by tester request

=====

The learning of the NLP, UMA and of the gain adjustment can in addition be triggered by a tester request. For this, the B\_lrndia must be set to 1. The adaption can only be activated again by the tester, if a transition B\_lrndia = true -> false -> true has been executed. During a SG-cycle ON it is allowed, that the DV-E adaption can be started repeatedly. To ensure that, if a currently running adaption is interrupted by tester request, adaption will run again correctly udkplsv = UPVGNENN / UDKPVID - UDKPIDUS is initialized.

In the case of a conditional compilation with SY\_TWDKS = 1 for adaption, at the end of the intake manifold module test, the environmental conditions for the adaption by tester request are left out if B\_lrnwt = 1. (B\_lrnwt = 1 only exists for SY\_TWDKS = 1).

Also see chapter 6 . 'Blocking of the injection'.

## 8. Permanent RAM and EEPROM storage

=====

The following RAM-cells are stored in the permanent RAM and in the EEPROM:

RAM	Permanent RAM	EEPROM
B_lrnerf	B_lrnerf	yes
B_lrnws	B_lrnws	yes
tnachl_w	tnachl_w	--
udknlpl	udknlplr	yes
udknlp2	udknlp2r	yes
udkpat_w	udkpatr_w	--
udkplas_w	udkplasr_w	yes
udkplvo_w	udkplvor	yes
udkplvv_w	udkplvvr	yes
udkp2as_w	udkp2asr_w	yes
wdknlp_w	wdknlpr_w	yes

## APP BGDVE 3.110 Application hint

### 1. Deactivation of parts of the function

=====

When switching off the following parts of the functions, it must be noted that an initial adaptation cannot be performed correctly.

Label	Passive value	deactivated ...
CWDVEFO	0	Open spring check
DUDKNLPO	5 V	NLP check and learning (DV-E exchange detection)
DUDKNLPU	5 V	dto.
FPRAT	143.25 °C	DV-E spring check (open,return)
LRNVB_T	FFFF (=1310.72 s)	UMA-learning in case of repetition
UAN_U.MT	143.25 °C	UMA learning and gain adjustment
TMSUTMUMA	143.25 °C	temp. UMA adaptation
WDKSTMUMA	0 %DK	dto.

### 2. Check of the DV-E return spring

=====

The engine speed threshold FPRNMAX should be adjusted such that when turning the starter, the threshold is not exceeded without injection. Thus it is ensured that in the case of DV-E exchange detection and simultaneous prohibition of the injection, see chapter 6 of the function description, the DV-E adaptation is performed correctly.

### 3. Learning of the UMA and gain adj.

=====

The engine speed threshold UANNMAX should be adjusted such that when turning the starter, the threshold is not exceeded without injection. Thus it is ensured that in the case of DV-E exchange detection and simultaneous prohibition of the injection, see chapter 6 of the function description, the DV-E adaptation is performed correctly.

**4. Temporary UEA adaptation**  
=====

An increase of the offset must take place so quickly that the DV-E-ES does not come into the temperature deactivation. The decrease of the offset is performed slower by a factor of 4. This value cannot be adjusted. That means, that the ramp-step may not be less than 4 increments, corresponds to 4,884 mV. The maximum permitted offset is determined by means of the parameter calculation program (see ANM). The time, after which a decrease of the offset is permitted (TTMUMASTA), should be roughly adjusted to the cooling behaviour of the DV-E. The value is preset to 2 minutes.

**5. DV-E exchange detection**  
=====

The time TDKNACH to avoid an incorrect DV-E exchange detection in case of a quick change of the ignition ON -> OFF -> ON should be adjusted such that during this time the throttle valve can definitely stabilize in the NLP. When using a DV-E5, this time should not be less than 2 s. It must be ensured that the min. ECU after-run time TNLSGMN in the function MOTAAUS is greater than TDKNACH.

For the extended DV-E exchange detection, a DK-setpoint of wdks\_w < 4.7%DK should be fixed in characteristic map FPWDKAPP for wped = 0.

**6. Air for the limphome position (NLP) of the DV-E**  
=====

The data made available by the DCM file assume a DV-E with a standard NLP of 5 DK over UMA. If the NLP diameter is changed, the parameters DUDKNLPU, DUDKNLPO, WDKPFPRZ1, WDKPFPRZ2, WDKNLPMI and WDKNLPMA need to be adjusted. For the adjustment the K3/ESI1-tolerance calculation should be used.

**7. Blocking of the injection**  
=====

So that a complete DV-E adaptation is performed when a DV-E exchange is detected with the ignition ON, the system constant SY\_DVEADA should generally be set = 1. If the injection is not prohibited with detected DV-E exchange, no DV-E basic adaptation is performed when the engine is started and therefore initialization values are loaded for the continued trip. --> idle speed fluctuations are possible.

**8. Selection of the DK-diameter for a good idle behaviour/**  
=====

Consideration of additional air leakage in the system  
=====

It generally applies: the larger the DK-diameter, the smaller are the desired DK-angles for the idle control. Possibly occurring additional air leakage sources in the system must be considered. Therefore the DK-diameter should not be too large compared to the displacement.

With this strategy variations between 0 %DK and 1 %DK during idling can be avoided. (this is acceptable from the point of view of the DV-E-control, however, some customers do not accept it.)

A reduction of the offset UDKPAOFF between UMA and UEA to minimize air leakage is not permitted!

**9. Other**  
=====

With changes of the DV-E dynamics, such as e.g. shortened setting times, the functions DV-E spring check, UMA learning and the gain adjustment need to be checked. Please also pay attention to the block ANM!

**DDVE 7.30 Diagnosis: EGAS-Actuator DV-E****FDEF DDVE 7.30 Function definition****1. Introduction**  
=====

In block diagrams fault type information as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the fault path XYZ back into the central diagnostic management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external fault paths, which occur as inputs, access methods are available, which read these pieces of information directly from the fault path status managed in the DFPM.

**2. Fault paths**  
=====



bgdve diagnosis

ggdve diagnosis

adve diagnosis

### ddve-main

#### 2.1 Function GGDVE

=====

For each fault path x = DK, DK1P or DK2P of this diagnostic function the following variables have been defined:

Status fault path x:	sfpx
Error flag x:	E_x
Cycle flag x:	Z_x
Fault type x:	TYP_x: (B_mxx, B_mnx, B_six, B_npx)
Clear fault path:	B_clx
Default value active:	B_bkx (optional)
Fault path code x:	CDTX
Fault class x:	CLAX
Fault severity x:	TSFX
CARB code x:	CDCX
Table of ambient cond. x:	FFTX

B\_dkp1e

B\_dkp1mx

B\_dkp1mn

B\_dkp1np

B\_dkp2e

B\_dkp2mx

B\_dkp2mn

B\_dkp2np

### ddve-ggdve-diag

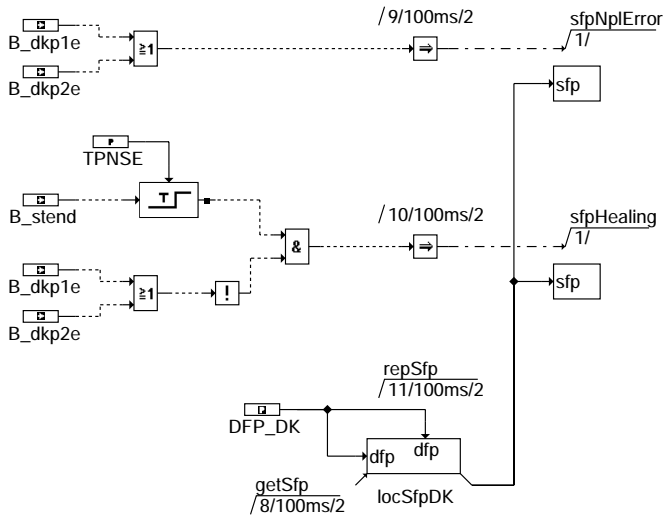
DK1P

DK

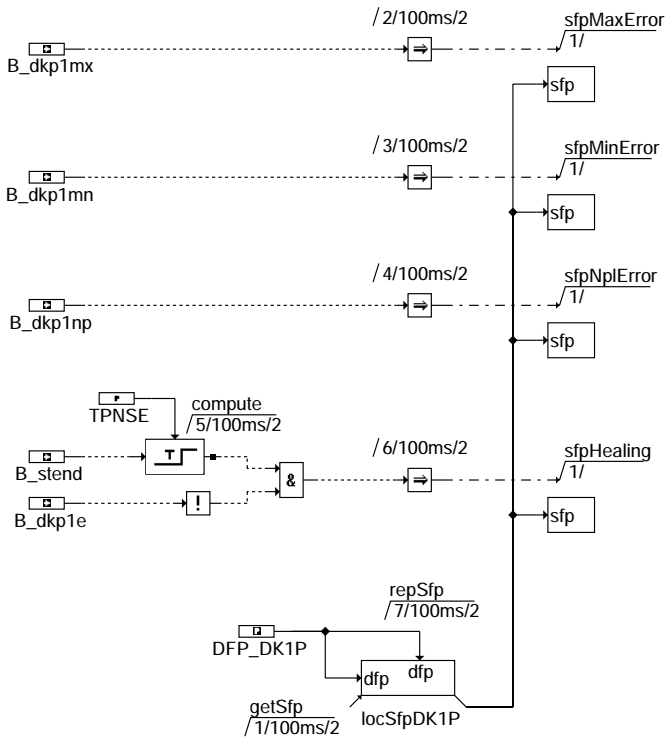
DK2P

ddve-main

ddve-ggdve-diag



### ddve-dk

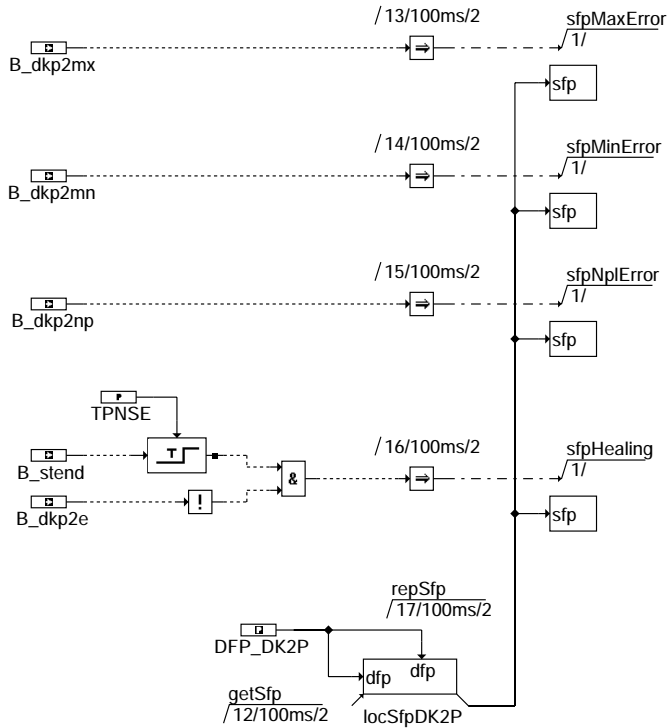


### ddve-dk1p

ddve-dk

ddve-dk1p





## ddve-dk2p

### 2.2 Function BGDVE =====

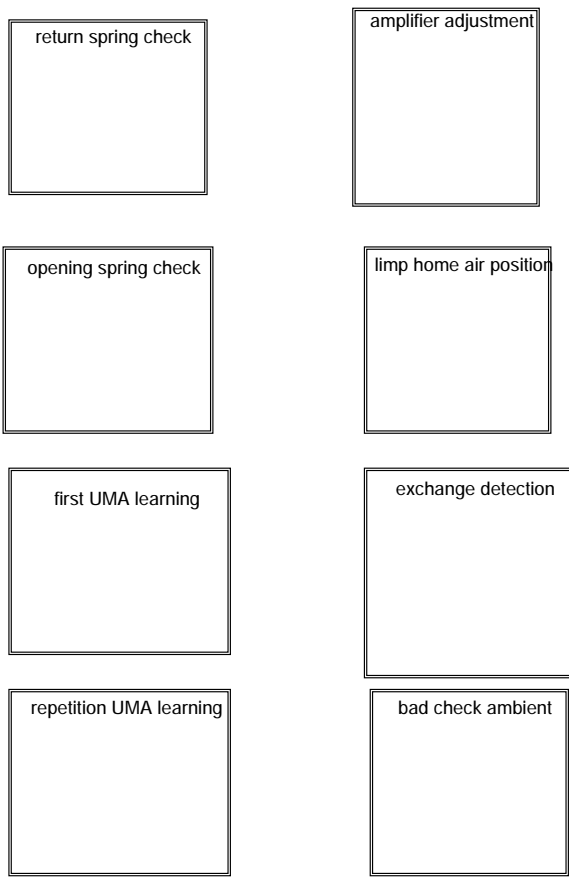
For each fault path x = DVEF, DVEFO, DVEN, DVET, DVEV, DVEU, DVEUW or DVEUB of this diagnostic function the following variables have been defined:

Status fault path x:	sfp <sub>x</sub>
Error flag x:	E <sub>-x</sub>
Cycle flag x:	Z <sub>-x</sub>
Fault type x:	TYP <sub>-x</sub> : (B <sub>-mxx</sub> , B <sub>-mnx</sub> , B <sub>-six</sub> , B <sub>-npx</sub> )
Clear fault path:	B <sub>-clx</sub>
Default value active:	B <sub>-bkx</sub> (optional)
Fault path code x:	CDTX
Fault class x:	CLAX
Fault severity x:	TSPX
CARB code x:	CDCX
Table of ambient cond. x:	FFTX

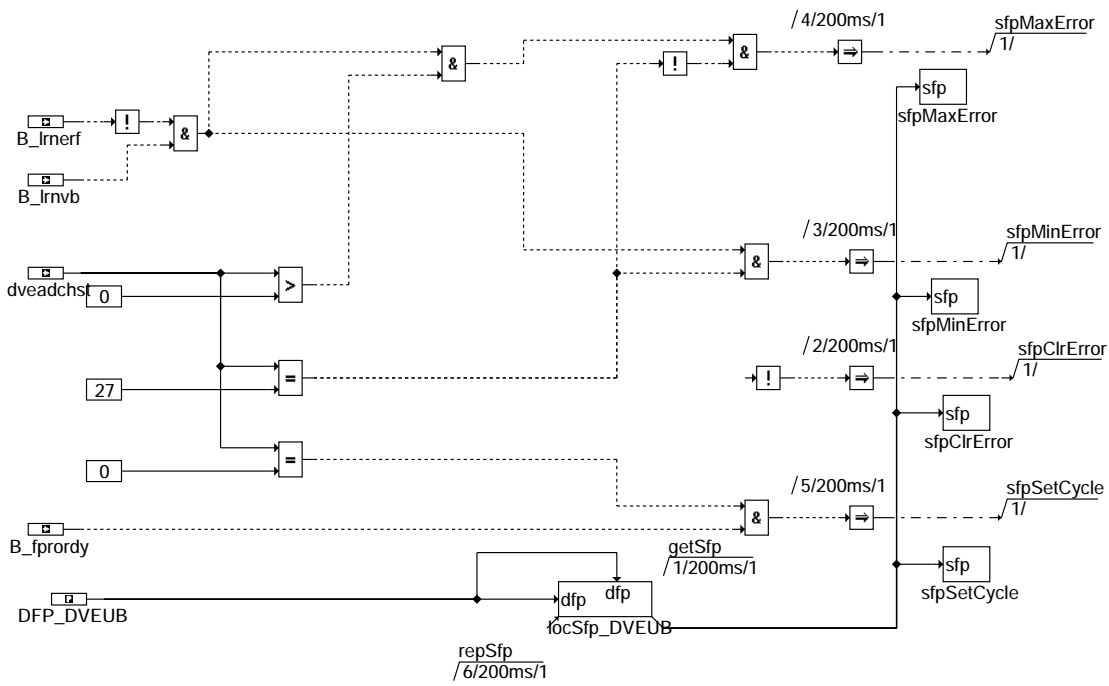
ddve-dk2p



- B\_abgle
- B\_fproab
- B\_fproe
- B\_fprook
- B\_fprordy
- B\_fprrdy
- B\_fprzab
- B\_fprze
- B\_lrnakt
- B\_lrnrdy
- B\_lrnrf
- B\_lrnvb
- B\_lrnws
- B\_nlpe
- B\_nlperf
- B\_nlpnew
- B\_pwf
- B\_umae
- B\_umauab
- fprstep\_c
- dveadchst
- lrnstep\_c

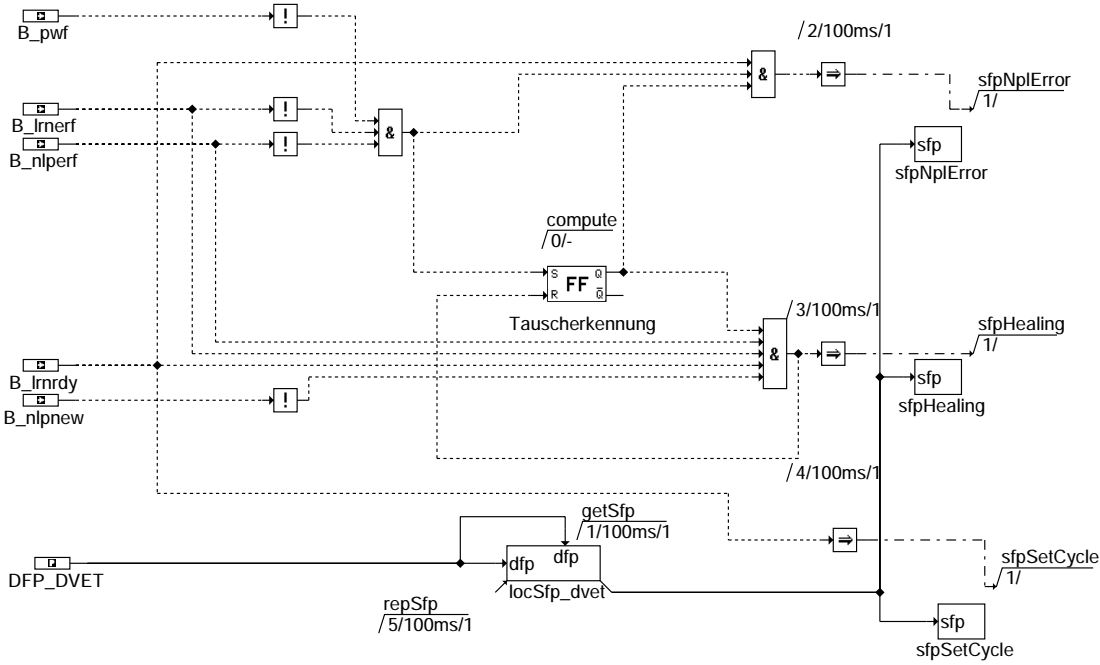


ddve-bgdve-diag



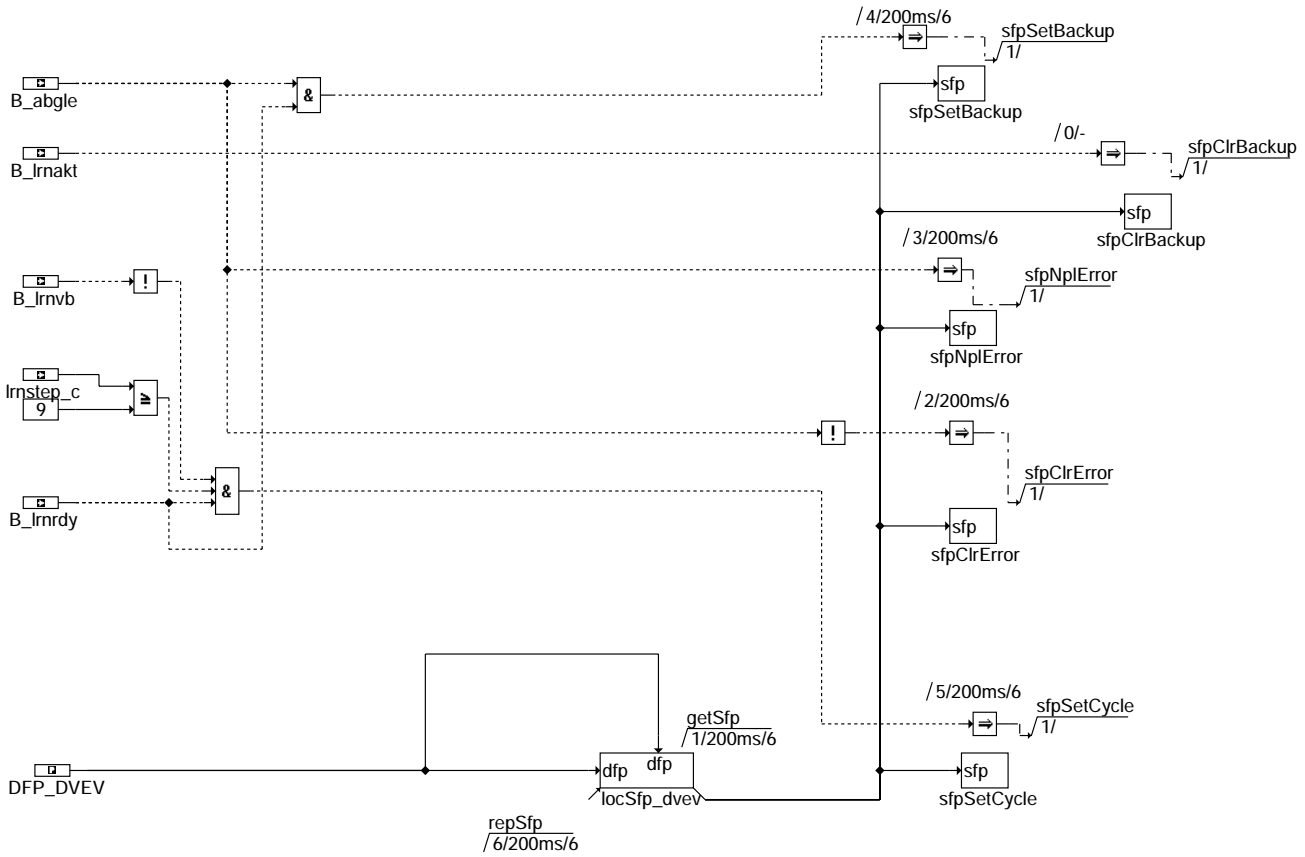
bad check ambient

ddve-bad-check-



### exchange detection

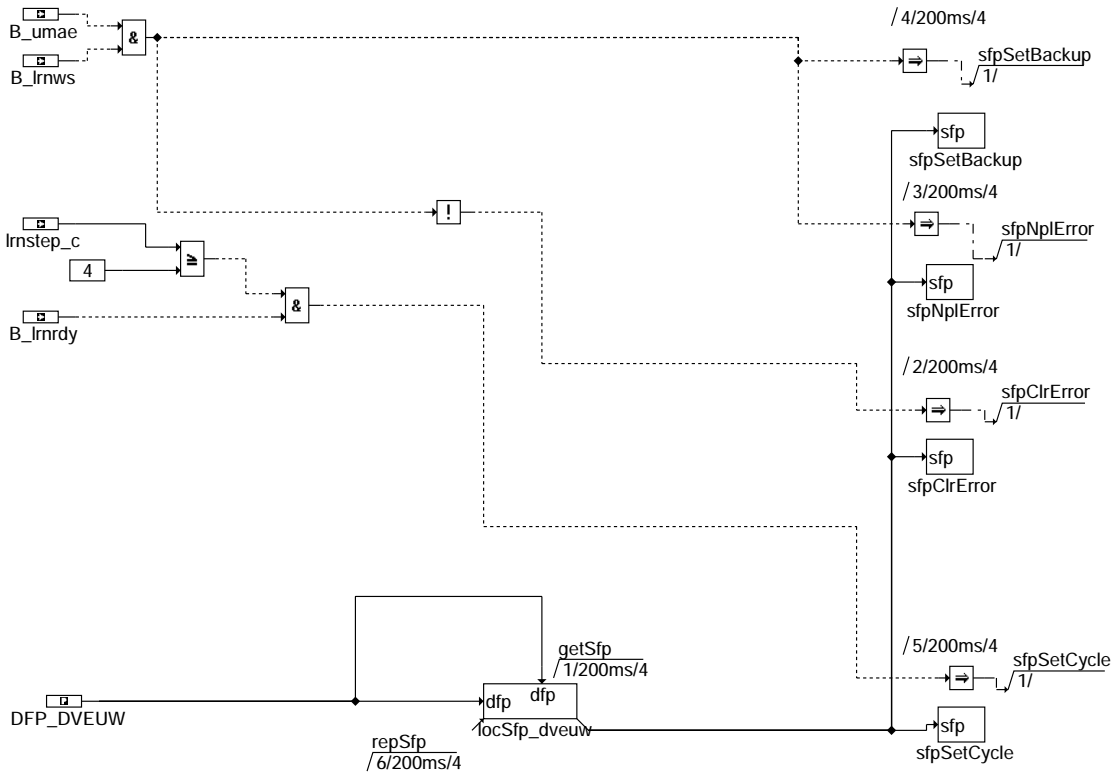
#### ddve-exchange-d



### amplifier adjustment

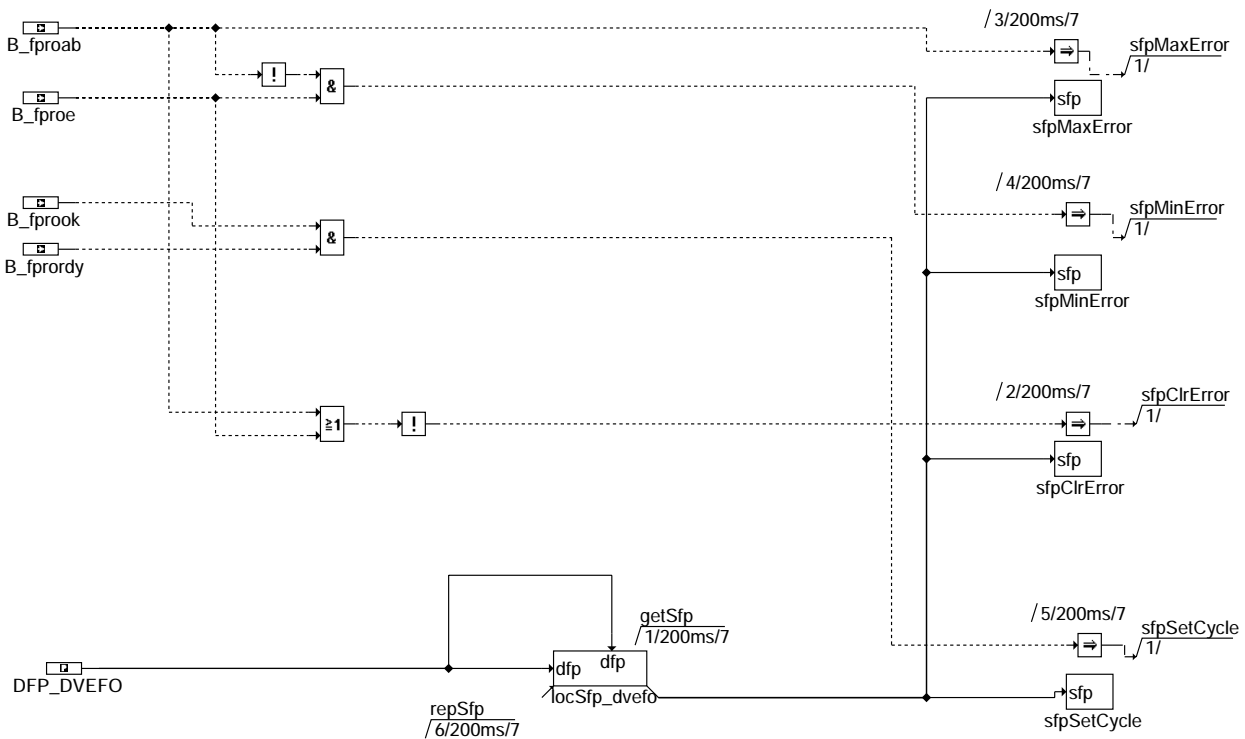
#### ddve-amplifier-





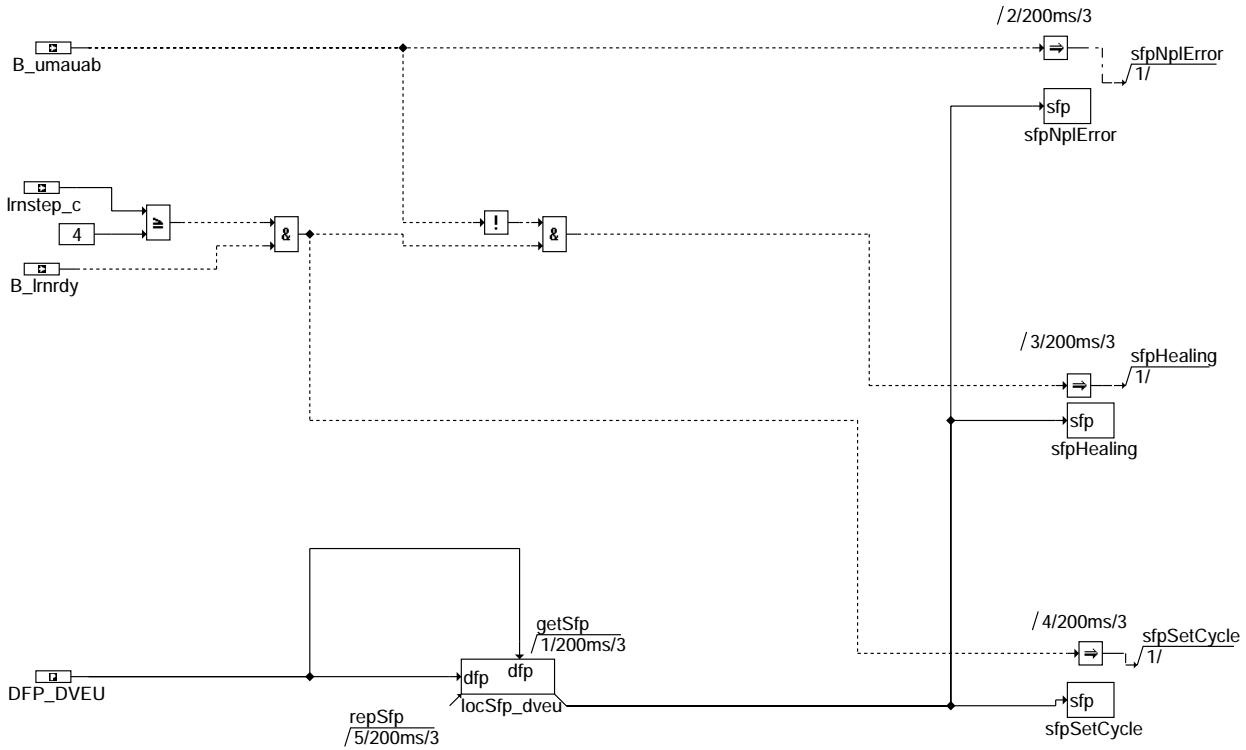
### repetition UMA learning

ddve-repetition



### opening spring check

ddve-opening-sp



### first UMA learning

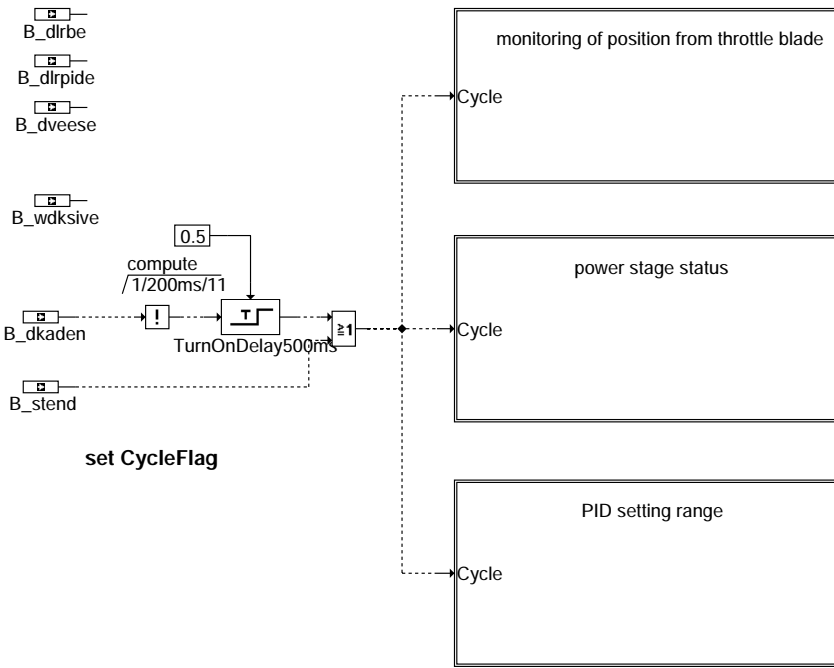
#### ddve-first-uma-

#### 2.3 Function ADVE =====

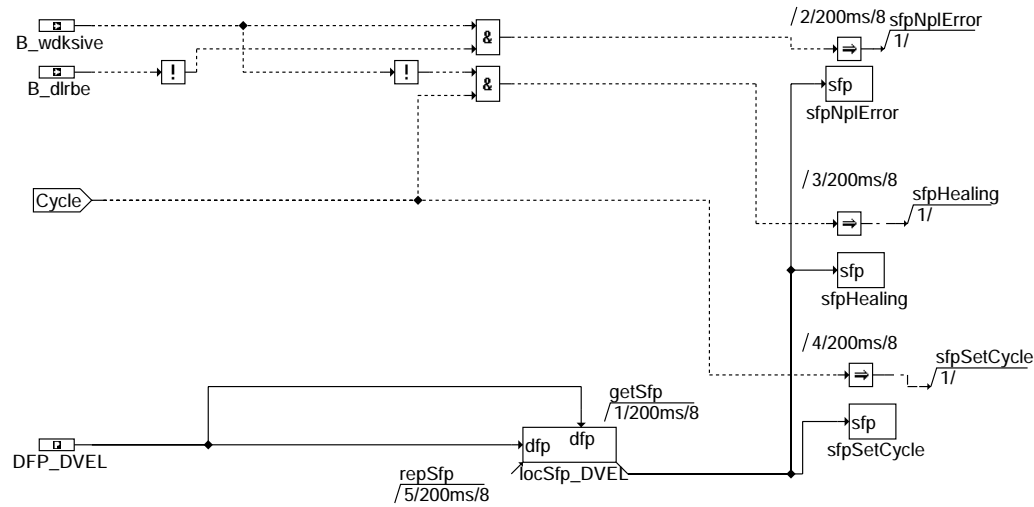
For each fault path x = DVEL, DVEE or DVER of this diagnostic function the following variables have been defined:

Status fault path x:	sfp <sub>x</sub>
Error flag x:	E_ <sub>x</sub>
Cycle flag x:	Z_ <sub>x</sub>
Fault type x:	TYP_ <sub>x</sub> : (B_ <sub>mxx</sub> , B_ <sub>mnx</sub> , B_ <sub>six</sub> , B_ <sub>np<sub>x</sub></sub> )
Clear fault path:	B_ <sub>clx</sub>
Default value active:	B_ <sub>b<sub>kx</sub></sub> (optional)
Fault path code x:	CDTX
Fault class x:	CLAX
Fault severity x:	TSEFX
CARB code x:	CDCX
Table of ambient cond. x:	FFTX

ddve-first-uma-

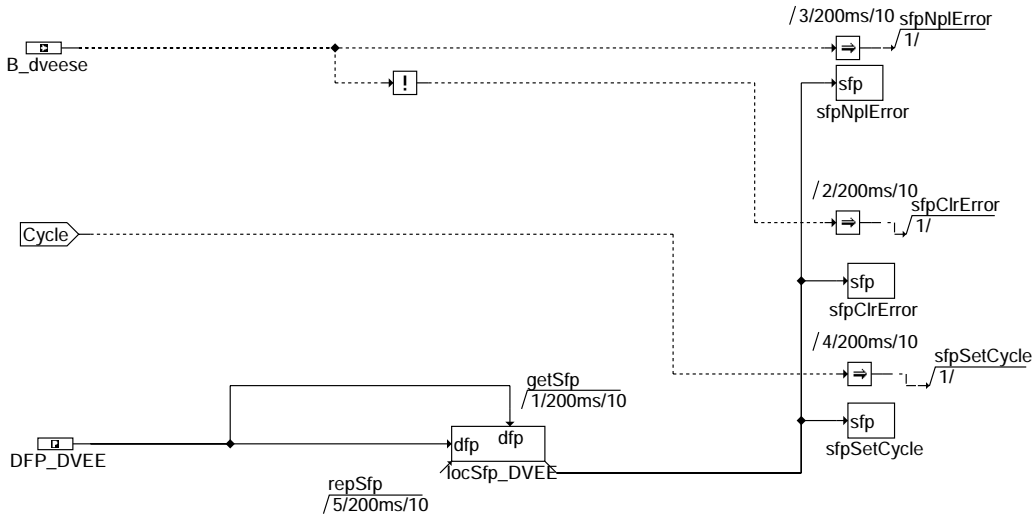


**ddve-adve-diagn**



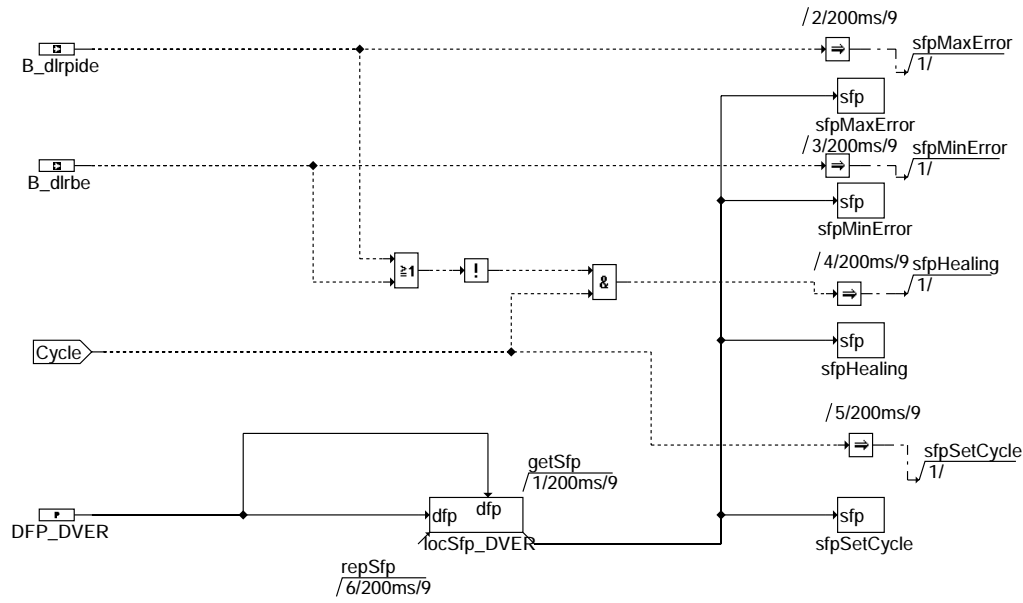
**monitoring of position from throttle blade**

**ddve-monitoring**



### power stage status

#### ddve-power-stag



### PID setting range

#### ddve-pid-settin

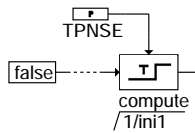
```

3. Initialization
=====
3.1 Function GGDVE
=====
    
```

ddve-power-stag

ddve-pid-settin





ddve-init

## ABK DDVE 7.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TPNSE			FW	Test time after start end for DVE diagnostic routine
Variable	Source		Type	Description
BLOKNR			EIN	DAMOS source for block number
B_ABGLE	BGDVE		EIN	Condition: Error during amplifier adjustment
B_BKDVEN	DDVE		LOK	Backup value activated: DV-E limphome air position
B_BKDVEU	DDVE		LOK	Backup value activated: DV-E UMA-learning
B_BKDVEUW	DDVE		AUS	Condition default value active: Fault during relearning of UMA
B_BKDVEV	DDVE		AUS	Backup value activated: DV-E amplifier adjustment
B_CLDVEF			EIN	Flag for clearance: DV-E cause of failure: spring check
B_CLDVEFO			EIN	Flag for detection: Fault in spring test "Open"
B_CLDVEN			EIN	Flag for clearance: DV-E cause of failure: limphome air position
B_CLDVEU			EIN	Flag for clearance: DV-E cause of failure: UMA-learning
B_CLDVEUW			EIN	Flag for deletion: Fault during UMA re-learning
B_CLDVEV			EIN	Flag for clearance: DV-E cause of failure: amplifier adjustment
B_DKADEN	BGDVE		EIN	Condition: Use DK setpoint from DK adaptation and DK check
B_DKP1E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 1
B_DKP1MN	GGDVE		EIN	Condition lower-range violation DK potentiometer 1
B_DKP1MX	GGDVE		EIN	Condition upper-range violation DK potentiometer 1
B_DKP1NP	GGDVE		EIN	Condition signal DK potentiometer 1 not plausible
B_DKP2E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 2
B_DKP2MN	GGDVE		EIN	Condition: lower-range violation DK potentiometer 2
B_DKP2MX	GGDVE		EIN	Condition: upper-range violation DK potentiometer 2
B_DKP2NP	GGDVE		EIN	Condition: signal DK potentiometer 2 not plausible
B_DLRBE	ADVE		EIN	Condition: DLR correction range exceeded
B_DLRPIDE	ADVE		EIN	Condition: Fault, DLR correction range at limit
B_DVEESE			EIN	Condition: DV-E power stage fault
B_FPROAB	BGDVE		EIN	Condition: Abort of DV-E open spring check, spring does not open
B_FPROE	BGDVE		EIN	Condition: Opening spring test fault
B_FPROOK	BGDVE		EIN	Condition: Opening spring test OK
B_FPRORDY	BGDVE		EIN	Condition: Opening spring test completed
B_FPRRDY	BGDVE		EIN	throttle return spring check ended
B_FPRZAB	BGDVE		EIN	Condition: Abort of DV-E return spring check, spring does not close
B_FPRZE	BGDVE		EIN	Condition: Error in the DV-E return spring check
B_LRNAKT	BGDVE		EIN	learning active bit
B_LRNERF	BGDVE		EIN	learning success bit
B_LNRNDY	BGDVE		EIN	learning complete
B_LRNVB	BGDVE		EIN	learning prohibition bit
B_LRNWS	BGDVE		EIN	learned value save bit
B_MNDK	DDVE		LOK	error type: short circuit to ground throttle potentiometer
B_MNDK1P	DDVE		LOK	Fault type min.: Throttle valve 1. Poti
B_MNDK2P	DDVE		LOK	Fault type min.: Throttle valve 2. Poti
B_MNDVEE	DDVE		LOK	error typ min.: DV-E power stage
B_MNDVEF	DDVE		AUS	Fault typ min.: DV-E cause of failure: spring open check
B_MNDVEFO	DDVE		AUS	error typ min.: cause of failure: spring check "open"
B_MNDVEL	DDVE		LOK	error typ min.: DV-E position deviation
B_MNDVEN	DDVE		LOK	Fault typ min.: DV-E cause of failure: limphome air position
B_MNDVER	DDVE		LOK	Fault type min.: DV-E control range, exceeded for a short time
B_MNDVEU	DDVE		LOK	Fault typ min.: DV-E cause of failure: UMA-learning
B_MNDVEUB	DDVE		LOK	error typ min.: end of DV-E adaption because of ambient conditions
B_MNDVEV	DDVE		LOK	Fault typ min.: DV-E cause of failure: amplifier adjustment
B_MXDK	DDVE		LOK	error type: short circuit to Ubat throttle potentiometer
B_MXDK1P	DDVE		LOK	Fault type max.: Throttle valve 1. Poti
B_MXDK2P	DDVE		LOK	Fault type max.: Throttle valve 2. Poti
B_MXDVEE	DDVE		LOK	error type max.: DV-E power stage
B_MXDVEF	DDVE		AUS	Fault typ max.: DV-E cause of failure: spring return check
B_MXDVEFO	DDVE		AUS	error type max.: cause of failure:spring check "open"
B_MXDVEL	DDVE		LOK	error type max.: DV-E position deviation
B_MXDVEN	DDVE		LOK	Fault typ max.: DV-E cause of failure: limphome air position
B_MXDVER	DDVE		LOK	Fault type max.: DV-E control range, violation for a long time
B_MXDVEU	DDVE		LOK	Fault typ max.: DV-E cause of failure: UMA-learning
B_MXDVEUB	DDVE		LOK	Fault type max.: Abort of DV-E-adaptation due to ambient condition
B_MXDVEV	DDVE		LOK	Fault typ max.: DV-E cause of failure: amplifier adjustment
B_NLPE	BGDVE		EIN	Condition: Error in NLP-check and learning
B_NLPERF	BGDVE		EIN	Permanent RAM, condition: NLP acquisition successful
B_NLPNEW	BGDVE		EIN	Condition: NLP position not yet known
B_NPDK	DDVE		LOK	Condition potentiometer signals from throttle valve not plausible
B_NPDK1P	DDVE		LOK	Fault type not plausible: Throttle valve 1. Poti
B_NPDK2P	DDVE		LOK	Fault type not plausible: Throttle valve 2. Poti
B_NPDVEE	DDVE		LOK	Fault type not plausible: DV-E power stage
B_NPDVEF	DDVE		LOK	Fault type not plausible: DV-E failure during spring check



Variable	Source	Type	Description
B_NPDVEL	DDVE	LOK	Fault type not plausible: DV-E position deviation
B_NPDVEN	DDVE	AUS	Fault type not plausible: DV-E fault in checking the limp-home air position
B_NPDVER	DDVE	LOK	Fault type not plausible: DV-E control range
B_NPDVET	DDVE	LOK	Fault type "not plausible": DV-E exchange detection without adaptation
B_NPDVEU	DDVE	AUS	Fault type not plausible: DV-E failure during UMA learning
B_NPDVEUW	DDVE	AUS	Fault type "not plausible" during relearning of UMA
B_NPDVEV	DDVE	AUS	Fault type not plausible: DV-E failure during amplifier adjustment
B_PWF		EIN	Condition for powerfail
B_SIDK1P	DDVE	LOK	error type: throttle valve potentiometer 1
B_SIDVEE	DDVE	LOK	error type: DV-E power stage
B_SIDVEF	DDVE	LOK	Fault type sig.: DV-E failure during spring check
B_SIDVEL	DDVE	LOK	error type: DV-E position deviation
B_SIDVEN	DDVE	LOK	Fault type sig.: DV-E failure during check of limp-home air position
B_SIDVER	DDVE	LOK	error type: DV-E control range
B_SIDVEU	DDVE	LOK	Fault type sig.: DV-E failure during UMA-learning
B_SIDVEV	DDVE	LOK	Fault type sig.: DV-E failure during amplifier adjustment
B_STEND	BBSTT	EIN	condition end of start
B_UMAE	BGDVE	EIN	Condition: Error during UMA learning
B_UMAUB	BGDVE	EIN	Condition: UMA learning stopped during first initialization (SKA)
B_WDKSIVE	ADVE	EIN	Condition: Fault in comparing DK angle nominal value/actual value
DFF_DVEE	DDVE	DOK	ECU internal fault-path no.: DV-E output stage
DFF_DVEF	DDVE	DOK	ECU-int. fault-path no.: DV-E failure during spring check
DFF_DVEFO	DDVE	DOK	Fault path: DV-E fault in spring check "Open"
DFF_DVEL	DDVE	DOK	ECU internal fault-path no.: DV-E position deviation
DFF_DVEN	DDVE	DOK	ECU-internal fault-path no.: DV-E failure during check of limp-home air position
DFF_DVER	DDVE	DOK	ECU-internal fault-path no.: DV-E control range
DFF_DVET	DDVE	DOK	Fault path: DV-E exchange detection without adaptation
DFF_DVEU	DDVE	DOK	ECU-internal fault-path no.: DV-E failure during UMA learning
DFF_DVEUB	DDVE	DOK	Fault path: DV-E adaptation abort because of environmental conditions
DFF_DVEUW	DDVE	DOK	Fault path: UMA re-learning
DFF_DVEV	DDVE	DOK	ECU int. fault path no.: DV-E fault in amplifier adjustment
DVEADCHST	BGDVE	EIN	DV-E adaptation: Status test conditions
E_DK	DDVE	AUS	Error flag: throttle position sensor
E_DK1P	DDVE	AUS	Error flag: Throttle valve 1. Poti
E_DK2P	DDVE	AUS	Error flag: Throttle valve 2. Poti
E_DVEE	DDVE	AUS	Error flag: DV-E power stage
E_DVEF	DDVE	AUS	Error flag: DV-E cause of failure: spring check
E_DVEFO	DDVE	AUS	error flag: DV-E cause of failure: spring check "open"
E_DVEL	DDVE	AUS	Error flag: DV-E position deviation
E_DVEN	DDVE	AUS	Error flag: DV-E cause of failure: limphome air position
E_DVER	DDVE	AUS	Error flag: DV-E control range
E_DVET	DDVE	AUS	Errorflag: DV-E-exchange detection
E_DVEU	DDVE	AUS	Error flag: DV-E cause of failure: UMA-learning
E_DVEUB	DDVE	AUS	Error flag: Abort of DV-E adaptation due to ambient condition
E_DVEUW	DDVE	AUS	Error flag: Fault during relearning of UMA
E_DVEV	DDVE	AUS	Error flag: DV-E cause of failure: amplifier adjustment
FPRSTEP_C	BGDVE	EIN	step counter throttle return spring check
LRNSTEP_C	BGDVE	EIN	counter for learning time for a learning step
SFPDK		EIN	Status fault path DK: Throttle valve
SFPDK1P		EIN	Status fault path DK1P: Throttle valve potentiometer 1
SFPDK2P		EIN	Status fault path DK2P: Throttle valve potentiometer 2
SFPDVEE		EIN	Status word: DV-E power stage
SFPDVEF		EIN	Status word: DV-E cause of failure: spring check
SFPDVEFO		EIN	status fault path: DV-E-open spring check
SFPDVEL		EIN	Status word: DV-E position deviation
SFPDVEN		EIN	Status word: DV-E cause of failure: limphome air position
SFPDVER		EIN	Status word: DV-E control range
SFPDVET		EIN	Status fault path: DV-E exchange detection without adaptation
SFPDVEU		EIN	Status word: DV-E cause of failure: UMA-learning
SFPDVEUB		EIN	Status fault path: Abort of DV-E adaptation due to ambient condition
SFPDVEUW		EIN	Status fault path: UMA relearning
SFPDVEV		EIN	Status word: DV-E cause of failure: amplifier adjustment
Z_DK	DDVE	AUS	cycle flag: throttle position potentiometer
Z_DK1P	DDVE	AUS	Cycle flag: Throttle valve 1. Poti
Z_DK2P	DDVE	AUS	Cycle flag: Throttle valve 2. Poti
Z_DVEE	DDVE	AUS	Cycle flag: DV-E power stage
Z_DVEF	DDVE	AUS	Cycle flag: DV-E cause of failure: spring check
Z_DVEFO	DDVE	AUS	Cycle flag: DV-E fault for spring test "Open"
Z_DVEL	DDVE	AUS	Cycle flag: DV-E position deviation
Z_DVEN	DDVE	AUS	Cycle flag: DV-E cause of failure: limphome air position
Z_DVER	DDVE	AUS	Cycle flag: DV-E control range
Z_DVET	DDVE	AUS	Cycle flag: DV-E exchange detection without adaptation
Z_DVEU	DDVE	AUS	Cycle flag: DV-E cause of failure: UMA-learning
Z_DVEUB	DDVE	AUS	Cycle flag: Abort of DV-E adaptation due to ambient condition
Z_DVEUW	DDVE	AUS	Cycle flag: Fault during relearning of UMA
Z_DVEV	DDVE	AUS	Cycle flag: DV-E cause of failure: amplifier adjustment

**FW DDVE 7.30 Fixed Values**

Parameter	Value	Description
TPNSE		Test time after start end for DVE diagnostic routine

**FB DDVE 7.30 Detailed description of function**

## 1. Diagnosis

=====

## 1.1 Function GGDVE

=====

Three fault paths were defined for the workshop and CARB diagnosis.

- Path 'DK': Indicates that one poti is faulty and that the other poti is plausible to the default signal from load and speed or that both potentiometers are not plausible.
- Path 'DK1P': Indicates that poti 1 is faulty.
- Path 'DK2P': Indicates that poti 2 is faulty.

## 1.2 Function BGDVE

=====

Eight fault paths were defined for the workshop and CARB diagnosis.

- Path 'DVEF': Indicates that the DV-E return spring check was performed incorrectly.
- Path 'DVEFO': Indicates that the check of the just opening DV-E spring was performed incorrectly.
- Path 'DVEN': Indicates that the detected limp-home air position is incorrect.
- Path 'DVET': Indicates that at detected DV-E exchange no new adaptation was performed.
- Path 'DVEV': Indicates that the gain adjustment was performed incorrectly.
- Path 'DVEU': Indicates that UMA-learning was performed incorrectly during the initial initialization.
- Path 'DVEUW': Indicates that UMA-learning was performed incorrectly during repetition.
- Path 'DVEUB': Indicates that UMA-learning was aborted due to violated input conditions.

## 1.3 Function ADVE

=====

Three fault paths were defined for the workshop and CARB diagnosis.

- Path 'DVEL': Indicates that the throttle valve of the DV-E does not reach the desired position any longer
- Path 'DVEE': Indicates that the DV-E output stage has deactivated, e.g. due to excess temperature, excess current or undervoltage
- Path 'DVER': Indicates that the DLR lies outside of the valid control range.

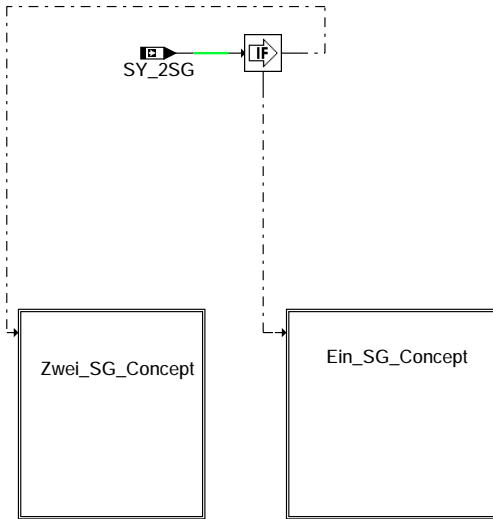
**APP DDVE 7.30 Application hint****SREAKT 10.10 EGAS: safety concept, failure reactions****FDEF SREAKT 10.10 Function definition**

## 1. Fault Coordination of the DV-E Triggering

=====

## 1.1 During Operation

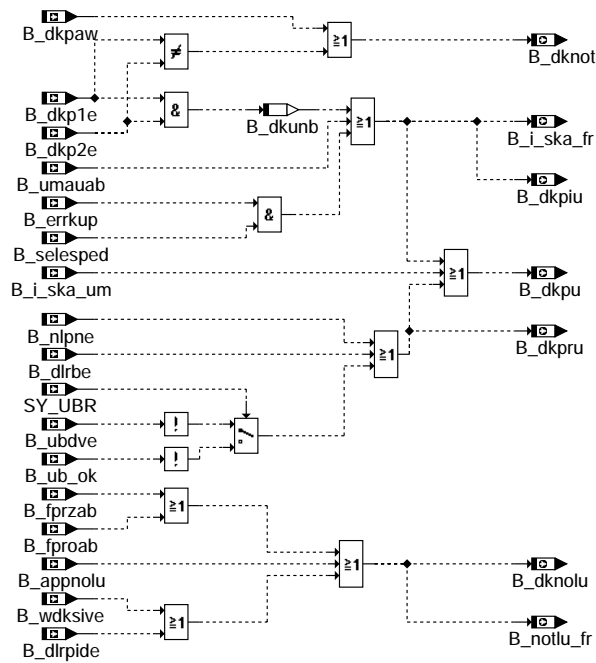
=====



### Fehlerreaktion

sreakt-sreakt

if (SY\_2SG = false) then



### Fehlerreaktion 1\_SG\_Concept

sreakt-ein-sg-concept

sreakt-sreakt

sreakt-ein-sg-concept

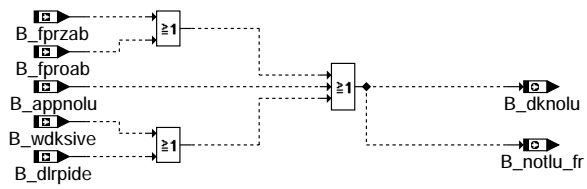


if (SY\_2SG) then



### Fehlerreaktion\_2\_SG\_Concept

sreakt-zwei-sg-concept

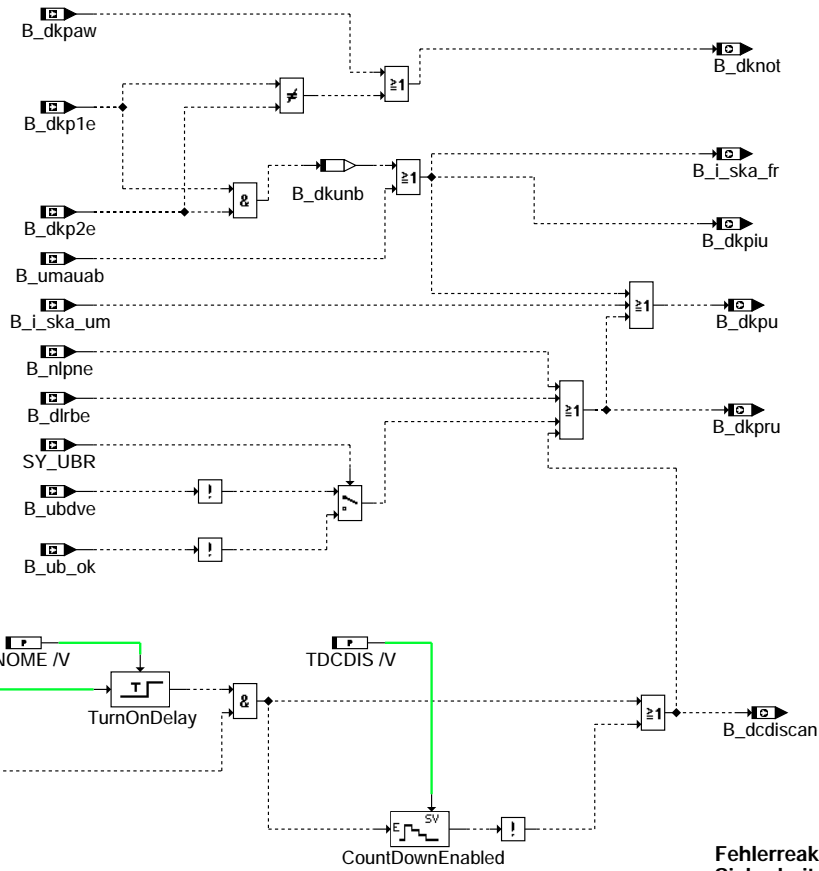


### Fehlerreaktion\_2\_SG\_Concept DK-Notluftfahren

sreakt-dk-notluftfahren

sreakt-zwei-sg-concept

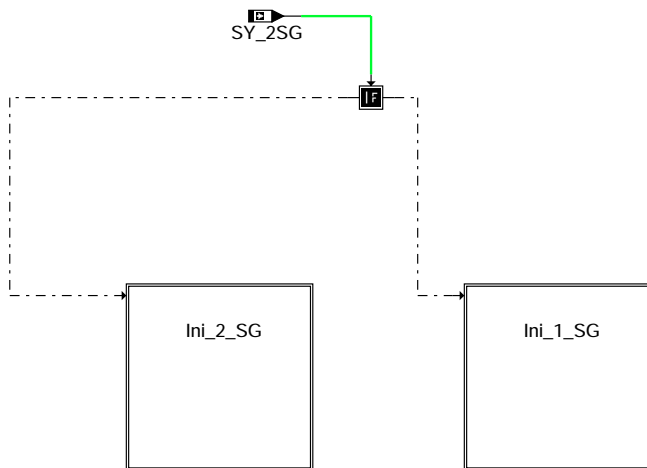
sreakt-dk-notluftfahren



**Fehlerreaktion 2\_SG\_Concept  
Sicherheitskraftstoffabschalt.**

**sreakt-sicherheitskraftstoffabschalt.**

1.1 Initialization  
=====



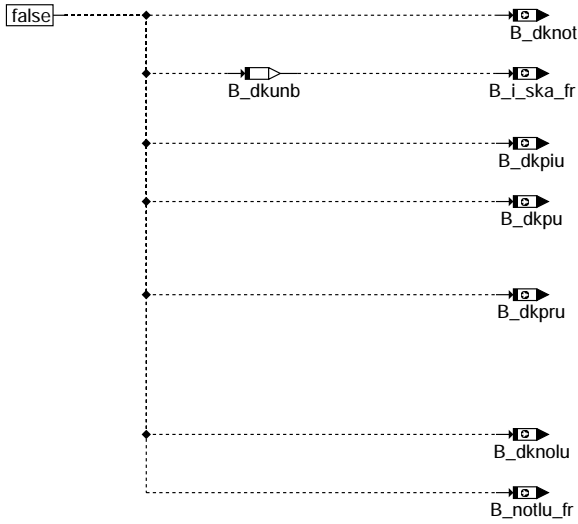
**Initialisierung**

sreakt-init

sreakt-sicherheitskraftstoffabschalt.

sreakt-init

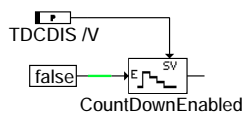
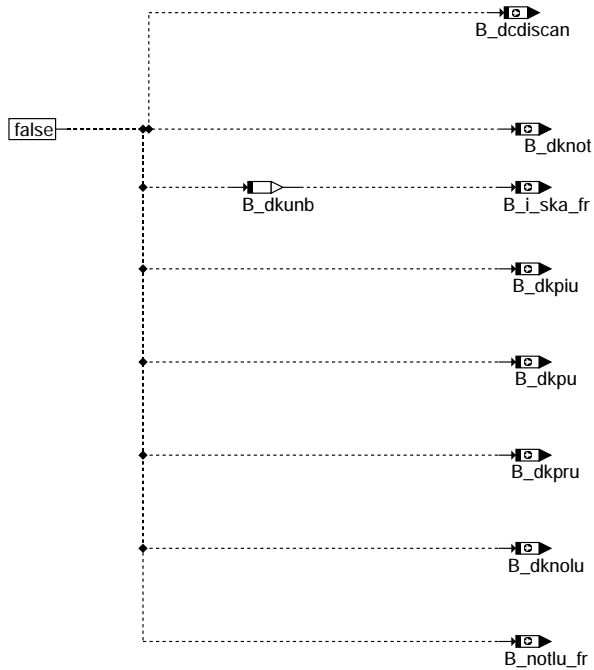
if (SY\_2SG = false)



### Initialisierung für 1\_SG

sreakt-ini-1-sg

if (SY\_2SG) then



### Initialisierung für 2\_SG

sreakt-ini-2-sg

2. Fault of the Pedal Sensor

=====

cf. GGPEDx.y

sreakt-ini-1-sg

sreakt-ini-2-sg



## ABK SREAKT 10.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TDCDIS			FW	Debouncing time for irreversible SKA in case of CAN fault
TNOME			FW	Debouncing time for idle presetting value in case of CAN fault
Variable	Source		Type	Description
B_APPNOLU	ADVE		EIN	Condition: Throttle limp-home air driving requested by application
B_DCDISCAN	SREAKT		AUS	Condition: DV-E power-stage-switch-off because of CAN-ERROR
B_DKNOLU	SREAKT		AUS	condition: power supply of throttle actuator cut off
B_DKNOT	SREAKT		AUS	condition: continued operation with a single remaining throttle actuator poti
B_DKP1E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 1
B_DKP2E	GGDVE		EIN	condition: defect in throttle actuator potentiometer 2
B_DKPAW			EIN	Condition DK-potentiometer selection for DK-sensor standby operation
B_DKPIU	SREAKT		AUS	Condition: irreversible SKA
B_DKPRU	SREAKT		AUS	Condition: reversible SKA
B_DKPU	SREAKT		AUS	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DKUNB	SREAKT		LOK	condition: unknown throttle blade position
B_DLRBE	ADVE		EIN	Condition: DLR correction range exceeded
B_DLRPIDE	ADVE		EIN	Condition: Fault, DLR correction range at limit
B_ERRKUP	DVKUP		EIN	Condition: engine switch-off caused by electronic clutch
B_ESGCAN			EIN	Condition error ecu-CAN for 2 ME-ecu's
B_FPROAB	BGDVE		EIN	Condition: Abort of DV-E open spring check, spring does not open
B_FPRZAB	BGDVE		EIN	Condition: Abort of DV-E return spring check, spring does not close
B_LSKA_FR	SREAKT		AUS	FR error reaction irreversible SKA (safety fuel shut-down)
B_J_SKA_UM	UFREAC		EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_MASTERHW			EIN	Condition Master-SG corresponding with code-pin (plausible)
B_NLPNE	ADVE		EIN	Condition: NLP not reached for DK standby trip
B_NOME_UM	UFMER		EIN	Condition replacement values are used caused by failures in the received message
B_NOTLU_FR	SREAKT		AUS	Request for NFB from Function controller
B_SELESPED			EIN	condition: car with selespeed
B_UBDVE	ADVE		EIN	Condition: Battery voltage for DV-E control OK
B_UB_OK	ADVE		EIN	Battery voltage o.k.
B_UMAUAB	BGDVE		EIN	Condition: UMA learning stopped during first initialization (SKA)
B_WDKSIVE	ADVE		EIN	Condition: Fault in comparing DK angle nominal value/actual value
SY_2SG	PROKON		EIN	system constant 2 motronic systems
SY_UBR	PROKON		EIN	system constant onboard battery voltage scanned from main relay input

## FW SREAKT 10.10 Fixed Values

Parameter	Value	Description
TDCDIS		Debouncing time for irreversible SKA in case of CAN fault
TNOME		Debouncing time for idle presetting value in case of CAN fault

## FB SREAKT 10.10 Detailed description of function

Task of the function is the evaluation of the fault states, which are generated in the modules of the DV-E triggering (cf. DVEUE2.x). These resulting faults start appropriate default functions dependent on the detected fault (throttle poti limp-home driving, throttle limp-home air driving or safety fuel deactivation).

For the application of the throttle limp-home air driving, the throttle limp-home air driving can be triggered in the function ADVE3.x via a code word. The bit B\_appnolu is then set.

Faults and fault reactions of the pedal sensor are treated in the function GGPED.

## APP SREAKT 10.10 Application hint

1-ECU-Concept:  
=====

No application is necessary.

2-ECU-Concept:  
=====

The time TNOME must be chosen distinctly smaller than MVER\_T\_UM from the torque monitoring.  
For example: TNOME = 200 ms. When used for the 2-ECU concept the system constant SY\_2SG must be set to true.

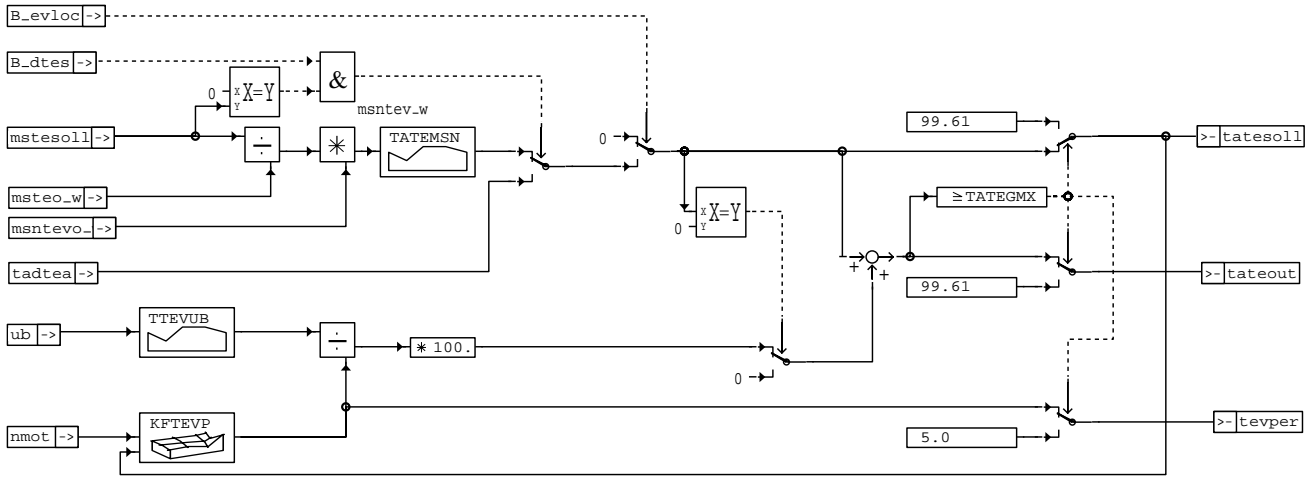
Systems with Main Relay for the Separate Voltage Supply of the DV-E After Terminal 15 OFF:  
=====

On systems with a main relay for the voltage supply of the DV-E5 with an additional measuring path for the voltage after the main relay, the system constant SY\_UBR must be set to true for conditional compiling to realize the cutoff chatter function.



## ATEV 2.0 Purge valve drive (duty cycle)

### FDEF ATEV 2.0 Function definition



atev-atev

### ABK ATEV 2.0 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFTEVP	NMOT	TATESOLL	KF	Characteristic map for period time of the PCV
TATEGMX			FW	Maximum PCV duty cycle for pulsed PCV activation
TATEMSN	MSNTEV_W		KL	characteristic line of the PCV duty-cycle depending on the desired mass-flow
TTEVUB	UB		KL	Battery-voltage depending delay time of canister purge valve

Variable	Source	Type	Description
B_DTES	GKRA	EIN	Condition for active diagnosis of canister purge system
B_EVLOC	BGEVAB	EIN	Status: all injection valves are activated
MSNTEVO_W	BGTEV	EIN	normalized mass flow through the complete open PCV
MSTEO_W	BGTEV	EIN	Mass flow the 100 % opened TEV
MSTESOLL_W	TEB	EIN	desired purge mass flow
NMOT	SWADAP	EIN	engine speed
TADTEA	DTEV	EIN	TEV duty cycle from canister purge diagnosis
TATEOUT	ATEV	AUS	output duty cycle for canister purge valve
TATESOLL	ATEV	AUS	desired duty cycle of the PCV
TEVPER	ATEV	AUS	periode time of purge control valve
UB	SWADAP	EIN	battery voltage

### FW ATEV 2.0 Fixed Values

Parameter	Value	Description
TATEGMX		Maximum PCV duty cycle for pulsed PCV activation

### FB ATEV 2.0 Detailed description of function

The function ATEV calculates the desired duty-cycle of the PCV (tatesoll) for further treatment in BGTEV and also the output sources for the PCV-timer tateout (duty cycle) and tevper (period time).

Tatesoll is calculated from the following sources:

mstesoll\_w = desired purge mass flow through the PCV  
 msteo\_w = purge mass flow through the complete open PCV  
 msntevo\_w = normalized overcritical purge mass flow through the complete open PCV  
 Kennlinie TATEMSN = characteristic line for the PCV duty-cycle depending on the desired normalized overcritical purge mass flow

Normalized overcritical purge mass flow PCV:  $msntev\_w = mstesoll\_w / msteo\_w * msntevo\_w$

Output PCV duty-cycle:  $Tateout = tatesoll + delay\ time\ of\ PCV / Period\ time * 100\%$

Remarks:

- As tatesoll = 0%, tateout = 0% too.
- Tateout ist limited to 99.61 % begrenzt (max. value HEX is FF => PCV timer should activate the PCV all the time).

Further features:

- Switching tateout to 99.61% if tateout >= TATEGMX
- As tateout = 99.61% tevper is set to 5 ms => a fast closing of the PCV is possible, because the PCV timer can change it's duty-cycle every 5 ms.



## APP ATEV 2.0 Application hint

TTEVUB: Delay time of the PCV depending on the battery voltage

-----

7 V	9 V	11 V	13 V	15 V	17 V
11 ms	9.5 ms	7 ms	5.5 ms	4.5 ms	3.5 ms

KFTEVP: Characteristic map for the period time of the PCV

Values in ms:

	800	1200	2000	3000	4500	1/min
0%	128	110	100	80	60	
10%	110	100	80	70	50	
20%	80	80	60	50	40	
30%	70	60	50	40	30	
50%	60	40	30	30	30	
70%	60	40	40	40	40	
80%	80	80	80	80	80	<= if TEV delay is higher than 7 ms (at ubat > 11V)
90%	120	120	120	120	120	choose higher period times to avoid tateout = 99.61% at tatesoll < 90%
100%	120	120	120	120	120	

TATEGMX: 97% - Explanation: up to tateout = 97% there is continuous dosing. Then tateout and tatesoll jump to 99.61% !  
Reason: Above a max. duty cycle the purge control valve current does not fall to zero.

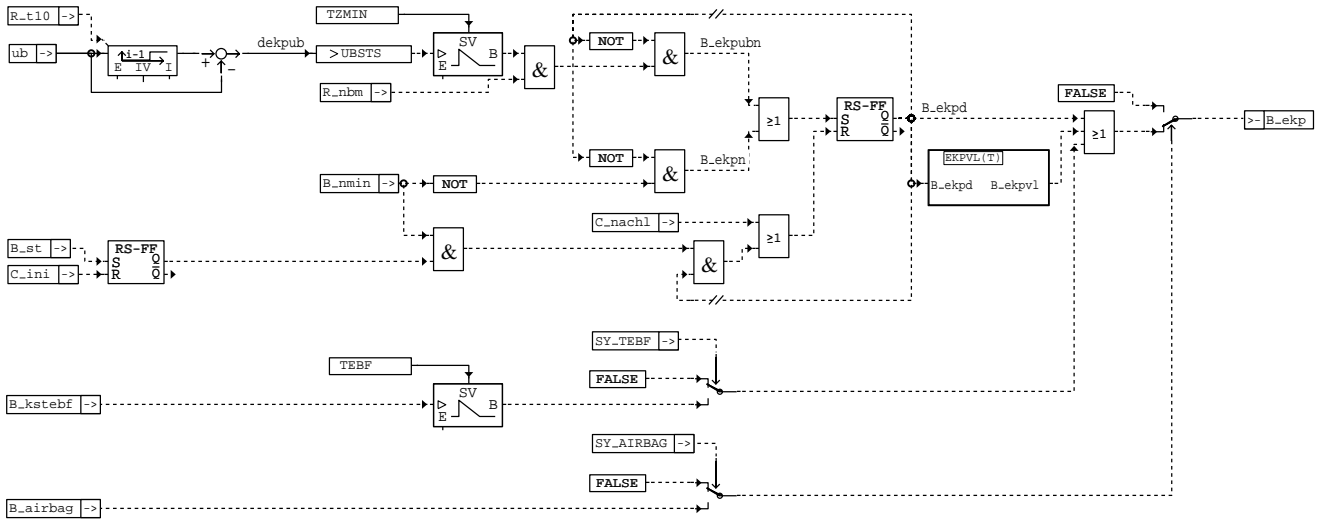
TATEMSN: Characteristic line for the PCV duty-cycle depending on the desired normalized overcritical purge mass flow

TATEMSN ist exactly the inverse characteristic line to MSNTATE ! Please consider when calibrating !

Example for first calibration: (small TEV2)	0	0.488	0.976	1.464	1.952	2.440	2.928	3.416	3.904	4.400	[kg/h]
	0	11.1	22.2	33.3	44.4	55.5	66.6	77.7	88.8	100	[%]
(big TEV2)	0	0.634	0.1.27	1.903	2.5375	3.172	3.8066	4.441	5.075	5.72	[kg/h]
	0	11.1	22.2	33.3	44.4	55.5	66.6	77.7	88.8	100	[%]

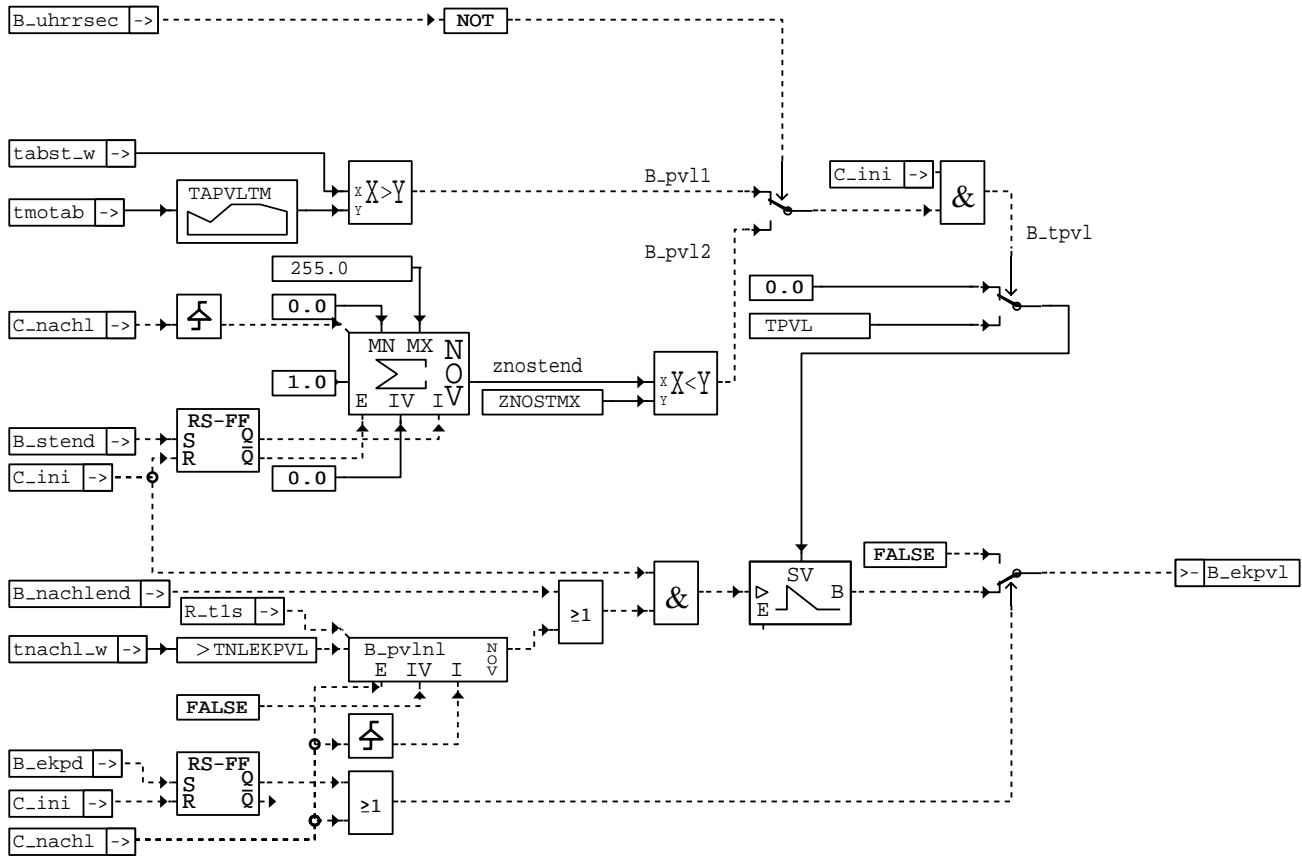
## AEKP 4.10 EKP control

### FDEF AEKP 4.10 Function definition



aeqp-aeqp

aeqp-aeqp



aekp-ekpvl

Subfunction EKPVL(T)

aekp-ekpvl



Electric fuel pump (EKP) control with lead time and suppression of interference during start

Signals may interfere the speed sensor (DG) line caused by operation of electric consumers during engine stop. These signals can exceed the switching threshold of the DG-preparation circuit and might be recognized as toothed disk pulses. This can lead to a false switch-on of the EKP. Monitoring of tooth speed and battery voltage during start can prevent this.

1. B\_ekpubn: Monitoring of battery voltage, EKP-start control



test of condition:  $dekpub = ub_{old} - ub_{act} > UBSTS$  and next tooth signal within TZMIN

1 : On  
B\_ekpubn: 0 : Off

2. B\_ekpn: Speed calculation, EKP-start control (if 1. not recognized)

B\_ekpn is set if B\_nmin is not set.

3. B\_ekpvl: EKP-lead time

The decision if EKP-lead time is necessary or desired can be reached in two different manners. If precise information about soak time is available EKP-lead time is released only when  $tabst_w > TAPVLTM$ . The characteristic line TAPVLTM contains the maximum soak time in minutes up to that no lead time is necessary depending on the engine temperature when the engine is stopped. If no precise information about soak time is available ( $B_{uhrsec} = 0$ ) EKP-lead time is released when number of ignition=on-->off without reaching end of start is less than ZNOSTMX. No lead time if ignition is switched on during ECM-afterrun ( $B_{nachlend}=0$ ) and when  $tnachl_w < TNLEKPVL$ . This ensures that lead time is available at the next start even when the ignition is switched on once again after the engine is stopped i.e. to close windows (power-windows).

4. B\_kstebf: Initial fuelling

If SY\_TEBF=true the EKP can be activated for TEBF seconds for initial fuelling of the fuel system. For further information see %TKMWL if available.

**ABK AEKP 4.10 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
TAPVLTM	TMOTAB		KL	threshold soak time for EKP-lead time
TEBF			FW	EKP operation for initial fuelling
TNLEKPVL			FW	threshold ECM-afterrun for EKP-lead time
TPVL			FW	time for fuel pump precontrol
TZMIN			FW	timeframe for recognition of teeth after battery voltage drop
UBSTS			FW	threshold for recognition of battery voltage drop
ZNOSTMX			FW	number of ignition=on without reaching end of start for no EKP-lead time
Variable	Source		Type	Description
B_AIRBAG			EIN	condition airbag activated
B_EKP	AEKP		AUS	Release of EKP-supply
B_EKPD	AEKP		LOK	condition EKP continuous duty
B_EKPN	AEKP		LOK	EKP starting condition engine speed
B_EKPUBN	AEKP		LOK	EKP starting condition speed sensor signal within TZMIN
B_EKPVL	AEKP		LOK	condition EKP lead time
B_KSTEBF			EIN	condition initial fuelling
B_NACHLEND	MOTAUS		EIN	condition ECU switch off delay regularly finished
B_NMIN	GGDPG		EIN	condition lower speed: $n < NMIN$
B_PVL1	AEKP		LOK	condition EKP-lead time for systems with clock
B_PVL2	AEKP		LOK	condition EKP-lead time for systems without clock
B_PVLNL	AEKP		LOK	condition EKP-lead time from ECM-afterrun duration
B_ST	SWADAP		EIN	condition for start
B_STEND	BBSTT		EIN	condition end of start
B_TPVL	AEKP		LOK	condition EKP-lead time for TPVL seconds
B_UHRRSEC	PROKON		EIN	Condition clock with a relative counter of seconds
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_NACHL			EIN	ECU condition for ECU switch off delay
DEKPUB	AEKP		LOK	change in battery voltage between two following measurements
R_NBM	GGDPG		EIN	Schedule of tooth signal
R_T10			EIN	Time schedule 10 ms
R_T1S			EIN	Time schedule 1 s
SY_AIRBAG	PROKON		EIN	system constant airbag-signal present
SY_TEBF	PROKON		EIN	system constant initial filling fuel system (service device)
TABST_W	BGTABST		EIN	soak time



Variable	Source	Type	Description
TMOTAB	GGTFM	EIN	engine coolant temperature at engine stop or cut-off cranking
TNACHL_W	MOTAUS	EIN	time of ECU switch off delay
UB	SWADAP	EIN	battery voltage
ZNOSTEND	AEKP	LOK	Number ignition on without reaching end of start

### FW AEKP 4.10 Fixed Values

Parameter	Value	Description
TEBF		EKP operation for initial fuelling
TNLEKPV		threshold ECM-afterrun for EKP-lead time
TPVL		time for fuel pump precontrol
TZMIN		timeframe for recognition of teeth after battery voltage drop
UBSTS		threshold for recognition of battery voltage drop
ZNOSTMX		number of ignition=on without reaching end of start for no EKP-lead time

### FB AEKP 4.10 Detailed description of function

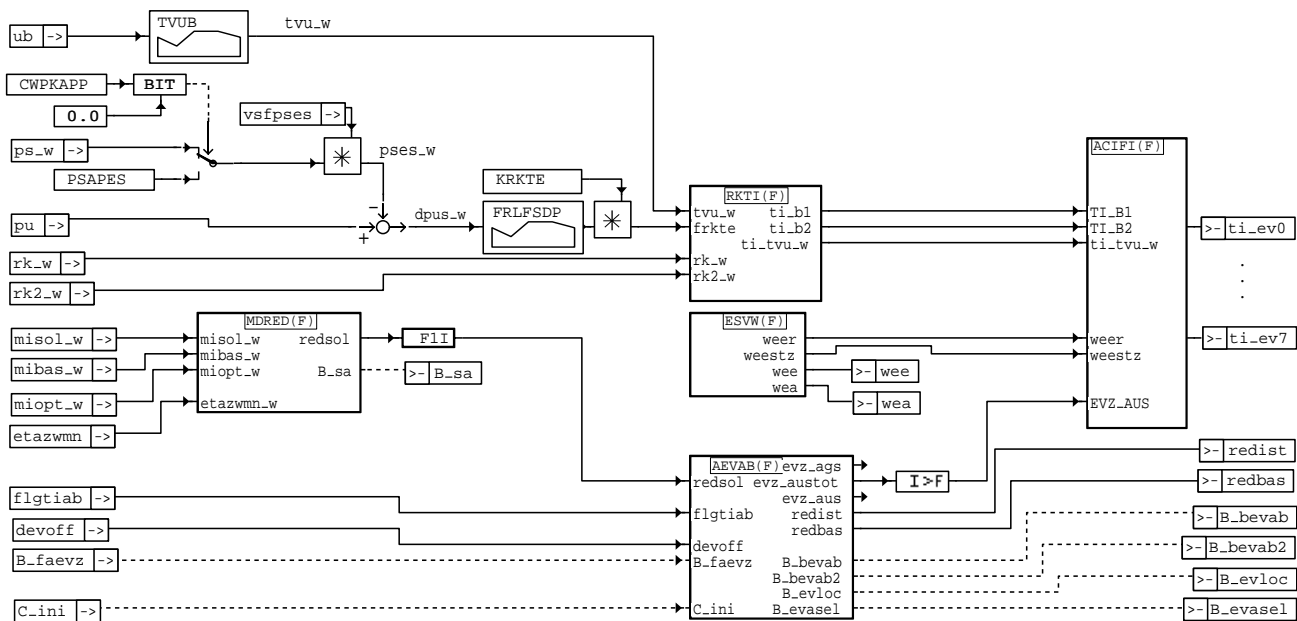
EKP-supply may not be released with B\_ekp = 0. For additional security, the EKP-supply may be locked by crash-sensor or signal from airbag-ECU.

### APP AEKP 4.10 Application hint

EKP-lead time is essential to obtain short starting time. TNLEKPV should always be less than TNLSGMX (%MOTAUS).

## AES 1.50 Overview calculation of injection time

### FDEF AES 1.50 Function definition



aes-aes

### ABK AES 1.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWPKAPP			FW	code word application of reference pressure for fuel-pressure controller
FRLFSDP	DPUS_W		KL	injection correction for RLFS
KKRKTE			FW	conversion from relative fuel mass rk into effective injection time te
PSAPES			FW	intake manifold pressure to apply injection
TVUB	UB		KL	voltage correction

Variable	Source	Type	Description
B_BEVAB	AES	AUS	condition: Inj. valve cut off on Bank/Bank1
B_BEVAB2	AES	AUS	condition: Inj. valve cut off on Bank2
B_EVASEL	AES	AUS	Status:all local injector relevant to DASE are switched on
B_EVLOC	AES	AUS	Status: all injection valves are activated
B_FAEVZ		EIN	condition cylinder fade out by tester
B_SA	AES	AUS	Condition fuel cut-off
C_INI	SWADAP	EIN	ECU-condition for intialisation
DEVOFF		EIN	injector fade out pattern at tester requirement
DPUS_W	AES	AUS	delta between ambient and intake manifold pressure



Variable	Source	Type	Description
ETAZW MN	ZW MN	EIN	minimum ignition angle effectiveness
ETAZW MN_W	AES	LOK	minimum ignition angle effectiveness
EVZ_AGS	AES	LOK	injection cut off pattern total of one or two ECU
EVZ_AUS	AES	LOK	injection cut off pattern
EVZ_AUSTOT	AES	LOK	injection cut off pattern total
FLGTIAB	DMDMIL	EIN	state flag ti turn-of by catalyst damaging misfiring rates
FRKTE	AES	LOK	factor: conversion rel. fuel mass rk into effect. injection time te
MIBAS_W	MDBAS	EIN	indicated basic torque
MIOPT_W	MDBAS	EIN	optimum indicated torque
MISOL_W	MSF	EIN	indicated resultant nominal torque
PSES_W	AES	LOK	intake manifold pressure corrected bei application system
PS_W	EGFE	EIN	intake manifold pressure (absolute) (Word)
PU	BGPU	EIN	Ambient pressure
REDBAS	AES	AUS	Base cut-off step
REDIST	AES	AUS	real cylinder cut-off step
REDSOL	AES	LOK	calculated desired cylinder cut-off step
RK2_W	MSF	EIN	relative fuel mass Bank2
RK_W	MSF	EIN	relative fuel mass
TI_B1	AES	LOK	injection time for valves on bank1
TI_B2	AES	LOK	injection time for valves on Bank2
TI_EV0	AES	AUS	injection time 1. cylinder in firing sequence
TI_EV1	AES	LOK	injection time 2. cylinder in firing sequence
TI_EV7	AES	AUS	injection time 8th cylinder in firing sequence
TI_EV8	AES	LOK	injection time 9th cylinder in firing sequence
TI_TVU_W	AES	LOK	injection time correction as function of battery voltage ECU-quantization
TVU_W	AES	LOK	supply of voltage correction
UB	SWADAP	EIN	battery voltage
VSFPSES	VS_VERST	EIN	factor for modifying intake manifold pressure during Application injection
WEA	AES	AUS	anglemark injection break off
WEE	AES	AUS	angle injection-end in normal operation
WEER	AES	LOK	resulting crankshaft angle for end of injection
WEESTZ	AES	LOK	angle injection-end for triggering simultaneous injection at start

### FW AES 1.50 Fixed Values

Parameter	Value	Description
CWPKAPP		code word application of reference pressure for fuel-pressure controller
KRKTE		conversion from relative fuel mass rk into effective injection time te
PSAPES		intake manifold pressure to applicate injection

### FB AES 1.50 Detailed description of function

The function AES shows the calculation of the injection time (injection valve control time) from the relative fuel mass rk\_w, rk2\_w.

The injection time is calculated bank-selectively and results as:

$$ti\_b1 = rk\_w * frkte + tvu\_w$$

$$ti\_b2 = rk2\_w * frkte + tvu\_w$$

wherein

ti_b1, ti_b2	bank-selective injection time
rk_w, rk2_w	relative fuel mass, bank-selective
frkte	correction for returnless fuel systems (FRLSDP) and translation of relative fuel mass rk into effective injection time te (KRKTE).
tvu_w	battery voltage compensation of the injection valves ( response delay with differing battery voltage)
FRLFSDP	correction of injection fuel mass at returnless fuel systems

In the AEVAB function, a valve cutoff pattern ev\_zaustot is formed from the fixed valve cutoff patterns of the misfire flag DASE (flgtiab), the tester specification for cutoff of an injection valve for tests at the end of line assembly (devoff) where B\_faevz = true, the error of injection valves E\_ev and from the reduction stage redsol specified by the torque reduction.

Based on the valve cutoff pattern the information bits B\_bevab, B\_bevab2 are formed, indicating the bank on which injection valves are shut off.



## APP AES 1.50 Application hint

Calculation of constant KRKTE:

$$KRKTE \text{ [ms/\%]} = \frac{\rho_{0Air} \text{ [g/dm}^3\text{]} * V_{hZyl} \text{ [dm}^3\text{]}}{100[\%] * Lst * Normmk \text{ [min/ms]} * 1.05 * Qstat \text{ [g/min]}}$$

$$KRKTE = 50.2624 * V_h / Qstat$$

where

$\rho_{0Air} = 1.293 \text{ g/dm}^3$  (0°C and 1013hPa)  
 $V_{hZyl} = \text{dm}^3$  Displacement of a cylinder in dm<sup>3</sup>  
 $Qstat = \text{g/min}$  Valve constant with n-Heptane  
 $1.05$  Valve correction for petrol/n-Heptane  
 $Lst = 14.7$  Air/fuel ratio for Lambda = 1.0  
 $Normmk = 0.00001667 \text{ min/ms}$  Adaptation of units

Calculation of the correction for returnless fuel systems:

$$FRLFSDP = V_{pdr\_evmes} / (pdr\_akt + (p_u - p_s))$$

Wherein  $pdr\_evmes$  = absolute pressure in the fuel circulation upstream of the injection valve at measuring  $Qstat$  (3000 hPa)  
 $pdr\_akt$  = actuell system pressure in fuel circulation  
 $p_u$  = ambient pressure  
 $p_s$  = intake manifold pressure

At systems with reference pressure at intake manifold  $p_u - p_s = 0$ .  
The correction for the complete characteristic a this one is:

$$FRLFSDP = V_{pdr\_evmes} / pdr\_akt$$

For a fuel pressure of 3000 hPa the result for FRLFSDP is:

Wherein  $dpus = p_u - p_s$

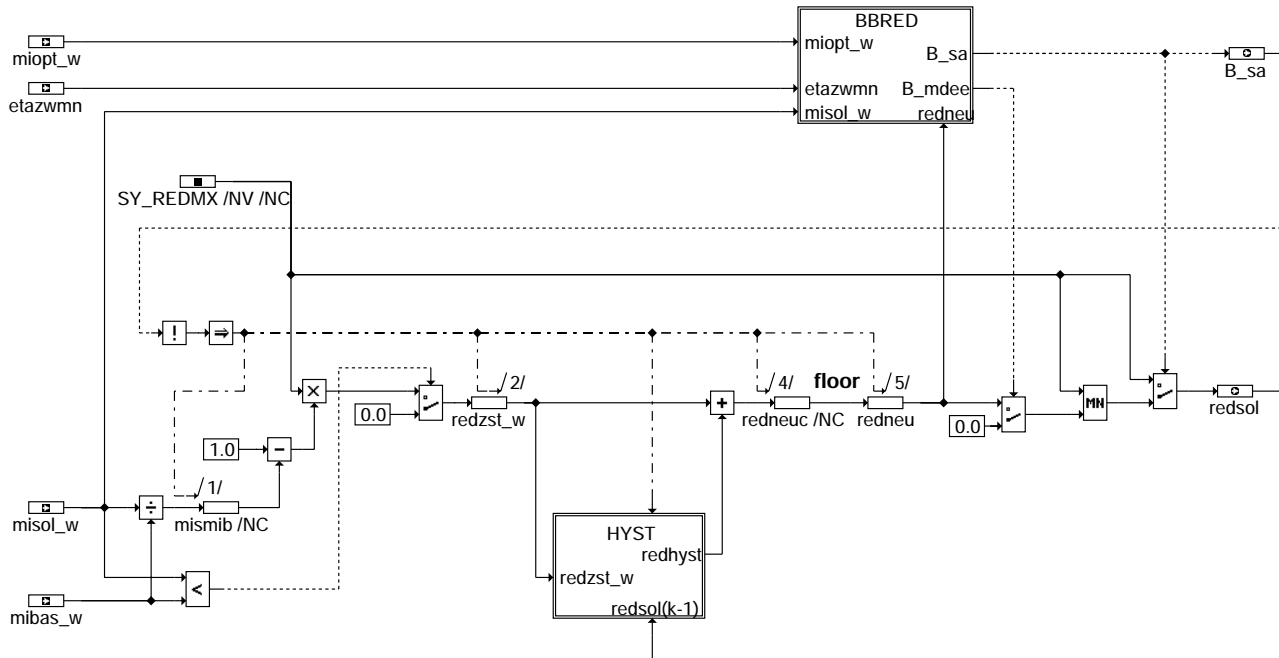
Induction engine 3000 hPa /3500 hPa		Turbo engine:		
$dpus$ [hPa]	FRLFSDP	$dpus$ [hPa]	FRLFSDP	
0	1.0	-1200	1.299	$p_{BoostPress} = 1800 \text{ hPa}, p_u = 600 \text{ hPa}$
100	0.9837	-1000	1.2247	
200	0.9682	-800	1.1678	
300	0.9535	-600	1.1180	
400	0.9393	-400	1.0742	
500	0.9258	-200	1.0351	
600	0.9129	0	1.0	
700	0.9005	200	0.9682	
800	0.8885	400	0.9393	
		600	0.9129	
		800	0.8885	

There are 11 interpolation points implemented for induction and turbo engine.

during application air charge measuring, the modelled intake manifold pressure is not correct.  
 At returnless fuel systems the intake manifold pressure can be set by the application system VS100 with parameter PSAPES. Therefore bit 0 at CWPKAPP must be set.  
 The init value for PSAPES is 1013 hPa. The VS20 application System can correct the pressure PSAPES by the factor  $vsfpes$  with a range of 0 ... 2. The corrected pressure for calculation  $dpus\_w$  is  $pses\_w$ .

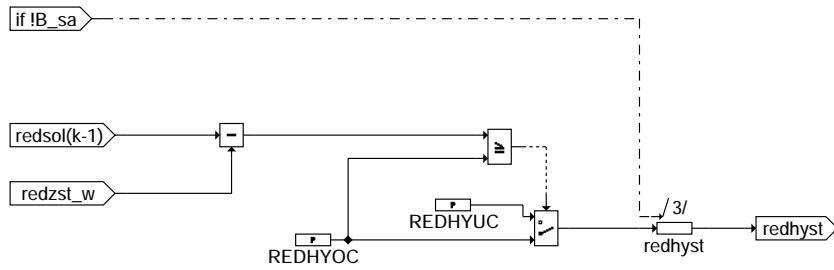
## MDRED 1.50 Calculation reduction step from torque demand

### FDEF MDRED 1.50 Function definition



#### mdred-main

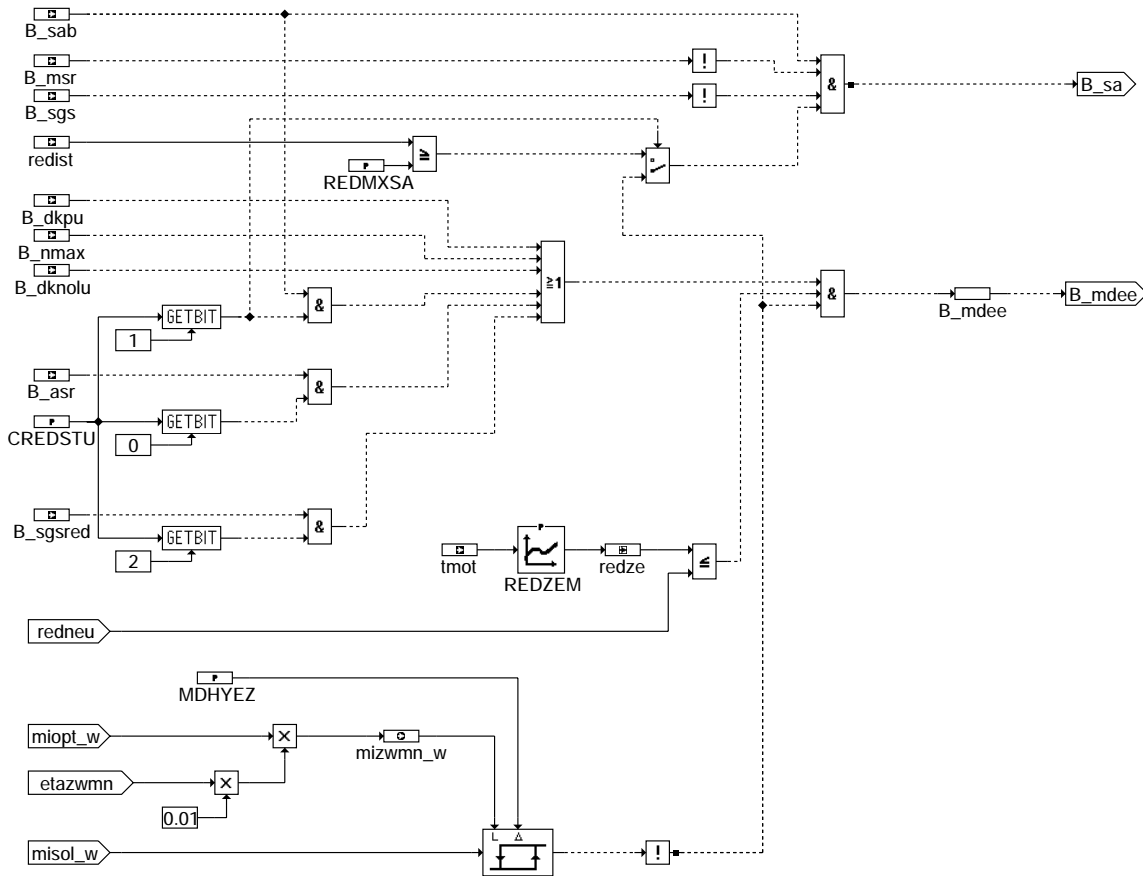
Sub-function HYST: Hysteresis to prevent bouncing of the masking stage:



#### mdred-hyst

Sub-function BBRED: Operating conditions of torque intervention over injection masking:





mdred-bbred

### ABK MDRED 1.50 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CREDSTU			FW	code word for reduction step on/off
MDHYZ			FW	torque-hysteresis for decision cylinder fuel cut-off
REDHYOC			FW	hysteresis of reduction step at bigger desired red. step than actual value
REDHYUC			FW	hysteresis of reduction step at smaller desired red. step than actual value
REDMXSA			FW	maximum reduction step for sequential fuel cutoff
REDZEM	TMOT		KL	threshold between ignition intervention and injector disabling
SY_REDMX			SYS (REF)	system constant: max. cylinder cutoff step

Variable	Source	Type	Description
B_ASR	MDKOG	EIN	condition for ASR active
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_MDEE	MDRED	LOK	condition: torque reduction by injection fade out is permitted
B_MSR	MDKOG	EIN	Condition MSR
B_NMAX	NMAXMD	EIN	1 = maximum engine speed exceeded
B_SA	MDRED	AUS	Condition fuel cut-off
B_SAB	MSF	EIN	Condition fuel cut-off requested
B_SGS	MDKOG	EIN	condition: torque intervention for engine speed synchr. during gear shift
B_SGSRED	CAN	EIN	condition: reducing torque intervention for eng. speed synchr. during gear shift
ETAZWMN	ZWMIN	EIN	minimum ignition angle effectiveness
MIBAS_W	MDBAS	EIN	indicated basic torque
MIOPT_W	MDBAS	EIN	optimum indicated torque
MISOL_W	MSF	EIN	indicated resultant nominal torque
MIZWMN_W	MDRED	AUS	indicated engine torque at the latest spark angle
REDHYST	MDRED	LOK	hysteresis for cylinder cut-off step
REDIST	BGEVAB	EIN	real cylinder cut-off step
REDNEU	MDRED	LOK	new calculated cylinder cut-off step
REDSOL	MDRED	AUS	calculated desired cylinder cut-off step
REDZE	MDRED	LOK	threshold of cylinder cut-off step between two interventions
REDZST_W	MDRED	LOK	cylinder cut-off step without hysteresis and roundness
TMOT	SWADAP	EIN	Engine temperature



## FW MDRED 1.50 Fixed Values

Parameter	Value	Description
CREDSTU		code word for reduction step on/off
MDHYEZ		torque-hysteresis for decision cylinder fuel cut-off
REDHYOC		hysteresis of reduction step at bigger desired red. step than actual value
REDHYUC		hysteresis of reduction step at smaller desired red. step than actual value
REDMXSA		maximum reduction step for sequential fuel cutoff

## FB MDRED 1.50 Detailed description of function

This function provides the injection masking stages corresponding to the nominal torque request  $misol_w$  (referred to the indexed engine torque  $mibas_w$ , which results at the static ignition angle  $zibase$  and basic  $\lambda$   $lambdas$ ). A hysteresis is used to ensure that no "bouncing" occurs in the selection of the reduction stages (cf. sub-function "HYST"). Cutting the decimal places ("Floor function") results in the new reduction stage. The sub-function "BBRED" determines whether injection masking is permitted ( $B_{mdee}$ ) and whether deceleration cut-off occurs ( $B_{sa}$ ).

The actual reduction stage  $redist$  results from a max selection between  $redbas$  (basic reduction stage due to bank shut-off or due to misfire detection) and the reduction stage  $redsol$  calculated from  $misol$ .

Sub-function HYST: Hysteresis to prevent bouncing of the masking stage

The hysteresis is determined by the difference between  $REDHYUC$  and  $REDHYOC$  and the offset of the hysteresis referred to the old value of  $redsol$ , divided by  $(1-REDHYOC)$ .  $REDHYUC$  must always be greater than  $REDHYOC$ . If the calculated masking stage  $redzst$  exceeds the current value of  $redsol$  by more than  $1-REDHYOC$  (if  $redzst_w > redsol(k-1)-REDHYOC$ ) or  $REDHYUC$  (if  $redzst_w \leq redsol(k-1)-REDHYOC$ ) stages, then the next masking stage must be selected.

Sub-function BBRED: Operating conditions of torque intervention over injection masking

The characteristic  $REDZEM$  in relation to the engine temperature can be used to establish the reduction stage  $redze$  from which injection masking is actually permitted. If the calculated reduction stage  $redneu$  is less than the value specified in the characteristic  $REDZEM$ , ignition angle intervention is activated. Injection masking is only possible when  $redsol \geq redze$  (see above) or when the requested torque  $misol_w$  is less than the possible torque  $mizwm$  at the latest ignition angle and the condition such as  $B_{ska}$ ,  $B_{dknolu}$  or  $B_{nmax}$  is set. At  $B_{asr} = 1$  cylinder masking is possible if in addition the 0th bit of  $CREDSTU$  is set to 1. Otherwise the injection angle intervention is limited to  $zwmn$  and no cylinder masking is possible. If  $misol_w$  is less than  $mizwm_w$  and  $B_{sab}$  is set, the condition  $B_{sa}$  is set and the nominal reduction stage  $redsol$  equals  $REDMX$ , so that deceleration cut-off occurs. In MSR intervention ( $B_{msr} = 1$ ), deceleration cut-off is prohibited.

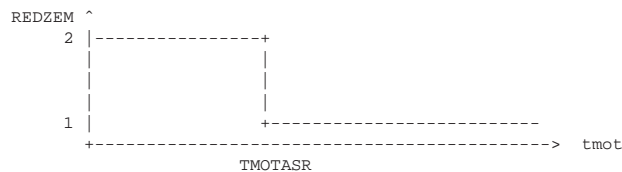
## APP MDRED 1.50 Application hint

Typical value:

$REDMX$  = No. of cylinders  
 $REDHYOC$  = 0.5 (for simultaneous injection and ignition interventions)  
 $REDHYUC$  = 0.6 (for simultaneous injection and ignition interventions)  
 $MDHYEZ$  = 5 Nm  
 $CREDSTU[0] = 0$  (cylinder masking during ASR not possible)

Characteristic  $REDZEM$  (typical value, see diagram below)

This characteristic determines the threshold between injection masking and ignition intervention. According to the engine temperature it can be used to program the reduction stage from which injection masking no longer results in overheating of the catalytic converter.



Example for the calculation of  $REDHYUC$ ,  $REDHYOC$  :

Target is a hysteresis of 0.1, at  $\Delta = (redzst - redsol(k-1)) \geq 0.5$  a higher stage should be selected. From the equations  
 $REDHYUC - REDHYOC = 0.1$   
 $\Delta = 1 - REDHYOC$

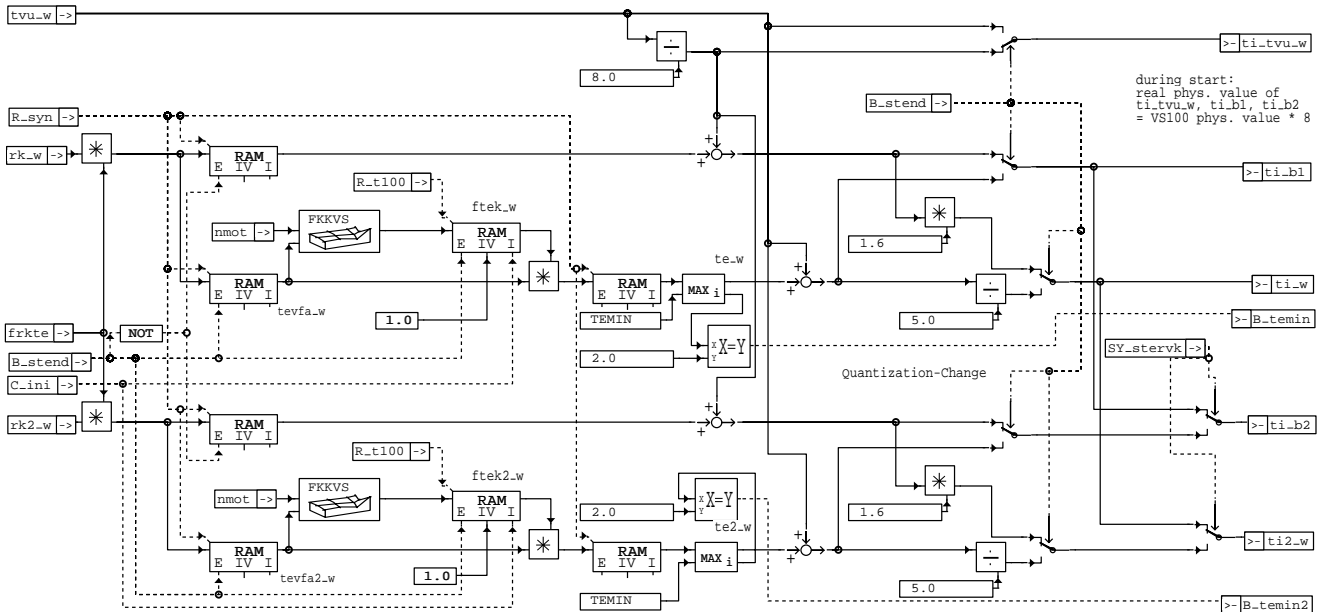
we get:

$REDHYOC = 0.5;$                        $REDHYUC = 0.6;$



## RKTI 1.60 Calculation of injection time $t_i$ from relative fuel mass $r_k$

### FDEF RKTI 1.60 Function definition



during start:  
real phys. value of  
 $t_{i, tvu_w}, t_{i, b1}, t_{i, b2}$   
= VS100 phys. value \* 8

rkti-rkti

### ABK RKTI 1.60 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FKKVS	NMOT	TEVFA2_W	KF	Factor to correct fuel delivery system
TEMIN			FW	minimum effective injection time
Variable	Source		Type	Description
B_STEND	BBSTT		EIN	condition end of start
B_TEMIN	RKTI		AUS	Condition: TEMIN-limitation active, bench 1
B_TEMIN2	RKTI		AUS	Condition: TEMIN-limitation active, bench 2
C_JNI	SWADAP		EIN	ECU-condition for intialisation
FRKTE			EIN	factor: conversion rel. fuel mass $r_k$ into effect. injection time $t_e$
NMOT	SWADAP		EIN	engine speed
RK2_W	MSF		EIN	relative fuel mass Bank2
RK_W	MSF		EIN	relative fuel mass
R_SYN	GGDPG		EIN	Synchro schedule
R_T100			EIN	Time schedule 100 ms
SY_STERVK	PROKON		EIN	system constant condition: stereo exhaust system upstream of cat
TI2_W	RKTI		AUS	injection time cylinder 2 (word)
TI_B1	RKTI		AUS	injection time for valves on bank1
TI_B2	RKTI		AUS	injection time for valves on Bank2
TI_TVU_W	RKTI		AUS	injection time correction as function of battery voltage ECU-quantization
TI_W	RKTI		AUS	injection time
TVU_W			EIN	supply of voltage correction

### FW RKTI 1.60 Fixed Values

Parameter	Value	Description
TEMIN		minimum effective injection time

### FB RKTI 1.60 Detailed description of function

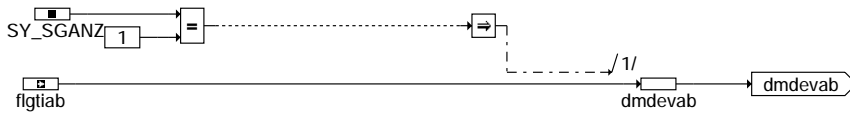
The function calculates the effective injection time  $t_{evfa}$  from the relative fuel mass  $r_{k,w}, r_{k2,w}$  and the factor  $frkte$ . At an ideal fuel system there will be Lambda combustion chamber 1.0 with  $t_i = t_{evfa} + t_{vu}$ . A real fuel system has to be corrected by the map  $FKKVS$  for pulsations in returnless fuel systems, nonlinearities of injection valves ... . The injection time  $t_{i,b1}, t_{i,b2}$  is calculated by addition of the battery voltage correction and the corrected effective injection time  $t_{e,w}, t_{e2,w}$ . The CIFI controls the relevant injection valves with times  $t_{i,b1}$  and  $t_{i,b2}$ .

In a single-bank system ( $SY\_stervk = false$ ) the injection time of Bank1 is passed as  $t_{i,b1}$  and  $t_{i,b2}$  to the CIFI.

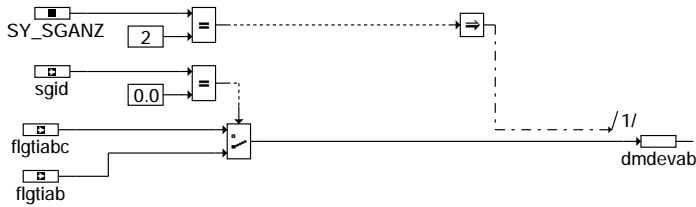
To implement the large injection times occurring during starting, the  $t_{i,b1}, t_{i,b2}, t_{i,tvu,w}$  quantisation is increased by a factor of 8 during starting, and the values range thus extended to 1677.696ms. The interface to cifi is so realized by a 16-Bit RAM, also during start.

$t_{i,w}$  is calculated selective to cylinder bank and shows the correct VS100-measured value during start and normal operating with constant resolution of 16 us.

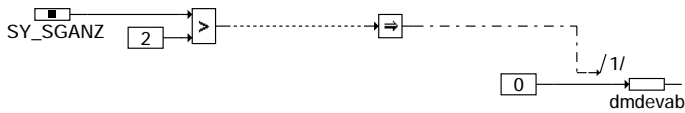




one ecu --> dmdevab = flgtiab

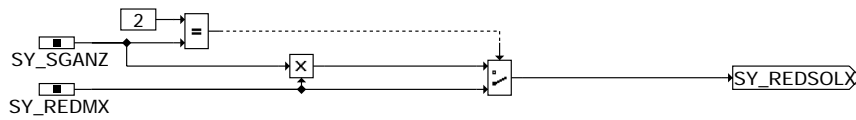


two ecu --> master ecu : dmdevab = flgtiabc  
 . slave ecu: if communication is ok dmdevab = flgtiab  
 . else dmdevab = 0



more than 2 ecu's: misfire detection is not implemented in this function

aevab-dmdevab

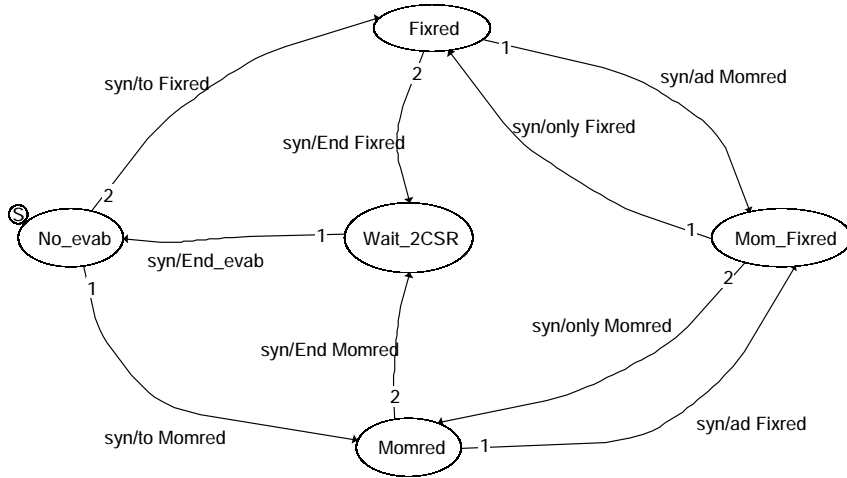


1 ecu: SY\_REDSOLX = SY\_REDMX --> 1 cylinder at 1 step of redsol  
 2 ecu: SY\_REDSOLX = 2 \* SY\_REDMX --> 1 cylinder at 1 step of redsol  
 3 ecu: SY\_REDSOLX = SY\_REDMX --> 3 cylinder at 1 step of redsol

aevab-redsolmx

aevab-dmdevab

aevab-redsolmx



stateevab: No\_evab = 0; Fixed = 1; Mom\_Fixed = 2; Momred = 3; Wait\_2CSR = 4;

**No\_evab:** no inj. valve cutoff active  
**Fixed:** inj. valve cutoff by fixed inj. valve active  
**Momred:** inj. valve cutoff begins with inj.valve = zzyl + SY\_ZYLZA/2 active  
**Momfixed:** combination of Fixed and Momred active  
**Wait\_2CSR:** waiting for 2 camshaft revolutions with activated injection, Lambda controller and misfire detection are deactivated

aevab-abm

state: Noevab

Cond No\_evab

specification of transitions from state No\_evab to other states

Act No\_evab

specification of actions in state No\_evab

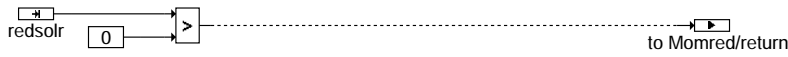
aevab-no-evab

aevab-abm

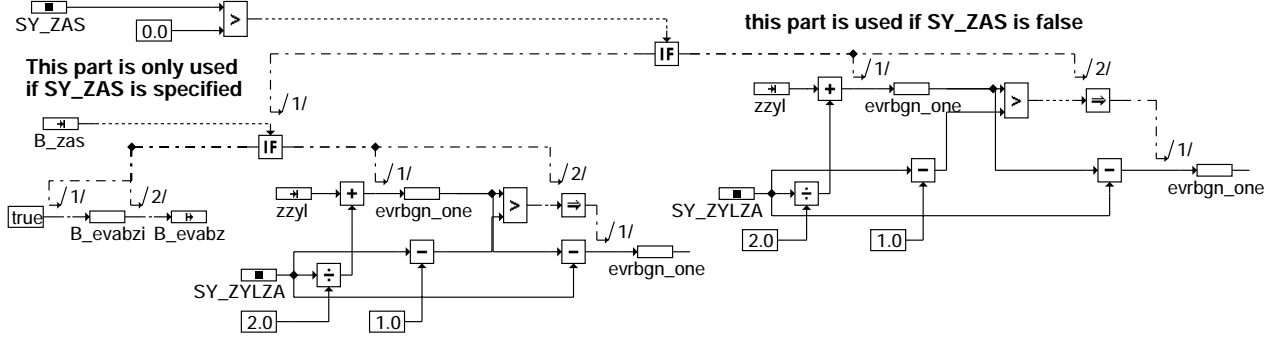
aevab-no-evab

state No\_evab

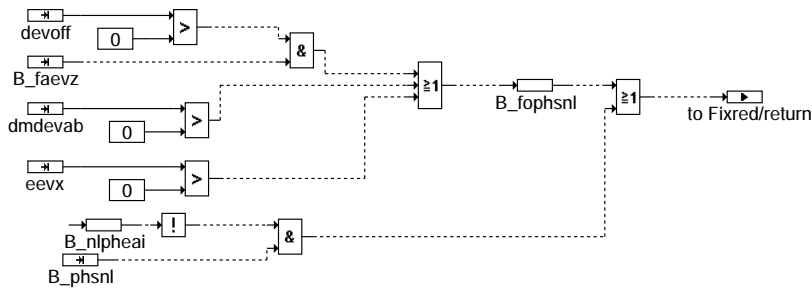
condition code for transition: to Momred



action code for transition: to Momred



condition code for transition: toFixed

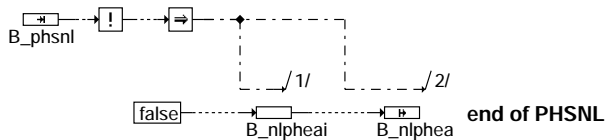


aevab-cond-no-evab

entry Code in state: No\_evab



action code in state: No\_evab



aevab-act-no-evab

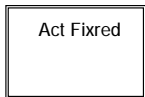
## state Fixed



specification of transitions from state Fixed to other states



specification of entry code into state Fixed

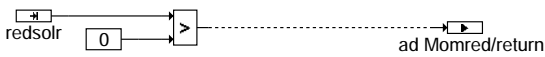


specification of action code in state Fixed

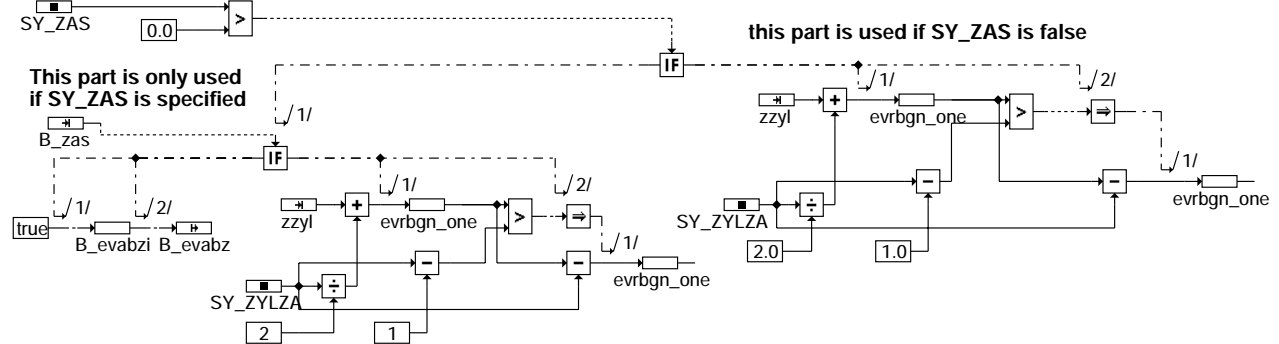
aevab-fixed

### state Fixed

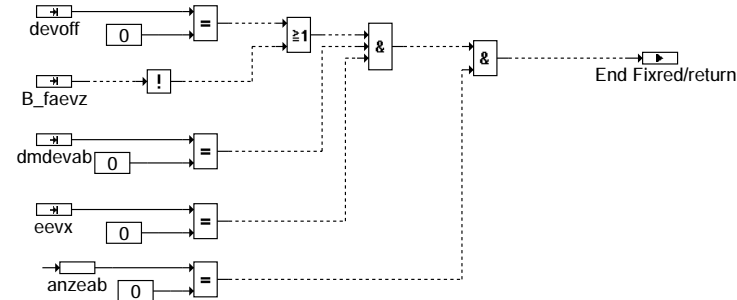
#### condition code for transition: ad Momred



#### action code in transition: ad Momred



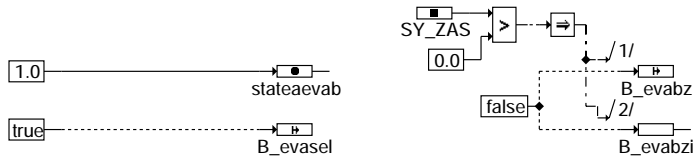
#### condition code for transition: End Fixed



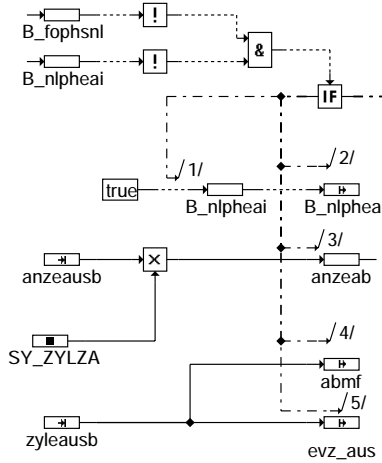
aevab-cond-fixed



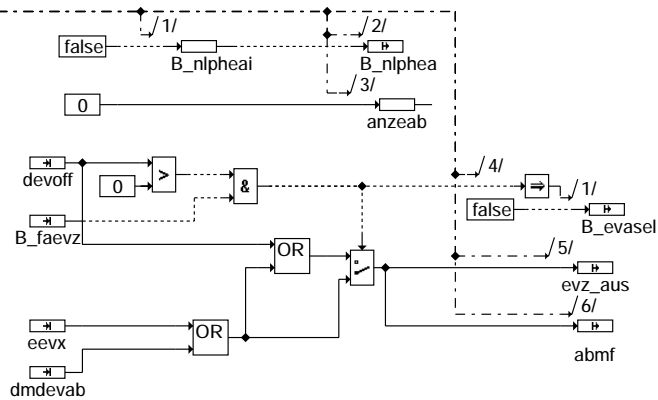
entry code in state: Fixed



begin Fixed activated by %NLPH

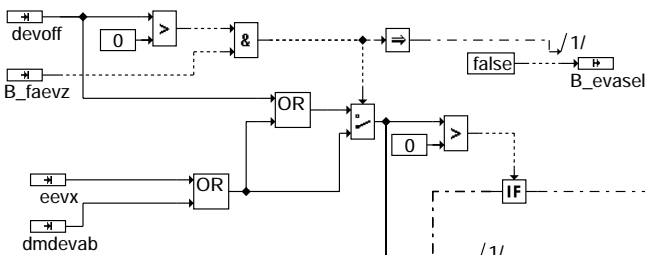
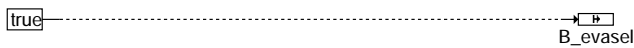


begin Fixed normally

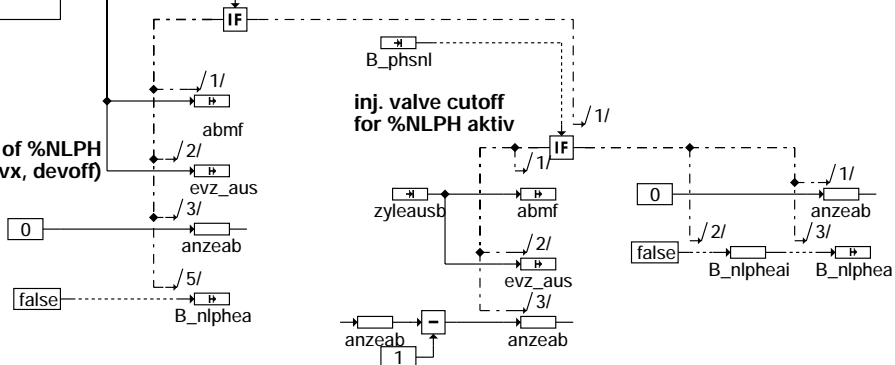


aevab-entr-fixed

action code in state: Fixed



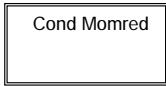
disable injection valve cutoff of %NLPH by other cutoff conditions (eevx, devoff)



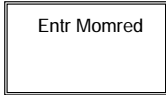
inj. valve cutoff for %NLPH aktiv

aevab-act-fixed

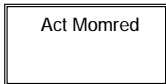
state Momred



specification of transitions from state Momred to other states



specification of entry code into state Momred



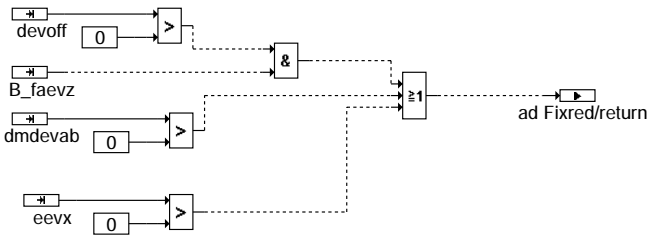
specification of action code in state Momred

aevab-momred

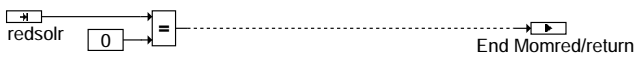
aevab-momred

state : Momred

condition code in transition: ad Fixed



condition code in transition: End Momred



aevab-cond-momred

aevab-cond-momred

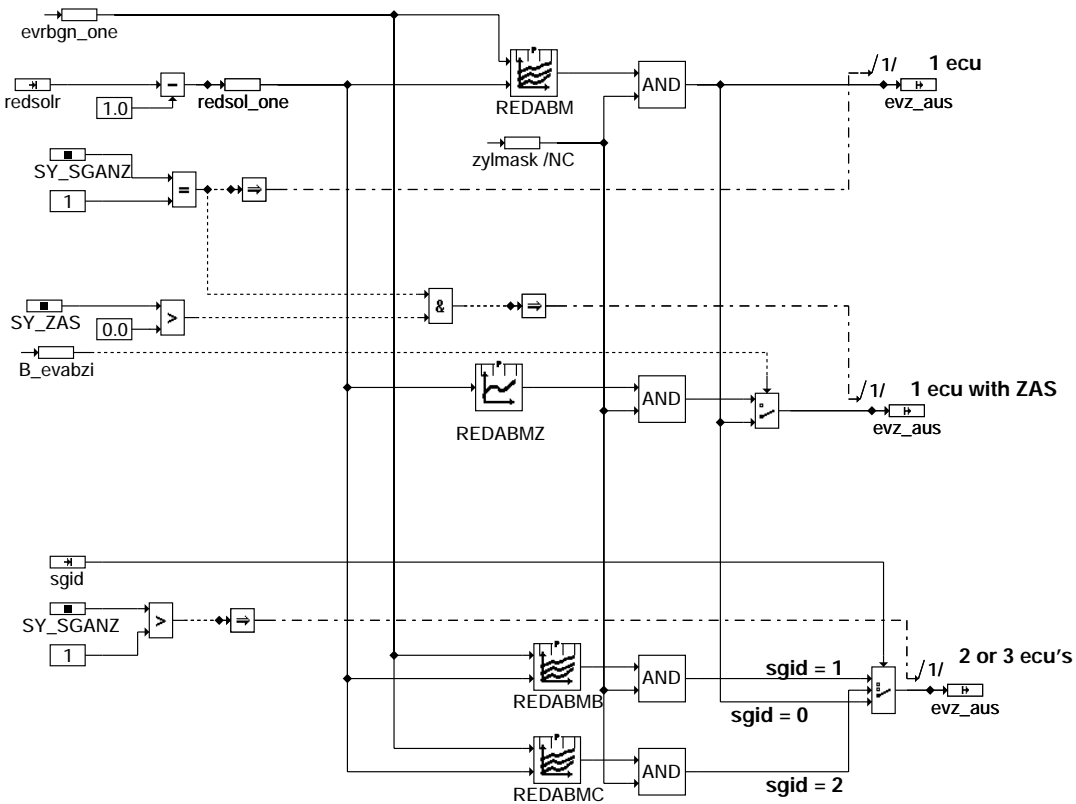
entry code into state: Momred



there is additional calculated complete action code of state Momred  
see in specification of action code in state Momred

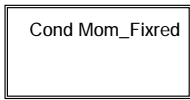
aevab-entr-momred

action code in state: Momred also calculated as entry code into state Momred



aevab-act-momred

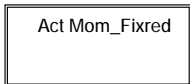
## state Mom\_Fixed



specifications of transitions from state Mom\_fixed to other states



specification of entry code into state Mom\_Fixed



specification of action code in state Mom\_Fixed

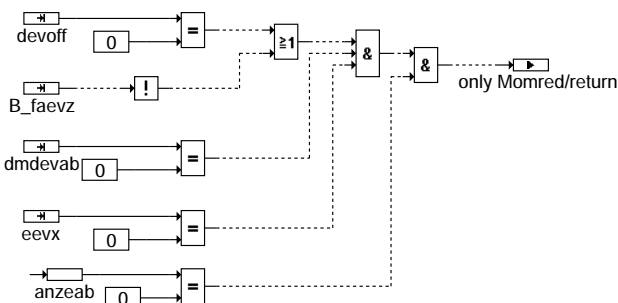
aevab-mom-fixed

## state Mom\_Fixed

### condition code in transition: only Fixed

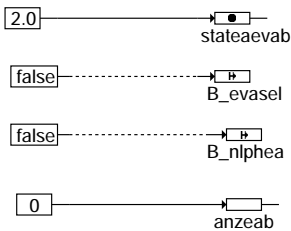


### condition code in transition : only Momred



aevab-cond-mom-fixed

### entry code in state: Mom\_Fixed



there is also calculated complete action code of state Mom\_Fixed see in specification of action code in state Mom\_Fixed

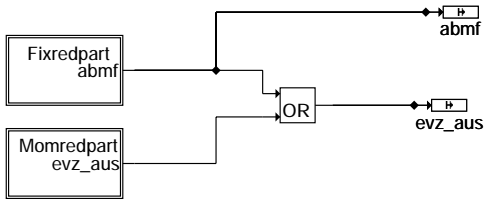
aevab-entr-mom-fixed

aevab-mom-fixed

aevab-cond-mom-fixed

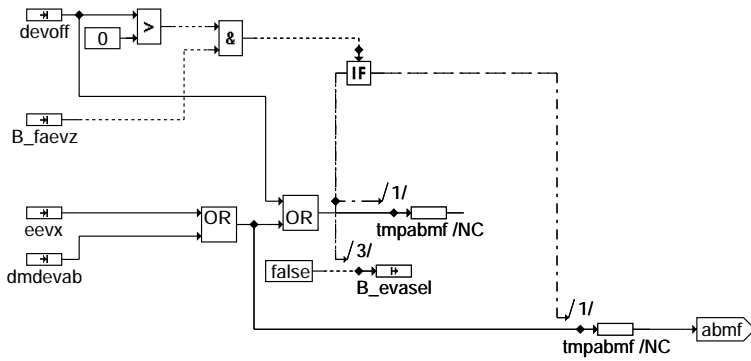
aevab-entr-mom-fixed

-----  
action code in state: Mom\_Fixed



aevab-act-mom-fixed

-----  
action code in state Mom\_Fixed: Fixredpart  
is also calculated as entry code into state Mom\_Fixed

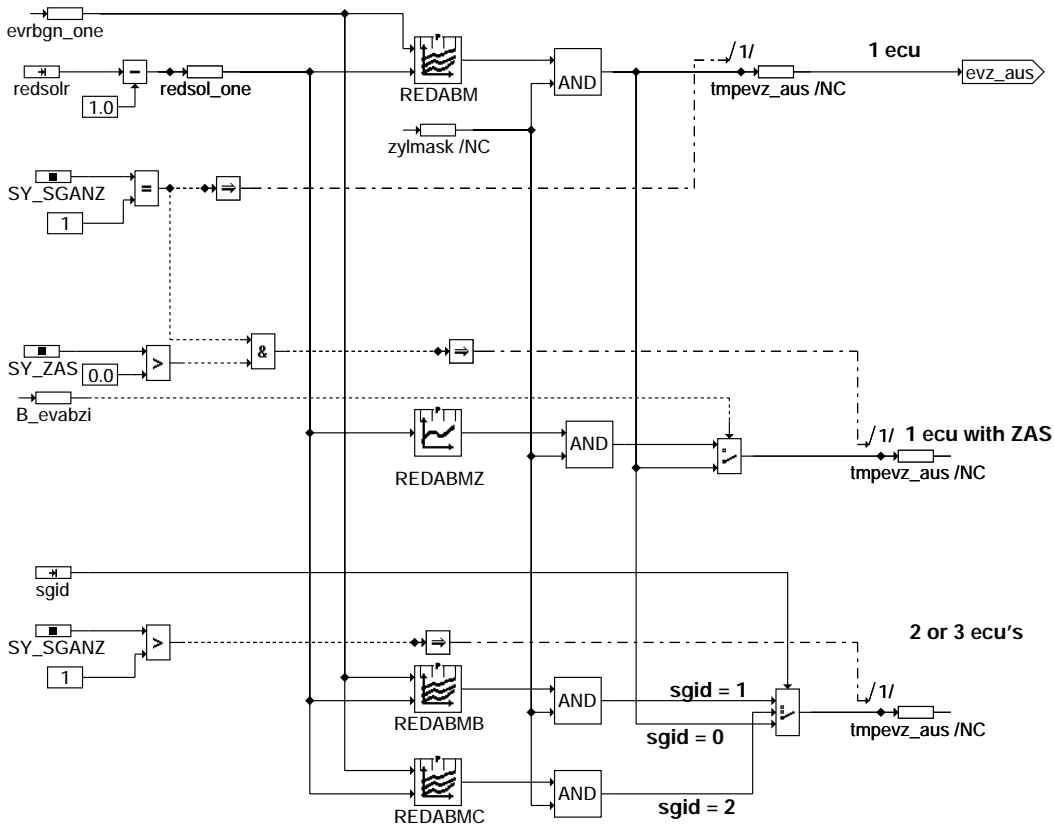


aevab-fixredpart

aevab-act-mom-fixed

aevab-fixredpart

action code in state Mom\_Fixed: Momredpart  
is also calculated in entry into state Mom\_Fixed



normal

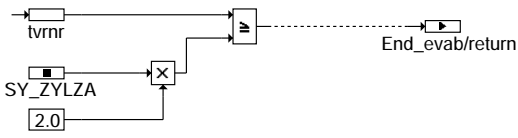
aevab-momredpart

aevab-momredpart

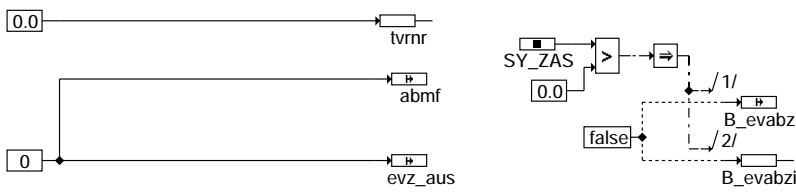


state: Wait\_2CSR

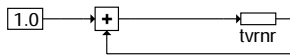
condition in transition: End\_evab



entry code into state: Wait\_2CSR



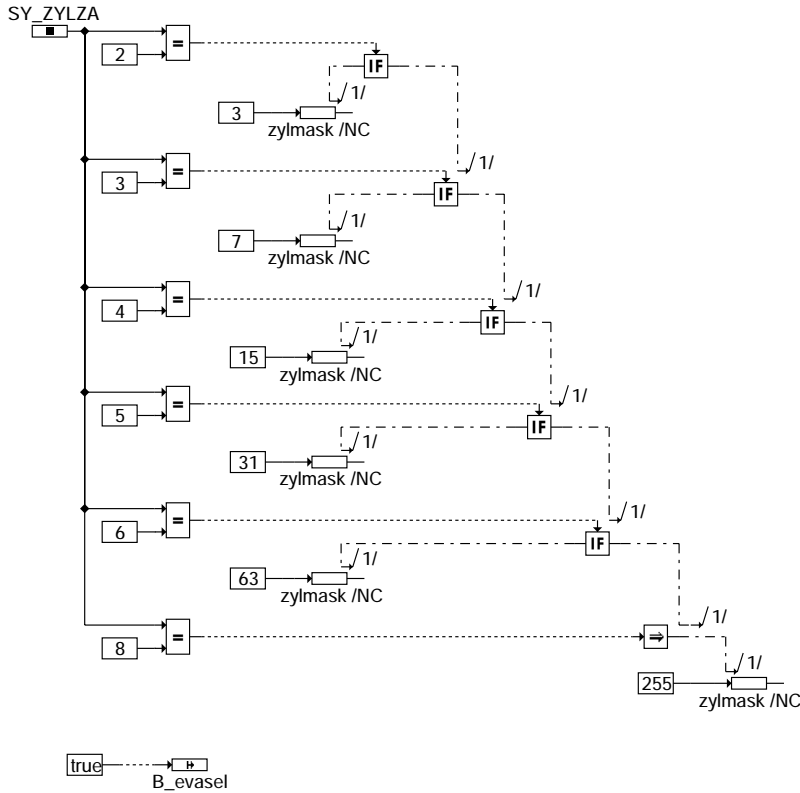
action code in state: Wait\_2CSR



aevab-wait-2csr

aevab-wait-2csr

### initialization



### aevab-initstatemachine

#### ABK AEVAB 6.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWEVAB			FW	codeword injection valve cutoff
REDABM	EVRBGN_ONE	REDSOL_ONE	KF	fuel cut-off table for torque reduction
REDABMB	EVRBGN_ONE	REDSOL_ONE	KF	fuel cut-off table for torque reduction slave1 or ecu B (SGB)
REDABMC	EVRBGN_ONE	REDSOL_ONE	KF	fuel cut-off table for torque reduction slave 2 or ecu C
REDABMZ	REDSOL_ONE		KL	fuel cut-off table for torque reduction during ZAS
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_REDMX			SYS (REF)	system constant: max. cylinder cutoff step
SY_SGANZ			SYS (REF)	system constant number engine control unit
SY_ZAS			SYS (REF)	system constant cylinder deactivation ZAS included
SY_ZYLZA			SYS (REF)	system constant number of cylinders

Variable	Source	Type	Description
ABMF	AEVAB	AUS	injection cut off pattern at fixed position
ANZEAB	AEVAB	LOK	Number of segments EV deactivation for emergency operation phase synchronisation
ANZEAUSB	NLPH	EIN	number of injections to fade out; limited between 4 and 7
B_DKUEVAB	AEVABU	EIN	Injection valve cut off by throttle blade uncorrect
B_EVABZ	AEVAB	AUS	Injection valve cutoff activated by ZAS
B_EVABZI	AEVAB	LOK	Injection valve cutoff activated by ZAS AEVAB internal
B_EVASEL	AEVAB	AUS	Status:all local injector relevant to DASE are switched on
B_FAEVZ		EIN	condition cylinder fade out by tester
B_FOPHSNL	AEVAB	LOK	injection valve cutoff by fixed pattern without .....
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)
B_NLPHEA	AEVAB	AUS	Injector deactivation for limp-home phase synchronization active
B_NLPHEAI	AEVAB	LOK	Ev Deactivation for emergency operation phase synchronization active AEVAB inter
B_PHSNL	NLPH	EIN	Condition phase search during phase sensor limp-home
B_ZAS		EIN	condition: beginning of cylinder shutdown
DEVOFF		EIN	injector fade out pattern at tester requirement
DFF_EV1	AEVAB	DOK	ECU int. fault path no.: injector 1
DFF_EV2	AEVAB	DOK	ECU int. fault path no.: injector 2
DFF_EV3	AEVAB	DOK	ECU int. fault path no.: injector 3
DFF_EV4	AEVAB	DOK	ECU int. fault path no.: injector 4
DFF_EV5	AEVAB	DOK	ECU int. fault path no.: injector 5
DFF_EV6	AEVAB	DOK	ECU int. fault path no.: injector 6
DFF_EV7	AEVAB	DOK	ECU int. fault path no.: injector 7
DFF_EV8	AEVAB	DOK	ECU int. fault path no.: injector 8
DMDEVAB	AEVAB	LOK	inject. valve cutoff pattern of misfire detection for the actual ecu
DUMMY	AEVAB	LOK	
EEVX	AEVAB	AUS	Injection valve Errorbyte





Variable	Source	Type	Description
EVRBGN_ONE	AEVAB	LOK	ev.nr. -1 at begin of cylinder cut-off for REDABM
EVZ_AUS	AEVAB	AUS	injection cut off pattern
E_EV1	DEVE	EIN	error flag: injection valve of cyl. 1
E_EV2	DEVE	EIN	error flag: injection valve of cyl. 2
E_EV3	DEVE	EIN	error flag: injection valve of cyl. 3
E_EV4	DEVE	EIN	error flag: injection valve of cyl. 4
E_EV5	DEVE	EIN	error flag: injection valve of cyl. 5
E_EV6	DEVE	EIN	error flag: injection valve of cyl. 6
E_EV7	DEVE	EIN	error flag: injection valve of cyl. 7
E_EV8	DEVE	EIN	error flag: injection valve of cyl. 8
FLGTIAB	DMDMIL	EIN	state flag ti turn-of by catalyst damaging misfiring rates
FLGTIABC		EIN	state flag ti turn-of by catalyst damaging misfiring rates CAN
REDSOL	SWADAP	EIN	calculated desired cylinder cut-off step
REDSOLR	AEVAB	AUS	realized cylinder cut-off step
REDSOL_ONE	AEVAB	LOK	calculated desired cylinder cut-off step -1 for REDABM
SGID		EIN	ECU-ID
STATEAEVAB	AEVAB	AUS	No. of the active state in AEVAB
TVRNR	AEVAB	LOK	delay time from end of fuel cut of to normal combustion
ZYLEAUSB	NLPH	EIN	cylinder to fade out; binary description
ZZYL	GGDPG	EIN	SW-cylinder counter

### FW AEVAB 6.20 Fixed Values

Parameter	Value	Description
CWEVAB		codeword injection valve cutoff

### FB AEVAB 6.20 Detailed description of function

The function Output Injection Valve cutoff, AEVAB, determines which of the injection valves must be disconnected. This decision is made according to the fix injection valve cutoff patterns established by the misfire detection, %DMD... (flgtiab, flgtiabc bei SY\_SGANZ =2), according to the disconnection of an injection valve commanded by the garage testing engineer (devoeff), or the injection valve final amplifier errors, or the injection valve cutoff pattern established by means of code word CWEVAB, or according to the engine torque reduction via the reduction ratio redsol.

The functioning is described by means of a state machine (see diagram aevab-abm).

The function is always in one of the states represented graphically during any logical decision. Any change-over from one state to another always follows the sense of the arrows drawn in the diagram/text.

Invariable (fix) injection valve cutoff patterns are such patterns where e determined individual injection valve must be disconnected, e.g. in the event of a final amplifier error or if the misfire detection has written an error into the RAM cell flgtiab.

In contrast to this, a reduction in the engine torque requires the next possible injection valve to be disconnected.

Any injection valve cutoff via invariable cutoff patterns is indicated in the RAM cell abmf. This cell is used to calculate the base reduction, redbas.

The I.V. cutoff pattern from the mapping REDABM (Master), or from REDABMB, REDABMC (Slave1, 2 in the event of more than 2 ecu's) is respectively indicated in RAM cell evz\_aus.

See also the application information in this FDEF.

In order to achieve the functionality of injection valve cutoff during a cylinder disconnection (SY\_ZAS = true), the same mechanism is used as for torque reduction. This is, redsol is used as an "interface" to pass over the number of injection valves which require to be disconnected. This reduction is used to address the characteristic line REDABMZ. In this case, the disconnection does not start out with any injection valve whatever but according to the invariable pattern from the characteristic curve REDABMZ. Therefore, evrbgn\_one is not used as RAM address.

The function AEVAB is also used to do the synchronizing during emergency phase loop search.

To do so, the injection valve zyleausb (Bit Nr. 0 = 1 corresponds to I.V.1, ...) is disconnected for anzeausb times. Now, the misfire detection determines the cylinder associated to this injection valve which equals to the synchronizing for ignition purposes.

Description of the individual states:

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Initialization: Condition Init

-----  
This condition is run once at S\_kl15 = 1 to initialize the RAM cells.

No injection valve disconnection active: Condition No\_evab

-----  
The function is in this state if no injection valve cutoff is requested.

Torque reduction: Condition Momred  
-----

If only the torque reduction is active, redsol establishes the number of injection valves to be disconnected.

On systems with two ecu's (2SG), there are different disconnection strategies:

disconnection only on the Master control device first; only when the Master is completely disconnected, the injection valve disconnection starts out on the Slave control device or disconnection, one by one, sequentially and mutually on Master and Slave, i.e. M,S,M,S,...

The injection valve disconnection starts out with the valve which has the number  $evrbgn\_one = zzylabm + SY\_ZYLZA/2$ ; counting mode of  $zzylabm$ : (0 ...  $SY\_ZYLZA-1$ ), counting mode of  $evrbgn\_one$ : ( $Ev1 = 0 \dots Ev8 = 7$ ).

Here,  $zzylabm$  represents the cylinder which is about to be fired. However, fuel has already been injected also into the successive cylinder which will be fired next because of the injection advance angle; this means the injection valve of the successive cylinder cannot be disconnected but only the next injection valve but one. This next-plus-one injection is determined by the offset  $SY\_ZYLZA/2$ . This rule is a compromise because the number of the next injection valve to be activated does not exist in the present CIFI version. In this way, an injection valve is disconnected after one camshaft revolution at the latest.

For 1 ecu (1SG) or for the Master (>1SG), the injection valve cutoff pattern  $evz\_aus$  is determined according to the invariable mapping REDABM using the value  $evrbgn\_one$  and value  $redsol\_one = redsol-1$ . The I.V. cutoff pattern for the 2SG Slave device is described by the mapping REDABMS.

If  $SY\_GRDWOF = 0$ , the variable  $zzylabm$  is generated from  $zzy1$ , else from  $zzy1bi$ .

In the event of a cylinder disconnection ( $SY\_ZAS = true$ ),  $evrbgn\_one$  is not considered because the injection valves to be disconnected follow an invariable association scheme. The disconnection patterns are contained in the characteristic curve REDABMZ.  $B\_evabz = true$  indicates that an injection valve disconnection has been activated via  $B\_zas$ .

During DV substitution operation ( $B\_dknolu$ ,  $B\_dkpu$ ), a complete injection valve disconnection is requested by  $redsol = SY\_REDMX$  above the engine speed threshold  $NMXSKA$ . If  $B\_dkuevab = true$ , the above request is fed back to the torque calculation via the regular injection valve disconnection by setting  $redsolr = SY\_REDMX$ .

Disconnection by means of invariable injection valve cutoff patterns: Condition Fixed  
-----

The invariable injection valve cutoff patterns  $flgtiab$ ,  $devoff$ ,  $eevx$  are linked by a logical OR operation and are available for the disconnection of the injection valves in the form of the bit pattern  $abmf$ .

On concepts for 2 control devices (2SG),  $abmf$  contains the injection valves which are respectively to be disconnected on Master and Slave.

Since the injection valves are only disconnected according to invariable cutoff patterns in this condition,  $evz\_aus$  is set =  $abmf$ .

The condition Fixed is also used in the exceptional case of synchronizing during phase generator emergency operation, i.e. in the event that the injection valve indicated by  $zyleausb$  is disconnected for  $anzeausb$  injection cycles while  $B\_phsnl = true$ ; Fixed is however only used in these conditions if no other invariable-pattern disconnection is active.

While the synchrony is being searched, the bit  $B\_nlphea$  is = true. This bit is usually reset to the state  $No\_evab$  when the request condition,  $B\_nlph$ , assumes the value false. If another invariable-pattern disconnection or a torque reduction is requested by  $redsol$  during phase synchronizing, the invariable-pattern I.V. disconnection used to search the phase synchrony is terminated and  $B\_nlphea$  is set to the value false. The search for phase synchrony remains locked until  $B\_nlphea = false$  is detected in condition  $No\_evab$ .

Disconnection by means of invariable disconnection patterns and torque reduction: condition Mom.Fixed  
-----

The I.V. cutoff pattern  $evz\_aus$  which is to be executed is formed by means of a logical OR operation from the invariable cutoff patterns  $devoff$ ,  $flgtiab$ ,  $eevx$  and the cutoff pattern of the torque reduction, REDABM or REDABMS.

$abmf = devoff \text{ OR } flgtiab \text{ OR } ee vx$

$evz\_aus = abmf \text{ OR } REDABM \text{ (or respectively REDABMS)}$

In the event that the disconnection is induced by a torque reduction, the explanation given for condition Momred applies.

Condition Wait\_2CSR:  
-----

This condition causes a delay of two camshaft revolutions (2CSR) before via  $B\_evasel = true$  unlocks the misfire detection and  $B\_evloc = true$  causes, for example, the  $labmda$  control to be released again.



The cutoff patterns evz\_austot which at the end must really be carried out via function the AEVABZK is analyzed in function BGEVAB:

Here, the bank where one or more injection valves are disconnected is determined.

B\_bevab = true: at least 1 I.V. on Bank1 is disconnected.

B\_bevab2 = true: at least 1 I.V. on Bank2 is disconnected.

The disconnection of any injection valve in general and of any final amplifier error is indicated by B\_evloc.

B\_evloc = false means: an injection valve is disconnected or a final amplifier error is present.

The function AEVAB locks the misfire recognition by setting B\_evasel = false if either a change-over towards condition Momevab or towards condition Fest\_evab occurs, or if a testing engineer intervention is active via devoff.

Request for disconnection	cutoff conditions	cutoff information	Misfire recognition
Tester intervention	devoff > 0 & B_faevz = TRUE	-> B_evloc = false	-> B_evasel = false Misfire recognition locked
Torque reduction	redsol > 0	-> B_evloc = false	-> B_evasel = false Misfire recognition locked
Final amplifier error diagnosis	eevx > 0	-> B_evloc = false	-> B_evasel = true Misfire recognition active
Misfire recognition	flgtiab > 0	-> B_evloc = false	-> B_evasel = true Misfire recognition active, Search for further errors
Cylinder disconnection	B_zas	-> B_evloc = false	-> B_evasel = false Misfire recognition locked

During cylinder disconnection (ZAS, disconnection of a bank), this functionality is implemented by means of a torque reduction (redsol intervention).

However, the injection valve disconnection pattern from characteristic curve REDABMZ is used if B\_zas =true since in this case, the first disconnected injection valve is a determined individual valve. All torque interventions use the I.V. disconnection pattern of this characteristic curve until the torque reduction is reset (redsol = 0).

Any I.V. disconnection during ZAS (cylinder disconnection) is indicated via B\_evabz.

During application on the test bench, it is often necessary to operate the engine without injection. Code word CWEVAB allows to disconnect the individual injection valves. Here, Bit 0 corresponds to I.V.1 (Ev1). By default, all injection valves are active: CWEVAB = 0

Description of the change-over conditions of function AEVAB:

```

-----
Condition: Init -----
Transition:-----
  End Init:      ---
                ---
                C_ini = FALSE
                ---
                ---                               -- End of Initialization
Condition: No_evab -----
Transition:-----
  to Fixred:
                ---
                ((devoff >0) and (B_faevz = TRUE)) or (flgtiab > 0 ) or (eevx > 0) or ((B_nlpheai = FALSE)&B_phsnl=TRUE)
                ---
                ---                               -- Start of an I.V. cutoff by means of an
                ---                               invariable I.V. cutoff pattern by misfire
                ---                               detection flgtiab, I.V. final amplifier error
                ---                               ee vx, Tester request
                ---                               devoff or phase generator emergency operation.
Transition:-----
  to Momred:
                ---
                redsolr > 0
                ---
                ---                               -- --- Start of an I.V. cutoff by torque reduction
                ---                               --- via the reduction ratio redsol
Condition: Momred -----
Transition:-----
  ad Fixred:
                ---
                ((devoff >0) and (B_faevz = TRUE)) or (flgtiab > 0) or (eevx > 0)
                ---
                ---                               ----- Tester, I.V. final amplifier diagnosis or
                ---                               misfire detection request the disconnection of
                ---                               further I.V.'s in addition to the torque reduction
Transition:-----
  End Momred:  ---
                (redsolr = 0 )
                ---
                ---                               -- --- From here on, no more I.V. cutoff
                ---                               --- is commanded via the torque reduction
Condition: Fixred -----
Transition:-----
  ad Momred:  ---
                redsolr > 0
                ---
                ---                               -- --- Torque reduction requests further
                ---                               --- I.V. cutoff in addition to the I.V.
                ---                               disconnections commanded by misfire recognition,
                ---                               I.V. final amplifier diagnosis or tester
Transition:-----
  End Fixred:
                ---
                ((devoff=0) and (B_faevz = FALSE)) and (flgtiab = 0) and (eevx = 0) and (anzeab = 0)
                ---
                ---                               -- --- From here on, no request for I.V. disconnection
                ---                               by Tester, I.V. diagnosis, detection or phase
                ---                               generator emergency operation is present any more
    
```



```

Condition: Mom_Fixed -----
Transition:-----
  Only Momred:                --- End of the disconnection
                               --- by misfire detection, tester request or
                               --- phase generator emergency operation.

                               ((devoff=0) and (B.faezv = FALSE)) and (flgtiab = 0) and (eevx = 0) and (anzeab = 0)
                               ---
Transition:-----
  Only Fixed:                 --- End of the I.V. cutoff by
                               --- Torque reduction

                               redsolr = 0
                               ---
Condition: Wait_2CSR -----
Transition:-----
  End evab:                   ---
                               tvrnr >= (2*SY_ZYLZA)                -- --- End of the I.V. cutoff, each cylinder has
                               --- been fired once, i.e. normal operation is.
                               --- ensured
    
```

### APP AEVAB 6.20 Application hint

System constant values for the functionality injection valve cutoff  
Definition in %PROKON

=====

```

SY_SGANZ:      Number of control devices (SG) used in the project
                1: 1SG (one device used)
                2: 2SG (two devices used)
                3: 3SG (three devices used)

SY_ZZBANK:     Injection valves associated to the exhaust gas bank of the Master control device (SGA)

SY_ZZBANKB:    Injection valves associated to the exhaust gas bank of the Slave1 control device (SGB)

SY_ZZBANKC:    Injection valves associated to the exhaust gas bank of the Slave2 control device (SGC)
    
```

Meaning of SY\_ZZBANKx: (applies to all above system constant values)

```

Bit position    7 6 5 4 3 2 1 0
Inj.Valve Nr.  8 7 6 5 4 3 2 1 Counted on the Engine: 1 ... SY_ZYLZA
Association    x x x x x 1 0 0: I.V. belongs to exhaust gas bank 1 of control device x
                1: I.V. belongs to exhaust gas bank 2 of control device x
    
```

```

SY_ZAS:        Project implements cylinder disconnection

SY_EGAS:       Project with EGAS system

SY_ZYLZA:      Number of cylinders of one control device with respect to injection and ignition

SY_REDMX:      Number of cylinders of one control device with respect to injection and ignition
    
```

Meaning of other input values:

Only present if SY\_2SG = true

Identification code for Master/Slave : is specified in %SGA

```

B_masterhw = true    --> control device (SG) is MasterSG

B_masterhw = false   --> control device (SG) is SlaveSG; whether it is Slave1 or Slave2 is determined by sgid

sgid:               0: MasterSG or SGA
                    1: Slave1 control device, called SGB in the further text
                    2: Slave2 control device, called SGC in the further text
    
```

Only present during cylinder disconnection (SY\_ZAS = true):

```

B_zas = true        -> Request for disconnection of the cylinders which are governed by ZAS
    
```



## Possible functional features via injection valve disconnection:

=====

## Projects with one control device (SG):

-----

SY\_SGANZ = 1 ( 1 control device used)

redsol 0 ... SY\_REDMX --> reduction ratio = 1 Cylinder / SG --> 1 cyl. per reduction stage

## Functional features:

Cylinder disconnection ZAS Input: B\_zas,  
cutoff pattern: evz\_aus = f(REDABMZ)

n

Misfire detection DMD\* Input: flgtiab  
cutoff pattern: evz\_aus = f(flgtiab)

Torque reduction MDRED Input: redsol  
cutoff pattern: evz\_aus = f(REDABM)

Phase generator emergency operation NLPH Input: B\_phsnl, zyleausb, anzeausb  
cutoff pattern: evz\_aus = f(zyleausb)

I.V. disconnection by testing engineer Input: B\_faevz, devoff  
cutoff pattern: evz\_aus = f(devoff)

I.V. disconnection by VS100 Code word CWEVAB Bit 0 = Ev1 .... Default value = 0

## Projects with two control devices (2SG):

-----

SY\_SGANZ = 2 ( 2 control devices used, Master/SGA, Slave/SGB)

redsol 0 ... SY\_SGNR \* SY\_REDMX --> Reduction ratio = 0.5 cylinders / per SG --> 1 cyl. / reduction stage

## Functional features:

Cylinder disconnection ZAS not implemented

Misfire recognition DMD\* Input: flgtiab, flgtiabc  
Program runs on SGB cutoff pattern: evz\_aus = f(flgtiabc) for Master/ SGA  
evz\_aus = f(flgtiab) for Slave/SGB

Torque reduction MDRED Input: redsol  
cutoff pattern: evz\_aus = f(REDABM) for Master/SGA  
evz\_aus = f(REDABMB) for Slave/SGB

Phase generator emergency operation NLPH not implemented

I.V. cutoff by testing engineer Input: B\_faevz, devoff  
cutoff pattern: evz\_aus = f(devoff)

I.V. cutoff by VS100 Code word CWEVAB Bit 0 = Ev1 .... Default value = 0



Projects with three control devices (3SG):  
-----

SY\_SGANZ = 3 ( 3 control devices used)

redsol 0 ... SY\_REDMX --> reduction level = 1 cylinder per SG --> 3 cyl. per reduction stage

Functional features:

Cylinder disconnection ZAS not implemented

Misfire detection DMD\* Input: ?? Method not yet specified  
cutoff pattern: no effect

Torque reduction MDRED Input: redsol  
cutoff pattern: evz\_aus = f(REDABM) for Master/SGA  
evz\_aus = f(REDABMB) for Slavel/SGB  
evz\_aus = f(REDABMC) for Slave2/SGC

Phase generator emergency operation NLPH not implemented

I.V. cutoff by testing engineer Input: B\_faevz, devoff  
cutoff pattern: evz\_aus = f(devoff)

I.V. cutoff by VS100 Code word CWEVAB Bit 0 = Evl .... Default value = 0

Example for the configuration of a 8-cylinder engine: the engine can be operated using one control device (1SG) or two control devices (2SG)

1SG:	2SG:
SY_SGANZ = 1	SY_SGANZ = 2
SY_ZYLZA = 8	SY_ZYLZA = 4
sgid not present	sgid = 1/0
SY_REDMX = 8	SY_REDMX = 4

The cutoff pattern itself is memorized in the constant mapping REDABM = f(evrbgn\_one, redsol\_one) or in REDABMB, REDABMC for the Slave control device (SGB). The access to this mapping depends on the cylinder which is about to be fired, zzylabm, and the torque reduction ratio redsol requested by the torque reduction.

The first injection valve to be disconnected is determined by evrbgn\_one = zzylabm + SY\_ZYLZA/2 because the injection valves which follow next after the cylinder which is about to be fired have already completed their injection cycle and a disconnection is no longer possible.

The characteristic curve REDABM starts out with index 0. Therefore, a conversion is carried out for any indexed access:  
redsol\_one = redsol - 1 Only these two variables are present in the system.



The associations between injection valves and ignition order, injection order, the bank association of the injection valves and the association between the disconnection pattern REDABM and the I.V.s are described in the following section.

Example 8-cylinder engine 1SG (one control device):

```

=====
                Axially-mounted front engine cylinder scheme
                ^
                | Vehicle front side
    Bank2      5      1
                6      2      Bank1
                7      3
                8      4
                XX
                Clutch side

Cylinder Nr.      1 5 4 8 6 3 7 2 <--- Firing order in direction of the arrow,
                                cylinder nr. according to above cylinder scheme
I.V. Nr.          8 7 6 5 4 3 2 1 <--- Injection order in direction of the arrow, user counting scheme 1 ... SY_ZYLZA
I.V. Nr.          7 6 5 4 3 2 1 0 <--- Injection order in direction of the arrow,
                                SG internal counting mode 0 ... SY_ZYLZA-1 corresponds to counting mode of zzyl
SY_ZZBANK = zzbek = 90 dec
                                0 1 0 1 1 0 1 0   Cylinder-Bank association Bit = false (0): I.V. belongs to Bank1,
                                | | | | | | | |   Bit = true (1): I.V. belongs to Bank 2
REDABM-Bit position
cutoff pattern REDABM      7 6 5 4 3 2 1 0
    redsol_one:            0      0 0 0 0 0 0 0 1   evrbgn_one: 0
                            | 1      0 0 0 1 0 0 0 1   01 dec redsol_one = redsol -1, if redsol > 0
                            | 2      0 0 0 1 0 1 0 1   17
                            | 3      0 1 0 1 0 1 0 1   21
                            | 4      0 1 0 1 0 1 1 1   85
                            | 5      0 1 1 1 0 1 1 1   87
                            | 6      0 1 1 1 1 1 1 1   119
                            v 7      0 1 1 1 1 1 1 1   127
                                1 1 1 1 1 1 1 1   255
    
```

The pattern with evrbgn\_one = 1 is generated by a logical shift to the left side by one position, i.e. any "1" which goes out of the matrix on the left side is inserted on the left side.

```

                                evrbgn_one: 1
    redsol_one:            0      0 0 0 0 0 0 1 0   02 dec
                            1      0 0 1 0 0 0 1 0   34
                            2      0 0 1 0 1 0 1 0   42
                            3      1 0 1 0 1 0 1 0   170
                            4      1 0 1 0 1 0 1 1   171
                            5      1 0 1 1 1 0 1 1   187
                            6      1 0 1 1 1 1 1 1   191
                            7      1 1 1 1 1 1 1 1   255
    
```

Rotation/shifting of the respective preceding pattern

evrbgn\_one = SY\_ZYLZA-1 last pattern

Here, another time an explanation of the way how injection valves and cylinders are counted:

Injection valve 1 (Ev1) according to the user counting mode is identical to injection valve 0 (Ev0) according to the internal control device counting mode. This injection valve is opened for the time  $t_{i.ev0}$  and provides the fuel mass required for cylinder  $zzyl = 0$  according to the SG-internal counting mode, i.e. cylinder 2 according to the firing order of the engine from the above example.

Injection valve 1 and the cylinder nr. 2 according to the firing order are associated one to another by the wiring (harness). This injection valve 1 is disconnected if the value of REDABM-Bit0 or correspondingly evz\_aus-Bit0 has the value 1.



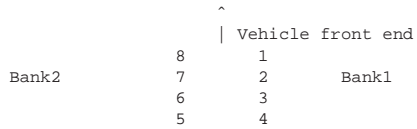




Example 8-cylinder engine with one control device (1SG):  
=====

Disconnection of the cylinders mutually on Bank1 and on Bank2:

Axially-mounted rear engine cylinder scheme



Clutch side

	Slave (SGB)	Master (SGA)	
Cylinder Nr.	6 2 8 4	7 3 5 1 <---	Firing order in direction of the arrow, cylinder nr. according to engine counting scheme
I.V..Nr.	8 7 6 5	4 3 2 1 <---	Inj. order in direction of the arrow, counting mode 1 ... SY_ZYLZA for the entire engine
I.V..Nr.	4 3 2 1	4 3 2 1 <---	Injection order in direction of the arrow, counting mode 1 ... SY_ZYLZA Slave/Master
I.V..Nr.	3 2 1 0	3 2 1 0 <---	Injection mode in direction of the arrow, SG internal counting mode 0 ... SY_ZYLZA-1
			which corresponds to the zysl counting mode Slave/Master
SY_ZZBANKB	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	SY_ZZBANK The cylinder association is always stated with respect to Bank1: Bit = false (0) means the injection valve belongs to Bank1 Bit = true (1) means the injection valve belongs to Bank 2

REDABM-Bit pos. | | | | | | | | 7 6 5 4 3 2 1 0

REDABMB-Bit pos. 7 6 5 4 3 2 1 0

	REDABMB:	REDABM:	evrbgn.one: 0
redsol.one: 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1	redsol.one = redsol -1 if redsol > 0
1	0 0 0 0 0 0 0 1	0 0 0 0 0 0 0 1	
2	0 0 0 0 0 0 0 1	0 0 0 0 0 0 1 1	
3	0 0 0 0 0 0 1 1	0 0 0 0 0 0 1 1	
4	0 0 0 0 0 0 1 1	0 0 0 0 0 1 1 1	
5	0 0 0 0 0 1 1 1	0 0 0 0 0 1 1 1	
6	0 0 0 0 0 1 1 1	0 0 0 0 1 1 1 1	
7	0 0 0 0 1 1 1 1	0 0 0 0 1 1 1 1	
	\-----/	\-----/	
	V	V	
	Slave (SGB)	Master (SGA)	

Rotation/shifting of the respective preceding pattern: see above in the section on 1SG concept

Cylinder disconnection (ZAS):  
-----

To the characteristic curve REDABMZ (= injection valve cutoff pattern) applies the same as applies to REDABM. However, the parameter evrbgn.one does not exist.

For redsol.one = 0 to SY\_ZYLZA/2, the I.V. cutoff pattern must be drawn in for the ZAS cylinders. For higher redsol.one values, more and more injection valves are disconnected.

The cutoff pattern which is finally applied is generated by means of a logical OR operation from the invariable cutoff patterns and the I.V. cutoff patterns selected by the torque reduction (REDABM, REDABMB, REDABMC, REDABMZ).

Invariable cutoff patterns: eevx final amplifier error  
flgtiab Cylinders with irregular misfire which is detected by the function misfire detection  
devoeff injection valves to be disconnected by the tester

Entire invariable cutoff pattern:  
abmf = eevx OR flgtiab OR devoeff

Entire injection valve cutoff pattern:

If no cylinder disconnection is active:  
evz\_aus = abmf OR [REDABM ( evr\_bgn.one, redsol.one)] If 2 control devices are used (2SG), the mapping REDABMB or REDABMC is used on the Slave side instead of REDABM.

If a cylinder disconnection is active:  
evz\_aus = abmf OR [REDABMZ (redsol.one)] Not possible if two control devices are used (2SG)

On EGAS systems, it is the function AEVABZK which establishes whether an injection valve cutoff has been caused by the torque reduction (redsol) or by interventions of a monitoring function; on systems without EGAS, only the torque reduction is active. If a torque intervention is active, evz\_austot = evz\_aus; during interventions by monitoring functions, evz\_austot = 255. During torque interventions, only those bits in evz\_aus are set which correspond to physically installed injection valves. This means that evz\_aus is always < 255 on control devices where SY\_ZYLZA < 8. This allows to distinguish whether a torque intervention or a monitoring is active when evz\_aus is measured.

The calculation of the actually performed reduction (redist = number of the disconnected I.V.'s in evz\_austot, or redbas = number of the disconnected I.V.'s in abmf) is performed in function BGEVAB. The physical injection valve disconnection is governed by function %ACIFI. If a disconnection is performed, the corresponding final amplifier does not receive any input although the associated ti\_evx is > 0.

There are different criteria for the definition of the injection valve cutoff pattern:

- on projects with one control device (1SG), the injection valves are disconnected mutually: first one valve on one bank, then a second on the other bank, and so on according to the increase in the reduction ratio;
- it is possible to implement the disconnection either in a way that always the respective next injection valve according to the firing order is disconnected, or in a way that an injection valve with a constant "firing order distance" with respect to the actually fired cylinder is disconnected which reduces the engine roughness if two successive injection valves are disconnected.
- on projects with two control devices (2SG), first all injection valves on one engine side (Master side) are disconnected and only as the reduction continues, the valves on the other side are disconnected.

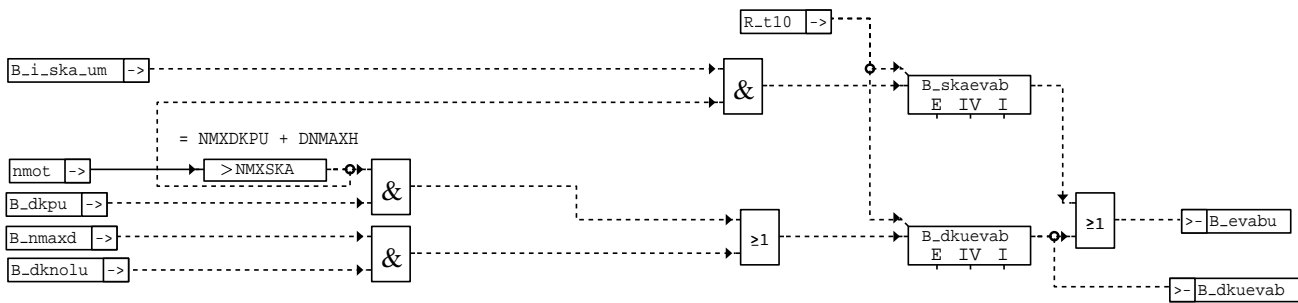
In normal conditions, the cutoff patterns which are shifted via evrbgn.one are generated by rotating/shifting the matrix of evrbn.one - 1 towards the left side.

The beginning of the I.V. cutoff is synchronized to the cylinder which is about to be fired when the function is activated, i.e. the first injection valve would be disconnected no sooner than 2 camshaft revolutions later.

If the invariable offset SY\_ZYLZA/2 is applied, this beginning can be shifted to an earlier point of time so that the first injection valve is disconnected after 1 camshaft revolution.

## AEVABU 1.10 Output injection-valve cut-off by monitoring functions (EGAS)

### FDEF AEVABU 1.10 Function definition



aevabu-aevabu

### ABK AEVABU 1.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
NMXSKA			FW	Maximum permitted engine speed in case of unknown throttle position -> cut off
Variable	Source		Type	Description
B_DKNOLU	SWADAP		EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP		EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_DKUEVAB	AEVABU		AUS	Injection valve cut off by throttle blade uncorrect
B_EVABU	AEVABU		AUS	Fuel cutoff by .....
B_I_SKA_UM	UFREAC		EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_NMAXD			EIN	condition rpm limiting with injection masking
B_SKAEVAB	AEVABU		LOK	Fuel cutoff by safety fuel shut-down
NMOT	SWADAP		EIN	engine speed
R_T10			EIN	Time schedule 10 ms

### FW AEVABU 1.10 Fixed Values

Parameter	Value	Description
NMXSKA		Maximum permitted engine speed in case of unknown throttle position -> cut off

### FB AEVABU 1.10 Detailed description of function

This function realizes the interventions of the monitoring functions for the injection valve shut-off. Via the condition B\_i\_ska\_um a so-called safety fuel deactivation is requested, when the engine speed is > NMXSKA. For non-plausible poti values of the EGAS-actuator and engine speed > NMXSKA, a complete injection valve shut-off is requested. If the EGAS-actuator is at zero current, a complete injection valve shut-off is requested at B\_nmaxd. The injection valve shut-off pattern for a complete fuel shut-off is realized in the function AEVABZK in the RAM-cell evz\_austot.

### APP AEVABU 1.10 Application hint

NMXSKA = NMXDKPU + DNMAXH

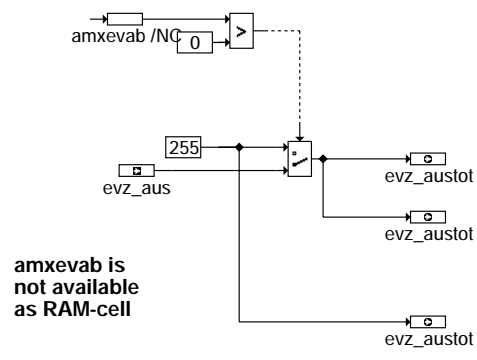
## AEVABZK 1.20 Output injection-valve cut-off %MDRED + total shutdown by monitoring functions

### FDEF AEVABZK 1.20 Function definition

#### AEVABZK 1.20

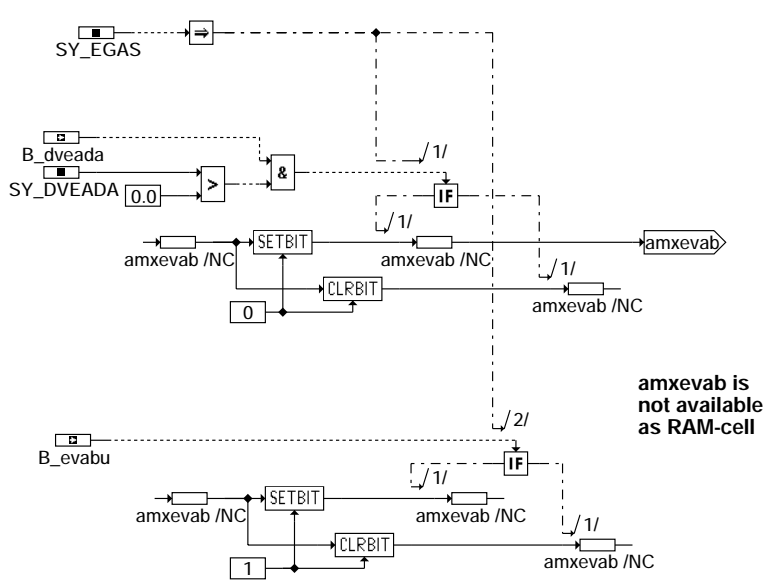
injection valve cutoff part	single parts to cutoff injection valves
injection valve cutoff part by throttle blade actuator	<div style="border: 1px solid black; padding: 2px;">THROTL_ACT</div> amxeval
injection valve cutoff part by two or more ECUs	<div style="border: 1px solid black; padding: 2px;">TWO_ECUs</div> amxeval
injection valve cutoff part by function KOEVAB	<div style="border: 1px solid black; padding: 2px;">KOEVAL</div> amxeval
injection valve cutoff part at ignition switch off by S_KL15	<div style="border: 1px solid black; padding: 2px;">S_KL15_OFF</div> amxeval

#### injection valve cutoff functionality



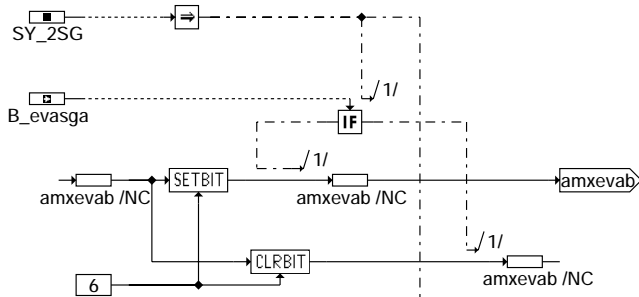
injection may also be disabled if immobilizer is active

#### aevabzk-main



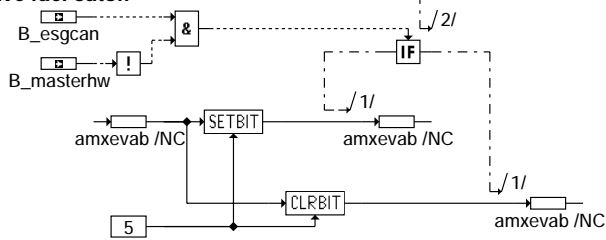
#### aevabzk-throtl-act

**ECU-Selection is wrong  
--> fuel cutoff**

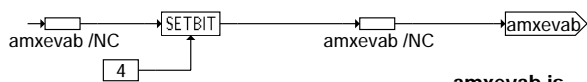


**amxeval is not available as RAM-cell**

**communication error master slave  
--> slave fuel cutoff**

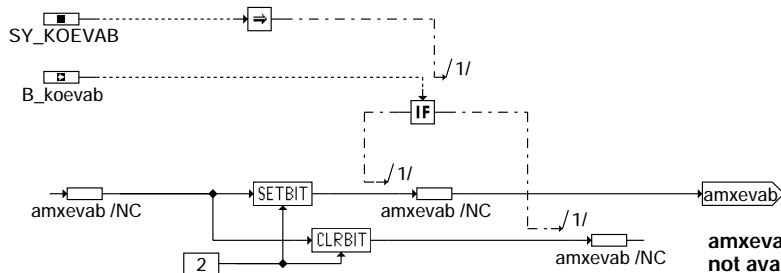


**aevabzk-two-ecus**



**amxeval is not available as RAM-cell**

**aevabzk-s-kl15-off**



**amxeval is not available as RAM-cell**

**aevabzk-koeevab**

**ABK AEVABZK 1.20 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_DVEADA			SYS (REF)	system constant BGVE: disabling injection and ignition during DV-E-adaptation
SY_EGAS			SYS (REF)	System constant E-GAS present
SY_KOEVAB			SYS (REF)	coordination injection valve cutoff by function KOEVAB

Variable	Source	Type	Description
B_DVEADA	BGDVE	EIN	condition: disabling injection during DV-E-adaptation
B_ECULOCK		EIN	Locking request immobilizer
B_ESGCAN		EIN	Condition error ecu-CAN for 2 ME-ecu's
B_EVABU	AEVABU	EIN	Fuel cutoff by .....
B_EVASGA		EIN	condition fuel cutoff by ECU-ID selection
B_KOEVAB	KOEVAB	EIN	injection valve cutoff active by function KOEVAB
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)



Variable	Source	Type	Description
EVZ_AUS	AEVAB	EIN	injection cut off pattern
EVZ_AUSTOT	AEVABZK	AUS	injection cut off pattern total

### FW AEVABZK 1.20 Fixed Values

Parameter	Value	Description
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### FB AEVABZK 1.20 Detailed description of function

The function transmits the injection valve cutoff pattern, `evz_aus`, via the RAM cell `evz_austot` to the function ACIFI on non-EGAS systems. The fuel cutoff itself is performed in function ACIFI.

During ecu after-running, the cutoff pattern 255 is sent. (Subfunction S\_KL\_15\_OFF)

On EGAS systems (Subfunction THROTL\_ACT), the injection valve cutoff pattern `evz_aus` is usually as well sent via `evz_austot` to the function ACIFI.

However, if monitoring functions request an injection valve cutoff via the input `B_evabu`, then `evz_austot` = 255 is transmitted to the function ACIFI which is equal to a request for a complete injection cutoff.

If the EGAS actuator is exchanged, the lower mechanical end position must be learned again by adaptation. During this period, no engine speed > starter motor speed may occur. `B_dveada` prevents that the engine can be started up before the EGAS actuator position has been adapted after an exchange of the EGAS actuator has been recognized; i.e. if `SY_DVEADA` > 0, then `evz_austot` = 255 (complete injection valve cutoff).

The subfunction TWO\_ECUS shows the additional functional features of the injection valve disconnection on systems with more than one ecu's.

The subfunction KOEVAB allows to implement injection valve cutoff types specific to a project, e.g. injection valve cutoff in the event of errors by the automatic gearbox, recognized engine backward movement, engine stalling etc.

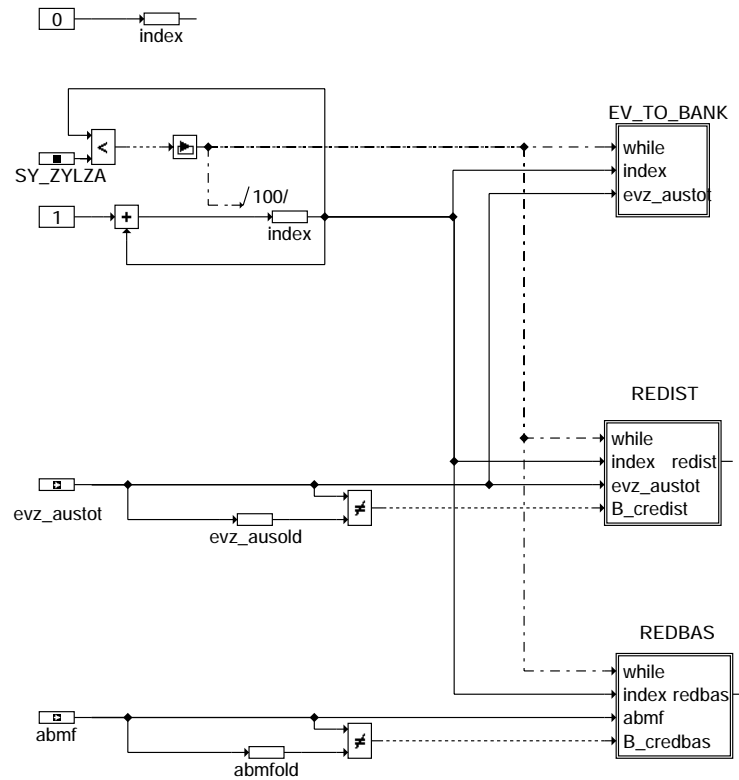
To release the diagnosis "misfire detection", the bit `B_evases` is generated as follows: `B_dmdstop` (locks the misfire detection via function AEVAB during torque interventions) is linked by means of an OR operation to the other types of injection valve cutoff of function AEVABZK. If `B_evases` = true --> misfire detection is released.

### APP AEVABZK 1.20 Application hint

### BGEVAB 1.20 Calculation of the actual reduction stage by ignition-valve cut-off

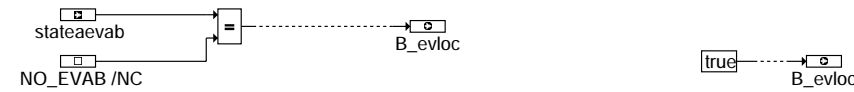
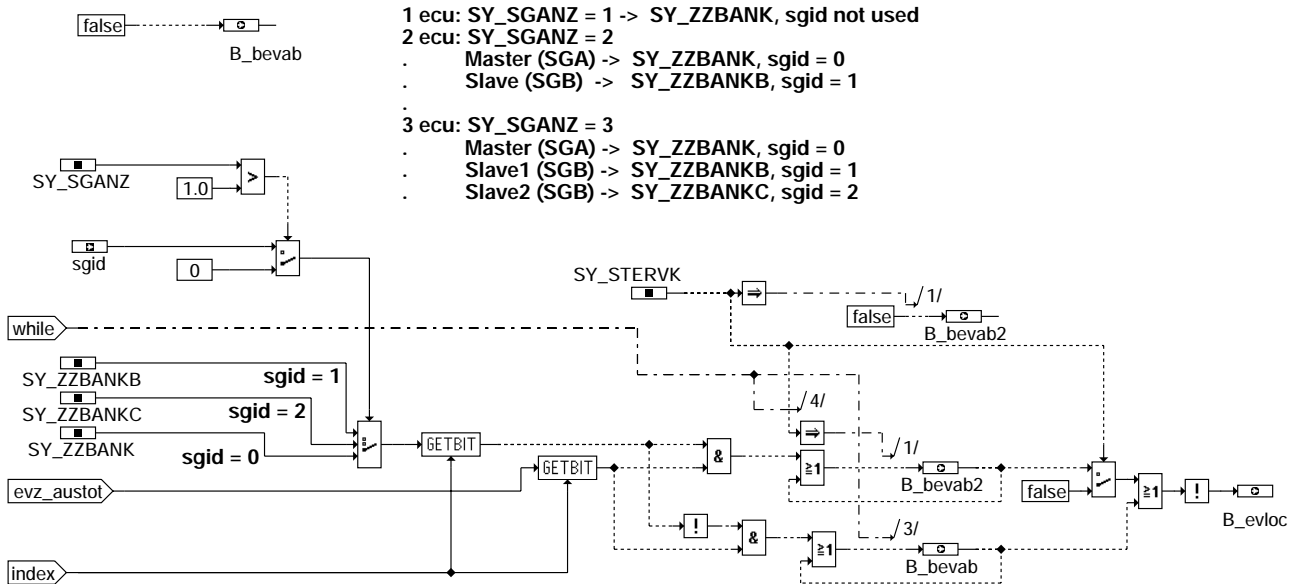
#### FDEF BGEVAB 1.20 Function definition

##### BGEVAB 1.20

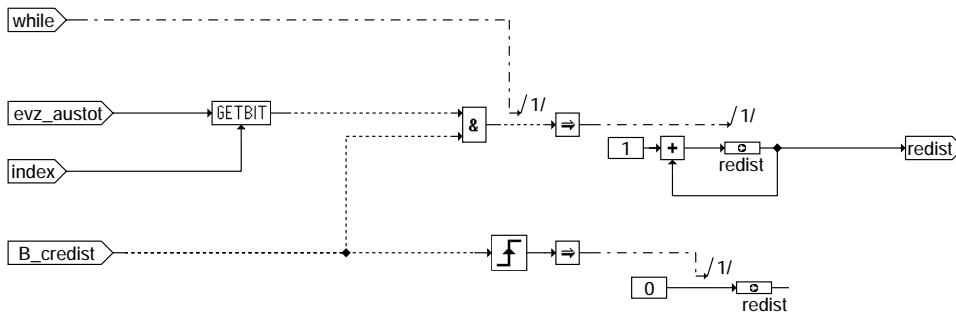


bgevab-main

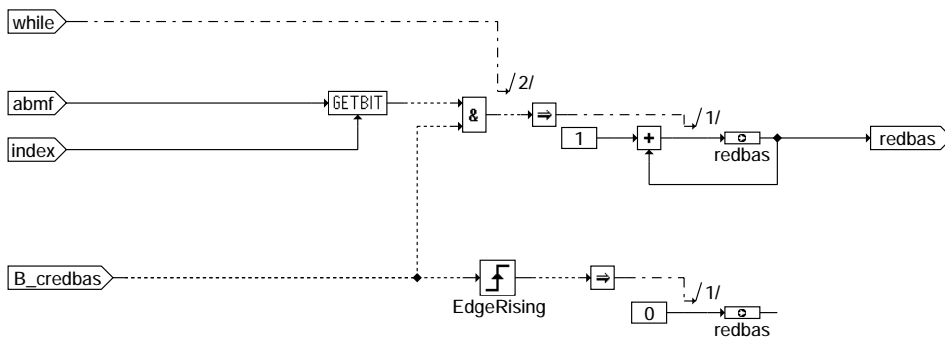
bgevab-main



**bgevab-ev-to-bank**



**bgevab-redist**



**bgevab-redbas**

**ABK BGEVAB 1.20 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
SY_SGANZ			SYS (REF)	system constant number engine control unit
SY_STERVK			SYS (REF)	system constant condition: stereo exhaust system upstream of cat
SY_ZYLZA			SYS (REF)	system constant number of cylinders
SY_ZZBANK			SYS (REF)	system constant assignment of cyl. to bank1/bank2, 0 bank1, 1 b.2, binary value
SY_ZZBANKB			SYS (REF)	system const. ass. of cyl. to exhaust bank1/2 for slave1/SGB; 0 b1, 1 b2 binary
SY_ZZBANKC			SYS (REF)	system const. ass. of cyl. to exhaust bank1/2 for slave2/SGC; 0 b1, 1 b2 binary



Variable	Source	Type	Description
ABMF	AEVAB	EIN	injection cut off pattern at fixed position
ABMFOLD	BGEVAB	LOK	injection cut off pattern at fixed position at time t-1
B_BEVAB	BGEVAB	AUS	condition: Inj. valve cut off on Bank/Bank1
B_BEVAB2	BGEVAB	AUS	condition: Inj. valve cut off on Bank2
B_EVLOC	BGEVAB	AUS	Status: all injection valves are activated
EVZ_AUSOLD	BGEVAB	LOK	injection cut off pattern total at time t-1
EVZ_AUSTOT	AEVABZK	EIN	injection cut off pattern total
REDBAS	BGEVAB	AUS	Base cut-off step
REDIST	BGEVAB	AUS	real cylinder cut-off step
SGID		EIN	ECU-ID
STATEAEVAB	AEVAB	EIN	No. of the active state in AEVAB

### FW BGEVAB 1.20 Fixed Values

Parameter	Value	Description
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### FB BGEVAB 1.20 Detailed description of function

The function uses the injection valve cutoff pattern `evz_austot` to calculate the true reduction ratio `redist`, and the conditions `B_beavab`, 2, which state on which exhaust gas bank an Ev is disconnected. Since the function is also applicable to projects with multiple control devices, a distinction must be made between cylinder banks and exhaust gas banks. One control device (ecu) does always control one cylinder bank which may include either one exhaust gas bank (`SY_STERVK = false`) or 2 exhaust gas banks (`SY_STERVK = true`).

`B_beavab = true`: at least one Ev of exhaust gas Bank1 is disconnected.  
`B_beavab2 = true`: at least one Ev of exhaust gas Bank2 is disconnected.

Any final amplifier fault and any disconnection of an injection valve is displayed in `B_evloc`.

In the event of a disconnected Ev or a faulty final applies: `B_evloc = false`

If a cylinder is disconnected, the misfire detection is locked by the tester; in the event of a torque reduction, the bit `B_evasel = false`. This bit is calculated in `%AEVAB`.

Disconnection request	Disconnection condition	Disconnection information	Misfire recognition
Tester fire detection locked	<code>devoff &gt; 0</code>		<code>-&gt; B_evloc = false</code> <code>-&gt; B_evasel = false</code>
Torque reduction fire detection locked	<code>redsol &gt; 0</code>	<code>&amp; B_faevz = TRUE</code>	<code>-&gt; B_evloc = false</code> <code>-&gt; B_evasel = false</code> Mis-
amplifier diagnosis fire detection active	<code>eevx &gt; 0</code>		<code>-&gt; B_evloc = false</code> <code>-&gt; B_evasel = true</code> Mis-
Misfire recognition fire detection active,	<code>flgtiab &gt; 0</code>		<code>-&gt; B_evloc = false</code> <code>-&gt; B_evasel = true</code> Mis-
ther errors.			
Cylinder disconnection detection locked	<code>B_zas = true</code>		<code>-&gt; B_evloc = false</code> <code>-&gt; B_evasel = false</code> Misfire de-

#### Determination of the true resulting reduction ratio, `redist`:

Each injection valve (Ev) which is to be disconnected corresponds to a reduction of 1. Accordingly, `redist` results from the number of bits set in the function `evz_austot` (which is equal to the number of Ev's to be disconnected). For reasons of running time, the counting is done only `SY_ZYLZA` times. The calculation is done only if the value of `evz_austot` has changed (`evz_austot <> evz_ausold`). Here, `evzausold` is the value of `evz_austot` from the preceding calculation.

The bits `B_beavab` and `B_evloc` (`B_beavab2` applies only if `SY_STERVK = true`) are derived from the injection valve cutoff pattern, `evz_austot`.

`B_evloc = false` means that at least one injection valve is disconnected (independently of the Bank where this occurs).

`B_beavb = true` means that an Ev of Bank1 is disconnected.

#### Example:

<code>SY_ZZBANK:</code>	<code>0 1 0 0 1 0 1 1</code>	Bit = 0 --> injection valve associated to Bank1
<code>evz_austot:</code>	<code>0 0 0 0 0 1 0 0</code>	1 inj. valve disconnected, inj.valve associated to Bank1 --> <code>B_beavab = true</code>

The base reduction `redbas` is calculated from the number of Ev's to be disconnected according to the fixed inj.valve cutoff patterns `flgtiab`, `devoff`, `eevx`. They all are memorized in the RAM cell `abmf`. The calculation is only done if the content of the cell `abmf` changes.

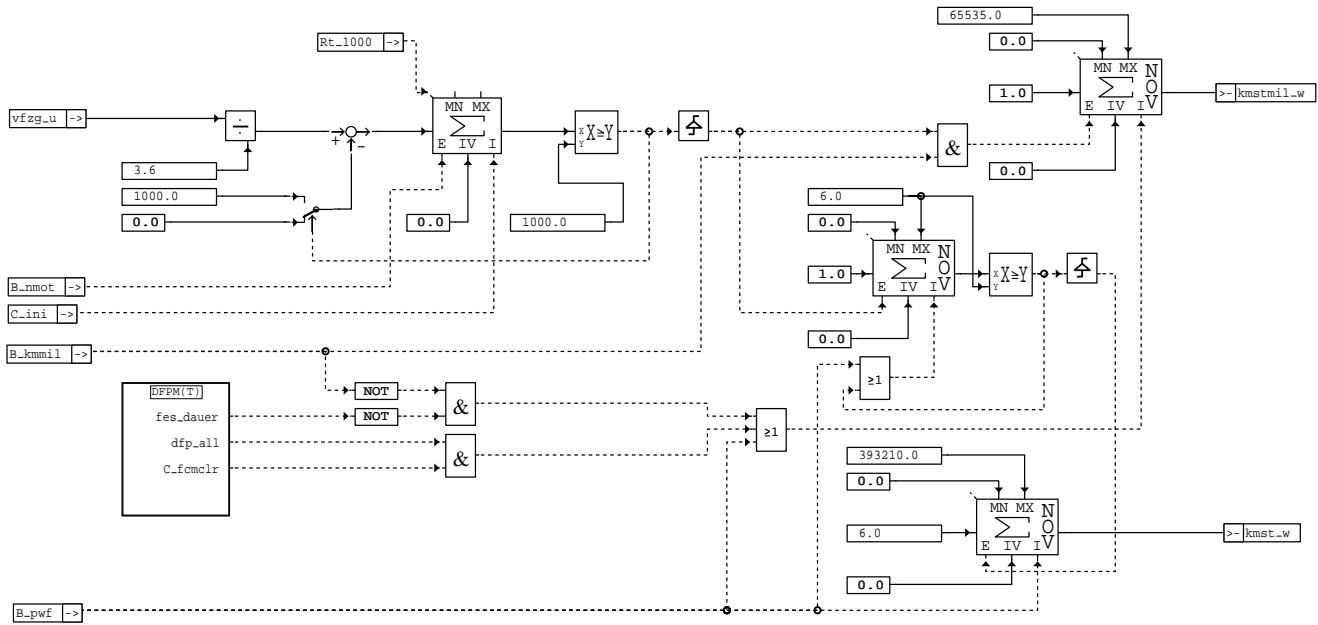
The method is the same as for the calculation of `redist`.

In this case, the injection valves do not need to be assigned to a bank since `abmf` is a subset of `evz_austot` and are accounted for earlier when `redist` is calculated.

## APP BGEVAB 1.20 Application hint

## BGKMST 2.10 Calculation of odometer value (Km)

### FDEF BGKMST 2.10 Function definition



### bgkmst-bgkmst

### ABK BGKMST 2.10 Abbreviations

Variable	Source	Type	Description
B_KMMIL	DMIL	EIN	MIL turn-on related to mileage
B_NMOT	GGDPG	EIN	condition engine speed: $n > NMIN$
B_PWF		EIN	Condition for powerfail
C_FCMLR	BGKMST	LOK	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
KMSTMIL_W	BGKMST	AUS	Drive distance with MIL on
KMST_W	BGKMST	AUS	Drive distance since last power fail
R_T1000		EIN	Time schedule 1000 ms
VFZG_U	DFFTCNV	EIN	Vehicle speed

### FW BGKMST 2.10 Fixed Values

Parameter	Value	Description

### FB BGKMST 2.10 Detailed description of function

EOBD fordert die Erfassung der mit aktivierter MIL zurückgelegten Fahrstrecke. Diese wird in kmstmil\_w aus der Fahrgeschwindigkeit vfzg\_u aufintegriert. Die Quantisierung und Ausgabe von kmstmil\_w erfolgt gemäß SAE J1979, Mode 1, PID\$21. ->%TC1MODx.y

Für Kundendiensttester wird zusätzlich die Fahrstrecke kmst\_w seit powerfail ermittelt.

### APP BGKMST 2.10 Application hint

Zur Steuerung der Funktion über B\_kmmil wird eine entsprechend angepasste DMIL benötigt. ->%DMIL  
Achtung: B\_kmmil ermittelt nur den MIL-Status der Motorsteuerung, andere Systeme müssen eine entsprechende Funktion aufweisen.

Zur Werteausgabe ist eine entsprechend angepasste SCAN-TOOL-Kommunikation nötig: ->%TC1MOD

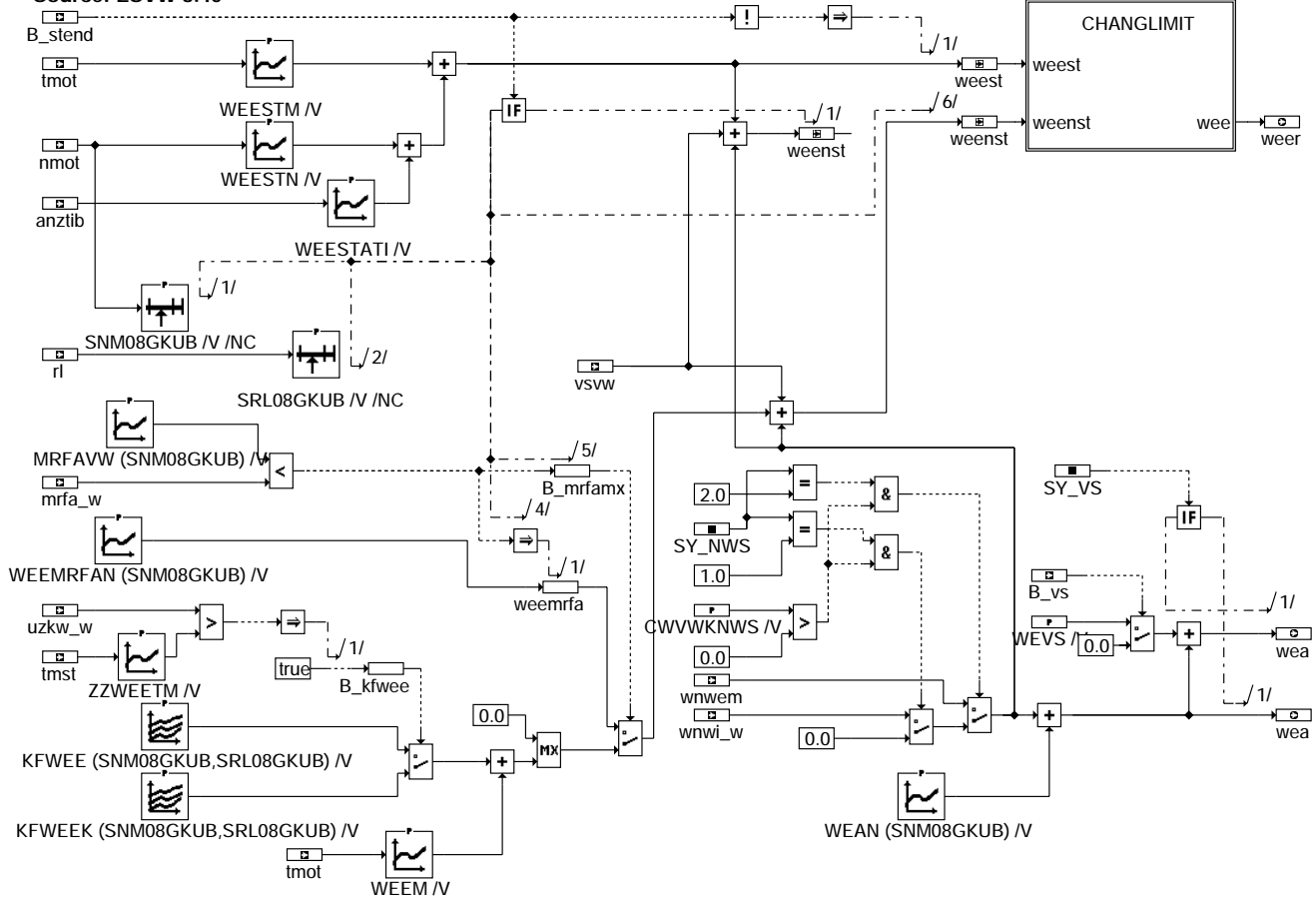




## ESVW 3.40 Injection : calculation of injection angle

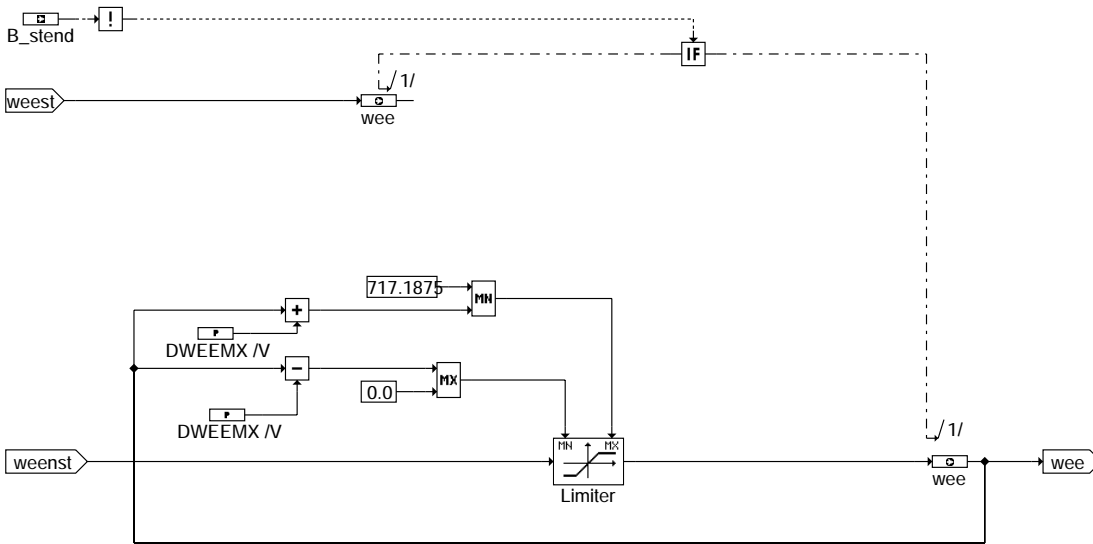
### FDEF ESVW 3.40 Function definition

Source: ESVW 3.40



esvw-main

### CHANLIMIT (T) limitation of wee change



esvw-changlimit



## ABK ESVW 3.40 Abbreviations

WESBM Angle Intake valve closure (Es) before reference mark (BM)

Es Control time for intake valve closure  
LWOT Charge Changing Upper Dead Center  
ZOT Ignition Upper DC, IUDC  
UTH Compression Bottom DC

Parameter	Source-X	Source-Y	Type	Description
CWVWKNWS			FW	code word: correction of injection angle for active cam control
DWEEMX			FW	max. change of "angle end of injection" per ignition
KFWEE	NMOT	RL	KF	characteristic map angle end of injection
KFWEEK	NMOT	RL	KF	map for end of injection angle (cold parameters)
MRFVW	NMOT		KL	threshold to switch end of injection angle at max. driver request
SY_NWS			SYS (REF)	system constant camshaft control: none, 2 point, continuous
SY_VS			SYS (REF)	system constant valve stroke control: no, 2 position
WEAN	NMOT		KL	angle injection break off
WEEM	TMOT		KL	correction of prestorage angle
WEEMRFAN	NMOT		KL	end of injection angle at max relative driver request
WEESTATI	ANZTIB		KL	Offset for injection end angle towards early
WEESTM	TMOT		KL	correction of pretiming of injection during start
WEESTN	NMOT		KL	end of injection angle during start
WEVS			FW	Angle correction for valve stroke adaptation
ZZWEETM	TMST		KL	Switchover threshold pattern angle

Variable	Source	Type	Description
ANZTIB	ACIFI	EIN	injection counter limited
B_KFWEE	ESVW	LOK	condition map KFWEE activ
B_MRFAMX	ESVW	LOK	angle injection-end activated by maximum desired driver request torque
B_STEND	BBSTT	EIN	condition end of start
B_VS		EIN	Condition valve lift high
MRFVW	MDFVW	EIN	relative driver request torque from cruise control and pedal, =0 in limp-home
NMOT	SWADAP	EIN	engine speed
RL	SWADAP	EIN	relative air charge
TMOT	SWADAP	EIN	Engine temperature
TMST	GGTFM	EIN	engine temperature at start
UZKW_W	GGDPG	EIN	revolution counter crankshaft
VSVW	VS_VERST	EIN	change in the phase injection angle by the application system
WEA	ESVW	AUS	anglemark injection break off
WEE	ESVW	AUS	angle injection-end in normal operation
WEEMRFA	ESVW	LOK	angle injection-end at maximum of desired driver request torque
WEENST	ESVW	LOK	angle injection-end after end of start
WEER	ESVW	AUS	resulting crankshaft angle for end of injection
WEEST	ESVW	LOK	angle injection-end at start
WNWEM		EIN	Camshaft angle intake (average value)
WNWLW		EIN	actual shifting angle of the camshaft (word)

## FW ESVW 3.40 Fixed Values

Parameter	Value	Description
CWVWKNWS		code word: correction of injection angle for active cam control
DWEEMX		max. change of "angle end of injection" per ignition
WEVS		Angle correction for valve stroke adaptation



## FB ESVW 3.40 Detailed description of function

### Formation of the advance angle:

The advance angles defined in the characteristic curves and mappings refer to the intake valve closure (at a valve stroke of 0 mm). On systems with intake camshaft shifting (2-point or continuous), they refer to the late position of the camshaft. When calculating the end of the injection interval after engine start, any angular difference towards earlier in the camshaft position is accounted for, i.e. if the intake valve closes earlier, the injection interval is also terminated earlier. The end of the injection interval is calculated as follows:  $wee = KFWE + WEEM + wnwi$  (2-point CS shifting), or  $wee = KFWE + WEEM + wnwem$  (continuous CS shifting).  $wee$  and  $weer$  differ only with respect to the quantization. The variable  $vsvw$  allows to achieve a change the advance angle using the VS20 adjustment system.

During engine start applies:  $wee = weest = WEESTM + WEESTN$ .

During engine start, the camshaft shifting is not considered. The camshaft is considered to be in the late end position until the engine start has finished.

The speed dynamic during engine start requires  $weest$  to be calculated in the Synchro-Raster.

During normal operation, the advance angle is calculated as follows:  $wee = weenst = KFWE + WEEM$ . The sudden changes in the advance angles which occur during the switch-over, especially when switching over to the mapping WEEMRFAN, are limited by the transient limitation of the function CHANGLIMIT.

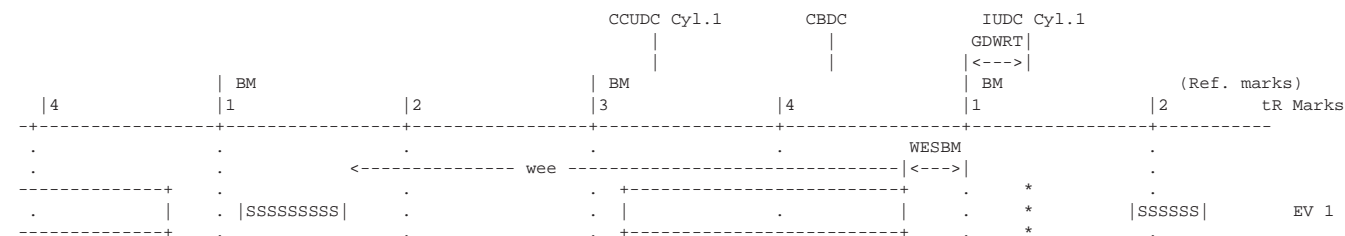
### ti triggering:

The function ACIFI calculates the angle where the injection must start, using duration of  $ti$ , engine speed and advance angle, and starts the  $ti$  output when the associated negative tooth slope passes. Both length of the injection interval,  $ti$ , and starting point of the injection are calculated for any TR mark.

### Output of a termination angle wea:

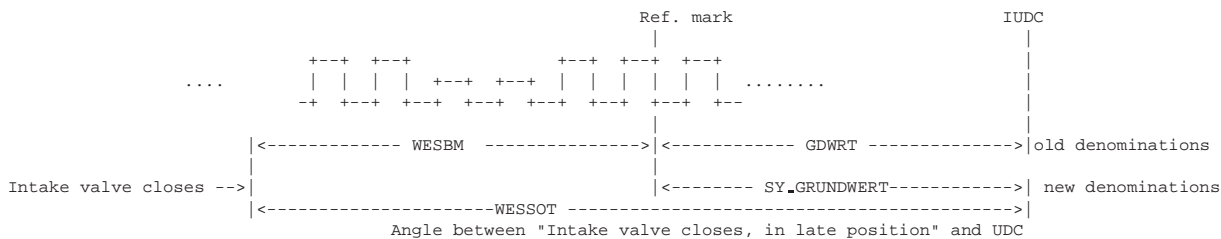
The characteristic curve WEAN f(nmot) transmits a termination angle,  $wea$ , in order to avoid that after-dashes are injected into a closing intake valve. Here, the time of flight needed by the fuel, which is approx. 6...10ms, must be considered (see the description in the APP section of the present function). This angle also considers the intake valve shifting angle. The termination angle is used in function %BRGLP to release after-dashes whereas the physical after-dashes are calculated and sent by the function ACIFI.

### Specification of the advance angle:



\* Ignition output  
|SSSSS| Sequential Injection

### Position of the upper reference mark:



## APP ESVW 3.40 Application hint

### Start of injection interval during engine start:

On many engines, it is favourable to inject onto the closed intake valve to prevent the spark plug from being wetted directly. On engines where the spark plug is located in an uncritical position, especially on 4-valve engines, it makes sense to inject when the intake valve is about to open so that the air flow helps to achieve a better mixture preparation.

Note: the valve control timing apply to the beginning of aperture and to the end of closure of the intake valve, i.e. they apply to a valve stroke of 0 mm. The distance WEBSM which ranges from the reference mark to the closure of the intake valve must be referred to this point.

Since in practice, the point where the intake valve closes is often defined as 1 mm valve stroke (and WEBSM is in this case increased with respect to a valve stroke of 0mm), it is important to check which definition is in use when data is exchanged between different projects.

### WEBSM:

WEBSM is the angle between intake valve closure and the reference mark or the tR mark of the respective cylinder. Here, the associated tR mark is the last mark before the respective IUDC (=ZOT). The distance between tR mark and IUDC is memorized as the value of SY\_GRUNDWERT.

Accordingly, WEBSM must be adapted if the intake control timing or the position of the reference mark are changed.

In such a case, values in (CS are stated in the advance angle mappings and characteristic curves which express a pre-positioning with respect to the intake valve closure (Es).



WESBM is calculated according to the control time "intake valve closes" (Es) and the distance GDWRT between the BM reference mark and the IUDC (=ZOT) as follows:

$$\text{WESBM } (^{\circ}\text{CS}) = 180 (^{\circ}\text{CS}) - \text{Es } (^{\circ}\text{CS after CBDC (=UTH)}) - \text{SY\_GRUNDWERT } (^{\circ}\text{KW})$$

!!! If WESBM should assume negative values according to this formula, the point "intake valve closes" must be defined as 1 mm valve stroke. Once defined, the value of WESBM may no longer be changed during the application process.

Position of the injection interval:

When the end of the injection interval is implemented, the following aspects should be considered:

- the injection interval should not start before the angle "intake valve closes" of the preceding cycle.
- as the advance angle increases, the ti calculation may suit the actual conditions lesser (dynamics, bucking, lambda control)
- the fuel time-of-flight must be considered (according to the fuel pressure, to the air speed in the suction pipe and to the specific distance between injection valve and intake valve. A typical fuel time-of-flight may be e.g. 7ms.

Calculation of the time-of-flight:

The time-of-flight [ms] results from the distance spanned by the fuel droplets (which is the distance between injection valve and intake valve) divided by the mean flight speed of the fuel droplets. The distance is typically about 100mm, the average speed is about 15m/s. -->flighttime = 6,67ms.

This time allows to derive a camshaft angle which varies according to the engine speed.

$$\text{-->flightangle}[^{\circ}] = \{360^{\circ} * n [1/\text{min}] * \text{flighttime} [\text{ms}] / 60000[\text{ms}/\text{min}]\}$$

For example: flighttime 7ms --> 1000 1/min: 42°; 6000 1/min: 252°.

Experience shows that the flight angle varies up to an engine speed of 4000 RPM; above this speed, the flight angle may assumed to be constant. ( The value for 4000 RPM is 160°CS in the above example.)

Start of injection interval during normal operation:

In order to ensure a sufficient injection advance angle even in the event of extreme engine speed dynamic, and to avoid that fuel is injected into the open intake valve, the injection interval is shifted according to engine speed, considering a dynamic advance. Injection should start only when the angle "Intake valve closes" (Es) of the preceding intake cycle has passed by. An excessive injection advance angle should be avoided also to keep the ti calculation as up-to-date as possible (see also the application information for %UKSEFI, %ESUK, %BGRLLP).

Advance angle mapping KFWEEM/KFWEEM:

After the end of engine start, the advance angle is formed from KFWEEM + WEEM. The switch-over to KFWEEM is done after ZZWEETM crankshaft revolutions.

ZZWEETM depends on the engine temperature tmst during engine start. If engine and suction pipe are cold, this path implements a reduction in the advance angle.

If engine and suction pipe are warm, an increase in the injection advance angle is used to enhance the mixture preparation inside the suction pipe.

Characteristic curve WEEMRFAN:

This mapping is used to adjust the injection advance angle so that the fuel is injected into the open intake valve if the driver commands full power. The intention is to have the components cooled down by the vaporization inside the cylinder, which yields also an increase in the filling ratio. The threshold which determines from when onwards to apply this characteristic curve is defined in the characteristic curve MRFAVN.

Change limitation DWEEMX:

The partial function CHANGE LIMITATION represents a transient limitation for wee or weer.

If fuel is injected into the open intake valve for long time, the wall film present in the suction pipe reduces to zero.

When the switch-back to injection in advance is performed in these conditions, the wall film forms again and causes the mixture to be lean for short time.

Limitation of this injection advance angle distributes the loss caused by wall film formation over several injection intervals and therefore, reduces the leaning-down effect. However, it is not possible to prevent the leaning-down completely using this primitive method.

The change limitation applies to sudden changes towards wider and smaller injection advance angles after the end of engine start.

Group base points are used for the characteristic curves and mappings:

Suggested values of the base points:

WEESTM,WEEM: Source tmot : -30, -10, 10, 30, 50, 75, 100, 130 degrees

KFWEEM, KFWEEM, WEAN, WEEMRFAN, MRFAVN: Source nmot: 500, 1000, 1500, 2000, 3000, 4000, 5000, 6000 1/min

KFWEEM, KFWEEM: Source rl : 20, 40, 60, 80, 100, 125, 150, 175 %

MRFAVN: Values 200% --> B\_mrfamx is always false

WEESTN: Source nmot: 125, 300, 700, 1200 1/min

Values: 0 0 degrees

DWEEMX: 6 degrees/Ignition Resolution is 6 degr.

720 degr. -> no change limitation active

ZZWEETM: Source tmst: -30, -20, -10, 0, 10, 20, 40, 70 degr.

Values: 0 0 CS Revolutions 0: KFWEEM is active directly after engine start  
>0: KFWEEM is active for this number of CS revolutions

WEESTATI: Source anztib\_w 2, 4, 5, 6, 7, 8

Values 0 degr. CS

The characteristic curve can be used to achieve a sudden change in the injection advance angle towards early for a determined injection interval during engine start at high engine speed dynamic. This sudden change depends directly on the counter for already performed injections, anztib\_w. This counter starts to count only after the injection has been activated which must be



accounted for when determining the injection advance angle.

This means the sudden change in the injection advance angle needs to be triggered off one or two ti's earlier.

SY\_NWS = 1.0 -> Accounts for wnwi according to CWVWKNWS on two-point CS shifting systems

SY\_NWS = 2.0 -> Accounts for wnwm according to CWVWKNWS on systems with continuous CS shifting

CWVWKNWS = 0: CS shifting towards earlier is not accounted for in the advance angle

CWVWKNWS > 0: SH shifting towards earlier is accounted for in the advance angle

WEVS: On systems with variable valve stroke (SY\_VS = true), the termination angle wea is shifted by the value WEVS towards earlier  
Initial data assignment: WEVS = 0.

Further information on how to apply the advance angle is included in the application information for application of the transition compensation %UKSEFI, %ESUK, load prediction %BGRLP.

## ACIFI 9.70 Output for cylinder-individual injection

### FDEF ACIFI 9.70 Function definition

No text for FDEF available!

### ABK ACIFI 9.70 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWESWEZ			FW	enable codeword restart fuel feed
FWEAB			FW	recursion constant for fuel cut-in factor decreasing
FWEAUF			FW	recursion constant for fuel cut-in factor increasing
FWEMXT	TMOT		KL	maximum factor for fuel cut-in temperature characteristic
FZN1	NMOT		KL	Cylinder individual factor at neutral camshaft position EV 1
FZNWN1	NMOT		KL	Cylinder individual factor at active camshaft position EV 1
TMESP			FW	Engine temperature threshold quick start
TVFZNW			FW	Delay time for activation of CIFI factors after camshaft phasing
WEESTS			FW	limit for end of injection angle during start

Variable	Source	Type	Description
ANZTI	ACIFI	AUS	injection counter
ANZTIB	ACIFI	AUS	injection counter limited
ANZTIB_W	ACIFI	AUS	injection counter with limit
ANZTI_W	ACIFI	AUS	injection counter
B_CWESAKT	ACIFI	AUS	Codeword CWESWEZ bit 3 true
B_NWS	NWS	EIN	Condition camshaft control
B_SA	MDRED	EIN	Condition fuel cut-off
EVZ_AUSTOT	AEVABZK	EIN	injection cut off pattern total
FWEG	ACIFI	AUS	
FWEZ0	ACIFI	AUS	
NMOT	SWADAP	EIN	engine speed
TI_B1	RKTI	EIN	injection time for valves on bank1
TI_B2	RKTI	EIN	injection time for valves on Bank2
TI_EV0	ACIFI	AUS	injection time 1. cylinder in firing sequence
TI_TVU_W	RKTI	EIN	injection time correction as function of battery voltage ECU-quantization
TMOT	SWADAP	EIN	Engine temperature
ZZBANK		EIN	cylinder allocation to injection banks

### FW ACIFI 9.70 Fixed Values

Parameter	Value	Description
CWESWEZ		enable codeword restart fuel feed
FWEAB		recursion constant for fuel cut-in factor decreasing
FWEAUF		recursion constant for fuel cut-in factor increasing
TMESP		Engine temperature threshold quick start
TVFZNW		Delay time for activation of CIFI factors after camshaft phasing
WEESTS		limit for end of injection angle during start

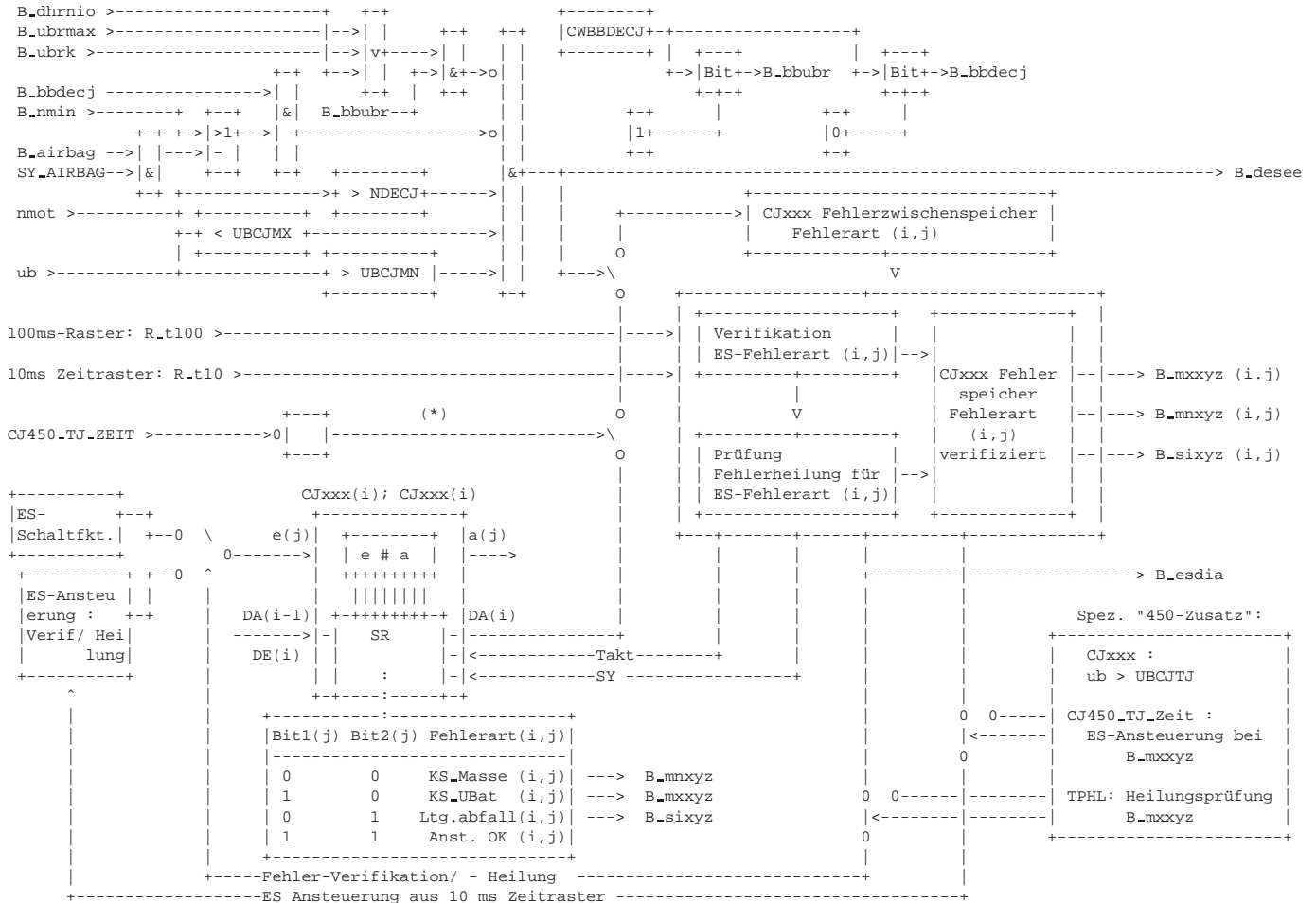
### FB ACIFI 9.70 Detailed description of function

### APP ACIFI 9.70 Application hint

## DECJ 14.30 Diagnosis; Power stage CJ9x

### FDEF DECJ 14.30 Function definition

The following presentation of the output stage diagnostics applies in its entirety for the types CJ450 (with excess temperature shut-off): Restrictions for the other versions: effects (\*) and "Special 450-supplement" block not applicable



Bit1(j), bit2(j) in CJxxx fault shift register SR is set for an unplausible comparison of e(j) with a(j)  
Assignment : i = variable for output stage IC ; j = variable for output stage / IC (see %DEKON for ES assignment)

For the case of output stages of the type CJ405, CJ420, CJ920 (with display for excess temperature):  
The same bit pattern is used to detect excess temperature as for detection of a line drop. Differentiation for diagnostics and verification by means of control : ES off --> line drop , ES on --> display of excess temperature (not implemented in ME7)

Scan CJxxx fault shift register SR with control SY and clock pulse  
Initiate fault healing check according to { THP } - run through of 100 ms time base

For output stages of the type CJ450 (with shut-off for excess temperature):  
Call the CJxxx fault healing check for B\_mnxyz according to { THP } \* { THPL } -run through of 100 ms time base.

The output stage faults stored in the CJxxx fault memory as verified fault types (i,j) are transferred into the OBDII fault memory, except for output stages of the types CJ405, CJ420, CJ920 (with display of excess temperature).  
Organization of the fault memory in accordance with the functional description %DFPM.

## ABK DECJ 14.30 Abbreviations

ES	Output stage	
SR	CJxxx fault shift register	
DE	Data input (serial) in CJxxx fault shift register	
DA	Data output (serial) from CJxxx fault shift register	
B_mnxyz	Fault type: less than minimum value fault path "xyz" (wildcard)	
B_mxxyz	Fault type: greater than maximum value fault path "xyz" (wildcard)	
B_sixyz	Fault type: signal inactive fault path "xyz" (wildcard)	
UBCJMN	Immediate constant	Minimum battery voltage for enabling CJxxx output stage diagnostics
UBCJMX	Immediate constant	Maximum battery voltage for enabling CJxxx output stage diagnostics
UBCJTJ	Immediate constant	Battery voltage threshold for CJ450 KS_UBat healing check
NDECJ	Immediate constant	Engine speed threshold for CJxxx output stage diagnostics
THP	Immediate constant	Number of time base run through for fault healing check
THPL	Immediate constant	CJ450 KS_UBat healing check after THP * THPL runs

For output stages of the type CJ450 (with shut-off for excess temperature):  
CJ450\_TJ\_ZEIT Immediate constant Turn-on time of the CJ450 ES for KS\_UBat healing check



Variable	Source	Type	Description
B_AIRBAG		EIN	condition airbag activated
B_BBDECJ	DECJ	AUS	condition stall protection DECJ
B_BBUBR	DECJ	AUS	condition operation mode f. powerst. diagn. to be disabled by supply voltage err
B_DESEE	DECJ	AUS	Diagnosis power stage: entry conditions fulfilled
B_ESDIA	DECJ	AUS	Power stage diagnosis active
B_NMIN	GGDPG	EIN	condition lower speed: n < NMIN
B_UBRK		EIN	condition main relay contact fault
B_UBRMAX		EIN	condition onboard battery voltage via main relay higher than UBRDMX
NMOT	SWADAP	EIN	engine speed
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
UB	SWADAP	EIN	battery voltage

### FW DECJ 14.30 Fixed Values

UBCJMN	{ UBCJMN }	Minimum battery voltage for enabling CJxxx output stage diagnostics
UBCJMX	{ UBCJMX }	Maximum battery voltage for enabling CJxxx output stage diagnostics
UBCJTJ	{ UBCJTJ }	Battery voltage threshold for CJ450 KS_UBat healing check
NDECJ	{ NDECJ }	Engine speed threshold for CJxxx output stage diagnostics
THP	{ THP }	Fault healing check after (THP * 100 ms-[time base]) seconds

For output stages of the type CJ450 (with shut-off for excess temperature):

THPL	{ THPL }	CJ450 KS_UBat healing check after THP * THPL run through
CJ450_TJ_ZEIT	{ CJ450_TJ_ZEIT }	Turn-on time of the CJ450 ES for KS_UBat healing check

Parameter	Value	Description
-----------	-------	-------------

**FB DECJ 14.30 Detailed description of function**

Output stage diagnostics in IC hardware:

The output stage component includes 4 output stages (ES) resp. 14 ES (on CJ920). The input level and the output level are checked in each ES for plausibility by monitoring the hardware. Any detected fault is stored in a shift register (SR) as 2-bit information for each ES (see Table PDEF for coding) and can be read out from here via a serial interface.

Short-circuit to ground and (KS\_Masse) and line drop (Ltg.abfall) are detected when the ES are in the disabled state; whereas a short circuit to UBat (KS\_Bat) is detected for a conducting ES. The defective ES is switched off to protect the ES IC in the case of KS\_UBat. Reactivation is possible following a change in the flank from high --> low at the input or by reset.

Special feature of the CJ450:

The output stages have a limiting maximum current. KS\_UBat can only be detected by a shut-off for excess temperature.

The serial transfer shift register -> CPU is controlled by 3 CPU ports (SY = low : changeover of fault set parallelly to shift serially, SY: low -> high : shift register deleted upon completion of the transfer; clock pulse: the information is shifted by a positive clock pulse flank, DA: serial data output shift register). The interface is extended without additional CPU ports by cascading the shift register (connection of DA to DE of the next IC). The level of the DA line is set to low for an entry of a fault in the shift register.

Realization of the software interface for ES diagnostics:

The assignment of the output stage IC's is described in terms of configuration bytes in %DEKON. At the same time, the diagnostic routine can be determined by assigning 2 bits to each output stage.

bit 1	bit 0	
0	0	Diagnostics active with OBDII fault storage and with healing check
0	1	Diagnostics active without OBDII fault storage, with healing check
1	0	Diagnostics active without OBDII fault storage and without healing check
1	1	Diagnostics inactive

Read-out of the IC shift register is only permissible in a programmable UBat and speed range.

The UBat thresholds UBCJMN and UBCJMX are determined by the functional limit of the IC. The computation base must already be started in the system in which operation of the CJxxx diagnostics is performed. The diagnostics routine is disabled until the programmable speed threshold NDECJ is exceeded. It is possible to suppress the start range by means of the speed threshold NDECJ. The index >i< is assigned to the power stage IC's and the index >j< to the individual output stages.

The level of the DA line is sampled in each 100 ms time base run through for the condition B\_desee = true. For a low level of the DA line, there is an ES fault present as detected by the hardware which must now be selected according to output stage and fault type by reading out the interface. The level of the line SY is pulled down to low in order to start the read-out process and one bit of information is subsequently shifted on the DA line out of the shift register and stored in a buffer memory in the CPU as a "fault to be verified" with each positive flank on the clock pulse line. Allocation of the fault type and the corresponding output stage is now possible from the position of the set bit information.

The diagnostics software takes over control of an output stage with a detected fault for verification of the fault (B\_esdia = true). The output stage detected as being out of order is disabled. The shift register is deleted by setting and resetting the SY line in the ES IC. The output stage is controlled in the 10 ms time base such that the fault types KS\_Masse, line drop and KS\_UBat can be generated. The fault status in the shift register is "frozen" by setting the SY line to low. The ES control is returned to the pertinent ES driver software (B\_esdia = false). The CJxxx shift register cascade is read out during the subsequent run through the 100 ms time base. If fault type and output stage can now be verified, there then follows a transfer into a fault memory for verified output stage faults and the transfer into the OBDII fault memory. Following readout, the shift register in the CJxxx is enabled again by setting the SY level to high.

A time counter is started at the same time as fault verification. A check for healing of those output stages detected as being defective is performed after elapse of this counter. The time THP is set by a defined number of program runs.

The healing check of the output stages is carried out in the same manner as described for fault verification. During the healing check, those output stages are controlled which are stored with a verified fault type.

For output stages of the type CJ450 (with shut-off for excess temperature):

Fault verification and healing check for KS\_UBat:

A short circuit to UBat cannot be detected with certainty by the standard control procedure for KS\_UBat during the check for verification and healing because of the thermal time constant. The fault KS\_UBat is therefore considered as being verified when it has occurred twice.

The fault healing check switches over to its own time control. The healing check is performed following a time period is formed as the product of the run times THP \* THPL. Control of the defective ES is then for longer than 1 sec (specified in CJ450-TJ-ZEIT), if the UBat threshold (UBCJTJ) is exceeded. The possibility of transferring the fault from the ES IC is disabled throughout the control time CJ450-TJ-ZEIT.



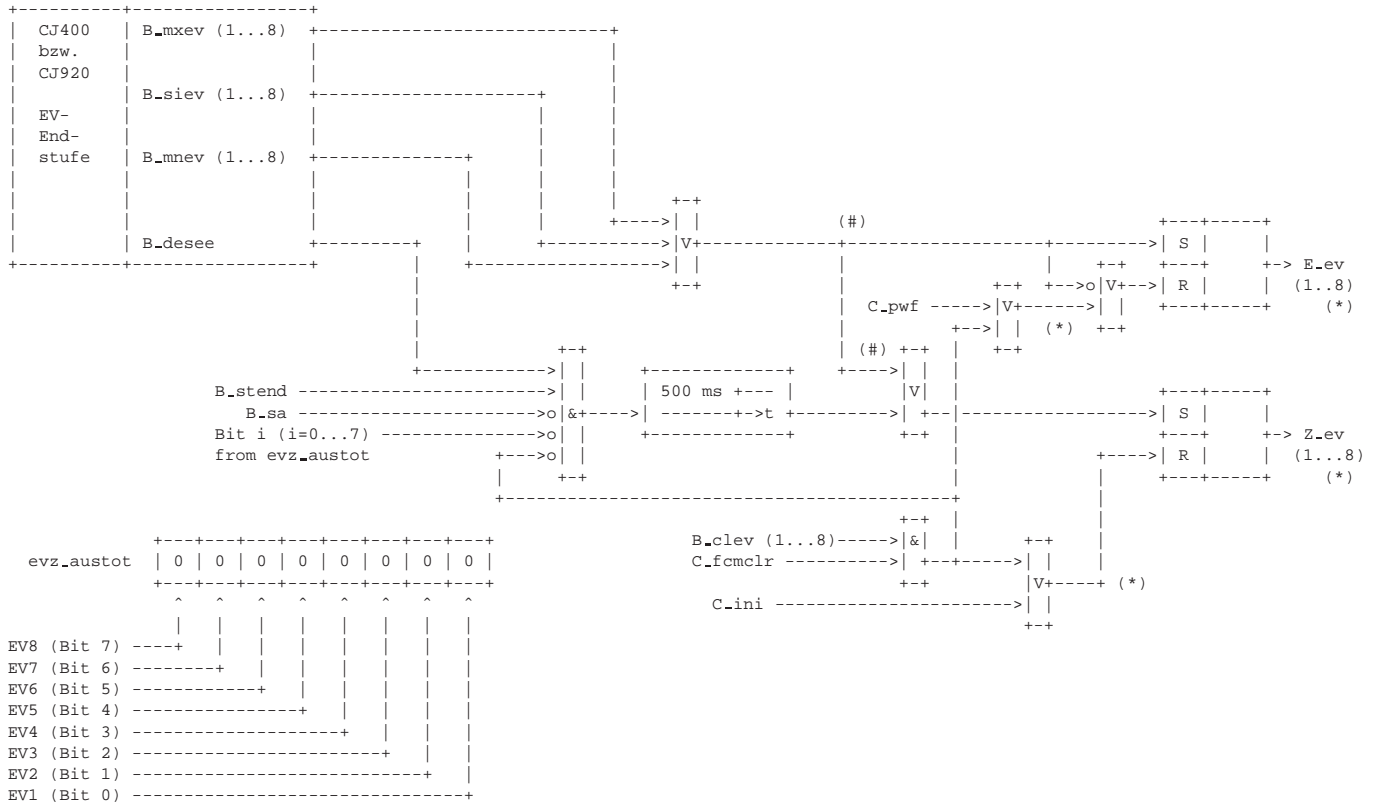


## APP DECJ 14.30 Application hint

## DEVE 6.40 Diagnosis; power stage of injector valve

### FDEF DEVE 6.40 Function definition

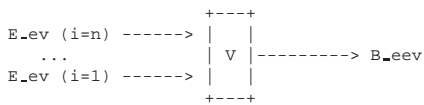
Diagnosis CJ 400, resp. CJ 920 see %DECJ



Bits (E\_evi, Z\_evi), that do not exist because of ZYLZA<8, are set per definition:

```
E_evi (i>ZYLZA) = false
Z_evi (i>ZYLZA) = true
```

Example: For a 6-zylinder engine E\_ev7 = E\_ev8 = false and Z\_ev7 = Z\_ev8 = true.



(\*) deviant from the description this path is served in the module %DFPM resp. the flags are managed in %DFPM;  
(#) deviant from the description this path is served in the module %DECJ;

Error memory management:

```
Status error path EV: sfpev
Error flag EV: E_ev
Cycle flag EV: Z_ev
Error type EV: Typ_ev
Kind of error EV: B_mxev
                  B_mnev
                  B_siev
```

```
Clear error path: C_fmclr & B_clev
Error path EV: CDTEV
Error class EV: CLAEV
Error intensity EV: TSFEV
Carb code EV: CDCEV
Ambient conditions EV: FFTEV
```



## ABK DEVE 6.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCEV1	BLOKNR		KL	code word CARB: injector 1
CDCEV2	BLOKNR		KL	code word CARB: injector 2
CDCEV3	BLOKNR		KL	code word CARB: injector 3
CDCEV4	BLOKNR		KL	code word CARB: injector 4
CDCEV5	BLOKNR		KL	code word CARB: injector 5
CDCEV6	BLOKNR		KL	code word CARB: injector 6
CDCEV7	BLOKNR		KL	code word CARB: injector 7
CDCEV8	BLOKNR		KL	code word CARB: injector 8
CDTEV1			FW	code word tester: injection valve of cyl. 1
CDTEV2			FW	code word tester: injection valve of cyl. 2
CDTEV3			FW	code word tester: injection valve of cyl. 3
CDTEV4			FW	code word tester: injection valve of cyl. 4
CDTEV5			FW	code word tester: injection valve of cyl. 5
CDTEV6			FW	code word tester: injection valve of cyl. 6
CDTEV7			FW	code word tester: injection valve of cyl. 7
CDTEV8			FW	code word tester: injection valve of cyl. 8
CLAEV1			FW	error class: injector power stage 1
CLAEV2			FW	error class: injector power stage 2
CLAEV3			FW	error class: injector power stage 3
CLAEV4			FW	error class: injector power stage 4
CLAEV5			FW	error class: injector power stage 5
CLAEV6			FW	error class: injector power stage 6
CLAEV7			FW	error class: injector power stage 7
CLAEV8			FW	error class: injector power stage 8
FFTEV1	BLOKNR		KL	freeze frame table: injector power stage 1
FFTEV2	BLOKNR		KL	freeze frame table: injector power stage 2
FFTEV3	BLOKNR		KL	freeze frame table: injector power stage 3
FFTEV4	BLOKNR		KL	freeze frame table: injector power stage 4
FFTEV5	BLOKNR		KL	freeze frame table: injector power stage 5
FFTEV6	BLOKNR		KL	freeze frame table: injector power stage 6
FFTEV7	BLOKNR		KL	freeze frame table: injector power stage 7
FFTEV8	BLOKNR		KL	freeze frame table: injector power stage 8
TSFEV1			FW	fault active time: injector of cyl 1
TSFEV2			FW	fault active time: injector of cyl 2
TSFEV3			FW	fault active time: injector of cyl 3
TSFEV4			FW	fault active time: injector of cyl 4
TSFEV5			FW	fault active time: injector of cyl 5
TSFEV6			FW	fault active time: injector of cyl 6
TSFEV7			FW	fault active time: injector of cyl 7
TSFEV8			FW	fault active time: injector of cyl 8
ZYLZA			FW	number of cylinders
Variable	Source		Type	Description
B_CLEV			EIN	condition clear fault path injector power stage
B_DESEE	DKOSE		EIN	Diagnosis power stage: entry conditions fulfilled
B_EEV	DEVE		AUS	condition injector fault (power stage)
B_MNEV1			EIN	Error type: short circuit to ground at power stage injector 1
B_MNEV2			EIN	Error type: short circuit to ground at power stage injector 2
B_MNEV3			EIN	Error type: short circuit to ground at power stage injector 3
B_MNEV4			EIN	Error type: short circuit to ground at power stage injector 4
B_MNEV5			EIN	Error type: short circuit to ground at power stage injector 5
B_MNEV6			EIN	Error type: short circuit to ground at power stage injector 6
B_MNEV7			EIN	Error type: short circuit to ground at power stage injector 7
B_MNEV8			EIN	Error type: short circuit to ground at power stage injector 8
B_MXEV1			EIN	Error type: short circuit to B+ at power stage injector 1
B_MXEV2			EIN	Error type: short circuit to B+ at power stage injector 2
B_MXEV3			EIN	Error type: short circuit to B+ at power stage injector 3
B_MXEV4			EIN	Error type: short circuit to B+ at power stage injector 4
B_MXEV5			EIN	Error type: short circuit to B+ at power stage injector 5
B_MXEV6			EIN	Error type: short circuit to B+ at power stage injector 6
B_MXEV7			EIN	Error type: short circuit to B+ at power stage injector 7
B_MXEV8			EIN	Error type: short circuit to B+ at power stage injector 8
B_SA	MDRED		EIN	Condition fuel cut-off
B_SIEV1			EIN	Error type: interruption at power stage injector 1
B_SIEV2			EIN	Error type: interruption at power stage injector 2
B_SIEV3			EIN	Error type: interruption at power stage injector 3
B_SIEV4			EIN	Error type: interruption at power stage injector 4
B_SIEV5			EIN	Error type: interruption at power stage injector 5
B_SIEV6			EIN	Error type: interruption at power stage injector 6
B_SIEV7			EIN	Error type: interruption at power stage injector 7
B_SIEV8			EIN	Error type: interruption at power stage injector 8
B_STEND	BBSTT		EIN	condition end of start
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
EVZ_AUSTOT	AEVABZK		EIN	injection cut off pattern total
E_EV1	DEVE		AUS	error flag: injection valve of cyl. 1
E_EV2	DEVE		AUS	error flag: injection valve of cyl. 2
E_EV3	DEVE		AUS	error flag: injection valve of cyl. 3
E_EV4	DEVE		AUS	error flag: injection valve of cyl. 4
E_EV5	DEVE		AUS	error flag: injection valve of cyl. 5



Variable	Source	Type	Description
E_EV6	DEVE	AUS	error flag: injection valve of cyl. 6
E_EV7	DEVE	AUS	error flag: injection valve of cyl. 7
E_EV8	DEVE	AUS	error flag: injection valve of cyl. 8
Z_EV1	DEVE	AUS	cycle flag: injection valve of cyl. 1
Z_EV2	DEVE	AUS	cycle flag: injection valve of cyl. 2
Z_EV3	DEVE	AUS	cycle flag: injection valve of cyl. 3
Z_EV4	DEVE	AUS	cycle flag: injection valve of cyl. 4
Z_EV5	DEVE	AUS	cycle flag: injection valve of cyl. 5
Z_EV6	DEVE	AUS	cycle flag: injection valve of cyl. 6
Z_EV7	DEVE	AUS	cycle flag: injection valve of cyl. 7
Z_EV8	DEVE	AUS	cycle flag: injection valve of cyl. 8

## FW DEVE 6.40 Fixed Values

Parameter	Value	Description
CDTEV1		code word tester: injection valve of cyl. 1
CDTEV2		code word tester: injection valve of cyl. 2
CDTEV3		code word tester: injection valve of cyl. 3
CDTEV4		code word tester: injection valve of cyl. 4
CDTEV5		code word tester: injection valve of cyl. 5
CDTEV6		code word tester: injection valve of cyl. 6
CDTEV7		code word tester: injection valve of cyl. 7
CDTEV8		code word tester: injection valve of cyl. 8
CLAEV1		error class: injector power stage 1
CLAEV2		error class: injector power stage 2
CLAEV3		error class: injector power stage 3
CLAEV4		error class: injector power stage 4
CLAEV5		error class: injector power stage 5
CLAEV6		error class: injector power stage 6
CLAEV7		error class: injector power stage 7
CLAEV8		error class: injector power stage 8
TSFEV1		fault active time: injector of cyl 1
TSFEV2		fault active time: injector of cyl 2
TSFEV3		fault active time: injector of cyl 3
TSFEV4		fault active time: injector of cyl 4
TSFEV5		fault active time: injector of cyl 5
TSFEV6		fault active time: injector of cyl 6
TSFEV7		fault active time: injector of cyl 7
TSFEV8		fault active time: injector of cyl 8
ZYLZA		number of cylinders

## FB DEVE 6.40 Detailed description of function

The precondition for the diagnosis of the EV power stage is the use of a power stage of the type CJ400/CJ920. The detection of a non-plausible state at the power stage and the reading of the kind of error from the IC is described in the section %DECJ.

The kinds of errors from the CJ400-diagnosis are combined according to their effect on the EV for the further processing in other ECU functions. Short circuit to UBat (B\_mxev) or wire disconnection (B\_siev) lead to the EV permanently being closed. With a short circuit to ground (B\_mnev), however, the EV is permanently open.

The cycle flag Z\_ev is set by the CJ400-diagnosis in case of a detected power stage error. The cycle flag is set by this function if it is indicated by the condition B\_desev that a CJ400-diagnosis can be performed and if the EV power stage was active for a certain time. This is ensured by the conditions B\_stend and B\_sa. In addition it is ensured by the byte evz\_austot that no EV power stage was switched off by the cylinder cutout.

--> no powerstage-diagnosis during ECU after-run





Parameter	Source-X	Source-Y	Type	Description
CDCKPE	BLOKNR		KL	Code word CARB: fuel pump relay power stage
CDTKPE			FW	Code word tester: fuel pump relay power stage
CLAKPE			FW	Error class: fuel pump relay power stage
FFTKPE	BLOKNR		KL	Freeze frame table: fuel pump relay power stage
TSFKPE			FW	Fault active time: fuel pump relay power stage
Variable	Source		Type	Description
B_CLKPE			EIN	Condition clear fault path fuel pump relay power stage
B_DESEE	DKOSE		EIN	Diagnosis power stage: entry conditions fulfilled
B_MNKPE			EIN	Condition fault type short circuit to ground of fuel pump power stage detected
B_MXKPE			EIN	fault type short circuit to Ubat of fuel pump power stage detected
B_SIKPE			EIN	Condition for fault type open circuit of fuel pump power stage detected
C_FCMCLR			EIN	system state: reset fault memory
C_JNI	SWADAP		EIN	ECU-condition for intialisation
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
EKPFZ	DEKPE		LOK	Power stage diagnostic EKP relais: counter for dejettering of error
EKPPZ	DEKPE		LOK	Power stage diagnostic EKP relais: counter test puls trigger
E_KPE	DEKPE		AUS	Error flag: fuel pump relay power stage
Z_KPE	DEKPE		AUS	Cycle flag: fuel pump relay power stage

### FW DEKPE 11.11 Fixed Values

Parameter	Value	Description
CDTKPE		Code word tester: fuel pump relay power stage
CLAKPE		Error class: fuel pump relay power stage
TSFKPE		Fault active time: fuel pump relay power stage

**FB DEKPE 11.11 Detailed description of function**

The EKP power stage is switched on as soon as the engine speed impulses are detected. When switching the ignition off via terminal 15 or in case of engine stop the relay power stage is switched off (see description operating modes EKP: AEKP). With this kind of triggering it is not possible to detect a short circuit to ground or a wire disconnection during normal operating, since the ES is not operated in a control state which allows this error detection.

So that the power stage diagnosis can be performed the power stage is switched off by means of a test pulse of max. 250 microsec. duration (this switching time does not yet lead to an opening of the relay contacts). It must be ensured that the 250 microsec. duration is not prolonged unpermissibly by interrupts thus leading to the EKP relay being switched off. The generation of test pulse and the triggering of the EKP-relay power stage is performed in the 100 ms grid; thereafter the EKP-relay triggering follows as is defined in the section %AEKP.

After an engine start (C\_ini =1: engine speed pulses are detected, program changes to normal operating) the counter (EKPPZ) is preset with the starting value EKPPA. The counter is decremented in the 100 ms grid (R\_100), if the condition B\_desee indicates that an error detection is possible from the ES-IC.

Until the counter reaches the value 0 the EKP-relay power stage is triggered via a 250 microsec. pulse. The output of the impulse is always performed once the CJ400-diagnosis module is in the state OK so that a detected error can be read immediately in the ES-IC.

**Setting of the cycle bit Z\_kpe:**

The cycle bit can be set as soon as test pulses were transmitted to the power stage and if it was indicated by the condition B\_desee that an error diagnosis was possible on the power stage IC. After the output of the test pulse the switching possibilities of the power stage have been checked. Once the debouncing counter EKPPZ reaches the value 0 the cycle bit is set. With the setting of the error bit also the cycle bit is set, if a power stage error is detected with the output sequence of the test pulses.

**Setting of the error bit E\_kpe in case of wire disconnection or short circuit to ground:**

If these errors are given at the power stage, it can be detected during the output sequence of the test pulses. For the error debouncing the error bit is not set until the counter EKPPZ was decremented to the value 0. The error type detected last is then entered into the error memory.

**Setting of the error bit E\_kpe in case of short circuit to UBat:**

A short circuit to Ubat can be detected during normal operating. The special error treatment (verification, check of healing) of the EKP-relay power stage takes place in the CJ400-diagnosis module. For the protection of the power stage there is a switch-off of the switching transistor on the IC. This switch-off becomes active if the error type short circuit to Ubat is entered into the CJ400-shift register. The interlock is released by means of an edge change at the power stage input for a another triggering. For error verification and for check of healing this HW-interlock is removed with a pulse lasting for 10 microsec. The ECU software then immediately enables the power stage again.

**Error verification, error healing check wire disconnection and short circuit to ground:**

It must be ensured that the relay contacts do not open during an error verification or a healing check. For this reason it is not possible to use the standard CJ400-verification or -healing check.

For the error verification of the power stage error short circuit to ground the power stage is triggered by the test pulse. If following this an error can be read via the CJ400-diagnosis, this error detection is debounced by means of the counter EKPPZ. Once the counter reaches the count 0 the error bit is set and the detected error type is entered into the error memory.

A healing check can then no longer be performed during the following engine operation. If the power stage is triggered again by the output of the test pulse sequence after a new start and no power stage is detected, then this is considered as a criterion for an error healing. The error bit E\_kpe is reset.

**Setting of the error bit E\_kpe in case of short circuit to UBat:**

A short circuit to Ubat can be detected during normal operating. The special error treatment (verification, check of healing) of the EKP-relay power stage takes place in the CJ400-diagnosis module. For the protection of the power stage there is a switch-off of the switching transistor on the IC. This switch-off becomes active if the error type short circuit to Ubat is entered into the CJ400-shift register. The interlock is released by means of an edge change at the power stage input for a another triggering. For error verification and for check of healing this HW-interlock is removed with a pulse lasting for 10 microsec. The ECU software then immediately enables the power stage again.

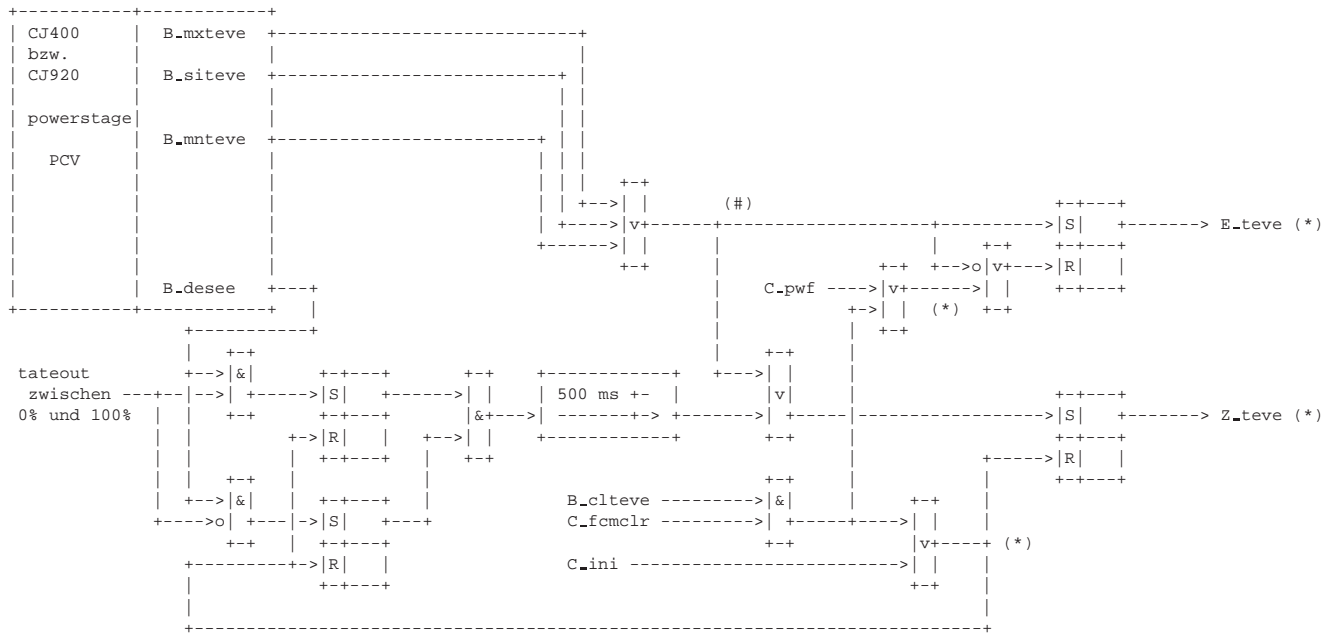
**APP DEKPE 11.11 Application hint**

Filter time in the CJ400 for the setting of the flip-flop in the shift register: 60 to 200  $\mu$ sec

Estimation of the max. capacitance at the power stage output: < 1nF --> then with LA the max. voltage threshold 12 V is reached in 120 usec.

**DTEVE 9.31 Diagnosis; power stage of canister purge valve****DDEF DTEVE 9.31 Function definition**

Diagnostic function for CJ 400 , CJ 920 see %DECJ



(\*) this path is calculated in %DFPM and the flags are flags of the status register  
 (#) this path is calculated in %DECJ

In case of fault:  
 - B\_atev: B\_gasp = TRUE (see %LRA)

Fault code management:

```
status fault-path TEVE: SFPTEVE
Errorflag TEVE: E_teve
Cycleflag TEVE: Z_teve
possible kinds of fault TEVE: B_mxteve
                             B_mnteve
                             B_siteve
```

```
Reset fault path C_fcmlr & B_clteve
Fault path TEVE : CDTTEVE
Fault class TEVE: CLATEVE
Fault rate TEVE: TSFTEVE
CARB Code TEVE: CDCTEVE
Freeze frame Table TEVE: FFTTEVE
```

### ABK DTEVE 9.31 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCTEVE	BLOKNR		KL	code word CARB: canister purge valve power stage
CDTTEVE			FW	code word tester: canister purge valve (power stage)
CLATEVE			FW	fault class: canister purge valve power stage
FFTTEVE	BLOKNR		KL	freeze frame table: canister purge valve (power stage)
TSFTEVE			FW	fault active time: canister purge valve driver stage

Variable	Source	Type	Description
B_ATEV	DTEVE	AUS	condition power stage diagnostic TEV on
B_CLTEVE		EIN	condition clear fault path TEVE
B_DESEE	DKOSE	EIN	Diagnosis power stage: entry conditions fulfilled
B_MNTEVE	DTEVE	AUS	fault type: short circuit ground canister purge valve power stage
B_MXTEVE	DTEVE	AUS	fault type: short circuit Ubat canister purge valve power stage
B_SITEVE	DTEVE	AUS	fault type: cable disconnection of canister purge valve power stage
B_ZTEV	DTEVE	AUS	condition power stage diagnostic TEV closed
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_TEVE	DTEVE	AUS	error flag: canister purge valve power stage
TATEOUT	ATEV	EIN	output duty cycle for canister purge valve
Z_TEVE	DTEVE	AUS	cycle flag: canister purge valve power stage



## FW DTEVE 9.31 Fixed Values

Parameter	Value	Description
CDTTEVE		code word tester: canister purge valve (power stage)
CLATEVE		fault class: canister purge valve power stage
TSFTEVE		fault active time: canister purge valve driver stage

## FB DTEVE 9.31 Detailed description of function

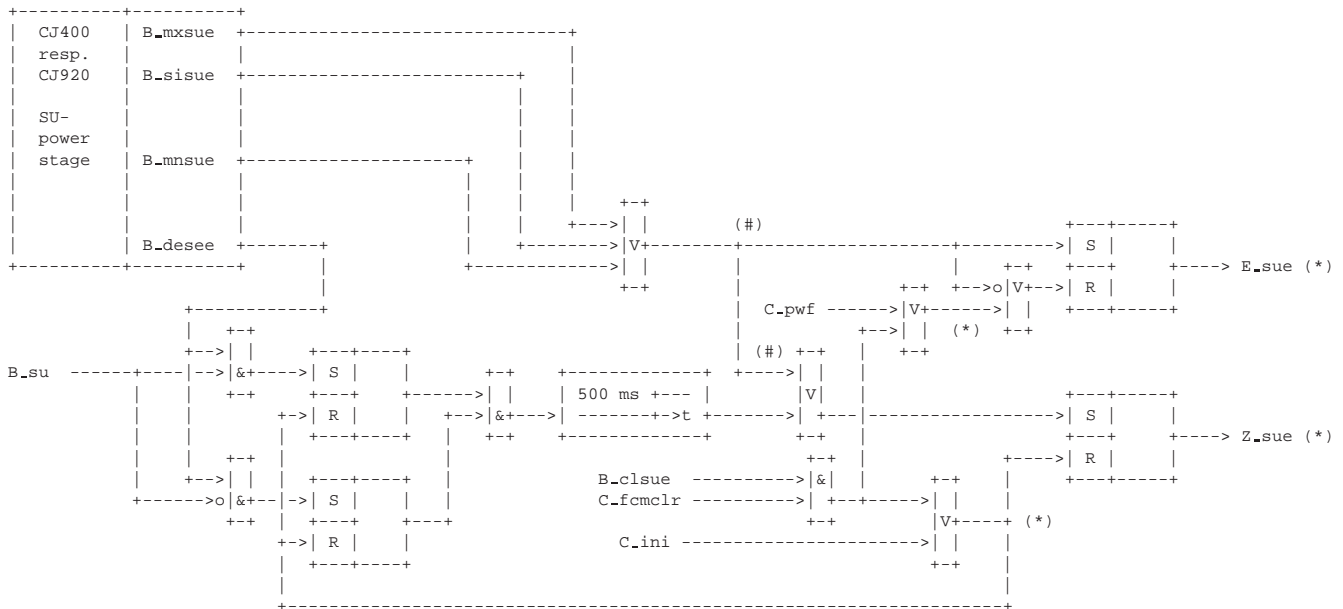
### APP DTEVE 9.31 Application hint

See general application of diagnostic parameters of power stages

## DSUE 7.20 Diagnosis; driver for intake manifold flap

### FDEF DSUE 7.20 Function definition

Diagnosis CJ 400, resp. CJ 920 see %DECJ



(\*) deviant to the description this path is served in the module %DFPM resp. the flags are managed in %DFPM;  
(#) deviant to the description this path is served in the module %DECJ;

### Fault Code Memory Management:

Status fault path SUE: sfpsue  
Error flag SUE: E\_sue  
Cycle flag SUE: Z\_sue  
Fault type SUE: B\_mxsue  
                  B\_mnsue  
                  B\_sisue

Clear fault path: C\_fcmclr & B\_clsue  
Fault path SUE: CDT SUE  
Fault class SUE: CLASUE  
Fault severity SUE: TSFSUE  
Carb-Code SUE: CDCSUE  
Ambient conditions SUE: FFTSUE

## ABK DSUE 7.20 Abbreviations

### FW DSUE 7.20 Fixed Values

Parameter	Value	Description
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## FB DSUE 7.20 Detailed description of function

Precondition for the diagnosis of the SU power stage is the use of a power stage of the type CJ401.  
The detection of not plausible states at the power stage and the reading of the fault type is described in the section %DECJ.

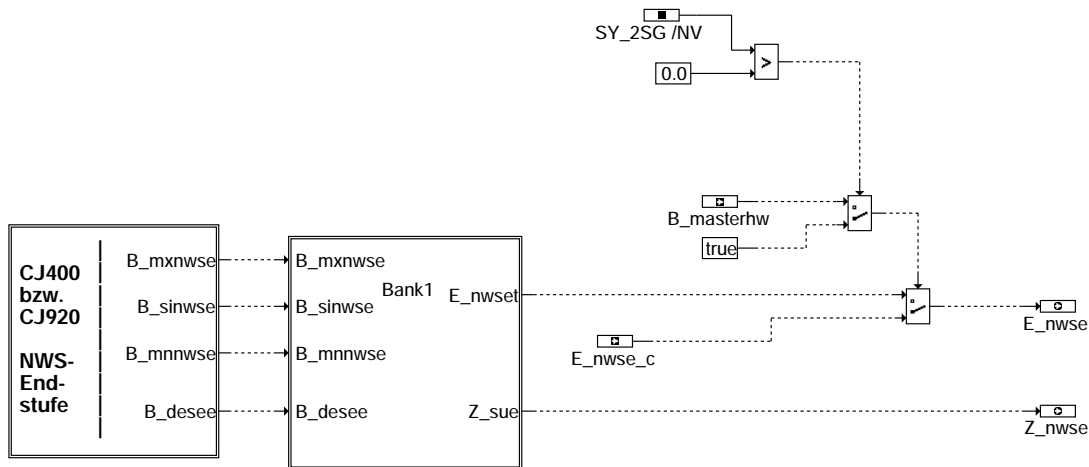
### Setting of the Cycle Flag:

The setting of the cycle flag is performed for one via a fault entry and for the other via a securely tested not due fault. This secure test is given, if both switch-states of the power stage, so switched on and switched off, were reached once. If a fault is detected in one of the states fault verification is activated in %DECJ, which is performed independent of the external power-stage request and which is definitely terminated after approx. 500 ms. Thereafter the cycle bit is set.

## APP DSUE 7.20 Application hint

## DNWSE 5.40 Diagnosis; camshaft control power stage

### FDEF DNWSE 5.40 Function definition



#### dnwse-main

→ B\_mxnwse

→ B\_sinwse

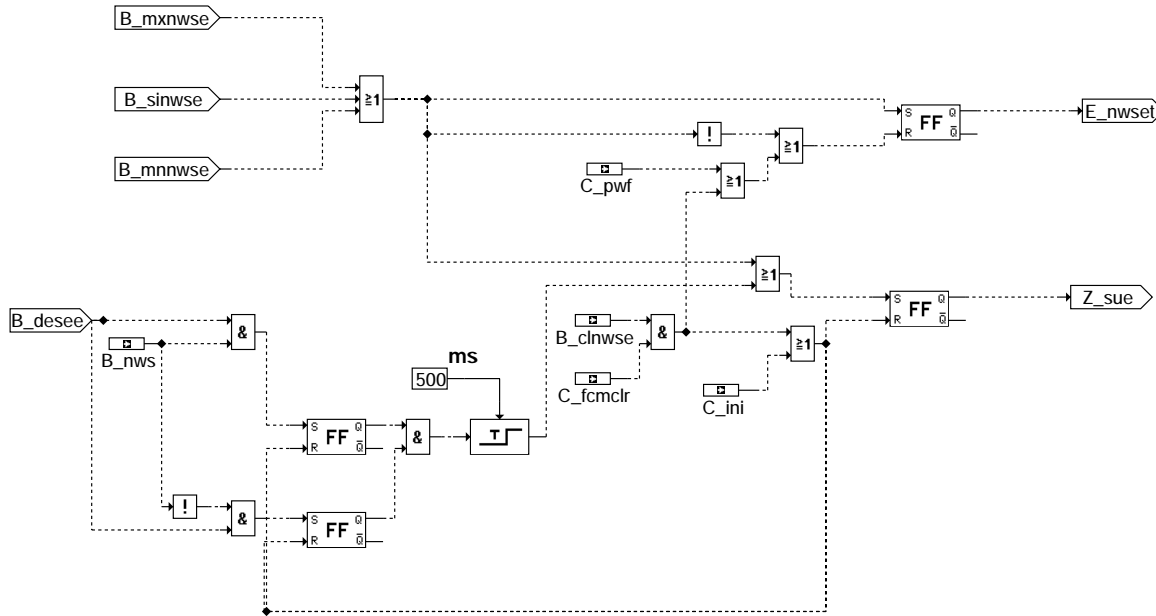
→ B\_mnnwse

→ B\_desee

#### dnwse-dnwse

dnwse-main

dnwse-dnwse



**dnwse-bank1**

Diagnosis CJ 400, or. CJ 920 see %DECJ

(\*) Contrary to the description, this path is served by the module %DFPM and the flags are handled in %DFPM;  
 (#) Contrary to the description, this path is served by the module %DECJ;

**Fault memory management:**

Status fault path NWSE: SFPNWSE  
 Error flag NWSE: E\_nwse  
 Cycle flag NWSE: Z\_nwse  
 Fault type NWSE: B\_mxnwse  
                   B\_mnnwse  
                   B\_sinwse

Reset fault path: C\_fcmlr & B\_clnwse  
 Fault path NWSE : CDTNWSE  
 Fault class NWSE: CLANWSE  
 Fault rate NWSE: TSFNWSE  
 Carb Code NWSE: CDCNWSE  
 Freeze frame table NWSE: PFTNWSE

**ABK DNWSE 5.40 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
SY_2SG			SYS (REF)	system constant 2 motronic systems
Variable	Source		Type	Description
B_CLNWSE			EIN	condition clear fault path camshaft control power stage
B_MASTERHW			EIN	Condition Master-SG corresponding with code-pin (plausible)
B_NWS	NWS		EIN	Condition camshaft control
C_FCMCLR			EIN	system state: reset fault memory
C_INI	SWADAP		EIN	ECU-condition for intialisation
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
E_NWSE	DNWSE		AUS	error flag: power stage of camshaft control valve
E_NWSE_C			EIN	
Z_NWSE	DNWSE		AUS	cycle flag: power stage of camshaft control valve

**FW DNWSE 5.40 Fixed Values**

Parameter	Value	Description
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## FB DNWSE 5.40 Detailed description of function

The requirement for diagnosis of the camshaft control (NWS) power stage is the use of a CJ400 or CJ920 type power stage. Recognition of an implausible state at the power stage and retrieval of the fault type from the IC is described in the section %DECJ.

The fault types from the CJ400 diagnosis are compiled for further processing in other ECU functions according to their effects on the camshaft control. Short circuit to UBat or cable failure result in the camshaft control moving to the retarded end position. In contrast, a short circuit to ground (B\_mnnwse) results in the NWS being constantly at the advanced end position.

The cycle flag Z\_nwse is set in the event of a power stage fault in the CJ400 diagnosis. The cycle flag is set by this function if the condition B\_dese indicates that a CJ400 diagnosis can be performed and if the NWS power stage has been actuated to both states via the condition B\_nws.

## APP DNWSE 5.40 Application hint

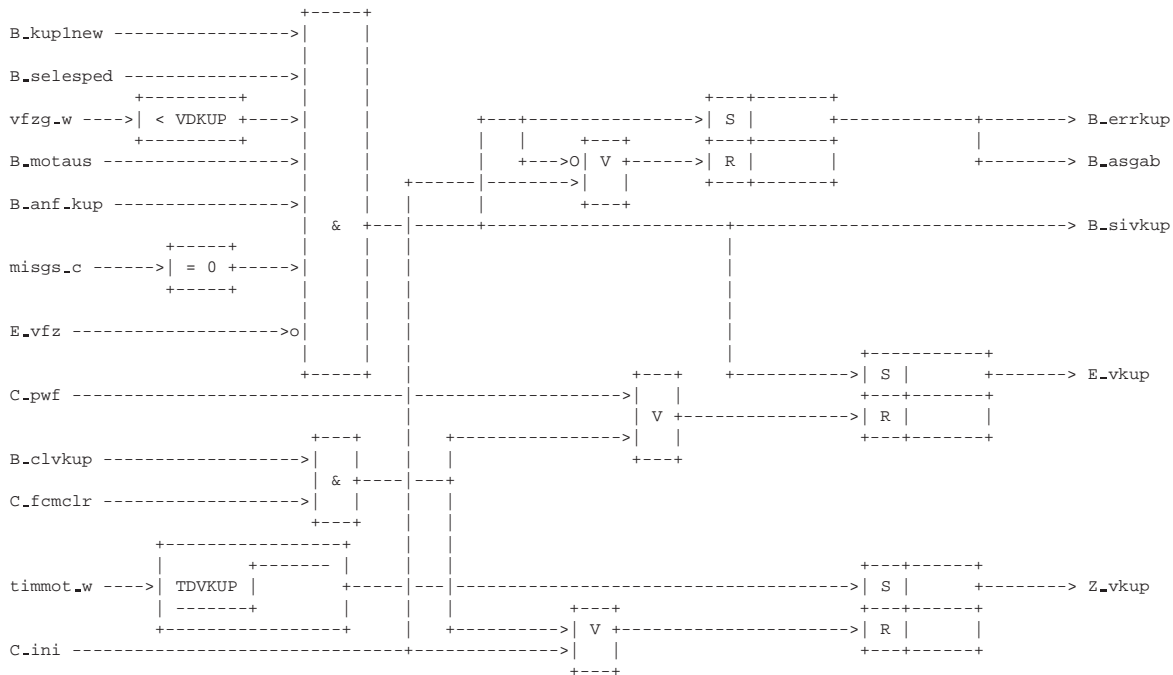
## DVKUP 4.30 Diagnosis; Switch-off engine by electronic clutch control (KUP)

### FDEF DVKUP 4.30 Function definition

Check criteria: B\_motaus = 1 & vfzg\_w < VDKUP & B\_kuplnew = 1 & B\_selesped = 1 & B\_anf\_kup = 1 & misgs\_c = 0 & E\_vfz

Fault cure criteria: C\_pwf = 1 or clear fault memory (C\_fcmclr = 1 & B.clvkup = 1)

Measures: Switch-off injection pulses (see %MDRED)



### Fault management:

status fault path:	SFPVKUP	clear fault path:	C_fcmclr & B.clvkup
error flag:	E_vkup	fault path:	CDTVKUP
cycle flag:	Z_vkup	fault class:	CLAVKUP
fault type:	B_sivkup	fault active time:	TSFVKUP
		CARB-code:	CDCVKUP
		ambient conditions:	FFTVKUP

### ABK DVKUP 4.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCVKUP	BLOKNR		KL	code word CARB: electr. clutch, speed dependent
CDTVKUP			FW	code word tester: electr. clutch, speed dependent
CLAVKUP			FW	fault class: "Engine off"-request from F1-gearbox (KUP)
FFTVKUP	BLOKNR		KL	freeze frame table: "Engine OFF"-request from F1-gearbox (KUP)
TDVKUP			FW	bounce free time for diagnosis electronic clutch control vehicle speed depending
TSFVKUP			FW	fault active time: electr. clutch, speed dependent
VDKUP			FW	vehicle speed threshold for diagn. electr. clutch contr. (engine switch-off)
Variable	Source		Type	Description
B_ANF_KUP			EIN	CAN-signal: bit shift phase (B_ANF_KUP) from el. clutch
B_ASGAB	DVKUP		AUS	Engine shut off by ASG
B_CLVKUP	DVKUP		LOK	condition clear fault path VKUP



Variable	Source	Type	Description
B_ERRKUP	DVKUP	AUS	Condition: engine switch-off caused by electronic clutch
B_KUP1NEW		EIN	condition CAN-KUP1-message received
B_MOTAUS		EIN	CAN-signal: "Engine off"-request from F1-gearbox (KUP)
B_SELESPED		EIN	condition: car with selespeed
B_SGSRED	CAN	EIN	condition: reducing torque intervention for eng. speed synchr. during gear shift
B_SIVKUP	DVKUP	LOK	signal fault: "Engine off"-request from F1-gearbox (KUP)
C_FCMCLR	DVKUP	LOK	system state: reset fault memory
C_INI	DVKUP	LOK	ECU-condition for intialisation
C_PWF	DVKUP	LOK	ECU-condition powerfail initialisation
E_VFZ	EGAG	EIN	Error flag: vehicle speed signal
E_VKUP	DVKUP	LOK	error flag: electr. clutch, speed dependent
MISGS_C		EIN	indicated torque request from SGS
SFPVKUP	DVKUP	LOK	status fault path: "Engine off"-request from F1-gearbox (KUP)
TIMMOT_W	DVKUP	LOK	Timer:time after engine start n>NINI (word)
VFZG_W	GGVFZG	EIN	Vehicle speed
Z_VKUP	DVKUP	LOK	cycle flag: electr. clutch, speed dependent

### FW DVKUP 4.30 Fixed Values

Parameter	Value	Description
CDTVKUP		code word tester: electr. clutch, speed dependent
CLAVKUP		fault class: "Engine off"-request from F1-gearbox (KUP)
TDVKUP		bounce free time for diagnosis electronic clutch control vehicle speed depending
TSFVKUP		fault active time: electr. clutch, speed dependent
VDKUP		vehicle speed threshold for diagn. electr. clutch contr. (engine switch-off)

### FB DVKUP 4.30 Detailed description of function

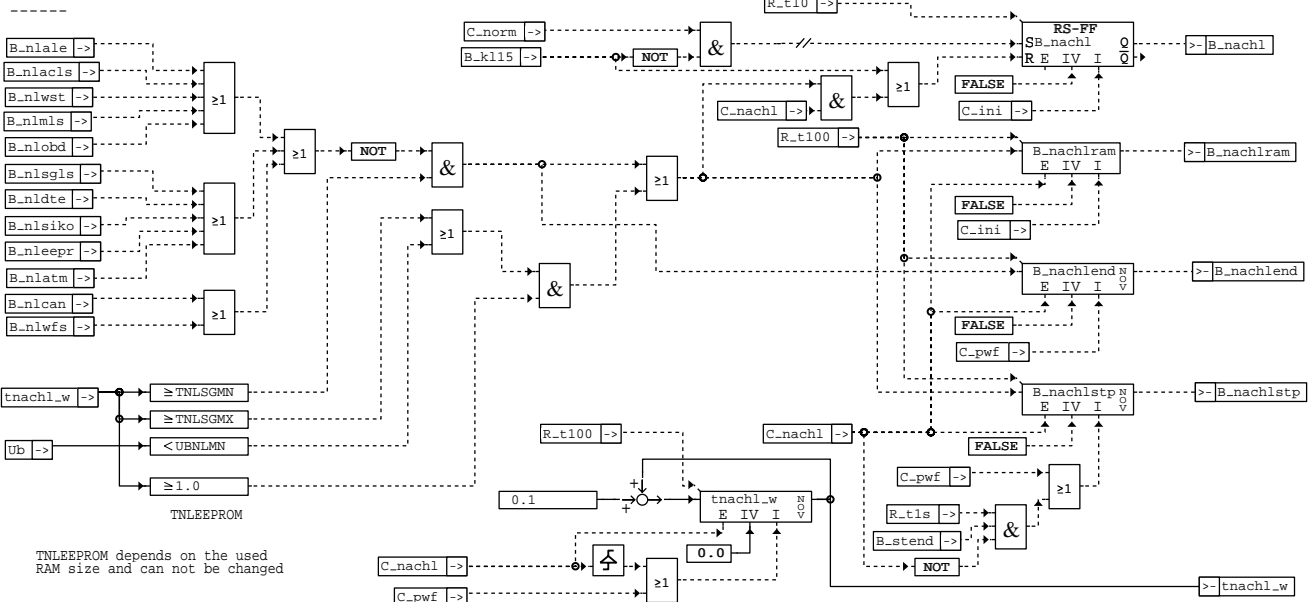
### APP DVKUP 4.30 Application hint

## MOTAUS 5.30 Engine switch-off

### FDEF MOTAUS 5.30 Function definition

The function %MOTAUS describes the switch-off behaviour of the engine electronic control unit which is activated via S\_KL15 (see %SYSCON) once the driver's desire to switch off the engine was detected and which is initiated by the setting of the condition B\_kl15:

MOTAUS



motaus-motaus

### ABK MOTAUS 5.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TNLSGMN			FW	minimum time for ECM-switch-off delay
TNLSGMX			FW	maximum time for ECM-switch-off delay
UBNLMN			FW	Lower limit for Battery target voltage



Variable	Source	Type	Description
B_KL15		EIN	condition ignition switch on
B_NACHL	MOTAUS	AUS	ECU control for ECU switch off delay
B_NACHLEND	MOTAUS	AUS	condition ECU switch off delay regularly finished
B_NACHLRAM	MOTAUS	AUS	Condition ECU switch off with system check
B_NACHLSTP	MOTAUS	AUS	condition ECU switch off delay finished
B_NLACLS		EIN	request for ECM afterrun from the AC-fan-control
B_NLALE	ALE	EIN	request for ECM afterrun from the function ALE
B_NLATM	ATM	EIN	request for ECM exhaust-temp.modell ATM
B_NLCAN		EIN	Condition for ECU switch off delay by demand of CAN
B_NLDTE		EIN	request for ECM afterrun from leak detection
B_NLEEPR		EIN	Condition write of EEPROM during afterrun
B_NLMLS	LFS	EIN	request for ECM afterrun from the engine-fan-control
B_NLOBD		EIN	request for ECM afterrun from OBD
B_NLSGLS		EIN	request for ECM afterrun from the ECM-fan-control
B_NLSIKO		EIN	Condition monitoring of EGAS during afterrun
B_NLWFS		EIN	ECU condition for ECU switch off delay by the immobilizer ECU
B_NLWST	BGTABST	EIN	Request for ECM afterrun for recognition of re-start
B_STEND	BBSTT	EIN	condition end of start
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_NACHL		EIN	ECU condition for ECU switch off delay
C_NORM		EIN	ECU-condition normal engine management operation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
R_T10		EIN	Time schedule 10 ms
R_T100		EIN	Time schedule 100 ms
R_T1S		EIN	Time schedule 1 s
TNACHL_W	MOTAUS	AUS	time of ECU switch off delay
UB	SWADAP	EIN	battery voltage

### FW MOTAUS 5.30 Fixed Values

Parameter	Value	Description
TNLSGMN		minimum time for ECM-switch-off delay
TNLSGMX		maximum time for ECM-switch-off delay
UBNLMN		Lower limit for Battery target voltage

### FB MOTAUS 5.30 Detailed description of function

After the ignition key (B\_kl15=0) was switched off the condition B\_nachl is set during normal operation for the transition to the ECU-switch-off delay. Once the ECU-switch-off delay is terminated the condition B\_nachl is reset. Via this the end of the ECU-switch-off delay is started in the system state control. By setting the Bit B\_nachlram the RAM is released for the RAM test (this effects a loss of the RAM data). After this the ECU is switched off.

With the beginn of switch-off delay the time tnachl\_w is started which gives the current time of the ECU-switch-off delay.

The switching off of the ECU-switch-off delay is activated,

- if no further requests come from the different functions during the switch-off delay, i.e. all B\_nl\* = false, and if the minimum switch-off delay time (TNLSGMN) has passed,
- or - if the maximum switch-off delay time (TNLSGMX) was reached or the battery voltage is under a lower threshold and the minimum switch-off delay time (TNLEEPROM - time to store for EEPROM) has passed.

Is the ECU-switch-off delay executed correctly that means the ECU will be switched off once all requests were taken back- then this is documented in the condition B\_nachlend (permanent RAM) by true. If the condition B\_nachlend is false this indicates an abort of the ECU-switch-off delay by reset, by the ignition key being switched on again or by the maximum switch-off delay time TNSGLMX being reached.

When resetting the bit B\_nachl the bit B\_nachlstp is stored at permanent flag. This bit indicates if the ECU-switch-off was stopped right ( this is the case if no demands exist anymore or TNCEEPROM is gone and maximum ECU-switch-off time TNLSGMX is gone or battery voltage is at a lower threshold). Is B\_nachlstp = FALSE that means it might be KL15 was switched on again.

For the condition of the ECU-switch-off a redundat switch-off track is existing. At the transition of the ECU-switch-off an extern timer is set in the ASIC, which stops the ECU-switch-off after the time is finished.

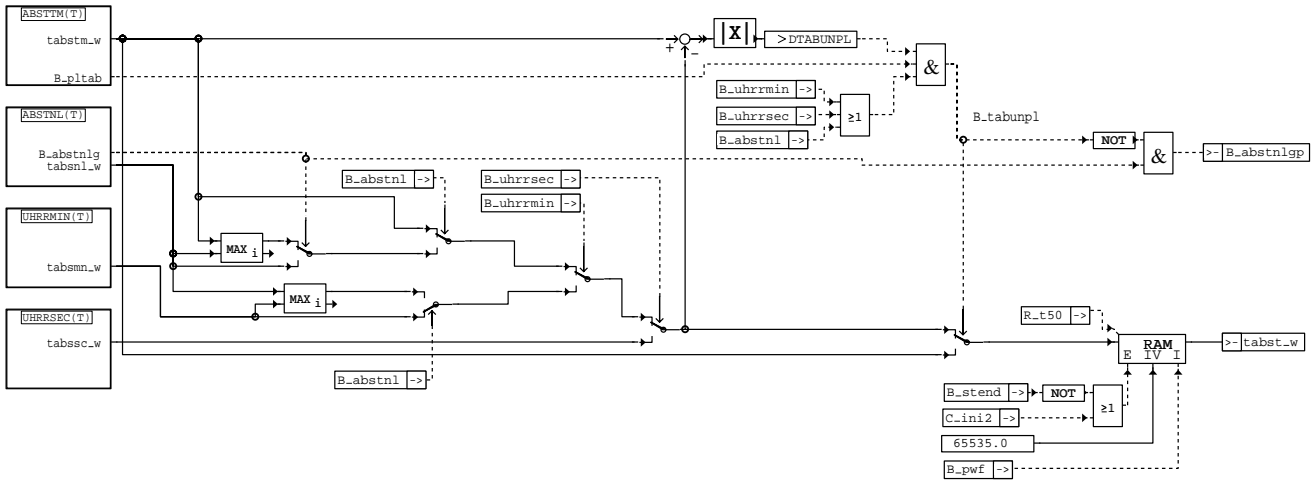
### APP MOTAUS 5.30 Application hint

Data for initial application:

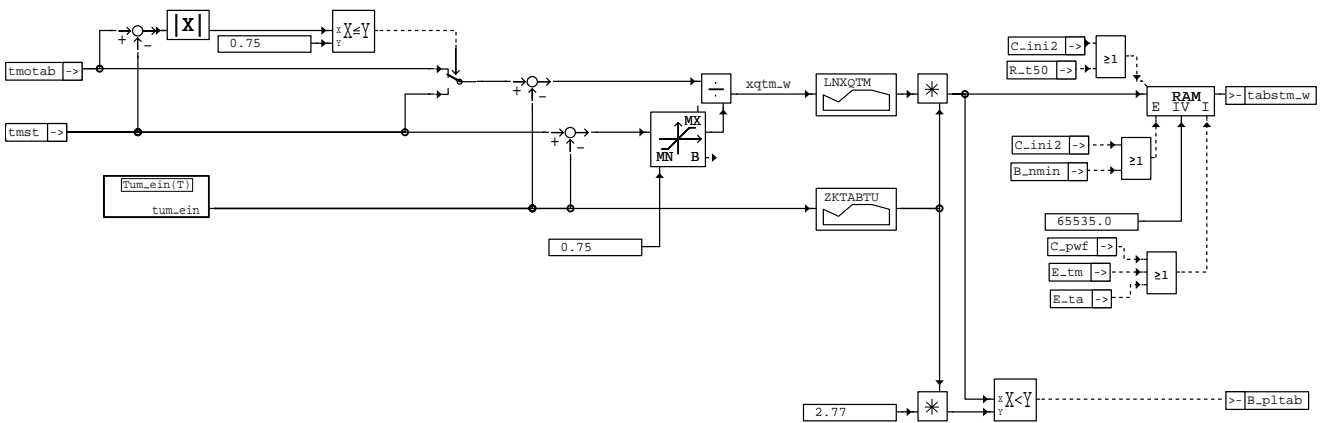
TNLSGMN = 5 sec  
TNLSGMX = 25.6 sec  
UBNLMN = 7 V

## BGTABST 7.10 Calculated variable: cut-off time

### FDEF BGTABST 7.10 Function definition

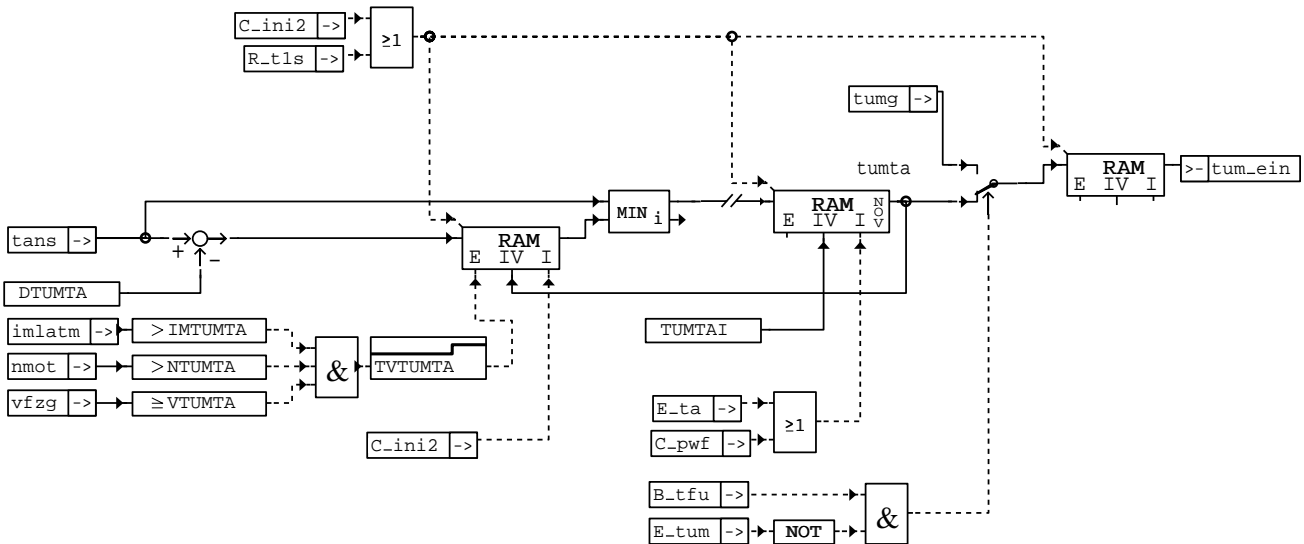


### bgtabst-bgtabst



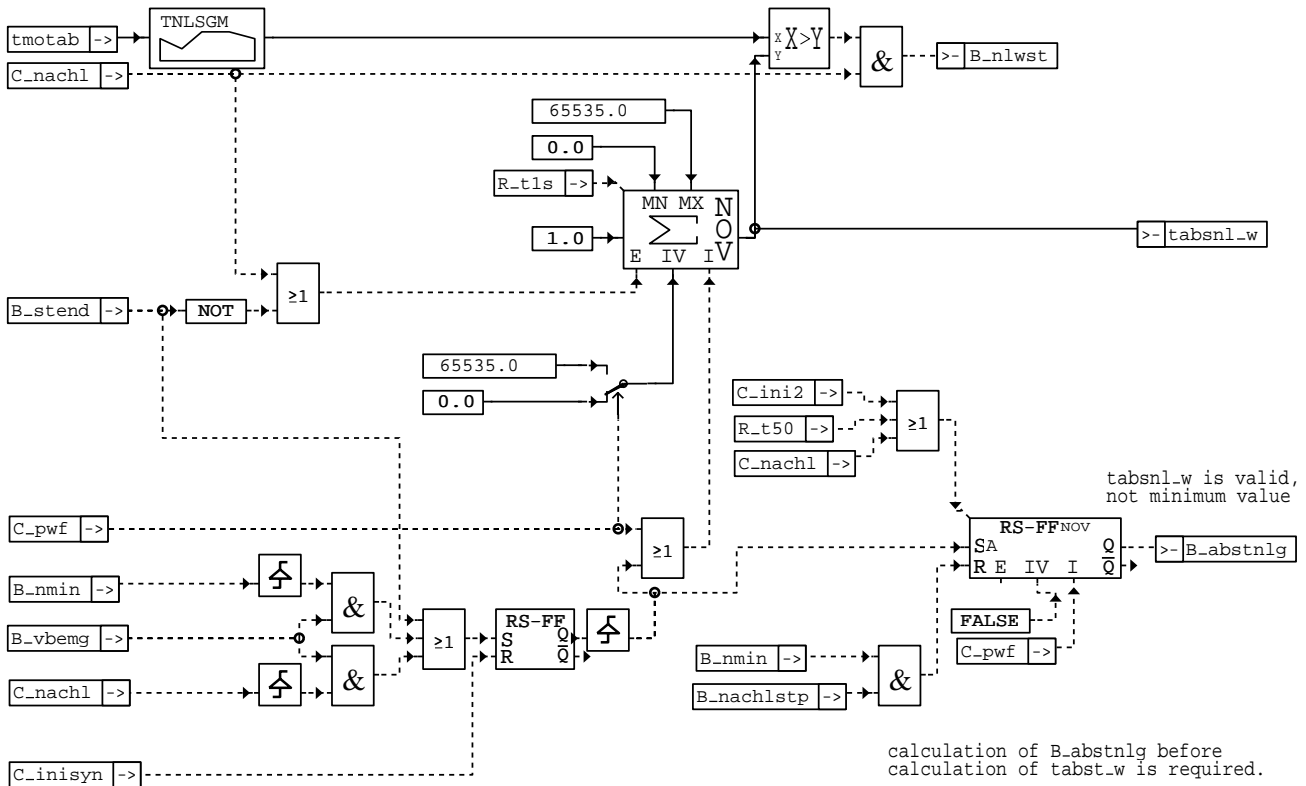
### bgtabst-absttm

Subfunction ABSTTM: Soak time determination from engine cooling



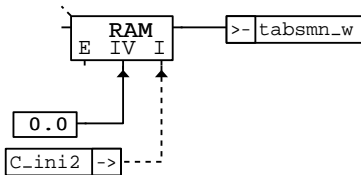
### bgtabst-tum-ein

Subfunction TUM\_EIN: Calculation of the ambient temperature



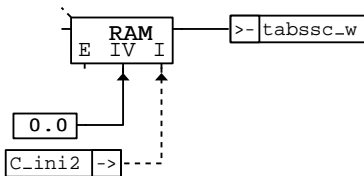
### bgtabst-abstnl

Subfunction ABSTNL: Soak time determination with ECM-afterrunning



### bgtabst-uhrrmin

Subfunction UHRRMIN: Soak time determination with relative minute counter



### bgtabst-uhrrsec

Subfunction UHRRSEC: Soak time determination with relative second counter

### ABK BGTABST 7.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DTABUNPL			FW	threshold soak time unplausible
DTUMTA			FW	offset intake-air temperature -> ambient temperature
IMTUMTA			FW	threshold integrated air mass for determination ambient temperature
LNXTM	XQTM		KL	natural logarithm from temperature quotient
NTUMTA			FW	threshold engine speed for determination ambient temperature
TNLSGM	TMOTAB		KL	Delay time for ECU shut-off
TUMTAI			FW	initial value of ambient temperature
TVTUMTA			FW	delay for threshold velocity for determination ambient temperature



Parameter	Source-X	Source-Y	Type	Description
VTUMTA			FW	threshold velocity for determination ambient temperature
ZKTABTU	TUM_EIN		KL	time constant for engine cooling
Variable	Source		Type	Description
B_ABSTNL	PROKON		EIN	condition soak time calculation via ECM-afterrun
B_ABSTNLG	BGTABST		LOK	condition soak time calculation via ECM-afterrun is valid
B_ABSTNLGP	BGTABST		AUS	condition soak time calculation via ECM-afterrun is valid and plausible
B_NACHLSTP	MOTAUS		EIN	condition ECU switch off delay finished
B_NLWST	BGTABST		AUS	Request for ECM afterrun for recognition of re-start
B_NMIN	GGDPG		EIN	condition lower speed: n < NMIN
B_PLTAB	BGTABST		LOK	condition plausibility check soak time possible
B_PWF			EIN	Condition for powerfail
B_STEND	BBSTT		EIN	condition end of start
B_TABUNPL	BGTABST		LOK	condition soak time unplausible
B_TFU	PROKON		EIN	condition ambient temperature sensor exists
B_UHRRMIN	PROKON		EIN	Condition clock with a relative counter of minutes
B_UHRRSEC	PROKON		EIN	Condition clock with a relative counter of seconds
B_VBEMG	ESSTT		EIN	condition detection of combustion possible
C_JNI2			EIN	ECU-condition for initialisation phase 2
C_JNISYN			EIN	ECU-condition for intialisation of angle synchronization
C_NACHL			EIN	ECU condition for ECU switch off delay
C_PWF	SWADAP		EIN	ECU-condition powerfail initialisation
E_TA	GGTFA		EIN	error flag: TANS
E_TM	GGTFM		EIN	Error flag: engine temperature tmot
E_TUM			EIN	Error Flag: ambient (air) temperature tumg
IMLATM	ATM		EIN	integrated air mass flow from engine start to maximum value
NMOT	SWADAP		EIN	engine speed
R_T1S			EIN	Time schedule 1 s
R_T50			EIN	Time schedule 50 ms
TABSMN_W	BGTABST		LOK	soak time from relative counter of minutes
TABSNL_W	BGTABST		LOK	soak time from ECM-afterrunning
TABSSC_W	BGTABST		LOK	soak time from relative counter of seconds
TABSTM_W	BGTABST		LOK	soak time from engine cooling
TABST_W	BGTABST		AUS	soak time
TANS	SWADAP		EIN	Intake air temperature
TMOTAB	GGTFM		EIN	engine coolant temperature at engine stop or cut-off cranking
TMST	GGTFM		EIN	engine temperature at start
TUMG			EIN	Ambient air temperature
TUMTA	BGTABST		LOK	ambient temperature from intake-air temperature
TUM_EIN	BGTABST		LOK	ambient temperature for soak time calculation
VFZG	SWADAP		EIN	vehicle speed (km/h)
XQTM_W	BGTABST		LOK	temperature quotient

### FW BGTABST 7.10 Fixed Values

Parameter	Value	Description
DTABUNPL		threshold soak time unplausible
DTUMTA		offset intake-air temperature -> ambient temperature
IMTUMTA		threshold integrated air mass for determination ambient temperature
NTUMTA		threshold engine speed for determination ambient temperature
TUMTAI		initial value of ambient temperature
TVTUMTA		delay for threshold velocity for determination ambient temperature
VTUMTA		threshold velocity for determination ambient temperature





## FB BGTABST 7.10 Detailed description of function

The soak time tabst\_w can be determined by different methods depending on the given surroundings. These are defined by the codeword CWUHR. The following methods are distinguished:

1. Soak time determination with relative second counter: A relative second counter is required, that is available either ECM-internal and works permanent, or ECM-external, which works permanent and communication between ECM and counter is possible throughout ECM operation (i.e. via CAN). If these requirements are fulfilled B\_uhrrsec = 1 (bit 1 of CWUHR).
2. Soak time determination with relative minute counter: A relative minute counter is required, that is available either ECM-internal and works permanent, or ECM-external, which works permanent and communication between ECM and counter is possible throughout ECM operation (i.e. via CAN). If these requirements are fulfilled B\_uhrrmin = 1 (bit 0 of CWUHR).
3. Soak time determination with ECM-afterrunning: B\_abstnl = 1 (bit 2 of CWUHR) if ECM-afterrunning is available for determination of short soak times. After the engine is stalled or shut-off a time counter is started at the beginning of ECM-afterrunning. The necessary (permissible) duration of ECM-afterrunning for re-start detection is given in characteristic TNLSGM depending on engine temperature. If the engine is not started within the duration of ECM-afterrunning the time counting will be stopped at the end of afterrunning and the minimum soak time stored in tabsnl\_w. Longer soak time is then detected as described in 5. . If ignition is switched on again within the duration of afterrunning tabsnl\_w is stored and updated until end of start.
4. Soak time determination with relative minute counter and ECM-afterrunning: Combination of 2. and 3.: B\_uhrrmin = 1 and B\_abstnl = 1 (bits 0 and 2 of CWUHR).
5. Soak time determination from engine cooling: If neither relative second counter nor relative minute counter are available for soak time determination longer soak times are determined from engine cooling. Therefore  $xqtm_w = (tmotab - tumta) / (tmst - tumta)$  is calculated. Characteristic LNXQTM contains values for the natural logarithm  $\ln(xqtm_w)$ . Soak time tabstm\_w is then obtained by multiplication of  $\ln(xqtm_w)$  and time constant  $ZKTABTU = f(tumta)$ . The ambient temperature tumta is the difference between tans and DTUMTA. If a sensor for ambient temperature is available, tumg is used instead of tumta.

## APP BGTABST 7.10 Application hint

1. Soak time determination with relative second counter: This method of soak time determination is the most precise and therefore should be preferred. If plausibility test is desired subfunction ABSTTM and threshold for plausibility check DTABUNPL must be applied (see 5.). If no plausibility check within %BGTABST is desired DTABUNPL must be set on its maximum value 65535. This way of soak time determination is not realized in the actual version.
2. Soak time determination with relative minute counter: Application like 1. . If ECM-afterrunning is available, see 4. . This way of soak time determination is not realized in the actual version.
3. Soak time determination with ECM-afterrunning: This method of soak time determination is suitable for detecting short soak times. A combination with a relative minute counter (see 4.) or evaluation of engine cooling (see 5.) is necessary to detect longer soak time. Characteristic TNLSGM in subfunction ABSTNL must contain the desired or permitted duration of ECM-afterrunning in seconds for re-start detection depending on engine temperature.
4. Soak time determination with combination of relative minute counter and ECM-afterrunning: With this method it is possible to determine soak time with a resolution of 1 s during afterrunning and with a resolution of 1 min after that. For application of subfunction ABSTNL see 3. .
5. Soak time determination from engine cooling: This method is less precise than the above described and should be used only if the hardware requirements for these are not fulfilled. Soak time is calculated as multiplication of time constant (depending on ambient temperature) ZKTABTU and natural logarithm of xqtm\_w. The logarithm is calculated via characteristic LNXQTM.

data for LNXQTM:

xqtm	1,000	1,102	1,199	1,352	1,551	1,750	2,000	2,801	4,200	6,000	9,999	16,00
LNXQTM	0,0000	0,0967	0,1816	0,3012	0,4387	0,5596	0,6931	1,0298	1,4348	1,7917	2,3025	2,7725

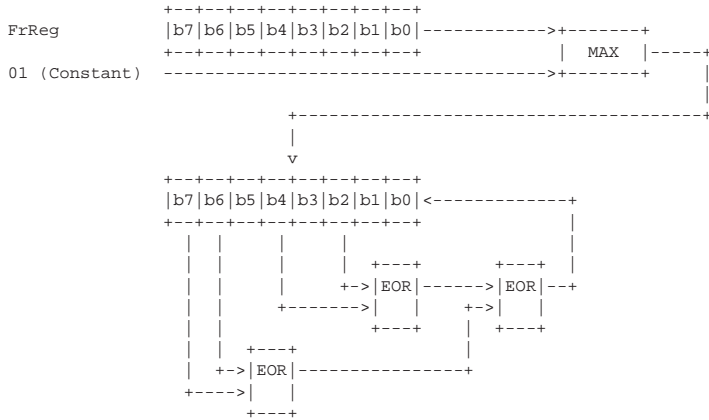
Time constant ZKTABTU must be applied for four ambient temperatures, i.e.  $T_u = -20^\circ\text{C}, 0^\circ\text{C}, 20^\circ\text{C}$  und  $40^\circ\text{C}$ . Therefore measurements of engine temperature after engine is stalled at  $T_1 = tmotab = 80^\circ\text{C}$  are required. The second temperature  $T_2 = tmot$  must be determined after soak time dt for that highest accuracy is desired (i.e. 1800 s).

$$ZKTABTU = dt / \ln((T_1 - T_u) / (T_2 - T_u)) .$$

B\_tfu = 1 (bit 0 of CWTF, see %PROKON) if ambient temperature can be measured directly with a separate sensor. In this case the measured ambient temperature is used for the calculation of soak time. If no sensor for measurement of ambient temperature is available ambient temperature tumta is calculated from intake-air temperature. For initialization of tumta TUMTAI =  $20^\circ\text{C}$  is suggested.

**UMFSEL 1.10 ETS monitoring concept: inquiry selection in the monitoring module(UM)**

**FDEF UMFSEL 1.10 Function definition**



FrReg = MAX(1,FrReg) \* 2 + ((b7 EOR b6) EOR (b4 EOR b2))

Inquiry = LowNibble (FrReg)

**ABK UMFSEL 1.10 Abbreviations**

**FW UMFSEL 1.10 Fixed Values**

Parameter	Value	Description
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**FB UMFSEL 1.10 Detailed description of function**

Random Inquiry Selection in the Supervisor Module for the Inquiry/Response Communication in the Functional Processor

The supervisor module (UM) poses 16 different inquiries via a random generator and expects an unambiguous response to each inquiry from the functional processor (FR). If the FR does not find a correct response, it sends a defined 17th response, which is in any case detected as being incorrect by the UM, since it is incorrect for each possibly posed inquiry.

The inquiries posed to the FR are determined by means of a pseudo-random generator. The random generator is based on an 8-bit shift register with 4 feedback connections, which are connected by an exclusive OR operation. The pseudo-random sequence repeats itself after 255 shift operations. The content of the shift register provides the new inquiry selection in the low-nibble.

If an inquiry is incorrectly responded to, then this inquiry is repeated and the content of the shift register is maintained.

**APP UMFSEL 1.10 Application hint**

**UMFPW 2.10 ETS monitoring concept: flash programming request in the monitoring module (UM)**

**FDEF UMFPW 2.10 Function definition**

**ABK UMFPW 2.10 Abbreviations**

**FW UMFPW 2.10 Fixed Values**

Parameter	Value	Description
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## FB UMFPW 2.10 Detailed description of function

Transition of the monitoring module (UM) into flash programming mode  
-----

The output stages may be shut down during flash programming. This state is not critical from the technical safety viewpoint. Consequently it is permissible that the interface between the function controller (FR) and the monitoring module is not served for an active flash programming.

The following occurs via the evaluation of a defined incorrect response operating as flash programming request information: In this case the inquiry/response communication is interrupted following this defined response for flash programming request. The UM finds itself in an eternal loop in which it disables the output stages. If the flash programming process is completed, a software reset is triggered by the function controller.

Reaction to valid response for normal operation:  
UM in normal operation, enable output stages, error counter - 1

Reaction to another defined response for flash programming:  
UM in flash programming mode, eternal loop until reset with disabled output stages

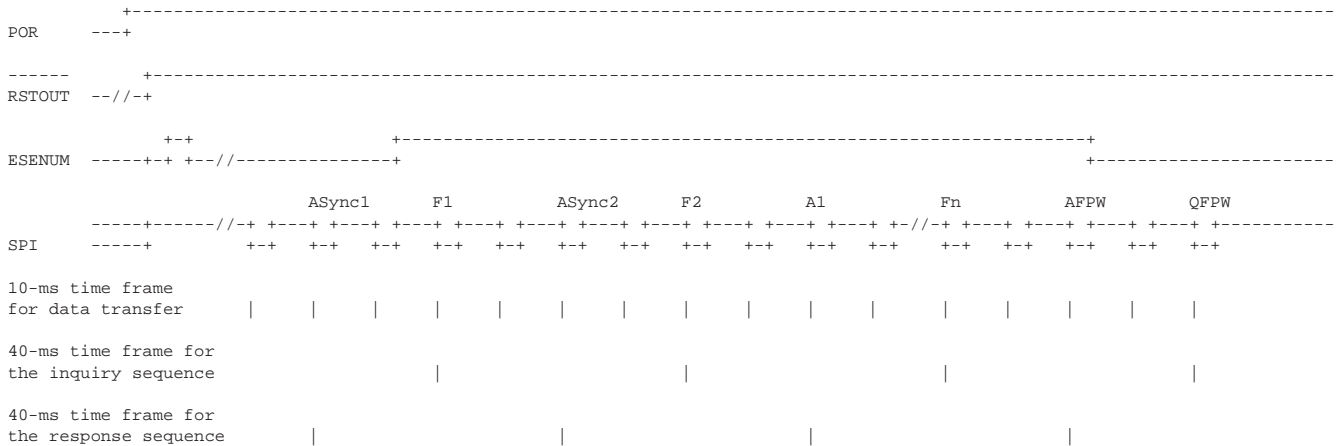
Reaction to invalid response:  
error counter + 1, at final status reset with disabled output stages

Due to the communication between function controller and monitoring module via a synchronous serial interface which the functions computer controls as master, the switchover to flash programming mode in the monitoring module cannot be detected by the missing operation of the interface in the function controller. A defined flash programming request acknowledgement QFPW having the value 0FFh is transmitted for this.

For a correct selection in normal operation, the possibility of a flash programming request AFPW from the function controller is not given. Neither shall the monitoring module erroneously detect a flash programming request AFPW as response from the function controller via the serial interface. It is for this reason that safeguarding the response by additional information at a defined position in the data block as complement of the flash programming request is meaningful.

If the monitoring module is found to be erroneously in the flash programming mode, the function controller triggers a reset after having detected a flash programming request acknowledgement instead of a valid inquiry. If a transmission error leads to the monitoring module not accepting the flash programming request, then there is a normal inquiry in place of the flash programming request acknowledgement. The function controller can, on the basis of this, re-generate the request to go over onto flash programming mode. This delay must be accepted from a possible external flash programming device.

| Flash  
| programming  
| active



POR = Power on reset

RSTOUT = Reset output from the function controller, reset input at the monitoring module

ESENUM = Output stage enable of the monitoring module

SPI = Synchronous serial interface between function controller and monitoring module

ASync1 = First synchronization response from the function controller  
ASync2 = Second synchronization response from the function controller

AFPW = Flash programming request from the function controller  
QFPW = Flash programming acknowledgement from the monitoring module  
F1 = first inquiry from the monitoring module  
F2 = second inquiry from the monitoring module  
Fn = nth inquiry from the monitoring module



**APP UMFPW 2.10 Application hint**

**UMAUSC 1.11 ETS monitoring concept: test of the shut-down path of the monitoring module**

**FDEF UMAUSC 1.11 Function definition**

**ABK UMAUSC 1.11 Abbreviations**

**FW UMAUSC 1.11 Fixed Values**

Parameter	Value	Description
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**FB UMAUSC 1.11 Detailed description of function**

Testing of the shut-down path from the supervising module  
-----

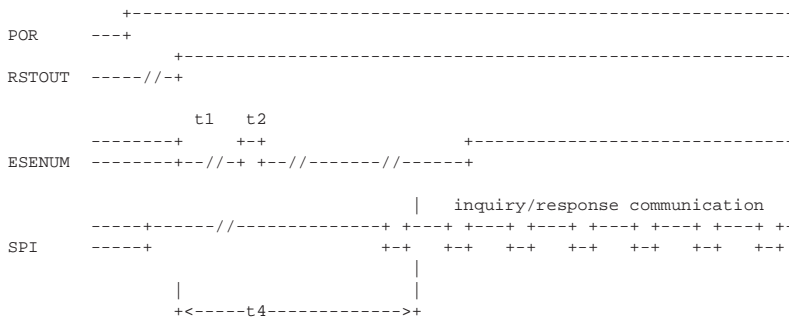
The shut-down path by means of the supervising module (UM) is tested by the function controller (FR) within its supervising function of the supervising module (UM).

Following completion of its initialization, the UM switches the output stages on for a short time and then off again in order that the FR is able to test the shut-down functions of the output stages. This occurs during a defined time window following release of the UM reset.

The status message from an output stage module is checked after the FR has switched on the output stages. The output stage shut-down is thereby evaluated before the FR sends the first information to the UM and the UM enables the output stages.

Following the reset, the communications is established between the function controller and the supervising module as follows:

- the FR terminates its initialization and releases the RSTOUT
- the UM runs through its initialization
- the UM switches the output stages on and off again
- the FR checks the shut-down of the output stages by the UM
- the inquiry/response communication begins (see %UMTOUT)



t1: time for UM initialization  
t2: time for enable of the output stages  
t4: minimum time for requesting the shut-down status message

POR = Power on reset

RSTOUT = Reset output from the function controller, reset input at the monitoring module

ESENUM = Output stage enable of the monitoring module

SPI = Synchronous serial interface between function controller and monitoring module

It is thereby of importance that the initialization sequences are kept short in order to maintain a short period of time prior to enable of the output stages.

**APP UMAUSC 1.11 Application hint**

**UMKOM 2.10 ETS monitoring concept: Inquiry/response communication between UM/FR**

**FDEF UMKOM 2.10 Function definition**

**ABK UMKOM 2.10 Abbreviations**

**FW UMKOM 2.10 Fixed Values**

Parameter	Value	Description
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## FB UMKOM 2.10 Detailed description of function

Inquiry/response communication between the monitoring module and the function controller

- The main flow of information for the monitoring function comprises
- a1) Forwarding the inquiries from the monitoring module (UM) to the function controller (FR)
  - a2) The feedback of the fault counter status from the monitoring module to the function controller
  - b) The response from the function controller to the monitoring module

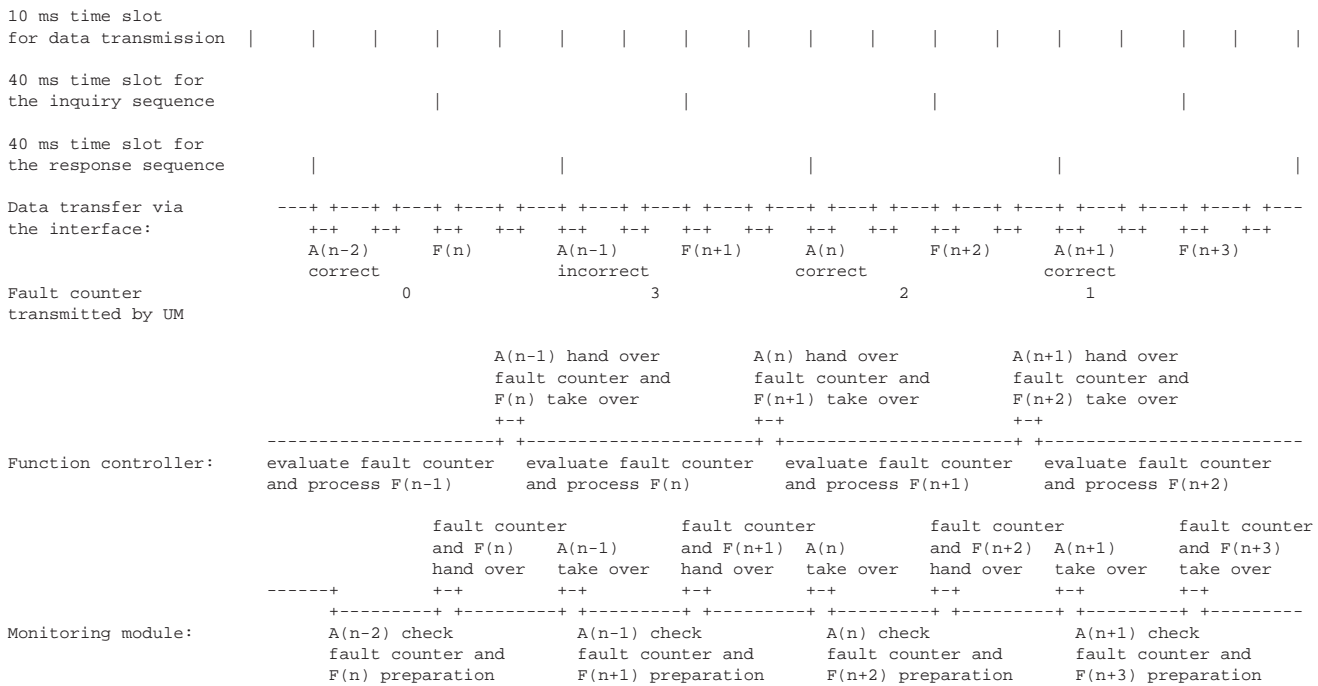
It is meaningful that 16 valid inquiry/response pairs are established for response by the fault reaction in the monitoring module following 5 incorrect responses in succession.  
It is hereby important that the 16 valid inquiries from the monitoring module can be detected exactly by the function controller.

Furthermore, it is meaningful that the response is formed at the 16-bit level at least, in order to obtain a minimum of 65520 impossible responses, i.e. irrespective of the inquiry, as well as the 16 possible responses.  
The responses expected from the inquiries raised shall be defined, i.e. shall not depend on the number of the modules interfacing with the program process control in the FR.  
This means that a conversion of the program process control contents is performed in a meaningful way in the FR.  
In order to do this, a 17th invalid response must be specified at the interface to the monitoring module in addition to the 16 valid responses.

The expectation of a correct response assigned to the inquiry thereby set does not allow an uncontrolled behaviour that performs a cyclic operation of the monitoring module without any appropriate processing in the function controller.

It is meaningful for an optimum utilization of the interface to interleave the inquiries set and the responses outputted, i.e. to obtain the response to the preceding inquiry following the setting of an inquiry and to output the current response in the function controller after setting the subsequent inquiry.  
The provision of an inquiry just received is not possible without a time delay as the monitoring software in the FR is included in evaluation the response.

The FR outputs the response to the preceding inquiry during the processing of the last inquiry. Hence there is regular data transmission and synchronization taking place between the FR and the UM (refer also to %UMTOU).



The inquiries shall not correspond to the expected responses, i.e. if the UM sets the 00, then the response to this should not be 00. The following assignment shall be complied with:

Inquiry	Response
00	12
01	03
02	08
03	04
04	14
05	13
06	15
07	09
08	02
09	00
10	07
11	10
12	05
13	11
14	06
15	01

An internal counter is increased by 3 if the monitoring module receives an incorrect response and which, for a final status of  $\geq 13$ , triggers a defined fault reaction. This fault reaction definitely shuts all output stages down under all circumstances and leads to a transfer to the safe state by this. In addition to this, the monitoring module triggers a software reset at the function controller in parallel to shutting down the output stages, in order to permit a correct restart for limited incorrect response with respect to time.

For errors in the content of the responses, the fault counter in the monitoring module is raised in increments of 3 up to a final status of  $\geq 13$ , or is decremented to 0 for responses which are correct.

In order to keep the time for enabled output stages as short as possible (long off, short on) for permanently present faults and the fault reaction defined by software reset, the fault counters in the function controller and monitoring module are pre-assigned with the status 11 (11 = final status -3 +1, i.e. -3 for increase at fault and +1 for lowering at OK).

An output stage is only then enabled if the communication starts up correctly and the fault counter in the monitoring module is decremented to 10.

In addition to this, the FR must correctly supply the first permanently defined synchronization response in order that the UM gives the output stage release.

If the second permanently defined synchronization response is incorrect, the monitoring module runs immediately from 10 back to its final status of 13 and thereby into the fault reaction.

The first fault counter values transmitted by UM must be correct as well in order that the FR does not run into a fault reaction but rather to decrementing its fault counter.

If the monitoring module receives an incorrect response then it repeats the incorrectly responded inquiry such that inquiry-specific faults lead to a fault reaction.

The inquiry which the monitoring module sends to the function controller is expected again within the defined time slot.

For a detection of the correct value for the fault counter transmitted by the UM, it is permissible to conclude that the UM is working correctly.

The targeted put in of the 17th response which is intentionally and definitely incorrect, the function controller tests the monitoring module by comparing the fault counter of the monitoring module with its own expected value for the fault counter. The function controller thereby then gives a incorrect response in normal operation if the fault counter transmitted by UM of the UM is exactly 0.

If the fault counter of the monitoring module deviates from the expected value from the function controller, then the last response form (correct or incorrect) is repeated. This occurs automatically by inclusion of an incorrect response at a fault counter value of 0 transmitted by the UM. In addition to this, the value expected for the fault counter on the basis of the fault counter transmitted by UM and the expected treatment (+3 for an incorrect or -1 for a correct response) is defined again.

If the fault counter of the monitoring module deviates from the value expected from the function controller, then the FR increases a fault counter by 3, for a final status of 13 of which will also trigger a software reset.

If the expected fault counter status arrives at the function controller then the fault counter is decremented to 0.

The monitoring module information is thereby transferred in one byte:

High-nibble = fault counter status (range of values 0 to 12=0Dh, for flash program acknowledgement 15=0Fh)

Low-nibble = inquiry (range of values 0 to 0Fh)

The RAM cell for the inquiry setting is thereby also assured by the transfer in a common byte with the evaluation of the fault counter information.

Sequence at the beginning with transition to the normal operation state:



10 ms time slot for data transfer																			
40 ms time slot for the inquiry sequence																			
40 ms time slot for the response sequence																			

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	ASync1	F1		ASync2	F2		A1	F3		A2	F4		A3						
fault counter transmitted by UM	correct	10		correct	9		correct	8		correct	7		corr.						

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A3	F5		A4	F6		A5	F7		A6	F8		A7						
fault counter transmitted by UM	correct	6		correct	5		correct	4		correct	3		corr.						

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A7	F9		A8	F10		A9	F11		A10	F12		A11						
fault counter transmitted by UM	correct	2		correct	1		correct	0		incorrect	3		corr.						

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A11	F13		A12	F14		A13	F15		A14	F16		A15						
fault counter transmitted by UM	correct	2		correct	1		correct	0		incorrect	3		corr.						

A10 is then the first incorrect response which the function controller introduces. From this point onwards, every fourth response introduced is incorrect, provided there is no fault otherwise present. The inquiries F10 and F12 as well as F16 and F14 are identical by doing this as those inquiries with incorrect responses are repeated.

Sequence for faults independent of the inquiry:

10 ms time slot for the data transfer																			
40 ms time slot for the inquiry sequence																			
40 ms time slot for response sequence																			

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A1	F3		A2	F4		A3	F5		A4	F6		A5						
fault counter transmitted by UM	correct	0		incorrect	3		incorrect	6		incorrect	9		incorr.						

Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A5	F7		A6															
fault counter transmitted by UM	incorrect	12		incorrect	15 >= 13 --> fault reaction														

The fault is thus active following five incorrect responses.  
The fault reaction time is thus for faults which are independent of the inquiries 5\*40 ms = 200 ms.

Sequence for inquiry-specific faults:



10 ms time slot for data transfer																			
40 ms time slot for the inquiry sequence																			
40 ms time slot for response sequence																			
Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A1		F3=x		A2		F4		A3		F5=x		A4		F6		A5		
fault counter transmitted by UM	correct		1	correct		0	incorrect		3	correct		2	incorr.						
Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A5		F7=x		A6		F8		A7		F9=x		A8		F10		A9		
fault counter transmitted by UM	incorrect		5	correct		4	incorrect		7	correct		6	incorr.						
Data transfer via the interface:	---	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	---
	A9		F11=x		A10		F12		A11		F13=x		A12		F14		A13		
fault counter transmitted by UM	incorrect		9	correct		8	incorrect		11	correct		10	incorr.						
Data transfer via the interface:	---	+																	---
	A13																		
fault counter transmitted by UM	incorrect		13 >= 13																

The fault reaction is active by this for inquiry-specific fault reactions after six incorrect responses at the latest (with correct responses between).  
The fault reaction time is thus for inquiry-specific faults 11\*40 ms = 440 ms.

### APP UMKOM 2.10 Application hint

### UMTOUT 2.10 ETS monitoring concept: time-out for UM/FR-communication

#### FDEF UMTOUT 2.10 Function definition

#### ABK UMTOUT 2.10 Abbreviations

#### FW UMTOUT 2.10 Fixed Values

Parameter	Value	Description
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#### FB UMTOUT 2.10 Detailed description of function

Testing of the timing between monitoring module and function controller

The monitoring module (UM) is hardware which is independent of the function controller (FR) and has its own clock.

The UM makes different inquiries to the FR in an arbitrary sequence which require a correct response within a defined time period. The window watchdog function of the monitoring module is to wait for the response at the right point in time.

Operation is no longer permissible in the event of defective communication between the function controller and monitoring module. This is assured by cyclic triggering of error reactions by the monitoring module as reaction to timing errors.

The error reaction is defined as disabled output stages and software reset, thereby enabling the system to be restarted. This reaction is active immediately for time-out errors.

The time monitoring is to be executed as follows:

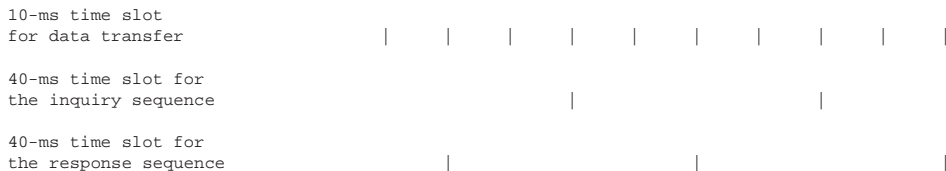
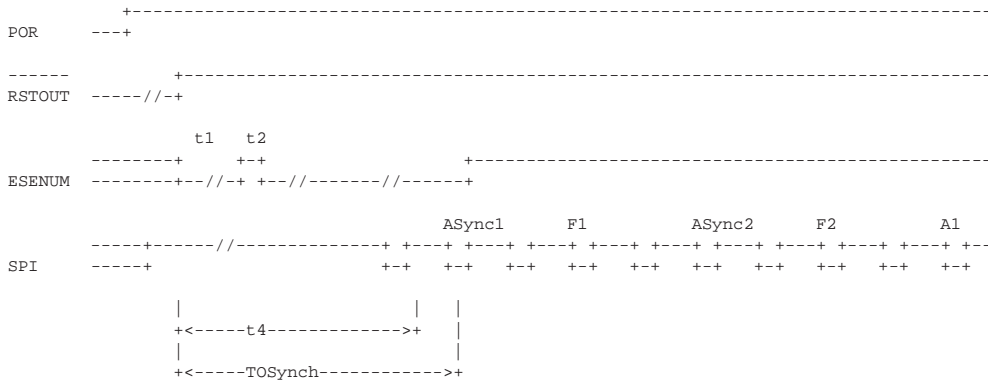
- The monitoring module checks the timing of synchronization by means of the interface operating controlled from the function controller. To do this, time information from the operating system of the monitoring module shall be made available which check for limiting values. This can take place in 10ms, 20ms or 40ms time slot.
- The function controller cannot directly watch the timing via the coupling because of its master function at the interface. The function controller thus tests the contents of the monitoring module inquiry and error counter for plausibility (see %UMKOM)





The communication is established between the function controller and the monitoring module after the reset as follows:

- the FR terminates its initialization and releases the RSTOUT
  - the UM runs through its initialization
  - the UM switches the output stages on and off again (see %UMAUSC)
  - the FR checks the shut-down of the output stages by the UM (see %UMAUSC)
  - the FR sends an initial defined response ASync1
  - the UM synchronizes automatically to the first response from the FR
  - the UM sends its first inquiry following a defined period of time after the response
  - the FR sends its second defined response ASync2
  - the UM sends its second inquiry
  - the FR sends its response to the first inquiry from UM
- The cyclic interlock sequence of inquiry/response is continued



t1: time used to initialize the UM  
t2: time for release of the output stages  
t4: max. time for requesting the shut-down status message  
TOSynch: Synchronization time-out

POR = Power on reset

RSTOUT = Reset output from the function controller, reset input at the monitoring module

ESENUM = Output stage enable of the monitoring module

SPI = Synchronous serial interface between function controller and monitoring module

ASync1 = First synchronization response from the function controller  
ASync2 = Second synchronization response from the function controller  
A1 = Response from the function controller to the first inquiry from the monitoring module  
F1 = First inquiry from the monitoring module  
F2 = Second inquiry from the monitoring module

## APP UMTOUT 2.10 Application hint

## URROM 2.20 ETS monitoring concept: ROM-test

### FDEF URROM 2.20 Function definition

#### ABK URROM 2.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ROMRSTA_LJM			FW	Max. number of resets for error detection in the ROM check during initialization
Variable	Source		Type	Description
ROMRSTC_LJM	URROM		LOK	Counter for resets for error detection in the ROM check during initialization

**FW URROM 2.20 Fixed Values**

Parameter	Value	Description
ROMRSTAJUM		Max. number of resets for error detection in the ROM check during initialization

**FB URROM 2.20 Detailed description of function**

ROM test

-----

Procedure:

- \* Wordwise checksum over the entire ROM range in blocks with assigned check word.

Frequency:

- \* In each driving cycle

Errors that can be detected:

- \* Losses / falsifications of data in memory cells
- \* Readability of memory cells
- \* Faults on address / data lines
- \* Bus faults

ROM test in the function computer

-----

Secondary condition:

- \* Permanent RAM available
- \* Computer afterrunning defined
- \* Time required for ROM test during initialization not acceptable (ROM code e.g. larger than 64 Kbyte)

Point in time:

- \* During a standard initialization prior to enabling the surveillance module
  - \* Repeat check of the discrepant block or all the blocks in the event of several discrepant blocks in case the corresponding information in the permanent RAM contains the identifier "Discrepant ROM test".
- \* During computer afterrunning
  - \* All blocks of the entire ROM range

Error reaction from possible repeated checks:

- \* Output stages become or remain suppressed,
- \* Software reset by transfer of the reset path "SUPERVISOR\_RESET\_ROM",
- \* Repeat of the ROM test,
- \* Engine start-up possible if the ROM has been detected as being error-free

In the event that a checksum error is detected in the ROM test during initialization, then an error counter in the permanent RAM is incremented before a software reset is triggered.

This error counter is deleted again when an error-free condition is detected during the ROM test, or the final status has been reached for the error counter.

Deleting the error counter when the final status has been reached shall also ensure that the foreseen number of ROM tests is carried out again for "Ignition off/on".

This is meaningful in order to make a transition possible into the normal operating mode in case the error is no longer present the next time the ignition is switched on.

A return to the boot block or into the internal ROM when the final status of the error counter is reached enables the Flash content to be programmed again.

This is above all then important if a status that has been programmed by mistake remains in the reset ROM-test loop because of an error in the checksum.

If it is only that a checksum has been incorrectly entered, then although typical by triggering a powerfail, the transition into the normal operating mode is possible by programming the Flash. This does not apply for checksum errors in the range to be cyclically checked (refer to %URMEM).

Error reaction from computer afterrunning:

- \* Repeat of the check during the next standard initialization
- \* Transfer of the identifier "Discrepant ROM test" to the subsequent driving cycle as information in the permanent RAM
  - With the allocation of the block detected as being discrepant, or the information "Several ROM blocks discrepant"

ROM test in the surveillance module

-----

Secondary condition:

- \* Time required for the ROM test during initialization is acceptable (ROM code e.g., not larger than 64 Kbyte)

Point in time:

- \* During standard initialization
  - \* All blocks of the entire ROM range

Error reaction:

- \* Output stages become or remain shutdown,
- \* Output of software reset to the function computer (i.e. system reset),
- \* Repeat of the ROM test,
- \* Engine start-up possible if the ROM is detected as being error-free,
- \* No operation of data transfer to the function computer

**APP URROM 2.20 Application hint****URRAM 2.10 ETS monitoring concept: RAM-test****FDEF URRAM 2.10 Function definition****ABK URRAM 2.10 Abbreviations**

Variable	Source	Type	Description
RST_TV	URMEM	EIN	Variable in the permanent RAM for reset pulse control factor from funct. monito.

**FW URRAM 2.10 Fixed Values**

Parameter	Value	Description
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**FB URRAM 2.10 Detailed description of function**

RAM test

-----

Procedure:

- \* Write the complement of the addresses in the RAM cells to be tested, subsequently test the contents and write the value of the addresses in the RAM cells to be tested, read out, check and clear as the check result is OK.

Frequency:

- \* in each driving cycle

Detectable errors:

- \* setability/clearability of all bits
- \* writability/readability of the memory cells
- \* errors on address/data lines
- \* address decoder errors

RAM test in the function controller

-----

Marginal conditions:

- \* permanent RAM present
- \* controller afterrun defined
- \* time required for RAM test in the initialization is not acceptable (external RAM e.g. larger than 8 Kbyte)

RAM cells to be tested:

- \* CPU RAM (internal RAM and onchip XRAM)
- \* external RAM

Point in time:

- \* in the standard initialization prior to release of the monitoring module
  - \* external RAM only permanent RAM (without OBP RAM) in the initial initialization, i.e. prior to first use
  - \* repeated test for external RAM without permanent RAM in case the information in the permanent RAM does not contain the identifier "RAM test error-free".
  - \* Writability test of the permanent RAM cell for the information "RAM test error-free" by the chess board pattern with the following sequence: save contents, write 55H, test for 55H, write AAH, test for AAH, save back contents.
- \* in the standard initialization following release of the monitoring module and prior to enable of the interrupts
  - \* CPU RAM (internal RAM and onchip XRAM)
- \* in the afterrun following run-down of the operating system and disabling of the interrupts
  - \* external RAM without permanent RAM

Error reaction from initial or standard initialization or repeated testing or writability test:

- \* output stages will be or remain shut down,
- \* software reset,
- \* repetition of the RAM test,
- \* engine start possible if RAM is detected as being error-free,
- \* no serving of the data transfer to the monitoring module

Error reaction from computer afterrun:

- \* repeat test in the next standard initialization
- \* destruction of the identifier "RAM test error-free" at the following drive cycle as information in the permanent RAM

RAM test in the monitoring module

-----

Marginal condition:

- \* time required for RAM test in the initialization acceptable (only internal RAM)

RAM cells to be tested:

- \* CPU RAM (internal RAM and onchip XRAM)

Point in time:

- \* in the standard initialization
  - \* CPU RAM (internal RAM and onchip XRAM)



**Error reaction:**

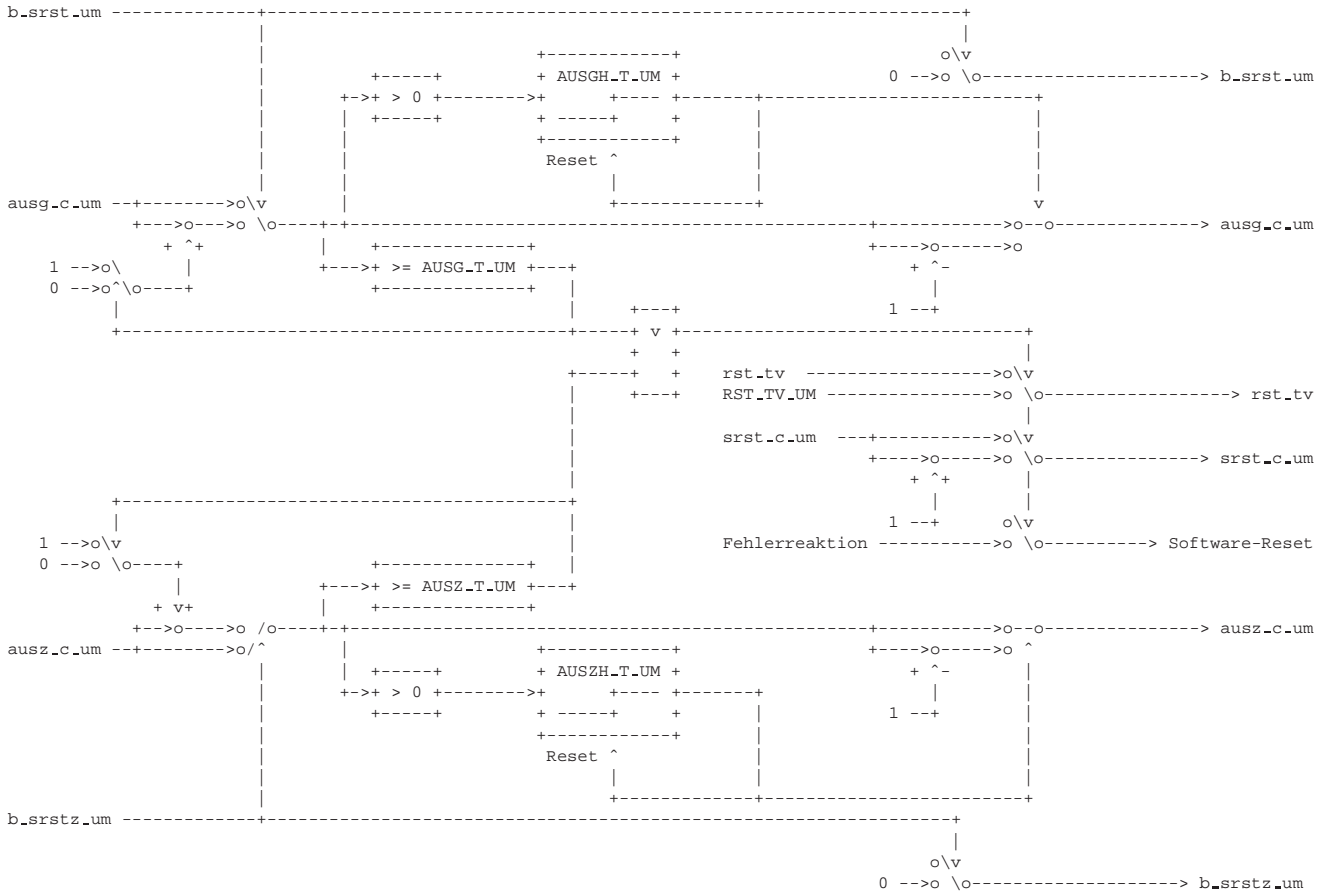
- \* output stages will be or remain shut down,
- \* software reset at the function controller (i.e. system reset),
- \* repetition of the RAM test,
- \* engine start possible if RAM is detected as being error-free,
- \* no serving of the data transfer to the function controller

**APP URRAM 2.10 Application hint**

**URMEM 3.10 ETS monitoring concept: cyclic memory test**

**FDEF URMEM 3.10 Function definition**

Zyklischer Speichertest: Auswertung der Fehlerreaktionsanforderungen im Modul URAUSG



**ABK URMEM 3.10 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
AUSGH.T_UM			FW	Rectification time for faults in cyclic RAM check of watchdog function
AUSG.T_UM			FW	Fault tolerance threshold for the cyclic RAM check in the watchdog function
AUSZH.T_UM			FW	rectification time for faults in cyclic ROM check of watchdog function
AUSZ.T_UM			FW	Fault tolerance threshold for the cyclic ROM check in the watchdog function
RST_TV_UM			FW	Identifier for requesting a reset pulse control factor from function monitoring
WAIT.T_UM			FW	Waiting time for reset pulse duty cycle from the watchdog function
Variable	Source		Type	Description
AUSGH.C_UM	URMEM		LOK	rectification counter for faults in cyclic RAM check of watchdog function
AUSG.C_UM	URMEM		LOK	Fault counter for cyclic RAM check in the watchdog function
AUSZH.C_UM	URMEM		LOK	rectification counter for faults in cyclic ROM check of watchdog function
AUSZ.C_UM	URMEM		LOK	Fault counter for cyclic ROM check in the watchdog function
B_SRSTZ_UM	URMEM		LOK	Software-reset request from the cyclic ROM securing of the watchdog function
B_SRST_UM	URMEM		LOK	Software-reset request from the cyclic RAM securing of the watchdog function
RAM.C_UM	URMEM		LOK	Fault counter in the permanent RAM for RAM-consistency check (diagnosis) in the
ROMZ.C_UM	URMEM		LOK	Fault counter in the permanent RAM for ROM check (diagnosis) in the watchdog fun
RST_TV	URMEM		AUS	Variable in the permanent RAM for reset pulse control factor from funct. monito.
SRST.C_UM	URMEM		LOK	Counter in the permanent RAM for Software-reset (diagnosis) from the watchdog fu
URMCKSCO	URMEM		LOK	checksum over function-monitoring code in cyclic ROM test
URMCKSDA	URMEM		LOK	checksum over function-monitoring data in cyclic ROM test



Variable	Source	Type	Description
URMPATCO	URMEM	LOK	patch address in function-monitoring code for checking cyclic ROM test
WRILC_UM	URMEM	LOK	Fault counter in the permanent RAM for RAM-writability check (diagnosis) in the

### FW URMEM 3.10 Fixed Values

Parameter	Value	Description
AUSGH_T_UM		Rectification time for faults in cyclic RAM check of watchdog function
AUSG_T_UM		Fault tolerance threshold for the cyclic RAM check in the watchdog function
AUSZH_T_UM		rectification time for faults in cyclic ROM check of watchdog function
AUSZ_T_UM		Fault tolerance threshold for the cyclic ROM check in the watchdog function
RST_TV_UM		Identifier for requesting a reset pulse control factor from function monitoring
WAIT_T_UM		Waiting time for reset pulse duty cycle from the watchdog function

### FB URMEM 3.10 Detailed description of function

#### Cyclic memory test

-----

Das Modul muß zur Programm-Ablauf-Kontrolle (siehe %URPAK) beitragen.

Innerhalb dieser Funktion dürfen für Zwischengrößen nur die Temporärvariablen verwendet werden. Diese werden im Befehlstests (siehe %URCPU) ebenso verwendet und sind somit auf Beschreibbarkeit geprüft.

Die Funktion soll im 40ms-Raster abgearbeitet werden.

#### Cyclic RAM safeguarding

-----

A cyclic safeguarding must be performed in the RAM of the monitoring functionality.

A cyclic partial RAM test must therefore take place in the function controller and in the monitoring module via UM functionality, i.e. the RAM cells which are used in the monitoring outside of their generation. Excluded from this can be those RAM cells which are detected as being incorrect on account of their evaluation in the other controller in case of error and without self-diagnosis, or which are safeguarded by other inherent test mechanisms. One example of this is the response from the function controller to the monitoring module. The response will determine the error, irrespective of whether the contents of the RAM cell are incorrect for the response in the function controller or in the monitoring module.

The RAM contents are stored as values together with one's complement during their generation and one of the two values tested for writability.

Test for writability by cyclic RAM test using chess board pattern works in the following way:

- save contents,
- write 55h resp. 5555h, test for 55h resp. 5555h,
- write AAh resp. AAAAh, test for AAh resp. AAAAh,
- save back contents.

A system reset is demanded if the values do not agree.

The double storage as value and complement is tested for consistency prior to further use. The RAM cell in question must therefore also be initialized as value and complement if these are already used in the first run and are tested beforehand. Bit information is thereby supervised by means of a byte variable, whereby the bit information 0 and 1 correspond to defined constants, the values of which are tested for consistency with the bit prior to the bit being used.

Die Variablen für das 1-er Komplement sind unsichtbar, d.h. sie werden nicht über DAMOS bekannt gemacht. Sie tauchen deshalb auch nicht in anderen FDEFs für die Funktionsüberwachung auf.

The error reaction is defined as a system reset in all paths of the cyclic RAM safeguarding, i.e. trigger disable output stages and software reset (function controller) respectively disable output stages and software reset at the function controller (monitoring module).

This enables a restart of the system in the event of interferences.

Triggering a software reset in the function controller takes place in the module URAUSG by means of a software reset demand (safeguarded by a double storage) from the cyclic RAM safeguarding. This software reset demand enables a debouncing and a healing (adjusted to the fault identification) to be chosen. An identifier for "Reset duty cycle" is stored in the permanent RAM before the debounced trigger of a software reset. In the following initialization the ROM- and RAM-check and a defined waiting time before releasing the power stages (resp. the end of the initialization) is activated by this identifier.

In case of a permanent defect in the RAM which no longer permit a writing, or which inhibit a consistency of the data in question, a new system reset is always triggered and the system remains in the error reaction.

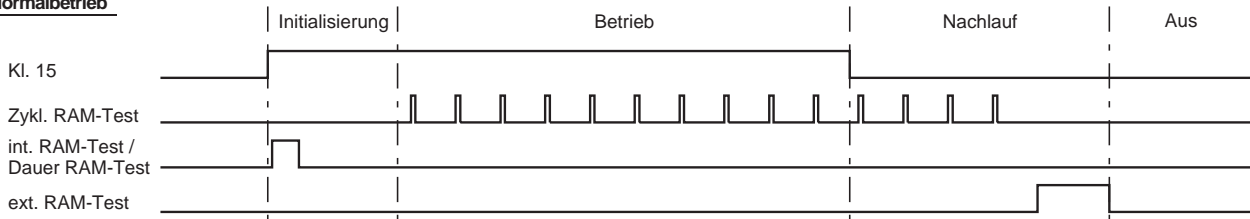
Bei jeder Erkennung eines Beschreibbarkeits-Fehlers wird im Dauer-RAM ein Fehlerzähler (wri\_c\_um) inkrementiert.

Bei jeder Erkennung eines Konsistenz-Fehlers wird im Dauer-RAM ein Fehlerzähler (ram\_c\_um) inkrementiert.

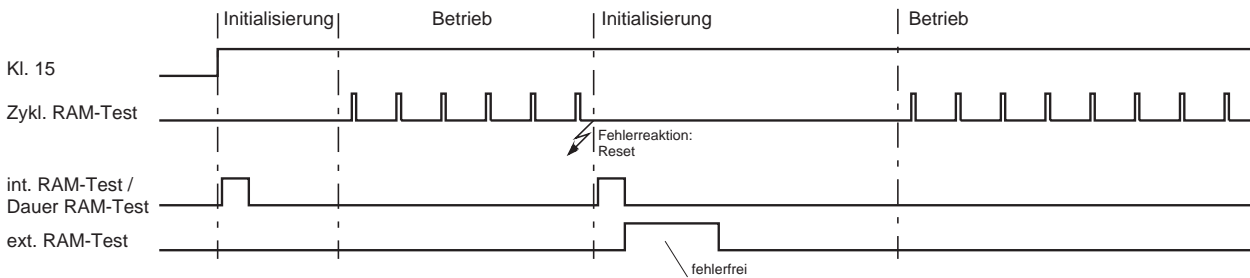
Diese beiden Fehlerzähler im Dauer-RAM werden nur in dieser FDEF genannt, sie sind jedoch Ausgangsgröße für jedes Modul der Funktionsüberwachung, welches der zyklischen RAM-Absicherung unterliegt.



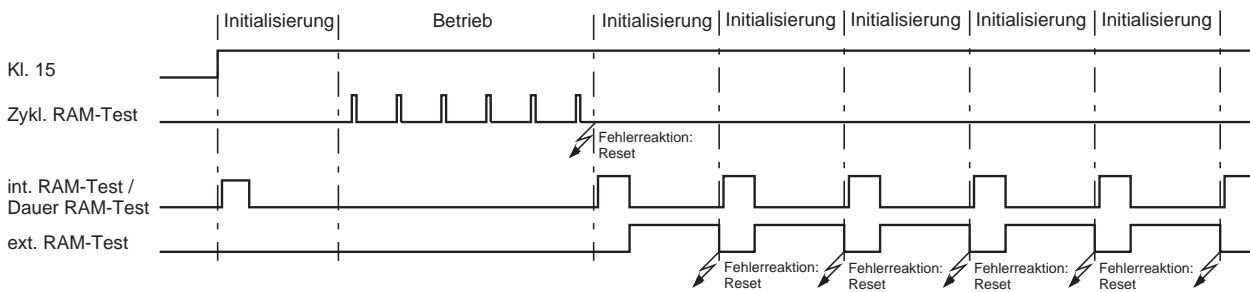
### Normalbetrieb



### Fehlerfall a) sporadischer Fehler im zyklischen RAM-Test



### Fehlerfall b) Fehler im zyklischen RAM-Test



### urmem-folie-2190

#### Cyclic partial ROM check

A cyclic partial check must be performed in the ROM for safeguarding of the monitoring functionality.

A cyclic partial ROM test must therefore take place in the function controller via monitoring functions, i.e. the ROM area which is used by the monitoring and is not otherwise supervised.

Excluded from this can thus be the operation of the interface as well as the compilation of the information for the other controller, as an error here will be found in the other controller whatever the case.

Furthermore, those ROM areas can be excluded which are exclusively used for monitoring the second controller. It is sufficient to test these ROM contents once during the driving cycle in order to prevent sleeping errors in the monitoring.

The monitoring controller can thus be designed to be without cyclic ROM check.

A cyclic ROM check in the monitoring module will only be helpful in the event of double errors, i.e. if, in addition to the error in the monitoring module, a second error occurs that has to be detected from the monitoring module in the function controller.

For the cyclic partial ROM test, the ROM area in question (code and data) are stored either as a whole or in parts with a respective check-sum. The ROM area is cyclically summed word-wise and compared with the applicable check-sum in the ROM.

Ist die Checksumme fehlerhaft, so wird der betroffene ROM-Bereich wiederholt geprüft, damit eine Entprellung der Fehlerreaktion über den fehlerhaften ROM-Bereich erfolgt und nicht durch den anderen eventuell fehlerfreien Bereich zeitlich verlängert wird.

Bei der Bildung der Checksummen wird der betroffene ROM-Bereich unterteilt, so daß im Raster der Überwachungssoftware (40ms) jeweils ein Teil abgearbeitet wird. Hierbei ist zu beachten daß bei einer Fehlererkennung die Drosselklappe nach spätestens 3s (einschließlich Entprellzeit und Rücklaufzeit der Drosselklappe) geschlossen sein muß.

Bei einer Drosselklappen-Schließzeit von 0.4s bei -40°C und einer Entprellung in URAUSG mit 2 µs deshalb ein einzelner ROM-Bereich innerhalb von 1.3s geprüft sein.

Falsifications of the RAM contents used (in particular of the ROM pointer) lead to an error not being detected with certainty and must therefore be supervised separately in the RAM (see cyclic RAM safeguarding).

Zur Überprüfung des zyklischen ROM-Tests kann folgendermaßen Code innerhalb der Funktionsüberwachung abgeändert werden :

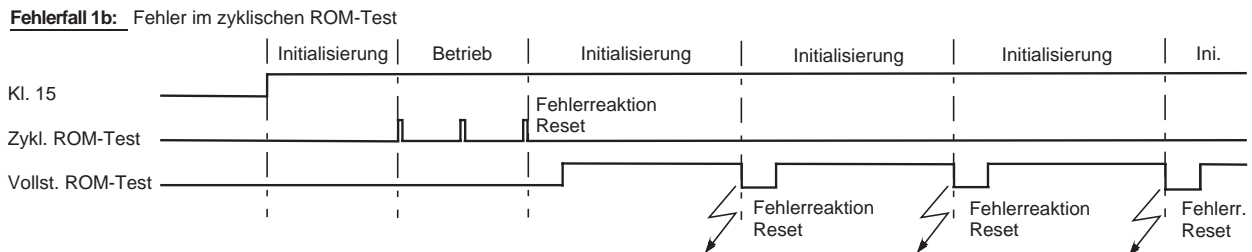
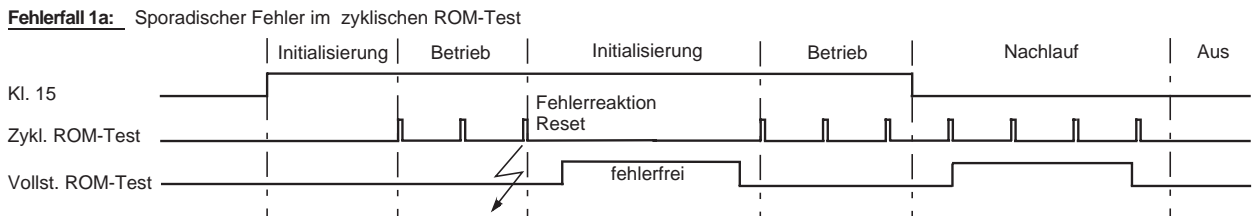
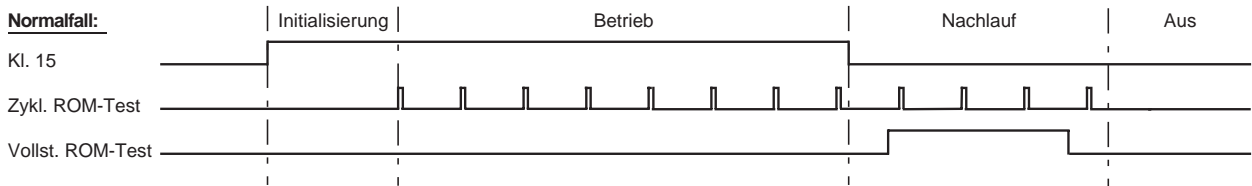
Die durch den zyklischen ROM-Test berechnete Checksumme über die Daten der Funktionsüberwachung wird in der RAM-Zelle urmcksda und die Checksumme über das Programm der Funktionsüberwachung in der RAM-Zelle urmcksco angezeigt. Ferner wird die Adresse eines sog. Dummy-Codes im Programm der Funktionsüberwachung in der RAM-Zelle urmpatco angegeben. An dieser Adresse steht der 2-Byte Befehl 0xE105 (C16x-Maschinenbefehl). Dieser Befehl darf nur in folgende 2-Byte Befehle abgeändert werden : 0xCC00, 0xE005, 0xE104 oder 0xE106 (C16x-Maschinenbefehl). Dadurch ergibt sich eine veränderte Checksumme, die in urmcksco angezeigt wird, bevor dann die Fehlerreaktion ausgelöst wird. Durch Änderungen an Daten der Funktionsüberwachung kann ebenfalls ein Ansprechen des zyklischen ROM-Tests erzwingen werden.

The error reaction is - unlike the complete ROM test in the afterrun - defined as disable output stages and software reset. It enables the system to be restarted in the event of any interferences. Triggering a software reset in the function controller takes place in the module URAUSG by means of a software reset demand (safeguarded by a double storage) from the cyclic ROM safeguarding. This software reset demand enables a debouncing and a healing (adjusted to the fault identification) to be chosen. Zusätzlich wird im Dauer-RAM bei jedem erkannten Fehler ein Fehlerzähler (romz\_c\_um) inkrementiert.

An identifier for "Reset duty cycle" is stored in the permanent RAM before the debounced trigger of a software reset. In the following initialization the ROM- and RAM-check and a defined waiting time before releasing the power stages (resp. the end of the initialization) is activated by this identifier. In case of a permanent defect in the ROM of the monitoring function, a software reset is repeatedly triggered in an attempt to successfully conclude the ROM test in order to resume a normal driving mode.

**Zyklischer ROM-Test:** Checksumme über Ebene 2 mit Beitrag zur Programmablaufkontrolle (PAK). Block 1: Programm ; Block 2: Daten

**Vollständiger ROM-Test:** Checksumme über Programm und Daten in 16K - Blöcken



urmem-folie-2189

### APP URMEM 3.10 Application hint

Die Daten der Funktionsüberwachung sind Bestandteil des Überwachungskonzepts und dürfen nicht beliebig verändert werden.

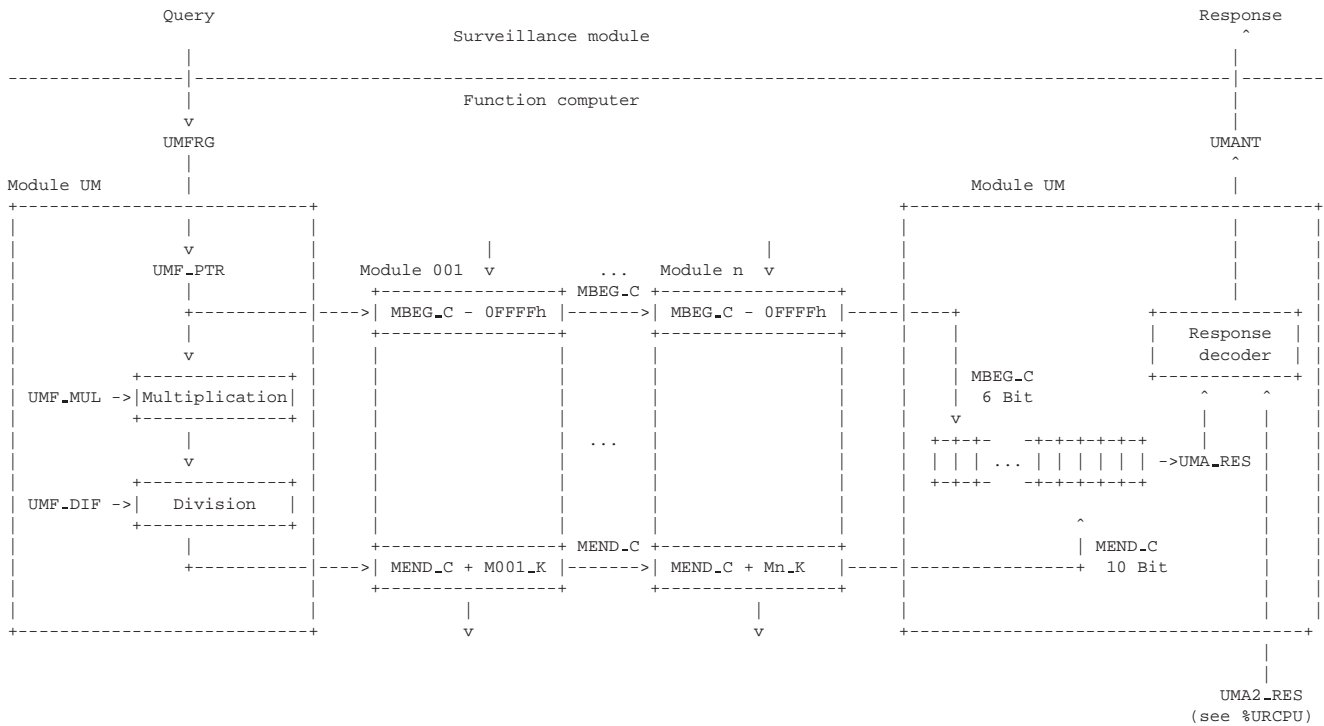
Die Start-, Endadressen und Checksummen des zyklischen RAM- bzw. ROM-Tests müssen zur Serie festgeschrieben und dokumentiert werden.

Bei Folge-Programmständen müssen die Start-, Endadressen und Checksummen kontrolliert bzw. angepaßt werden. Bei veränderter Checksumme müssen die Änderungen in der Funktionsüberwachung bekannt sein - bei gleicher Checksumme gegenüber dem Vorgänger-Programmstand wird die Codegleichheit der Funktionsüberwachung sichergestellt.



## URPAK 1.11 ETS monitoring concept: program flow check

### FDEF URPAK 1.11 Function definition



### ABK URPAK 1.11 Abbreviations

### FW URPAK 1.11 Fixed Values

Parameter	Value	Description
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### FB URPAK 1.11 Detailed description of function

Program process control

Function

Process control ensures cyclic execution of major sections of the program in a defined time frame.

In addition to this, errors shall be detected when working through the command sequences by an application of CPU commands used both at the functional level as well as in functional surveillance for working through the process control.

The following processing is executed for this:

- Defined query recognition from a given input information complex
- Defined arithmetical operations at the beginning after receipt of the query in the major program sections and at the end prior to allocation of the response
- Allocation of the results from the program process control to a defined, correct or incorrect response to the surveillance module

Secondary conditions

A program module is detected of being processed when this has been correctly begun and completed.

This module frame in the form of an initial and final processing must satisfy the following conditions:

- Each pertinent module must be processed within the prescribed time frame. Processing of program process control must be active at all times so as not to permit any error in the processing matrix.
- Any processing not performed for a module may not be substituted by the singular or multiple processing of another module.
- Errors in the program flow of these major program sections must result in a defined error response.
- The program process control must lead to different responses for differing queries, in order to prevent that a unique correctly executed process control will always lead to a correct response.
- Protection of the ROM in defined area must be separate in order to ensure that the program code between initial and final processing is correct (see %URMEM).

The requirements a), b) and c) can be fulfilled by the module-specific definition of individual primary numbers and the continuous cyclic processing of these for formation of a response to a query from the separate HW surveillance module.

The inclusion into program process control of the query raised fulfils the requirement d).





### Realization example

The processing of query, response and the program process control are active in afterrunning and normal operation because the surveillance module (UM) cannot differentiate between afterrunning and normal operation. This applies in the same manner for those modules with a cyclic contribution to the program process control.

The query UMF<sub>RG</sub> set by the surveillance module is checked for validity of the range of values and standardized into a range of values (UMF<sub>PTR</sub>) that can be processed by the program process control. In the event of a violation of the range of values, the incorrectly set query leads to a false response.

The current query UMF<sub>PTR</sub> is looped through all the modules associated with the safety-relevant program and is included in the program process control.

The start-counter module (MBEG<sub>C</sub>) is initialized by the current query (UMF<sub>PTR</sub>) and incremented in each function surveillance module to do this.

The finish-count module (MEND<sub>C</sub>) is initialized with the result from a multiplication and division routine with the current query (UMF<sub>PTR</sub>) as well as constant contributions for process control and increased in each function surveillance module by a module-specific value.

The result UMA<sub>RES</sub> is determined (UMA<sub>RES</sub> = 1024 \* MBEG<sub>C</sub> + MEND<sub>C</sub>) from both of these counters at the end of the program process control. This result is compared with 16 valid results in the response decoder prior to transfer of a new query. There are two constants from function surveillance for each module to do this:

1. Number of recalls in the 40-ms time frame
2. Module-specific code

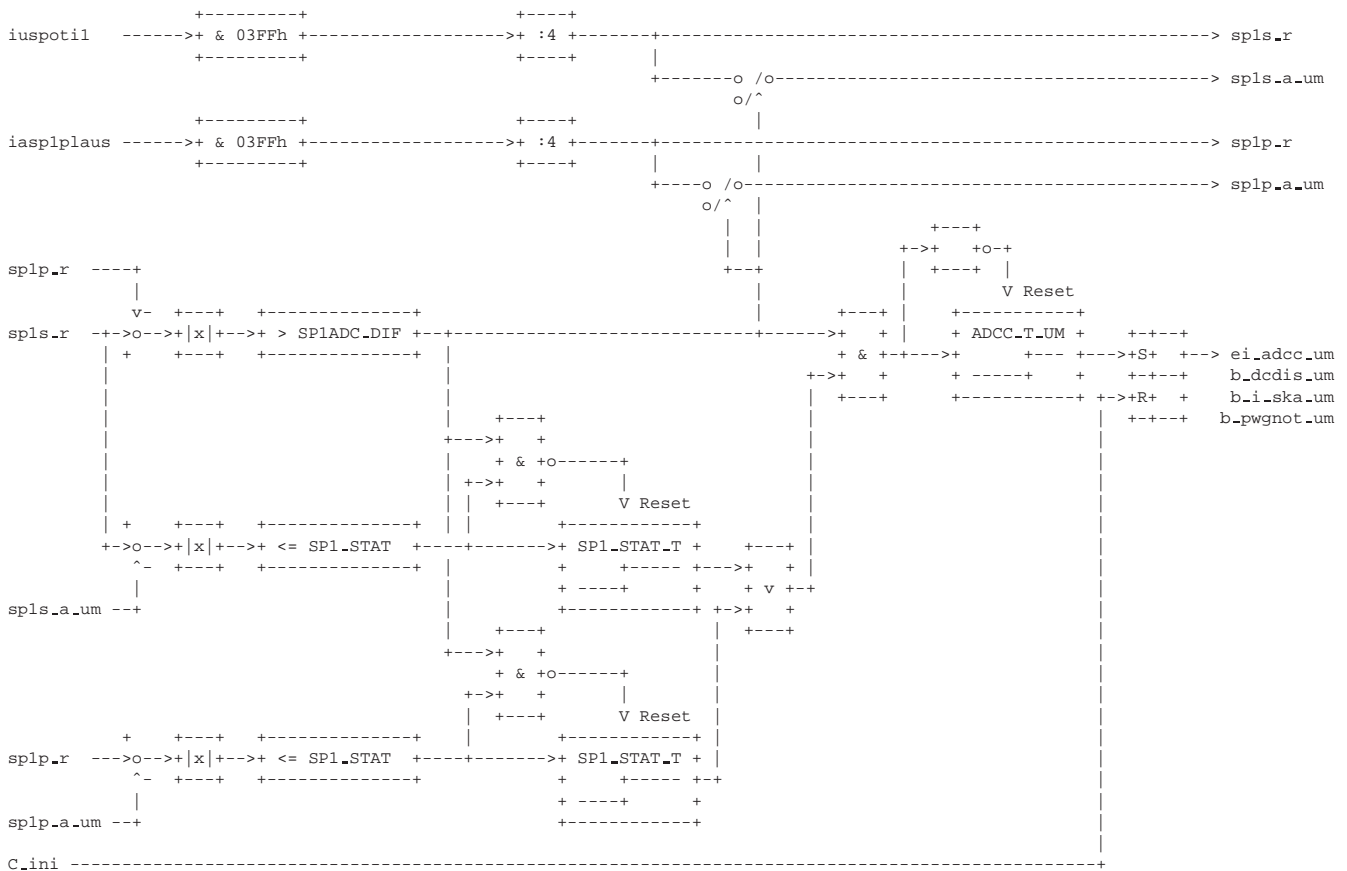
The correct response is provided for a valid result, otherwise a response defined in UMANT as being incorrect.

The transfer of the response determined as well as the query set are transferred every 40 ms during operation. This ensures continuous program process control that is meaningful. A processing cycle is started when a new query is received. This processing is terminated after 40 ms by receipt of the next query.

### APP URPAK 1.11 Application hint

## URADCC 2.20 ETS monitoring concept: test of the AD-converter

### FDEF URADCC 2.20 Function definition



### ABK URADCC 2.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ADCC_T_UM			FW	Error time for ADC values for sp1s that become increasingly less mutually plaus.
SP1ADC_DIF			FW	Max. Diff. bet. setp.-val.poti1 & setp.-val.poti1 from surv. module in sta. case



Parameter	Source-X	Source-Y	Type	Description
SP1_STAT			FW	Bandwidth for detection of sp1s stationary
SP1_STAT_T			FW	Time for detection of sp1s stationary
Variable	Source		Type	Description
ADCC_C_UM	URADCC		LOK	Error counter ADC values for sp1s that become increasingly less mutually plaus.
B_DCDIS_UM	URADCC		AUS	Fault reaction information of the function monitoring
B_LSKA_UM	URADCC		AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_PWGNOTUM	URADCC		AUS	= b_pwgnot_um function monitoring fault response PWG idling (= b_pwgnot_sr)
EI_ADCC_UM	URADCC		AUS	Irreversible error bit for the AD converter surveillance
IASP1PLAUS			EIN	ADC value incl. channel no. setpoint value for poti 1 loop (PWG) from second ADC
IUSPOT1			EIN	ADC value incl. channel number nominal value potentiometer 1 loop (PWG)
SP1P_A_UM	URADCC		LOK	Old 10-ms value for setpoint value poti 1 (PWG) from surveillance module for ADC
SP1P_ST_UM	URADCC		LOK	Stationary counter for setpoint value potentiometer 1 from surveillance module
SP1S_A_UM	URADCC		LOK	Old 10-ms value for setpoint value poti 1 (PWG) for the function surveillance
SP1S_ST_UM	URADCC		LOK	Stationary counter for setpoint value potentiometer 1

### FW URADCC 2.20 Fixed Values

Parameter	Value	Description
ADCC_T_UM		Error time for ADC values for sp1s that become increasingly less mutually plaus.
SP1ADC_DIF		Max. Diff. bet. setp.-val.poti1 & setp.-val.poti1 from surv. module in sta. case
SP1_STAT		Bandwidth for detection of sp1s stationary
SP1_STAT_T		Time for detection of sp1s stationary

### FB URADCC 2.20 Detailed description of function

AD-converter test  
-----

The module must contribute to control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

The ADC value for the reference variable from the pedal value sensor is read in on the function computer by means of the on-chip ADC and a second AD converter that is on a second and different component in the surveillance modulator.

In the case of large pedal dynamics, these values cannot be compared for a bandwidth that is meaningful and it is for this reason, or the difference in threshold is exceeded, that a check is made whether at least one of the two comparison values lies in a defined stationary bandwidth. An error counter only runs when at least one of the two AD values is stationary, the final status of which sets the error information, the error-reaction information as well as the error-reaction idle-speed requirement and the SKA safety fuel shutdown.

The current pedal value is saved at exactly that time as the age for the subsequent processing cycle if a stationary consideration must follow because of the deviation in both AD conversion results.

If both AD-conversion results lie in the permissible bandwidth, then the counter for the stationary consideration and the error-tolerance counter as well, are deleted for the AD-converter error.

The detection for a stationary value is only meaningful and possible when scanning is in the 10-ms time frame.

### APP URADCC 2.20 Application hint

The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
b_dcdis_um		VAR/AUS	Error-reaction info from func. surveillance (shutdown of throttle-valve actuator output stage)
b_i_ska_um		VAR/AUS	Function surveillance error-reaction irreversible SKA (safety fuel shutdown)
b_pwgnot_um		VAR/AUS	Function surveillance error-reaction: PWG idle-speed requirement active
ei_adcc_um		VAR/AUS	Irreversible error bit for monitoring AD converter
iuspot1		VAR/EIN	ADC value incl. channel number setpoint-value potentiometer 1
iasplplaus		VAR/EIN	ADC value incl. channel number setpoint-value potentiometer 1 from surveillance module
sp1s_r		VAR/TMP	Temporary current setpoint-value potentiometer 1-value for the function surveillance
sp1p_r		VAR/TMP	Temporary current setpoint-value potentiometer 1-value from surveillance module for the ADC test
sp1s_a_um		VAR/LOK	Old value for setpoint-value potentiometer 1 for function surveillance
sp1p_a_um		VAR/LOK	Old Value for setpoint-value potentiometer 1 from the surveillance module for the ADC test
adcc_c_um		VAR/LOK	Error counter ADC values that are not mutually plausible for sp1s
sp1s_st_um		VAR/LOK	Stationary counter for sp1s_r
sp1p_st_um		VAR/LOK	Stationary counter for sp1p_r

Label	Dependency	Type	Designation
ADCC_T_UM		FW	Error time for ADC values for sp1s that are not mutually plausible
SP1_STAT		FW	Bandwidth for detection of sp1s stationary
SP1_STAT_T		FW	Time for detection of sp1s stationary
SP1ADC_DIF		FW	Maximum difference between sp1s_r and sp1p_r in the stationary case



## FB URCPU 4.11 Detailed description of function

Instruction test with Level 2'

This section describes the instruction test with the help of Level 2'. Level 2' is a image of Level 2, which is formed from the following components:

%UFFGRC	Cruise control monitoring for function monitoring
%UFMSRC	MSR monitoring for function monitoring
%UFMZUL	Permissible torque for function monitoring
%UFMZP	Torque filter for function monitoring
%UFMIST	Actual torque for function monitoring
%UFMVER	Torque comparison for function monitoring
%UFREAC	Fault reaction monitoring for function monitoring

The reason for introducing this transparent instruction test by means of the safety-relevant torque comparison in Level 2 is, to detect an incorrect processing at Level 2. Without the instruction test in Level 2', a incorrect processing of the monitoring function, as executed in Level 2, cannot be detected with certainty. It would thereby be problematical if the function monitoring is active without being detected as such. An active function monitoring which is incorrect becomes apparent in the fault reaction and is thereby detected.

It is assured by the instruction test over the monitoring function that the instructions used here are processed correctly in the test case. Through the inclusion of the performed test results in forming the response for the monitoring module, i.e. in the monitoring module, the test is performed for the instruction test running correctly in a separate intelligent component. Inquiry-specific test data are thereby selected (refer also to %UMKOM, %UMFSEL), which act as input signals for the Level 2'. The execution of the instruction test in its own RAM and ROM areas thereby lead to the function monitoring running without being influenced by the instruction test itself. A utilization of the sub-programs from Level 2 (setpoint search, interpolation) is thereby meaningful.

Dependent on the inquiry set from the monitoring module, a permanently defined set of test data is specified for the Level 2'.

All variables used in the instruction test, i.e. those local variables are superimposed with test data as well, in order to reach a defined result.

The test data are chosen such that the differing torque interventions will be effective as a function of the inquiries set. Taking the nominal torque into account in the response contribution thereby leads to each nominal torque formation path being included in the response regardless of the inquiry set, and hence to a fault detection in the event of a fault which is independent of the inquiry.

The 16-bit response contribution `uma2_res` is determined as follows:

```
uma2_res = word (mped_uc) + word (mmsr_uc) + word (mfgr_uc) + word (mzfo_uc) - word (mi_uc) + word (mver_c_uc)
          + 256* reac_c1_uc + 2048* reac_c2_uc + 16384 (in case b_i_ska_uc=1)
and
uma2_res = word (mped_uc) + word (mmsr_uc) + word (mfgr_uc) + word (mzfo_uc) - word (mi_uc) + word (mver_c_uc)
          + 256* reac_c1_uc + 2048* reac_c2_uc + 0 (in case b_i_ska_uc=0)
```

This response contribution must vary according to the specific inquiry. It is requested in addition for the conversion into a valid response.

By this, the 16-bit contribution of the program flow check `uma_res` and the 16-bit contribution of the instruction test `uma2_res` are required with exact bit correctness as 32-bit information for decoding into a correct response.

## APP URCPU 4.11 Application hint

The selection of the test data is made such that fault states are set.

Each monitoring path must be operated as often as possible at intervals which are as short as possible and the result must flow into the formation of the response.

After freezing the data in Level 2, the data from Level 2' shall follow as required.

## DUR 1.22 Diagnosis from computer monitoring

### FDEF DUR 1.22 Function definition





## ABK DUR 1.22 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCURRAM	BLOKNR		KL	Code word CARB: monitoring of the controller: RAM
CDCURROM	BLOKNR		KL	Code word CARB: monitoring of the controller: ROM
CDCURRST	BLOKNR		KL	Code word CARB: monitoring of the controller: Reset
CDKURRAM			FW	Code word customer: monitoring of the controller: RAM
CDKURROM			FW	Code word customer: monitoring of the controller: ROM
CDKURRST			FW	Code word customer: monitoring of the controller: Reset
CDTURRAM			FW	Code word tester: monitoring of the controller: RAM
CDTURROM			FW	Code word tester: monitoring of the controller: ROM
CDTURRST			FW	Code word tester: monitoring of the controller: Reset
CLAURRAM			FW	Fault class: monitoring of the controller: RAM
CLAURROM			FW	Fault class: monitoring of the controller: ROM
CLAURRST			FW	Fault class: monitoring of the controller: Reset
FFTURRAM	BLOKNR		KL	Freeze frame table: monitoring of the controller: RAM
FFTURROM	BLOKNR		KL	Freeze frame table: monitoring of the controller: ROM
FFTURRST	BLOKNR		KL	Freeze frame table: monitoring of the controller: Reset
TSFURRAM			FW	Fault active time: monitoring of the controller: RAM
TSFURROM			FW	Fault active time: monitoring of the controller: ROM
TSFURRST			FW	Fault active time: monitoring of the controller: Reset

Variable	Source	Type	Description
B_CLURRAM		EIN	Flag for clearance: monitoring of the controller: RAM
B_CLURROM		EIN	Flag for clearance: monitoring of the controller: ROM
B_CLURRST		EIN	Flag for clearance: monitoring of the controller: Reset
B_NPURRAM	DUR	AUS	fault type not plaus.: monitoring of the controller: RAM
B_NPURROM	DUR	AUS	fault type not plaus.: monitoring of the controller: ROM
B_NPURRST	DUR	AUS	fault type not plaus.: monitoring of the controller: Reset
E_URRAM	DUR	AUS	error flag: monitoring of the controller: RAM
E_URROM	DUR	AUS	error flag: monitoring of the controller: ROM
E_URRST	DUR	AUS	Error flag: monitoring of the controller: Reset
RSTPFAD	DUR	AUS	Reset-path as environment condition for the diagnosis of processor monitoring
SFPURRAM	DUR	AUS	status word: monitoring of the controller: RAM
SFPURROM	DUR	AUS	status word: monitoring of the controller: ROM
SFPURRST	DUR	AUS	status word: monitoring of the controller: Reset
Z_URRAM	DUR	AUS	cycle flag: monitoring of the controller: RAM
Z_URROM	DUR	AUS	cycle flag: monitoring of the controller: ROM
Z_URRST	DUR	AUS	cycle flag: monitoring of the controller: Reset

## FW DUR 1.22 Fixed Values

Parameter	Value	Description
CDKURRAM		Code word customer: monitoring of the controller: RAM
CDKURROM		Code word customer: monitoring of the controller: ROM
CDKURRST		Code word customer: monitoring of the controller: Reset
CDTURRAM		Code word tester: monitoring of the controller: RAM
CDTURROM		Code word tester: monitoring of the controller: ROM
CDTURRST		Code word tester: monitoring of the controller: Reset
CLAURRAM		Fault class: monitoring of the controller: RAM
CLAURROM		Fault class: monitoring of the controller: ROM
CLAURRST		Fault class: monitoring of the controller: Reset
TSFURRAM		Fault active time: monitoring of the controller: RAM
TSFURROM		Fault active time: monitoring of the controller: ROM
TSFURRST		Fault active time: monitoring of the controller: Reset

## FB DUR 1.22 Detailed description of function

Diagnosis from the Processor Monitoring  
-----

The diagnostic function must be processed during the initialization after the initialization section for the reset duty cycle and after the DFPM initialization, since all cycle bits are cleared during the DFPM initialization.

Also cyclic processing during operation is possible, e.g. in the 100 ms task should inclusion in the initialization be problematic.

Separation is performed into faults from the RAM test, from the ROM test and into other faults with the defined fault reaction Reset.

In the process, the following assignment applies:

```

SUPERVISOR_RESET_TV      = Reset to generate a duty cycle between reset and operation (cf. %URMEM, %UFREAC)

SUPERVISOR_RESET_ROM    = Reset from the ROM test during the initialization (cf. %URROM)
=> rstpfad = 01
SUPERVISOR_RESET_ROMZ   = Reset from the cyclic partial ROM test via the monitoring components (cf. %URMEM)
=> rstpfad = 02

SUPERVISOR_RESET_RAM    = Reset from the RAM test during the initialization via the external RAM (cf. %URRAM)
=> rstpfad = 03
SUPERVISOR_RESET_RAMI   = Reset from the RAM test during the initialization via the internal RAM (cf. %URRAM)
=> rstpfad = 04
SUPERVISOR_RESET_RAMZ   = Reset from the cyclic partial RAM securing of the monitoring variables (cf. %URMEM)
=> rstpfad = 05

SUPERVISOR_RESET_FU     = Reset from the fault-reaction monitoring of the watchdog function (cf. %UFREAC)
=> rstpfad = 06
SUPERVISOR_RESET_UM     = Reset from the incorrect fault-counter feedback of the supervisor module (cf. %UMKOM)
=> rstpfad = 07
SUPERVISOR_DISPS_RESET  = Reset from the deactivation-path test (cf. %UMAUSC)
=> rstpfad = 08
SUPERVISOR_NOQUEST_RESET= Reset from missing inquiry by the supervisor module (cf. %UMTOUT/%UMKOM),
                        at communication via SPI with the functional processor as master not possible
=> rstpfad = 09

```

The assignment of the code rstpfad is fixed for the evaluation in the diagnosis. In case of symbolic inquiry for a reset cause to be entered, this assignment then needs to be corrected according to above-mentioned list.

The entry into the fault memory can, however, only take place, if no static fault is given, which prevents reset with its fault reaction that the entry takes place resp. can be read. Thereby the entries into the fault memory defined above are possible for faults, which are no longer given at the moment of the entry.

Thus a sequence is conceivable, in which e.g. a storage fault is detected during the initialization, which leads to the reset. If this storage fault is no longer given during the initialization in one of the following checking sequences, then normal operation is resumed without functional limitation and the no longer given fault is entered into the fault memory.

In block diagrams fault type information as well as cycle and error flags are illustrated as outputs. The output, however, is not performed by the transmission of individual bits but by writing the entire status word sfpxyz of the fault path xyz back into the central diagnostic management DFPM. The bits E\_xyz, Z\_xyz, B\_mnxyz etc. are contents of this status word. For error and cycle flags of external fault paths which occur as inputs, access methods are available which read these information directly from the fault path status managed in the DFPM.

The following variables are defined for each fault path XYZ of this diagnostic function:

```

Status fault path XYZ:      sfpxyz
Error flag xyz:             E_xyz
Cycle flag xyz:             Z_xyz
Fault type xyz:             TYP_xyz: (B_mnxyz, B_sixyz, B_npxyz)
Clear fault path:          B_clxyz
Default value active:      B_bkxyz (optional)
Fault path code xyz:       CDTXYZ
Fault class xyz:           CLAXYZ
Fault severity xyz:        TSFXYZ
CARB code xyz:            CDCXYZ
Table of ambient cond. xyz: FFTXYZ

```

The following fault paths xyz are treated in this function definition:

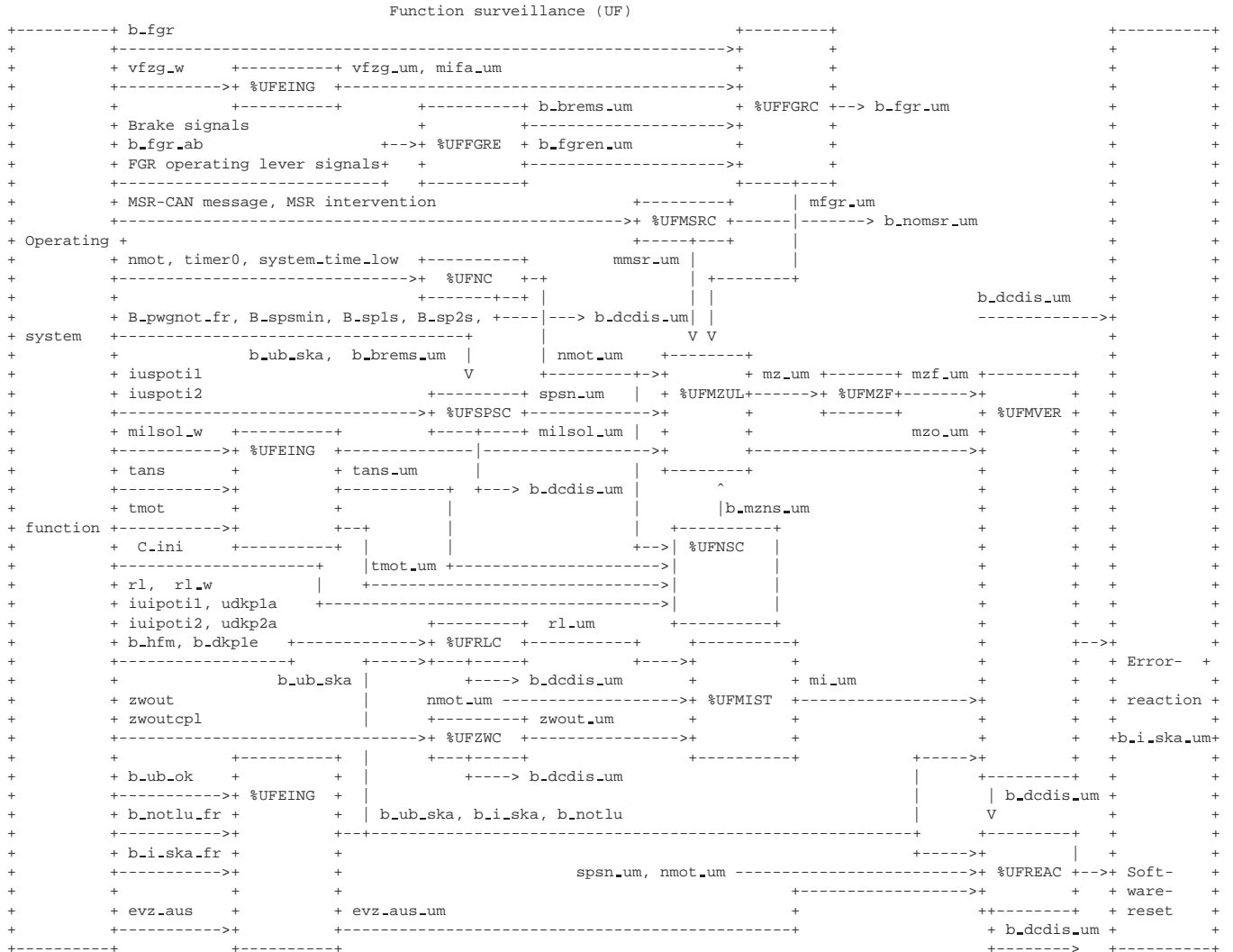
Fault path name	Used abbreviation (substitutes "xyz")
Processor monitoring: ROM	URROM
Processor monitoring: RAM	URRAM
Processor monitoring: Reset	URRST



## APP DUR 1.22 Application hint

## UFUE 4.11 ETS monitoring concept: function monitoring overview

### DDEF UFUE 4.11 Function definition



### ABK UFUE 4.11 Abbreviations

Variable	Source	Type	Description
B_DCDIS_UM	UFUE	LOK	Fault reaction information of the function monitoring
B_FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control
B_FGR_UM	UFUE	AUS	CC/ACC torque intervention in function monitoring permitted
B_J_SKA	UFUE	LOK	FR error reaction irreversible SKA (safety fuel shut-down)
B_J_SKA_FR	SREAKT	EIN	FR error reaction irreversible SKA (safety fuel shut-down)
B_J_SKA_UM	UFUE	AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_MZNS_UM	UFUE	LOK	afterstart torque increase of ETC-monitoring is active
B_NOMSR_UM	UFUE	AUS	MSR moment required not used in function monitoring
B_NOTLU	UFUE	LOK	Request standby air driving from the function
B_NOTLU_FR	SREAKT	EIN	Request for NFB from Function controller
B_UB_OK	ADVE	EIN	Battery voltage o.k.
B_UB_SKA	UFUE	LOK	Battery voltage not OK, undervoltage shut-off active
C_JNI	SWADAP	EIN	ECU-condition for intialisation
EVZ_AUS	AEVAB	EIN	injection cut off pattern
EVZ_AUS_UM	UFUE	LOK	Injection cut off pattern in function monitoring
IUIPOT1		EIN	ADC value incl. channel number throttle valve actual value potentiometer 1 loop
IUIPOT2		EIN	ADC value incl. channel number throttle valve actual value potentiometer 2 loop
IUSPOT1		EIN	ADC value incl. channel number nominal value potentiometer 1 loop (PWG)
IUSPOT2		EIN	ADC value incl. channel number nominal value potentiometer 2 loop (PWG)
MFGR_UM	UFUE	LOK	Torque request from cruise control for function monitoring
MIFA_UM	UFUE	LOK	FGR-/ACC- or driver requested torque of function for function monitoring
MILSOL_UM	UFUE	LOK	driver torque request for charge used in function monitoring
MILSOL_W	MDKOL	EIN	driver torque request for charge
ML_UM	UFUE	LOK	Calculated actual torque in function monitoring
MMSR_UM	UFUE	LOK	Permissible MSR torque request for function monitoring





Variable	Source	Type	Description
MZF_UM	UFUE	LOK	Filtered permissible torque of function monitoring
MZO_UM	UFUE	LOK	Tolerance offset for permissible torque in function monitoring
MZ_UM	UFUE	LOK	Permissible torque resulting from the coordination of function monitoring
NMOT	SWADAP	EIN	engine speed
NMOT_UM	UFUE	LOK	engine speed in function monitoring
RL	SWADAP	EIN	relative air charge
RL_UM	UFUE	LOK	Relative air charge in function monitoring
RL_W	EGFE	EIN	relative air charge (Word)
SPSN_UM	UFUE	LOK	Pedal value (8-bit) with lower limit to idling in function monitoring
TANS	SWADAP	EIN	Intake air temperature
TANS_UM	UFUE	LOK	Intake air temperature of the watchdog function
TMOT	SWADAP	EIN	Engine temperature
TMOT_UM	UFUE	LOK	Engine temperature in the watchdog function
UDKP1A	BGDVE	EIN	sensor voltage poti 1 of throttle actuator at (lower) mechanical stop
UDKP2A	BGDVE	EIN	sensor voltage poti 2 of throttle actuator at (lower) mechanical stop
VFZG_UM	UFUE	LOK	engine speed in function monitoring
VFZG_W	GGVFZG	EIN	Vehicle speed
ZWOUT	ZUE	EIN	Ignition angle output value
ZWOUTCPL	ZUE	EIN	Single complement of the ignition angle for function monitoring
ZWOUT_UM	UFUE	LOK	Ignition angle in function monitoring

### FW UFUE 4.11 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB UFUE 4.11 Detailed description of function

This section is an overview of der function surveillance at the torque level.

The sections are active in the 10-ms, 20-ms or 40-ms time frame. The allocation to the respectively valid frame is executed on a module-specific basis.

These are thereby called up in the 10-ms time frame in the following sequence:

%UFEING	Transfer of input signal for function surveillance
%UFFGRE	FGR input information for function surveillance
%UFNC	Speed monitoring for function surveillance
%UFNSC	Afterstart-monitoring for function surveillance
%UFZWC	Ignition-timing monitoring for function surveillance
%UFRLC	Load signal monitoring for function surveillance
%UFSPSC	Pedal setpoint value monitoring for function surveillance
%UFFGRC	FGR monitoring for function surveillance
%UFMSRC	Monitoring MSR torque interventions for function surveillance
%UFMIST	Actual torque in function surveillance
%UFMZUL	Permissible torque in function surveillance
%UFMZP	Torque filter for function surveillance
%UFMVER	Torque comparison in function surveillance
%UFNSC	Afterstart-monitoring for function surveillance
%UFREAC	Error-reaction monitoring in function surveillance

### APP UFUE 4.11 Application hint

## UFOBP 1.10 ETS monitoring concept: OBP operation of function monitoring

### FDEF UFOBP 1.10 Function definition

### ABK UFOBP 1.10 Abbreviations

### FW UFOBP 1.10 Fixed Values

Parameter	Value	Description
-----------	-------	-------------



## FB UFOBP 1.10 Detailed description of function

OBP operation of the function surveillance  
-----

The module must contribute to control of the program sequence (refer to %URPAK).

### Requirement:

The surveillance module (UM) may not be shut down during the on-board check (OBP), such that its monitoring function is continuously active in normal operation as well, and cannot be shut down either. It is for this reason that the function computer (FR) in the OBP has to serve the surveillance module (UM) as in normal operation. In normal operation, the query initiated by the surveillance module (UM) is iterated through the function surveillance modules with the help of the process sequencing control, and valid response is formed from this for the surveillance module (UM).

A special program section that iterates through a special OBP module of the program sequencing control and forms a valid response for the surveillance module (UM) is used in OBP operation so that order effects on the OBP are excluded for changes in function surveillance.

### Definition:

This special OBP module of function surveillance monitors the ignition and injection outputs in the Capture Compare Unit for a shutdown capture-compare mode. A software reset is triggered in the case of a fault.

## APP UFOBP 1.10 Application hint

## UFEING 13.10 ETS monitoring concept: Input signal transfer used in function monitoring

### FDEF UFEING 13.10 Function definition

Transfer of the Input Signals for the Watchdog function  
-----

```

b_ub_ok ----->+ +----> b_ub_ska
                    +----+
b_i_ska_fr -----> b_i_ska
b_notlu_fr -----> b_notlu

evz_austot -----> evz_aus_um

tmot -----> tmot_um
tans -----> tans_um
    
```

### ABK UFEING 13.10 Abbreviations

Variable	Source	Type	Description
B_J_SKA	UFEING	AUS	FR error reaction irreversible SKA (safety fuel shut-down)
B_J_SKA_FR	SREAKT	EIN	FR error reaction irreversible SKA (safety fuel shut-down)
B_NOTLU	UFEING	AUS	Request standby air driving from the function
B_NOTLU_FR	SREAKT	EIN	Request for NFB from Function controller
B_JUB_OK	ADVE	EIN	Battery voltage o.k.
B_JUB_SKA	UFEING	AUS	Battery voltage not OK, undervoltage shut-off active
EVZ_AUSTOT	AEVABZK	EIN	injection cut off pattern total
EVZ_AUS_UM	UFEING	AUS	Injection cut off pattern in function monitoring
MILSOL_UM	UFEING	AUS	driver torque request for charge used in function monitoring
MILSOL_W	MDKOL	EIN	driver torque request for charge
TANS	SWADAP	EIN	Intake air temperature
TANS_UM	UFEING	AUS	Intake air temperature of the watchdog function
TMOT	SWADAP	EIN	Engine temperature
TMOT_UM	UFEING	AUS	Engine temperature in the watchdog function

### FW UFEING 13.10 Fixed Values

Parameter	Value	Description
-----------	-------	-------------



## FB UFEING 13.10 Detailed description of function

Input signal transfer for watchdog function  
-----

The module must be of assistance in the check of the program execution (see %URPAK).

The RAM and ROM areas affected by the function must be stored cyclically (see %URMEM).

The input signals needed for the watchdog function must be transferred cyclically to the watchdog function.

The following informations are input signals for %URADCC:

iuspotil        ADC-value incl. channel number setpoint poti 1  
iasplplaus     ADC-value incl. channel number setpoint poti 1 from the supervisor module

The following informations are input signals for %UFRLC:

b\_wdk2sel      Fault at throttle valve (DK) poti 1, throttle sensor default function with DK poti 2  
b\_hfm          Condition HFM ready for measurement, i.e. load signal from HFM and not from DK info  
rl              Relative air charge, i.e. load information rl from the function  
rl\_w          Relative air charge, i.e. load information rl\_w from the function  
iuipotil       ADC-value incl. channel number for throttle valve poti 1  
iuipoti2       ADC-value incl. channel number for throttle valve poti 2  
udkp1a        Voltage throttle valve poti 1 at the (lower) limit stop  
udkp2a        Voltage throttle valve poti 2 at the (lower) limit stop

The following informations are input signals for %UFZWC:

zwout          Ignition angle for the function  
zwoutcpl      Complement of the ignition angle to make the ignition angle plausible in the watchdog function

The following informations are input signals for %UFSPSC:

iuspotil       ADC-value incl. channel number setpoint poti 1  
iuspoti2       ADC value incl. channel number setpoint poti 2  
b.sp1s        SP1S is reference variable in the pedal sensor default function  
b.sp2s        SP2S is reference variable in the pedal sensor default function  
b.spsmin      In the pedal sensor default function the idle input applies  
b\_pwgnotfr    Pedal sensor default function from the function is active

The following informations are input signals for %UFFGRE:

S.blS          Stop-light switch information: Brake is applied  
S.brS          Stop-light switch information: Brake is not applied  
b.fgrab       FGR/ACC deactivation conditions active in the function  
S.fgrwb       Switch resume/accelerate on the FGR stalk  
S.fgrsv       Switch set/decelerate on the FGR stalk  
S.fgrat       Switch OFF-TIP on the FGR stalk  
S.fgrhs        Main switch on the FGR stalk

The following information is input signals for %UFNC:

nmot          Engine speed

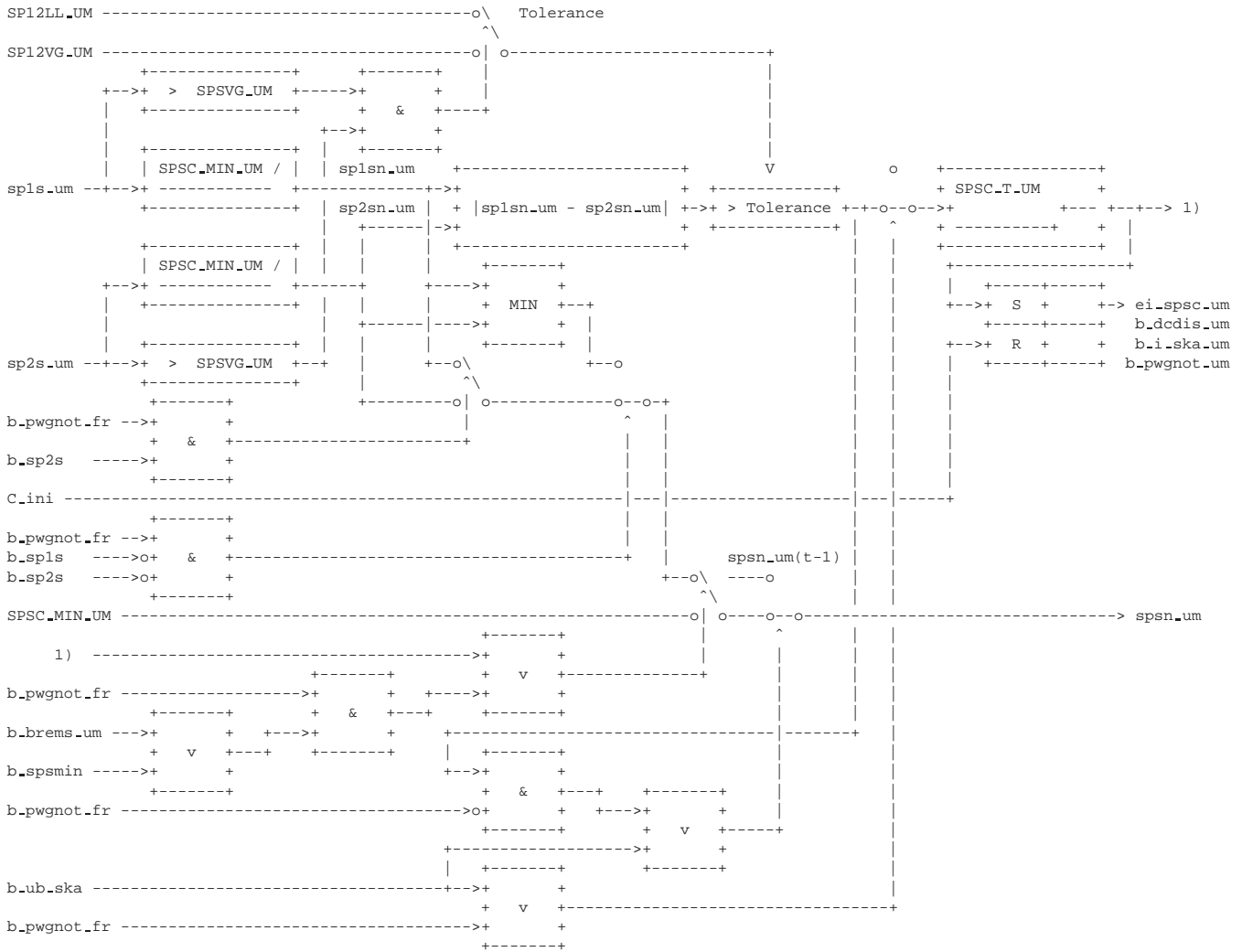
The ASR/MSR data arrive in the function processor via CAN and are made available unprocessed to the watchdog function for the evaluation in %UFMSRC.

## APP UFEING 13.10 Application hint

The data of the watchdog function are part of the monitoring concept and they may therefore not be changed arbitrarily.

Label	Source	Type	Description
b.i.ska_fr		VAR/EIN	functional fault reaction irrev. SKA (safety fuel deactivation)
b.i.ska		VAR/AUS	functional fault reaction irrev. SKA (safety fuel deactivation)
b.notlu_fr		VAR/EIN	functional fault reaction throttle actuator power stage at zero current
b.notlu		VAR/AUS	functional fault reaction throttle actuator power stage at zero current
b_ub.ok		VAR/EIN	battery voltage O.K., no undervoltage deactiv. of DK actuator power stage active
b_ub.ska		VAR/AUS	undervoltage deactivation of DK actuator power stage active
evz_austot		VAR/EIN	cylinder cutout mask for injection cutout as input info for the CIFI
evz_aus_um		VAR/AUS	cylinder cutout mask for injection cutout for the watchdog function
tans		VAR/EIN	intake air temperature
tans_um		VAR/AUS	intake air temperature in the watchdog function
tmot		VAR/EIN	engine temperature
tmot_um		VAR/AUS	engine temperature in the watchdog function





### ABK UFSPSC 2.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SP12LL_UM			FW	maximum difference between SP1S and SP2S below full load
SP12VG_UM			FW	maximum difference between SP1S and SP2S above full load range
SPSC_MIN_UM			FW	= SPSC_MIN_UM Pedal idling gas limit for function monitoring
SPSC_T_UM			FW	Fault time for nominal values in func. monitor, which are mutually not plaus.
SPSVG_UM			FW	Threshold full load for switch over of max. tolerance

Variable	Source	Type	Description
B_BREMS_UM	UFFGRE	EIN	condition of function monitoring: brake pedal pressed
B_DCDIS_UM	UFSPSC	AUS	Fault reaction information of the function monitoring
B_LSKA_UM	UFSPSC	AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_PWGNOTFR	GGPED	EIN	FR error reaction pedal-travel sensor limphone
B_PWGNOTUM	UFSPSC	AUS	= b_pwgnot_um function monitoring fault response PWG idling (= b_pwgnot_sr)
B_SP1S	GGPED	EIN	message to SR: SP1S is command variable
B_SP2S	GGPED	EIN	SP2S is valid set value for PWG failure driving
B_SPSMIN	GGPED	EIN	message to SR: '1' = pedal-travel sensor limphone with SPSMIN
B_UB_SKA	UFEING	EIN	Battery voltage not OK, undervoltage shut-off active
EI_SPS_C_UM	UFSPSC	AUS	irrevers. error bit for pedal value plausibility check in function monitoring
IUSPOT1		EIN	ADC value incl. channel number nominal value potentiometer 1 loop (PWG)
IUSPOT2		EIN	ADC value incl. channel number nominal value potentiometer 2 loop (PWG)
SP1SN_UM	UFSPSC	LOK	Value from SP1S with lower limit to idling for function monitoring
SP1S_UM	UFSPSC	LOK	Current value for nominal value potentiometer 1 (PWG) for function monitoring
SP2SN_UM	UFSPSC	LOK	Value from SP2S with lower limit to idling for function monitoring
SP2S_UM	UFSPSC	LOK	Current value for nominal value potentiometer 2 (PWG) for function monitoring
SPSC_C_UM	UFSPSC	LOK	Error counter for mutually non-plausible values in function monitoring
SPSN_UM	UFSPSC	AUS	Pedal value (8-bit) with lower limit to idling in function monitoring



## FW UFSPSC 2.30 Fixed Values

Parameter	Value	Description
SP12LL_UM		maximum difference between SP1S and SP2S below full load
SP12VG_UM		maximum difference between SP1S and SP2S above full load range
SPSC_MINUM		= SPSC_MIN_UM Pedal idling gas limit for function monitoring
SPSC_T_UM		Fault time for nominal values in func. monitor. which are mutually not plaus.
SPSVG_UM		Threshold full load for switch over of max. tolerance

## FB UFSPSC 2.30 Detailed description of function

Pedal setpoint monitoring for the function surveillance  
-----

The module must contribute to control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

The pedal setpoint value must be monitored on the basis of redundant information.

Monitoring the pedal setpoint value cannot be executed if the power supply to the sensors is no longer assured. Accordingly, monitoring the pedal setpoint value is not carried out if the throttle-valve actuator output stage is shut down by an undervoltage. A check is then made in the error-reaction monitoring of function surveillance (%UFREAC) whether the undervoltage shutdown has actually been executed and is not just being indicated.

For pedal setpoint monitoring, the lower values for both sets of input information are limited to the idle-speed value.

Both pedal setpoints limited to the lower values are then compared with a permissible tolerance range. This tolerance is extended if both pedal setpoint values are in the full-gas range.

If the pedal setpoint values are matching, then the error counter for monitoring the pedal setpoint value is deleted and the reference variable sp1s\_um is taken as the valid value for the pedal setpoint, sps\_um for the subsequent processing.

If, in the event of a fault, there is no switchover to the PWG standby function (pedal-value variable), then the valid pedal setpoint value is not updated and, following elapse of an error time that is longer than that in the function, a set of error information, the error reaction and the error-reaction information are set. In addition to this, the pedal setpoint value is then set to the idle-speed requirement.

If the PWG standby function is active, then the valid pedal setpoint value is set to the idle-speed requirement when the brake is operated.

If the brake is not operated, then the valid pedal setpoint value is updated for an active PWG standby function with the help of the information from the reference variable for component monitoring in the function. In case neither the idle-speed requirement nor a defined reference variable (SP1S or SP2S) is signaled, then the minimum-value selection from SP1S and SP2S is continued to be used as the pedal setpoint value requirement.

## APP UFSPSC 2.30 Application hint

The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
b_brems_um	VAR/EIN		Resulting brake information for function surveillance (operated in case of doubt)
b_dodis_um	VAR/AUS		Error-reaction info. (shutdown of throttle-valve actuator output stage) of function surveillance
b_sp1s	VAR/EIN		SP1S is the reference variable in the PWG standby function
b_sp2s	VAR/EIN		SP2S is the reference variable in the PWG standby function
b_spsmin	VAR/EIN		The idle-speed requirement applies in the PWG standby function
b_i_ska_um	VAR/AUS		Function-surveillance error reaction irrev. SKA (safety fuel shutdown)
b_pwgnot_fr	VAR/EIN		Message to function surveillance: PWG standby function active
b_pwgnot_um	VAR/AUS		Function-surveillance error reaction: PWG idle-speed requirement active
b_ub_ska	VAR/EIN		Battery voltage not OK, undervoltage shutdown of the throttle-valve actuator output stage active
ei_spsc_um	VAR/AUS		Irreversible error bit for plausibility of setpoint value in function surveillance
iuspoti1	VAR/EIN		ADC value incl. channel number setpoint-value potentiometer 1
iuspoti2	VAR/EIN		ADC value incl. channel number setpoint-value potentiometer 2
sp1s_um	VAR/LOK		Setpoint-value potentiometer 1 for function surveillance
sp2s_um	VAR/LOK		Setpoint-value potentiometer 2 for function surveillance
sp1sn_um	VAR/LOK		Value limited to lower idle-speed limit by setpoint-value poti 1 for function surveillance
sp2sn_um	VAR/LOK		Value limited to idle-speed limit by setpoint-value potentiometer 2 for function surveillance
spsn_um	VAR/AUS		Valid pedal setpoint value for function surveillance
spsc_c_um	VAR/LOK		Error counter setpoint values not mutually plausible in function surveillance

Label	Dependency	Type	Designation
SP12LL_UM		FW	Maximum difference between SP1S and SP2S below the full-gas threshold
SP12VG_UM		FW	Maximum difference between SP1S and SP2S above the full-gas threshold
SPSVG_UM		FW	Full-gas setpoint-value threshold for switching over the max. diff. in function surve.
SPSC_MIN_UM		FW	Pedal idle-speed limit for function surveillance
SPSC_T_UM		FW	Error time for setpoint values not mutually plausible in function surveillance





## FW UFNC 3.20 Fixed Values

Parameter	Value	Description
NC_T_UM		Fault tolerance time for engine speed monitoring in function monitoring
NDIF_UM		Permissible difference between nmot and nz_um in function monitoring
NMIN_UM		Minimum speed for engine speed surveillance in function monitoring
NZMUL_UM		Multiplier for conv. of the number of teeth in engine speed for func. monitor.
TZTOL_UM		Tolerance between time and tooth counter detection in timer increments
ZSYNC_UM		Initialization value for missing synchronization in the watchdog function

## FB UFNC 3.20 Detailed description of function

Monitoring of engine speed for watchdog function  
-----

The module must be of assistance in the check of the program execution (see %URPAK).

The RAM and ROM areas affected by this function must be stored cyclically (see %URMEM).  
Only the temporary variables may be used as intermediate variables within this function. These are used just as in the command tests (see %URCPU) and they are thus checked for writability.

This function shall be processed in the 40ms cycle.

The engine speed must be monitored on the basis of redundant information.  
For this purpose the engine speed is secured for the watchdog function with a variable of the engine speed sensing, which is also relevant for the ignition output.

Usage of the tooth counter is useful for this.

The counter for the tooth edges serves as compare-setting for the ignition and it is evaluated in the 40ms cycle as number of increments per measuring cycle, i.e. as number of teeth during the measuring period.

In the process a time matching the current tooth counter value is also taken over, in order to be able to take into account deviations from the standard cycle time due to floating processing in the 10ms cycle.

In the process the following sequence is executed in the 40ms cycle, which is generated from the 10ms cycle:

- 1) Read timer count from operating-system timer being executed with fixed quantization (SYSTEM\_TIME\_LOW)
- 2) Read tooth count from event counter being executed
- 3) Consistency check:  
Read timer count again and in case of too high temporal offset rsatz (> TZTOL\_UM) to the first read timer count read the tooth count again so that a possibly triggered synchro between reading of timer and tooth counter does not prevent the unity.
- 4) Take over timer count into tcap\_um and event counter into zcap\_um
- 5) Form the difference between current and previous timer count:  $tdif\_um = tcap\_um - talt\_um$
- 6) Form the difference between current and previous tooth count:  $zdif\_um = zcap\_um - zalt\_um$
- 7) Convert number of teeth zdif\_um to accompanying engine speed nz\_um:

The number of teeth is converted to an engine speed, as is used in the watchdog function, by the following conversion formula:

$$nz\_um = \frac{zdif\_um}{tdif\_um} * NZMUL\_UM$$

- 8) Check calculated and functional engine speed for maximum allowed offset:  
 $|nz\_um - nmot| > NDIF\_UM$  means too high deviation

In case the engine speed values match each other the fault counter is cleared and nmot is transferred to nmot\_um for further use.

The maximum value from nmot and nz\_um is transferred to nmot\_um as valid engine speed value in case of fault.

If the minimum engine speed for the watchdog function NMIN\_UM is exceeded even with the calculated engine speed nz\_um, then the fault counter nc\_c\_um is incremented until it reaches its final value of NC\_T\_UM, otherwise the fault counter nc\_c\_um is cleared.

In case the final value is reached a fault information ei\_nc\_um is set and the fault reaction irreversible safety fuel deactivation is triggered (b\_i\_ska\_um=1, b\_dcds\_um=1).

- 9) Store the current timer and tooth count as previous one:

$$\begin{aligned} talt\_um &= tcap\_um \\ zalt\_um &= zcap\_um \end{aligned}$$

The missing valid values in talt\_um and zalt\_um can lead to the fault counter nc\_c\_um starting to count up to 1 when the program is called up for the first time.

Dynamic sequences at high engine speeds, which can lead to differing engine speed information in nmot and zdif\_um, are taken into consideration in the permissible tolerance NDIF\_UM during the comparison.

Low engine speeds are possibly updated less frequently in nmot than in zdif\_um.

This must be permitted by the fault tolerance time NC\_T\_UM and the tolerance NDIF\_UM during the comparison.





A malfunction at the speed sensor input can lead to a synchronization loss with the phase sensor signal. Thereby no SYNC-cycle is processed, in which ignition and injection are served.

Such a malfunction can last for longer than the fault tolerance time NC-T.UM and may not lead to the fault detection of the engine speed monitoring.

Deshalb werden die Drehzahlaufbereitung und -überwachung während dieser Zeit ausgeblendet, d.h. der Fehlerzähler nc\_c.um wird gelöscht und nmot in nmot\_um zur Weiterverwendung übernommen, damit für diesen Fall die Drehzahl in der Funktionsüberwachung mit der in der Funktion konsistent ist. Dies erfolgt aufgrund der beiden Kennungen zsync\_um = Initialisierungswert (ZSYNC-I.UM) und zsync\_ur = 1-er Komplement des Initialisierungswertes (~ZSYNC-I.UM).

Die Kennungen zsync\_um und zsync\_ur werden alle 80 ms mit dem Initialisierungswert beschrieben. Sobald eine Synchronisation erfolgt und das SYNC-Raster abgearbeitet wird, werden beide Kennungen zerstört (zsync\_um = 0 und zsync\_ur = ~0). Dann setzen auch Einspritzung und Zündung wieder ein. Damit erfolgen die Drehzahlaufbereitung und -überwachung, sobald die Kennungen zsync\_um und zsync\_ur zerstört werden.

Hierbei muß garantiert werden, daß innerhalb 80 ms mindestens ein SYNC-Raster abgearbeitet wird. Bei einer Zylinderanzahl von minimal 3 und einem Inkrementgeber mit 58 Zähnen entspricht das einer Drehzahl von maximal 483,3 U/min und wird als Erstbedingung für NMIN.UM zugrundegelegt. Eine höhere Zylinderanzahl ist unkritischer, da die entsprechende Segmentzeit bei gleicher Drehzahl bzw. die entsprechende Drehzahl bei gleicher Segmentzeit kleiner werden.

Durch die Abfrage zweier Bedingungen wird vermieden, daß eine Fehlinformation den Zustand "nicht synchronisiert" simuliert. Eine Beschreibbarkeitsprüfung (siehe %URMEM) darf für beide Kennungen nicht erfolgen, weil diese ungerechtfertigt einen Fehler erkennen kann, wenn im höherpriorisierten SYNC-Raster die Kennungen zerstört werden. Aus dem gleichen Grund darf keine Komplementprüfung durchgeführt werden.

Das ist zulässig, weil ein schlafender Fehler in der Beschreibbarkeit oder im richtigen Wert einmal pro Fahrzyklus in der RAM-Prüfung (%URRAM) erkannt wird.

## APP UFNC 3.20 Application hint

The data of the watchdog function are part of the monitoring concept and may therefor not be changed arbitrarily.

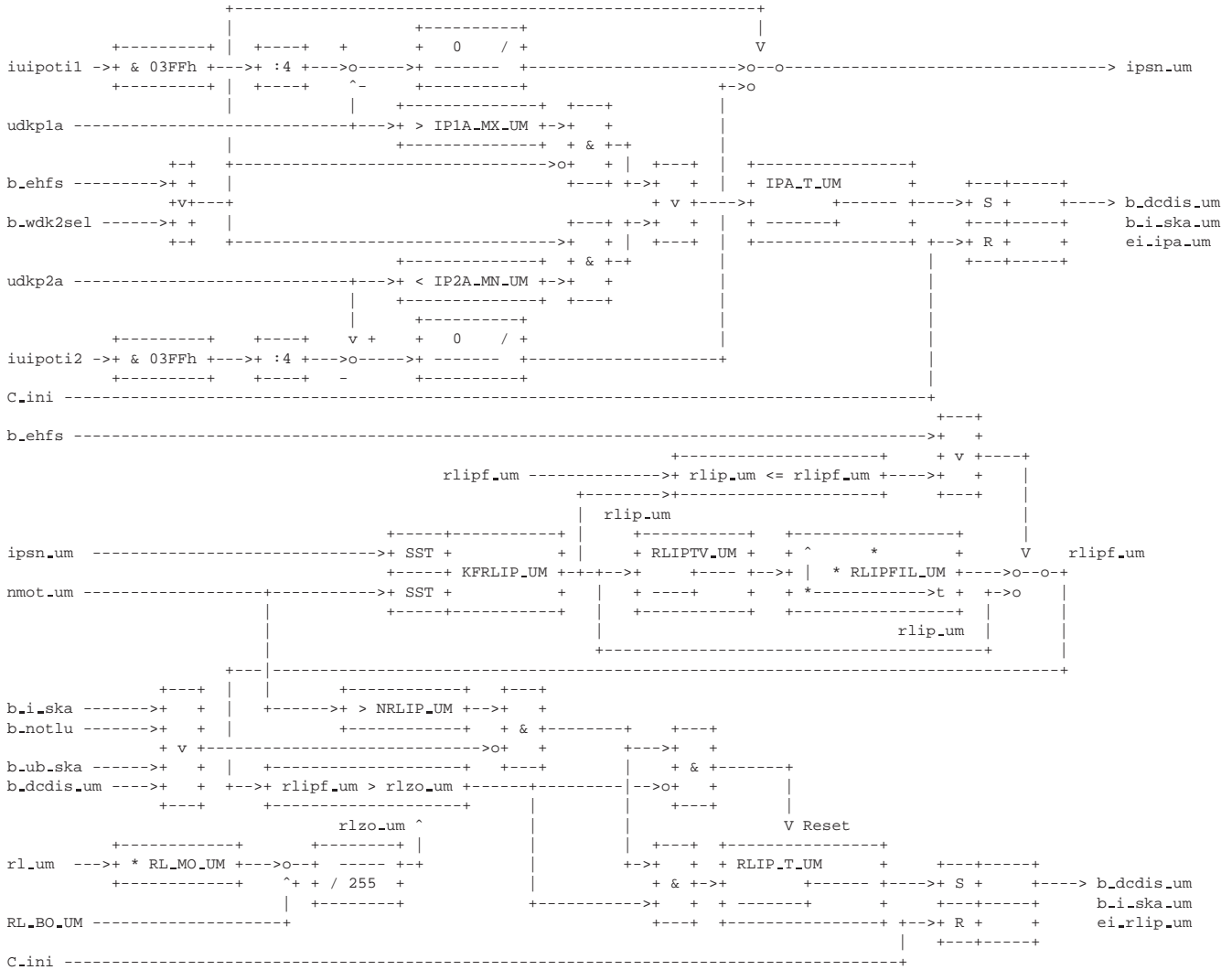
Label	Source	Type	Description
b_dcdis_um		VAR/AUS	Fault-reaction info (deactivation of throttle actuator output stage) of watchdog function
b_i_ska_um		VAR/AUS	Watchdog function fault reaction irrev. SKA (safety fuel deactivation)
ei_nc_um		VAR/AUS	irreversible fault bit during the speed plausibility check of the watchdog function
nc_c_um		VAR/LOK	Fault counter for engine speed comparison of the watchdog function
nmot		VAR/EIN	Engine speed for the function
nmot_um		VAR/AUS	Engine speed for the watchdog function
nz_um		VAR/LOK	Engine speed from the cycle-time-corrected number of teeth
r10msCtr		VAR/EIN	Counter of the 10ms cycle
talt_um		VAR/LOK	Timer value of the previous calculation instant in the 40ms cycle
tcap_um		VAR/LOK	Timer value of the current calculation instant in the 40ms cycle
tdif_um		VAR/LOK	Difference between current and previous calculation instant in timer steps
zalt_um		VAR/LOK	Tooth counter value of the previous calculation instant in the 40ms cycle
zcap_um		VAR/LOK	Tooth counter value of the current calculation instant in the 40ms cycle
zdif_um		VAR/LOK	Difference between current and previous tooth counter value
zsync_um		VAR/LOK	Identifier for synchronization in the watchdog function
zsync_ur		VAR/LOK	one's complement to the identifier 1-er for synchronization in the watchdog function

Label	Dependency	Type	Description
NC_T.UM		FW	Fault tolerance time for engine speed comparison in the watchdog function
NDIF.UM		FW	permitted difference between nmot and from no. of teeth calculated speed nz_um
NMIN.UM		FW	minimum engine speed for watchdog function
NZMUL.UM	En, Esystem	FW	Multiplier for conversion of the no. of teeth into engine speed
TZTOL.UM	Esystem	FW	Tolerance between time and tooth counter sensing in timer increments
ZSYNC_I.UM		FW	Initialization value for missing synchronization in the watchdog function





Load signal surveillance through plausibility check with the throttle valve information



### ABK UFRLC 5.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
IP1A_MX_UM			FW	Max. voltage for DK actual value pot. 1 at lower limit for function monitoring
IP2A_MN_UM			FW	Min. voltage for DK actual value pot. 2 at lower limit for function monitoring
IPA_T_UM			FW	Fault tolerance time for lower DK limit in invalid range for func. monitoring
KFRLIP_UM	IPSN_UM	NMOT_UM	KF	characteristic map for load signal calculation on throttle angle
NRLIP_UM			FW	Engine speed threshold for the r/rlip comparison in function monitoring
RLC_T_UM			FW	Fault tolerance time for rl comparison with the function in function monitoring
RLIPFIL_UM			FW	Filter time constant for delayed load information rlipt_um in function monitor.
RLIPTV_UM			FW	Delay time for load information rlip_um in functioning monitoring
RLIP_T_UM			FW	Fault tolerance time for the r/rlip comparison in function monitoring
RL_BO_UM			FW	Offset for tolerance straight line f(rl_um) for rlipf_um in function monitoring
RL_MO_UM			FW	Increase for tolerance straight line f(rl_um) for rlipf_um in function monitor.

Variable	Source	Type	Description
B_DCDIS_UM	UFRLC	AUS	Fault reaction information of the function monitoring
B_EHFS	DHFM	EIN	Condition substitute value main charge sensor
B_HFM	DHFM	EIN	Condition: HFM ready to measure
B_J_SKA	UFEING	EIN	FR error reaction irreversible SKA (safety fuel shut-down)
B_J_SKA_UM	UFRLC	AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_NOTLU	UFEING	EIN	Request standby air driving from the function
B_UB_SKA	UFEING	EIN	Battery voltage not OK, undervoltage shut-off active
B_WDK2SEL	GGDVE	EIN	Condition: DV-E position control is performed with actual-value-poti 2
C_INI	SWADAP	EIN	ECU-condition for intialisation
EI_IPA_UM	UFRLC	AUS	Irrevers. error bit for lower DK limit in invalid range of function monitoring
EI_RLC_UM	UFRLC	AUS	Irrevers. error bit for comparison of rl with the function in function monitor.
EI_RLIP_UM	UFRLC	AUS	Irreversible error bit for r/rlip comparison in function monitoring
IPA_C_UM	UFRLC	LOK	Fault counter for lower DK limit in invalid range for function monitoring
IPSN_UM	UFRLC	LOK	Active DK actual-value potenti. info. without lower limit for function monitor.



Variable	Source	Type	Description
IUIPOT11		EIN	ADC value incl. channel number throttle valve actual value potentiometer 1 loop
IUIPOT12		EIN	ADC value incl. channel number throttle valve actual value potentiometer 2 loop
NMOT_UM	UFNC	EIN	engine speed in function monitoring
RL	SWADAP	EIN	relative air charge
RLC_C_UM	UFRLC	LOK	Error counter for rl comparison with the function in function monitoring
RLIPF_UM	UFRLC	LOK	Relative air charge from secondary load signal after low pass in funct. monito.
RLIP_UM	UFRLC	LOK	relative air charge from auxiliary load signal
RLZO_UM	UFRLC	LOK	Upper tolerance limit for rl from secondary load signal in function monitoring
RL_UM	UFRLC	LOK	Relative air charge in function monitoring
RL_W	EGFE	EIN	relative air charge (Word)
RL_W_UM	UFRLC	LOK	relative air charge (Word)
UDKP1A	BGDVE	EIN	sensor voltage poti 1 of throttle actuator at (lower) mechanical stop
UDKP2A	BGDVE	EIN	sensor voltage poti 2 of throttle actuator at (lower) mechanical stop

### FW UFRLC 5.10 Fixed Values

Parameter	Value	Description
IP1A_MX_UM		Max. voltage for DK actual value pot. 1 at lower limit for function monitoring
IP2A_MN_UM		Min. voltage for DK actual value pot. 2 at lower limit for function monitoring
IPA_T_UM		Fault tolerance time for lower DK limit in invalid range for func. monitoring
NRLIP_UM		Engine speed threshold for the rl/rlip comparison in function monitoring
RLC_T_UM		Fault tolerance time for rl comparison with the function in function monitoring
RLIPFIL_UM		Filter time constant for delayed load information rlipt_um in function monitor.
RLIPTV_UM		Delay time for load information rlip_um in functioning monitoring
RLIP_T_UM		Fault tolerance time for the rl/rlip comparison in function monitoring
RL_BO_UM		Offset for tolerance straight line f(rl_um) for rlipf_um in function monitoring
RL_MO_UM		Increase for tolerance straight line f(rl_um) for rlipf_um in function monitor.

### FB UFRLC 5.10 Detailed description of function

Load signal surveillance for function monitoring

The module must contribute to the control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40 ms time frame.

The load signal must be checked on the basis of redundant information.

Load signal surveillance through plausibility check of the load information from the function

The consistency of the variables rl and rl\_w generated in the SYNC frame is assured in that both variables are read out twice in succession.

In the event that rl\_w from the 1st read-out is identical to the rl\_w from the 2nd read-out, then rl and rl\_w from the 1st read-out are transferred as the current variables, otherwise the rl and rl\_w values from the 2nd read-out are taken as the current variables.

It is detected by means of the RL comparison between the word variable used in the function and the 8-bit variable whether a transfer of the load information has been performed such that the same load information is used in the function as in function monitoring.

The load information in the function thereby serves as the basis for computing the injection time and the load information in function monitoring for calculating the actual moment.

If the signals rl\_w and rl converted to rl are not identical, then a fault tolerance time is run the elapse of which into the final state will set the fault information, the fault response as well as the fault response information.



Load signal surveillance through plausibility check using throttle valve information

For the transfer of the input signals for determination of the load information from the DK, a check is made for the valid voltage range at the lower limit of the selected DK sensor.

Exceeding the threshold for the lower limit of the DK sensor 1 for DK sensor 2 not selected, or falling below the

threshold for the lower limit of DK sensor 2 for DK sensor 2 selected will lead to initiation of a fault tolerance time.

The fault tolerance time is deleted if there is no evidence of the threshold having been violated.

The final status of the fault tolerance time sets the fault information, the fault response as well as the fault response information.

The throttle valve position can be converted into rl information by using the speed information.

As the throttle valve information is faster than the load information from the load sensor, the load information determined from the DK position for the check of an upper tolerance limit is delayed over a low pass for increasing load information from the DK. The comparison of both sets of load information is performed with the help of an upper limit for the load information from the DK, which is calculated as a dependency of the currently effective load information.

The currently effective load information rl\_um is thereby determined from the main load sensor or, if this has been detected as being discrepant, from the first DK sensor.

Therefore the comparison variable rlip\_um from ipsn\_um is switched over to the second DK sensor for a load sensor detected as being defective or for a DK sensor standby function.

If the load information is generated from the auxiliary load signal DK sensor 1, then the lag element and the low pass are shut down because the comparison of both sets of DK information and their load information is present at the same time.

If the deviation is greater than the permissible tolerance, which is determined by possible influences which cannot be eliminated, then a fault tolerance time is initiated.

The fault tolerance time is deleted if the load information from the DK is within permissible tolerances.

One restriction for the upper limit straight line rlzo\_um = f(rl\_um) for rlipf\_um, i.e. the rl from the DK actual value information, is permissible, as a discrepantly high load signal leads to a response by the moment comparison and thus does not have to be taken into consideration.

In addition to this, the filter settings would be critical for a comparison of the lower values.

The fault counter is halted if the engine speed falls below a defined fixed threshold, until this threshold is surpassed again.

The load information is not significant below this speed threshold from a technical safety viewpoint

and the computation from the throttle valve information can include errors under certain circumstances.

Furthermore, the fault counter is halted for an active undervoltage shut-off because the DK information can no longer be evaluated with reliability.

The final status of the fault tolerance time sets the fault information, the fault response as well as the fault response information.

If the filter is active, the drum storage for the dead time as well as the starting value for the low-pass filter must be occupied beforehand with the currently determined load value.

### APP UFRLC 5.10 Application hint

The data in function monitoring are part of the surveillance concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
b.dcdis_um		VAR/AUS	Fault response information (shut-off of the DK actuator output stage) of function monitoring
b.wdk2sel		VAR/EIN	Fault at DK potentiometer 1, DK sensor standby function with DK potentiometer 2
b.i.ska_um		VAR/AUS	Function monitoring fault response irrev. SKA (safety fuel shut-off)
b.ehfs		VAR/EIN	Condition substitute value main charge sensor
b.ub.ska		VAR/EIN	Battery voltage not OK, undervoltage shut-off of the DK actuator output stage active
ei.ipa_um		VAR/AUS	Irrev. fault bit for lower DK limit in invalid range in function monitoring
ei.rlc_um		VAR/AUS	Irreversible fault bit for rl comparison with the function
ei.rlip_um		VAR/AUS	Irreversible fault bit for rl/rlip comparison
ipa.c_um		VAR/LOK	Fault counter for lower DK limit in invalid range for function monitoring
ipsn_um		VAR/LOK	Active DK actual value potentiometer information converted to rising straight line without lower limit
iuipot11		VAR/EIN	ADC value incl. channel number for throttle valve potentiometer 1
iuipot12		VAR/EIN	ADC value incl. channel number for throttle valve potentiometer 2
nmot_um		VAR/EIN	Engine speed for function monitoring
rlc.c_um		VAR/LOK	Fault counter for rl comparison with the function
rlip_um		VAR/LOK	rl information from the DK actual value potentiometer information for function monitoring
rlip.c_um		VAR/LOK	Fault counter for plausibility check between rl_um and rlipf_um
rlipf_um		VAR/LOK	rl from DK actual value potentiometer after the low-pass filter for function monitoring
rlipf.low_um		VAR/LOK	Fine adjustment of rl from DK actual value potentiometer after TP for function monitoring
rlzo_um		VAR/LOK	Tolerance limit for rl from DK actual value potentiometer as a function of valid rl_um
rl		VAR/EIN	Relative air charge, i.e. load information rl from the function
rl_w		VAR/EIN	Relative air charge, i.e. load information rl_w from the function
rl_um		VAR/LOK	Load information rl from the function for function monitoring
rl_w_um		VAR/LOK	load information rl_w from the function for function monitoring
udkp1a		VAR/EIN	Voltage throttle valve potentiometer 1 at the (lower) limit
udkp2a		VAR/EIN	Voltage throttle valve potentiometer 2 at the (lower) limit

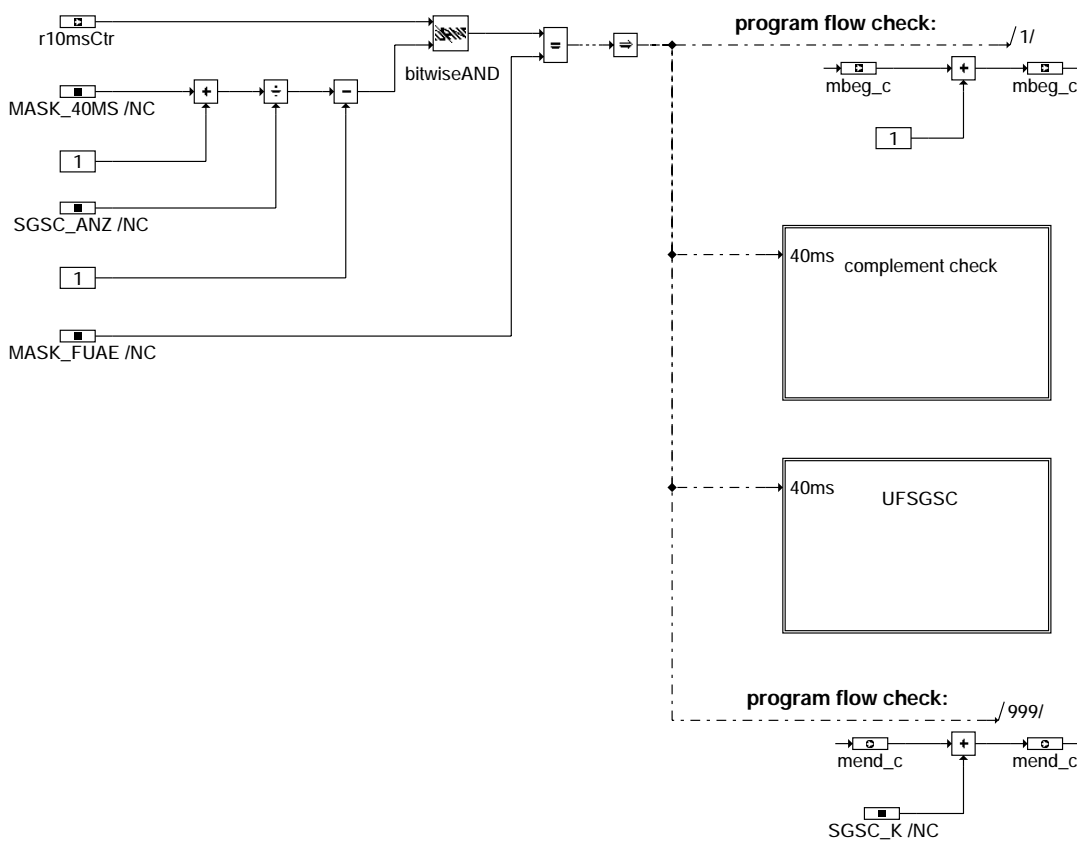


Label	Dependency	Type	Designation
IPA_T_UM		FW	Fault tolerance time for lower DK limit in the invalid range for function monitoring
IP1A_MX_UM		FW	Max. voltage for DK actual value potentiometer 1 at the lower limit for function monitoring
IP2A_MN_UM		FW	Min. voltage for DK actual value potentiometer 2 at the lower limit for function monitoring
KFRLIP_UM	ipsn_um, nmot_um	KF	Performance characteristics for rl information
NRLIP_UM		FW	Engine speed threshold for the rl comparison
RLC_T_UM		FW	Fault tolerance time for rl comparison with the function
RLIP_T_UM		FW	Fault tolerance time for plausibility check between rl_um and rlipf_um
RLIPTV_UM		FW	Delay time for load information rlip_um
RLIPFIL_UM		FW	Filter time constant for delayed load information rlipt_um
RL_MO_UM		FW	Inclination for tolerance straight line for rlipf_um as a dependency of rl_um
RL_BO_UM		FW	Offset for tolerance straight line for rlipf_um as a dependency of rl_um

## UFGSGC 4.10 EGAS-monitoring concept: SGS-intervention-monitoring for the function overview

### FDEF UFGSGC 4.10 Function definition

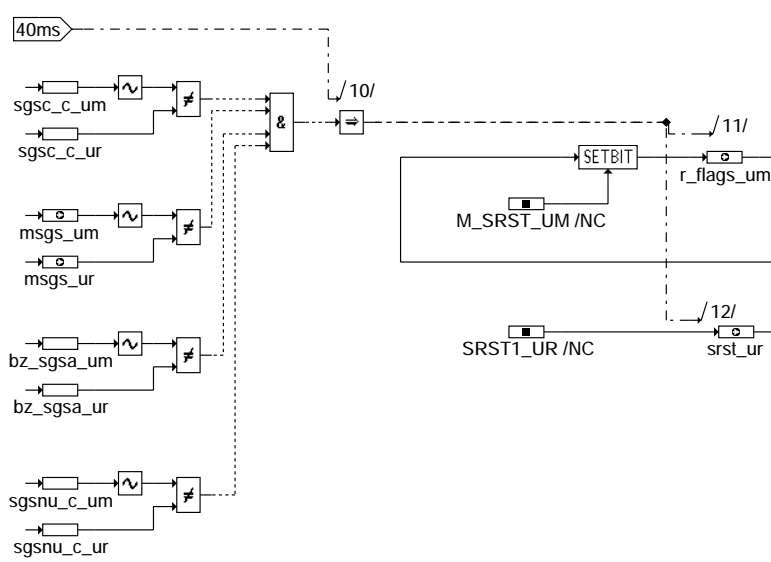
Overview:



ufsgsc-main

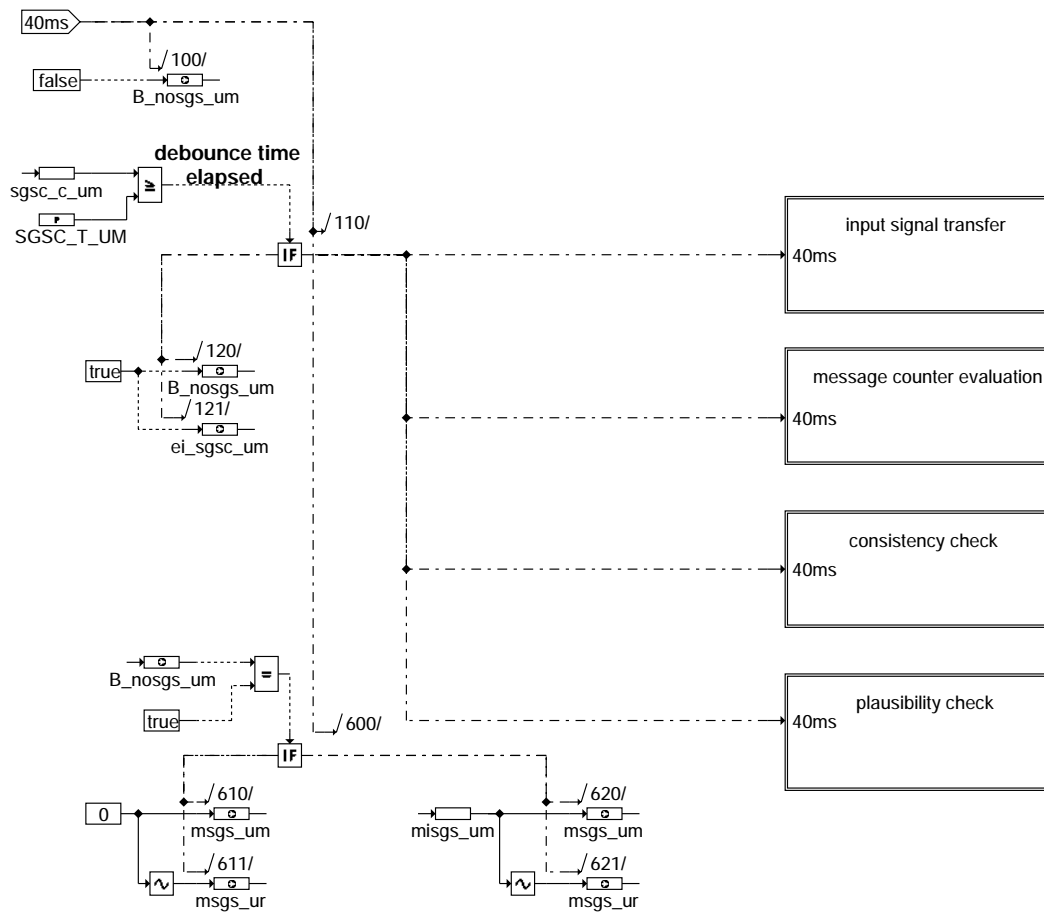
ufsgsc-main

Complement check:



ufsgsc-complement-check

SGS-Monitoring:

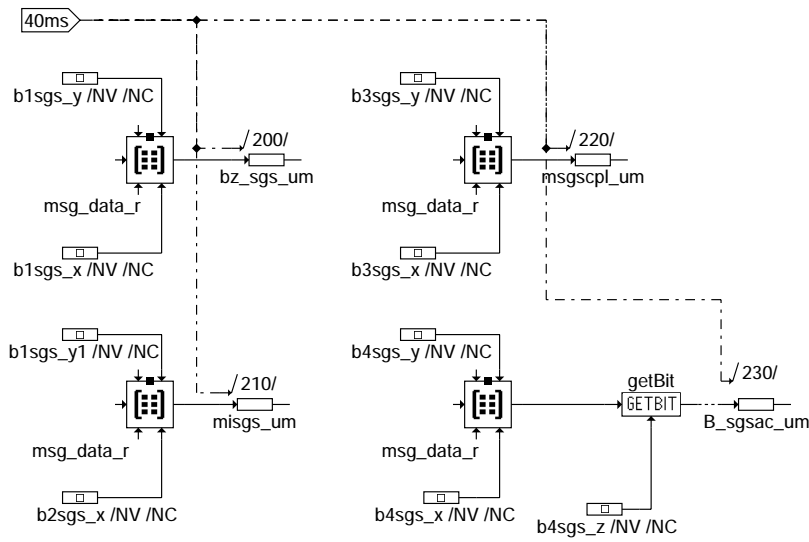


ufsgsc-ufsgsc

ufsgsc-complement-check

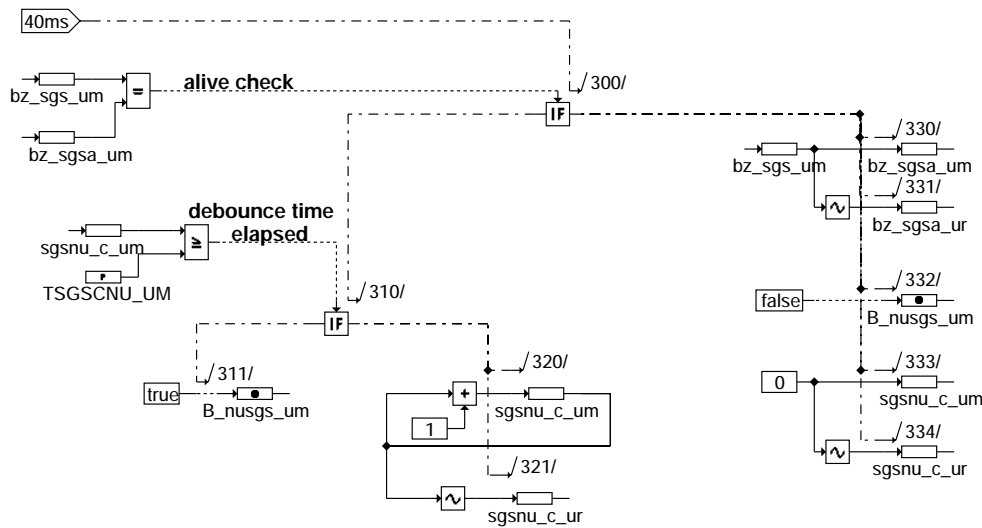
ufsgsc-ufsgsc

Input signal transfer:



ufsgsc-input-signal-transfer

Alive check:



ufsgsc-message-counter-evaluation

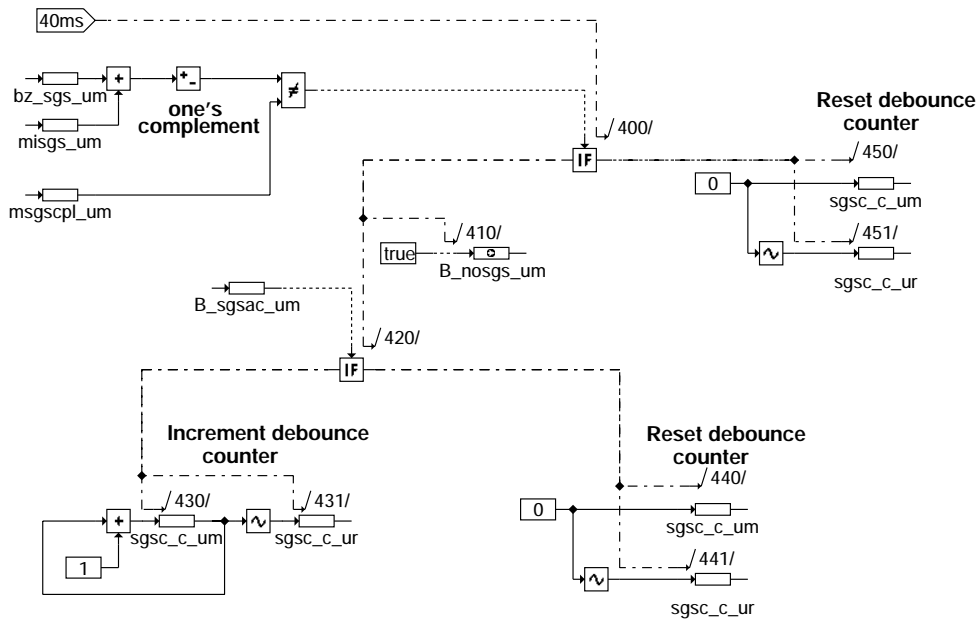
ufsgsc-input-signal-transfer

ufsgsc-message-counter-evaluation



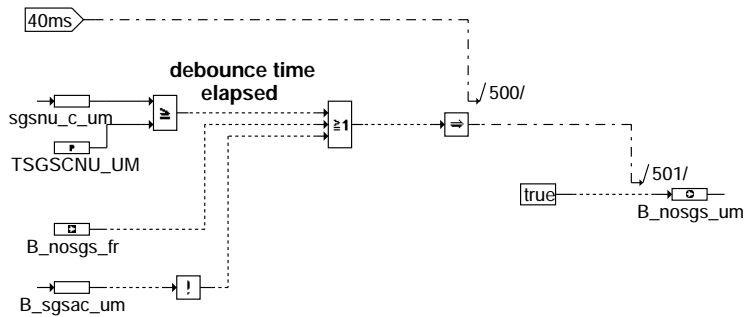


Consistency check:



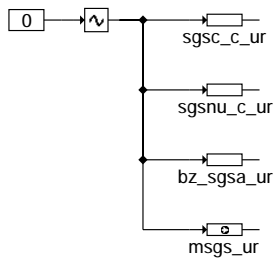
ufsgsc-consistency-check

Plausibility check:



ufsgsc-plausibility-check

Initialization phase:



ufsgsc-ini

ufsgsc-consistency-check

ufsgsc-plausibility-check

ufsgsc-ini



## FB UFGSGC 4.10 Detailed description of function

SGS-intervention-monitoring of function surveillance  
-----

The module must contribute to program flow check (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

The transmission data arrive via CAN in the functions computer and are made available for function surveillance.  
The data are read out directly from the CAN buffer.

b1sgs\_x Constant for CAN-buffer for SGS-message counter  
b1sgs\_y Constant for CAN-buffer for SGS-message counter  
b2sgs\_x Constant for CAN-buffer for SGS-intervention  
b2sgs\_y Constant for CAN-buffer for SGS-intervention  
b3sgs\_x Constant for CAN-buffer for SGS-surveillance  
b3sgs\_y Constant for CAN-buffer for SGS-surveillance  
b4sgs\_x Constant for CAN-buffer for SGS-Intervention activ  
b4sgs\_y Constant for CAN-buffer for SGS-Intervention activ  
b4sgs\_z Constant for CAN-buffer for SGS-Intervention activ (bitposition)

The torque msgsgs\_um ist calculated by value and complement.

The SGS-Intervention is allowed, if

1. the SGS-Intervention is also valid in Level I
2. the message-counter is updated in the right way
3. there is a valid SGS-Request (torque request by the transmission)
4. the message is consistent
5. the SGS-Intervention is not irreversible forbidden in Level II

The flag B\_nosgs\_um is deleted, if all these points are true. The value misgs\_um is copied to msgsgs\_um.  
Otherwise, the value msgsgs\_um is set to 0.

If the message is inconsistent, the torque msgsgs\_um remains to 0.  
The identifier ei\_sgsgc\_um is set following elapse of the error tolerance time.

Monitoring for updatedness  
-----

- The message counter bz\_sgs is incremented from the transmitting control unit. If the message counter is incremented every 20 ms, then the old and the new message counters differ by at least one and by a maximum of two in each 40-ms test cycle.

For detection of discrepant updating, i.e. in case the old and the new message counter do not differ, there is only one reversible error reaction active since an interruption in the CAN message shall not lead to a ban of the function until "Ignition off".

Monitoring for plausibility and message consistency  
-----

The Message counter is added to the torque Request and compared with the complement of the value mksgs\_cpl.  
This value is calculated by the transmitting ECU by the same way. If there is a inconsistency, the SGS-Intervention is forbidden by Level II.  
If the SGS-Intervention (intervention by the transmission) is not carried out by Level I, the SGS-Torque request will not be monitored in Level II.

## ABK UFGSGC 4.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
MASK_40MS			SYS (REF)	40ms mask for function monitoring
MASK_FUAE			SYS (REF)	Mask for task splitting in monitoring functions (part 1: inputs)
M_SRST_UM			SYS (REF)	Mask B_srst_um - information SW-reset from cyclic RAM-check
SGSC_ANZ			SYS (REF)	number of module calls of %UFGSGC (refer to %URPAK) in the monitoring function
SGSC_K			SYS (REF)	Constant for module %UFGSGC (see %URPAK)
SGSC_T_UM			FW	Fault time for SGS intervention surveillance in function monitoring
SRST1_UR			SYS (REF)	value for RAM data redundancy of bit B_SRST_UM = 1
TSGSCNU_UM			FW	Debounce time for information interruption
Variable	Source		Type	Description
BZ_SGSA_UM	UFGSGC		LOK	SGS-message counter from former calculation
BZ_SGSA_JR	UFGSGC		LOK	RAM data redundancy for bz_sgsa_um
BZ_SGS_UM	UFGSGC		LOK	SGS-message counter for function monitoring
B_NOSGS_FR			EIN	No SGS intervention from FR
B_NOSGS_UM	UFGSGC		AUS	SGS moment required not transferred to function monitoring
B_NUSGS_UM	UFGSGC		AUS	Condition for discrepant updating
B_SGSAC_UM	UFGSGC		LOK	Condition SGS intervention activ for function monitoring
EI_SGSGC_UM	UFGSGC		AUS	Irreversible error bit for SGS surveillance function monitoring
MBEG_C	UFGSGC		AUS	module-beginning counter for check of the program run (%URPAK)



Variable	Source	Type	Description
MEND_C	UFGSC	AUS	module-end counter for check of program run (%URPAK)
MISGS_UM	UFGSC	LOK	indicated torque request from SGS for monitoring system
MSGSCPL_UM	UFGSC	LOK	One's complement of sum of torque demand and message counter
MSGJ_UM	UFGSC	AUS	desired torque of gear box control at monitoring function
MSGJ_UR	UFGSC	AUS	double storage: msgj_um
MSG_DATA_R		EIN	can message buffer
R10MSCTR		EIN	10ms task-counter of the function
R_FLAGS_UM	UFGSC	AUS	byte for fault reactions of function monitoring
SGSC_C_UM	UFGSC	LOK	debounce counter for transmission monitoring in function monitoring
SGSC_C_UR	UFGSC	LOK	Double storage: sgsc_c_um
SGSNU_C_UM	UFGSC	LOK	Debounce counter for detected information interruption in level 2
SGSNU_C_UR	UFGSC	LOK	Double storage: Debounce counter for detected information interruption in level 2
SRST_UR	UFGSC	AUS	RAM data redundancy for Bit B_srstLum

### FW UFGSC 4.10 Fixed Values

Parameter	Value	Description
SGSC_T_UM		Fault time for SGS intervention surveillance in function monitoring
TSGSCNU_UM		Debounce time for information interruption

### APP UFGSC 4.10 Application hint

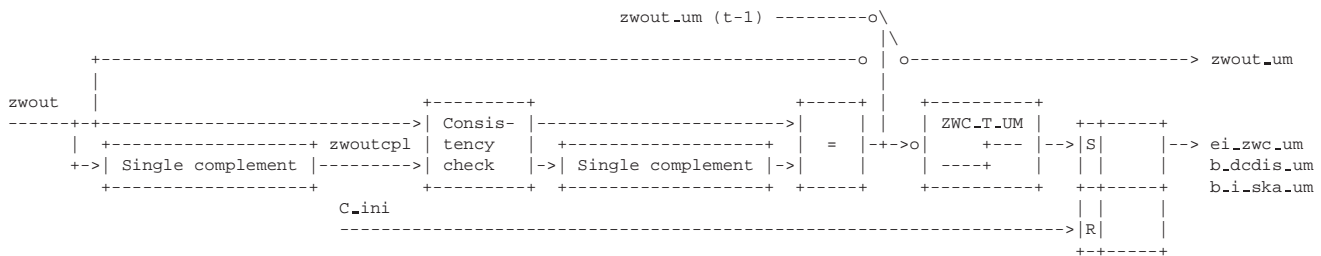
The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

It is important that monitoring in the function (e.g. DCAN, CAN, DCAS) and the monitoring in function surveillance are mutually compatible so that the function does not execute the MSR torque request if a message error has been detected in the function or during function surveillance.

## UFZWC 2.20 ETS monitoring concept: Monitoring of ignition angle for function monitoring

### FDEF UFZWC 2.20 Function definition

Variable from the SYNC matrix ---> | <----- %UFZWC - Ignition-timing monitoring -----> |



### ABK UFZWC 2.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ZWC_T_UM			FW	Fault tolerance time for ignition angle monitoring in function monitoring.
ZYLANZ_UM			FW	Cylinder number for ignition angle monitoring in function monitoring

Variable	Source	Type	Description
B_DCDIS_UM	UFZWC	AUS	Fault reaction information of the function monitoring
B_I_SKA_UM	UFZWC	AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
EI_ZWC_UM	UFZWC	AUS	irrevers. error bit for ignition angle monitoring from function monitoring
ZWC_C_UM	UFZWC	LOK	Error counter for ignition angle monitoring in function monitoring
ZWOUT	ZUE	EIN	Ignition angle output value
ZWOUTCPL	ZUE	EIN	Single complement of the ignition angle for function monitoring
ZWOUT_UM	UFZWC	AUS	Ignition angle in function monitoring

### FW UFZWC 2.20 Fixed Values

Parameter	Value	Description
ZWC_T_UM		Fault tolerance time for ignition angle monitoring in function monitoring.
ZYLANZ_UM		Cylinder number for ignition angle monitoring in function monitoring



## FB UFZWC 2.20 Detailed description of function

Ignition-timing monitoring for function surveillance  
-----

The module must contribute to control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

Statistically, there is an adjustment of the ignition timing to retardation in certain operating states. Such ignition-timing adjustments reduce the engine torque given as an efficiency of 100 %, to e.g. 70 %.

The efficiency or ignition timing must also be taken into account as an input variable of function surveillance because function surveillance executes a torque comparison.

In the event that the ignition timing is acting in function surveillance with an efficiency of e.g. 70 %, and in function surveillance a discrepant ignition timing is taken for an efficiency of e.g. 50 % (value is incorrect from overwriting from another position), then there is a dormant error present. For function surveillance, this means a detected actual torque that is too low for the torque comparison.

If an additional error then occurs in the function that leads to an increase in performance, then function surveillance would not detect this error.

Monitoring the ignition timing is necessary for this reason.

This cannot be interpreted as a double error because without being able to detect the dormant error that can exist over many driving cycles, the performance-increasing error applies in the function as the prime error.

Requirement  
-----

Double storage of the ignition timing is implemented in the SYNC matrix, in that the complement of the current ignition timing zwout (refer to %ZUE) is saved as well after zwoutcpl. A writability check (according to %URMEM) is not necessary because the ignition timing is acting directly as an output variable and the absence of writability does not cause an update of the ignition timing.

Ignition-timing monitoring by plausibility of the double storage  
-----

Consistency check:  
-----

Consistency is assured for the variables zwout and zwoutcpl generated in the SYNC matrix in that both variables are read out twice in succession.

In case zwout from the 1st reading is identical with zwout from the 2nd reading, then zwout, zwoutcpl from the first reading are transferred as the currently applicable variables; otherwise zwout and zwoutcpl from the 2nd reading are taken as the current variables.

Double-storage check:  
-----

Both of the current variables are compared with one another, whereby the one variable must be the complement of the other variable. In the event of an error, the ignition timing zwout\_um is not updated for function surveillance and the error counter is incremented by ZYLANZ\_UM (number of cylinders). An incrementation by ZYLANZ\_UM is necessary in order that a cylinder-specific error will lead to a detection of the error.

The ignition timing zwout\_um is otherwise transferred from the current Variable zwout for function surveillance and the error counter is decremented by 1 to the error-counter status of 0.

## APP UFZWC 2.20 Application hint

The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

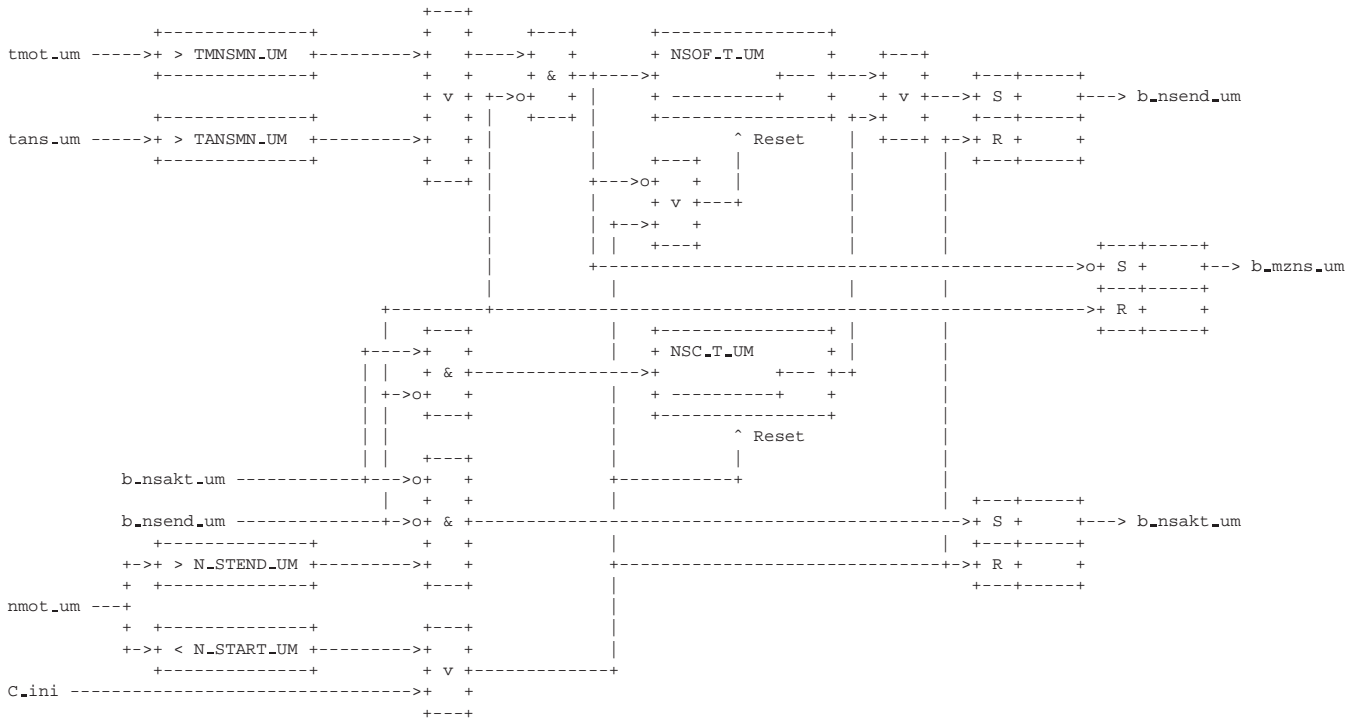
Label	Source	Type	Designation
b_dcdis_um		VAR/AUS	Error-reaction information (shutdown of the throttle-valve actuator output stage) of function surveillance
b_i_ska_um		VAR/AUS	Function surveillance error reaction irrev. SKA (safety fuel shutdown)
ei_zwc_um		VAR/AUS	Irreversible error bit by ignition-timing plausibility of function surveillance
zwout		VAR/EIN	Ignition timing for the function
zwoutcpl		VAR/EIN	Ignition-timing complement for plausibility of the ignition timing in functional surveillance
zwout_um		VAR/AUS	Ignition timing for function surveillance
zwc_c_um		VAR/LOK	Error counter in ignition-timing monitoring

Label	Dependency	Type	Designation
ZYLANZ_UM		FW	Number of cylinders for monitoring the ignition timing in function surveillance
ZWC_T_UM		FW	Error tolerance time in ignition-timing monitoring



## UFNSC 2.10 ETS monitoring concept: Afterstart monitoring for function monitoring

### FDEF UFNSC 2.10 Function definition



### ABK UFNSC 2.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
NSC_T_UM			FW	After-start monitoring time for the watchdog function
NSOF_T_UM			FW	Debouncing time for the switch-off of the after-start expansion
N_START_UM			FW	Engine speed threshold for underspeed exit for the watchdog function
N_STEND_UM			FW	Engine speed threshold for end of start in the watchdog function
TANSMN_UM			FW	Intake air temp. threshold for after-start expansion in the watchdog function
TMNSMN_UM			FW	Engine temp. threshold for the after-start expansion in the watchdog function

Variable	Source	Type	Description
B_MZNS_UM	UFNSC	AUS	afterstart torque increase of ETC-monitoring is active
B_NSACT_UM	UFNSC	LOK	After-start active for the watchdog function
B_NSEND_UM	UFNSC	LOK	After-time monitoring time elapsed for the watchdog function
C_JNI	SWADAP	EIN	ECU-condition for intialisation
NMOT_UM	UFNC	EIN	engine speed in function monitoring
TANS_UM	UFEING	EIN	Intake air temperature of the watchdog function
TMOT_UM	UFEING	EIN	Engine temperature in the watchdog function

### FW UFNSC 2.10 Fixed Values

Parameter	Value	Description
NSC_T_UM		After-start monitoring time for the watchdog function
NSOF_T_UM		Debouncing time for the switch-off of the after-start expansion
N_START_UM		Engine speed threshold for underspeed exit for the watchdog function
N_STEND_UM		Engine speed threshold for end of start in the watchdog function
TANSMN_UM		Intake air temp. threshold for after-start expansion in the watchdog function
TMNSMN_UM		Engine temp. threshold for the after-start expansion in the watchdog function



## FB UFNSC 2.10 Detailed description of function

After-start monitoring for the watchdog function

The module must be of assistance in the check of the program run (see %URPAK).

The RAM and ROM areas affected by the function must be stored cyclically (see %URMEM).

The function is to be processed in the 40ms grid.

In order to improve the monitoring quality it is possible to switch to an increased permissible torque (see %UFMZUL) during the after-start dependent on the engine and intake air temperature.

The after-start expansion becomes active, as soon as the conditions for B\_mzns\_um are fulfilled, that means as soon as

- \* the identifier after-start monitoring times elapsed B\_nsend\_um is not set (B\_nsakt\_um is set) and
- \* the engine temperature is less than the threshold TMNSMN\_UM and
- \* the air temperature is less than the threshold TANSMN\_UM.

The after-start monitoring time (NSC\_T\_UM) is started, if the identifier after-start active (b\_nsakt\_um) is being set.

The irreversible switchover from after-start to normal operation is performed with the resetting of the condition B\_mzns\_um after a debouncing time NSOF\_T\_UM, if

- \* the engine temperature is greater than the threshold TMNSMN\_UM or
- \* the air temperature is greater than the threshold TANSMN\_UM.

Furthermore the switchover is performed compulsorily after the setting of the identifier after-start monitoring time elapsed (b\_nsend\_um).

The transition at the end of the after-start is filtered (see %UFMZP).

In case of an underspeed exit, i.e. engine speed < threshold for start N\_START\_UM, the following actions are performed:

- Clearing of the debouncing time
- Clearing of the after-start monitoring time
- Clearing of the identifier after-start monitoring time elapsed
- Clearing of the identifier after-start active

Cross-reference: This function of the watchdog function corresponds to the after-start detection on the functional level in %MDZUL.

## APP UFNSC 2.10 Application hint

The data of the watchdog function are part of the monitoring concept and they may therefore not be changed arbitrarily.

Label	Source	Type	Description
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b_mzns_um		VAR/AUS	After-start expansion of the perm. torque active for watchdog function
b_nsakt_um		VAR/LOK	After-start active for the watchdog function
b_nsend_um		VAR/LOK	After-start monitoring time elapsed for the watchdog function
tans_um		VAR/EIN	Intake air temperature in the watchdog function
tmot_um		VAR/EIN	Engine temperature in the watchdog function
nmot_um		VAR/EIN	Engine speed for the watchdog function

Label	Dependency	Type	Description
-------	------------	------	-------------

NSOF_T_UM		FW	Debouncing time for switch-off of after-start expansion in the watchdog function
NSC_T_UM		FW	After-start monitoring time for the watchdog function
N_START_UM		FW	Engine speed threshold for underspeed exit for the watchdog function
N_STEND_UM		FW	Engine speed threshold for end of start for the watchdog function

## UFFGRC 1.30 ETS monitoring concept: Monitoring of Cruise Control of function monitoring

### DDEF UFFGRC 1.30 Function definition

```

+---+
b_fgren_um ----->+ +
+ +
b_brems_um ----->+ + b_fgr_um
+ & +----->
+ + |
+ + |
v_fzg_um --->+ > VMIN_UM ----->+ + |
+-----+ +-----+ +-----+ +---+
+---+ +
+ & +-----+
b_fgr ----->+ + |
+---+ |
V mfg_r_um
00 -----o--o----->
mifa_um -----o
    
```



## ABK UFFGRC 1.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
VMIN_UM			FW	Minimum speed for FGR operation in function monitoring
Variable	Source		Type	Description
B_BREMS_UM	UFFGRE		EIN	condition of function monitoring: brake pedal pressed
B_FGR	MDFAW		EIN	condition: driver's set engine torque determined by cruise control
B_FGREN_UM	UFFGRE		EIN	CC/ACC turn-on from control lever valid in function monitoring
B_FGR_UM	UFFGRC		AUS	CC/ACC torque intervention in function monitoring permitted
MFR_UM	UFFGRC		AUS	Torque request from cruise control for function monitoring
MIFA_UM			EIN	FGR-/ACC- or driver requested torque of function for function monitoring
VFZG_UM			EIN	engine speed in function monitoring

## FW UFFGRC 1.30 Fixed Values

Parameter	Value	Description
VMIN_UM		Minimum speed for FGR operation in function monitoring

## FB UFFGRC 1.30 Detailed description of function

Monitoring an increasing intervention in the function surveillance

The module must contribute to control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

The increasing torque intervention is only then transferred from the function when this has been detected as being permissible on the basis on an independent assessment.

A check is made in order to enable an FGR-/ACC intervention as to whether a valid turn-on condition was present and that no shutdown is pending.

A check is made in addition to this whether the brake information is inactive and the minimum speed has been surpassed. Furthermore, the FGR/ACC torque request is only then transferred into the torque coordination of function surveillance when FGR/ACC torque intervention is active in the function.

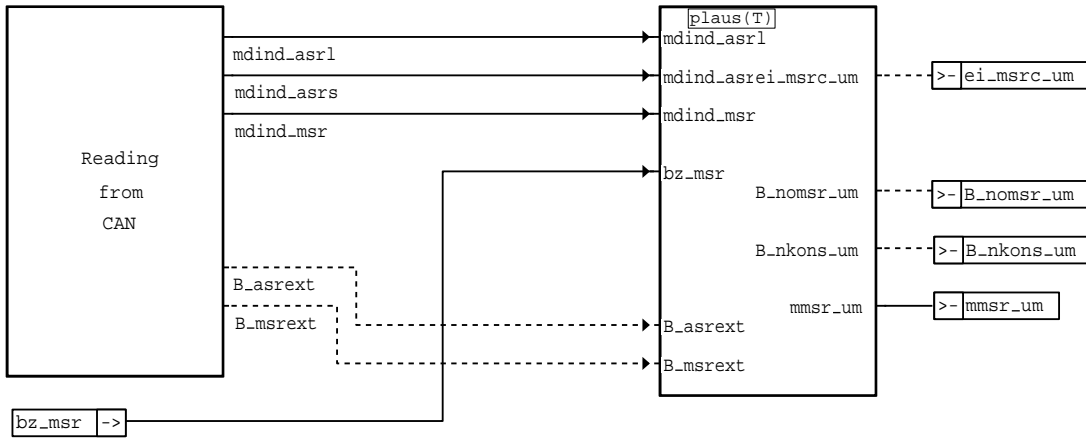
## APP UFFGRC 1.30 Application hint

The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

Label	Source	Art	Designation
b_fgr		VAR/EIN	FGR/ACC torque intervention active
b_fgren_um		VAR/EIN	FGR turn-on condition from operating lever valid without FGR shutdown being present from the function
b_fgr_um		VAR/AUS	FGR/ACC torque intervention permitted in function surveillance
b_brems_um		VAR/EIN	Redundant brake information active in function surveillance
mifa_um		VAR/EIN	FGR-/ACC or driver-requested torque from function in function surveillance
mfr_um		VAR/AUS	Permissible FGR torque for function surveillance
vfzg_um		VAR/EIN	Vehicle speed in function surveillance
Label	Dependency	Art	Designation
VMIN_UM		FW	Minimum speed for FGR operation in function surveillance

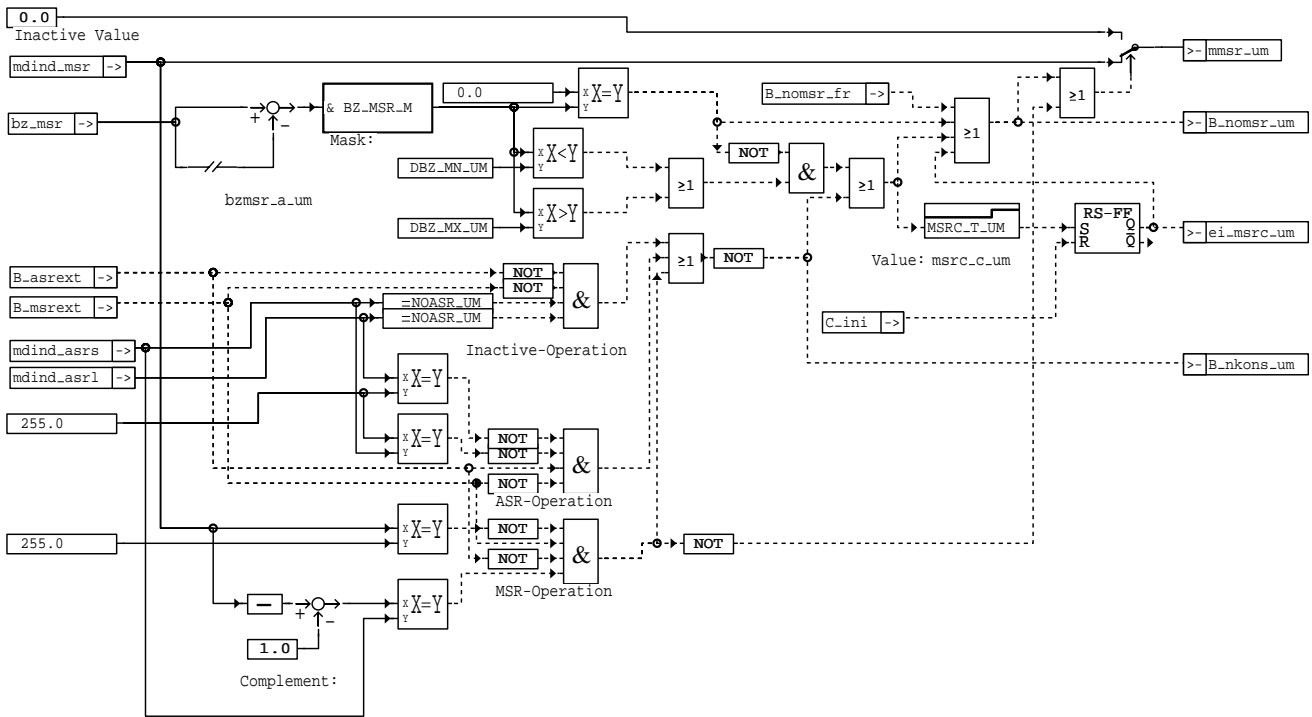
## UFMSRC 5.10 ETS monitoring concept: MSR intervention surveillance for function monitoring

### FDEF UFMSRC 5.10 Function definition



### ufmsrc-ufmsrc

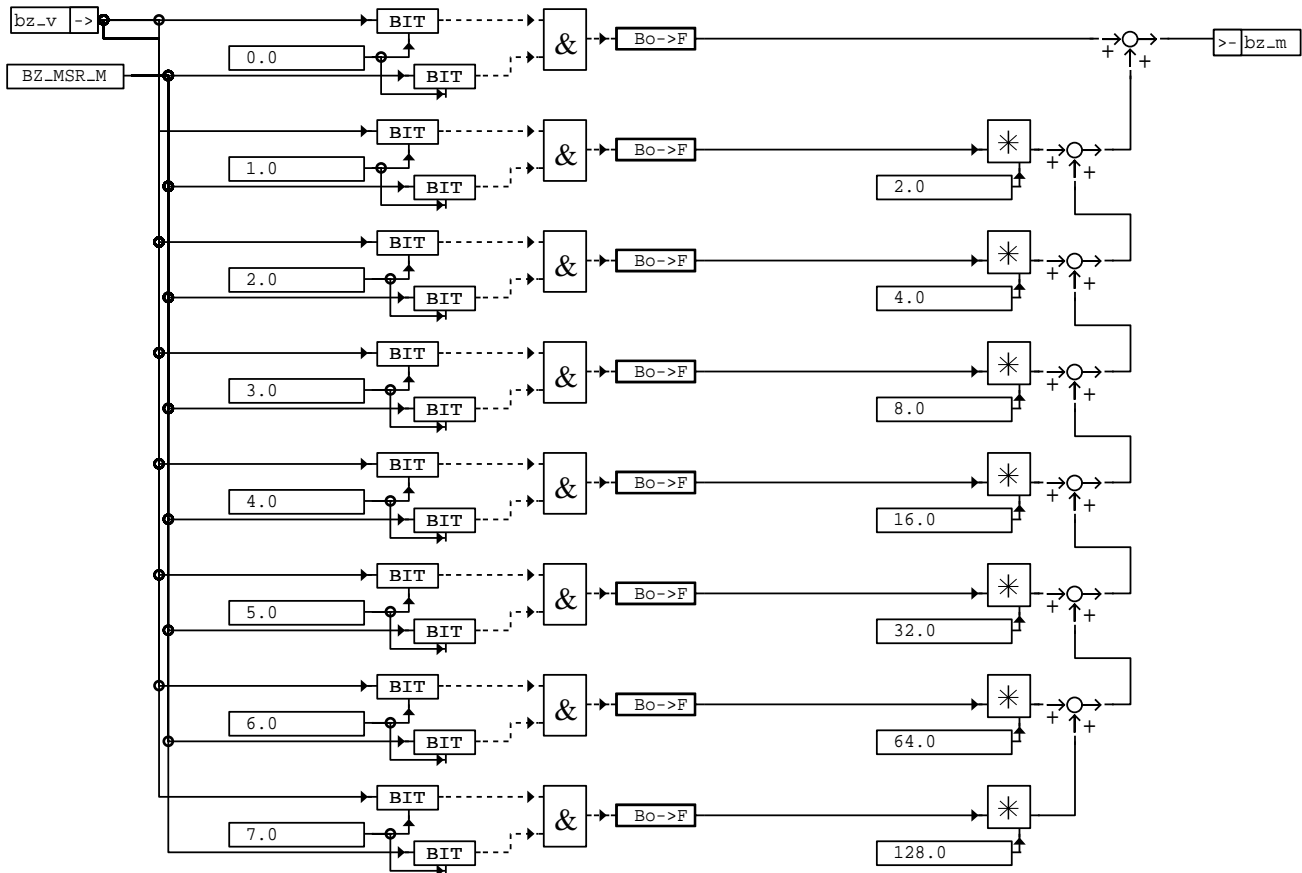
#### Overview



### ufmsrc-plaus



Plausibility Check



**ufmsrc-mask**

Mask (Operation Bit by Bit And)

**FB UFMSRC 5.10 Detailed description of function**

MSR intervention-monitoring of function surveillance

The module must contribute to program-flow control (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

The ASR/MSR data arrive via CAN in the functions computer and are made available for function surveillance without further processing. The data are read out directly from the CAN buffer.

The identifier ei\_msrm is set following elapse of the error tolerance time.

The bit b\_nomsr\_um is deleted if the ASR/MSR data are error-free. The MSR value specified for the torque, md\_ind\_msr, is then transferred into the incrementation value mmsr\_um for 'MSR-intervention plausible'. The MSR torque-increase request mmsr\_um is otherwise set to 0.



Monitoring for updatedness  
-----

- The 4-bit message counter `bz_msr` is incremented from the transmitting control unit. If the message counter is incremented every 10 ms, then the old and the new message counters differ by at least three and by a maximum of five in each 40-ms test cycle. If the message counter is incremented by the control unit every 20 ms, then the old and the new message counter differs by at least one and by a maximum of three in each 40-ms test cycle.

For detection of discrepant updating, i.e. in case the old and the new message counters do not differ, there is only one reversible error reaction active since an interruption in the CAN message shall not lead to a ban of the function until 'Ignition off'.

Monitoring for plausibility and message consistency  
-----

1) ASR active message (`b_asrext=1`)

- MSR inactive (`b_msrext=0`)
- `miasrl_can`

255

- `miasrs_can`

255

2) MSR active message (`b_msrext=1`)

- ASR inactive (`b_asrext=0`)
- ASR torque requirement for rapid intervention for assurance of the MSR values `mdind_asrs = CPL (mdind_msr)`
- `mimsr_can`

255

3) Inactive message (`b_asrext=0` and `b_msrext=0`)

- ASR torque requirement for rapid intervention inactive, i.e. `mdind_asrs = NOASR_UM`
- ASR torque requirement for intervention via air path inactive, i.e. `mdind_asrl = NOASR_UM`

## ABK UFMSRC 5.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
BZ_MSR_M			FW	MSR message counter mask (0Fh for 4-bit message counter)
DBZ_MN_UM			FW	Smallest permissible delta of the message counter
DBZ_MX_UM			FW	Largest permissible delta of the message counter
MSRC_T_UM			FW	Error tolerance time for monitoring of MSR intervention in function monitoring
NOASR_UM			FW	Inactive mask for ASR

Variable	Source	Type	Description
BZMSR_A_UM	UFMSRC	LOK	Old MSR message counter
BZ_M	UFMSRC	DOK	CAN message counter after masking
BZ_MSR		EIN	MSR message counter
BZ_V	UFMSRC	DOK	message counter prior to the masking
B_ASREXT	UFMSRC	LOK	condition for externe ASR
B_MSREXT	UFMSRC	LOK	Condition external MSR demand
B_NKONS_UM	UFMSRC	AUS	Condition MSR message is not consistent
B_NOMSR_FR	CAN	EIN	No ASR-/MSR intervention from FR
B_NOMSR_UM	UFMSRC	AUS	MSR moment required not used in function monitoring
C_JNI	SWADAP	EIN	ECU-condition for intialisation
EI_MSR_C_UM	UFMSRC	AUS	Irreversible error bit for monitoring of MSR in function monitoring
MDIND_ASRL	UFMSRC	LOK	ASR moment requirement for intervention over air path
MDIND_ASRS	UFMSRC	LOK	ASR moment requirement for rapid intervention
MDIND_MSR	UFMSRC	LOK	MSR moment requirement
MMSR_UM	UFMSRC	AUS	Permissible MSR torque request for function monitoring
MSRC_C_UM	UFMSRC	LOK	Error counter for monitoring of MSR intervention of function monitoring

## FW UFMSRC 5.10 Fixed Values

Parameter	Value	Description
BZ_MSR_M		MSR message counter mask (0Fh for 4-bit message counter)
DBZ_MN_UM		Smallest permissible delta of the message counter
DBZ_MX_UM		Largest permissible delta of the message counter
MSRC_T_UM		Error tolerance time for monitoring of MSR intervention in function monitoring
NOASR_UM		Inactive mask for ASR





## FB UFMZF 1.10 Detailed description of function

Torque filter for the function surveillance

The module must contribute to control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40-ms time frame.

Delays occur for jumps from full load to idle-speed for the air mass measured in the manifold and are converted into a load signal. This means a lower value for the permissible torque. The actual torque that essentially depends on the load signal and the engine speed supplies higher values however during this delay.

In order that the function surveillance does not respond on account of an actual-torque value that is too high compared with the permissible torque, the permissible torque is delayed over a dead time and filtered by a low-pass filter of the first order, i.e. clearing the manifold pipe for a falling driver-requested torque is simulated by this.

The dead time and the low-pass filter do not act for jumps in the torque from idle-speed to full load because functional monitoring allows an actual torque that is too low compared with the permissible torque.

## APP UFMZF 1.10 Application hint

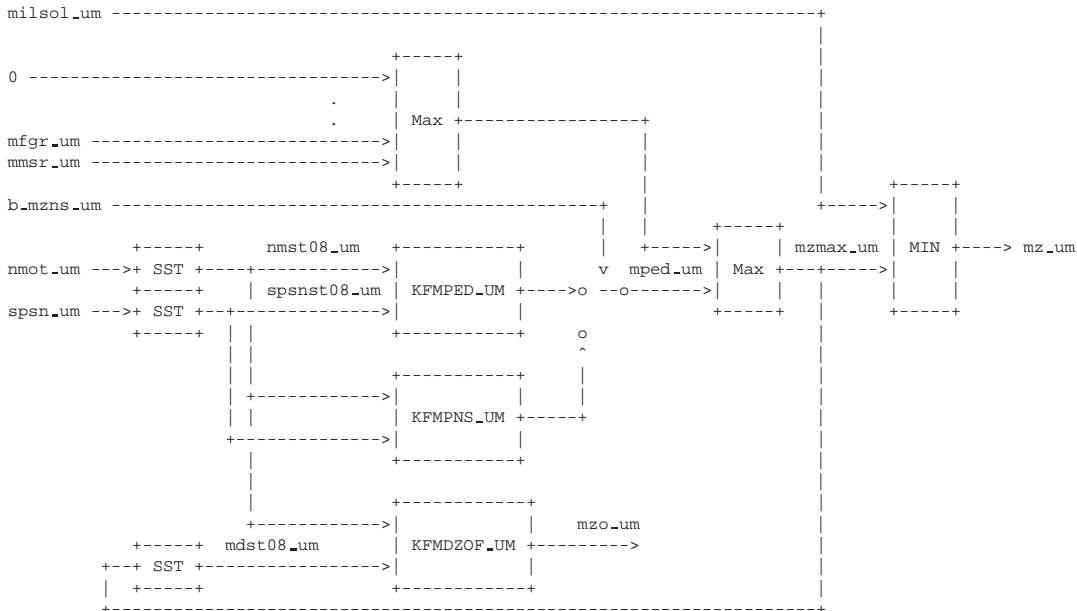
The data of function surveillance are part of the monitoring concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
mz_um		VAR/EIN	Permissible torque from the driver request
mzf_um		VAR/AUS	Filtered permissible torque
mzf_low_um		VAR/LOK	Filtered permissible torque carried to after the decimal point

Label	Dependency	Type	Designation
MZFTV_UM		FW	Delay time for permissible torque MZ_UM
MZFFIL_UM		FW	Filter time constant for delayed torque

## UFMZUL 5.10 ETS monitoring concept: Calculation of permissible torque in UF

### FDEF UFMZUL 5.10 Function definition



### ABK UFMZUL 5.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFMZOF_UM	MZ_UM	NMOT_UM	KF	map for offset tolerance depending on permissible torque
KFMPEP_UM	SPSN_UM	NMOT_UM	KF	map for permissible torque from the pedal position in function monitoring
KFMPEPNS_UM	SPSN_UM	NMOT_UM	KF	map for permissible torque from pedal position for a cold engine
Variable	Source	Type	Description	
B_MZNS_UM	UFNSC	EIN	afterstart torque increase of ETC-monitoring is active	
MFGR_UM	UFFGRC	EIN	Torque request from cruise control for function monitoring	
MMSR_UM	UFMSRC	EIN	Permissible MSR torque request for function monitoring	



Variable	Source	Type	Description
MPED_UM	UFMZUL	LOK	Permissible indicated torque from accelerator pedal in function monitoring
MZMAX_UM	UFMZUL	LOK	Permissible torque from the maximum selection in function monitoring
MZO_UM	UFMZUL	AUS	Tolerance offset for permissible torque in function monitoring
MZ_UM	UFMZUL	AUS	Permissible torque resulting from the coordination of function monitoring

### FW UFMZUL 5.10 Fixed Values

Parameter	Value	Description
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### FB UFMZUL 5.10 Detailed description of function

Permissible Torque of the Watchdog Function

The module must be of assistance in the check of the program execution (see %URPAK).

The RAM and ROM areas affected by the function must be stored cyclically (see %URMEM).

The function shall be processed in the 40ms cycle.

The torque KFMPED\_UM permissible due to the accelerator position is calculated (and filtered, cf. %UFMZP) via a map interpolation dependent on the pedal set point and the engine speed. The offset is stored in the map KFMDZOF in dependency on the permissible torque mz\_UM and on the engine speed. The offset torque mzo\_UM is not filtered. Due to the addressing of the offset over engine speed and permissible desired torque a high offset can be used for high permissible torque.

As long as the bit B\_mzns\_UM is active during post-start (cf. %UFNSC), the map KFMPNS\_UM (instead of KFMPED\_UM) is used with cold engine. This map is also filtered and the same offset is taken into account. Thereby the increased drag torque at cold engine can on one hand be taken into consideration, on the other hand it is possible to reduce the permissible torque at warm engine so as to achieve a controllable reaction in case of a fault.

With permitted increasing torque intervention by the road speed controller mfr\_UM from %UFFGRC or with permitted increasing torque intervention of the MSR mmsr\_UM from %UFMSRC the permissible torque becomes valid by the maximum selection between mped\_UM, mfr\_UM and mmsr\_UM. Future external interventions, which must additionally be secured, are taken into account in the maximum selection between mfr\_UM and mmsr\_UM. This is expressed in the function definition by the points and the input with 0.

Thereafter the minimum selection between the mzmax\_UM determined by the coordination of the permissible torque and the currently valid desired torque for the air path milsol\_UM is formed. The resulting permissible torque can thereby pass through the subsequent torque filter for the elimination of the manifold time constant. In addition the watchdog function is thus - with correct milsol - used for the fact that no higher torque than desired is allowed for.

Cross reference: This function of the watchdog function corresponds to the function %MDZUL in the functional plane.

### APP UFMZUL 5.10 Application hint

The data of the watchdog function are part of the monitoring concept and they may therefore not be changed arbitrarily.

Label	Source	Type	Description
b_mzns_UM		VAR/EIN	Condition for permissible torque during post-start
mped_UM		VAR/LOK	permissible torque from the pedal position
mfr_UM		VAR/EIN	permissible torque from the road speed control
mmsr_UM		VAR/EIN	permissible torque from the MSR setting
mzo_UM		VAR/AUS	tolerance offset for the permissible torque
mz_UM		VAR/AUS	resulting permissible torque
mzmax_UM		VAR/LOK	permissible torque from the maximum selection in the coordination

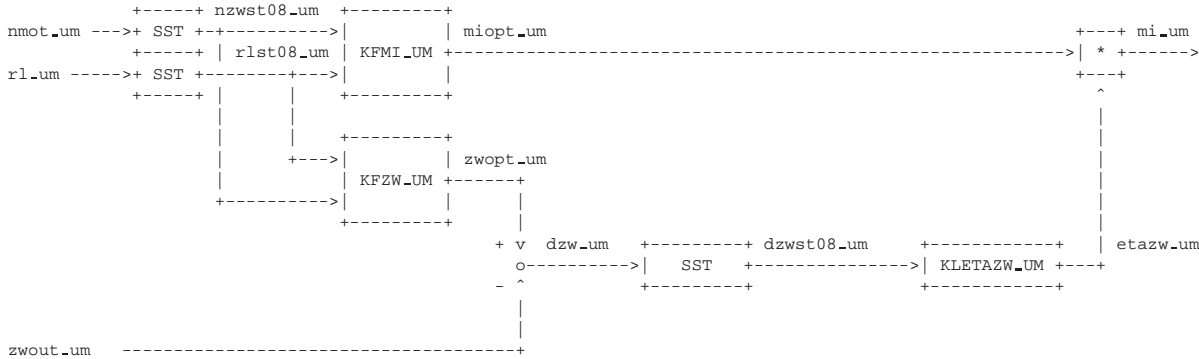
Label	Dependency	Type	Description
SPSNV08_UM	spsn_UM	KL	pedal set point base points
NMV08_UM	nmot_UM	KL	engine speed base points for torque
MDST_08_UM	mz_UM	KL	torque base points
KFMPED_UM	spsnst08_UM, nmst08_UM	KF	map for permissible torque from the pedal position
KFMPNS_UM	spsnst08_UM, nmst08_UM	KF	map for permissible torque from the pedal position during post-start
KFMDZOF_UM	mdst08_UM, nmst08_UM	KF	map for offset tolerance in dependency on the permissible torque

While the offset so far was stored dependent on engine speed and pedal set point (KFMDZOF\_UM) it is now stored dependent on permissible torque and engine speed (KFMDZOF). Changing the data is possible as follows:  
For a fixed engine speed and a fixed pedal set point an offset torque is obtained from the map KFMDZOF. This offset is now entered into the map KFMDZOF for the respective engine speed base points and the torque base point, which results from the map KFMPED\_UM (at same engine speed and same pedal angle).



## UFMIST 2.10 ETS monitoring concept: Calculation of the actual torque in UF

### FDEF UFMIST 2.10 Function definition



### ABK UFMIST 2.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KFMI_UM	RL_UM	NMOT_UM	KF	map of optimum engine torque
KFZW_UM	RL_UM	NMOT_UM	KF	map of optimum ignition angle
KLETAZW_UM	DZW_UM		KL	ignition efficiency depending on delta ignition angle

Variable	Source	Type	Description
DZW_UM	UFMIST	LOK	Delta ignition angle between zwopt and zwout in function monitoring
ETAZW_UM	UFMIST	LOK	Efficiency of actual ignition angle in function monitoring
MIOPT_UM	UFMIST	LOK	Optimum indicated torque in function monitoring
MI_UM	UFMIST	AUS	Calculated actual torque in function monitoring
NMOT_UM	UFNC	EIN	engine speed in function monitoring
RL_UM		EIN	Relative air charge in function monitoring
ZWOPT_UM	UFMIST	LOK	Optimum ignition angle in function monitoring
ZWOUT_UM	UFZWC	EIN	Ignition angle in function monitoring

### FW UFMIST 2.10 Fixed Values

Parameter	Value	Description
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### FB UFMIST 2.10 Detailed description of function

Actual moment of function monitoring

The module must contribute to the control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processed in the 40 ms time frame.

The actual moment is calculated as a function of the speed, load and ignition timing.  
The ignition timing is thereby defined as positive in front of OT and negative after OT.

### APP UFMIST 2.10 Application hint

The data from function monitoring are part of the surveillance concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
rl_um		VAR/EIN	Relative air charge in function monitoring
zwout_um		VAR/EIN	Actual ignition timing in function monitoring
nmot_um		VAR/EIN	Engine speed in function monitoring
miopt_um		VAR/LOK	Optimum induced moment in function monitoring
zwopt_um		VAR/LOK	Optimum ignition timing in function monitoring
dzw_um		VAR/LOK	Difference in ignition timing in function monitoring
etazw_um		VAR/LOK	Ignition timing in function monitoring
mi_um		VAR/AUS	Actual moment in function monitoring

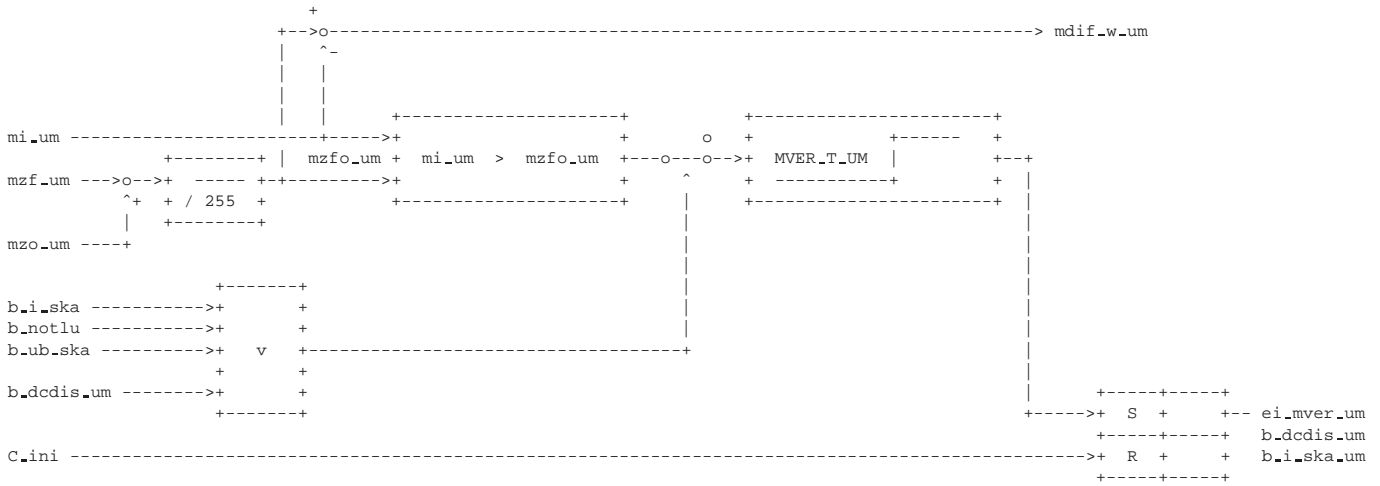
  

Label	Dependency	Load	Designation
RLV08_UM	rl_um	KL	Load signal setpoints in function monitoring
NZWV08_UM	nmot_um	KL	Speed setpoints for determining the actual moment in function monitoring
DZWV08_UM	dzw_um	KL	Speed setpoints for difference in ignition timing
KFMI_UM	rlst08_um, nzwst08_um	KF	Performance characteristics for optimum induced moment in function monitoring
KFZW_UM	rlst08_um, nzwst08_um	KF	Performance characteristics for optimum ignition timing in function monitoring
KLETAZW_UM	dzwst08_um	KL	Characteristic for ignition timing efficiency in function monitoring



## UFMVER 2.10 ETS monitoring concept: Torque comparison of function monitoring

### FDEF UFMVER 2.10 Function definition



### ABK UFMVER 2.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
MVER_T_UM			FW	Fault time for moment comparison in function monitoring
Variable	Source		Type	Description
B_DCDIS_UM	UFMVER		AUS	Fault reaction information of the function monitoring
B_I_SKA	UFEING		EIN	FR error reaction irreversible SKA (safety fuel shut-down)
B_I_SKA_UM	UFMVER		AUS	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B_NOTLU	UFEING		EIN	Request standby air driving from the function
B_UB_SKA	UFEING		EIN	Battery voltage not OK, undervoltage shut-off active
EIMVER_UM	UFMVER		AUS	Irreversible error bit for torque comparison from function monitoring
MDIF_W_UM	UFMVER		AUS	Difference between permissible and actual torque in function monitoring
MI_UM	UFMIST		EIN	Calculated actual torque in function monitoring
MVER_C_UM	UFMVER		LOK	Error counter for torque comparison of function monitoring
MZFO_UM	UFMVER		LOK	Filtered permissible moment including offset in function monitoring
MZF_UM	UFMZ		EIN	Filtered permissible torque of function monitoring
MZO_UM	UFMZUL		EIN	Tolerance offset for permissible torque in function monitoring

### FW UFMVER 2.10 Fixed Values

Parameter	Value	Description
MVER_T_UM		Fault time for moment comparison in function monitoring

### FB UFMVER 2.10 Detailed description of function

Moment comparison in function monitoring

The module must contribute to the control of the program sequence (refer to %URPAK).

The RAM and ROM ranges affected by the function must be cyclically safeguarded (refer to %URMEM).

The function shall be processing in the 40 ms time frame.

During moment comparison, the actual moment (refer to %UFMIST) is checked if this has exceeded the permissible moment (refer to %UFMZUL).

A comparison of the moment cannot be performed if the nominal pedal value has not been updated because the supply to the pickup is no longer assured.

Thus the moment comparison is not executed for an undervoltage shut-off of the DK actuator output stage.

If the fault response "DK actuator output stage currentless" is effective because of other faults, there shall be no detection of faults in the moment comparison in addition to these.

It is for this reason that the moment comparison is no longer executed in this case either.

In this case a check is then made in the fault response surveillance of function monitoring (%UFREAC) as to whether the undervoltage shut-off or the fault response "DK actuator output stage currentless" is in fact executed and not just indicated.

If the actual moment exceeds the permissible moment for longer than an applicable fault time MVER\_T\_UM, then the fault bit ei\_mver\_um, the fault response information b\_dcdis\_um (shut-down of the DK actuator output stage) and the function monitoring fault response b\_i\_ska\_um (irreversible SKA) are set.

If the actual moment mi\_um is not greater than the permissible moment mzf\_o\_um which is given by adding the filtered permissible moment mzf\_um to the tolerance offset mzo\_um, then the fault counter mver\_c\_um is deleted.



## APP UFMVER 2.10 Application hint

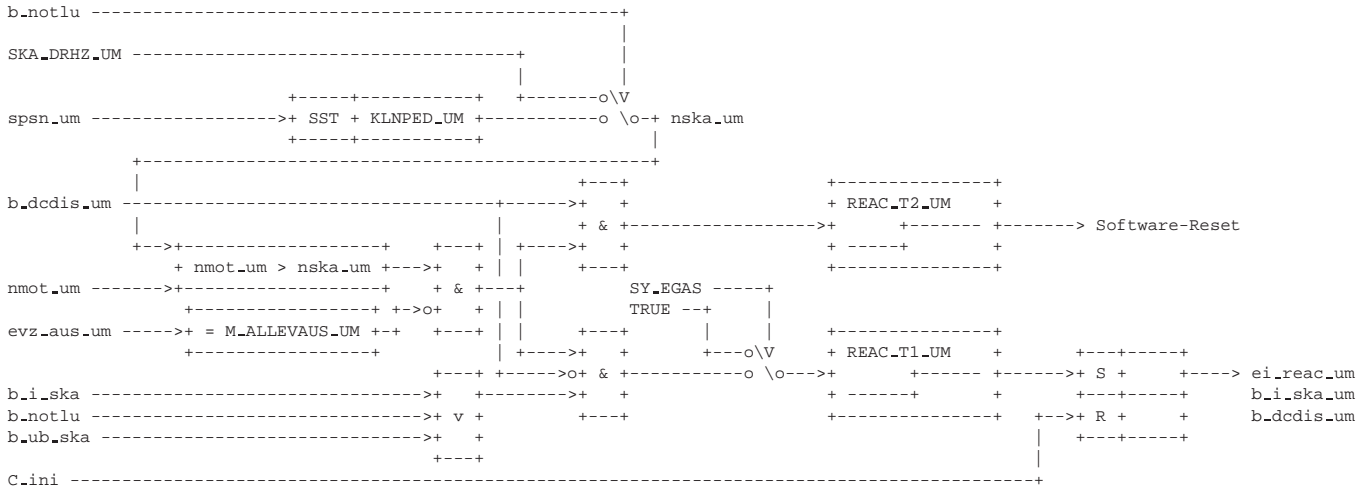
The data in function monitoring are part of the surveillance concept and therefore may not be arbitrarily changed.

Label	Source	Type	Designation
mzf_um		VAR/EIN	Filtered permissible moment
mzfo_um		VAR/EIN	Filtered permissible moment with offset
mzo_um		VAR/EIN	Offset for permissible moment
mi_um		VAR/EIN	Actual moment
mdif_w_um		VAR/AUS	Difference between permissible and actual moment
mver_c_um		VAR/LOK	Fault counter for moment comparison in function monitoring
ei_mver_um		VAR/AUS	Irreversible fault bit for moment comparison in function monitoring
b_dcdising		VAR/AUS	Fault response information (shut-down of the DK actuator output stage) in function monitoring
b_i_ska_um		VAR/AUS	Function surveillance fault response irrev. SKA (safety fuel shut-off)
b_i_ska		VAR/EIN	Function fault response irreversible SKA (safety fuel shut-off)
b_notlu		VAR/EIN	Function fault response DK actuator ES currentless
b_ub_ska		VAR/EIN	Undervoltage shut-off of the DK actuator output stage active

Label	Dependency	Type	Designation
MVER_T_UM		FW	Fault time for moment comparison in function monitoring

## UFREAC 4.30 ETS monitoring concept: Monitoring of fault reaction of function monitoring

### FDEF UFREAC 4.30 Function definition



### ABK UFREAC 4.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
KLNPED_UM	SPSN_UM		KL	Speed lim. as func. of nominal pedal value, in DK drive standby func.,func.mon.
NOREA_UM			FW	ident. to request no engine operation possible from %UFREAC of watchdog function
REAC_T1_UM			FW	Fault time for functional-fault reaction monitoring in UF
REAC_T2_UM			FW	Fault time for function monitoring - fault reaction monitoring in UF
RST_TV_UM			FW	Identifier for requesting a reset pulse control factor from function monitoring
SKADRHZ_UM			FW	Engine limiting speed for entire fuel cut-off SKA
SY_EGAS			SYS	System constant E-GAS present
WAIT_T_UM			FW	Waiting time for reset pulse duty cycle from the watchdog function

Variable	Source	Type	Description
B_DCDIS_UM	UFREAC	AUS	Fault reaction information of the function monitoring
B_I_SKA	UFEING	EIN	FR error reaction irreversible SKA (safety fuel shut-down)
B_I_SKA_UM	UFREAC	AUS	Fault reaction demand from function monitoring: irrev.SK A (safety fuel cut-off)
B_NOTLU	UFEING	EIN	Request standby air driving from the function
B_UB_SKA	UFEING	EIN	Battery voltage not OK, undervoltage shut-off active
C_INI	SWADAP	EIN	ECU-condition for intialisation
EI_REAC_UM	UFREAC	AUS	irreversible error bit of fault reaction monitoring from function monitoring
EVZ_AUS_UM	UFEING	EIN	Injection cut off pattern in function monitoring
NMOT_UM	UFNC	EIN	engine speed in function monitoring
NSKA_UM	UFREAC	LOK	Limiting speed for active fault response in function monitoring
REAC_C1_UM	UFREAC	LOK	error counter 1 for fault reaction monitoring in function monitoring response
REAC_C2_UM	UFREAC	LOK	error counter 2 for fault reaction monitoring in function monitoring
REAC_C_UM	UFREAC	LOK	Fault counter in perm. RAM for monitor. of fault react. (diag.) in watchdog func
RST_TV	UFREAC	AUS	Variable in the permanent RAM for reset pulse control factor from funct. monito.
SPSN_UM	UFSPSC	EIN	Pedal value (8-bit) with lower limit to idling in function monitoring





## FW UFREAC 4.30 Fixed Values

Parameter	Value	Description
NOREA_UM		ident. to request no engine operation possible from %UFREAC of watchdog function
REAC_T1_UM		Fault time for functional-fault reaction monitoring in UF
REAC_T2_UM		Fault time for function monitoring - fault reaction monitoring in UF
RST_TV_UM		Identifier for requesting a reset pulse control factor from function monitoring
SKADRHZ_UM		Engine limiting speed for entire fuel cut-off SKA
WAIT_T_UM		Waiting time for reset pulse duty cycle from the watchdog function

## FB UFREAC 4.30 Detailed description of function

Fault Reaction Monitoring of the Watchdog Function  
-----

The module must be of assistance in the check of the program execution (see %URPAK).

The RAM and ROM areas affected by the function must be stored cyclically (see %URMEM).

Within this function only the temporary variables may be used for intermediate variables. These are used in the command test (cf. %URCPU) in the same way and they have therefore been checked for writability.

Within this function separate routines of the watchdog function of the software module UFIUP (no FDEF) need to be used for interpolations.

The function is to be processed in the 40ms cycle.

The functionality of the fault reactions needs to be monitored.

This is important, since the fault reaction needs to be definitely performed for the watchdog function.

This applies to fault reactions from the function on the basis of which the watchdog function is either totally or partially deactivated and also to the fault reactions from the watchdog function, without which it would not reach its target of performance reduction in case of fault.

If a desired deactivation of the throttle actuator output stage with the accompanying speed limitation via injection cut-out does not take place, then in case of deactivation request from the function an attempt is made after a defined fault-tolerance time to activate on an additional path by means of the fault-reaction request and information in the watchdog function.

If the deactivation of the throttle actuator output stage was initiated by the watchdog function, then in case of a fault, i.e. if the speed limitation via injection cut-out does not become active, a software reset is triggered after a defined fault-tolerance time. In this case, the identifier is loaded into the permanent RAM for reset duty cycle prior to the software reset being triggered.

Via this identifier the RAM and ROM check (usually taking place during the after-run) as well as a defined waiting time prior to output stage enabling resp. to end of initialization is activated during the subsequent initialization.

(Interim solution beginning)

If the adjustable identifier NOREA\_UM has not been set or if the software reset was not triggered from here (%UFREAC).

If the adjustable identifier NOREA\_UM has been set and if the software reset was triggered from here (%UFREAC), the identifier reset duty cycle is cleared and a jump to the boot block resp. to the internal ROM is performed. In this operating mode no engine operating is any longer possible but only the possibility exists to program the flash content anew. This operating mode can only be exited, if terminal 15 is switches off and hence on again.

After terminal 15 = on, normal operation is resumed. Should a permanent fault trigger this fault reaction again, this again leads to engine operation any longer possible. The driver therefore decides by himself, whether or how long he wants to keep engine operation off, if a permanent fault is given.

(Interim solution end)

Remark regarding the described Interim solution:

Demand made by Audi, VW for a quicker conversion for series production

If the system constant SY\_EGAS is false in an EGAS-system, then the function UFREAC requests a safety fuel deactivation. Since the EGAS-relevant parts are not compiled at not set system constant SY\_EGAS in the function AEVAB, it is not possible for the function AEVAB to translate the safety fuel deactivation.

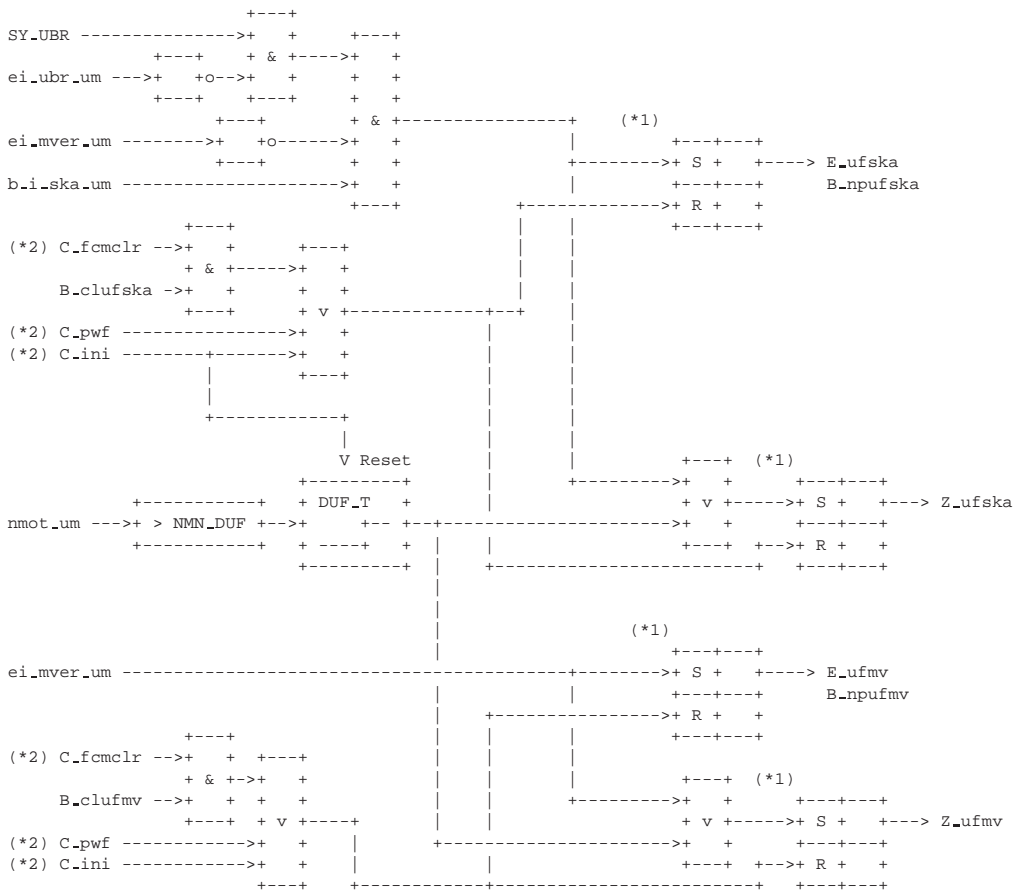
The system constant SY\_EGAS is checked already during the compiling procedure. If it is not defined in EGAS-systems, the fault message is made that it needs to be defined. A fault message is also made, if the system constant exists but if it has been set to false. No code is generated in either case. This is illustrated in the diagram by the reset.

## APP UFREAC 4.30 Application hint

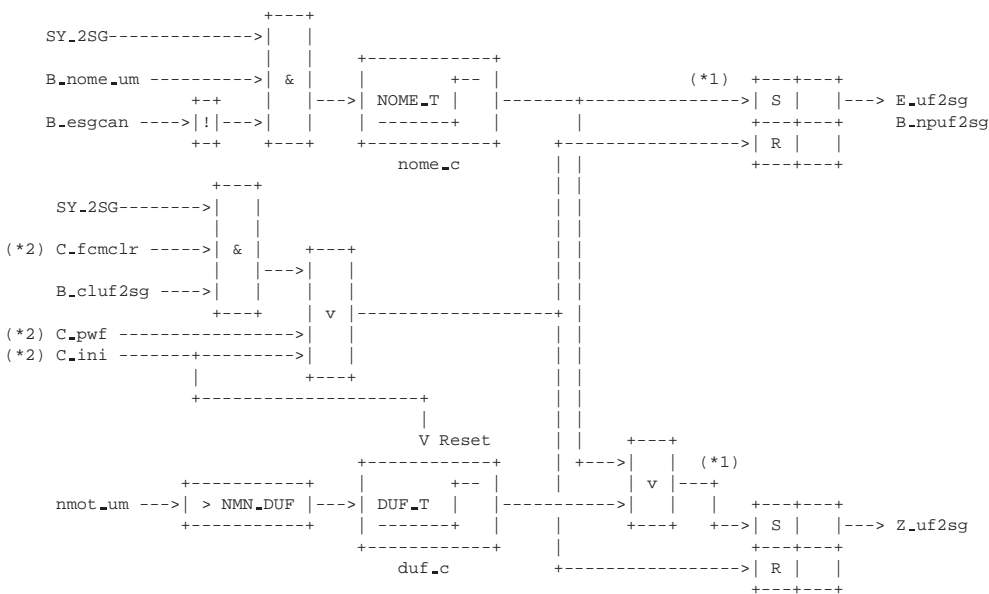
The data of the watchdog function are part of the monitoring concept and may not be changed arbitrarily.

## DUF 6.30 Diagnostic interface of the function monitoring

### FDEF DUF 6.30 Function definition

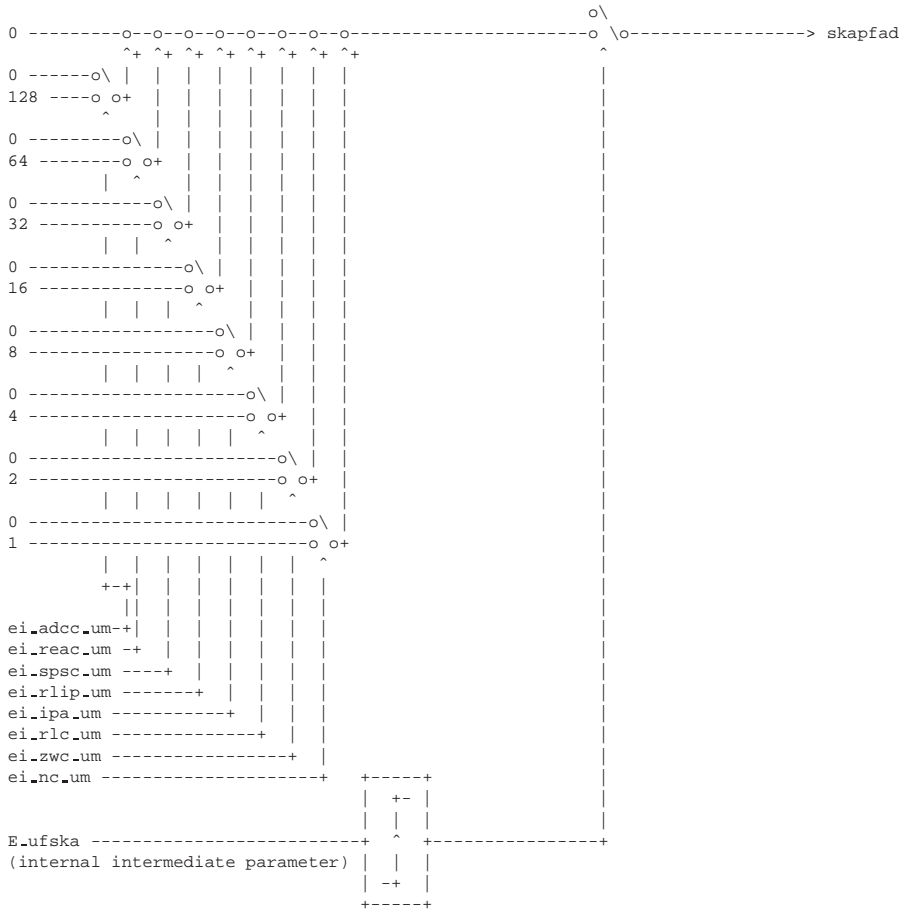


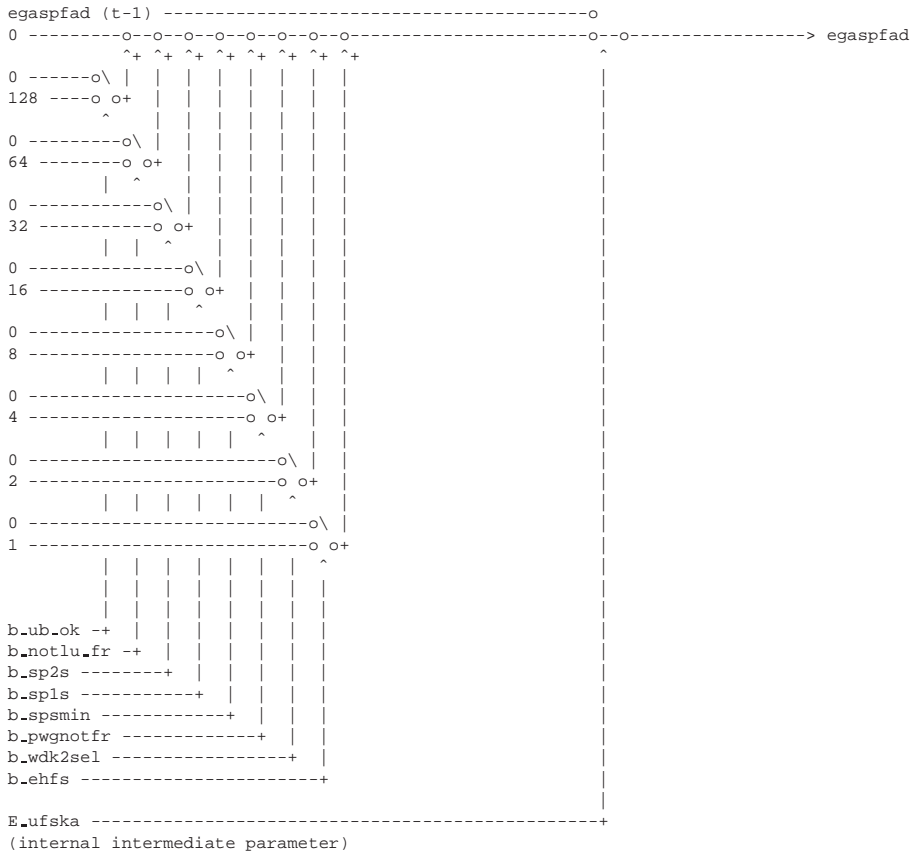
- (\*1): Contrary to the description, this part is realized in the module %DFPM
- (\*2): The activities triggered by C.(\*) are implemented in separate processes in the SW

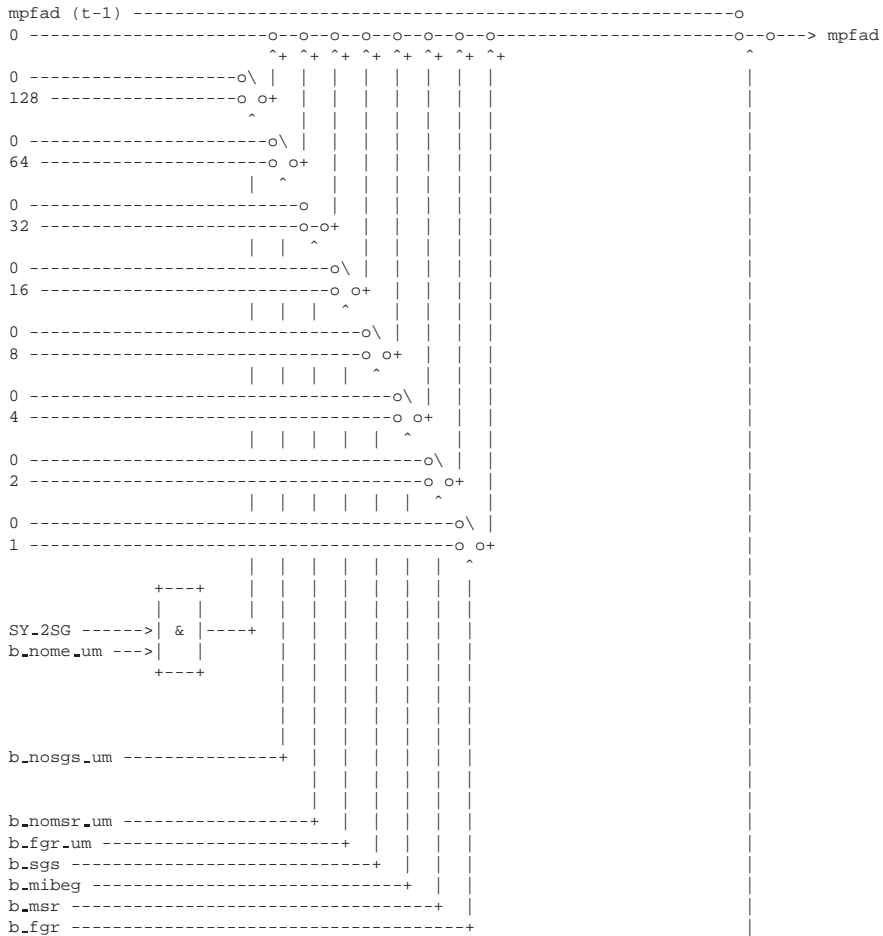


The code is only produced, if SY\_2SG is set.

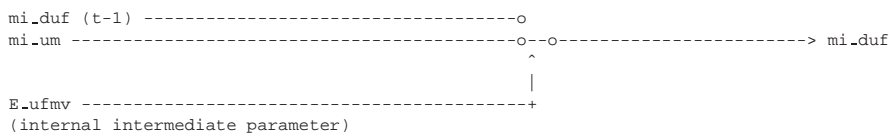
- (\*1): Contrary to the description, this part is realized in the module %DFPM
- (\*2): The activities triggered by C.(\*) are implemented in separate processes in the SW







E\_ufmv  
(internal intermediate parameter)



E\_ufska:

Environmental condition 1 : skapfad      Environmental condition 2 : egaspfad

E\_ufmv:

Environmental condition 1 : mpfad      Environmental condition 2 : mi\_duf

E\_uf2sg:

Environmental condition 1: mer\_cl\_um      Environmental condition 2 : mer\_c2\_um

### ABK DUF 6.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCUF2SG	BLOKNR		KL	Code word CARB: monitoring of the function: data from other ECU
CDCUFMV	BLOKNR		KL	Code word CARB: monitoring of the function: torque comparison
CDCUFSKA	BLOKNR		KL	Code word CARB: monitoring of the function: safety fuel cut-off
CDKUF2SG			FW	Code word customer: monitoring of the function: data from other ECU
CDKUFMV			FW	Code word customer: monitoring of the function: torque comparison
CDKUFSKA			FW	Code word customer: monitoring of the function: safety fuel cut-off
CDTUF2SG			FW	Code word tester: monitoring of the function: data from other ECU
CDTUFMV			FW	Code word tester: monitoring of the function: torque comparison



Parameter	Source-X	Source-Y	Type	Description
CDTUF2SG			FW	Code word tester: monitoring of the function: safety fuel cut-off
CLAUF2SG			FW	Fault class: monitoring of the function: data from other ECU
CLAUFMV			FW	Fault class: monitoring of the function: torque comparison
CLAUF2SG			FW	Fault class: monitoring of the function: safety fuel cut-off
DUF.T			FW	time for setting the cycle flags of function monitoring diagnosis
FFTUF2SG	BLOKNR		KL	Freeze frame table: monitoring of the function: data from other ECU
FFTUFMV	BLOKNR		KL	Freeze frame table: monitoring of the function: torque comparison
FFTUF2SG	BLOKNR		KL	Freeze frame table: monitoring of the function: safety fuel cut-off
NMN.DUF			FW	engine speed threshold for setting the cycle flag of the function monitoring dia
NOME.T			FW	Time for fault detection UF2SG
SY_2SG			SYS	system constant 2 motronic systems
SY_UBR			SYS	system constant: Voltage behind main relay ubr exists
TSFUF2SG			FW	Fault active time: monitoring of the function: data from other ECU
TSFUFMV			FW	Fault active time: monitoring of the function: torque comparison
TSFUF2SG			FW	Fault active time: monitoring of the function: safety fuel cut-off

Variable	Source	Type	Description
B.CLUF2SG		EIN	flag for clearing measures: watchdog function: data of the other ME
B.CLUFMV		EIN	Flag for clearance: monitoring of the function: torque comparison
B.CLUF2SG		EIN	Flag for clearance: monitoring of the function: safety fuel cut-off
B.EHFS	DHFM	EIN	Condition substitute value main charge sensor
B.ESGCAN		EIN	Condition error ecu-CAN for 2 ME-ecu's
B.FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control
B.FGR.UJM	UFUE	EIN	CC/ACC torque intervention in function monitoring permitted
B.J.SKA.UJM	UFREAC	EIN	Fault reaction demand from function monitoring: irrev.SKA (safety fuel cut-off)
B.MIBEG	MDKOG	EIN	condition torque limit active
B.MSR	MDKOG	EIN	Condition MSR
B.NOME.UJM	UFMER	EIN	Condition replacement values are used caused by failures in the recieved message
B.NOMSR.UJM	UFUE	EIN	MSR moment required not used in function monitoring
B.NOSGS.UJM	UFSGSC	EIN	SGS moment required not transferred to function monitoring
B.NOTLU.FR	SREAKT	EIN	Request for NFB from Function controller
B.NPUF2SG	DUF	AUS	failure type unplausible: Function monitoring: Data from other ECU
B.NPUFMV	DUF	AUS	fault type not plaus.: monitoring of the function: torque comparison
B.NPUF2SG	DUF	AUS	fault type not plaus.: monitoring of the function: safety fuel cut-off
B.PWGNOTFR	GGPED	EIN	FR error reaction pedal-travel sensor limphome
B.SGS	MDKOG	EIN	condition: torque intervention for engine speed synchr. during gear shift
B.SP1S	GGPED	EIN	message to SR: SP1S is command variable
B.SP2S	GGPED	EIN	SP2S is valid set value for PWG failure driving
B.SPSMIN	GGPED	EIN	message to SR: '1' = pedal-travel sensor limphome with SPSMIN
B.JB.OK	ADVE	EIN	Battery voltage o.k.
B.WDK2SEL	GGDVE	EIN	Condition: DV-E position control is performed with actual-value-poti 2
DUF.C	DUF	AUS	Time counter for setting cycle flags of the function surveillance diag. routine
EGASPFAD	DUF	AUS	ETS-path as environmental condition for diagnosis of function monitoring
EI.ADCC.UJM	URADCC	EIN	Irreversible error bit for the AD converter surveillance
EI.JPA.UJM	UFRLC	EIN	Irrevers. error bit for lower DK limit in invalid range of function monitoring
EI.MVER.UJM	UFMVER	EIN	Irreversible error bit for torque comparison from function monitoring
EI.NC.UJM	UFNC	EIN	irreversible error bit for engine speed comparison from function monitoring
EI.REAC.UJM	UFREAC	EIN	irreversible error bit of fault reaction monitoring from function monitoring
EI.RLC.UJM	UFRLC	EIN	Irrevers. error bit for comparison of rl with the function in function monitor.
EI.RLIP.UJM	UFRLC	EIN	Irreversible error bit for rl/rlip comparison in function monitoring
EI.SPSC.UJM	UFSPSC	EIN	irrevers. error bit for pedal value plausibility check in function monitoring
EI.UBR.UJM		EIN	Irreversible error bit for fault entry main relay
EI.ZWC.UJM	UFZWC	EIN	irrevers. error bit for ignition angle monitoring from function monitoring
E.UF2SG	DUF	AUS	Error flag:function monitoring: Data from other ECU
E.UFMV	DUF	AUS	Error flag: monitoring of the function: torque comparison
E.UF2SG	DUF	AUS	Error flag: monitoring of the function: safety fuel cut-off
MER.C1.UJM		EIN	fault counter 1 for message counter in function monitoring
MER.C2.UJM		EIN	fault counter 2 for message counter in function monitoring
MI.DUF	DUF	AUS	actual torque at response of torque comparison in the function monitoring
MI.UJM	UFMIST	EIN	Calculated actual torque in function monitoring
MPFAD	DUF	AUS	Torque path in function and function monitoring as environmental cond. of diag.
NMOT.UJM	UFNC	EIN	engine speed in function monitoring
NOME.C	DUF	AUS	fault counter for UF2SG
SFPUFMV	DUF	AUS	status word: monitoring of the function: torque comparison
SFPUF2SG	DUF	AUS	status word: monitoring of the function: safety fuel cut-off
SKAPFAD	DUF	AUS	freeze frame information for SKA
Z.UF2SG	DUF	AUS	cycle flag: function monitoring: Data from other ECU
Z.UFMV	DUF	AUS	cycle flag: monitoring of the function: torque comparison
Z.UF2SG	DUF	AUS	cycle flag: monitoring of the function: safety fuel cut-off

### FW DUF 6.30 Fixed Values

Parameter	Value	Description
CDKUF2SG		Code word customer: monitoring of the function: data from other ECU
CDKUFMV		Code word customer: monitoring of the function: torque comparison
CDKUF2SG		Code word customer: monitoring of the function: safety fuel cut-off
CDTUF2SG		Code word tester: monitoring of the function: data from other ECU
CDTUFMV		Code word tester: monitoring of the function: torque comparison
CDTUF2SG		Code word tester: monitoring of the function: safety fuel cut-off
CLAUF2SG		Fault class: monitoring of the function: data from other ECU
CLAUFMV		Fault class: monitoring of the function: torque comparison



Parameter	Value	Description
CLAUFska		Fault class: monitoring of the function: safety fuel cut-off
DUF.T		time for setting the cycle flags of function monitoring diagnosis
NMN.DUF		engine speed threshold for setting the cycle flag of the function monitoring dia
NOME.T		Time for fault detection UF2SG
TSFUF2SG		Fault active time: monitoring of the function: data from other ECU
TSFUFMV		Fault active time: monitoring of the function: torque comparison
TSFUFska		Fault active time: monitoring of the function: safety fuel cut-off

## FB DUF 6.30 Detailed description of function

Diagnosis from functional surveillance  
-----

As a minimum, the diagnostic function shall be processed in the 100-ms time frame.

It is not active during afterrunning.

In this function, three different fault pathes are served:

- Faults by the torque monitoring, that can also be due to a fault by the load monitoring
- Faults by the monitoring with the fault reaction safty-fuel-cut-off, which only can result by an intern fault of the ECU (UFSKA).
- Faults caused by a bad communication between two ECU's (UF2SG).

The distinction is made between faults from the torque comparison that can also be due to faults in load signals, and other faults from the surveillance with the fault response SKA that can only arise from internal fault responses in the computer.

Both fault entries from functional surveillance are mutually excluding, i.e. if the fault response SKA comes from the one of the fault cases defined in skapfad, then the torque comparison can no longer respond, and if the fault response comes first from the torque comparison, then there is no longer a fault E.ufska stored from the complex skapfad.

Apart from that, there will be no fault E.ufska from the Path skapfad, if there is a main relay (SY\_UBR = true ) and the fault ei\_ubr.um results in an fault mmemory entry by the function %GGUBR.

The time for setting the cycle flags in the error-free case will always run then when a defined engine-speed threshold has been exceeded.

The following environment conditions are provided at this function specification, because the Bit-Information had to be united.

The RAM cell skapfad is only filled in the case of a fault, i.e with a positive flank to E.ufska.

The RAM cell egaspfad is no longer filled as soon as a fault, i.e. E.ufska, has been detected.

The RAM cell mpfad is no longer filled as soon as a fault, i.e. E.ufmv, has been detected.

The following environment condition are provided at this function specification, because the information is changed by the fault reaction bi\_ska.um. The fault reaction closes the throttle, therefore the load and the torque decreases

The RAM cell mi\_duf is no longer filled as soon as a fault, i.e. E.ufmv, has been detected.

The following environment conditions are not provided in this function, they aere providet in the fault management system.

The RAM cell mer.cl.um

The RAM cell mer.c2.um

Fault-type information as well as the cycle and error flags are shown as outputs in the block diagrams. The output is not however by transfer of single bits, but rather by writing back the entire status word sfpxyz of the fault path XYZ into the centralized diagnostics management DFPM. The bits E\_xyz, Z\_xyz, B\_mxyz etc. are the contents of this status words. Access methods are available for those error and cycle flags from other fault paths, that occur as inputs. These methods read in the information directly from the fault path status managed by the DFPM.

The following variables are defined for each fault path XYZ of this diagnostic function:

Status Fault path XYZ:	sfpxyz
Fault flag xyz:	E_xyz
Cycle flag xyz:	Z_xyz
Fault type xyz:	TYP_xyz: (B_mxyz, B_mxyz, B_sixyz, B_npxyz)
Delete fault path:	B_clxyz
Standby value active:	B_bkxyz (optional)
Fault path code xyz:	CDTXYZ
Fault class xyz:	CLAXYZ
Fault severity xyz:	TSFXYZ
CARB Code xyz:	CDCXYZ
Table of environmental conditions xyz:	FFTXYZ

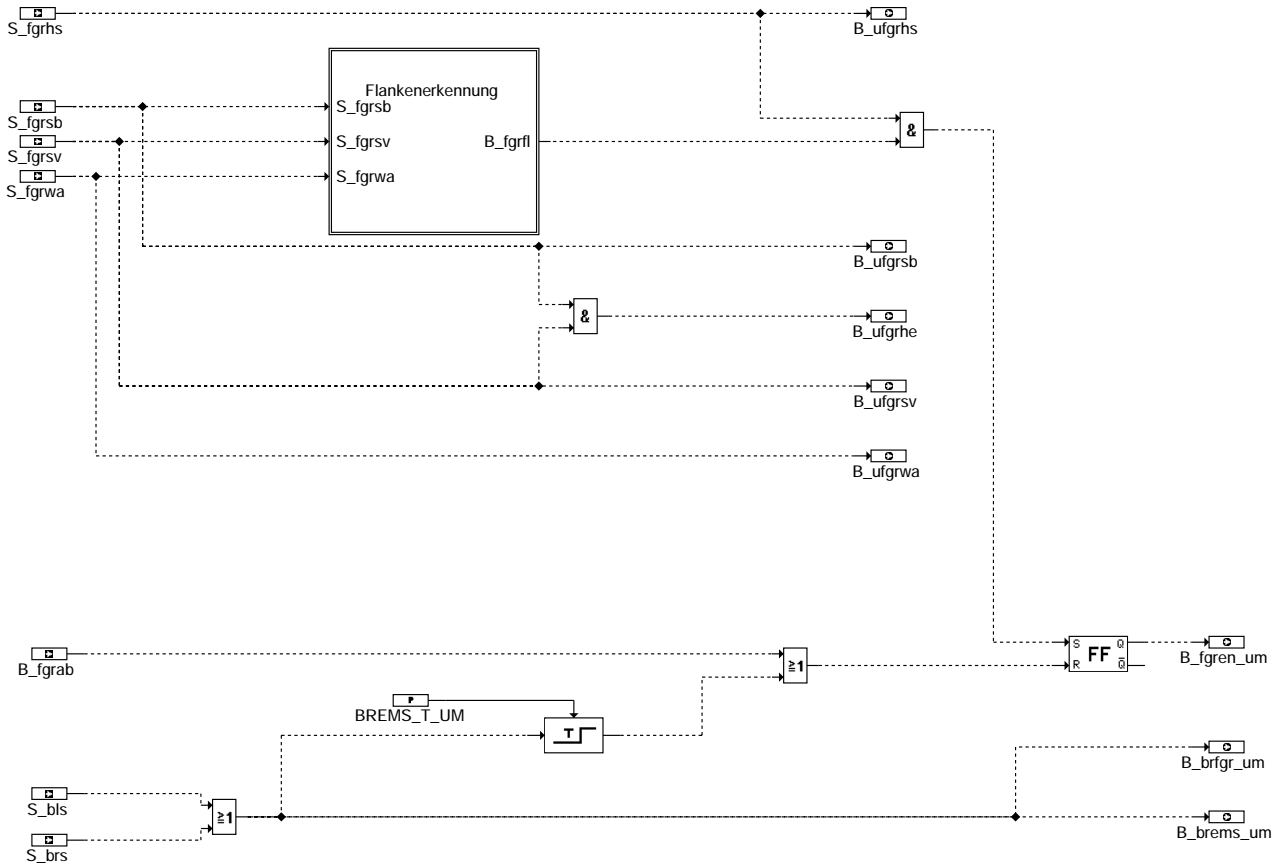
The following fault paths xyz are covered in this FDEF:

Fault path name	Abbreviation used (replaces "xyz")
Function monitoring: Torque comparison	UFMV
Function monitoring: SKA	UFSKA
Function monitoring: communication 2 ECU's	UF2SG

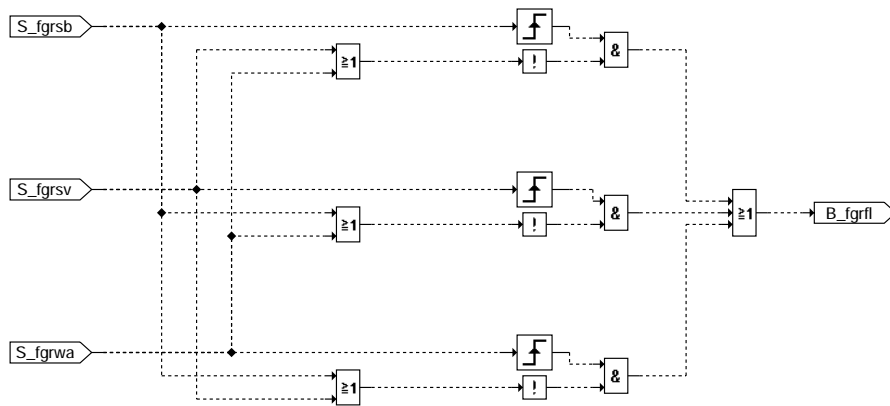
APP DUF 6.30 Application hint

## UFFGRE 17.10 ETS monitoring concept: CC input information used in function monitoring

### FDEF UFFGRE 17.10 Function definition



### uffgre-main



### uffgre-flankenerkennung

No text for FDEF available!

### ABK UFFGRE 17.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
BREMS.T_UM			FW	Debounce time for operated brake in function monitoring
Variable	Source		Type	Description
B_BREMS_UM	UFFGRE		AUS	condition of function monitoring: brake pedal pressed
B_BRFRGR_UM	UFFGRE		AUS	condition of function monitoring: brake pedal pressed





Variable	Source	Type	Description
B_FGRAB	FGRUE	EIN	CC/ACC shut-off from the function
B_FGRENJUM	UFFGRE	AUS	CC/ACC turn-on from control lever valid in function monitoring
B_UFGRHE	UFFGRE	AUS	voltage from cruise control level too high or faulty signal
B_UFGRHS	UFFGRE	AUS	information cruise control level "main switch ON"
B_UFGRSB	UFFGRE	AUS	information cruise control level "set / accelerate"
B_UFGRSV	UFFGRE	AUS	information cruise control level "set / coast"
B_UFGRWA	UFFGRE	AUS	information cruise control level "resume"
S_BLS		EIN	brake light switch (true=activated pedal)
S_BRS		EIN	Switch for brake
S_FGRHS		EIN	Main switch on FGR control lever
S_FGRSB		EIN	
S_FGRSV		EIN	Switch set/delay on FGR control lever
S_FGRWA		EIN	

### FW UFFGRE 17.10 Fixed Values

Parameter	Value	Description
BREMS.TJUM		Debounce time for operated brake in function monitoring

### FB UFFGRE 17.10 Detailed description of function

### APP UFFGRE 17.10 Application hint

## SCATT 20.70 SCAN TOOL-tester interface

### FDEF SCATT 20.70 Function definition

Allgemeine Hinweise:

Die Funktionskenntnis der Funktion %DFPM ist für die Arbeit mit dieser Funktion hilfreich!

#### Interface and Protocol

The protokoll driver verifies the transfer protocol and sets the Bit B.isoprot as follows:

B.isoprot = 0 communication according to ISO 9141-2  
B.isoprot = 1 communication according to ISO 14230-4

B.isoprot = 0 (communication according to ISO 9141-2):  
Only those PID's are responded to, which are reported as being supported by PID \$00.

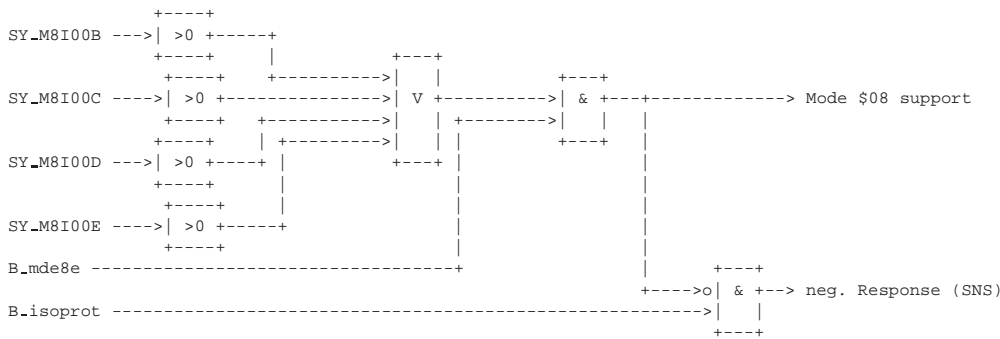
B.isoprot = 1 (communication according to ISO 14230-4):  
When a not supported mode is requested a message (negative response) is created:

No.	Mnemonic	Description
---	-----	-----
11h	SNS	requested mode is not supported (serviceNotSupported)

#### Message Structure

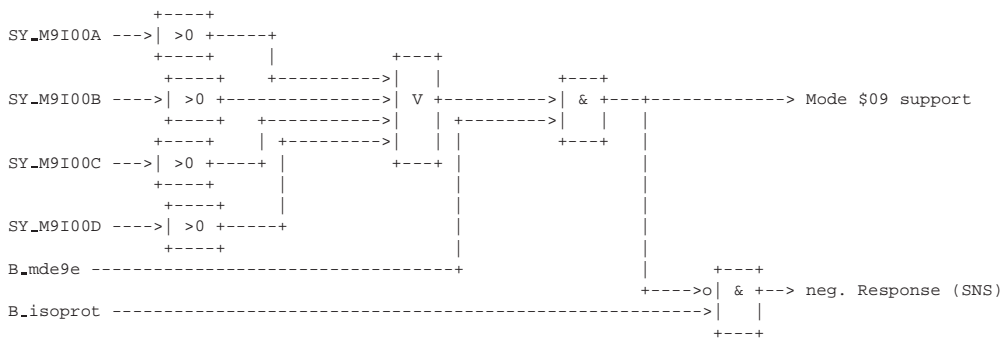
Mode \$01 - \$09 as well as the respective PID's are defined in SAE J1979.

Mode \$01: Request Current Powertrain Diagnostic Data	---> See %TC1MOD
Mode \$02: Request Current Powertrain Freeze Frame Data	---> See %TC2MOD
Mode \$03: Request Emission-Related Powertrain Diagnostic Trouble Codes (DTC)	---> See %SCATT
Mode \$04: Clear/Reset Emission-Related Diagnostic Information	---> See %SCATT
Mode \$05: Request Oxygen Sensor Monitoring Test Results	---> See %TC5MOD
Mode \$06: Request On-Board Monitoring Test Results for Non-Continuously Monitored Systems	---> See %TC6MOD
Mode \$07: Request On-Board Monitoring Test Results for Continuously Monitored Systems	---> See %SCATT
Mode \$08: Request Control of On-Board System, Test or Component	---> See %TC8MOD



In connection with Mode \$08 the following applies:  
The condition B\_m8te (see TC8MOD) is always set to false by the function %SCATT, when a another Mode is requested.  
When Mode \$08 is requested the condition B\_m8te is hence treated as described in %TC8MOD.

Mode \$09: Vehicle Information ---> See %TC9MOD



This description contains details regarding SAE J1979 Mode \$03, \$04 a. \$07.  
The realization of the SAE J1979 Modes \$01, \$02, \$05, \$06, \$08 and \$09 is described in the independent FDEF's %TC\*MOD (\* = 1, 2, 5, 6, 8 or 9).

### Mode \$03

Basis is SAE J1979 Mode \$03:  
Mode \$03 enables the access to the OBDII - relevant debounced fault codes stored in case of fault detection.  
Only OBDII - relevant faults and MIL-debounced faults with (fes.scatt = 1) & (fes.gauer = 1) are outputted.  
Furthermore it is possible to filter fault paths of the misfire monitoring via %TCSORT.

#### Output

The output is performed chronological, i.e. in the order of their entry.  
The output is performed in blocks of three fault codes, i.e. per response block always three words are transferred.  
In case of more than 3 fault codes, the ECU have to send multiple messages.  
If the amount of faults is not equal to 3 or not divisible by 3, the remaining bytes are outputted with \$00.  
Description of the fault code structure see -->%DFPM.  
With empty fault code memory 3 times 0000 is outputted.

### Mode \$04

Basis is SAE J1979 Mode \$04:  
By Mode \$04 the fault memory is cleared dependent on the system constant SY\_DELFCMS.

The selection of the clearing routine is performed prior to the compiler run via the system constant SY\_DELFCMS.  
SY\_DELFCMS = 0 (=Default): with Mode \$04 all fault-code memory entries are cleared  
SY\_DELFCMS = 1 : with Mode \$04 only the SCAN TOOL relevant fault-code memory entries (s. %DCLA) are cleared

With a tester request for MODE \$04 stored faults are cleared in dependency on SY\_DELFCMS.  
In addition to the clearing of the fault memory the following actions still need to be performed by the functions, which serve Modes \$01, \$05 a. \$06:  
- Reset basic data for Mode \$01 PID \$01 (reset readiness in DIMC)  
- Clear sensor measured values for Mode \$05 (%DLSSA)  
- Clear on-board monitoring test results (Mode \$06)



## Mode \$07

Basis is SAE J1979 Mode \$07:

Für den Mode \$07 gibt es 2 Varianten um behördenrelevante Fehlerpfade anzuzeigen.

Mit der Systemkonstante SY\_M7VAR ist die Anzeigevariante auswählbar:

SY\_M7VAR = 0: Es werden nur vorhandene und nicht entprellte Fehlerpfade (pending) angezeigt.

SY\_M7VAR = 1: Es wird immer das letzte Prüfergebnis angezeigt, auch für entprellte (Mode \$03) Fehlerpfade.

if SY\_M7VAR = 0

Mode \$07 indicates fault paths, which are OBDII - relevant & currently exist & not yet debounced & do not belong to the diagnostic function (fault paths) supported by Mode \$06.

PCM-entries with ((fes.scatt = 1) & (fes.dauer = 0) & (dfp not in Mode \$06)) are outputted to the Scan Tool.

endif

if SY\_M7VAR = 1

Mode \$07 indicates fault paths, which are OBDII - relevant & currently exist & do not belong to the diagnostic function (fault paths) supported by Mode \$06.

PCM-entries with ((fps.erfact = 1) & (fes.scatt = 1) & (dfp not in Mode \$06)) are outputted to the Scan Tool.

endif

In addition it is possible to filter fault paths of the misfire detection via %TCSORT.

Output see above Mode \$03.

## ABK SCATT 20.70 Abbreviations

ISO: International Organization for Standardization

SAE: Society of Automotive Engineers, Inc.

PID: Parameter Identification

TID: Test Identification

fes.scatt and fes.dauer: see %DFPM

>dfp not in Mode \$06<: Verweis auf Ausblendetabelle in %TC6MOD

Parameter	Source-X	Source-Y	Type	Description
CWSCTMDE			FW	Code word f. switch-off of certain Scan Tool Modes/Services (Bit=0 -> mode off)
Variable	Source		Type	Description
B_JSOPROT			EIN	tester protocol by ISO-standards ISO 14230-4
B_M8TE	TC8MOD		EIN	condition to enable function evap system by SAE J1879 Mode 8 TID \$01
B_MDE8E			EIN	Condition: mode \$08 permitted
B_MDE9E			EIN	Condition: mode \$09 permitted
SY_DELFCS	PROKON		EIN	system constant: selection of the reset routine for scan tool mode \$04
SY_M7VAR			EIN	System constant for Mode \$07 DTC - output
SY_M8I00B	PROKON		EIN	System constant coding from DATA B in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00C	PROKON		EIN	System constant coding from DATA C in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00D	PROKON		EIN	System constant coding from DATA D in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00E	PROKON		EIN	System constant coding from DATA E in mode 8 PID \$00 according to SAE J1979
SY_M9I00A			EIN	System constant coding from DATA A in Mode \$09 VIT \$00 acc. to SAE J1979
SY_M9I00B			EIN	System constant coding from DATA B in Mode \$09 VIT \$00 acc. to SAE J1979
SY_M9I00C			EIN	System constant coding from DATA C in Mode \$09 VIT \$00 acc. to SAE J1979
SY_M9I00D			EIN	System constant coding from DATA D in Mode \$09 VIT \$00 acc. to SAE J1979

## FW SCATT 20.70 Fixed Values

Parameter	Value	Description
CWSCTMDE		Code word f. switch-off of certain Scan Tool Modes/Services (Bit=0 -> mode off)

## FB SCATT 20.70 Detailed description of function

The operating of the interface is described by the above-mentioned standards:

ISO9141-2 resp. ISO 14230-4: Description of the hardware requirements, of the diagnostic initialization and of the timing

SAE J1979: Description of the protocol and of the contents, also refers to a few other SAE-standards, in which further information is given.

## APP SCATT 20.70 Application hint

Fehlerspeicher lesen (Mode \$03 und Mode \$07) und Fehlerspeicher löschen (Mode \$04) erfolgen nach den Vorschriften der SAE J1979.

Die Ausgabe der Fehlercodes in Mode \$07 wird mit der Systemkonstante SY\_M7VAR auf eine Variante eingestellt.

Diese Varianteneinstellung erfolgt vor der Erzeugung des Hexfiles und ist nicht applizierbar!

Mode \$08 und Mode \$09 über CWSCTMDE abschalten:

Das Codewort CWSCTMDE ist in der projektspezifischen KONCW oder PROKON definiert.

CWSCTMDE.Bit 0: B\_mde8e

CWSCTMDE.Bit 1: B\_mde9e



## TC1MOD 20.120 Tester communication CARB; Mode 1

### FDEF TC1MOD 20.120 Function definition

#### General:

Basis of this description is SAE J1979 Mode \$01:

Mode \$01 shall enable access to the momentary resp. most current exhaust gas relevant data.

In the process only the original measured values (so e.g. no default values) are permitted.

The protokoll driver verifies the transfer protocol and sets the Bit B.isoprot as follows:

B.isoprot = 0 communication according to ISO 9141-2  
B.isoprot = 1 communication according to ISO 14230-4

B.isoprot = 0 (communication according to ISO 9141-2):

Only those PID's are responded to, which are reported as being supported by PID \$00.

B.isoprot = 1 (communication according to ISO 14230-4):

When a not supported PID is requested the following message (negative response) is created:

No.	Mnemonic	Description
12h	SFNS-IF	subFunctionNotSupported-invalidFormat

PID \$00: Bit-coded transfer of the PID's supported by the ECU (PID \$00 must by all means be contained in Mode 1).

On a tester request (Mode \$01 PID \$00), the calculation begins and the result shows DATA Byte #5 (DATA C) as register.

if (SY\_MlI00C.Bit 6 = 1) & (B\_slsfz = 1) or (SY\_MlI00C.Bit 6 = 0):

SY\_MlI00C -----> register

else

SY\_MlI00C.Bit 0 -----> register.Bit 0  
SY\_MlI00C.Bit 1 -----> register.Bit 1  
SY\_MlI00C.Bit 2 -----> register.Bit 2  
SY\_MlI00C.Bit 3 -----> register.Bit 3  
SY\_MlI00C.Bit 4 -----> register.Bit 4  
SY\_MlI00C.Bit 5 -----> register.Bit 5

%SLS (PID \$12) supported (yes / no)

```

B_slsfz -----+
+++++          |
| 0 +-----+  v
+++++          +-----o --- o-----> register.Bit 6
SY_MlI00C.Bit 6 -----o
    
```

SY\_MlI00C.Bit 7 -----> register.Bit 7

endif



Der Registerinhalt für DATA Byte #6 (DATA D) ist auf Testeranfrage (Mode \$01 PID \$00) zu berechnen:

```

if (SY_MlI00D.Bit 0 = 0)
    SY_MlI00D -----> register_B
else
    SY_MlI00D.Bit 0 -----+
    SY_MlI20A.Bit 7 -----+---+
    B_kmmilsct ----->| & +---+
    +-----+          +---+ | +---+ | +---+
    | SY_MlI20A & 7F hex | +-----+ +---+ | +---+ | & +-----> register_B.Bit 0
    |(nur Bit 0 bis Bit 6)+--->| > 0 +----->| V +----->| |
    +-----+ +-----+ +-----+ | +-----+ | +-----+
    SY_MlI20B --->| > 0 +-----+ | +---+ | +---+
    +-----+
    SY_MlI20C ----->| > 0 +-----+
    +-----+
    SY_MlI20D ----->| > 0 +-----+
    +-----+

    SY_MlI00D.Bit 1 -----> register_B.Bit 1
    SY_MlI00D.Bit 2 -----> register_B.Bit 2
    SY_MlI00D.Bit 3 -----> register_B.Bit 3
    SY_MlI00D.Bit 4 -----> register_B.Bit 4
    SY_MlI00D.Bit 5 -----> register_B.Bit 5
    SY_MlI00D.Bit 6 -----> register_B.Bit 6
    SY_MlI00D.Bit 7 -----> register_B.Bit 7

endif
    
```

The following table shows the allocation Bit and PID:

	SY_MlI00A	SY_MlI00B	register	register_B
DATA:	A	B	C	D
DATA Byte #:	3	4	5	6
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
PID in hex:	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20

The PID's \$20; \$40; \$60; \$80; \$A0; \$C0 and \$E0 are dealt with analogous.  
DATA A - D (SY\_MlI00A - SY\_MlI00D): Is entered by the SW developer.

- 0 = PID n is not supported in Mode 1 (not supported)
- 1 = PID n is supported in Mode 1 (supported)

**PID \$01: Status Information**

DATA A: Number of emission-related powertrain Trouble codes and MIL status  
 Bit 0 to 6: Number of codes stored in this module  
 The fault code memory is searched for entered, debounced and CARB-relevant faults.  
 Stored misfire faults are filtered via the function %TCSORTx.y, thereafter the amount of faults is adjusted.  
 This amount is entered into DATA A bit 0 to 6 (this corresponds to 0 ... 127 dec).

Bit 7: MIL status with 1 = MIL on, 0 = MIL off):  
 The %DMIL calculates the MIL - status and sets the Bit B.milstat.  
 --> Output B.milstat

DATA B: Bit-coded identification of the supported continuously active diagnostic routines and of their state:  
 (0 = not supported, 1 = supported)  
 Bit 0 = Misfire detection (comes from B\_cdmd %PROKONx.y)  
 Bit 1 = Fuel system (comes from B\_cdkvs from %PROKONx.y)  
 Bit 2 = Comprehensive Component (set to 1, since always present)  
 Bit 3 to 7 set to 0, since not used resp. not necessary in this constellation.  
 --> Output AKKU - contents in case of request  
 (AKKU-contents is only given in the request buffer and therefore not readable by VS100)



DATA C: Bit-coded identification of the supported sporadically active diagnostic routines:

(0 = not supported, 1 = supported)

- Bit 0 = Catalyst monitoring
- Bit 1 = Heated catalyst monitoring
- Bit 2 = Evaporative system monitoring
- Bit 3 = Secondary air system monitoring
- Bit 4 = A/C system refrigerant monitoring
- Bit 5 = Oxygen sensor monitoring
- Bit 6 = Oxygen sensor heater monitoring
- Bit 7 = EGR system monitoring

--> output evsup1 (comes from DIMC)

DATA D: Bit-coded identification of the test status of the respective function.

(0 = not supported or test is performed, 1 = test not yet performed). Assignment just as with DATA C.

--> Output of the RAM-cell ready from --> %DIMCx.y

PID \$02: Is not supported in Mode 1.

PID \$03: Output Status Fuel Supply System Bank 1 + 2

DATA A: Bit-coded output of status of fuel-supply system bank 1

Only one of the following bits each may be set to 1:

- Bit 0 = Open loop - has not yet satisfied conditions to go closed loop
- Bit 1 = Closed loop - using oxygen sensor(s) as feedback for fuel control
- Bit 2 = Open loop due to driving conditions (fuel cut-off etc.)
- Bit 3 = Open loop due to detected system fault
- Bit 4 = Control active with limitations
- Bit 5 to 7 = not used (are set to 0)

--> Output flglrs, corresponds to the SAE-quantization

DATA B: Bit-coded output of status of fuel-supply system bank 2

Coding like on the 1-bank system (DATA A)

On a 1-bank system (SY\_STERVK = false) is set to \$00.

```

SY_STERVK -----+
                |
                v
00 hex -----o --- o-----> output
flglrs2 -----o
(flglrs2 corresponds to the SAE-quantization)
    
```

PID \$04 DATA A: Calculated load value in percent of the max. load.

SAE-quantization: (Quant = 100%/256)

--> Output rml, corresponds to the SAE-quantization

PID \$05 DATA A: Engine coolant temperature

SAE-quantization: ( \$00 = -40 deg. C, \$FF = 215 deg. C, quant = 1 deg. C)

--> convert tmotlin to the SAE-quantization and output

PID \$06 DATA A: Short term fuel trim - Bank 1

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128, 0% at 128)

Calculate output:

```

+-----+-----+
+--> | = xxxx xxxx 1xxx xxxx |-----+
| +-----+-----+ |
| (MSB) (LSB) v |
fr_w -----o-----o-----> | : 100 hex |-----> register
| +-----+ +-----o +-----+
+-----> | + 100 hex |---+
+-----+
    
```

--> output register; corresponds to the SAE-quantization

PID \$07 DATA A: Long term fuel trim - Bank 1

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128 )





PID \$11 DATA A: Absolute throttle position sensor  
SAE-quantization: ( \$00 = 0 %, \$FF = 100 %, quant = 100%/255 )  
--> output wdkba, corresponds to the SAE-quantization

PID \$12 DATA A: Commanded secondary air status  
Presently only this constellation is known. If secondary air system is given then injection of air upstream 1st catalyst of each bank.  
B\_slsfz = 0; no answer (ISO 9141-2) resp. SFNS-IF = \$12 (ISO 14230-4)  
(B\_slsfz = 1) & (B\_sls = 1) corresponds in the AKKU bit 0 = 1,  
(B\_slsfz = 1) & (B\_sls = 0) corresponds in the AKKU bit 2 = 1, remaining bits are to be set to 0.  
--> output AKKU - contents in case of request  
(AKKU-contents is only given in the request buffer and therefore not readable by VS100)

PID \$13 DATA A: Location of oxygen sensors installed in the vehicle, where sensor 1 is closest to the engine  
(Bit = 1: sensor mounted)  
PID \$13 is an alternative to PID \$1D.

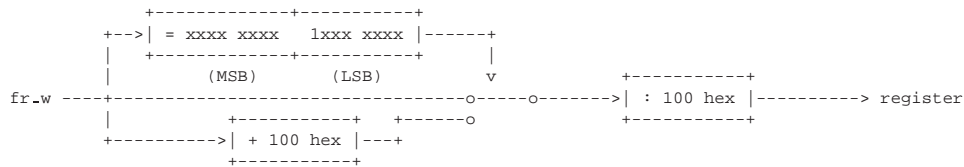
```
B_lsv --> Bit 0: Bank 1, sensor 1 (RB = upstream catalyst bank 1) mounted
B_lsh --> Bit 1: Bank 1, sensor 2 (RB = downstream catalyst bank 1) mounted
0 --> Bit 2: Bank 1, sensor 3 (not RB-typical)
0 --> Bit 3: Bank 1, sensor 4 (not RB-typical)
B_lsv2 --> Bit 4: Bank 2, sensor 1 (RB = upstream catalyst bank 2) mounted
B_lsh2 --> Bit 5: Bank 2, sensor 2 (RB = downstream catalyst bank 2) mounted
0 --> Bit 6: Bank 2, sensor 3 (not RB-typical)
0 --> Bit 7: Bank 2, sensor 4 (not RB-typical)
```

--> output AKKU, bit composition corresponds to the SAE-requirement.

The bits 2, 3, 6 a. 7 are set to "0" during the output, since this constellation is not RB-typical.

PID \$14 DATA A: Oxygen sensor output voltage of sensor upstream catalyst, bank 1 ( \$00 = 0 V, \$FF = 1,275 V, quant = 0,005 V)  
Is only supported on systems with 2-step Lambda control!  
--> usvkj (comes from DLSSAx.y and corresponds to the SAE-quantization)

DATA B: short term fuel trim of sensor upstr. cat, bank 1 ( \$00 = -100%, \$80 = 0%, %FF = +99,22%, quant = 100%/128, 0% at 128)  
Is only supported on systems with 2-step Lambda control!  
Calculate output:



--> output register; corresponds to the SAE-quantization

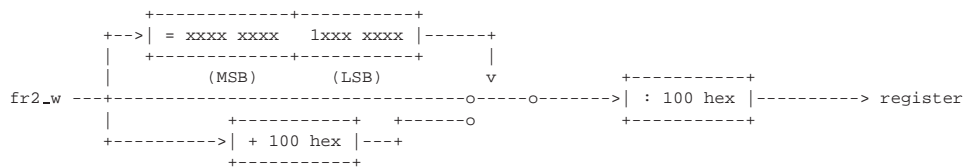
PID \$15 DATA A: Oxygen sensor output voltage of sensor downstream catalyst, bank 1 ( \$00 = 0 V, \$FF = 1,275 V, quant = 0,005 V)  
--> output ushkj (comes from DLSSAx.y), conversion corresponds to the SAE-quantization

DATA B: short term fuel trim of sensor downstr. cat, bank 1  
( \$00 = -100%, \$80 = 0%, %FF = +99,22%, quant = 100%/128, 0% at 128)  
--> output \$FF, since sensor is not used for the control.

PID \$16 + \$17: Sensor 3 + 4 of bank 1; not used here.

PID \$18 DATA A: Oxygen sensor output voltage of sensor upstream catalyst, bank 2 ( \$00 = 0 V, \$FF = 1,275 V, quant = 0,005 V)  
Is only supported on systems with 2-step Lambda control!  
--> usvkj2 (comes from DLSSAx.y and corresponds to the SAE-quantization)

DATA B: short term fuel trim of sensor upstr. cat, bank 2 ( \$00 = -100%, \$80 = 0%, %FF = +99,22%, quant = 100%/128, 0% at 128)  
Is only supported on systems with 2-step Lambda control!  
Calculate output:



--> output register; corresponds to the SAE-quantization





PID \$19 DATA A: Oxygen sensor output voltage of sensor downstream catalyst, bank 2 ( \$00 = 0 V, \$FF = 1,275 V, quant = 0,005 V )  
--> output ushkj2 (comes from DLSSAx.y), conversion corresponds to the SAE-quantization

DATA B: short term fuel trim of sensor downstr. cat, bank 2  
( \$00 = -100%, \$80 = 0%, %FF = +99,22%, quant = 100%/128, 0% at 128 )  
--> output \$FF, since sensor is not used for the control.

PID \$1A + \$1B: Sensor 3 + 4 of bank 2; not used here.

PID \$1C DATA A: OBD requirements

--> output CWOBD  
CWOBD in dec: Certification according to:  
01 OBDII-CARB  
02 OBD-EPA  
03 OBDII-CARB + OBD-EPA  
04 OBDI  
05 no OBD-requirements  
06 EOBD

Data are entered into CWOBD after an investigation of the project-specifically-used certification.

PID \$1D DATA A: Location of oxygen sensors (Bit = 1: Sensor mounted )  
(PID \$1D is only enabled if PID \$13 is not activated.)

B\_lsv --> Bit 0: Bank 1, sensor 1  
B\_lsh --> Bit 1: Bank 1, sensor 2  
B\_lsv2 --> Bit 2: Bank 2, sensor 1  
B\_lsh2 --> Bit 3: Bank 2, sensor 2  
0 --> Bit 4: Bank 3, sensor 1  
0 --> Bit 5: Bank 3, sensor 2  
0 --> Bit 6: Bank 4, sensor 1  
0 --> Bit 7: Bank 4, sensor 2

--> output AKKU - contents in case of request  
(AKKU-contents is only given in the request buffer and therefore not readable by VS100)

if (SY\_MlI00D.Bit 0 = 1)

PID \$20 Bit-coded transfer of the PID's >\$20 supported by the ECU  
PID \$20 must always be included in case of an activation of PID's >\$20.

Der Registerinhalt für DATA Byte #3 (DATA A) ist auf Testeranfrage (Mode \$01 PID \$20) zu berechnen:

if (SY\_MlI20A.Bit 7 = 0)

```
SY_MlI20A -----> register_2A

else
SY_MlI20A.Bit 0 -----> register_2A.Bit 0
SY_MlI20A.Bit 1 -----> register_2A.Bit 1
SY_MlI20A.Bit 2 -----> register_2A.Bit 2
SY_MlI20A.Bit 3 -----> register_2A.Bit 3
SY_MlI20A.Bit 4 -----> register_2A.Bit 4
SY_MlI20A.Bit 5 -----> register_2A.Bit 5
SY_MlI20A.Bit 6 -----> register_2A.Bit 6

SY_MlI20A.Bit 7 -----> | & -----> register_2A.Bit 7
B_kmmilsct -----> | |
+---+
```

endif

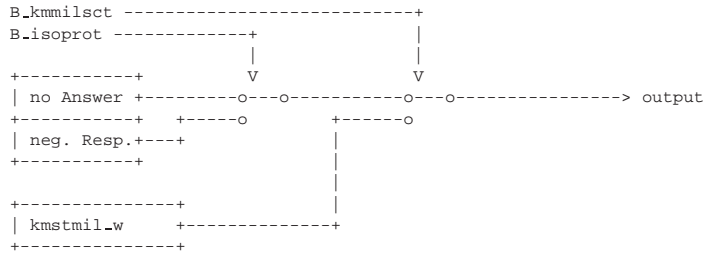
The following table shows the allocation Bit and PID:

	register_2A	SY_MlI20B	SY_MlI20C	SY_MlI20D
DATA:	A	B	C	D
DATA Byte #:	3	4	5	6
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
PID in hex:	21 22 23 24 25 26 27 28	29 2A 2B 2C 2D 2E 2F 30	31 32 33 34 35 36 37 38	39 3A 3B 3C 3D 3E 3F 40

The structure of PID \$20 is similar to PID \$00, however, for the PID's \$21 - \$40 and so on.  
For further details refer to PID \$00.



PID \$21 Trip with "MIL on"



DATA A: kmstmil\_w high-Byte  
DATA B: kmstmil\_w low-Byte  
SAE-quantization: ( Quant = 1km / incr, 0 ... 65535)

PID \$34 Equivalence ratio (Lambda) and oxygen sensor current Bank 1 - Sensor 1  
Is only supported on systems with wide range oxygen sensor (LSU)!

DATA A: Lambda high-Byte  
DATA B: Lambda low-Byte  
SAE-quantization: 1 Incr. = 0,0000305; Inkr; Range: 0 ... 1,999  
--> output lalsuvj\_w, corresponds to the SAE-quantization

DATA C: oxygen sensor current high-Byte  
DATA D: oxygen sensor current low-Byte  
SAE-quantization: 1 Inkr. = 0,0000305 ma; Range: -128 ma - 127,996 ma; \$8000 = 0 ma  
--> output iplsuvj\_w, corresponds to the SAE-quantization

PID \$38 Equivalence ratio (Lambda) and oxygen sensor current Bank 2 - Sensor 1  
Is only supported on systems with wide range oxygen sensor (LSU)!

DATA A: Lambda high-Byte  
DATA B: Lambda low-Byte  
SAE-quantization: 1 Incr. = 0,0000305; Inkr; Range: 0 ... 1,999  
--> output lalsuvj2\_w, corresponds to the SAE-quantization

DATA C: oxygen sensor current high-Byte  
DATA D: oxygen sensor current low-Byte  
SAE-quantization: 1 Incr. = 0,0000305 ma; Range: -128 ma - 127,996 ma; \$8000 = 0 ma  
--> output iplsuvj2\_w, corresponds to the SAE-quantization

endif

### ABK TC1MOD 20.120 Abbreviations

ISO: International Organization for Standardization  
SAE: Society of Automotive Engineers, Inc.  
PID: Parameter Identification

Parameter	Source-X	Source-Y	Type	Description
CWKMMILSCT			FW	Output:"Km at MIL on" for Scan Tool switch-off (0 = no output in PID \$21)
CWOBD			FW	code word for configuration OBD certification

Variable	Source	Type	Description
B_ISOPROT		EIN	tester protocol by ISO-standards ISO 14230-4
B_KMMILSCT		EIN	Output:"km at MIL on" for Scan Tool switch-off (0 = no output in PID \$21)""
B_MILSTAT	DMIL	EIN	MIL-Status for Scan-Tool Mode \$01 PID \$01
B_SLS	AK	EIN	Condition for active secondary air
B_SLSFZ	PROKON	EIN	condition: SLS fitted in vehicle
FLGLRS	LREB	EIN	CARB FREEZE FRAME byte, bank 1, for lambda control
FLGLRS2	LREB	EIN	CARB FREEZE FRAME byte, bank 2, for lambda control
FR2_W	LR	EIN	Lambda controller output (word)
FRA2_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FRA_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FR_W	LR	EIN	Lambda controller output (word)
IPLSUVJ2_W		EIN	sensor current IP LSU2
IPLSUVJ_W		EIN	sensor current IP LSU
KMSTMIL_W	BGKMST	EIN	Drive distance with MIL on
LALSUVJ2_W		EIN	Lambda actual value
LALSUVJ_W		EIN	Lambda actual value
MSHFM_W	GGHFM	EIN	air-mass flow HFM
NMOT_W	SWADAP	EIN	engine speed
PSDSS_U	DFFTCNV	EIN	Intake manifold pressure from pressure sensor (DS-S) with SAE quantisation
SY_M100A	PROKON	EIN	System constant coding from DATA A in Mode 1 PID \$00 acc. to SAE J1979
SY_M100B	PROKON	EIN	System constant coding from DATA B in Mode 1 PID \$00 acc. to SAE J1979
SY_M100C	PROKON	EIN	System constant coding from DATA C in Mode 1 PID \$00 acc. to SAE J1979



Variable	Source	Type	Description
SY_M1100D	PROKON	EIN	System constant coding from DATA D in Mode 1 PID \$00 acc. to SAE J1979
SY_M1120A		EIN	System constant coding from DATA A in Mode 1 PID \$20 acc. to SAE J1979
SY_M1120B		EIN	System constant coding from DATA B in Mode 1 PID \$20 acc. to SAE J1979
SY_M1120C		EIN	System constant coding from DATA C in Mode 1 PID \$20 acc. to SAE J1979
SY_M1120D		EIN	System constant coding from DATA D in Mode 1 PID \$20 acc. to SAE J1979
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
TANSLIN	GGTFA	EIN	intake air temperature, linearised and calculated
TMOTLIN	GGTFM	EIN	Engine coolant temperature, linearised and calculated
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
USVK	GGLSV	EIN	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyst 2
VFZG	SWADAP	EIN	vehicle speed (km/h)
WDKBA	GGDVE	EIN	throttle angle
ZWZYL1	ZUE	EIN	ignition angle cylinder 1

### FW TC1MOD 20.120 Fixed Values

Parameter	Value	Description
CWKMMILSCT		Output: "Km at MIL on" for Scan Tool switch-off (0 = no output in PID \$21)
CWOBD		code word for configuration OBD certification

### FB TC1MOD 20.120 Detailed description of function

#### APP TC1MOD 20.120 Application hint

The variable CWOBD must by all means be adjusted according to below-mentioned table in correspondence to the certification degree:

Certification according to	CWOBD in dec:
OBDII-CARB	01
OBD-EPA	02
OBDII-CARB + OBD-EPA	03
OBDI	04
no OBD-requirements	05
EOBD	06

PID \$21 über Codewort abschalten:  
CWKMMILSCT.Bit 0: B\_kmmilsc

## TC2MOD 20.70 Tester communication CARB; Mode 2

### FDEF TC2MOD 20.70 Function definition

Mode \$02

#### General:

Basis of this description is SAE J1979 Mode 2:  
Mode 2 shall enable access to freeze-frame data stored in case of fault detection.  
In the process only original measured values (so e.g. no default values) are permitted.

#### Communication Protocol:

The protocol driver detects the type of transfer protocol and describes the bit B\_isoprot:

B\_isoprot = 0 communication according to ISO 9141-2  
B\_isoprot = 1 communication according to ISO 14230-4

#### B\_isoprot = 0 (communication according to ISO 9141-2):

Only those PID's are responded to, which are reported as being supported by PID \$00.  
If no Freeze Frame is enabled (ffzdfp = 00), the inquiry for Mode \$02 freeze frame "00" is answered by those PID's, which are marked as being supported in the PID \$00.

#### B\_isoprot = 1 (communication according to ISO 14230-4):

When a not supported PID or freeze frame is requested, the following message (negative response) is created:

No.	Mnemonic	Description
---	-----	-----
12h	SFNS-IF	requested PID/TID is not supported (subFunctionNotSupported-invalidFormat)
22h	CNCORSE	no Freeze Frame #00 stored for Mode \$02 (conditionsNotCorrect or requestSequenceError)



**Freeze Frame:**

Description of freeze frame see --->%DFFT, %DTIP and %DFPM x.y.

Only once the fault was confirmed is the freeze frame with the number 00 stipulated by CARB formed and released for the output.

The content of the RAM-cell ffzdfp points to the dfp with the Freeze Frame 00.

The memory cell from the Freeze Frame table in the FCM for the Freeze Frame 00 is marked by the contraction frzx.ffzdfp (x stands for 0 to n; n is an internal FCM no.) in this description.

**PID \$00:** Bit-coded transfer of the PID's supported by the ECU (PID \$00 must by all means be contained in Mode 2).

**DATA Bytes #4 - #7**

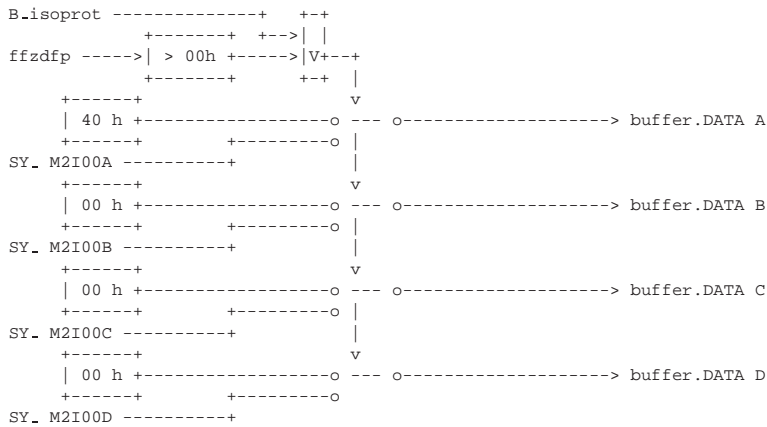
The software modules of the respective PID are included in the program dependent on the system constants SY\_M2I00A, SY\_M2I00B, SY\_M2I00C and SY\_M2I00D.

The support of the PID's > PID \$02 is only performed, if a freeze frame 0 is available, i.e. if ffzdfp > 00.

The PID's to be supported are determined and displayed at request by PID \$00.

**Determining of Support**

The buffer content for DATA byte #4 to #7 (DATA A to DATA D) is to be calculated at tester request (Mode \$02 PID \$00) in dependency on the content of the RAM - cell ffzdfp:



Support is performed dependent on the buffer contents for DATA A to DATA D.

**DATA A - D:**

	Buffer	Buffer	Buffer	Buffer
DATA:	A	B	C	D
DATA Byte #:	4	5	6	7
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
PID in hex:	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20

0 = PID n is not supported in Mode 2

1 = PID n is supported in Mode 2

**PID \$01:** not used in Mode 2

**PID \$02** Output of the fault code, which belongs to the freeze frame 00

With fault detection via the combustion miss detection the outputted fault paths are filtered with the function %TCSORT for the output to the tester.

A fault code consists of 2 bytes, which are transferred to Data A and Data B.

Data A is composed of the BCD-coded high-byte of the SAE-code incl. the letter P, e.g. P01xx.

Data B is composed of the BCD-coded low-byte of the SAE-code, e.g. Pxx37.

In case no freeze frame is stored, DATA A = 00 and DATA B = 00 is outputted.

PID \$03: Output Status Fuel Supply System Bank 1 + 2

DATA A: Bit-coded output of status of fuel-supply system bank 1

Only one of the following bits each may be set to 1:

Bit 0 = Controller readiness not yet reached  
 Bit 1 = Control active without limitation  
 Bit 2 = Open loop due to driving condition (fuel cut-off etc.)  
 Bit 3 = Open loop due to fault  
 Bit 4 = Control active with limitations  
 Bit 5 to 7 = not used (must be set to 0)

--> Output frz0.ffzdfp

DATA B: Bit-coded output of status of fuel-supply system bank 2

The codes are the same as with DATA A.

For 1-bank systems (SY\_STERVK = false), 00 hex needs to be sent.

```

SY_STERVK -----+
                |
                v
00 hex -----o --- o-----> output
frz1.ffzdfp -----o
  
```

PID \$04 DATA A: Calculated load in percent of the max. load.

--> Output frz2.ffzdfp

The content of frz2.ffzdfp corresponds to the SAE-quantization.

PID \$05 DATA A: Engine temperature

The content of frz3.ffzdfp corresponds to the SAE-quantization.

PID \$06 DATA A: Controller value of the Lambda control bank 1

--> Output frz4.ffzdfp

In frz4.ffzdfp the value of the high-byte of fr\_w is given. The content corresponds to the SAE-quantization

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128, 0% for 128)

PID \$07 DATA A: Adaptation value of the Lambda control bank 1

--> Output frz5.ffzdfp

In frz5.ffzdfp the value of the high-byte of fra\_w is given. The content corresponds to the SAE-quantization

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128, 0% for 128)

PID \$08 DATA A: Controller value of the Lambda control bank 2

--> Output frz6.ffzdfp

In frz6.ffzdfp the value of the high-byte of fr2\_w is given. The content corresponds to the SAE-quantization

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128, 0% for 128)

PID \$09 DATA A: Adaptation value of the Lambda control bank 2

--> Output frz7.ffzdfp

In frz7.ffzdfp the value of the high-byte of fra2\_w is given. The content corresponds to the SAE-quantization

SAE-quantization: ( \$00 = -100%, \$80 = 0%, \$FF = +99,22%, quant = 100%/128, 0% for 128)

PID \$0B DATA A: Manifold pressure (absolute)

--> Output frz8.ffzdfp

PID \$0C DATA A: Engine speed high-Byte

DATA B: Engine speed low-Byte

convert frz9.ffzdfp to SAE-quantization.

The RAM-cell frz9.ffzdfp contains the engine speed as 8-bit value with the quantization of 40 rpm per increment.

For the output this variable is to be converted to a 2-byte value with the SAE-quantization

SAE-quantization: (\$0000 ... \$FFFF = 0 ... 16383,75 rpm; 1 incr = 0,25 rpm)

Conversion: frz9.ffzdfp \* 160

--> output result.

PID \$0D DATA A: Vehicle speed

The content of frz10.ffzdfp corresponds to the SAE-quantization.



## ABK TC2MOD 20.70 Abbreviations

frz0\_ffzdfp ... frz10\_ffzdfp: Name of the cells, in which the freeze frame data for the freeze frame 00 are given  
ISO: International Organization for Standardization  
SAE: Society of Automotive Engineers, Inc.

Variable	Source	Type	Description
B_JSOPROT		EIN	tester protocol by ISO-standards ISO 14230-4
FFZDFP		EIN	fault path identification number (dfp) of freeze frame zero
FR2_W	LR	EIN	Lambda controller output (word)
FRA2_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FRA_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FR_W	LR	EIN	Lambda controller output (word)
SY_M2I00A	PROKON	EIN	System constant coding from DATA A in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00B	PROKON	EIN	System constant coding from DATA B in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00C	PROKON	EIN	System constant coding from DATA C in Mode 2 PID \$00 acc. to SAE J1979
SY_M2I00D	PROKON	EIN	System constant coding from DATA D in Mode 2 PID \$00 acc. to SAE J1979
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat

## FW TC2MOD 20.70 Fixed Values

Parameter	Value	Description
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## FB TC2MOD 20.70 Detailed description of function

### APP TC2MOD 20.70 Application hint

Attention: frz0\_ffzdfp ... frz10\_ffzdfp cannot be assigned a fixed address, since all faults are entered chronologically and since the assignment to the freeze frame 00 to any arbitrary fault memory line is performed dependent on the priority control.

## TC5MOD 20.30 Tester communication CARB; Mode 5

### FDEF TC5MOD 20.30 Function definition

Mode 5

Basis is SAE J1979 Mode \$05:  
Mode \$05 shall enable the output of Lambda sensor values.

### Interface and Protocol

The protokoll driver verifies the transfer protocol and sets the Bit B\_isoprot as follows:

B\_isoprot = 0 communication according to ISO 9141-2  
B\_isoprot = 1 communication according to ISO 14230-4

B\_isoprot = 0 (communication according to ISO 9141-2):  
Only those TID's are responded to, which are reported as being supported by TID \$00.

B\_isoprot = 1 (communication according to ISO 14230-4):  
When a not supported TID or an incorrect sensor number is requested a message (negative response) is generated:

No.	Mnemonic	Description
---	-----	-----
12h	SFNS-IF	requested TID is not supported (subFunctionNotSupported-invalidFormat)
22h	CNCORSE	incorrect sensor-no. in Mode \$05 (conditionsNotCorrect or requestSequenceError)



TID \$00: Bit-coded transfer of the TIDs supported by the ECU.  
Must by all means be contained in Mode \$05.

**Lambda sensor upstream catalyst:**

The system constants SY\_M5IV00A, SY\_M5IV00B SY\_M5IV00C a. SY\_M5IV00D apply to TID \$00.  
For the TID \$20, \$40 to \$80 the system constants SY\_M5V20A - D, resp. SY\_M5V40A - D and so on apply.

**Lambda sensor downstream catalyst:**

The system constants SY\_M5IH00A, SY\_M5IH00B SY\_M5IH00C a. SY\_M5IH00D apply to TID \$00.  
For the TID \$20, \$40 to \$80 the system constants SY\_M5H20A - D, resp. SY\_M5H40A - D and so on apply.

O2S upst. cat	SY_M5IV00A	SY_M5IV00B	SY_M5IV00C	SY_M5IV00D
O2S d.-st cat	SY_M5IH00A	SY_M5IH00B	SY_M5IH00C	SY_M5IH00D
DATA Byte #:	4	5	6	7
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
TID in hex:	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20

0 = TID n is not supported in Mode \$05 (not supported)  
1 = TID n is supported in Mode \$05 (supported)  
The TID's \$20; \$40; \$60; \$80; \$A0; \$C0 and \$E0 are dealt with analogous.  
The structure of TID \$20 is similar to TID \$00, however, only for the TID's \$21 - \$40 and so on..

Only values of those Lambda sensors are supported, which were reported in Mode \$01 at PID \$13 or PID \$1D.  
If neither PID \$13 nor PID \$1D is active in Mode \$01, then Mode \$05 is not supported.

TID \$01 and following according to TID \$00:

The transfer values are made available by the function "Signal Output Lambda Sensors" (%DLSSA).

**ABK TC5MOD 20.30 Abbreviations**

ISO: International Organization for Standardization  
SAE: Society of Automotive Engineers, Inc.

Variable	Source	Type	Description
BJSOPROT		EIN	tester protocol by ISO-standards ISO 14230-4
SY_M5IH00A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH00D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$00 acc. to SAE J1979 for sen. downst. cat.
SY_M5IH20A	PROKON	EIN	Sys. con. cod. DATA A in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20B	PROKON	EIN	Sys. con. cod. DATA B in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20C	PROKON	EIN	Sys. con. cod. DATA C in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IH20D	PROKON	EIN	Sys. con. cod. DATA D in mode 5 PID \$20 acc. to SAE J1979 sen. downstream cat.
SY_M5IV00A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV00D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$00 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV20D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$20 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV40D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$40 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV60D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$60 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80A	PROKON	EIN	Sys. const. cod. DATA A Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80B	PROKON	EIN	Sys. const. cod. DATA B Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80C	PROKON	EIN	Sys. const. cod. DATA C Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.
SY_M5IV80D	PROKON	EIN	Sys. const. cod. DATA D Mode 5 PID \$80 acc. to SAE J1979 for sen. upstr. cat.

**FW TC5MOD 20.30 Fixed Values**

Parameter	Value	Description
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**FB TC5MOD 20.30 Detailed description of function****APP TC5MOD 20.30 Application hint****TC6MOD 20.80 Tester communication CARB; Mode 6****FDEF TC6MOD 20.80 Function definition**

Mode \$06

Basis of this description is SAE J1979 Mode \$06:

Mode \$06 enables access to the most current test results and test thresholds of already tested functions.

The functions were named by the authority. The misfire detection, the diagnosis of the fuel supply system (DKVS) and of comprehensive components are not taken into consideration.

## Communication Protocol:

The protocol driver detects the type of transfer protocol and describes the bit B.isoprot:

B.isoprot = 0 communication according to ISO 9141-2  
B.isoprot = 1 communication according to ISO 14230-4

B.isoprot = 0 (communication according to ISO 9141-2):

Only those TID's are responded to, which are reported as being supported by TID \$00.

B.isoprot = 1 (communication according to ISO 14230-4):

When a not supported TID is requested a message (negative response) is created:

No.	Mnemonic	Description
---	-----	-----
12h	SFNS-IF	requested TID is not supported (subFunctionNotSupported-invalidFormat)

## Fault path table for the deactivation in Mode \$07

The following configuration table shows, which functions are served by Mode \$06, fault codes of these functions are not outputted (masked) in Mode \$07.





Functions	Compiler - Conditions	Masked Fault Paths	Fault Code
DKAT(LRS)	(SY_STERHK = false) & (SY_BDE = false) & (SY_M6I00A.Bit 7 = 1)	dfpkat,	CDCKAT
	(SY_STERHK = true) & (SY_BDE = false) & (SY_M6I00A.Bit 7 = 1)	dfpkat, dfpkat2	CDCKAT, CDCKAT2
DKATTH	(SY_STERVK = false) & (SY_BDE = true) & (SY_M6I00A.Bit 7 = 1)	dfpvtk,	CDCVTK
	(SY_STERVK = true) & (SY_BDE = true) & (SY_M6I00A.Bit 7 = 1)	dfpvtk, dfpvtk2	CDCVTK, CDCVTK2
DKATNO	(SY_STERHK = false) & (SY_BDE = true) & (SY_M6I00A.Bit 7 = 1)	dfpkatno	CDCKATNO
	(SY_STERHK = true) & (SY_BDE = true) & (SY_M6I00A.Bit 7 = 1)	dfpkatno, dfpkatno2	CDCKATNO, CDCKATNO2
DLSAHK	(SY_STERHK = false) & (SY_M6I00A.Bit 6 = 1)	dfplash	CDCLASH
	(SY_STERHK = true) & (SY_M6I00A.Bit 6 = 1)	dfplash, dfplash2	CDCLASH, CDCLASH2
DLSA	(SY_STETLR = false) & (SY_STERHK = false) & (SY_M6I00A.Bit 6 = 1)	dfplatv	CDCLATV
	(SY_STETLR = false) & (SY_STERHK = true) & (SY_M6I00A.Bit 6 = 1)	dfplatv, dfplatv2	CDCLATV, CDCLATV2
	(SY_STETLR = false) & (SY_STERVK = false) & (SY_M6I00A.Bit 6 = 1)	dfplatp	CDCLATP
	(SY_STETLR = false) & (SY_STERVK = true) & (SY_M6I00A.Bit 6 = 1)	dfplatp, dfplatp2	CDCLATP, CDCLATP2
DLSLSR(S)	(SY_STERVK = false) & (SY_M6I00A.Bit 5 = 1)	dfpsls, dfpslv	CDCSLS, CDCSLV
	(SY_STERVK = true) & (SY_M6I00A.Bit 5 = 1)	dfpsls, dfpsls2, dfpslv, dfpslv2	CDCSLS, CDCSLS2, CDCSLV, CDCSLV2
DAGRFC(S)	(SY_M6I00A.Bit 4 = 1)	dfpagrf	CDCAGRF
DLDP	(SY_DLDP = 1) & (SY_M6I00A.Bit 3 = 1)	dfpldp, dfptesf, dfptesg,	CDCLDP, CDCTESF, CDCTESG
DTEV	(SY_DTES.Bit 1 = 1) & (SY_M6I00A.Bit 3 = 1)	dfptes	CDCTES

#### Availability of Data

The data to be transferred are made available by diagnostic functions. The function descriptions of these diagnostic functions are mentioned in the corresponding TID's.

As long as the names of the transfer variables and of the fault paths do not change, this description always refers to the current project-specific version of the diagnostic function.

#### Diagnostic Functions

The diagnostic functions must store the Mode \$06 - values from the last test in the permanent RAM!

In case of initial start, after power-fail or clearing of fault memory, 00 hex must be entered into CID and 0000 hex must be entered into value and threshold as starting value.



Data Transfer

When a TID supported by Mode \$06 is requested, response is made by 7 DATA bytes.

- DATA #1: 46 hex (= Mode \$06)
- DATA #2: Test ID (TID)
- DATA #3: FF hex with TID \$00 or Component ID
- DATA #4: MSB of the measured value
- DATA #5: LSB of the measured value
- DATA #6: MSB of the threshold value (Limit)
- DATA #7: LSB of the threshold value (Limit)

Component ID (CID):

CID: identifies the individual value blocks,

a) CID Bit 7 = 0: fault if value > threshold; example:   

```

##### fault range
----- threshold
xxxxxxxxxxx o.k. range
    
```

CID Bit 7 = 1: fault if value < threshold; example:   

```

xxxxxxxxxxx o.k. range
----- threshold
##### fault range
    
```

b) CID Bit 0 ..6: number of the value block (max 127 possible)

TID \$00: Bit-coded transfer of the TID's supported by the ECU.  
TID \$00 always needs to be included in mode \$06.

DATA Byte #3: --> \$FF

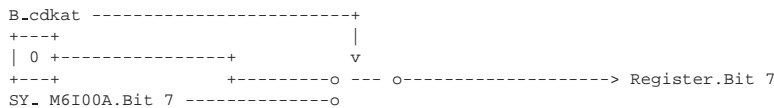
DATA Bytes #4 - #7

The SW-modules of the corresponding TID are included in the program dependent on the system constants SY\_M6I00A, SY\_M6I00B, SY\_M6I00C and SY\_M6I00D.

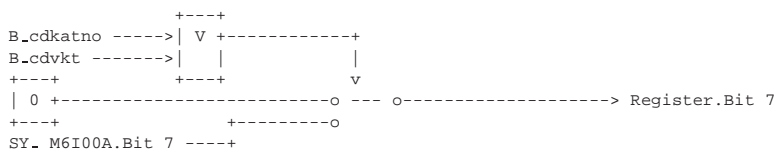
It is only possible to decide via an inquiry of the system constants and of the respective bit (B\_cd...) whether a TID is being supported, since many diagnostic functions have a deactivation possibility via the bit B\_cdxyz from CDXYZ.

The register contents for DATA byte #4 (DATA A) is to be calculated upon tester request (mode \$06 TID \$00) from SY\_M6I00A and B\_cd...:

if (SY\_M6I00A.Bit 7 = 1) & (SY\_BDE = false):  
support %DKAT(LRS)

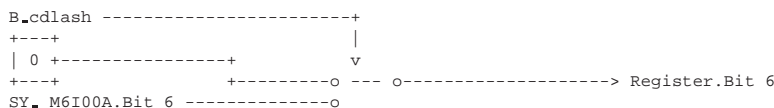


else if (SY\_M6I00A.Bit 7 = 1) & (SY\_BDE = true):  
support %DKATTH and/or %DKATNO



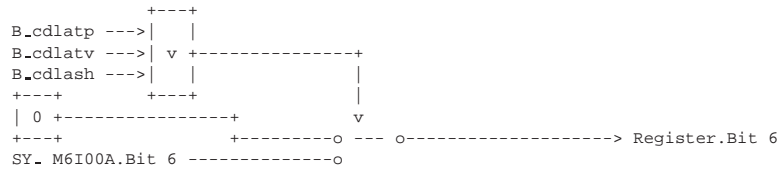
else Register.Bit 7 = 0

if (SY\_M6I00A.Bit 6 = 1) & (SY\_STETLR = true):  
support %DLSAHK in case of continuous LR



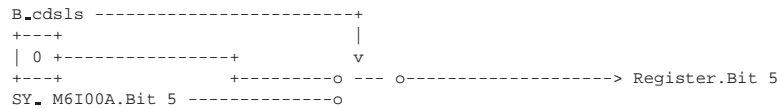


```
else if (SY_M6I00A.Bit 6 = 1) & (SY_STETLR = false):
    support %DLSAHK and/or DLSA in case of 2-step LR
```



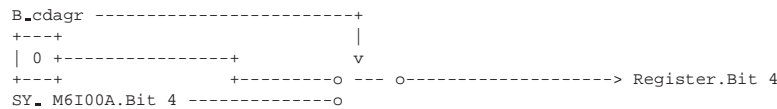
```
else Register.Bit 6 = 0
```

```
if (SY_M6I00A.Bit 5 = 1):
    support %DSLRLR(S)
```



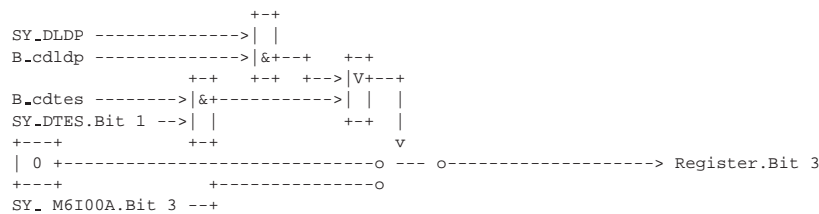
```
else Register.Bit 5 = 0
```

```
if (SY_M6I00A.Bit 4 = 1):
    support %DAGR*
```



```
else Register.Bit 4 = 0
```

```
if (SY_M6I00A.Bit 3 = 1):
    support %DTEV and %DLDP
```



```
else Register.Bit 3 = 0
```

By the following table it is possible to determine, which of the following TID's is being supported:

	Register	SY_M6I00B	SY_M6I00C	SY_M6I00D
DATA Byte #:	4	5	6	7
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
TID in hex:	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20

Each bit is assigned to a certain TID.  
If a bit has the value "0", the accompanying TID is not supported in mode \$06.  
In case of a bit value of "1", the accompanying TID is supported in mode \$06.

If SY\_M6I00A.Bit 7 = 1:

TID \$01: Catalyst conversion

The values tc6kat\* resp. m6\* are made available in the project-specific function(s) %DKAT(LRS) resp. %DKATNO and %DKATTH.

The data must have the following structure for the transfer:



Component ID DATA Byte #3	Measured Value *)		Threshold *)		
	Data Byte #4 MSB	Data Byte #5 LSB	Data Byte #6 MSB	Data Byte #7 LSB	

When (SY\_BDE = false) & (B\_cdkat = 1), the following value block is to be transferred:

tc6katc	00 hex	tc6katw	00 hex	tc6kats	%DKAT(LRS)
---------	--------	---------	--------	---------	------------

When (SY\_BDE = true) & (B\_cdvkt = 1), the following value block is to be transferred:

m6ckth	m6wkth_w	m6skth_w	%DKATTH
--------	----------	----------	---------

When (SY\_BDE = true) & (B\_cdkatno = 1), the following value block is to be transferred:

m6katnc	m6katnw_w	m6katns_w	%DKATNO
---------	-----------	-----------	---------

Only 2-bank systems need additionally:

When (SY\_BDE = false) & (SY\_STERHK = true) & (B\_cdkat = 1), the following value block is to be transferred additionally:

tc6katc2	00 hex	tc6katw2	00 hex	tc6kats2	%DKAT(LRS)
----------	--------	----------	--------	----------	------------

When (SY\_BDE = true) & (SY\_STERVK = true) & (B\_cdvkt = 1), the following value block is to be transferred additionally:

m6ckth2	m6wkth2_w	m6skth2_w	%DKATTH
---------	-----------	-----------	---------

When (SY\_BDE = true) & (SY\_STERHK = true) & (B\_cdkatno = 1), the following value block is to be transferred additionally:

m6katnc2	m6katnw2_w	m6katns2_w	%DKATNO
----------	------------	------------	---------

\*) Die values tc6tkatw and tc6kats are made available as 8-bit variables and the value m6\*\_w as 16-bit variables. The available 8 bit variables for value and threshold must be expanded to 16 bit variables. That means: 00hex must be entered into the MSB. The sequence MSB LSB (see table) must by all means be adhered to during the transfer to the tester!

Endif

If SY\_M6I00A.Bit 6 = 1:

TID \$02: Lambda sensor monitoring

The values for mode \$06 are made available in the project-specific functions %DLSA and %DLSAHK.

The data must have the following structure for the transfer:



Component ID DATA Byte #3	Measured Value *)		Threshold *)		
	Data Byte #4 MSB	Data Byte #5 LSB	Data Byte #6 MSB	Data Byte #7 LSB	

When (B\_cdlash = 1), the following 2 value blocks are to be transferred:

m6cshkf	00	m6wshkf	00	m6sshkf	%DLSAHK
m6cshkm	00	m6wshkm	00	m6sshkm	%DLSAHK

When (B\_cwlshdyn = 1), the following value block is to be transferred:

m6clsdy	00	m6wlsdy	00	m6slsdy	%DLSAHK
---------	----	---------	----	---------	---------

When (B\_cwlshsch = 1), the following value block is to be transferred additionally:

m6clsch	00	m6wlsch	00	m6slsch	%DLSAHK
---------	----	---------	----	---------	---------

When (SY\_STETLR = false) & (B\_cdlatp = 1), the following value block is to be transferred:

m6ctp	m6wtp_w		m6stp_w		%DLSA
-------	---------	--	---------	--	-------

When (SY\_STETLR = false) & (B\_cdlatv = 1), the following value block is to be transferred:

m6catv	00	m6watv	00	m6satv	%DLSA
--------	----	--------	----	--------	-------

For 2-bank systems the following value blocks in dependency on the accompanying enable bits are to be transferred additionally:

Component ID DATA Byte #3	Measured Value *)		Threshold *)		
	Data Byte #4 MSB	Data Byte #5 LSB	Data Byte #6 MSB	Data Byte #7 LSB	

When (SY\_STERHK = true) & (B\_cdlash = 1), the following 2 value blocks are to be transferred additionally:

m6cshkf2	00	m6wshkf2	00	m6sshkf2	%DLSAHK
m6cshkm2	00	m6wshkm2	00	m6sshkm2	%DLSAHK

When (SY\_STERHK = true) & (B\_cwlshdyn = 1), the following value block is to be transferred additionally:

m6clsdy2	00	m6wlsdy2	00	m6slsdy2	%DLSAHK
----------	----	----------	----	----------	---------

When (SY\_STERHK = true) & (B\_cwlshsch = 1), the following value block is to be transferred additionally:

m6clsch2	00	m6wlsch2	00	m6slsch2	%DLSAHK
----------	----	----------	----	----------	---------

When (SY\_STETLR = false) & (SY\_STERVK = true) & (B\_cdlatp = 1), the following value block is to be transferred additionally:

m6ctp2	m6wtp2_w		m6stp2_w		%DLSA
--------	----------	--	----------	--	-------

When (SY\_STETLR = false) & (SY\_STERHK = true) & (B\_cdlatv = 1), the following value block is to be transferred additionally:

m6catv2	00	m6watv2	00	m6satv2	%DLSA
---------	----	---------	----	---------	-------

\*) The variables m6w\*\_w and m6s\*\_w are made available as 16-bit variables.  
The available 8 bit variables for value and threshold must be expanded to 16 bit variables.  
That means: 00hex must be entered into the MSB.  
The sequence MSB LSB (see table) must by all means be adhered to during the transfer to the tester!

Endif

If SY\_M6I00A.Bit 5 = 1:

TID \$03 Secondary-air system

The values for m6\*msl\* are made available in the project-specific function %DSLRLR(S).

The data must have the following structure for the transfer:

Component ID	Measured Value *)		Threshold *)	
DATA Byte #3	Data Byte #4	Data Byte #5	Data Byte #6	Data Byte #7
	MSB	LSB	MSB	LSB
+-----+-----+-----+-----+-----+				

TID \$03 is only to be supported when (B\_cds1s = 1):

m6cms1	m6wms1_w	m6sms1_w
+-----+-----+-----+		

When (B\_cwds1t = 1), the following value block is to be transferred additionally:

m6cms1v	m6wms1v_w	m6sms1v_w
+-----+-----+-----+		

For 2-bank systems where (SY\_STERVK = true) the following applies additionally:

Component ID	Measured Value *)		Threshold *)	
DATA Byte #3	Data Byte #4	Data Byte #5	Data Byte #6	Data Byte #7
	MSB	LSB	MSB	LSB
+-----+-----+-----+-----+-----+				

When (SY\_STERVK = true) & (B\_cds1s = 1), the following value block is to be transferred additionally:

m6cms12	m6wms12_w	m6sms12_w
+-----+-----+-----+		

When (SY\_STERVK = true) & (B\_cwds1t = 1) the following value block is to be transferred additionally:

m6cms1v2	m6wms1v2_w	m6sms1v2_w
+-----+-----+-----+		

\*) The variables m6wms1\*\_w and m6sms1\*\_w are made available as 16-bit variables.

The sequence MSB LSB (see table) must by all means be adhered to during the transfer to the tester!

Endif

If SY\_M6I00A.Bit 4 = 1:

TID \$04 Exhaust-gas recirculation system

The values m6\*agr\* are made available by the project-specific function %DAGRFC(S).

The data must have the following structure for the transfer:

Component ID	Measured Value *)		Threshold *)	
DATA Byte #3	Data Byte #4	Data Byte #5	Data Byte #6	Data Byte #7
	MSB	LSB	MSB	LSB
+-----+-----+-----+-----+-----+				

TID \$04 is only to be supported when (B\_cdagr = 1):

m6cagr*	m6wagr*_w	m6sagr*_w
+-----+-----+-----+		

\*) The variables m6wagr\*\_w and m6sagr\*\_w are made available as 16-bit variables.

The sequence MSB LSB (see table) must by all means be adhered to during the transfer to the tester!

Endif

If SY\_M6I00A.Bit 3 = 1:

TID \$05 Purge control system

The values tc6ldp\* and tc6tes\* are made available by the project-specific functions %DLDP and %DTEV.

The data must have the following structure for the transfer:



Component ID	Measured Value *)		Threshold *)	
DATA Byte #3	Data Byte #4	Data Byte #5	Data Byte #6	Data Byte #7
	MSB	LSB	MSB	LSB

When (SY\_DTES.Bit 1 = 1) & (B.cdtes = 1), the following value block is to be transferred:

tc6tesc	tc6tesw	tc6tess	%DTEV
---------	---------	---------	-------

When (SY\_DLDP = 1) & (B.cdldp = 1), the following value block is to be transferred:

tc6ldpc	tc6ldpw	tc6ldps	%DLDP
---------	---------	---------	-------

\*) The variables tc6tes\* and tc6ldp\* are made available as 16-bit variables.  
The sequence MSB LSB (see table) must by all means be adhered to during the transfer to the tester!

Endif

### ABK TC6MOD 20.80 Abbreviations

ISO: International Organization for Standardization  
SAE: Society of Automotive Engineers, Inc.  
ID: Identification  
CID: Component ID  
TID: Test ID  
MSB: Most Significant Byte  
LSB: Least Significant Byte

dfpxyz: Diagnostic fault path of the function xyz

Parameter	Source-X	Source-Y	Type	Description
SY_BDE			SYS	system constant GDI
SY_DLDP			SYS	SY_DLDP = 1 there ist a DLDP in system
SY_DTES			SYS	system constant diagnosis evap system
Variable	Source		Type	Description
B_CDAGR	PROKON		EIN	function active per codeword CDAGR
B_CDKAT	PROKON		EIN	function active per codeword CDKAT
B_CDKATNO			EIN	function active via codeword CWDKATNO
B_CDLASH	PROKON		EIN	function active per codeword CDLASH
B_CDLATP	PROKON		EIN	function active per codeword CDLATP
B_CDLATV	PROKON		EIN	function active per codeword CDLATV
B_CDLDP	PROKON		EIN	function active per codeword CDLDP
B_CDSLS	PROKON		EIN	function active per codeword CDSLS
B_CDTES	PROKON		EIN	function active per codeword CDTES
B_CDVKT			EIN	function DKATTH active per euro switch
B_CWDSLTL			EIN	Condition: enable valve tightness
B_CWLSHDYN			EIN	cond. disabling of partial func. dynamics check of sensor downstream cat. %DLSAHK
B_CWLSHSCH			EIN	cond. disabling of partial func. fuel cut-off for sensor downstream cat. %DLSAHK
B_JSOPROT			EIN	tester protocol by ISO-standards ISO 14230-4
M6CATV	DLSA		EIN	Mode 6-Memory: Comp. ID for check Lambda sensor aging TV
M6CATV2	DLSA		EIN	Mode 6-Memory: Comp. ID for check Lambda sensor aging TV on bank 2
M6CKTH			EIN	Mode 6-Memory: Comp. ID for thermal catalyst monitoring
M6CKTH2			EIN	Mode 6-Memory: Comp. ID for thermal catalyst monitoring bank 2
M6CLSCH	DLSAHK		EIN	Mode 6-Memory: Comp. ID sensor voltage during fuel cut-off downstream cat.
M6CLSCH2	DLSAHK		EIN	Mode 6-Memory: Comp. ID sensor voltage during fuel cut-off downstream cat. bank2
M6CLSDY	DLSAHK		EIN	Mode 6-Memory: Comp. ID dynamic response measurement for sensor downstream cat
M6CLSDY2	DLSAHK		EIN	Mode 6-Memory: Comp. ID dyn. resp. measurement for sensor downstream cat. bank2
M6CMSL			EIN	Mode 6 - memory: Component ID for SAI- mass test
M6CMSL2			EIN	Mode 6 - memory: Component ID for SAI- mass test, bank 2
M6CMSLV			EIN	Mode 6 - memory: Component ID for SAI- tightness test
M6CMSLV2			EIN	Mode 6 - memory: Component ID for SAI- tightness test, bank 2
M6CSHKF	DLSAHK		EIN	Mode 6-Memory: Comp. ID rich volt. for sensor downstream cat.(osci. test)
M6CSHKF2	DLSAHK		EIN	Mode 6-Memory: Comp. ID rich volt. for sensor downstream cat.(osci. test) bank2
M6CSHKM	DLSAHK		EIN	Mode 6-Memory: Comp. ID lean volt. for sensor downstream cat.(osci. test)
M6CSHKM2	DLSAHK		EIN	Mode 6-Memory: Comp. ID lean volt. for sensor downstream cat.(osci. test) bank2
M6CTP	DLSA		EIN	Mode 6-Memory: Comp. ID for check Lambda sensor aging TP
M6CTP2	DLSA		EIN	Mode 6-Memory: Comp. ID for check Lambda sensor aging TP on bank 2
M6KATNC			EIN	output code SCAN-tool mode 6 from NOx cat. diagnosis
M6KATNS_W			EIN	output threshold SCAN-tool mode 6 from NOx cat. diagnosis
M6SATV	DLSA		EIN	Mode 6-Memory: Threshold value with Lambda sensor aging TV
M6SATV2	DLSA		EIN	Mode 6-Memory: Threshold value with Lambda sensor aging TV on bank 2
M6SKTH2_W			EIN	Mode 6 - memory: Threshold value for thermal catalyst monitoring bank 2
M6SKTH_W			EIN	Mode 6 - memory: Threshold value for thermal catalyst monitoring
M6SLSCH	DLSAHK		EIN	Mode 6-Memory: Threshold sensor voltage during fuel cut-off downstream cat.
M6SLSCH2	DLSAHK		EIN	Mode 6-Memory: Threshold sensor volt. during fuel cut-off downstream cat. bank2
M6SLSDY	DLSAHK		EIN	Mode 6-Memory: Threshold dynamic response measurement for sensor downstream cat.
M6SLSDY2	DLSAHK		EIN	Mode 6-Memory: Threshold dyn. resp. measurement for sensor downstream cat. bank2
M6SMSL2_W			EIN	Mode 6 - memory: Threshold value for test of auxiliary air mass, Bank 2
M6SMSLV2_W			EIN	Mode 6 - memory: Threshold value for valve tightness testing, Bank 2
M6SMSLV_W			EIN	Mode 6 - memory: Threshold value for valve tightness testing



Variable	Source	Type	Description
M6SMSL_W		EIN	Mode 6 - memory: Threshold value for test of auxiliary air mass
M6SSHKF	DLSAHK	EIN	Mode 6-Memory: Threshold rich volt. for sensor downstream cat.(osci. test)
M6SSHKF2	DLSAHK	EIN	Mode 6-Memory: Threshold rich volt. for sensor downstream cat.(osci. test) bank2
M6SSHKM	DLSAHK	EIN	Mode 6-Memory: Threshold lean volt. for sensor downstream cat.(osci. test)
M6SSHKM2	DLSAHK	EIN	Mode 6-Memory: Threshold lean volt. for sensor downstream cat.(osci. test) bank2
M6STP2_W	DLSA	EIN	Mode 6-Memory: Threshold value with Lambda sensor aging TP on bank 2
M6STP_W	DLSA	EIN	Mode 6-Memory: Threshold value with Lambda sensor aging TP
M6VKANW_W		EIN	verified mode6 result from NOx-catalyst monitoring for SCAN-Tool
M6WATV	DLSA	EIN	Mode 6-Memory: Measured value Lambda sensor aging TV
M6WATV2	DLSA	EIN	Mode 6-Memory: Measured value Lambda sensor aging TV on bank 2
M6WKTH2_W		EIN	Mode 6 - memory: Measured value of relative faults therm. catalyst monit. bank 2
M6WKTH_W		EIN	Mode 6 - memory: Measured value of relative faults thermal catalyst monitoring
M6WLSCH	DLSAHK	EIN	Mode 6-Memory: Measured value sensor voltage during fuel cut-off downstream cat.
M6WLSCH2	DLSAHK	EIN	Mode 6-Mem.: Measured value sensor volt. during fuel cut-off downst. cat. bank2
M6WLSDY	DLSAHK	EIN	Mode 6-Mem.: Measured value dyn. resp. measurement for sensor downst. cat.
M6WLSDY2	DLSAHK	EIN	Mode 6-Mem.: Measured value dyn. resp. measurement for sensor downst. cat. bank2
M6WMSL2_W		EIN	Mode 6 - memory: Measurement value of SAI- mass flow, bank 2
M6WMSLV2_W		EIN	Mode 6 - memory: Measurement value tightness, bank 2
M6WMSLV_W		EIN	Mode 6 - memory: Measurement value valve tightness
M6WMSL_W		EIN	Mode 6 - memory: Measurement value of SAI- mass flow
M6WSHKF	DLSAHK	EIN	Mode 6-Mem.: Measured value rich volt. for sensor downst. cat.(osci.test)
M6WSHKF2	DLSAHK	EIN	Mode 6-Mem.: Measured value rich volt. for sensor downst. cat.(osci.test) bank2
M6WSHKM	DLSAHK	EIN	Mode 6-Mem.: Measured value lean volt. for sensor downstr. cat.(osci.test)
M6WSHKM2	DLSAHK	EIN	Mode 6-Mem.: Measured value lean volt. for sensor downstr. cat.(osci.test) bank2
M6WTP2_W	DLSA	EIN	Mode 6-Mem.: Measured value Lambda sensor aging TP on bank 2
M6WTP_W	DLSA	EIN	Mode 6-Mem.: Measured value Lambda sensor aging TP
SY_M6I00A	PROKON	EIN	System constant coding from DATA A in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00B	PROKON	EIN	System constant coding from DATA B in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00C	PROKON	EIN	System constant coding from DATA C in Mode \$06 PID \$00 acc. to SAE J1979
SY_M6I00D	PROKON	EIN	System constant coding from DATA D in Mode \$06 PID \$00 acc. to SAE J1979
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
SY_STERVK	PROKON	EIN	system constant condition: stereo exhaust system upstream of cat
SY_STETLR	PROKON	EIN	System constant condition continuous Lambda control present
TC6KATC	DKAT	EIN	output code SCAN-tool mode 6 from catalyst diagnosis
TC6KATC2	DKAT	EIN	output code SCAN-tool mode 6 from catalyst diagnosis, bank 2
TC6KATS	DKAT	EIN	output threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATS2	DKAT	EIN	output threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATW	DKAT	EIN	output test threshold SCAN-tool mode 6 from catalyst diagnosis
TC6KATW2	DKAT	EIN	output test threshold SCAN-tool mode 6 from catalyst diagnosis, bank 2
TC6LDPC		EIN	Output of code SCAN-Tool Mode 6 from LDP-diagnosis
TC6LDPS		EIN	Output of threshold value SCAN-Tool Mode 6 from LDP-diagnosis
TC6LDPW		EIN	Output of test value SCAN-Tool Mode 6 from LDP-diagnosis
TC6TESC	DTEV	EIN	Output code SCAN tool mode 6 from purge control diagnosis
TC6TESS	DTEV	EIN	Output threshold SCAN tool mode 6 from purge control diagnosis
TC6TESW	DTEV	EIN	Output check value SCAN tool mode 6 from purge control diagnosis

### FW TC6MOD 20.80 Fixed Values

Parameter	Value	Description
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### FB TC6MOD 20.80 Detailed description of function

#### APP TC6MOD 20.80 Application hint

Application of the diagnostic thresholds is performed in the respective diagnostic functions.

## TC8MOD 20.20 Tester communication CARB; Mode 8

### DFEF TC8MOD 20.20 Function definition

Mode \$08

Basis of this section is SAE J1979 Mode 8 (as at June 95):

Mode 8 makes it possible to activate component and system tests.

Each request of various actions (e.g. close and open valves, test duration etc.) is performed out of the project-specific basic and diagnostic functions.

#### Communication

The protokoll driver verifies the transfer protocol and sets the Bit B\_isoprot as follows:

B\_isoprot = 0 communication according to ISO 9141-2  
B\_isoprot = 1 communication according to ISO 14230-4





B\_isoprot = 0 (communication according to ISO 9141-2):  
Only those TID's are responded to, which are reported as being supported by TID \$00.

B\_isoprot = 1 (communication according to ISO 14230-4):  
When a not supported TID is requested a message (negative response) is created:

No.	Mnemonic	Description
---	-----	-----
12h	SFNS-IF	requested TID is not supported (subFunctionNotSupported-invalidFormat)

#### Data Transfer

When a TID supported by Mode \$08 is requested, response is made by 7 DATA bytes.

DATA #1: 48 hex (= Mode \$08)

DATA #2: Test ID (TID)

DATA #3 to DATA #7: see respective TID

TID \$00: Bit-coded transfer of the TIDs supported by the ECU.  
TID \$00 must always be contained in Mode \$08.

The DATA - bytes #3 - #7 are also called DATA A - E.  
DATA A must be dated to \$00 hex

DATA B - E correspond to the system constants SY\_M8I00B - SY\_M8I00E.

Utilization of the system constants SY\_M8I00B, SY\_M8I00C, SY\_M8I00D a. SY\_M8I00E:

DATA:	SY_M8I00B	SY_M8I00C	SY_M8I00D	SY_M8I00E
	B	C	D	E
Bit:	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0	7 6 5 4 3 2 1 0
TID in hex:	01 02 03 04 05 06 07 08	09 0A 0B 0C 0D 0E 0F 10	11 12 13 14 15 16 17 18	19 1A 1B 1C 1D 1E 1F 20

0 = TID n is not supported in Mode 8

1 = TID n is supported in Mode 8

The TID's \$20; \$40; \$60; \$80; \$A0; \$C0 and \$E0 are dealt with analogous.

The structure of TID \$20 is similar to TID \$00, however, for the TID's \$21 - \$40 and so on.

TID \$01: Purge Control System; Leak Test

Bit B\_m8te is set when Mode 8 and TID \$01 are requested.

The bit B\_m8te must remain set until the triggered test function resets it again.

The Control Unit answers the tester with:

DATA #1 + DATA #2: as described in chapter data transfer,

DATA #3 - Data #7: 5 times 00 hex

### ABK TC8MOD 20.20 Abbreviations

ISO: International Organization for Standardization

SAE: Society of Automotive Engineers, Inc.

Variable	Source	Type	Description
B_ISOPROT		EIN	tester protocol by ISO-standards ISO 14230-4
B_M8TE	TC8MOD	AUS	condition to enable function evap system by SAE J1879 Mode 8 TID \$01
SY_M8I00B	PROKON	EIN	System constant coding from DATA B in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00C	PROKON	EIN	System constant coding from DATA C in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00D	PROKON	EIN	System constant coding from DATA D in Mode 8 PID \$00 acc. to SAE J1979
SY_M8I00E	PROKON	EIN	System constant coding from DATA E in mode 8 PID \$00 according to SAE J1979

### FW TC8MOD 20.20 Fixed Values

Parameter	Value	Description
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### FB TC8MOD 20.20 Detailed description of function

### APP TC8MOD 20.20 Application hint

## TC9MOD 10.10 Tester communication CARB; Mode 9, Request vehicle information

### FDEF TC9MOD 10.10 Function definition

No text for FDEF available!

### ABK TC9MOD 10.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
FA_CALID			TX	

Variable	Source	Type	Description
B_ISOPROT		EIN	tester protocol by ISO-standards ISO 14230-4
SY_M9I00A		EIN	System constant coding from DATA A in Mode \$09 VIT \$00 acc. to SAE J1979



Variable	Source	Type	Description
SY_M9I00B		EIN	System constant coding from DATA B in Mode \$09 VIT \$00 acc. to SAE J1979
SY_M9I00C		EIN	System constant coding from DATA C in Mode \$09 VIT \$00 acc. to SAE J1979
SY_M9I00D		EIN	System constant coding from DATA D in Mode \$09 VIT \$00 acc. to SAE J1979

### FW TC9MOD 10.10 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB TC9MOD 10.10 Detailed description of function

### APP TC9MOD 10.10 Application hint

## TCSORT 3.30 Tester communication CARB; sort function

### DFEF TCSORT 3.30 Function definition

Due to function-specific features the fault code memory (FCM) contains too much information for the user of a SCAN TOOL.

The method of misfire detection can be taken as example here:

Due to the detection strategy as a rule total faults (dfpmd) and single faults (dfpmd0x, x = event number (Zündereignisnummer ZEN)) are stored.

The ZEN shows the cylinder number via the firing order.

The CARB, however, explicitly prohibits the output of 'multiple misfire' to the SCAN-TOOL for misfire on only one cylinder.

The output of fault codes to the SCAN-TOOL can therefore not take place 1:1 from the fault memory in case of misfire detection.

Via the code word CWERFIL it is possible to chose 1 of 2 sorting versions. The result of the sorting can be seen in the following table (example for 3 cylinders).

CWERFIL = 0 dec; version A: Indicates only the multiple code for misfire on several cylinders and for 1 cylinder with misfire it indicates the code for this cylinder.

CWERFIL = 1 dec; version B: Indicates the multiple code for misfire on several cylinders and the code for the individual cylinders.

Generally the following applies to both versions for the fault output:

If only a single cylinder has misfire then only the code for this cylinder may be outputted to the SCAN TOOL with regard to misfire fault code.

Below a distinction between version A and B is made.

Version A (CWERFIL = 0):

As soon as misfires were detected on more than 1 cylinder and these were stored as fault paths in the FCM, a distinction must be made according to Mode 3 and Mode 7 dependent on the fault entry status fes.dauer.

Example: (dfpmd: (fes.dauer = 1)) & (dfpmd0a: (fes.dauer = 0)) & (dfpmd0b: (fes.dauer = 0))

That corresponds to case 3 in the table below: During the 1st driving cycle cylinder a has misfires and during the 2nd driving cycle cylinder b, without a fault healing detection being performed in the meantime.

=> Mode 3 and Mode 1 PID \$01 point to dfpmd. In Mode 7 no indication takes place.

Otherwise the following applies to version A:

If more than 1 misfire fault is given for the individual modes then only the SAE-code (CDCMD) for the multiple faultcode is to be outputted in the respective mode instead of the SAE-code (CDCMD01-n) for the single cylinders.

Version B (CWERFIL = 1):

In contrast to version A, version B outputs the multiple (CDCMD) code for misfires on several cylinders and the codes of the misfiring single cylinders (CDCMD00 - CDCMDnn).

Table: Example for 3 cylinders (cyl. a, cyl. b + cyl. c)

case	Misfire fault stored in the FCM				Version A CWERFIL = 0			Version B CWERFIL = 1	
	mult.	cyl. a	cyl. b	cyl. c	GST_M7	GST_M3	GST_M7	GST_M3	
1	dfpmd_u	dfpmd0a_u	---	---	30a	---	30a	---	
2	dfpmd_u	dfpmd0a_u	dfpmd0b_u	---	300	---	300, 30a, 30b	---	
3	dfpmd_e	dfpmd0a_u	dfpmd0b_u	---	---	300_f	30a, 30b	300_f	
4	dfpmd_e	dfpmd0a_e	dfpmd0b_u	---	---	300_f	30b	300_f, 30a	
5	dfpmd_e	dfpmd0a_e	---	---	---	30a_f	---	30a_f	
6	dfpmd_e	dfpmd0a_e	dfpmd0b_e	---	---	300_f	---	300_f, 30a, 30b	
7	dfpmd_u	---	---	---	300	---	300	---	
8	dfpmd_e	---	---	---	---	300_f	---	300_f	
9	dfpmd_e	dfpmd0a_u	dfpmd0b_u	dfpmd0c_e	---	300_f	30a, 30b	300_f, 30c	



#### Explanations:

GST\_M7 = Display Generic Scan Tool Mode 7  
GST\_M3 = Display Generic Scan Tool Mode 3  
dfpmd\_u = Misfire not debounced detected (pending)  
dfpmd\_e = Misfire debounced detected (MIL on)  
dfpmda/b/c = Misfire on cyl. a, b or c detected  
300 = Multiple code  
30a = Code for cylinder a  
30b = Code for cylinder b  
\*\*\*\_f = code to the freeze frame 00 (e.g. 30b\_f)

#### Effects on other functions

The result of this sorting function affects the following modes when outputted to the SCAN TOOL:

Mode 1	PID \$01 DATA A: Output of the number of faults	-->%TC1MODx.y
Mode 2	Output 'Freeze frame'	-->%TC2MODx.y
Mode 3	Output of the debounced faults	-->%SCATTx.y
Mode 7	Output of the not debounced faults	-->%SCATTx.y

#### ABK TCSORT 3.30 Abbreviations

fes.dauer = 1: Fault has resp. had switched on the MIL  
fes.scatt = 1: Fault entry is visible for SCAN TOOL only  
fes.dauer and fes.scatt are described in more detail in the DFPM x.y.

Parameter	Source-X	Source-Y	Type	Description
CWERFIL			FW	Codeword for selection of misfire fault codes for output to scan tool
Variable	Source		Type	Description
CW.ERFIL	PROKON		EIN	Status codeword for selection of misfire fault codes for output to scan tool

#### FW TCSORT 3.30 Fixed Values

Parameter	Value	Description
CWERFIL		Codeword for selection of misfire fault codes for output to scan tool

#### FB TCSORT 3.30 Detailed description of function

##### APP TCSORT 3.30 Application hint

Appl.- Tools: VS100 and Generic Scan tool

##### Version selection

Via the code word CWERFIL (see %PROKONx.y) it is possible to select a sorting version.

CWERFIL = 0 dec: Version A

CWERFIL = 1 dec: Version B

Which version is active can be seen by means of the RAM-cell cw\_erfil.

When data of CWERFIL are changed they are only accepted if B.ini = 1, that means a change of version is only possible if ignition on/off (INI).

##### Attention!

After a change from version A to B and vice versa, the fault code memory needs to be cleared and the misfire/s must be generated again.



## TCKOMUE 1.20 Tester communication CARB; Communication structure overview

### FDEF TCKOMUE 1.20 Function definition

Für die Kommunikation mit einem Generic Scan Tool sind mehrere Reizungsarten freigegeben. Die Steuergeräte von RB unterstützen die Kommunikation entsprechend den Normen ISO 9141-2 und ISO 14230-4.

ISO 9141-2: ist seit Einführung der OBDII - Bestimmungen bei RB - Steuergeräten im Einsatz,  
ISO 14230-4 per WUP (fast Ini.) bzw. per 5Baud (slow Ini.): Scan Tool Kommunikation über KWP2000

Ein Generic Scan Tool darf mit verschiedenen Reizungsarten versuchen, eine Kommunikation mit den im Fahrzeug verbauten Steuergeräten aufzubauen.

Die behördenrelevanten Steuergeräte müssen mindestens auf eine Reizungsart (Kommunikationsprotokoll) antworten.

Abhängig von der Systemkonstante SY\_INI\_OBD kann die jeweilige Reizungsart in die SG - Software implementiert werden.

SY_INI_OBD	unterstützte Reizungsarten (Protokolle)
0	ISO 14230-4 per WUP (fast Ini) und ISO 9141-2 per 5Baud
1	ISO 14230-4 per 5Baud
2	ISO 9141-2 per 5Baud
3	ISO 14230-4 per WUP (fast Ini.)
4	kein CARB-Protokoll

#### Wichtiger Hinweis:

Antwortet ein Steuergerät eine bestimmte Reizungsart, so müssen alle behördenrelevanten Steuergeräte in diesem Fahrzeug dieses Protokoll unterstützen!

### ABK TCKOMUE 1.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SY_INI_OBD			SYS	system constant to select the communication protocols for scan tool operation

### FW TCKOMUE 1.20 Fixed Values

Parameter	Value	Description
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### FB TCKOMUE 1.20 Detailed description of function

### APP TCKOMUE 1.20 Application hint

## CAN 89.80 CAN signal list

### FDEF CAN 89.80 Function definition

No text for FDEF available!

### ABK CAN 89.80 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
BOLATZ			FW	
CANINDLY			FW	
CBUSOFF			FW	
CMUTE			FW	
CWCAN			FW	
DMIGSL			FW	offset to SGS reduced torque demand for air path
DMIVW			FW	Wichtung Verlustmoment Offset Luftpfad
MDIMX			FW	maximum limit indicated engine torque
MSRMX			FW	
NGANGMIN			FW	minimum engine speed for gear detection
RAMDASR			FW	ramp steepness during advancement of ASR torque request
RAMPASR			FW	ramp steepness during advancement of ASR torque request
RAMPKUP			FW	ramp steepness during advancement of KUP torque request
TDCAN			FW	
TOCKUP			FW	Selespeed message. switch to default-values
UBDCAN			FW	battery voltage threshold for diagnosis of CAN-Timeout

Variable	Source	Type	Description
B_ANF_KUP		EIN	CAN-signal: bit shift phase (B_ANF_KUP) from el. clutch
B_ASC1NEW		EIN	condition CAN-ASC1 message current receive
B_ASRFZ	PROKON	EIN	Condition for ASR in the automobile
B_ASR_C		EIN	CAN-signal: condition for external ASR-request
B_AUTGET	PROKON	EIN	condition automatic gearbox



Variable	Source	Type	Description
B_BUSOFF		EIN	
B_CASRLVAL		EIN	CAN message from ASR is valid
B_CASRSVAL		EIN	CAN message from ASR is valid
B_CMSRVAL		EIN	CAN message from MSR is valid
B_CMUTE	CAN	AUS	
B_CVT	PROKON	EIN	Condition continuously variable transmission
B_DKNOLU	SWADAP	EIN	condition: power supply of throttle actuator cut off
B_DKPU	SWADAP	EIN	condition: safety fuel cut-off due to unknown or wrong throttle blade position
B_KL15		EIN	condition ignition switch on
B_KUP1NEW		EIN	condition CAN-KUP1-message received
B_MSR_C		EIN	CAN-signal: condition for external MSR-request
B_NOMSR_FR	CAN	AUS	No ASR-/MSR intervention from FR
B_NOMSR_JUM	UFUE	EIN	MSR moment required not used in function monitoring
B_NOSGS_FR	CAN	LOK	No SGS intervention from FR
B_NOSGS_JUM	UFSGSC	EIN	SGS moment required not transferred to function monitoring
B_NPBUOF	CAN	AUS	
B_SELESPED		EIN	condition: car with selespeed
B_SGSRH_C		EIN	condition: increased torque intervention f. eng. speed synchr. during gear shift
B_SGSKON_C		EIN	condition: constant torque intervention for eng. speed synchr. during gear shift
B_SGSRD_C	CAN	AUS	condition: reducing torque intervention for eng. speed synchr. during gear shift
B_SGSRD_C		EIN	condition: reducing torque intervention for eng. speed synchr. during gear shift
B_SIMUTE	CAN	AUS	
B_TDCAN	CAN	AUS	
B_TOCASR1	CAN	LOK	ASR1 message timeout - default values used
B_TOCKUP	CAN	LOK	Selespeed message timeout - default values used
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_NOSERE		EIN	
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BUOF	CAN	AUS	
E_BUSOFF	CAN	AUS	
E_CAS	DCAS	EIN	errorflag: CAN-interface, timeout ASC
E_CKUP		EIN	error flag: CAN-bus, timeout clutch
E_MUTE	CAN	AUS	
GANG_KUP	CAN	AUS	current gear received via CAN for F1 transmission
MDVERL_W	MDVER	EIN	Resistant torque of the engine
MIASRL_C		EIN	CAN-signal: request "slow ASR intervention"
MIASRL_W	CAN	AUS	desired indicated torque from ASR for slow intervention
MIASRS_C		EIN	CAN-signal: request "fast ASR intervention"
MIASRS_W	CAN	AUS	desired indicated torque from ASR for quick intervention
MIGSL_W	CAN	AUS	desired internal torque for charge limitation during GS.
MIGS_W	CAN	AUS	desired indicated torque form GS for quick intervention
MIMSR_C		EIN	CAN-signal: request "MSR intervention"
MIMSR_W	CAN	AUS	desired indicated torque from MSR
MISGSL_W	CAN	AUS	desired internal torque (air path) for engine speed synchr. during gear shift
MISGS_C		EIN	indicated torque request from SGS
MISGS_W	CAN	AUS	desired internal torque for engine speed synchronization during gear shift
NMOT_W	SWADAP	EIN	engine speed
STAT_MD_E	CAN	AUS	CAN signal: Status torque intervention
S_ASR	CAN	AUS	status ASR-active via CAN
S_MSR	CAN	AUS	input signal MSR
UB	SWADAP	EIN	battery voltage
ZWOUT	ZUE	EIN	Ignition angle output value
ZWSPA_E	ZWMIN	EIN	retarded ignition angle
Z_BUOF	CAN	AUS	
Z_MUTE	CAN	AUS	

### FW CAN 89.80 Fixed Values

Parameter	Value	Description
BOLATZ		
CANINDLY		
CBUSOFF		
CMUTE		
CWCAN		
DMIGSL		
DMIVW		
MDIMX		
MSRMX		
NGANGMIN		
RAMDASR		
RAMPASR		
RAMPKUP		
TDCAN		
TOCKUP		
UBDCAN		



## FB CAN 89.80 Detailed description of function

### APP CAN 89.80 Application hint

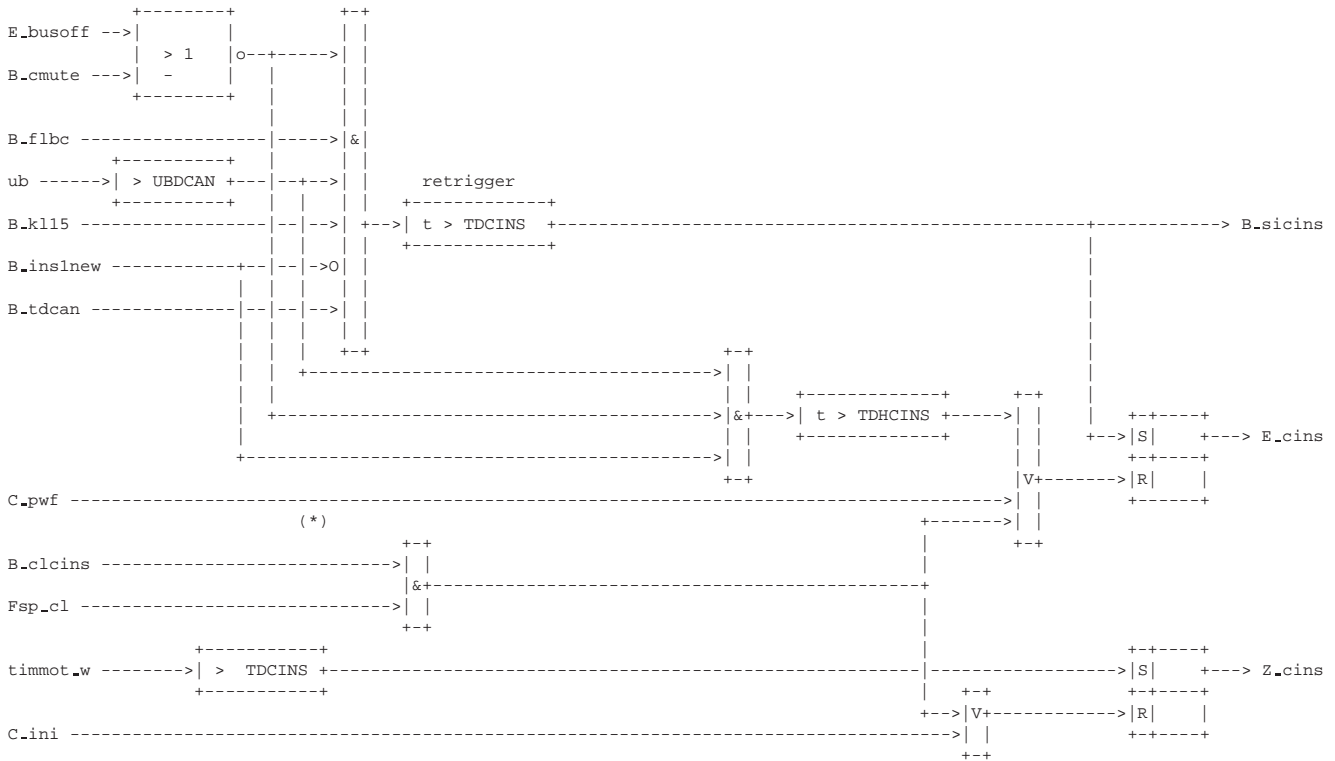
## DCINS 8.30 Diagnostics; CAN timeout instrument (Combi)

### FDEF DCINS 8.30 Function definition

Prüfkriterien: Keine CAN-Botschaft INSTR1: B\_inslnew = 0  
für t > TDCINS und Ub > UBDCAN und B\_kl15 = EIN und kein Busoff und kein Mute

Fehlerheilkriterien: Bedingungen sind nicht erfüllt

Ersatzgrößen: Sfst = 0 ;



(\*) abweichend zur Beschreibung wird dieser Pfad im Modul %DFPM bedient bzw. die Flags in %DFPM verwaltet;

#### Fehlerspeicherverwaltung:

Status Fehlerpfad :	SFPCINS	Löschen Fehlerpfad :	C_fmclr & B_clcins
Errorflag :	E_cins	Fehlerpfad :	CDTCINS
Zyklusflag :	Z_cins	Fehlerklasse :	CLACINS
Fehlerart :	B_sicins	Fehlerschwere :	TSFCINS
		Carb-Code :	CDCCINS
		Umweltbedingungen :	FFTCINS

### ABK DCINS 8.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCCINS	BLOKNR		KL	code word CARB: CAN interface, timeout instrument
CDTCINS			FW	code word tester: CAN-Timeout, Instruments
CLACINS			FW	fault class: CAN interface, timeout instruments
FFTCINS	BLOKNR		KL	Freeze frame table: CAN-Timeout, instrument panel
FLCCINS			FW	fault set debouncing: CAN interface, timeout instrument
HLCCINS			FW	fault reset debouncing: CAN interface, timeout instrument
TDCINS			FW	Time for timeout detection CAN interface combi-instrument
TDHCINS			FW	Time for fault rectification CAN timeout combined instrument
UBDCAN			FW	battery voltage threshold for diagnosis of CAN-Timeout

Variable	Source	Type	Description
B_CLCINS		EIN	condition clear fault path CINS
B_CMUTE	CAN	EIN	



Variable	Source	Type	Description
B_FLBC		EIN	condition: car with Florence Body Computer
B_JNS1NEW		EIN	Condition: CAN-message INSTR1 received
B_KL15		EIN	condition ignition switch on
B_SICINS	DCINS	AUS	signal error CAN interface instruments
B_TDCAN	CAN	EIN	
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for initialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BUSOFF	CAN	EIN	
E_CINS	DCINS	AUS	Error flag: CAN interface, timeout instrument
FSP_CL		EIN	clear fault memory
SFPCINS	DCINS	AUS	status fault path: timeout CAN interface instruments
TIMMOT_W		EIN	Timer:time after engine start n>NINI (word)
UB	SWADAP	EIN	battery voltage
Z_CINS	DCINS	AUS	Cycle flag: CAN interface, timeout instrument

### FW DCINS 8.30 Fixed Values

Parameter	Value	Description
CDTCINS		code word tester: CAN-Timeout, Instruments
CLACINS		fault class: CAN interface, timeout instruments
FLCCINS		fault set debouncing: CAN interface, timeout instrument
HLCCINS		fault reset debouncing: CAN interface, timeout instrument
TDCINS		Time for timeout detection CAN interface combi-instrument
TDHCINS		Time for fault rectification CAN timeout combined instrument
UBDCAN		battery voltage threshold for diagnosis of CAN-Timeout

### FB DCINS 8.30 Detailed description of function

Die Funktion überwacht die CAN-Botschaft INSTR1, (B\_ains1new) auf Timeout.

Sender der Botschaft ist das Kombiinstrument.

Die Timeoutüberwachung ist aktiv, wenn die Batteriespannung größer UBDCAN und Kl.15 ein und kein Busoff und kein Mute aktiv ist (In der Haltephase keine Überwachung). Die Abtastrate ist 10 ms. Auf Fehler E\_cins wird erkannt, wenn für  $t > TDCINS$  B\_ains1new = 0. Wird während der Überwachungszeit wieder eine Instr-Botschaft empfangen, wird der interne Überwachungszeitzähler zurückgesetzt. Fehlerheilung und Zurücksetzen des Fehlerflags E\_cins, wenn Instr-Botschaften für  $t > TDHCINS$  wieder empfangen wurden und kein Busoff und kein Mute aktiv ist.

Das Zyklusflag Z\_cins wird immer nach timmot\_w > TDCINS (Zeitähler ab Motorlauf) gesetzt.

Mit Befehl 'Löschen Fehlerspeicher' werden E\_cins und Z\_cins zurückgesetzt.

### APP DCINS 8.30 Application hint

### FDEF DCINS 8.30 Function definition

No text for FDEF available!

### ABK DCINS 8.30 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCCINS	BLOKNR		KL	code word CARB: CAN interface, timeout instrument
CDTCINS			FW	code word tester: CAN-Timeout, Instruments
CLACINS			FW	fault class: CAN interface, timeout instruments
FFTCINS	BLOKNR		KL	Freeze frame table: CAN-Timeout, instrument panel
FLCCINS			FW	fault set debouncing: CAN interface, timeout instrument
HLCCINS			FW	fault reset debouncing: CAN interface, timeout instrument
TDCINS			FW	Time for timeout detection CAN interface combi-instrument
TDHCINS			FW	Time for fault rectification CAN timeout combined instrument
UBDCAN			FW	battery voltage threshold for diagnosis of CAN-Timeout

Variable	Source	Type	Description
B_CLCINS		EIN	condition clear fault path CINS
B_CMUTE	CAN	EIN	
B_FLBC		EIN	condition: car with Florence Body Computer
B_JNS1NEW		EIN	Condition: CAN-message INSTR1 received
B_KL15		EIN	condition ignition switch on
B_SICINS	DCINS	AUS	signal error CAN interface instruments
B_TDCAN	CAN	EIN	
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for initialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BUSOFF	CAN	EIN	
E_CINS	DCINS	AUS	Error flag: CAN interface, timeout instrument
FSP_CL		EIN	clear fault memory
SFPCINS	DCINS	AUS	status fault path: timeout CAN interface instruments
TIMMOT_W		EIN	Timer:time after engine start n>NINI (word)
UB	SWADAP	EIN	battery voltage
Z_CINS	DCINS	AUS	Cycle flag: CAN interface, timeout instrument



## FW DCINS 8.30 Fixed Values

Parameter	Value	Description
CDTCINS		code word tester: CAN-Timeout, Instruments
CLACINS		fault class: CAN interface, timeout instruments
FLCCINS		fault set debouncing: CAN interface, timeout instrument
HLCCINS		fault reset debouncing: CAN interface, timeout instrument
TDCINS		Time for timeout detection CAN interface combi-instrument
TDHCINS		Time for fault rectification CAN timeout combined instrument
UBDCAN		battery voltage threshold for diagnosis of CAN-Timeout

## FB DCINS 8.30 Detailed description of function

### APP DCINS 8.30 Application hint

## DCAS 14.20 Diagnosis CAN timeout ASC interface

### FDEF DCAS 14.20 Function definition

No text for FDEF available!

### ABK DCAS 14.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCCAS	BLOKNR		KL	code word CARB: CAN interface, timeout ASC
CDTCAS			FW	code word tester: CAN interface, time out ASC [216]
CLACAS			FW	fault class: timeout asc-message
FFTCAS	BLOKNR		KL	Freeze Frame table: CAN, timeout ASC
FLCCAS			FW	fault set debouncing: CAN interface, timeout ASC
HLCCAS			FW	fault reset debouncing: CAN interface, timeout ASC
TDCAS			FW	Time for timeout detection CAN interface ASC
TDHCAS			FW	
UBDCAN			FW	battery voltage threshold for diagnosis of CAN-Timeout

Variable	Source	Type	Description
B_ASC1NEW		EIN	condition CAN-ASC1 message current receive
B_ASC2NEW		EIN	condition CAN-ASC2 interface with o.k. status
B_CLCAS		EIN	condition clear fault path CAS
B_CMUTE	CAN	EIN	
B_KL15		EIN	condition ignition switch on
B_SICAS	DCAS	AUS	signal error CAN interface ASC
B_TDCAN	CAN	EIN	
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BUSOFF	CAN	EIN	
E_CAS	DCAS	AUS	errorflag: CAN-interface, timeout ASC
SFPCAS	DCAS	AUS	status fault path: timeout CAN interface ASC
TIMMOT_W		EIN	Timer:time after engine start n>NINI (word)
UB	SWADAP	EIN	battery voltage
Z_CAS	DCAS	AUS	cyclus flag: CAN interface, timeout ASC

### FW DCAS 14.20 Fixed Values

Parameter	Value	Description
CDTCAS		code word tester: CAN interface, time out ASC [216]
CLACAS		fault class: timeout asc-message
FLCCAS		fault set debouncing: CAN interface, timeout ASC
HLCCAS		fault reset debouncing: CAN interface, timeout ASC
TDCAS		Time for timeout detection CAN interface ASC
TDHCAS		
UBDCAN		battery voltage threshold for diagnosis of CAN-Timeout

## FB DCAS 14.20 Detailed description of function

### APP DCAS 14.20 Application hint

## DCKUP 3.20 Diagnosis; CAN-Timeout interface electronic clutch control (KUP)

### FDEF DCKUP 3.20 Function definition

No text for FDEF available!

### ABK DCKUP 3.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCKUP	BLOKNR		KL	code word CARB: CAN-bus, timeout clutch
CDTCKUP			FW	code word tester: CAN-bus, timeout clutch
CLACKUP			FW	fault class: CAN-timeout KUP-message
FFTKUP	BLOKNR		KL	freeze frame table: CAN-timeout KUP-message
FLCKUP			FW	fault set debouncing: CAN-bus, timeout clutch





Parameter	Source-X	Source-Y	Type	Description
HLCKKUP			FW	fault reset debouncing: CAN-bus, timeout clutch
TDCINS			FW	Time for timeout detection CAN interface combi-instrument
TDCKUP			FW	time for CAN-timeout recognition KUP-message
TDHCKUP			FW	
UBDCAN			FW	battery voltage threshold for diagnosis of CAN-Timeout

Variable	Source	Type	Description
B_CLCKUP		EIN	condition clear fault path CKUP
B_CMUTE	CAN	EIN	
B_KL15		EIN	condition ignition switch on
B_KUP1NEW		EIN	condition CAN-KUP1-message received
B_SELESPEE		EIN	
B_SICKUP	DCKUP	LOK	signal error: CAN-timeout Kup-message
C_FCMCLR	DCKUP	LOK	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_BUSOFF	CAN	EIN	
E_CKUP		EIN	error flag: CAN-bus, timeout clutch
SFPCKUP	DCKUP	LOK	status fault path: CAN-timeout Kup-message
TIMMOT		EIN	Timer:time after engine start n>NINI
UB	SWADAP	EIN	battery voltage
Z_CKUP		EIN	cycle flag: CAN-bus, timeout clutch

### FW DCKUP 3.20 Fixed Values

Parameter	Value	Description
CDTCKUP		code word tester: CAN-bus, timeout clutch
CLACKUP		fault class: CAN-timeout KUP-message
FLCCKUP		fault set debouncing: CAN-bus, timeout clutch
HLCKKUP		fault reset debouncing: CAN-bus, timeout clutch
TDCINS		Time for timeout detection CAN interface combi-instrument
TDCKUP		time for CAN-timeout recognition KUP-message
TDHCKUP		
UBDCAN		battery voltage threshold for diagnosis of CAN-Timeout

### FB DCKUP 3.20 Detailed description of function

### APP DCKUP 3.20 Application hint

## TN 3.10 Output of engine speed signal

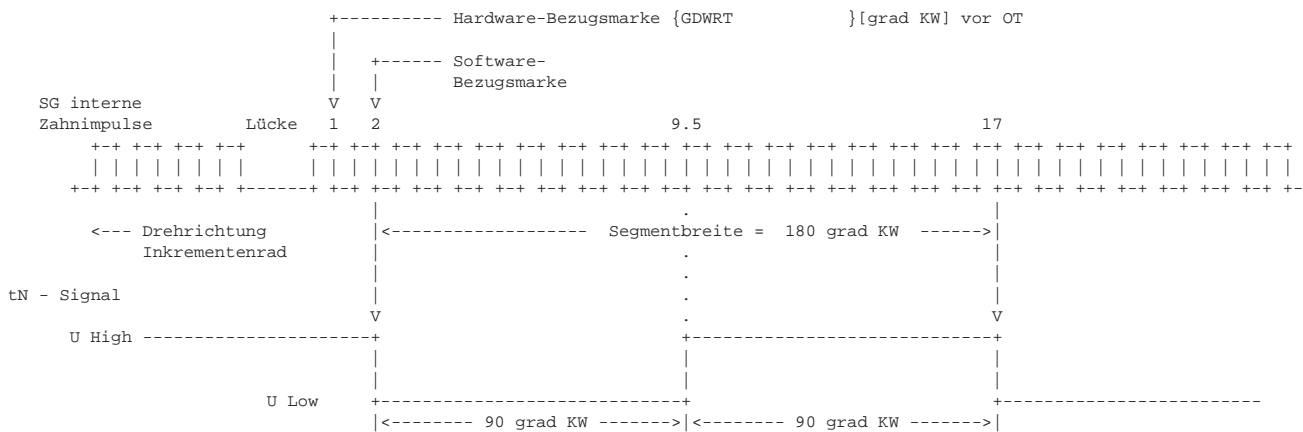
### FDEF TN 3.10 Function definition

Initialisierung : Nach S\_Kl.15 = "EIN" und Initialisierung der Endstufe beginnend mit High-Pegel.

Signalausgabe : 1.Signal-Ausgabe nach der 1. erkannten Lücke.  
Signal wird Segmentsynchron als symmetrischer Low/High-Impuls mit jeweils 90 grad KW Länge ausgegeben.

Haltephase : In der Haltephase wird bis n < NMIN (Drehzahlimpulse werden noch erkannt) das tN-Signal weiter ausgegeben.

Diagnose : Falls die Drehzahlerfassung nicht in Ordnung ist (Fehlerflag = E.n gesetzt), wird ein Low-Pegel ausgegeben.





## ABK TN 3.10 Abbreviations

{GDWRT } Immediate Konstante  
{NMIN } Immediate Konstante

## FB TN 3.10 Detailed description of function

## APP TN 3.10 Application hint

## EEPROM 11.30 EEPROM treatment

### FDEF EEPROM 11.30 Function definition

### ABK EEPROM 11.30 Abbreviations

### FW EEPROM 11.30 Fixed Values

Parameter	Value	Description
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## FB EEPROM 11.30 Detailed description of function

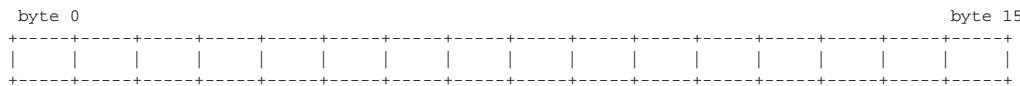
EEPROM treatment

Data which are to be maintained also in the event of powerfail are stored in the EEPROM.

Partitioning of the EEPROM

The project-specific structure and partition as well as the contents of the EEPROM are determined in a header file. The area of the EEPROM is divided into blocks and pages. A block may consist of one or several pages. Blocks have version numbers in order to be able to detect a changed EEPROM assignment and the consistency of EEPROM and program version. These blocks are used for the logical structuring and it is possible to initialize them individually. The version number and the length of the block are stored in the first two bytes of the first page of a block.

Structure of a page



The typical length of a page is 16 bytes (for presently used EEPROMs). For the configuration of the page a page descriptor exist in the flash-EPROM.

	configured	
page 0	<-----	page descriptor 0
storage mode		
page 1	<-----	page descriptor 1
page 2	<-----	page descriptor 2
page .	<-----	page descriptor .
page .	<-----	page descriptor .
page .	<-----	page descriptor .
page 31	<-----	page descriptor 31

The following is specified in the page descriptor:

- Is the check sum stored in the last two bytes of the page ?
- Is the page mirror-imaged in the RAM ?
- Is the page the first page in the block or the double storage of the first page ?
- Is external writing into the page allowed ?
- Is external reading of the page allowed ?
- Is the initialization of the data on detection of non-correctable errors (check sum test) allowed ?
- Is the page the first or the second page of a double storage ?

In the individual pages and blocks the data are to be divided such that the chosen integrity strategy, described below, is sufficient for all data and that the configuration of the page and of the block suits all data of the page. It is useful to store the first page of a block twice, so that in case of incorrect data in this page not the entire block is going to be initialized.

Access mode

In the permanent RAM a mirror-image of the EEPROM pages can be stored. This is configured in the page descriptor for each page. During the initialization of the ECU program the EEPROM pages (as far as they are configured as page with mirror-image in the permanent RAM and as far as it was determined by means of check sum test that the contents is correct) are copied into the corresponding mirror-image pages in the the permanent RAM. In case of changed data the contents of the mirror-imaged pages is written into the the corresponding pages in the EEPROM during the ECU after-run. Furthermore, it is possible to write event-triggered data into an EEPROM page and, as far as configured, into the corresponding mirror-image page.



The functions only have access to the data of the mirror and not to the EEPROM directly. An exception here, is the reading via external services (e.g. tester). Since the data in the mirror cannot be entered into the DAMOS (they are addressed by a structure) and since they are thus not available to application tools, it is necessary to use an additional RAM-cell for application relevant values, and to copy their contents cyclic or during the ECU

after-run into the mirror. During the copying procedure the check sum is updated via a routine (subtraction of the value to be overwritten and summing of the value to be written).

In the process the following must be paid attention to:

- When only copying during the ECU after-run there is a risk that the RAM-cell was corrupted since the latest writing procedure (program error or inverted bit). Data which were changed in such a way are then interpreted as correct data and they may possibly be stored in the EEPROM for a long time.
- Since the above-mentioned routine must be used for the copying into the mirror, it is run-time relevant in case of cyclic call-up in small time cycles.
- It is recommendable to perform a plausibility check on the value to be written, just prior to the writing procedure !

The EEPROM can be cleared completely (in future) and it can then be initialized again.

#### Data integrity

After each writing procedure into the EEPROM the correctness is checked by another reading and by comparing the transmitted data. Incorrect writing procedures are repeated up to two times..

The external reading and writing access (e.g. tester) can, as already mentioned above, be configurated via the page descriptor. Dependent on the demand made on the data integrity of a page it is possible to choose between different storage modes and combinations of them.

- Single storage
- Multiple storage (presently only double storage is realized)
- Check sum in the page in the EEPROM and in the mirror.

With multiple storage, however, only one mirror-image of the page is stored in the permanent RAM.

During the reading of a page the data contents is checked for correctness by means of the check sum.

If a loss of data is detected during the reading of the EEPROM pages in the ECU program initialization, then the redundant storage modes are used in the following order so as to determine the correct data:

1. Multiple storage (s) in the EEPROM
2. Mirror page in the permanent RAM
3. Default values from the flash EPROM

The correction for the mirror is performed immediately, i.e. during the reading in the ECU program initialization. For the EEPROM pages it is performed only during the after-run by overwriting them with the corrected mirror pages.

The contents of the EEPROM is project-specific and it is defined in the section EEDAT.



## APP EEPROM 11.30 Application hint

## DCDACC 1.10 Diagnosis; access to tester data

### FDEF DCDACC 1.10 Function definition

The scope of data per fault path and the access by the tester to the output data are set in this function using system constants.

The following data are set:

CDTdfp: SY\_CDTSIZE = SY\_SGANZ,

Available per fault path dfp is

either a CDT characteristic value (for SY\_SGANZ = 1)

or a block of CDT characteristic values (length = SY\_SGANZ).

Data assignment: Value in block no. 0 assigned here to ECU no. 1 and value in block no. 1 to ECU no. 2, etc.

CDCdfp: SY\_CDCCSIZE = 4 \* SY\_SGANZ,

Available per fault path dfp is

either a block of CDC characteristic values of length 4 (for SY\_SGANZ = 1)

or a block of CDC characteristic values of length 8 (for SY\_SGANZ = 2) etc.

Data assignment: Values in block nos. 0 - 3 assigned here to ECU no. 1 and values in block nos. 4 - 7 to ECU no. 2, etc.

CDKdfp: SY\_CDKSIZE = SY\_SGANZ,

Available per fault path dfp is

either a CDK characteristic value (for SY\_SGANZ = 1)

or a block of CDK characteristic values (of length = SY\_SGANZ).

Data assignment: Value in block no. 0 assigned here to ECU no. 1 and value in block no. 2 to ECU no. 2, etc.

CLAdfp: SY\_CLASIZE = SY\_SGANZ,

Available per fault path dfp is

either a CLA characteristic value (for SY\_SGANZ = 1)

or a block of CLA characteristic values (of length = SY\_SGANZ).

Data assignment: Value in block no. 0 assigned here to ECU no. 1 and value in block no. 1 to ECU no. 2, etc.

TSFdfp: SY\_TSFSIZE = 1, a TSF characteristic value is available per fault path.

Variation by e.g. SY\_SGANZ is not required here.

FFTdfp: SY\_FFTSIZE = SY\_DFPMEUV, a block of length SY\_DFPMEUV of FFT characteristic values is available.

Variation by e.g. SY\_SGANZ is not required here.

### ABK DCDACC 1.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
SY_CDCCSIZE			SYS	System constant: Number of values CDC to each fault path
SY_CDKSIZE			SYS	System constant: Number of values CDK to each fault path
SY_CDTSIZE			SYS	System constant: Number of values CDT to each fault path
SY_CLASIZE			SYS	System constant: Number of values CLA to each fault path
SY_DFPMEUV			SYS	system constant: environmental conditions in fault code memory
SY_FFTSIZE			SYS	System constant: Number of values FFT to each fault path
SY_SGANZ			SYS	system constant number engine control unit
SY_TSFSIZE			SYS	System constant: Number of values TSF to each fault path

### FW DCDACC 1.10 Fixed Values

Parameter	Value	Description

### FB DCDACC 1.10 Detailed description of function

### APP DCDACC 1.10 Application hint

## DFPM 3.10 OBDII; Fault path manager

### FDEF DFPM 3.10 Function definition

Overview: Diagnostic fault path manager within the system





## FB DFPM 3.10 Detailed description of function

### Overview:

1. Memory areas of the DFPM
  - 1.1 Status array (sfp)
  - 1.2 Fault code memory (fcm)
2. Methods
  - 2.1 Methods for actions of the diagnostic functions
  - 2.2 Methods for actions within DFPM
  - 2.3 Methods for event trigger
  - 2.4 Methods for MIL activation
  - 2.5 Methods for tester interface
3. DFPM processes
4. Used data
5. Description of the function
  - 5.1 Fault recognition; change of error flag E\_abc 0->1; call method fcmErr()
  - 5.2 Fault recognition; change of fault type; call method fcmTyp()
  - 5.3 o.k. recognition; change of error flag E\_abc 1->0; call method fcmOk()
  - 5.4 Test recognition; change of cycle flag Z\_abc 0->1; call method fcmZyf()
  - 5.5 Trigger recogn.; e.g. change of B\_dcyc 0->1; call method fcmTrig()
  - 5.6 Time trigger for fault active time within process dfpm\_time
  - 5.7 After-run within process dfpm\_nl
  - 5.8 Short overview of the strategy for MIL activation
6. References

### Description:

1. Memory areas of the DFPM  
The both memory areas status array (sfp) and fault code memory (fcm) are located within the buffered RAM.  
Data loss with power fail is possible.

- 1.1 Status array (sfpdfp); each fault path dfp has exactly one status word sfpdfp (16bit) with the following content:

- 
- |        |       |           |   |    |
|--------|-------|-----------|---|----|
| 1.1.0  | bit0  | E_dfp     | fault flag; test result of the latest test  |    |
| 1.1.1  | bit1  | Z_dfp     | cycle flag; confirmation for min. one successful test during the current driving cycle.       |    |
| 1.1.2  | bit2  |           | reserved  |    |
| 1.1.3  | bit3  |           | reserved  |    |
| 1.1.4  | bit4  |           | reserved  |    |
| 1.1.5  | bit5  |           | reserved  |    |
| 1.1.6  | bit6  | B_bkdfp   | flag for backup value; active whenever dfp uses backup values.                                |    |
| 1.1.7  | bit7  | B_cldfp   | clear flag; interface for fault path specific actions during erasure of the fault code memory |    |
|        |       |           |   |    |
| 1.1.8  | bit8  | B_mxdfp   | fault type flag; 'value higher than high limit' with latest test                              |    |
| 1.1.9  | bit9  | B_mndfp   | fault type flag; 'value lower than low limit' with latest test                                |    |
| 1.1.10 | bit10 | B_sidfp   | fault type flag; 'no signal' with latest test   |    |
| 1.1.11 | bit11 | B_npdfp   | fault type flag; 'result not plausible' with latest test                                      |    |
| 1.1.12 | bit12 | sfpdfp.12 | fault exists and is stored within FCM   | ## |
| 1.1.13 | bit13 | sfpdfp.13 | fault path at minimum once tested since power fail / FCM clear (dfp-ready)                    | ## |
| 1.1.14 | bit14 |           | reserved  |    |
| 1.1.15 | bit15 |           | reserved  |    |

- 1.2 fault code memory (fcm); only contains information of faulty tests with the following content (bytes):

-----  
Maximum SY\_fcmsize fault path entries are possible. ##

- |       |        |            |   |
|-------|--------|------------|---|
| 1.2.1 | byte1  | dfp        | fault path identifier; programm status-specific number from 1...n.  |
| 1.2.2 | byte2  | tsf        | counter for fault active time; each stored fault has a value with the measured time during the fault was active (E-dfp = 1). During after-run each fault path with tsf > TSFdfp and E_dfp=0 is set to emission related (like E_dfp=1). With first storage of the fault, the tsf is set to 0. With engine start and n > nmin tsf is set to 0, this is to allow measuring of tsf from last driving cycle during ign. on and engine not running. With tsf = 255 the counter is stopped without overflow. |
| 1.2.3 | byte3  | fps        | status of fault path with latest entry (E_dfp, etc.)  |
|       | bit3.0 | fps.erfact | copy of the latest E_dfp out of status array sfpdfp   |
|       | bit3.1 | fps.zyf    | copy of the latest Z_dfp out of status array sfpdfp   |
|       | bit3.2 | fps.ekd    | reserved, not used yet  |
|       | bit3.3 | fps.zkd    | reserved, not used yet  |
|       | bit3.4 | fps.fa     | entry of fault code during activity of service test equipment   |
|       | bit3.5 | fps.be     | entry of fault code during activity of end of line test equipment   |
|       | bit3.6 | fps.nnl    | reserved, not used yet  |
|       | bit3.7 | fps.nn2    | reserved, not used yet  |



1.2.4 byte4 typ type of fault at first and latest entry.

bit4.0 typ.actmax 'value was higher than high limit' with latest entry  
bit4.1 typ.actmin 'value was lower than low limit' with latest entry  
bit4.2 typ.actsig 'no signal' with latest entry  
bit4.3 typ.actnpl 'result not plausible' with latest entry  
bit4.4 typ.inimax 'value was higher than high limit' with first entry  
bit4.5 typ.inimin 'value was lower than low limit' with first entry  
bit4.6 typ.inisig 'no signal' with first entry  
bit4.7 typ.ininpl 'result not plausible' with first entry

1.2.5 byte5 fes status of fault entry; dynamical evaluation of CARB relation  
bit5.0 fes.erfprl error flag debounced  
bit5.1 fes.dauer FLC was min. one time at zero, FCM deletion due to CARB  
bit5.2 fes.scatt fault entry is visible for scan tool (dynamic) see ->%TCSORT ##  
bit5.3 fes.mil fault entry is relevant for MIL  
bit5.4 fes.blink fault entry with MIL blinking  
bit5.5 fes.multi sporadic fault  
bit5.6 fes.epcl fault entry is relevant for EPCL (see ->%DEPCLx.y)  
bit5.7 fes.nn2 reserved

1.2.6 byte6 cla class of fault path; entry from class table (see ->%DCLAx.y)

1.2.7 byte7 flc MIL-on - counter; trigger due to class table

1.2.8 byte8 hlc MIL-off - counter; trigger due to class table

1.2.9 byte9 dlc delete counter; For each detected fault an individual fault delete counter (DLCabc) is used.  
It determines the duration of storage of the corresponding fault. At each first detection (not yet debounced, 'probable fault') dlcdfp is set due to class table CLAdfp to DLCPRL (e.g. 80 dec).  
If this fault is neither confirmed nor detected as healed within these DLCPRL dcy/wuc, it will be deleted.  
As soon as a 'probable' fault is detected as healed, the dlcdfp is set to the value ADSTKD acc. CLAdfp.  
As soon as a 'probable' fault is confirmed, the dlcdfp is set to the value ADSTFD (40dez) acc. CARB.  
This value is fixed up to recognized healing (MIL off acc. this fault).  
As long as a 'probable fault' is not yet 'confirmed', or as soon as a fault is detected as healed, the corresponding dlcdfp is decremented by 1 in the stop phase of each cycle where 'warm-up cycle' was detected (B\_wuc=1). --> %DWUC.  
If dlcdfp reaches here the value 0, the fault (and if necessary its corresponding freeze frame) will be erased completely out of the memory.

1.2.10 byte10 First freeze frame value according to -->%DFRZx.y ##

1.2.11 Byte21 + SY\_ffesize First value of environmental conditions ##  
Entry of SY\_envblok blocks of ambient conditions out of FFTdfp ext. ambient conditions -->%DUMWEXx.y ##  
Structure of the block of ambient cond.: First top\_w, then FFTdfp with length SY\_dfpmenv ##

1.2.12 Byte21 + SY\_ffesize + SY\_envblok \* (SY\_dfpmenv + SY\_dfpmtim): hz frequency counter ##  
At the first detection of a fault, the frequency counter is set to the initial value 01.  
At each 'new detection' after detected healing, (e.g. at loose contacts) the frequency counter is increased by 1.  
Max. value 255 limits the frequency counter to the top; no overflow active.

1.2.13 Byte21 + SY\_ffesize + SY\_envblok \* (SY\_dfpmenv + SY\_dfpmtim) + 1: cks check sum ##  
check sum for this fault path entry

Depending on the overall length of the entry, one additional byte with value 00 is used to keep the entry within word-structure. ##

2. Methods  
-----

2.1 Methods for actions of the diagnostic functions  
2.1.1 getSfp() read-out of the status word sfpdfp of a fault path dfp out of the status array  
2.1.2 repSfp() write the statusword sfpdfp of a fault path dfp into the status array  
2.1.3 getErf() read-out of the error flag E\_dfp of a fault path dfp out of the status array  
2.1.4 getZyf() read-out of the cycle flag Z\_dfp of a fault path dfp out of the status array  
2.1.5 getClf() read-out of the clear flag B\_cldfp of a fault path dfp out of the status array

2.2 Methods for actions within DFFPM  
2.2.1 fcmErr() fault path sends message: fault detected  
2.2.2 fcmZyf() fault path sends message: cycle flag is set, test fulfilled  
2.2.3 fcmOk() fault path sends message: fault healing or o.k. detected  
2.2.4 fcmTyp() fault path sends message: change of fault type

2.3 Methods for trigger events  
2.3.1 fcmTrig() call of a specific trigger event (B\_dcy, B\_wuc etc.)

2.4 Methods for activation of MIL or EPCL  
2.4.1 getMil() search for MIL-related state within the fault code memory  
2.4.2 getEpcl() search for EPCL-related state within the fault code memory

2.5 Methods for tester interface  
2.5.1 getErrCnt read-out of the number of emission related fault entries  
2.5.2 getErrLine() read-out of the specific line of the fault code memory  
2.5.3 getErrDfp() read-out of the specific fault path of the fault code memory  
2.5.4 delFCM deletion of the complete fault code memory with status array and possibly parts of diagnostic function.  
2.5.5 delErrDfp() deletion of this specific fault path entry  
2.5.6 getInfoLine() read-out of short information out of selected FCM line



### 3. Processes inside DFPM

- 3.1 dfpm\_nl generates the DFPM-specific actions within the after-run
- 3.2 dfpm\_clr generates the DFPM specific actions within the FCM deletion
- 3.3 dfpm\_ini generates the DFPM-specific actions within the initialisation task
- 3.4 dfpm\_time generates the DFPM-specific actions within the time task (0.5 s)
- 3.5 dfpm\_check verification of the FCM for plausible entries.

### 4. Used data

#### 4.1 Overall data

- 4.1.1 CLA table with different data as described in ->%DCLAx.y
- 4.1.2 FFT table with the selectable ambient conditions; described in ->%DFFTx.y

#### 4.2 Fault path specific data

- 4.2.1 CLAdfp fixed value; management class for selection out of CLA
- 4.2.2 TSFdfp fixed value; threshold value for fault active time decision
- 4.2.3 FFTdfp block of fixed values with length SY\_dfpmenv; selection of the value out of FFT-table. ->%DFFTx.y ##
- 4.2.4 CDTdfp fixed value(16bit); fault path specific number for response to the service tester with RB-K3 standard.  
The CDTdfp numbers are RB-K3 standardized by K3/EKS3-My, -Pk in chronological order.  
attention: no. 00 is not allowed, sign for empty memory  
no. >=65280 dez (FF00h) are stop criteria for fault memorisation.
- 4.2.5 CDCdfp block of fixed values (4\*16bit); SAE-fault codes for output to the OBD scan tool. -->%DCDCx.y ##  
The fault path identifier dfp has to be converted to the format of the SAE standard J2012.  
For each of the four possible fault types there is a specific code.  
Data application due to customer requirements.

### 5. Description of functional details

Entry, update and verification of the entries in the fault code memory are carried out only by one of the following trigger:

- 5.1 fault detection; change in errorflag E\_dfp 0->1; call of method fcmErr()

Whenever an error flag E\_dfp inside status word sfpdfp is set by a diagnostic function, the method fcmErr() is active.

Firstly it is searched within the fault code memory for an existing entry of the fault path dfp.

- If dfp is not yet stored, a new entry is generated. ---> 5.1.1
- If dfp is stored, an update is generated. ---> 5.1.2

- 5.1.1 New entry: the following values are stored at the end of the fault code memory

```
dfp      fault path identifier
fps      fault path status
typ.ini  fault path type at first entry (B_mxdfp, etc.)
fes      fault path status of entry; dynamical evaluation of the CARB-related status
cla      class of the fault path; CLAdfp
flc      MIL on - counter; is set to initial value due to the class table and is decremented by 1, only if the
          trigger event and the cycle flag Z_dfp are true.
tsf      fault active time; set to 0
hlc      MIL off - counter; is set to initial value due to CLAdfp
dlc      delete counter; is set to initial value due to fault path status fes.
hz       frequency counter; set to 1
frz0...  freeze frame; stored due to FFT,          see -->%DFRZx.y
ini_env... ambient conditions due to FFTdfp and -->%DUMWEXx.y at initial detection      ##
cks      write check sum
```

- 5.1.2 Update: the following values are updated:

```
fps      fault path status; new value
typ.act  fault path type at the current entry (B_mxdfp, etc.)
fes      fault path status of entry; dynamical evaluation of the CARB-related status
flc      MIL on - counter; decremented by 1, only if the trigger event and the cycle flag Z_dfp are true.
hlc      MIL off - counter; is set to initial value due to CLAdfp
dlc      delete counter; is set to initial value due to fault path status fes.
hz       frequency counter; increment by 1
act_env(x) ambient conditions due to FFTdfp stored to place X at this detection (->%DUMWEXx.y)      ##
          X = minimum out of frequency counter HZ and SY_envblok      ##
          Not yet used blocks of ambient conditions are set to FFhex      ##
cks      write new check sum
```

- 5.2 Fault detection; change of fault type, call method fcmTyp()

Whenever a fault type flag B\_xxdfp inside status word sfpdfp is changed by a diagnostic function, method fcmTyp() is active.

The following values are updated inside the FCM:

```
typ.act  fault path type at the current entry (B_mxdfp, etc.)
cks      write new check sum
```





5.3 Detection of healing; change of error flag E\_abc 1->0; call method fcmOk()

Whenever the error flag E\_dfp inside status word sfpdfp is reset by a diagnostic function, method fcmOk() is active. The following values are updated inside the FCM:

With pending, not yet CARB-debounced fault path status:

```

fps      fault path status; new value
fes      fault path status of entry; dynamical evaluation of the CARB-related status
dlc      delete counter; is set to ADSTKD
cks      write new check sum
    
```

With CARB-debounced fault path status:

```

fps      fault path status; new value
fes      fault path status of entry; dynamical evaluation of the CARB-related status
flc      MIL on - counter; incremented by 1, only if the trigger event and the cycle flag Z_dfp are true.
hlc      MIL off - counter; decremented by 1, only if the trigger event and the cycle flag Z_dfp are true.
cks      write new check sum
    
```

5.4 Test recognition; change of cycle flag Z\_abc 0->1; call method fcmZyf()

Whenever the cycle flag Z\_dfp inside status word sfpdfp is set by a diagnostic function, method fcmZyf() is active. The following values are updated inside the FCM (only if fault code entry is existing):

```

fps      fault path status; new value
fes      fault path status of entry; dynamical evaluation of the CARB-related status
cks      write new check sum
    
```

Whenever this E\_dfp = 1 the following values are updated additionally:

```

flc      MIL on - counter; decremented by 1, only if the trigger event (e.g. B_dcy) is true.
hlc      MIL off - counter; set to initial value due to CLAdfp
    
```

or, if this E\_dfp = 0, the following values are updated additionally:

```

hlc      MIL off - counter; decremented by 1, only if the trigger event is true.
    
```

5.5 Trigger recogn.; e.g. change of B\_dcy 0->1; call method fcmTrig()

Whenever one of the trigger functions is fulfilled, method fcmTrig() is active. The following values are updated inside the FCM:

```

fes      fault path status of entry; dynamic evaluation of the CARB-related status
flc      MIL on - counter; filtered to trigger according to CLAdfp and decremented by 1, only if a fault currently exists but is not debounced.
hlc      MIL off - counter; filtered to trigger according to CLAdfp and decremented by 1, only if a current fault is healed but not debounced.
cks      write new check sum
    
```

5.6 Time trigger for fault active time within process dfpm\_time

The following values are updated inside the FCM (only if fault code entry is existing):

```

tsf      fault active time; incremented by 1, if a fault currently exists
cks      write new check sum
    
```

5.7 Afterrun within process dfpm.nl

```

flc      MIL on - counter; decremented by 1, only if Z_dfp=1, E_dfp=0 and tsf > TSPdfp.
          Set to initial value due to CLAdfp, only if Z_dfp=1, E_dfp=0 und tsf <= TSPdfp.
dlc      delete counter; only if B_wuc = 1, each dlc of the stored and healed entries is decremented by 1.
cks      write new check sum
    
```

5.8 Short overview of the strategie for MIL activation

Description is based on change of states, only in the following 5 cases the fault code manager gets active:

Case 1: Change within the cycle status (e.g. B\_dcy 0 -> 1)

Cycle status (e.g. B_dcy)	cycle flag Z_xyz	error flag E_xyz	MIL on counter FLC	MIL off counter HLC	comment
0 -> 1	0	0/1	FLC = FLC	HLC = HLC	waiting for cycle flag
0 -> 1	1	0	FLC = FLC	HLC = HLC-1	o.k.- recognition
0 -> 1	1	1	FLC = FLC-1	HLC = HLC	fault recognition

Case 2: fault path test is fulfilled ( Z\_xyz 0 -> 1)

Cycle status (e.g. B_dcy)	cycle flag Z_xyz	error flag E_xyz	MIL on counter FLC	MIL off counter HLC	comment
0	0 -> 1	0/1	FLC = FLC	HLC = HLC	waiting for cycle status
1	0 -> 1	0	FLC = FLC	HLC = HLC-1	o.k.- recognition
1	0 -> 1	1	FLC = FLC-1	HLC = HLC	fault recognition



Case 3: fault is detected ( E\_xyz 0 -> 1)

Cycle status (e.g. B_dcy)	cycle flag Z_xyz	error flag E_xyz	MIL on counter FLC	MIL off counter HLC	comment
0	0/1	0 -> 1	FLC = FLC	HLC = HLC	waiting for cycle status
1	0	0 -> 1	FLC = FLC	HLC = max.	stopped healing
1	1	0 -> 1	FLC = FLC-1	HLC = max.	fault recognition

Case 4: healing is detected ( E\_xyz 1 -> 0)

Cycle status (e.g. B_dcy)	cycle flag Z_xyz	error flag E_xyz	MIL on counter FLC	MIL off counter HLC	comment
0	0/1	1 -> 0	FLC = FLC	HLC = HLC	waiting for cycle status
1	0	1 -> 0	FLC = FLC	HLC = HLC	waiting for cycle flag
1	1	1 -> 0	FLC = FLC+1	HLC = HLC-1	active debouncing for healing

Case 5: actions during after-run

Cycle status (e.g. B_dcy)	cycle flag Z_xyz	error flag E_xyz	MIL on counter FLC	MIL off counter HLC	comment
0	0/1	0/1	FLC = FLC	HLC = HLC	driving cycle too short
1	0	0/1	FLC = FLC	HLC = HLC	cycle flag missing
1	1	0 & TSF<limit	FLC = max.	HLC = HLC	driving cycle not MIL rel.
1	1	0 & TSF>limit	FLC = FLC-1	HLC = HLC	driving cycle with sporadic fault
1	1	1	FLC = FLC	HLC = HLC	actions during driving cycle fulfilled

## 6. References

To complete the description of the whole fault code manager the following sections have to be included:

description of class table CLA	-->%DCLAL.y	
description of selectable trigger events	-->%DTRIGx.y	##
description of the selectable ambient conditions / freeze frame values	-->%DFFT1.y	
description of the used freeze frame values	-->%DFRZx.y	
description of the used extended ambient condition values /-strategy	-->%DUMWEXx.y, -->%DTOPx.y	##
description of SAE fault codes	-->%DCDCx.y	##
description of the evaluation 'driving cycle'	-->%DDCYx.y	
description of the evaluation 'warm up cycle'	-->%DWUCx.y	
activation of the MIL	-->%DMILx.y	
activation of the EPCL	-->%DEPCLx.y	
Inspection/Maintenance-readiness code	-->%DIMCx.y	
read-out of the fault code memory by generic scan tool	-->%SCATTx.y	
or servise tester e.g. KTS300	-->%TK...x.y	

## APP DFPM 3.10 Application hint

For function specific label selection within VS100, etc. the DFPM-related fault path data are available with DFPM\_<function>.

Class table CLA::

Default table is prepared by K3/EKS3-Mayer, -Frank.

The storage of a fault - but not its recognition with output of the replacement functions and error flags, can be suppressed by dating the class CLAdfp correspondingly.

Fault active time TSFdfp:

Attention ! With low TSFdfp, decrementation of FLC is going faster -> MIL activation very soon!

With TSFdfp = 127,5 sec (255dez) the evaluation is switched off due to tsf > TSFdfp.

Debouncing then corresponds to the version preceeding the introduction of the fault active counter TSF.

Fault codes CDTgfp:

Following strictly the RB standard for CDTabc-Codes supports the use of application facilities and systems with a SW that is conceived one time regardless of specific customers or projects.

For measurement and application purposes, the RAM cell dfp\_ap is established. At each fault detection, the identifier dfp of the triggering fault is stored in this cell so that the information of the last detected fault is always available.

If the currently stored fault is detected as "healed" or deleted, the dfp\_ap will be set to 00h.

delete counter dlc (initial value due to CLAdfp)

Stand MAIL OUT 91-57: CARB-debounced = 40 dez; CARB-pending (only special faults) = 80 dez.;

only service related faults = approx. 10 dez.

SAE fault codes CDCdfp: see -->%DCDCx.y

##

Quality:

To assure a correct DFPM-function due to the CARB regulations, it is very important to observe the correctness of the fault recognition and the information-exchange with the DFPM via status array.

CARB-related diagnostic evaluations have to be fulfilled within a FTP72 cycle.



## DFPMPWF 1.10 Diagnosis fault path management; detection of powerfail

### FDEF DFPMPWF 1.10 Function definition

Statusarray und Fehlerspeicher werden am Beginn der INI auf folgende Zusammenhänge durchsucht:

1. Steht zu jedem sfpxxx mit mem-flag = 1 der entsprechende Fehlerspeichereintrag im Fehlerspeicher ?
2. Steht zu jedem sfpxxx mit mem-flag = 0 der entsprechende Fehlerspeichereintrag **n i c h t** im Fehlerspeicher ?
3. Entspricht die Anzahl der ermittelten mem-flags der Anzahl im Fehlerspeicherzähler fcmend ?

Wird einer der o.g. Zusammenhänge verletzt, so wird auf (zumindest teilweisen) Informationsverlust geschlossen und über die powerfail-Routine aktiviert.

### ABK DFPMPWF 1.10 Abbreviations

#### FW DFPMPWF 1.10 Fixed Values

Parameter	Value	Description
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### FB DFPMPWF 1.10 Detailed description of function

#### APP DFPMPWF 1.10 Application hint

## DTRIG 1.10 OBDII; Selectable trigger for fault path management

### FDEF DTRIG 1.10 Function definition

The following trigger events are selectable by the shown number: for more info see -->%DCLA

number	trigger	comment
0	B_no	no trigger selected
1	B_tim	timetrigger, Quantification according -->%DFPMx.y
2	B_dcy	Driving Cycle, see -->%DDCYx.y
3	B_wuc	Warm Up Cycle, see -->%DWUCx.y
4	B_sp1	special trigger 1 see -->%DMDMILx.y
5	B_sp2	special trigger 2 see -->%DMDMILx.y
6	B_sp3	special trigger 3 see -->%DKVSx.y

### ABK DTRIG 1.10 Abbreviations

Variable	Source	Type	Description
B_DCY	DDCY	EIN	condition for 'driving cycle' fulfilled
B_NO	DTRIG	LOK	Infinite-trigger of the fault path manager
B_SP1	DMDMIL	EIN	FLC-trigger of misfire detection
B_SP2	DMDMIL	EIN	HLC-trigger of misfire detection
B_SP3		EIN	special cycle trigger diagnosis fuel supply system
B_TIM	DTRIG	LOK	time trigger for fault path management
B_WUC	DWUC	EIN	condition for detected 'warm up cycle'

### FW DTRIG 1.10 Fixed Values

Parameter	Value	Description
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## FB DTRIG 1.10 Detailed description of function

### APP DTRIG 1.10 Application hint

## DFFT 1.40 Diagnostics; Freeze frame selection table

### FDEF DFFT 1.40 Function definition

Reference table of the measurement values in FFTdfp available for selection: ( max. 99 ! )

Quantisation of the fault code memory entry is due to the according label or the additionally described calculation

For 'not supported' values (FF) is used (eg. values for bank #2 within single bank-system) ##

Values with xxx\_u are not shure existing as byte. Maybe they are created within %DFFTCNVx.y as xxx\_u ! ##

Structure: No. 0 Substitute for 'not\_used'  
 No. 1 to 15 Reserved for CARB-Freeze Frame (lt. SAE J1979)  
 No. 16 to 99 Reserved for common values out of platform  
 No. 100 to 255 Reserved for project- / customerspecific add-ons; see -->%DFFTKx.y

No.	Value	Description	
0		not_used	
1	flglrs	Control status Bank 1	
2	flglrs2	Control status Bank 2	
3	rml	relative air mass	##
4	tmot_u	Engine temperature acc. SAE J1979	##
5	fr_u	Control factor bank1 (byte)	##
6	fra_u	Adaptation factor bank1 (byte)	##
7	fr2_u	Control factor bank2 (byte); if single bank system (SY_stervk=0) 'not supported' is used	##
8	fra2_u	Adaptation factor bank2 (byte); if single bank system (SY_stervk=0) 'not supported' is used	##
9	not supported	reserved for Intake-manifold pressure Q: 1kPA SAE J1979 Mode2,PID\$0B	##
10	nmot	Engine speed; Quantization is recalculated with output. ->%TC2MOD	##
11	vfzg_u	Vehicle speed acc. SAE J1979	##
12-16	not used	Reserved for extension SAE	
17	ml	Mass air flow	
18	tmot	Engine coolant temperature quantification systemspecific	##
19	tans	Intake-air temperature	
20	ub	Battery voltage	
21	wdkba	throttle angle	
22	usvk	Sensor voltage upstream catalyst bank 1	
23	ushk	Sensor voltage downstream catalyst bank 1	
24	usvk2	Sensor voltage upstream catalyst bank 2	
		if single bank system (SY_stervk = 0) 'not supported' is used	##
25	ushk2	Sensor voltage downstream catalyst bank 2	
		if single bank system (SY_stervk = 0) 'not supported' is used	##
26	rl	relative air charge	##
27	upwg1_u	voltage of pedal sensor poti 1 (byte)	
28	upwg2_u	voltage of pedal sensor poti 2 (byte)	
29	upwg2d_u	double voltage of pedal sensor poti 2 (byte)	
30	skapfad	Pathidentifier out of SKA	
31	egaspfad	Pathidentifier out of EGAS	
32	mpfad	Pathidentifier out of torque calculation	
33	mi_duf	Pathidentifier out of torque comparison	
34	rstpfad	Pathidentifier out of reset	
35	wped	standardized angle of acclerator pedal	



No.	Value	Description
36	tumg	Ambient temperature
37	tmew	engine temperature, backup value out of model
38	udkp1_u	Voltage throttle poti 1 (byte)
39	udkp2_u	Voltage throttle poti 2 (byte)
40	wdks	desired throttle angle, referring to lower mechanical stop
41	tabgm	Exhaust temperature upstream catalyst, out of model
42	tabgm2	Exhaust temperature upstream catalyst bank 2, out of model if single bank system (SY_stervk = 0) 'not supported' is used ##
43	tkatm	Catalyst temperature, out of model
44	tkatm2	Catalyst temperature, bank 2, out of model if single bank system (SY_stervk = 0) 'not supported' is used ##
45	uhsv	Voltage at the heater output stage upstream of the catalyst
46	uhsv2	Voltage at the heater output stage upstream of the catalyst bank 2 if single bank system (SY_stervk = 0) 'not supported' is used ##
47	uhsh	Voltage at the heater output stage downstream of the catalyst
48	uhsh2	Voltage at the heater output stage downstream of the catalyst bank 2 if single bank system (SY_stervk = 0) 'not supported' is used ##
49	rinv_u	Internal resistance oxygen sensor upstream catalyst (byte)
50	rinv2_u	Internal resistance oxygen sensor upstream catalyst bank 2 (byte) if single bank system (SY_stervk = 0) 'not supported' is used ##
51	rinh_u	Internal resistance oxygen sensor downstream catalyst (byte)
52	rinh2_u	Internal resistance oxygen sensor downstream catalyst bank 2 (byte) if single bank system (SY_stervk = 0) 'not supported' is used ##
53	pu	Ambient pressure
54	tpsvkmf_u	filtered cycle duration of sensor signal upstream cat. (byte)
55	tpsvkmf2_u	filtered cycle duration of sensor signal upstream cat. bank 2 (byte) if single bank system (SY_stervk = 0) 'not supported' is used ##
56	(fr_u)	replaced by no. 5
57	(fra_u)	replaced by no. 6
58	(fr2_u)	replaced by no. 7
59	(fra2_u)	replaced by no. 8
60	tfst	fuel level 1l/inc
61	(r1)	replaced by no. 26
62-99	not used	add-ons up to max. #99 tbd only by the responsible for %DFPM !!
100-255	not used	Reserved for project- / customerspecific add-ons

### ABK DFFT 1.40 Abbreviations

Variable	Source	Type	Description
EGASPFAD	DUF	EIN	ETS-path as environmental condition for diagnosis of function monitoring
FLGLRS	LREB	EIN	CARB FREEZE FRAME byte, bank 1, for lambda control
FLGLRS2	LREB	EIN	CARB FREEZE FRAME byte, bank 2, for lambda control
FR2_U	DFFTCNV	EIN	Lambda controller output (byte)
FRA2_U	DFFTCNV	EIN	multiplicative correction of the mixture adaptation (byte)
FRA_U	DFFTCNV	EIN	multiplicative correction of the mixture adaptation (byte)
FR_U	DFFTCNV	EIN	Lambda controller output (byte)
MI_DUF	DUF	EIN	actual torque at response of torque comparison in the function monitoring
ML	SWADAP	EIN	air mass flow
MPFAD	DUF	EIN	Torque path in function and function monitoring as environmental cond. of diag.
NMOT	SWADAP	EIN	engine speed
PU	BGPU	EIN	Ambient pressure
RINH2_U	DFFTCNV	EIN	Act. value (byte) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH_U	DFFTCNV	EIN	Actual value (byte) internal res. Ri-Nernst cell lambda sensor downstream cat
RINV2_U	DFFTCNV	EIN	Actual value of internal resistance of lambda sensor 2, pre cat (byte)
RINV_U	DFFTCNV	EIN	Actual value of internal resistance of lambda sensor,pre cat (byte)
RL	SWADAP	EIN	relative air charge
RML	BGRML	EIN	relative air mass (calc. load value) acc. to SAE J1979
RSTPFAD	DUR	EIN	Reset-path as environment condition for the diagnosis of processor monitoring
SKAPFAD	DUF	EIN	freeze frame information for SKA
TABGM	ATM	EIN	exhaust gas temperature upstream cat from exhaust temperature model
TABGM2	ATM	EIN	exhaust gas temperature2 upstream cat from exhaust temperature model bank2
TANS	SWADAP	EIN	Intake air temperature
TFST	GGFST	EIN	fuel level in tank
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TMEW	GGTFM	EIN	model-based substitute value for engine temperature signal in case of error
TMOT	SWADAP	EIN	Engine temperature
TMOT_U	DFFTCNV	EIN	Engine temperature with defined quantisation for FSP-freeze frame
TPSVKMF2_U	DFFTCNV	EIN	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (byte)
TPSVKMF_U	DFFTCNV	EIN	filtered cycle duration of sensor signal upstream cat. (byte)
TUMG		EIN	Ambient air temperature
UB	SWADAP	EIN	battery voltage
UDKP1_U	DFFTCNV	EIN	sensor voltage from throttle-valve potentiometer 1 (byte)
UDKP2_U	DFFTCNV	EIN	sensor voltage from throttle-valve potentiometer 2 (byte)
UHSH		EIN	Voltage at ECU heating power stage, post cat
UHSH2		EIN	Voltage at ECU heating power stage 2, post cat
UHSV		EIN	Voltage at the heater output stage upstream of the catalyzer
UHVS2		EIN	Voltage at the heater output stage 2 upstream of the catalyzer
UPWG1_U	DFFTCNV	EIN	Voltage PWG potentiometer 1 (byte)
UPWG2D_U	DFFTCNV	EIN	Doubled PWG potentiometer-2 voltage (byte)
UPWG2_U	DFFTCNV	EIN	Voltage PWG potentiometer 2 (byte)
USHK	GGLSH	EIN	output voltage oxygen sensor downstream catalyst



Variable	Source	Type	Description
USHK2	GGLSH	EIN	output voltage oxygen sensor downstream catalyst 2
USVK	GGLSV	EIN	output voltage oxygen sensor upstream catalyst
USVK2	GGLSV	EIN	output voltage oxygen sensor upstream catalyst 2
VFZGJ	DFFTCNV	EIN	Vehicle speed
WDKBA	GGDVE	EIN	throttle angle
WDKS	FUEDKSA	EIN	desired throttle angle w.r.t. to lower mechanical stop
WPED	GGPED	EIN	Standardized accelerator pedal angle

### FW DFFT 1.40 Fixed Values

Parameter	Value	Description
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### FB DFFT 1.40 Detailed description of function

#### APP DFFT 1.40 Application hint

Achtung, bei Änderung, Applikation von FFTdfp müssen zwingend auch die Testerservices entsprechend angepasst werden.  
Z.B. muß bei Anwendung von DIAS auf das neue .hex-File referenziert werden.

## DFFTK 1.10 Diagnosis; customer-specific list for selection of freeze-frame values

### DDEF DFFTK 1.10 Function definition

Reference table of the measurement values in FFTdfp available for selection: ( max. 255 ! No. 100 to 255 )  
Quantisation of the fault code memory entry is due to the according label or the additionally described calculation  
For not supported values 00 is used (eg. values for bank #2 within single bank-system)

Structure: No. 100 to 255 Reserved for project- / customerspecific add-ons, no structure for the moment

No.	Value	Description
100	tbd	
255	tbd	

### ABK DFFTK 1.10 Abbreviations

Variable	Source	Type	Description
NMOT	SWADAP	EIN	engine speed
TMOT	SWADAP	EIN	Engine temperature

### FW DFFTK 1.10 Fixed Values

Parameter	Value	Description
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## FB DFFTK 1.10 Detailed description of function

### APP DFFTK 1.10 Application hint

## DFFTCNV 3.30 Diagnosis; freeze frame table, conversion to bytes

### FDEF DFFTCNV 3.30 Function definition

Ambient condition values which are not available in the system in byte-quantization are converted to the correct quantization e.g. word-values xxx\_w are converted to byte-values xxx\_u for use within %DFFTx.y and %DFFTKx.y.

The following calculations are supported by this module:

Basic value and calc.	byte value	quantization	type of data
rl_w	*1) rl_u		unsigned byte
upwg1_w / 4	upwg1_u	spg_ub_b5	unsigned byte
upwg2_w / 4	upwg2_u	spg_ub_b5	unsigned byte
upwg2d_w / 4	upwg2d_u	spg_ub_b5	unsigned byte
udkp1_w / 16	udkp1_u	spg_ub_b5	unsigned byte
udkp2_w / 16	udkp2_u	spg_ub_b5	unsigned byte
rinv_w / 32	rinv_u	r_ub_q64	unsigned byte
rinv2_w / 32	rinv2_u	r_ub_q64	unsigned byte
rinh_w / 32	rinh_u	r_ub_q64	unsigned byte
rinh2_w / 32	rinh2_u	r_ub_q64	unsigned byte
tpsvkmf_w / 4	tpsvkmf_u	t10msxs_ub_b10p2	unsigned byte
tpsvkmf2_w / 4	tpsvkmf2_u	t10msxs_ub_b10p2	unsigned byte
fr_w / 256	fr_u	fak_ub_b2	unsigned byte
fra_w / 256	fra_u	fak_ub_b2	unsigned byte
fr2_w / 256	fr2_u	fak_ub_b2	unsigned byte
fra2_w / 256	fra2_u	fak_ub_b2	unsigned byte
tmotlin	tmot_u	temp_ub_q1_040	acc. SAE-Quantization
vfzg	vfzg_u	vfzg_q1p0	acc. SAE-Quantization
psdss_w / 256	psdss_u		

##

\*1) ( 255 \* rl\_w / rlugd\_w ) \* ( nmot\_w / NMAX )

### ABK DFFTCNV 3.30 Abbreviations

Variable	Source	Type	Description
FR2_U	DFFTCNV	AUS	Lambda controller output (byte)
FR2_W	LR	EIN	Lambda controller output (word)
FRA2_U	DFFTCNV	AUS	multiplicative correction of the mixture adaptation (byte)
FRA2_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FRA_U	DFFTCNV	AUS	multiplicative correction of the mixture adaptation (byte)
FRA_W	LRA	EIN	multiplicative correction of the mixture adaptation (word)
FR_U	DFFTCNV	AUS	Lambda controller output (byte)
FR_W	LR	EIN	Lambda controller output (word)
PSDSS_U	DFFTCNV	AUS	Intake manifold pressure from pressure sensor (DS-S) with SAE quantisation
PSDSS_W		EIN	Intake manifold pressure measured with pressure sensor at manifold (DS-S)
RINH2_U	DFFTCNV	AUS	Act. value (byte) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH2_W	GGLSH	EIN	Act. value (word) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH_U	DFFTCNV	AUS	Actual value (byte) internal res. Ri-Nernst cell lambda sensor downstream cat
RINH_W	GGLSH	EIN	Actual value (word) internal res. Ri-Nernst cell lambda sensor downstream cat
RINV2_U	DFFTCNV	AUS	Actual value of internal resistance of lambda sensor 2, pre cat (byte)
RINV2_W	GGLSV	EIN	Actual value of internal resistance of lambda sensor 2, pre ca
RINV_U	DFFTCNV	AUS	Actual value of internal resistance of lambda sensor,pre cat (byte)
RINV_W	GGLSV	EIN	Actual value of internal resistance of lambda sensor,pre cat (word)
RL_U	DFFTCNV	AUS	relative air charge (byte) for ambient cond. of fault code memory
RL_W	EGFE	EIN	relative air charge (Word)
TMOTLIN	GGTFM	EIN	Engine coolant temperature, linearised and calculated
TMOT_U	DFFTCNV	AUS	Engine temperature with defined quantisation for FSP-freeze frame
TPSVKMF2_U	DFFTCNV	AUS	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (byte)
TPSVKMF2_W	DLSA	EIN	filtered cycle duration of sensor signal upstream cat (cylinder row 2) (word)
TPSVKMF_U	DFFTCNV	AUS	filtered cycle duration of sensor signal upstream cat. (byte)
TPSVKMF_W	DLSA	EIN	filtered cycle duration of sensor signal upstream cat. (word)
UDKP1_U	DFFTCNV	AUS	sensor voltage from throttle-valve potentiometer 1 (byte)
UDKP1_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UDKP2_U	DFFTCNV	AUS	sensor voltage from throttle-valve potentiometer 2 (byte)
UDKP2_W		EIN	sensor voltage from throttle potentiometer 2 (word)
UPWG1_U	DFFTCNV	AUS	Voltage PWG potentiometer 1 (byte)
UPWG1_W		EIN	Voltage PWG potentiometer 1 (word)
UPWG2D_U	DFFTCNV	AUS	Doubled PWG potentiometer-2 voltage (byte)
UPWG2D_W		EIN	Doubled PWG potentiometer-2 voltage (word)
UPWG2_U	DFFTCNV	AUS	Voltage PWG potentiometer 2 (byte)
UPWG2_W		EIN	Voltage PWG potentiometer 2 (word)
VFZG	SWADAP	EIN	vehicle speed (km/h)
VFZG_U	DFFTCNV	AUS	Vehicle speed



## FW DFFTCNV 3.30 Fixed Values

Parameter	Value	Description
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## FB DFFTCNV 3.30 Detailed description of function

### APP DFFTCNV 3.30 Application hint

## DFRZ 20.20 OBDII; description 'freeze frame'

### FDEF DFRZ 20.20 Function definition

With new fault entry the following freeze frame values are stored within the fault code memory:

CARB-freeze frame according to the values 1 to 11 out of the basic freeze frame table	see -->%DFFTx.y	##
Extended freeze frame values according data EFFDFPM with length SY_ffesize out of the basic freeze frame table		##

### ABK DFRZ 20.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
EFFDFPM	BLOKNR		KL	Declaration of freeze frame extension out of table DFFT
SY_FFESIZE			SYS	system constant: Size of Freeze Frame-extension

### FB DFRZ 20.20 Detailed description of function

#### APP DFRZ 20.20 Application hint

Selection of the extended freeze frame values is possible by data EFFDFPM out of data FFT -->%DFFTx.y

## DTIP 1.30 OBDII; tester interface package

### FDEF DTIP 1.30 Function definition

The following methods to get interaction with an external scan tool via according interface are supported:

```

getErrorCnt      readout of the number of stored fault entries

getErrorLine()  readout of the specific line of the fault code memory
                 content of the line see -->%DFCMx.y

getErrorDfp()   readout of the specific fault path of the fault code memory
                 content of the line see -->%DFCMx.y

delFCM          deletion of the complete fault code memory FCM with status words sfpdfp and possibly parts of diagnostic functions

delErrDfp()     deletion of this specific fault path entry with status word sfpdfp and possibly parts of the diagnostic function.

getInfoLine()   readout of short info out of selected FCM line (Byte 0 to Byte 5); see -->%DFCMx.y

getInfoDfp()   readout of short info out of this specific fault path entry (Byte 0 to Byte 5); see -->%DFCMx.y

delFcmScatt    deletion only of the scatt-related fault path entries with their status word sfpdfp.

                 readout of the fault code memory by OBDII scan tool           -->%SCATTx.y
                 or servive tester e.g. KTS500                             -->%T2...x.v; %TK...x.y
    
```

Additionally the CARB freeze frame no.0 is selected for output to scan tool according SAE J1972 mode 2.





## ABK DTIP 1.30 Abbreviations

## FB DTIP 1.30 Detailed description of function

## APP DTIP 1.30 Application hint

## DFPMEEP 1.11 Diagnostic; Fault Path Manager, EEPROM storage

### FDEF DFPMEEP 1.11 Function definition

Im EEPROM werden folgende Fehlerspeichereinhalte gesichert und für eine Restaurierung von max. 10 Einträgen des Fehlerspeichers nach Powerfail bereitgehalten:

Fehlerpfadstatus	fps	(byte)
Fehlerpfadtyp	typ	(byte)
Fehlerpfad-Testercode	CDTdfp	(word)
Fehlerpfadidentifizier	dfp	(byte)
Fehlereintragsstatus	fes	(byte)

Nach Powerfail wird der Fehlerspeichereintrag wie folgt restauriert:

(Nur dann, wenn dfp und CDTdfp im aktuell vorliegenden Programmstand noch mit den gespeicherten Werten übereinstimmen.)

dfp	aus EEPROM übernehmen
tsf	auf 00 dez setzen
fps	aus EEPROM übernehmen
typ	aus EEPROM übernehmen
fes.erfprl	auf 0 setzen
fes.dauer	auf 0 setzen
fes.scatt	entsprechend CLAdfp setzen
fes.mil	auf 0 setzen
fes.blink	auf 0 setzen
fes.multi	auf 0 setzen
fes.epcl	auf 0 setzen
fes.nn2	auf 0 setzen
cla	entsprechend CLAdfp setzen
flc	entsprechend Class auf INI-Wert setzen
hlc	entsprechend Class auf Kundendienstwert setzen
dlc	entsprechend Class auf INI-Wert setzen
frz 0 - 10	auf FF hex setzen
initim	auf 0 setzen, da top_w nach powerfail auch 0 ist
inifft 1 + 2	auf FF hex setzen
acttim	auf 0 setzen, da top_w nach powerfail auch 0 ist
actfft 1 + 2	auf FF hex setzen
hz	auf 1 dez setzen

Weitere Info z.B. auch zur Ablagesystematik im EEPROM: siehe ->%EEPROMx.y und %EEDATx.y

### ABK DFPMEEP 1.11 Abbreviations

Abk.	Art	Beschreibung
----	---	-----

### FB DFPMEEP 1.11 Detailed description of function

Der Fehlerspeicher wird zu Beginn des Nachlaufs auf aktuelle Fehlerspeichereinträge durchsucht und über den EEPROM-Spiegel aktualisiert. Auch ein evtl. Löschen des Fehlerspeichers wird erst im Nachlauf in das EEPROM übernommen. -->%EEPROMx.y  
Falls mehr als 10 Einträge im Fehlerspeicher eingetragen sind, werden nur diese ersten 10 Einträge im EEPROM gespeichert.

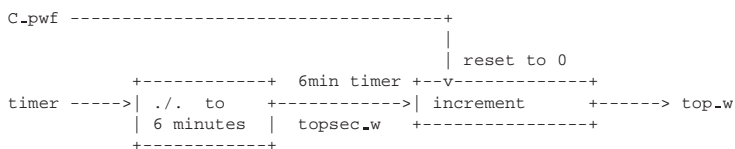
Nach Powerfail wird der Fehlerspeicher aus dem EEPROM heraus restauriert. Hierbei wird jeder betroffene Fehlerpfad auf den Zustand -geheilt nach einmaligem, nicht CARB-entprelltem Erkennen- gesetzt. Stimmt hierbei der CDTdfp aus dem EEPROM nicht mit dem CDTdfp aus dem ROM überein, so wird dieser Fehlereintrag nicht restauriert. (Datenkonsistenz bei Flash-Prog.)

Nicht restaurierbare Werte wie Freeze Frame, Umwelten etc. werden auf FF gesetzt.

### APP DFPMEEP 1.11 Application hint

## DTOP 1.0 Diagnosis; operating time

### FDEF DTOP 1.0 Function definition





### ABK DTOP 1.0 Abbreviations

Variable	Source	Type	Description
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
TOP_W	DTOP	AUS	operating time since powerfail

### FW DTOP 1.0 Fixed Values

Parameter	Value	Description
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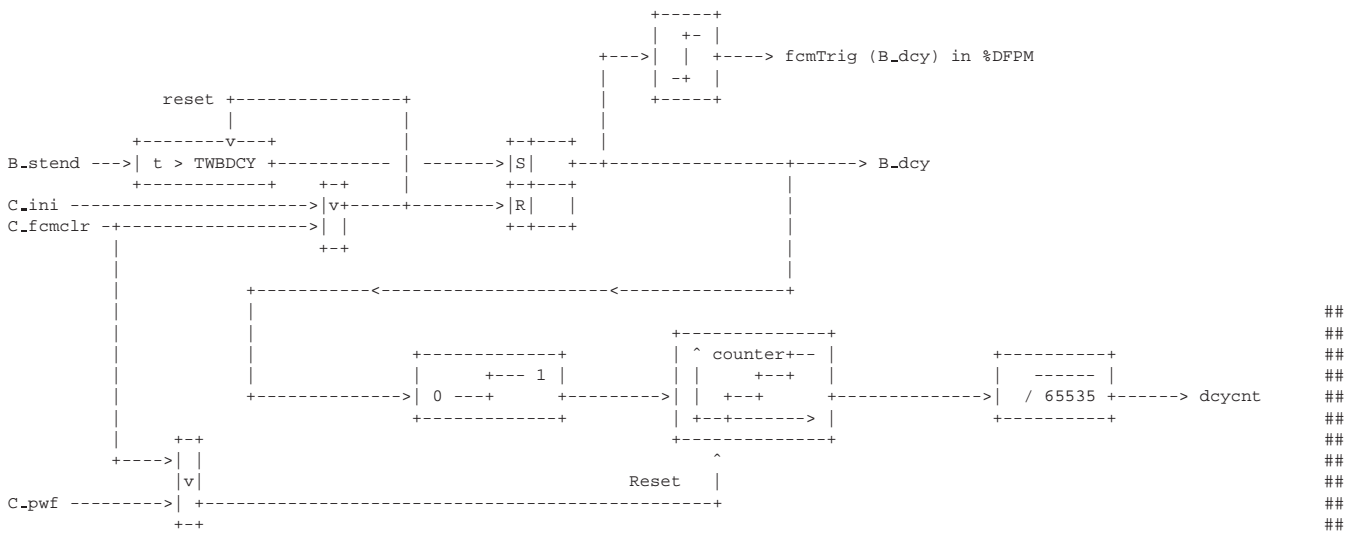
### FB DTOP 1.0 Detailed description of function

During engine running tow\_w is incremented every 6 minutes.

### APP DTOP 1.0 Application hint

## DDCY 15.10 OBDII; fulfillment condition 'driving cycle'

### FDEF DDCY 15.10 Function definition



### ABK DDCY 15.10 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TWBDCY			FW	waiting time for condition 'driving cycle'

Variable	Source	Type	Description
BBDCY	DDCY	AUS	Byte for condition B_dcy as trigger relevant in DCLA
B_DCY	DDCY	AUS	condition for 'driving cycle' fulfilled
B_STEND	BBSTT	EIN	condition end of start
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
DCYCNT	DDCY	AUS	driving cycle - counter

### FW DDCY 15.10 Fixed Values

Parameter	Value	Description
TWBDCY		waiting time for condition 'driving cycle'

### FB DDCY 15.10 Detailed description of function

TWBDCY seconds after engine start the 'driving cycle' condition B\_dcy is set and stored untill end of cycle. With change of B\_dcy 0 -> 1 inside the fault path manager all dcy-actions are run by method 'fcmTrig(B\_dcy) once per cycle.

With deletion of the fault code memory via C\_fmclr (even with running engine) B\_dcy is reset and TWBDCY is started again.

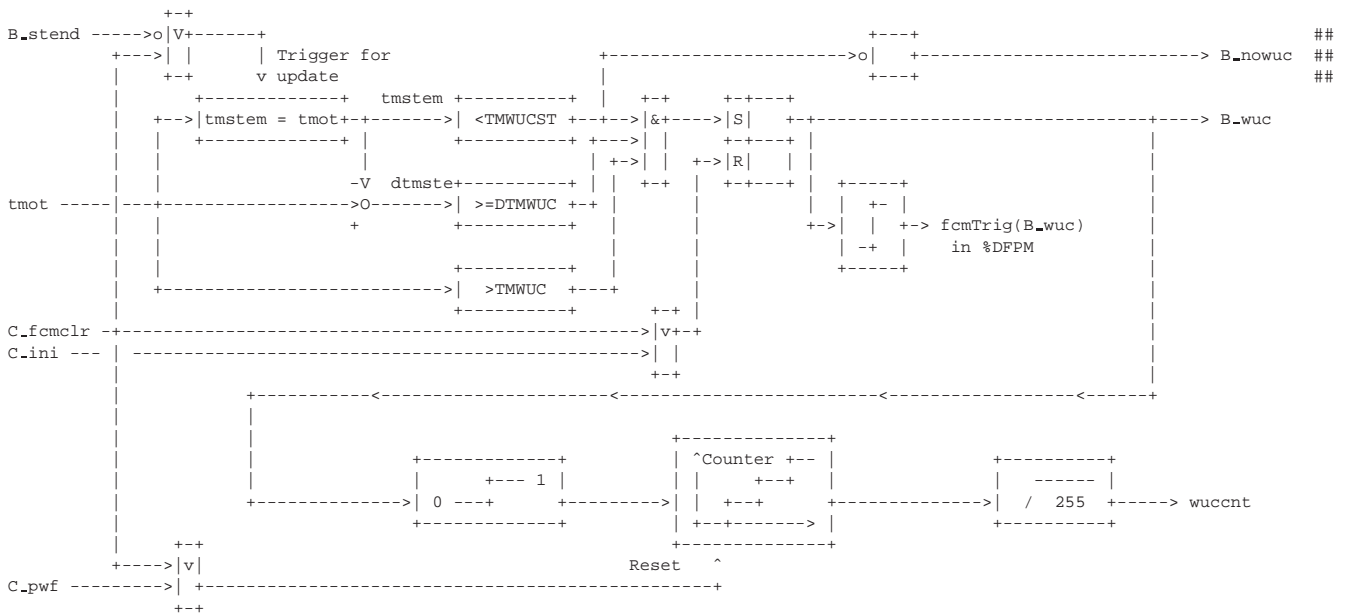
### APP DDCY 15.10 Application hint

Default value for TWBDCY: 5 sec; this for sure running of the engine in advance of 'sharpness' of the system. TWBDCY >> 5 sec gives more security, has to be CARB declared case by case.



## DWUC 14.20 OBDII; fulfillment condition 'warm up cycle'

### FDEF DWUC 14.20 Function definition



### ABK DWUC 14.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
DTMWUC			FW	delta engine temperture threshold for fulfilment "warm up cycle"
TMWUC			FW	engine temperture threshold for fulfilment "warm up cycle"
TMWUCST			FW	engine temperture threshold during cranking for fulfilment "warm up cycle"

Variable	Source	Type	Description
BBWUC	DWUC	AUS	Byte for condition B_wuc as trigger relevant in DCLA
B_NOWUC	DWUC	AUS	condition for 'no warm up cycle' detected
B_STEND	BBSTT	EIN	condition end of start
B_WUC	DWUC	AUS	condition for detected 'warm up cycle'
C_FCMLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
TMOT	SWADAP	EIN	Engine temperature
TMSTEM	DWUC	LOK	engine temperature at end of start memorized
WUCCNT	DWUC	AUS	Warm-up cycle - counter

### FW DWUC 14.20 Fixed Values

Parameter	Value	Description
DTMWUC		delta engine temperture threshold for fulfilment "warm up cycle"
TMWUC		engine temperture threshold for fulfilment "warm up cycle"
TMWUCST		engine temperture threshold during cranking for fulfilment "warm up cycle"

### FB DWUC 14.20 Detailed description of function

Following an engine start below the start temperature TMWUCST with subsequent heating by min. DTMWUC and reaching the upper temperature threshold TMWUC, the operating cycle is assigned the status 'warm-up cycle' with B\_wuc = 1. If the engine start is effected above the start temperature TMWUCST, it is signaled via B\_nowuc that no B\_wuc can be realized anymore during the actual driving cycle.

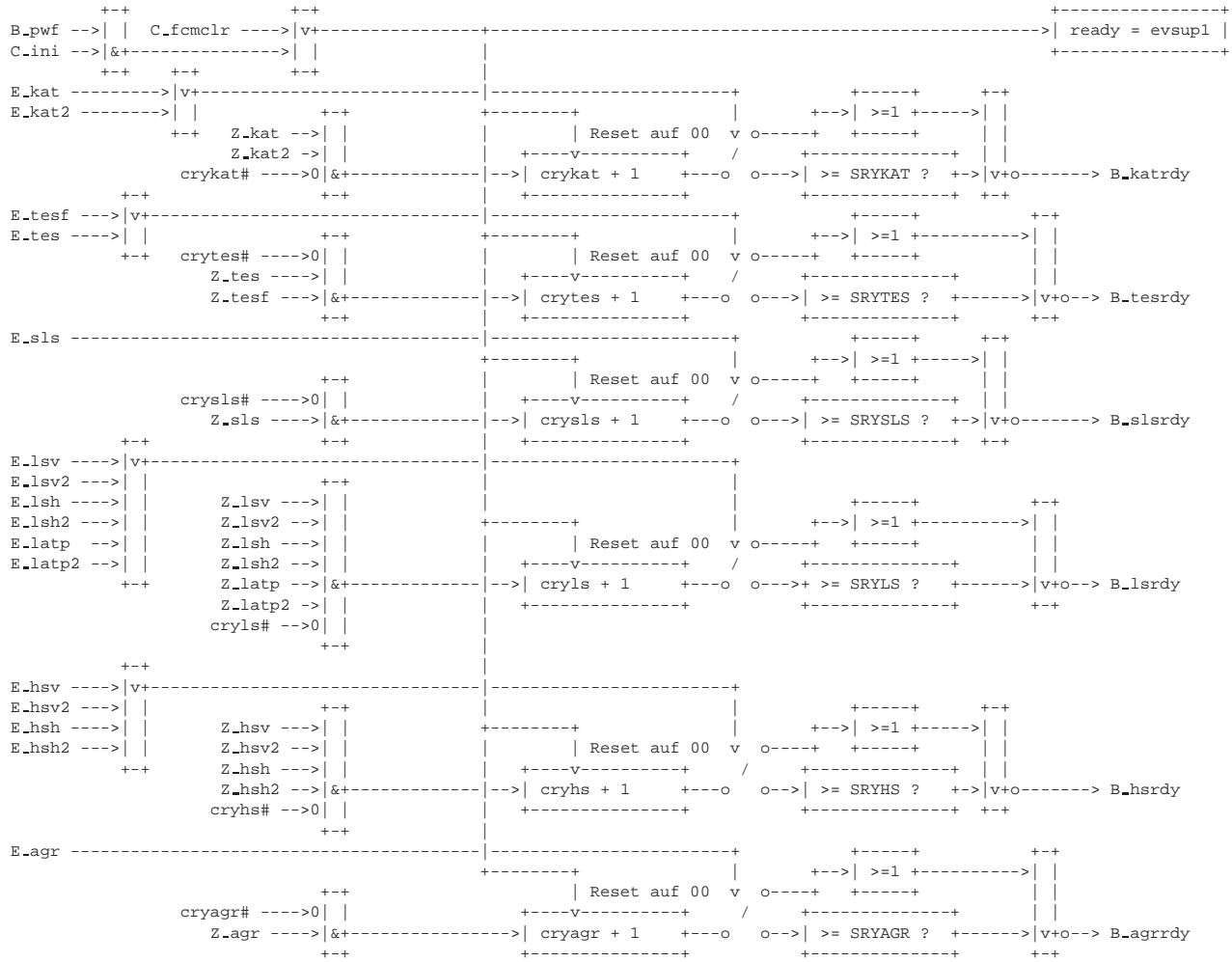
During the start (B\_st = 1), tmstem is continuously updated and remains stored at the start end (B.st 1->0) for the engine run. An update for tmstem is performed once for deletion of the fault memory (e.g. as well for a running engine). Amongst others, B\_wuc is also reset by the command 'delete fault memory' in C\_fcmlr.

The corresponding debouncing measures are executed by initiating with fcmTrig(B\_wuc), when the 'warm up cycle' is fulfilled. -> %DFPM

### APP DWUC 14.20 Application hint

Recommended values: DTMWUC = 21.00 deg. C  
TMWUC = 71.25 deg. C  
TMWUCST = < 69.75 deg. C





## ABK DIMC 41.10 Abbreviations

Variable	Source	Type	Description
B_AGRRDY	DIMC	AUS	status EGR tested for "ready byte"
B_CDAGR	PROKON	EIN	function active per codeword CDAGR
B_CDHSV	PROKON	EIN	function active per codeword CDHSV
B_CDLDP	PROKON	EIN	function active per codeword CDLDP
B_CDLSV	PROKON	EIN	function active per codeword CDLSV
B_CDSLS	PROKON	EIN	function active per codeword CDSLS
B_CDTES	PROKON	EIN	function active per codeword CDTES
B_HSRDY	DIMC	AUS	status O2 sensor heater tested for "ready byte"
B_KATFZ	PROKON	EIN	condition: cat fitted in vehicle
B_KATH	PROKON	EIN	Condition cat-heater installed in vehicle
B_KATHRDY	DIMC	AUS	status catalyst heater tested for "ready byte"
B_KATRDY	DIMC	AUS	status catalyst tested for "ready byte"
B_LSRDY	DIMC	AUS	status O2 sensors tested for "ready byte"
B_PWF		EIN	Condition for powerfail
B_SLSRDY	DIMC	AUS	status SAI system tested for "ready byte"
B_TESRDY	DIMC	AUS	status purge system tested for "ready byte"
CRYAGR		EIN	counter for setting readiness flag - EGR diagnosis
CRYHS		EIN	counter for setting readiness flag - oxygen sensor heater diagnosis
CRYKAT		EIN	counter for setting readiness flag - catalyst monitoring diagnosis
CRYLS		EIN	counter for setting readiness flag - oxygen sensor diagnosis
CRYSLs		EIN	counter for setting readiness flag - secondary air system diagnosis
CRYTES		EIN	counter for setting readiness flag - canister purge diagnosis
C_FCMCLR		EIN	system state: reset fault memory
C_INI	SWADAP	EIN	ECU-condition for intialisation
EVSUP1	DIMC	AUS	function identifier for support SAE J1979 mode 2
E_AGRF		EIN	error flag: EGR flow monitoring
E_HSH	DHLSHK	EIN	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK	EIN	error flag: lambda sensor heating downstream cat on the right
E_HSV	DHLSVK	EIN	error flag: lambda sensor heating upstream cat
E_HSV2	DHLSVK	EIN	error flag: lambda sensor heating upstream cat on the right
E_KAT	DKAT	EIN	error flag: catalyst conversion
E_KAT2	DKAT	EIN	error flag: catalyst conversion (cylinder row 2)
E_LATP	DLSA	EIN	error flag: lambda sensor aging tp



Variable	Source	Type	Description
E_LATP2	DLSA	EIN	error flag: lambda sensor aging tp (cylinder row 2)
E_LSH	DLSH	EIN	error flag: lambda sensor downstream cat
E_LSH2	DLSH	EIN	Errorflag: Lambda-Sensor downstream bank2
E_LSV	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_LSV2	DLSV	EIN	error flag: lambda sensor upstream catalyst
E_SLS		EIN	error flag: secondary air system
E_TES	DTEV	EIN	error flag: canister purge system diagnosis
READY	DIMC	AUS	readiness byte for support SAE J1979 mode 2
Z_AGRF		EIN	cycle flag: monitoring of EGR flow
Z_HSH	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat
Z_HSH2	DHLSHK	EIN	cycle flag of lambda sensor heating downstream cat, cylinder row 2
Z_HSV	DHLSVK	EIN	cycle flag of lambda sensor heating upstream cat
Z_HSV2	DHLSVK	EIN	cycle flag of lambda sensor heating upstream cat, cylinder row 2
Z_KAT	DKAT	EIN	cycle flag of catalyst conversion
Z_KAT2	DKAT	EIN	cycle flag: catalyst conversion (2nd bank)
Z_LATP	DLSA	EIN	cycle flag of lambda sensor aging tp
Z_LATP2	DLSA	EIN	cycle flag of lambda sensor aging tp (cylinder row 2)
Z_LSH	DLSH	EIN	cycle-flag: lambda sensor downstream cat
Z_LSH2	DLSH	EIN	cycle-Flag: Lambda-sensor downstream cat bank2
Z_LSV	DLSV	EIN	cycle flag: lambda sensor upstream of catalyst
Z_LSV2	DLSV	EIN	cycle flag: 2nd lambda sensor upstream of catalyst
Z_SLS		EIN	cycle flag: secondary air system
Z_TES	DTEV	EIN	cycle flag of canister purge system

### FW DIMC 41.10 Fixed Values

Parameter	Value	Description
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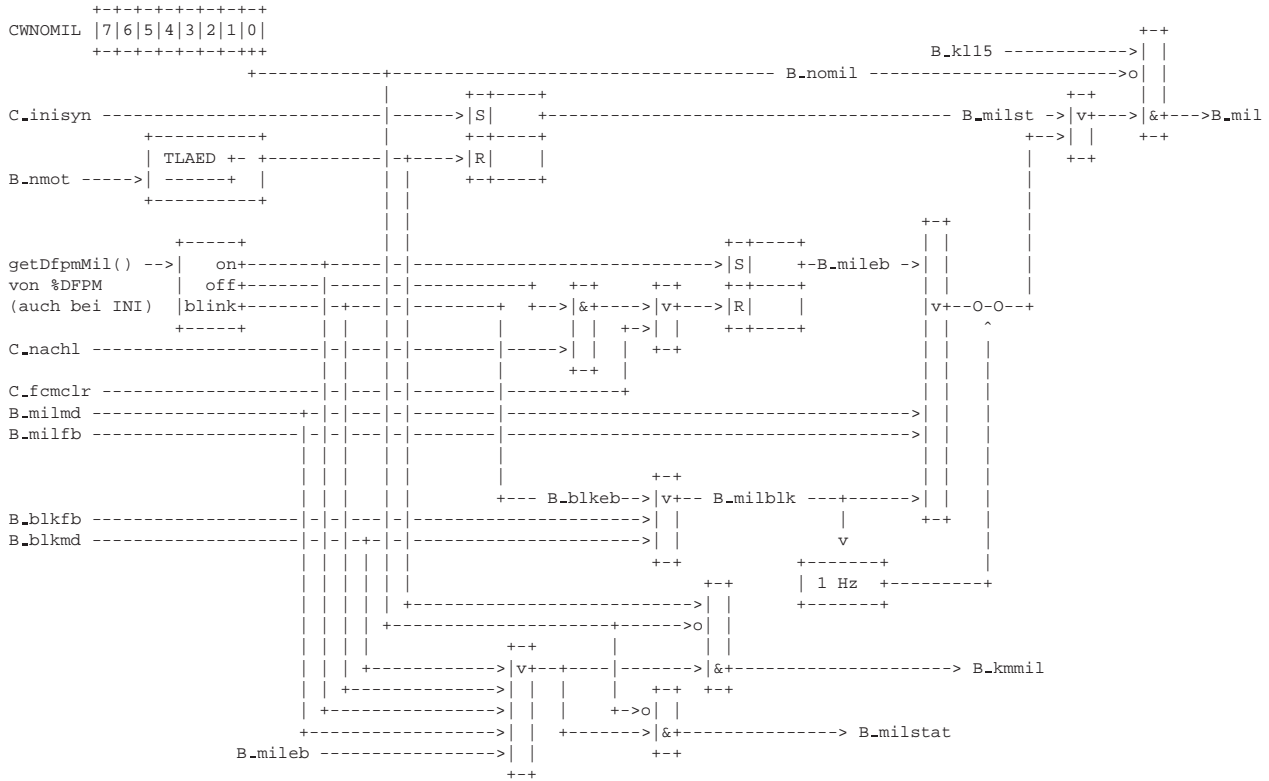
### FB DIMC 41.10 Detailed description of function

### APP DIMC 41.10 Application hint

The values of for the counter SRY.. are derived from the dating of the corr. FLC., refer to Classtab (Standard MY97 is 2)

## DMIL 26.40 OBDII; MIL control

### FDEF DMIL 26.40 Function definition



Faults which the MIL shall not control, can be dated accordingly (--> Classification table %DFPM)



## ABK DMIL 26.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CWNOMIL			FW	code word MIL-control not active
Variable	Source		Type	Description
B_BLKEB	DMIL		LOK	MIL activation blinking by own module
B_BLKFB			EIN	MIL-trigger blinking controlled by external ECU
B_BLKMD	DMDMIL		EIN	MIL-trigger blinking controlled by misfire detection
B_KL15			EIN	condition ignition switch on
B_KMMIL	DMIL		AUS	MIL turn-on related to mileage
B_MILBLK	DMIL		LOK	MIL turn-on blinking
B_MILEB	DMIL		LOK	MIL turn-on, self-controlled
B_MILFB			EIN	MIL controlled by external ECU
B_MILST	DMIL		LOK	MIL turn-on, test function during start
B_MILSTAT	DMIL		AUS	MIL-Status for Scan-Tool Mode \$01 PID \$01
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
B_NOMIL	DMIL		LOK	MIL turn-on blocked
C_FCMLR			EIN	system state: reset fault memory
C_INISYN			EIN	ECU-condition for intialisation of angle synchronization
C_NACHL			EIN	ECU condition for ECU switch off delay

## FW DMIL 26.40 Fixed Values

Parameter	Value	Description
CWNOMIL		code word MIL-control not active

## FB DMIL 26.40 Detailed description of function

Legislation requires the display of faults relevant to exhaust emission by a fault lamp (MIL) in the instrumentation board. The fault lamp may not be used for other purposes.

It shall display one of the following signs when triggered:

-Check Engine-; -Service Engine Soon-; -Check Powertrain- or -Service Powertrain Soon-

The MIL must illuminate for Ignition ON and standing engine for functional control.

For detected faults which are relevant to exhaust emission, the MIL must illuminate at latest following debounce of the legally permissible fault detection.

For special faults (e.g. detection of misfire rates damaging to the catalyzer), the MIL must blink immediately with 1 Hz.

The MIL may extinguish at the earliest after the legally permissible rectification debounce following detected rectification of all faults.

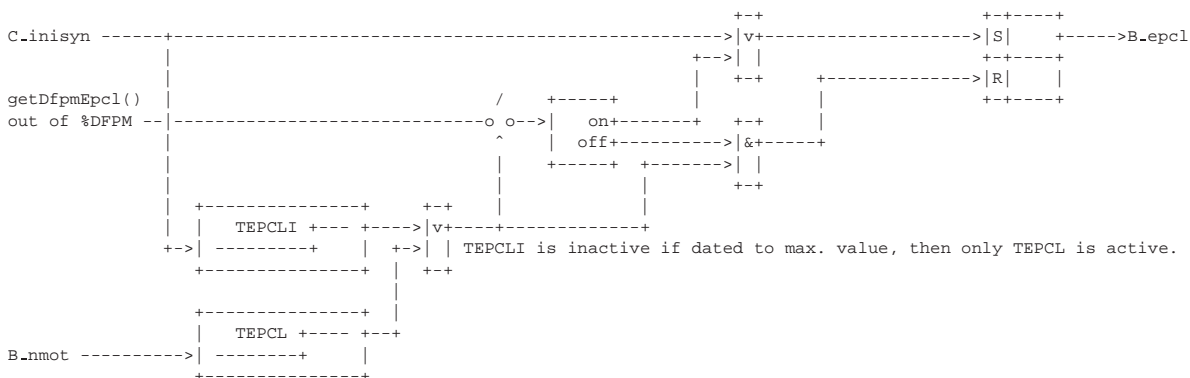
The MIL may only be controlled by one master SG on account of the checking function for ignition ON and the output stage diagnostics. Other SG's send requests for lamp control to this master SG, e.g. via CAN.

## APP DMIL 26.40 Application hint

Set TLAEED to 3 seconds.

## DEPCL 1.20 Diagnosis; electronic powertrain control lamp

### FDEF DEPCL 1.20 Function definition



Whithin the class table there is data CLAdfp defining which faults activate the EPCL. (--> see class table %DCLA)



## ABK DEPCL 1.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
TEPCL			FW	Time after engine start for end of EPCL test
TEPCLI			FW	Time after INI for end of EPCL test
Variable	Source		Type	Description
B_EPCL	DEPCL		AUS	Condition for activation of electronic powertrain control lamp
B_NMOT	GGDPG		EIN	condition engine speed: n > NMIN
C_JINISYN			EIN	ECU-condition for intialisation of angle synchronization

## FW DEPCL 1.20 Fixed Values

Parameter	Value	Description
TEPCL		Time after engine start for end of EPCL test
TEPCLI		Time after INI for end of EPCL test

## FB DEPCL 1.20 Detailed description of function

The EPCL has to be activated for min. a view seconds for visual control with ignition on and engine not running.

After the detection of a fault which has a strong impact to the driveability, the EPCL has to be activated immediately.

After healing of all relevant faults the EPCL may be switched off immediately.

To ensure the selftest of the power stage the EPCL has to be activated by only ECU.  
Other ECU's have to send a request to activate and deactivate the EPCL (e.g. via CAN).

## APP DEPCL 1.20 Application hint

For deactivation of EPCL with delaytime TEPCL after engine is running:

TEPCLI set to max. value; Default data for TEPCL is 3 sec.

For deactivation of EPCL with delaytime TEPCLI after INI:

TEPCLI auf z.B. 3 sec setzen; TEPCL >= TEPCLI setzen, sonst überwiegt TEPCL bei Schnellstart.

## RSTMON 2.10 Reset monitor

### FDEF RSTMON 2.10 Function definition

1. Reset monitor
- 1.1 Background:

In the ME7.0-Software there are a lot of reasons to Resets. In the development-phase there could be e.g. certain kind of errors, and wrong application data settings, which makes the ECU  $\mu$ C Reset itself. But there are also normal Reset-causes e.g. as the ignition switch is turned ON. To find the errors in the development-phase, one must be able to track the previous Reset-causes, preferably via the application tools VS-100 or VAT-2000.

### 1.2 Functional description:

The Reset-monitor is a SW-part which keeps track of the previous Reset-causes in the System. This is a cyclical buffer placed in Non-Volatile RAM, which is able to log the last 12 Reset-causes.

Before the SW causes a Reset, the variable resetIndication is set to match the appropriate cause. E.g. if a SW-Reset should be forced by the trap function handling Stack underflows, the resetIndication is set to "System stack underflow"-Reset (04h).

The resetIndication is read out in the ini-phase which follows the Reset. This takes place in a subroutine, which compares resetIndication with the last Reset-cause placed in the Reset-monitor. As long as the resetIndication is the same, no new entry is done in the Reset-monitor. Only a counter associated to the entry is then incremented.

An example of how the Reset-Monitor could look like is made in the following table:

Variable	Number of Resets (High Byte)	Reset-cause(Low Byte)
rstMon[0]	20h	06h
rstMon[1]	01h	03h
rstMon[2]	02h	06h
:	:	:

resetMonIdx = 2

The example should be read out in the following way:

At 1st took the 06-Reset place 20h times. Then the 03-Reset took place once, and after that the 06-Reset took place twice (which also was the previous Reset-cause, as the resetMonIdx is = 2).





The Reset-causes are to be read out according to the following table:

Name of Reset-cause	No:	Explanation
EXTERNAL_RESET	= 0,	reset due to RSTIN=low
WATCHDOG_RESET	= 1,	reset due to CPU-on-chip-Watchdog
DEADLINE_RESET	= 2,	reset due to deadline overrun
ILLBUS_TRAP_RESET	= 3,	reset due to ILLegal BUS Access
ILLINA_TRAP_RESET	= 4,	reset due to ILLegal INstruction Access
ILLOPA_TRAP_RESET	= 5,	reset due to ILLegal word OPerand Access
PRTFLT_TRAP_RESET	= 6,	reset due to PRoTection FauLT Flag
UNDOPC_TRAP_RESET	= 7,	reset due to UNdefined OPCode
STKUN_TRAP_RESET	= 8,	reset due to Stackunderflow
STKOV_TRAP_RESET	= 9,	reset due to Stack-overflow
NMI_TRAP_RESET	= 10,	reset due to Non-Maskable Interrupt and KL15-off Reset
KWP2000_RESET	= 11,	reset forced by KWP2000-service
AD_SCAN_ERROR_RESET	= 12,	reset due to AD scan error
SUPERVISOR_RESET_UM	= 13,	reset forced by supervisor modul (umkom)
SUPERVISOR_RESET_FU	= 14,	reset forced by safety monitoring moduls (ufxxxx, ufreac)
SUPERVISOR_RESET_RAMI	= 15,	reset forced by safety monitoring by internal ram-check (reservation)
SUPERVISOR_RESET_RAM	= 16,	reset forced by safety monitoring by ram-check in Init (urram)
SUPERVISOR_RESET_ROM	= 17,	reset forced by safety monitoring by rom-check in Init (urrom)
SUPERVISOR_RESET_RAMZ	= 18,	reset forced by safety monitoring by cyclic ram-check (urmem, urausg)
SUPERVISOR_RESET_ROMZ	= 19,	reset forced by safety monitoring by cyclic rom-check in Init (urmem)
SUPERVISOR_RESET_TV	= 20,	reset forced by safety monitoring to delay startup (urdelay)
SUPERVISOR_NOQUEST_RESET	= 21,	reset due to wrong question from
SUPERVISOR_DISPS_RESET	= 22,	reset due to failure in disabling power stage from UM
SUPERVISOR_RESET_UM_OBP	= 23,	reset forced by supervisor module ufobp)
SUPERVISOR_RESET_CCM_OBP	= 24,	reset forced by supervisor module (ufobp), CCM supervision
SUPERVISOR_NOQUEST_RESET_OBP	= 25,	reset forced by supervisor module (ufobp), wrong question
SUPERVISOR_RESET_RAMTAB	= 26,	reset forced due to illegal ramTableEntry
EEPROM_RESET	= 27,	reset forced by EEPROM module
ADDR_NOT_IN_SEG	= 28,	reset forced by powerfail-module (caused by addr. in diff. segments)
UNDEF_RESET	= 29	specifies end of enumeration

## 2. Trap functions

### 2.1 Background:

Trap functions are activated in response to special conditions that occur during the execution of instructions. Several hardware trap functions are provided by the C167 for handling erroneous conditions and exceptions that arise during the execution of an instruction.

### 2.2 Functional description:

The C167 is capable of detecting the following kind of exceptional HW events:

#### 1. Illegal External Bus Access

An external access has been attempted with no external bus defined. (Not an issue in ME7)

#### 2. Illegal Instruction Access

A branch to an odd address has been attempted.

#### 3. Illegal Word Operand Access

A word operand access (read or write) to an odd address has been attempted.

#### 4. Protection fault

A protect instruction with an illegal format has been detected.

#### 5. Undefined Opcode

The currently decoded instruction has no valid C167 opcode. (Used for the so called "error capturing instructions" in ME7.0)

All of the 5 faults listed above, lead to the execution of the interrupt service routine (ISR) for the so called "class B traps". To be able to search for the possible SW error which triggers the class B trap, there are two values which could be interesting. One of these is to know exactly which cause the class B trap has (one of those 5), and the second is to know at which program address the fault is triggered. This is solved via three variables, placed in non volatile RAM area, and visible for e.g. VS-100.

### 2.3 Execution example:

```

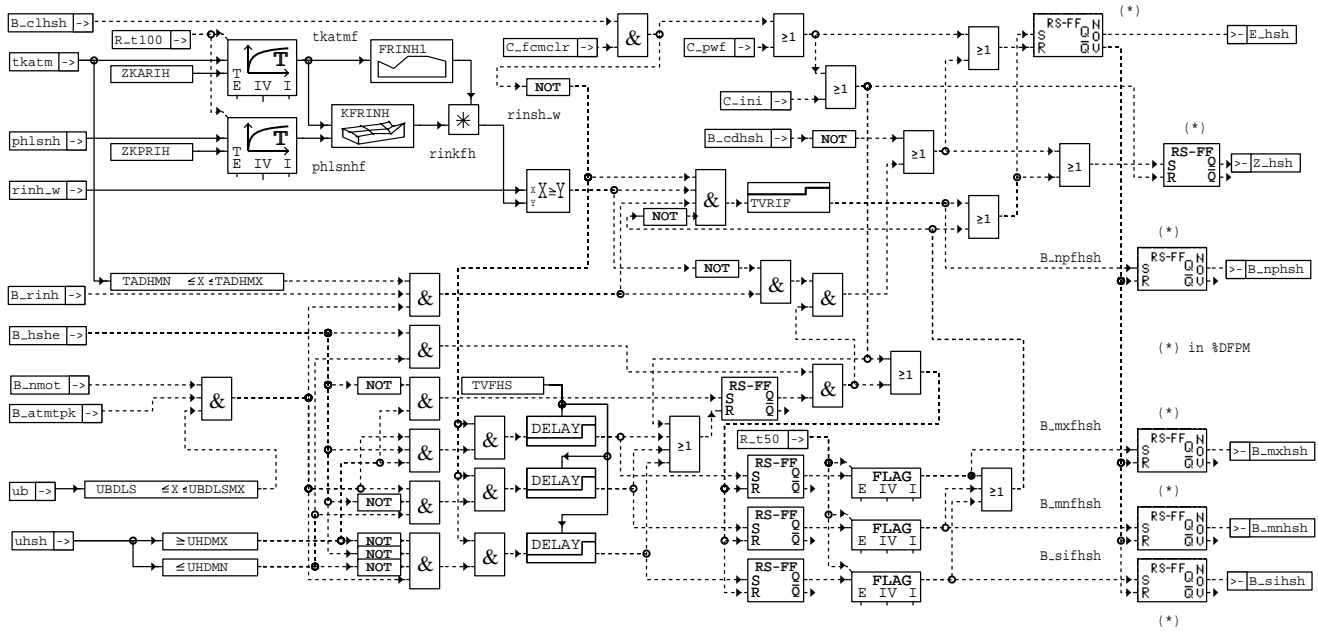
+----- enter class B trap isr
| +----- save value of Instruction Pointer (IP) -> mirrorIP
| | +----- save value of Code Segment Pointer (CSP) -> mirrorCSP
| | | +----- save value of Trap Flag Register (TFR) -> mirrorTFR
| | | | +--- Software Reset
| | | | | CLASS_B_TRAP as indication (for reset monitor)
| | | | |
+-----+-----> time
|
+---- start from Reset Vector (0x00000h)
    
```





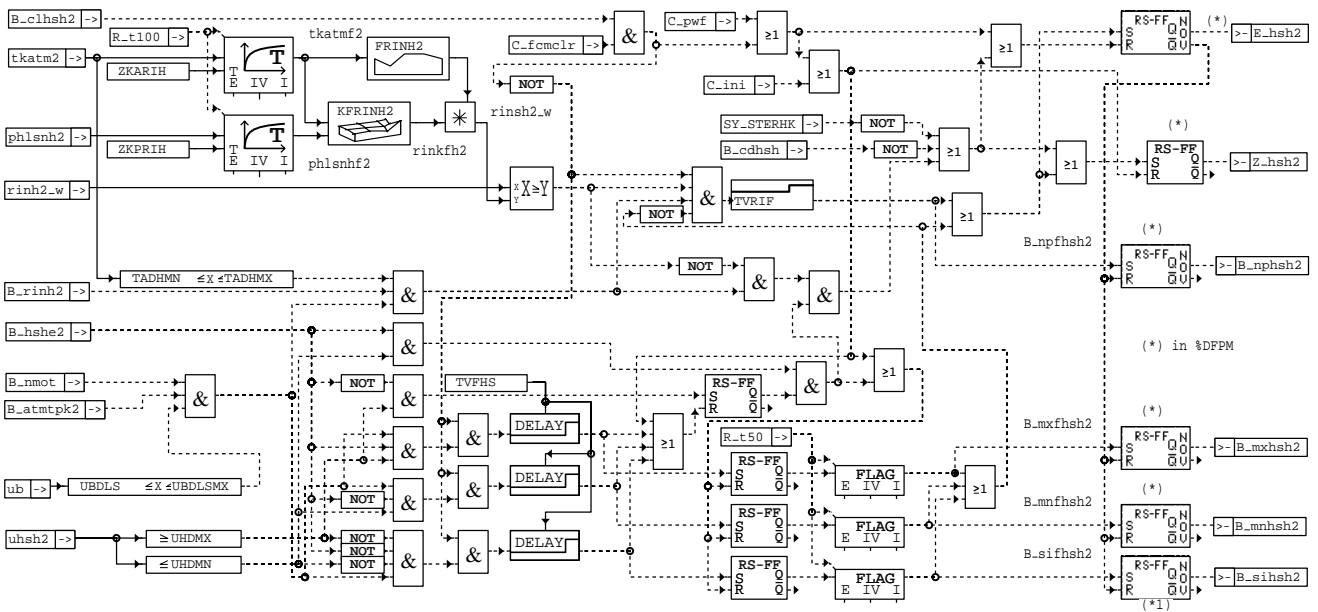
Status fault path: sfphsh  
 Error flag: E\_hsh  
 Cycle flag: Z\_hsh  
 Fault type: TYP\_hsh:  
 (B\_mxhsh, B\_mnhsh, B\_sihsh, B\_nphsh)  
 Clear fault path: B\_clhsh  
 Heater diagnosis downstream catalyst bank1

Default value active: B\_bkhsh (optional)  
 Fault path code: CDTHSH  
 Fault class: CLASHSH  
 Fault intensity: TSPHSH  
 CARB CODE: CDCHSH  
 Table of ambient cond.: FFTHSH



### dhlsk-dhlsk1

Heater diagnosis downstream catalyst bank2



### dhlsk-dhlsk2

#### ABK DHLSHK 2.40 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
CDCHSH	BLOKNR		KL	code word CARB: lambda sensor heating downstream cat
CDCHSH2	BLOKNR		KL	code word CARB: lambda sensor heating downstream cat
CDTHSH			FW	code word tester: oxygen sensor heater downstream catalyst
CDTHSH2			FW	code word tester: oxygen sensor heater downstream catalyst, cyl. row 2
CLASHSH			FW	Fault class: Heating, lambda sensor downstream of catalytic converter
CLASHSH2			FW	Fault class: Heating, lambda sensor 2 downstream of catalytic converter
FFTHSH	BLOKNR		KL	Table of ambient condition for heating O2-sensor post cat
FFTHSH2	BLOKNR		KL	Table ambient conditions heating lambda sensor downstream catalyst bank2
FRINH1	TKATMF		KL	Multiplication factor for RIN nominal value downstream of the catalyzer



Parameter	Source-X	Source-Y	Type	Description
FRINH2	TKATMF2		KL	Multiplication factor for RIN nominal value downstream of the catalyzer
KFRINH	TKATMF	PHLSNH	KF	MAP for Nernst resistor post cat
KFRINH2	TKATMF2	PHLSNH2	KF	MAP for Nernst resistor post cat bank 2
TADHMN			FW	lower Temperature threshold for die heater diagnostic routine
TADHMX			FW	upper Temperature threshold for die heater diagnostic routine
TSFHSH			FW	fault active time: lambda sensor heating catalyst downstream
TSFHSH2			FW	fault active time: lambda sensor heating catalyst downstream, bank2
TVFHS			FW	Dejettering time for heater power stage
TVRIF			FW	Delay time for Ri fault
UBDLS			FW	battery voltage threshold for release the sensor diagnosis
UBDLSMX			FW	upper battery voltage threshold for the sensor diagnosis
UHDMN			FW	Threshold for powered heater power stage
UHDMX			FW	Threshold for not powered heater power stage
ZKARIH			FW	Filter time const. sim. dyn. ceramic temp. for exhaust emis. temp. downstr. cat.
ZKPRIH			FW	Filter for sim. of dynamics for ceramic temp. from elec. heat. downstr.of cat.

Variable	Source	Type	Description
BLOKNR		EIN	DAMOS source for block number
B_ATMTPK	ATM	EIN	condition temperature downstream catalyst exceeds dew-point
B_ATMTPK2	ATM	EIN	condition temperature downstream catalyst exceeds dew-point2
B_CDHS	PROKON	EIN	function active per codeword CDHS
B_CLSH		EIN	condition clear failure path DHLSHK
B_CLSH2		EIN	condition clear failure path DHLSHK2
B_HSHE	HLS	EIN	condition for lambda sensor heating-switch downstream cat on
B_HSHE2	HLS	EIN	condition for lambda sensor2 heating-switch downstream cat on
B_MNFHSH	DHLSHK	LOK	Short circuit of heating O2 sensor post cat to ground
B_MNFHSH2	DHLSHK	LOK	Short circuit of heating O2 sensor post cat to ground
B_MNHSH	DHLSHK	AUS	Short circuit of heating O2 sensor post cat to ground
B_MNHSH2	DHLSHK	AUS	Short circuit of heating O2 sensor post cat to ground
B_MXFHSH	DHLSHK	LOK	Short circuit of heating O2 sensor post cat to Ubatt
B_MXFHSH2	DHLSHK	LOK	Short circuit of heating O2 sensor2 post cat to Ubatt
B_MXHSH	DHLSHK	AUS	Short circuit of heating O2 sensor post cat to Ubatt
B_MXHSH2	DHLSHK	AUS	Short circuit of heating O2 sensor 2 post cat to Ubatt
B_NMOT	GGDPG	EIN	condition engine speed: n > NMIN
B_NPFHSH	DHLSHK	LOK	Nernst resistance sensor downstream of the catalyzer too large
B_NPFHSH2	DHLSHK	LOK	Nernst resistance sensor 2 downstream of the catalyzer too large
B_NPHSH	DHLSHK	AUS	Nernst resistance sensor downstream of the catalyzer too large
B_NPHSH2	DHLSHK	AUS	Nernst resistance sensor 2 downstream of the catalyzer too large
B_RINH	GGLSH	EIN	Condition internal resistance of Ri-measur. of sensor active downstream cat.
B_RINH2	GGLSH	EIN	Condition internal resist. of Ri-meas. sensor active downstream cat. bank2
B_SIFHSH	DHLSHK	LOK	Load disconnection lambda sensor heating downstream cat.
B_SIFHSH2	DHLSHK	LOK	Load disconnection lambda sensor heating downstream cat. bank 2
B_SIHSH	DHLSHK	AUS	Load disconnection lambda sensor heating downstream cat.
B_SIHSH2	DHLSHK	AUS	Load disconnection lambda sensor heating downstream cat. bank 2
C_FCMCLR		EIN	system state: reset fault memory
C_JNI	SWADAP	EIN	ECU-condition for intialisation
C_PWF	SWADAP	EIN	ECU-condition powerfail initialisation
E_HSH	DHLSHK	AUS	error flag: lambda sensor heating downstream cat
E_HSH2	DHLSHK	AUS	error flag: lambda sensor heating downstream cat on the right
PHLSNH	HLS	EIN	Standardized heating power of the Lambda sensor downstream of the catalyzer
PHLSNH2	HLS	EIN	Standardized heating power of the Lambda sensor 2 downstream of the catalyzer
PHLSNH	DHLSHK	LOK	Standardized heating power of Lambda sensor downstream of catalyzer, filtered
PHLSNH2	DHLSHK	LOK	Standardized heating power of Lambda sensor 2 downstream of catalyzer, filtered
RINH2_W	GGLSH	EIN	Act. value (word) int. res. Ri-Nernst cell lambda sensor downstream cat bank2
RINH_W	GGLSH	EIN	Actual value (word) internal res. Ri-Nernst cell lambda sensor downstream cat
RINKFH	DHLSHK	LOK	Internal resistance Nernst cell of Lambda sensor from mapping upstream of cat.
RINKFH2	DHLSHK	LOK	Internal resistance Nernst cell of Lambda sensor 2 from mapping upstream of cat.
RINSH2_W	DHLSHK	LOK	Lim. value internal resistance Nernst cell of Lambda sensor 2 downstream of cat.
RINSH_W	DHLSHK	LOK	Lim. value internal resistance Nernst cell of Lambda sensor downstream of cat.
R_T100		EIN	Time schedule 100 ms
R_T50		EIN	Time schedule 50 ms
SFPHSH	DHLSHK	AUS	status fault path:
SFPHSH2	DHLSHK	AUS	status fault path:
SY_STERHK	PROKON	EIN	system parameter condition stereo downstream catalyst
TKATM	ATM	EIN	catalyst temperature (model)
TKATM2	ATM	EIN	catalyst temperature (model), bank2
TKATMF	DHLSHK	LOK	Filtered catalyzer temperature from model
TKATMF2	DHLSHK	LOK	Filtered catalyzer temperature from model, Bank2
UB	SWADAP	EIN	battery voltage
UHS		EIN	Voltage at ECU heating power stage, post cat
UHS2		EIN	Voltage at ECU heating power stage 2, post cat
Z_HSH	DHLSHK	AUS	cycle flag of lambda sensor heating downstream cat
Z_HSH2	DHLSHK	AUS	cycle flag of lambda sensor heating downstream cat, cylinder row 2

### FW DHLSHK 2.40 Fixed Values

Parameter	Value	Description
CDTHSH		code word tester: oxygen sensor heater downstream catalyst
CDTHSH2		code word tester: oxygen sensor heater downstream catalyst, cyl. row 2
CLASH		Fault class: Heating, lambda sensor downstream of catalytic converter
CLASH2		Fault class: Heating, lambda sensor 2 downstream of catalytic converter



Parameter	Value	Description
TADHMN		lower Temperature threshold for die heater diagnostic routine
TADHMX		upper Temperature threshold for die heater diagnostic routine
TSFHSH		fault active time: lambda sensor heating catalyst downstream
TSFHSH2		fault active time: lambda sensor heating catalyst downstream, bank2
TVFHS		Dejettering time for heater power stage
TVRIF		Delay time for Ri fault
UBDLS		battery voltage threshold for release the sensor diagnosis
UBDLSMX		upper battery voltage threshold for the sensor diagnosis
UHDMM		Threshold for powered heater power stage
UHDMX		Threshold for not powered heater power stage
ZKARIH		Filter time const. sim. dyn. ceramic temp. for exhaust emis. temp. downstr. cat.
ZKPRIH		Filter for sim. of dynamics for ceramic temp. from elec. heat. downstr.of cat.

### FB DHLSHK 2.40 Detailed description of function

With this DHLSHK an indirect check is performed on whether the heating of the Lambda sensor is operational, i.e. the measurement of the heater current by means of a shunt performed so far is abandoned.  
As criterion for the diagnosis the internal resistance of the Nernst cell of the Lambda sensor is used. With defective sensor heating the internal resistance (rinh\_w) is essentially larger. For the determination of rinh\_w the sensor voltage must be periodically connected to load with 0,5mA for 10ms (%GGLSH).  
In addition the switching behaviour of the heater power stage is monitored. For this an ADC-channel with a circuit per power stage is necessary, which is scanned in the 10ms grid. This circuit is necessary for the detection of "load drop".  
Circuit: 10 kOhm to ground, 10 kOhm to 5 Volt and connection ADC to power stage output via 22 kOhm.

#### Diagnosis internal resistance of the Nernst cell

Since the internal resistance rinh\_w is also dependent on the exhaust gas temperature and on the el. heating performance (phlsnh), the typical value of rinh\_w is stored in a map from tkatm and phlsnh.  
tkatm and phlsnh are filtered, since a change only affects rinh\_w after a delay.

#### Preconditions:

1. rinh\_w is updated (B\_rinh = 1)
2. The exhaust gas temperature is greater than the threshold TADHMN and lower than TADHMX
3. UB is within the diagnosis range

#### Diagnosis:

If rinh\_w is less than rinsh\_w, then B\_hsokh is set if additionally the switching behaviour of the power stage is OK.  
If rinh\_w is greater, then B\_nphsh is set.

#### Diagnosis switching behaviour of the heater power stage

For diagnosis purposes the power stage is switched off every 10s for 100ms (in %HLSHK). Then a check on whether the power stage is operational and whether the heater is connected to the battery voltage is performed.

#### Preconditions:

1. The power stage is switched on and off
2. UB must lie within the diagnosis range
3. The switch-off capability of the power stage (heater connected to UB) is stored

#### Diagnosis:

By a logic combination of the input and output of the power stage the power stage operation is checked.  
The faults are delayed by the time TVFHS in order to take into consideration fault reports, which are caused by calculation execution times between B\_hshe and uhsh.

#### Fault management

The debouncing of the heater faults is performed during two drives. If a heater fault is detected the fault lamp is only triggered if a fault is again detected during the second drive.

### APP DHLSHK 2.40 Application hint

Fault memory relevant values of the %DHLSHK are assigned to the %DFPM\_hsh in the function-orientated selection.

To be adjusted:

TADHMN = 200°C	UBDLSMX = 15.5V	UHSN = 13V (%HLS)	Filter values	LSH25P	LSH25PL	LSF4.7
TVFHS = 0.04s	UHDMM = 2.34V	TADHMX = 600°C	ZKARIH = 20s	46s	21s	
UBDLS = 10.7V	UHDMX = 3.6V		ZKPRIH = 35s	35s	10s	

TVRIF = 3s

#### KFRINH

The map values are determined by a measuring sensor with typical Nernst and heater internal resistance (Type "PM" from K3-LS/ESV). The measuring sensor must be of the same type as the intended control sensor.  
Adjust exhaust gas temperature to a base point value by an according selection of load and engine speed. It is possible to adjust phlsnh (performance) to a base point value by changing THSHKTA (in %HLSHK). Enter the value of rinh\_w into the map after approx. 60s.

LSF4.7					
phlsnh	E X .	G A S	T E M P E R A T U R E		
P	200	300	400	500	600
E	-----				
R	1.0	288	256	224	192
F	-----				
O	0.8	448	384	352	320
R	-----				
M	0.7	704	608	544	384
-----					

LSH25PL					
phlsnh	E X .	G A S	T E M P E R A T U R E		
P	200	300	400	500	600
E	-----				
R	1.0				
F	-----				
O	0.8				
R	-----				
M	0.7				
-----					

FRINH1/2 tkatmf/FRINH 200/63 300/50 400/30 500/10 600/5  
-----

The larger the factor FRINH is adjusted the more "inaccurate" the diagnosis of the internal resistance of the Nernst cell becomes. The map KFRINH , %ATM and the %HLSHK must already have been adjusted.

The faults E\_hsh and B\_nphsh should be entered, if the sensor heating operates with little heating performance only. This can be achieved by connecting a resistor in series to the heater and if FRINH is changed accordingly.

Necessary resistor: LSF4.7 ~ 11 Ohm, LSH25 ~ 5 Ohm.

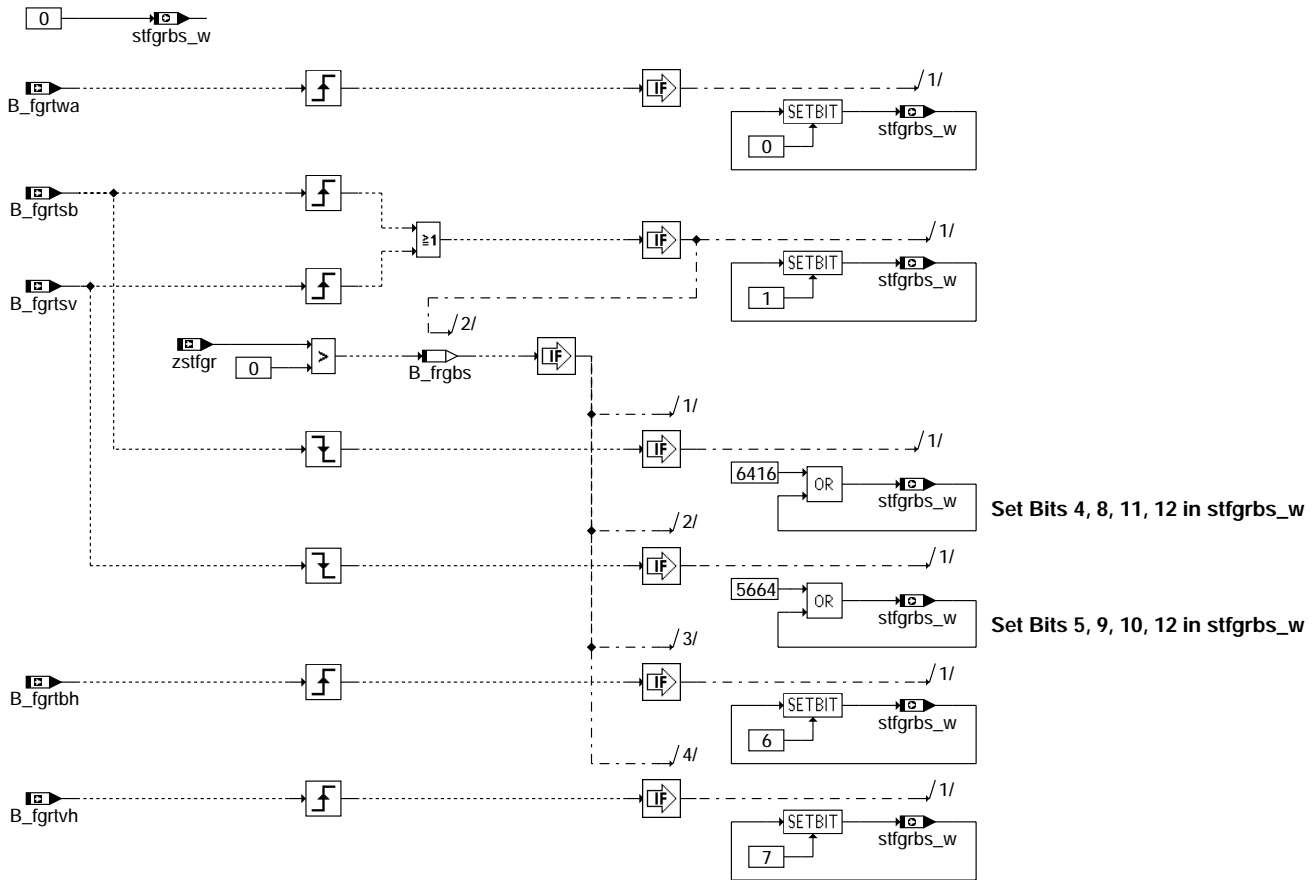
Approach:

Connecting the resistor in series to the heater, then do the same as description for KFRINH (only for phlsnh = 1 ).

FRINH = rin\_h.w with series-resistor / rin\_h.w without series-resistor.

## FGRBESI 2.10 Operating signals, vehicle-speed controller

### FDEF FGRBESI 2.10 Function definition



fgrbesi-fgrbesi

### ABK FGRBESI 2.10 Abbreviations

Variable	Source	Type	Description
B_FGRTBH	GGFGRH	EIN	Condition: FGR switch acceleration held (no Tip)
B_FGRTSB	GGFGRH	EIN	Condition: FGR switch set/accelerate
B_FGRTSV	GGFGRH	EIN	Condition: FGR switch set/decelerate
B_FGRTVH	GGFGRH	EIN	Condition: FGR switch decelerate held (no Tip)
B_FGRTWA	GGFGRH	EIN	condition: Cruise control button RESUME
B_FRGBS	FGRBESI	LOK	Condition: Enable operating signals vehicle-speed controller



Variable	Source	Type	Description
STFGRBS_W	FGRBESI	AUS	Status word operating signals, vehicle-speed controller
ZSTFGR	FGRFULO	EIN	Status of vehicle-speed controller

### FW FGRBESI 2.10 Fixed Values

Parameter	Value	Description
-----------	-------	-------------

### FB FGRBESI 2.10 Detailed description of function

The function evaluates the signals from the operating lever of the vehicle-speed controller (FGR) and converts these to the status word "FGR operating signals" stfgrbs.w. This then constitutes the interface for controlling the vehicle-speed controller states in the function %FGRFULO. Depending on the actual vehicle-speed controller state, certain activities are then triggered here by inquiring individual bits from stfgrbs.w. These are summarized in the following table:

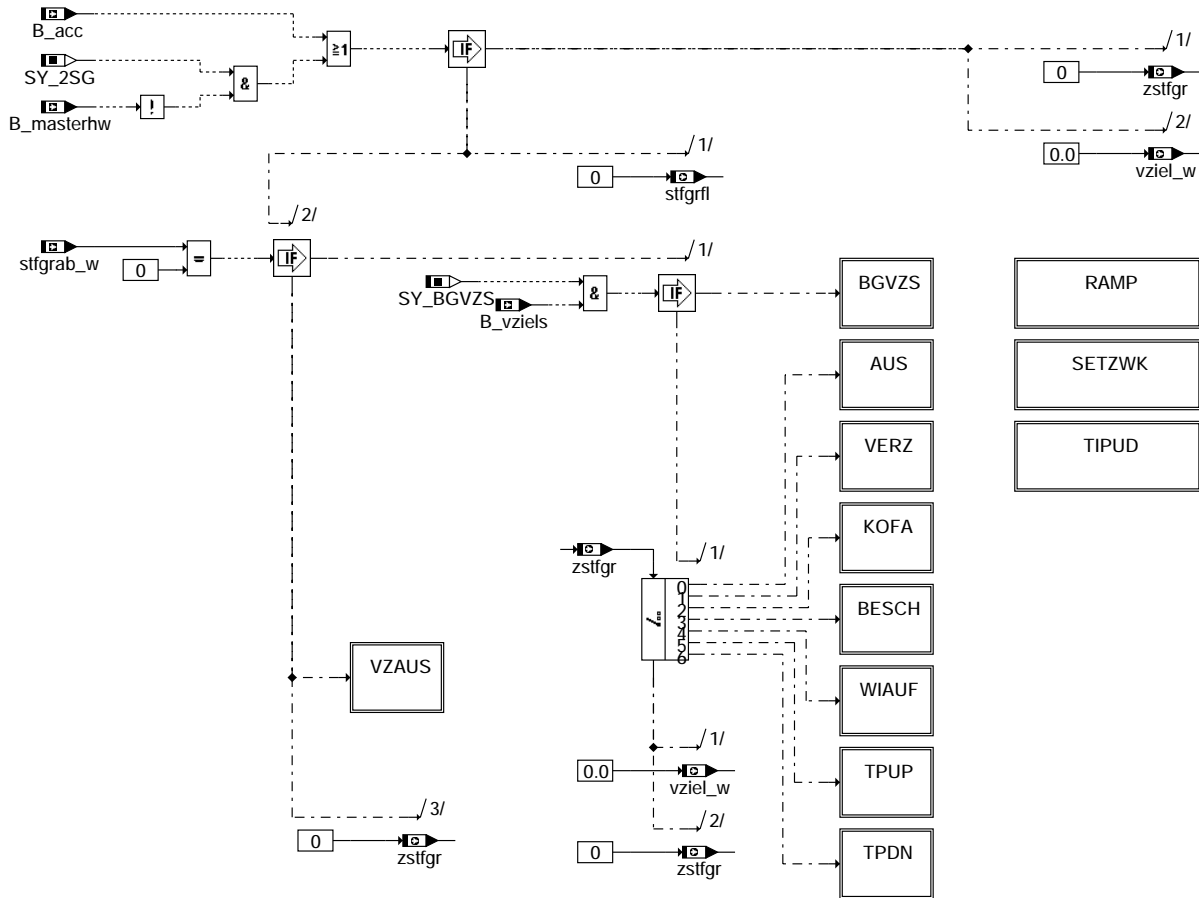
bit	Vehicle-speed controller state	Activity
0	Off	Switch-on with resumption
1	Off	Switch-on with setting
2	Off	Switch-on with acceleration
3	Off	Switch-on with deceleration
4	Constant driving	Tip-up
5	Constant driving	Tip-down
6	Constant driving, resumption, Tip-up, Tip-down	Acceleration off, control mode
7	Constant driving, resumption, Tip-up, Tip-down	Deceleration off, control mode
8	Accelerate	End acceleration
9	Decelerate	End deceleration
10	Tip-up	Set
11	Tip-down	Set
12	Constant driving, resumption	Set
13		
14	Not assigned	
15		

This variant is suitable for the vehicle-speed controller operating lever of the Fiat concern. This comprises three tip-type switches with the functions "Set/Accelerate", "Set/Decelerate" and "Resumption" as well as an indexed main switch that is evaluated as a vehicle-speed controller shutdown condition in the function %FGRABED.

## APP FGRBESI 2.10 Application hint

## FGRFULO 1.20 Function logic, vehicle-speed controller

### FDEF FGRFULO 1.20 Function definition

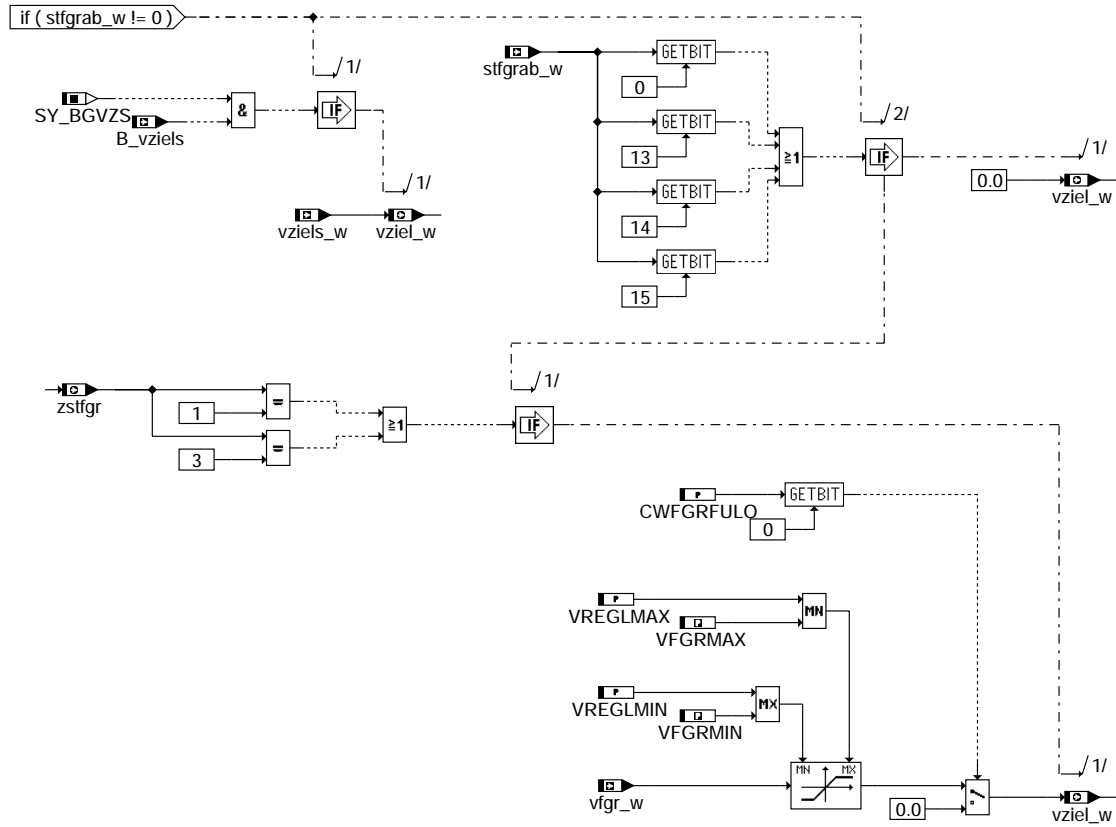


fgrfulo-fgrfulo

fgrfulo-fgrfulo



Sub-function VZAUS: Modifying the target speed for active shutdown conditions

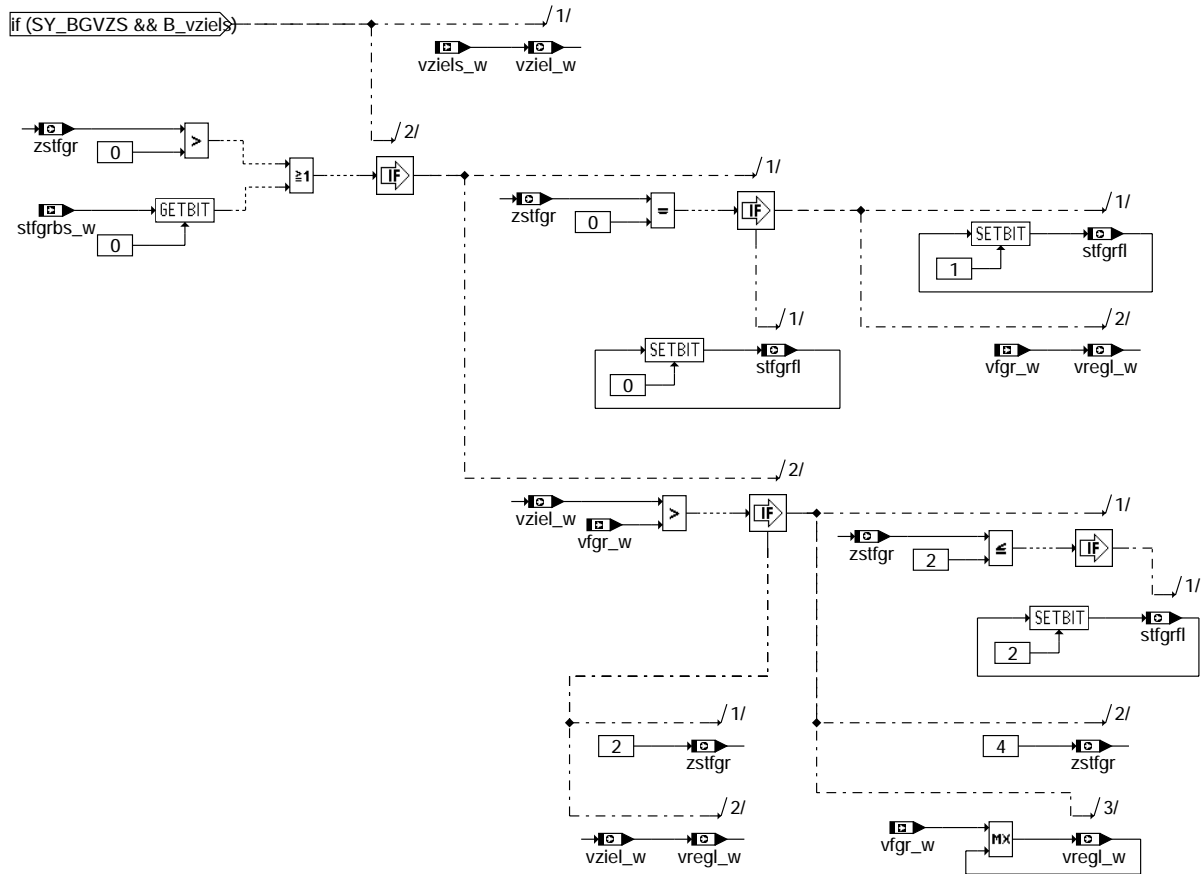


fgrfulo-vzaus

fgrfulo-vzaus



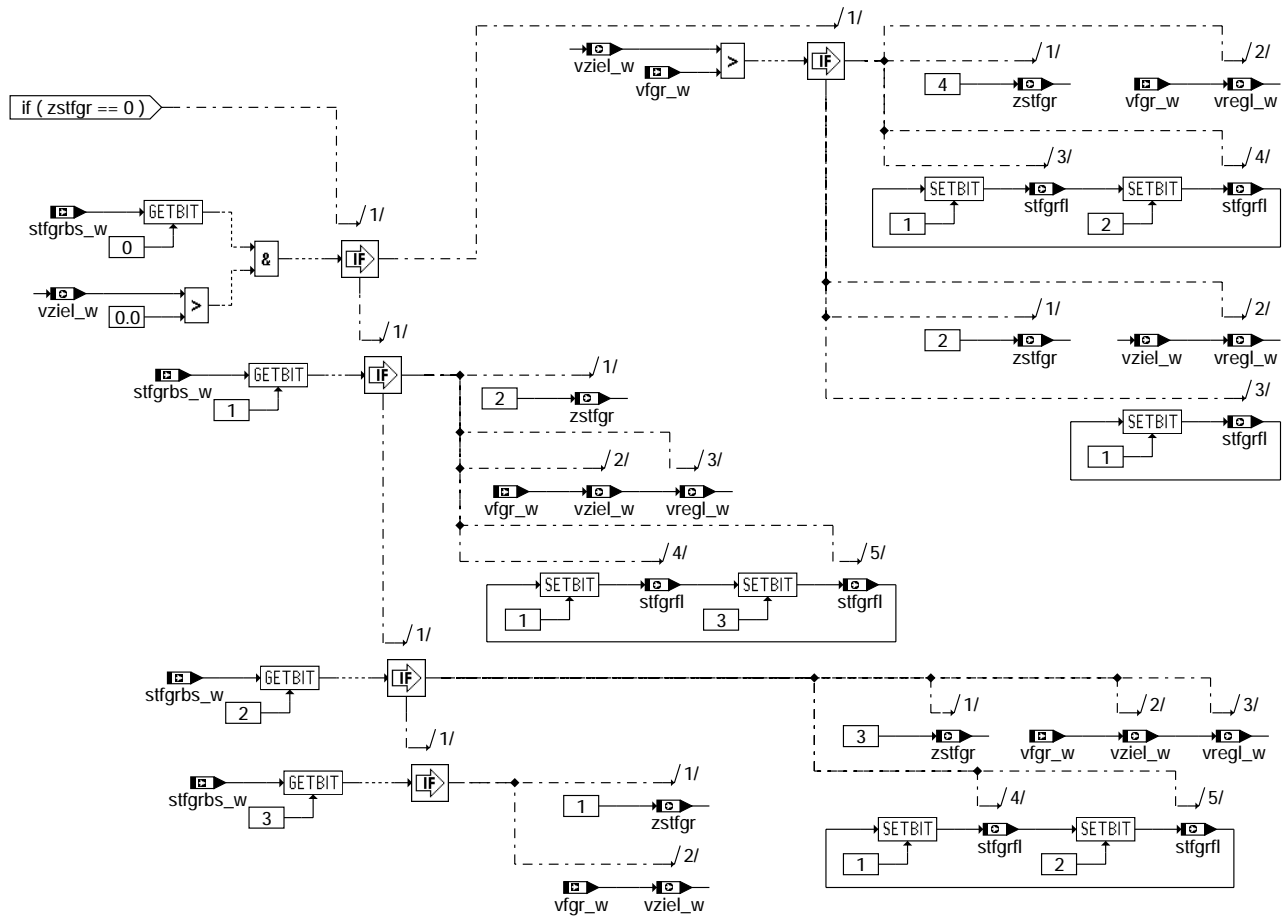
Sub-function BGVZS: Status transitions when transferring calculated set desired target speed



fgrfulo-bgvzs

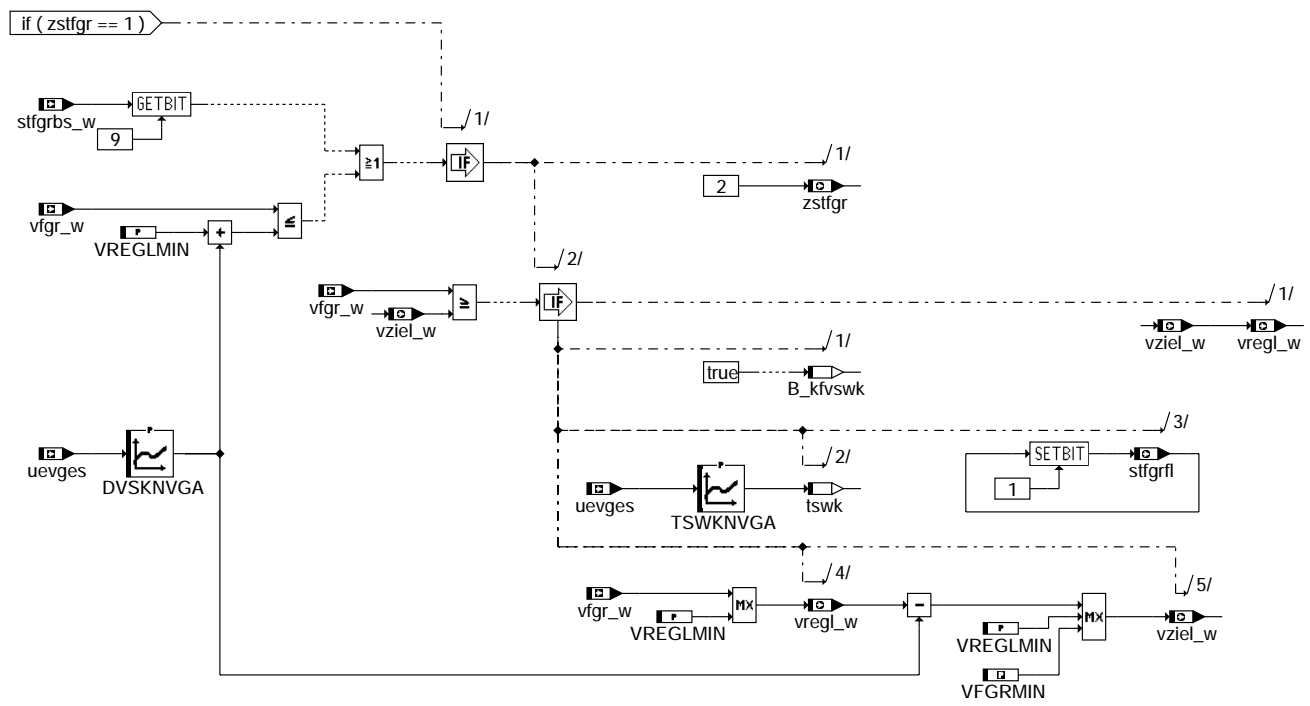
fgrfulo-bgvzs

Sub-function AUS: Transitions from the state "Off"



**fgrfulo-aus**

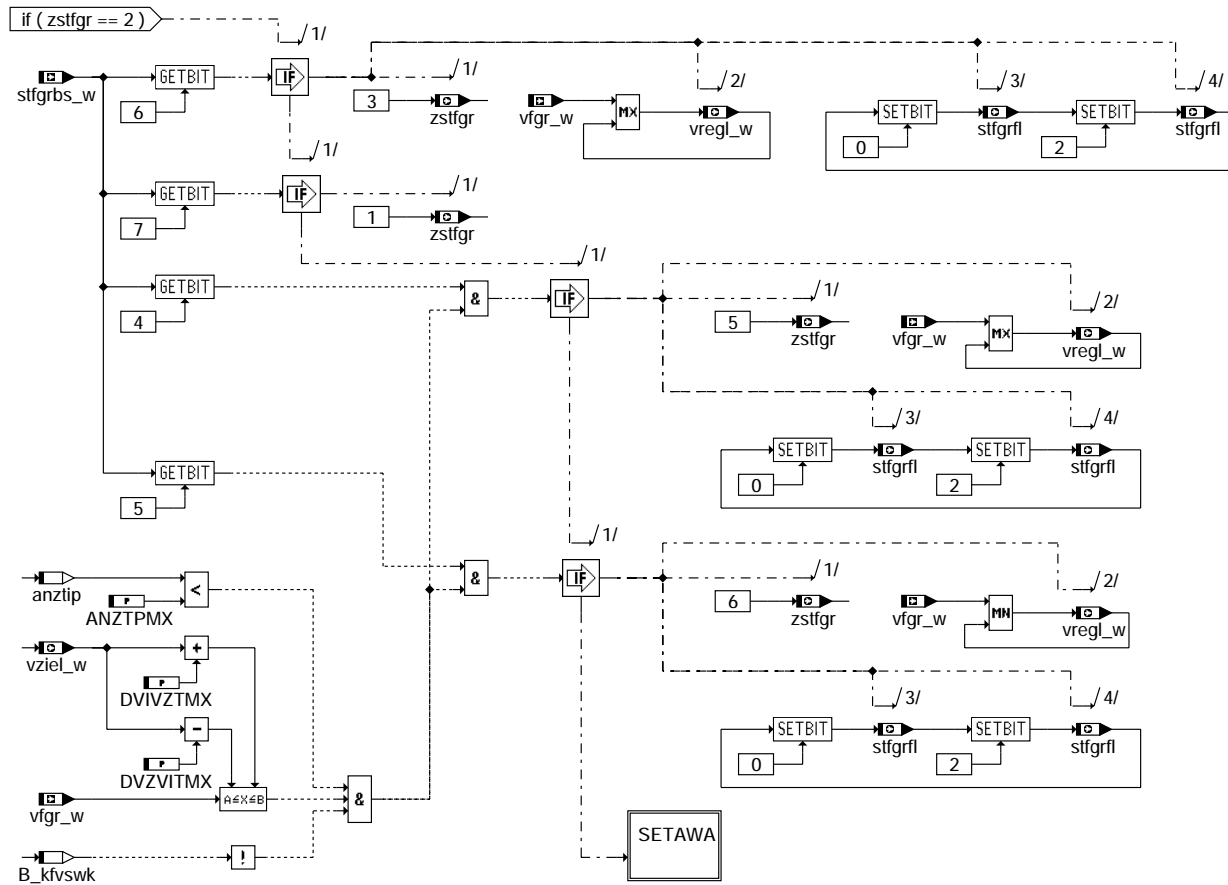
Sub-function VERZ: Transitions from the state "Decelerate"



**fgrfulo-verz**

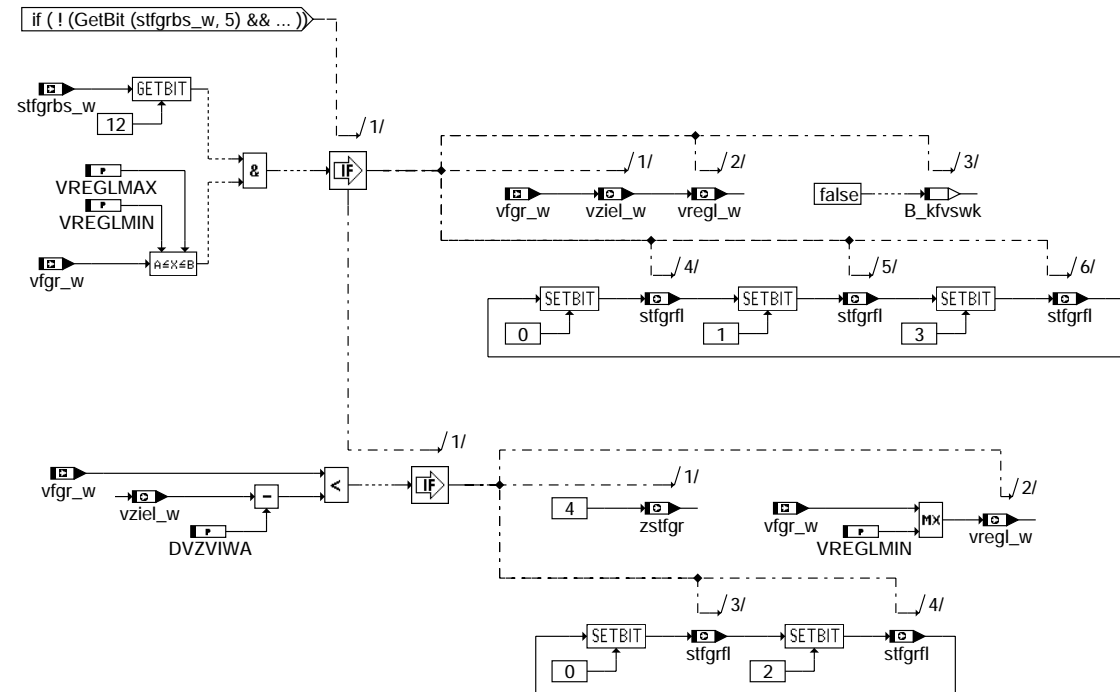


Sub-function KOFA: Transitions from the state "Constant driving"



### fgrfulo-kofa

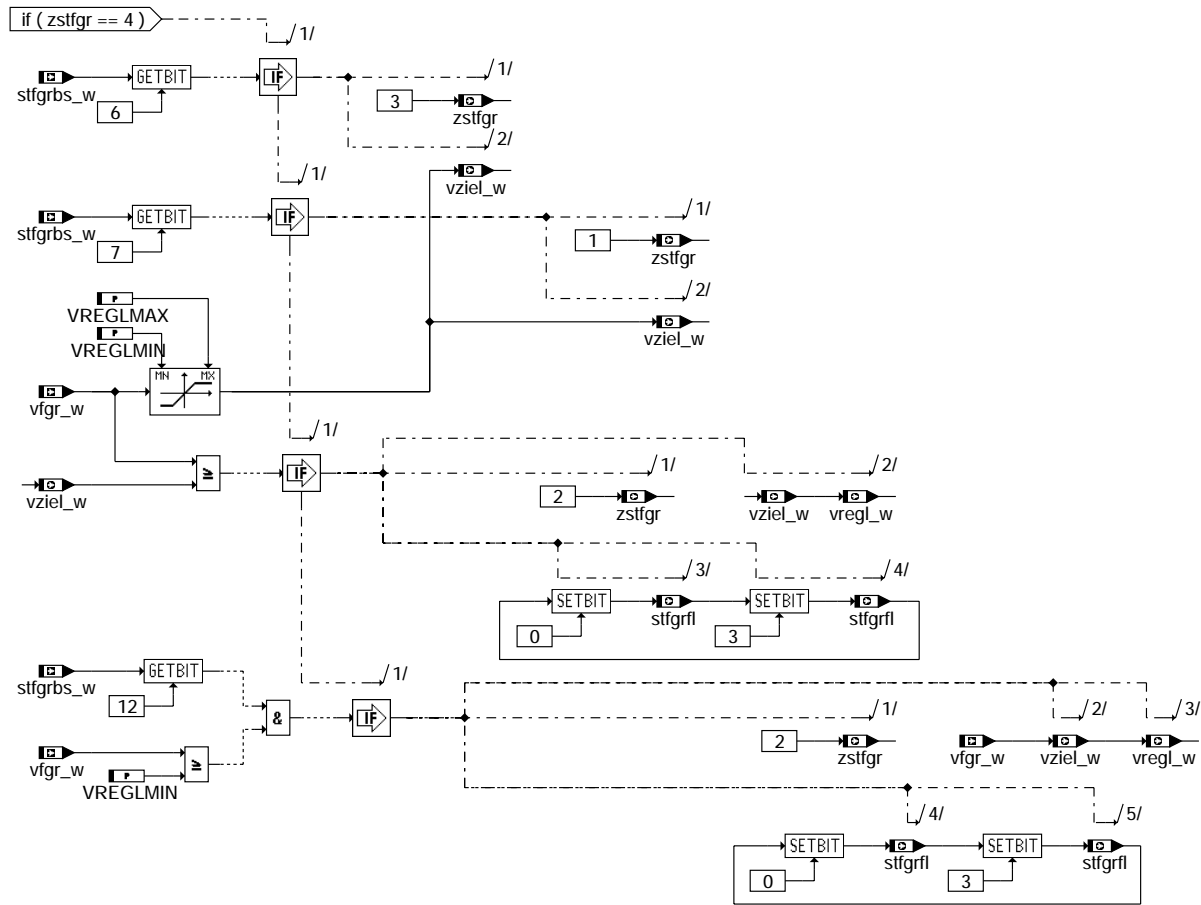
Sub-function SETAWA: Set and automatic resumption during constant driving



### fgrfulo-setawa



Sub-function WIAUF: Transitions from the state "Resumption"

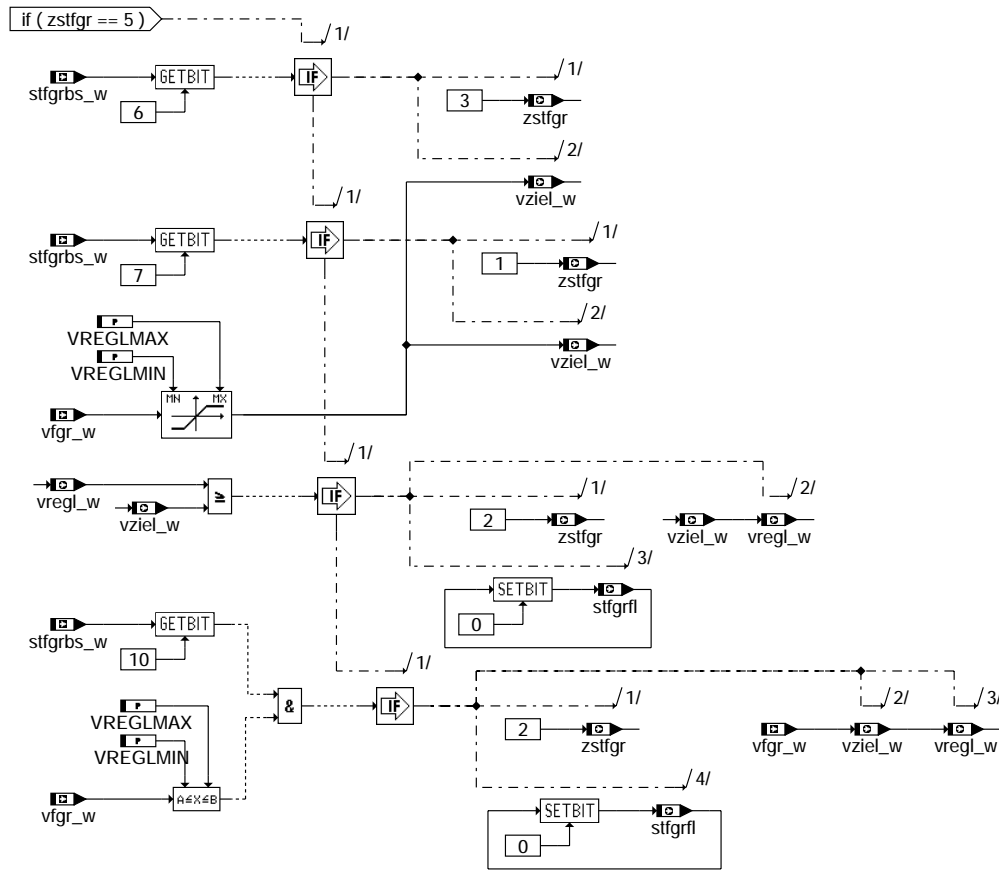


fgrfulo-wiauf

fgrfulo-wiauf



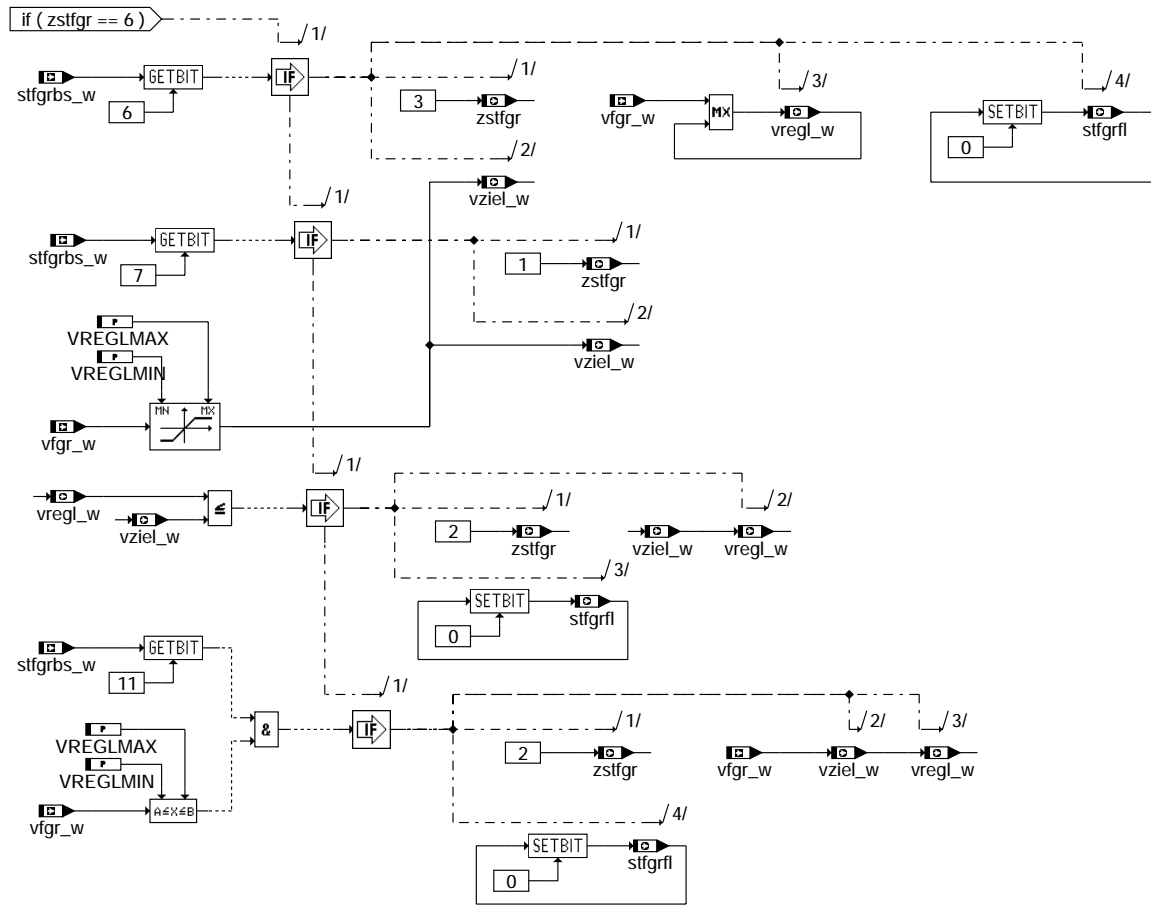
Sub-function TPUP: Transitions from the state "Tip-up"



fgfulo-tpup

fgfulo-tpup

Sub-function TPDN: Transitions from the state "Tip-down"

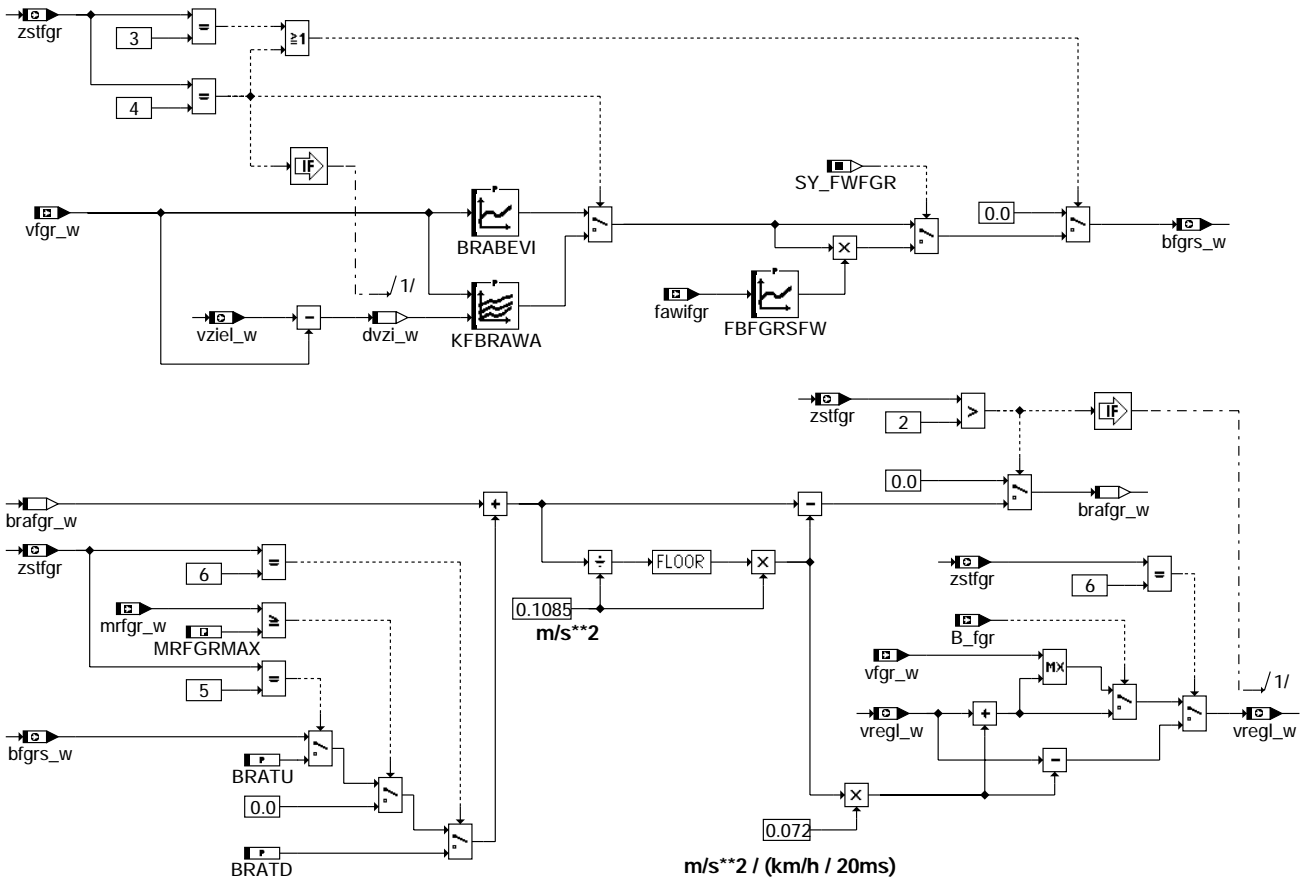


fgrfulo-tpdn

fgrfulo-tpdn



Sub-function RAMP: Target acceleration for ramps

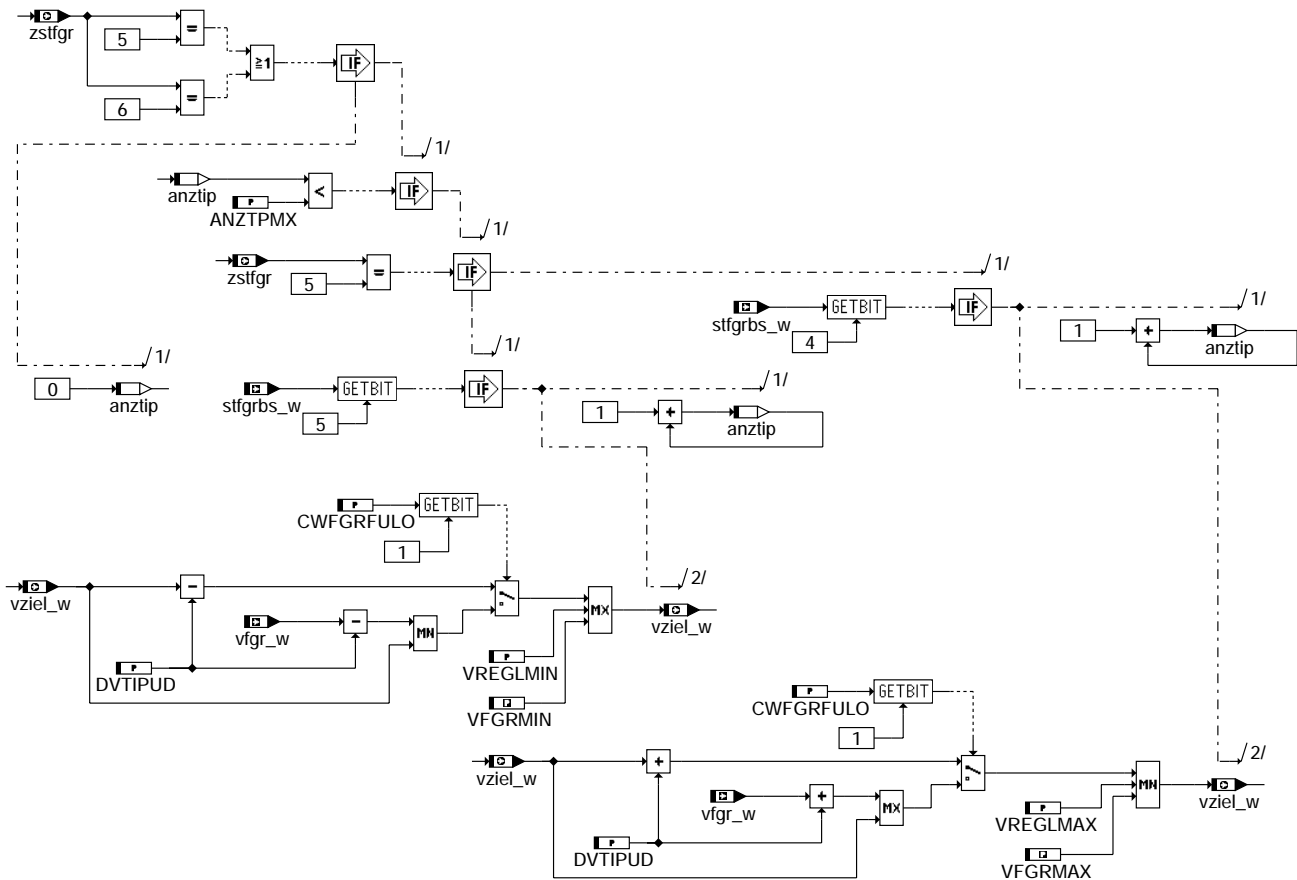


### fgfulo-ramp

Sub-function SETZWK: Set-value adjustment after acceleration and deceleration  
BILD /SYM SETZWK

TEXT/ANF

Sub-function TIPUD: Modifying the target speed for Tip-up and Tip-down



fgrfulo-tipud

### ABK FGRFULO 1.20 Abbreviations

Parameter	Source-X	Source-Y	Type	Description
ANZTPMX			FW	maximum number of tips (one after the other)
BRABEVI	VFGR_W		KL	acceleration at accelerating ramp
BRATD			FW	acceleration (amount) at tip-down ramp
BRATU			FW	acceleration at tip-up ramp
CWFGRFULO			FW	Code word FGRFULO
DVIVZTMX			FW	maximum delta between actual and target speed for tip permission
DVSKNBGA	UEVGES		KL	delta velocity for set value correction after acceleration
DVSKNVGA	UEVGES		KL	delta velocity for set value correction after deceleration
DVTIPUD			FW	changing actual speed at tip-up or tip-down
DVZVITMX			FW	maximum delta between target and actual speed for tip permission
DVZVIWA			FW	delta between target and actual speed for transition cruising to resuming
FBFGRSFW	FAWIFGR		KL	Correction factor for FGR target acceleration
KFBRAWA	VFGR_W	DVZI_W	KF	Target acceleration for resumption
MRFGRMAX			FW (REF)	maximum value for relative torque request from cruise control
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_BGVZS			SYS (REF)	
SY_FWFGR			SYS (REF)	
TSWKNBGA	UEVGES		KL	time to set value correction after acceleration finished
TSWKNVGA	UEVGES		KL	time to set value correction after deceleration finished
VFGRMAX			FW (REF)	max. permitted velocity during active cruise control
VFGRMIN			FW (REF)	Minimum permissible speed during FGR-operation
VREGLMAX			FW	max. permitted desired speed for cruise control
VREGLMIN			FW	min. permitted desired speed for cruise control

Variable	Source	Type	Description
ANZTIP	FGRFULO	LOK	Number of consecutive successful Tip-Up's or Tip-Down's
BFGRS_W	FGRFULO	AUS	FGR target acceleration
BRAFGR_W	FGRFULO	LOK	Ramp acceleration FGR
B_ACC		EIN	Condition: ACC-control unit exists
B_FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control
B_KFVSWK	FGRFULO	LOK	Condition: Constant driving before set-value correction
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)
B_VZIELS		EIN	Condition: Transfer calculated target speed
CTSWK	FGRFULO	LOK	Time counter for set value correction
DVZI_W	FGRFULO	LOK	Difference between target and actual speed
FAWIFGR		EIN	Driving resistance for FGR



Variable	Source	Type	Description
MRFGR_W	MSF	EIN	relative torque demand from cruise control
STFGRAB_W	FGRABED	EIN	Status word, cut-out conditions, vehicle-speed controller
STFGRBS_W	FGRBESI	EIN	Status word operating signals, vehicle-speed controller
STFGRFL	FGRFULO	AUS	Status byte FGR function logic
TSWK	FGRFULO	LOK	Time for set-value correction
UEVGES	BBGANG	EIN	Transmission ratio total
VFGR_W	GGVFZG	EIN	cruise control vehicle speed
VREGL_W	FGRFULO	AUS	desired speed for cruise control
VZIELS_W		EIN	Calculated nominal target for FGR
VZIEL_W	FGRFULO	AUS	target velocity cruise control
ZSTFGR	FGRFULO	AUS	Status of vehicle-speed controller

### FW FGRFULO 1.20 Fixed Values

Parameter	Value	Description
ANZTPMX		maximum number of tips (one after the other)
BRATD		acceleration (amount) at tip-down ramp
BRATU		acceleration at tip-up ramp
CWFGRFULO		Code word FGRFULO
DVIVZTMX		maximum delta between actual and target speed for tip permission
DVTIPUD		changing actual speed at tip-up or tip-down
DVZVITMX		maximum delta between target and actual speed for tip permission
DVZVIWA		delta between target and actual speed for transition cruising to resuming
VREGLMAX		max. permitted desired speed for cruise control
VREGLMIN		min. permitted desired speed for cruise control

### FB FGRFULO 1.20 Detailed description of function

The function controls the states of the vehicle-speed controller (FGR) depending on the operating signals (stfgrbs\_w from %FGRBESI) and the shutdown conditions (stfgrab\_w from %FGRABED). The meaning of the vehicle-speed controller state, zstfgr, is given in the following table:

```

+=====+
| zstfgr | FGR state |
+=====+
| 0      | Off       |
+-----+
| 1      | Decelerate |
+-----+
| 2      | Constant driving|
+-----+
| 3      | Accelerate |
+-----+
| 4      | Resumption |
+-----+
| 5      | Tip-up    |
+-----+
| 6      | Tip-down  |
+-----+
| 7-255 | Not assigned |
+-----+
    
```

The target speed vziel\_w and desired speed, vregl\_w, for the controller, as well as the status byte "FGR function logic", stfgrfl, are also made available. Certain activities are triggered by inquiring specific bits in stfgrfl in %FGRREGL. These activities are summarized in the following table:

```

+=====+
| bit | Activity |
+=====+
| 0   | Initialization of the stored control difference from the last computing step |
+-----+
| 1   | Initialization of the stored controller output from the last computing step |
+-----+
| 2   | Initialization of the offset speed voffs_w during ramp start |
+-----+
| 3   | Initialization of the load-dependent offset speed vlast_w |
+-----+
| 4   | Limitation of the controller output during transition from the state |
|     | "Accelerate" to "Constant driving" |
+-----+
| 5-7 | Not assigned |
+-----+
    
```

The vehicle-speed controller state is set to "Off" and the target speed cancelled in an ACC system (externally realized vehicle-speed controller with vehicle-to-vehicle ranging) or in the slave of a system where there are two ME ECU's. Otherwise the shutdown conditions are first checked. The vehicle-speed controller state is set to "Off" if a shutdown condition is fulfilled. The target speed is cancelled as well depending on the type of shutdown condition. Aborting the states "Accelerate" or "Decelerate" causes the actual speed to be taken as the new target speed. The target speed can also be canceled as an alternative in this case.

If none of the shutdown conditions is fulfilled, then different conditions are checked depending on the vehicle-speed controller

state. This can lead to a change in the vehicle-speed controller state as well to a modification of the desired or target speed.

o Off

The vehicle-speed controller only then cuts in when the actual speed, `vgr_w`, lies within the range between `VFGREMIN` and `VFGREMAX`.

o Resumption to the stored target speed:

The target speed is approached again if bit 0 in `stfgrbs_w` is set and there is a stored target speed available (`vziel_w` greater than 0). If the actual speed is less than the target speed, then the vehicle-speed controller state is set to "Resumption" and the nominal-speed ramps is started commencing at the actual speed. On the other hand, if the actual speed is greater than the target speed, then the vehicle-speed controller state is set to "Constant driving" and the desired speed set to the target speed.

o Taking the current actual speed as the target speed:

If bit 1 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Constant driving" and actual speed is taken as the target and as the desired speed.

o Accelerate from non-controlled driving:

If bit 2 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Accelerate" and the desired-speed ramp started commencing at the actual speed.

o Decelerate from non-controlled driving:

If bit 3 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Decelerate". The controller is however only activated after deceleration has finished (when the decelerate button has been released).

o Decelerate

o End of deceleration:

If bit 9 in `stfgrbs_w` is set or the actual speed reached the lower limit of the range permitted for the desired speed, then deceleration is terminated and the vehicle-speed controller state is set to "Constant driving". If the actual speed has fallen compared to the stored target speed, then this is taken as the new desired speed. The target speed is set to just below the actual speed is set so as to make the transition to stabilization more comfortable. The target speed is then set to the target speed (set-value adjustment) following elapse of defined period of time. Refer to the sub-function `SETZWK`.

o Constant driving

o Accelerate:

If bit 6 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Accelerate". The desired speed ramp then starts commencing at the maximum of the target and actual speed.

o Decelerate:

If bit 7 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Decelerate". The controller remains deactivated until deceleration has finished and the vehicle is decelerated by the drag torque from the engine.

o Tip-up:

If bit 4 in `stfgrbs_w` is set and the actual speed lies within a certain range about the target speed, then the vehicle-speed controller state is set to "Tip-up" is set. The desired-speed ramp is started commencing from the maximum of the target and actual speed. The target speed is increased by a small value in jumps (refer to sub-function `TIPUD`).

o Tip-down:

If bit 5 in `stfgrbs_w` is set and the actual speed lies within a certain range about the target speed, then the vehicle-speed controller state is set to "Tip-down". The desired-speed ramp is started commencing from the minimum of the target and actual speed. The target speed is decreased by a small amounts in jumps (refer to sub-function `TIPUD`).

o Set:

If bit 12 in `stfgrbs_w` is set and the actual speed lies within a range permissible for the desired speed, then the actual speed is taken as the target and as the desired speed.

o Automatic resumption:

If the actual speed falls below the target speed by a certain amount, then the vehicle-speed controller state is set to "Resumption" and the desired-speed ramp is started commencing from the actual speed. Uncontrolled acceleration by the vehicle is prevented in this way.

o Accelerate

o End of acceleration:

If bit 8 in `stfgrbs_w` is set or the actual speed reaches the upper limit permitted for the desired speed, then acceleration is terminated and the vehicle-speed controller state is set to "Constant driving". If the actual speed has increased compared to the stored target speed, then this is taken as the new desired speed. The target speed is set to just above the actual speed is set so as to make reaching stabilization comfortable. The target speed is then set to the target speed (set-value adjustment) following elapse of defined period of time. Refer to the sub-function `SETZWK`.

o Resumption

o Accelerate:

If bit 6 in `stfgrbs_w` is set, then the vehicle-speed controller state is set to "Accelerate". The desired-speed ramp continues to run.

o Decelerate:

If bit 7 in stfgrbs\_w is set, then the vehicle-speed controller state is set to "Decelerate". The controller remains deactivated until deceleration has finished and the vehicle is decelerated by the engine's drag torque.

- o Reaching the target speed:  
If the actual speed reaches the target speed, then the vehicle-speed controller state is set to "Constant driving" and the desired speed is set to the target speed.
- o Set:  
If bit 12 in stfgrbs\_w is set and the actual speed lies within a range permitted for the desired speed then the vehicle-speed controller state is set to "Constant driving" and the actual speed is taken as the target and as the desired speed.
- o Tip-up
  - o Accelerate:  
If bit 6 in stfgrbs\_w is set, then the vehicle-speed controller state is set to "Accelerate". The desired-speed ramp continues to run.
  - o Decelerate:  
If bit 7 in stfgrbs\_w is set, then the vehicle-speed controller state is set to "Decelerate" is set. The controller remains deactivated until deceleration has finished and the vehicle is decelerated by the engine's drag torque.
  - o Reaching the target speed:  
If the actual speed reaches the target speed, then the vehicle-speed controller state is set to "Constant driving" and the desired speed is set to the target speed.
  - o Set:  
If bit 10 in stfgrbs\_w is set and the actual speed lies within a range permitted for the desired speed then the vehicle-speed controller state is set to "Constant driving" and the actual speed is taken as the target and as the desired speed.
- o Tip-down
  - o Accelerate:  
If bit 6 in stfgrbs\_w is set, then the vehicle-speed controller state is set to "Accelerate". the desired-speed ramp runs upwards commencing at the actual speed.
  - o Decelerate:  
If bit 7 in stfgrbs\_w is set, then the vehicle-speed controller state is set to "Decelerate". The controller remains deactivated until deceleration has finished and the vehicle is decelerated by the engine's drag torque.
  - o Reaching the target speed:  
If the actual speed reaches the target speed, then the vehicle-speed controller state is set to "Constant driving" and the desired speed is set to the target speed.
  - o Set:  
If bit 11 in stfgrbs\_w is set and the actual speed lies within a range permitted for the desired speed then the vehicle-speed controller state is set to "Constant driving" and the actual speed is taken as the target and as the desired speed.

In the states "Accelerate", "Resumption", "Tip-up" and "Tip-down", the desired speed vregl\_w is modified depending on the applied target-acceleration values. When the states "Accelerate" and "Decelerate" has finished, the desired speed vregl\_w is set to the target speed vziel\_w after elapse of a certain time. The target speed is increased or decreased further in the states "Tip-up" and "Tip-down" if the appropriate operating signals are given (bit 4 or bit 5 in stfgrbs\_w) and the maximum number of successive permissible tip-routines has not yet been exceeded.

### APP FGRFULO 1.20 Application hint

CWFGRFULO:

Bit 0

0: vziel\_w = vfgr\_w for shutdown condition during acceleration or deceleration 1: vziel\_w = 0 for shutdown condition during acceleration or deceleration

Bit 1

0: Set Tip-up and Tip-down to target speed up  
1: Set Tip-up and Tip-down Set to actual speed up

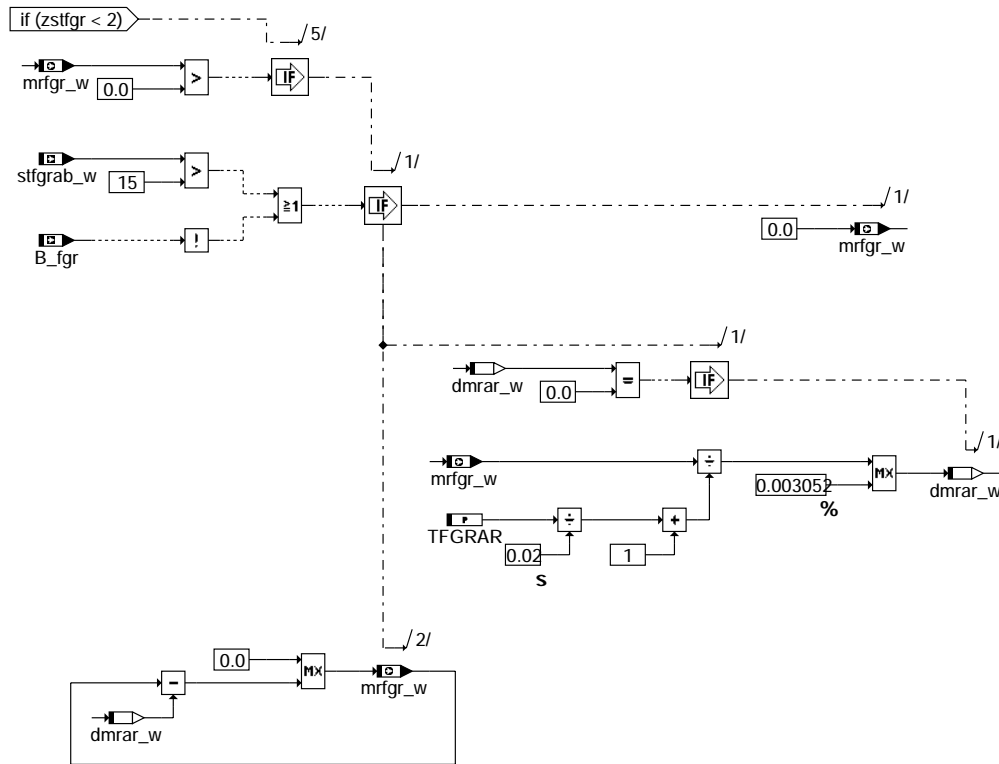
It must apply that:

VFGREMIN >= Max (VREGLMIN, VFGRMIN)

VFGREMAX <= VREGLMAX

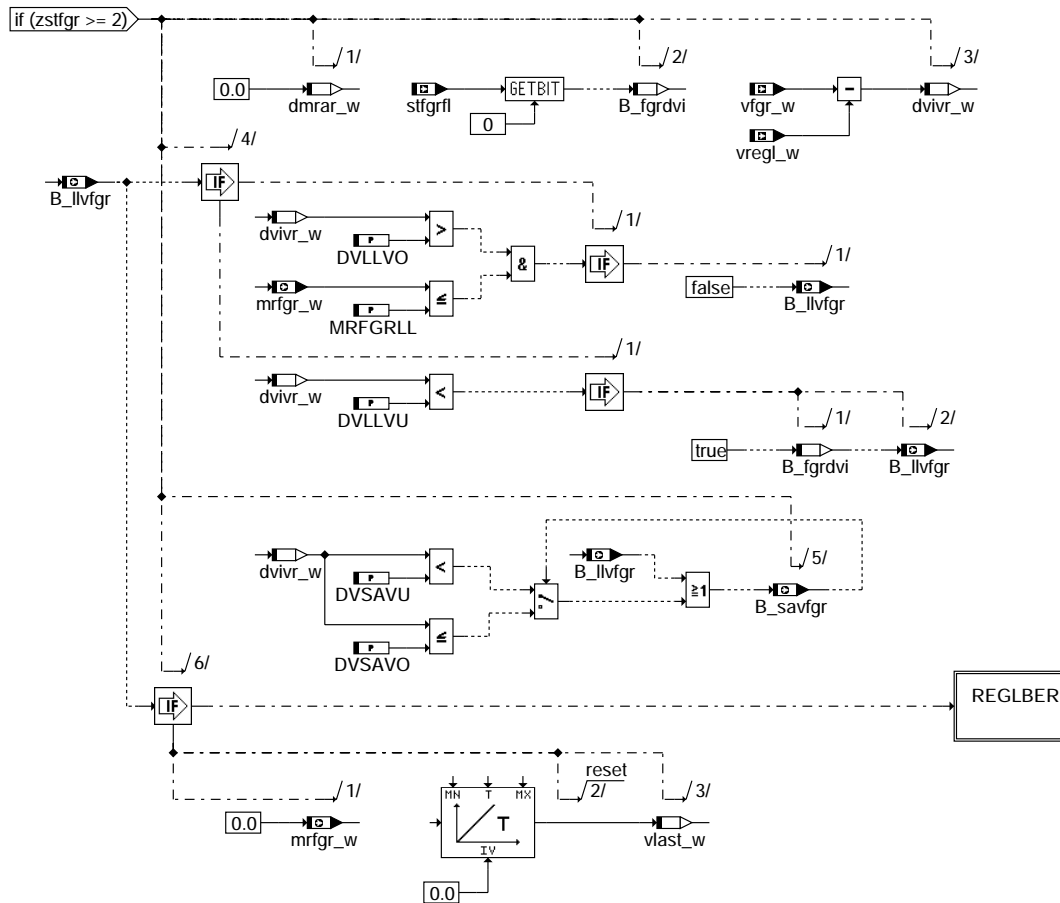


Sub-function ARAMP: Shutdown ramp for comfortable shutdown



### fgrrgl-aramp

Sub-function REGLAKT: Control active

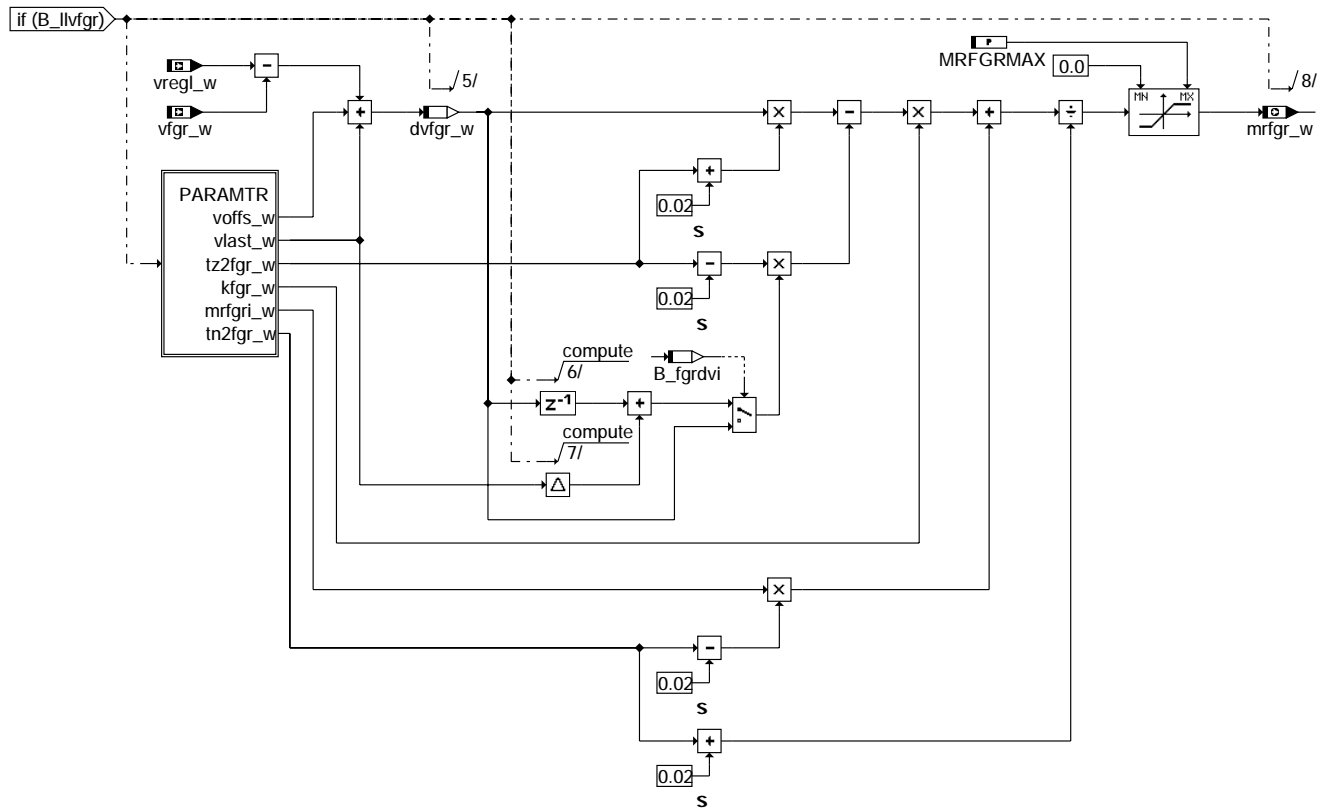


### fgrrgl-reglakt

fgrrgl-aramp

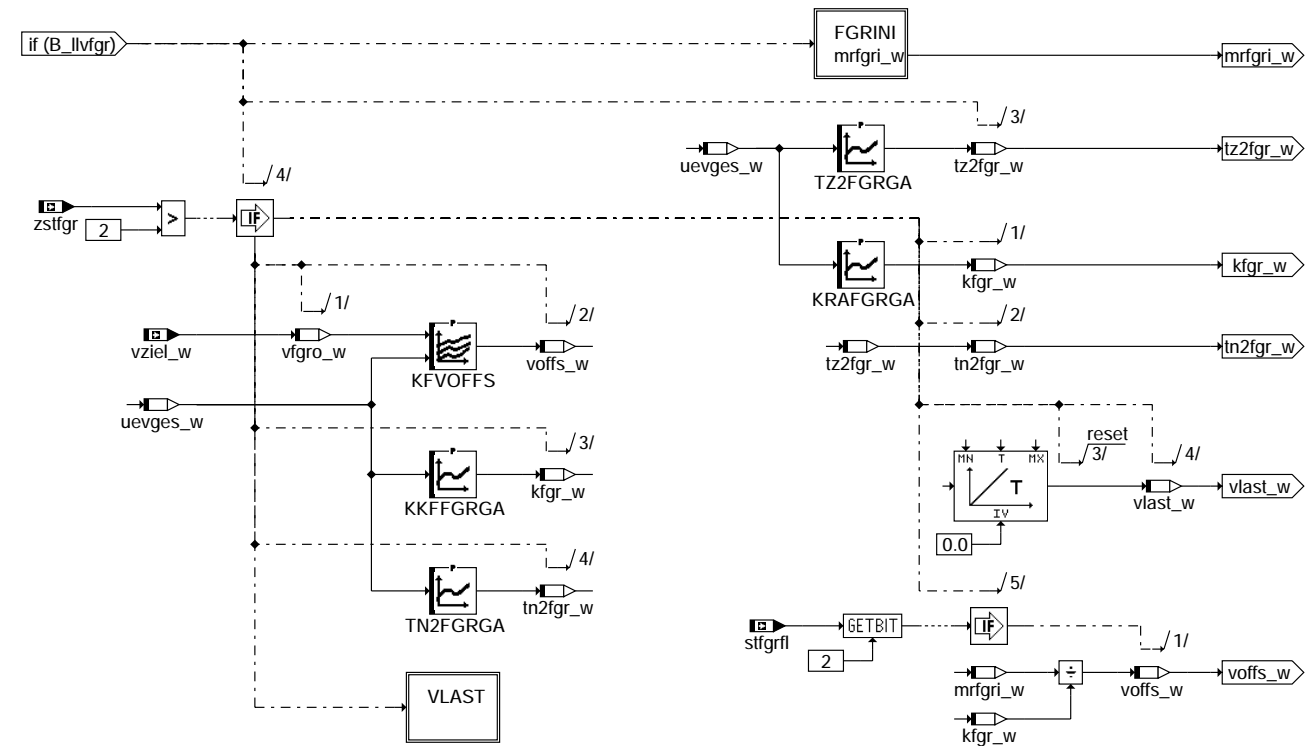
fgrrgl-reglakt

Sub-function REGLBER: Controller calculation with recursion formula



### fgrregl-reglber

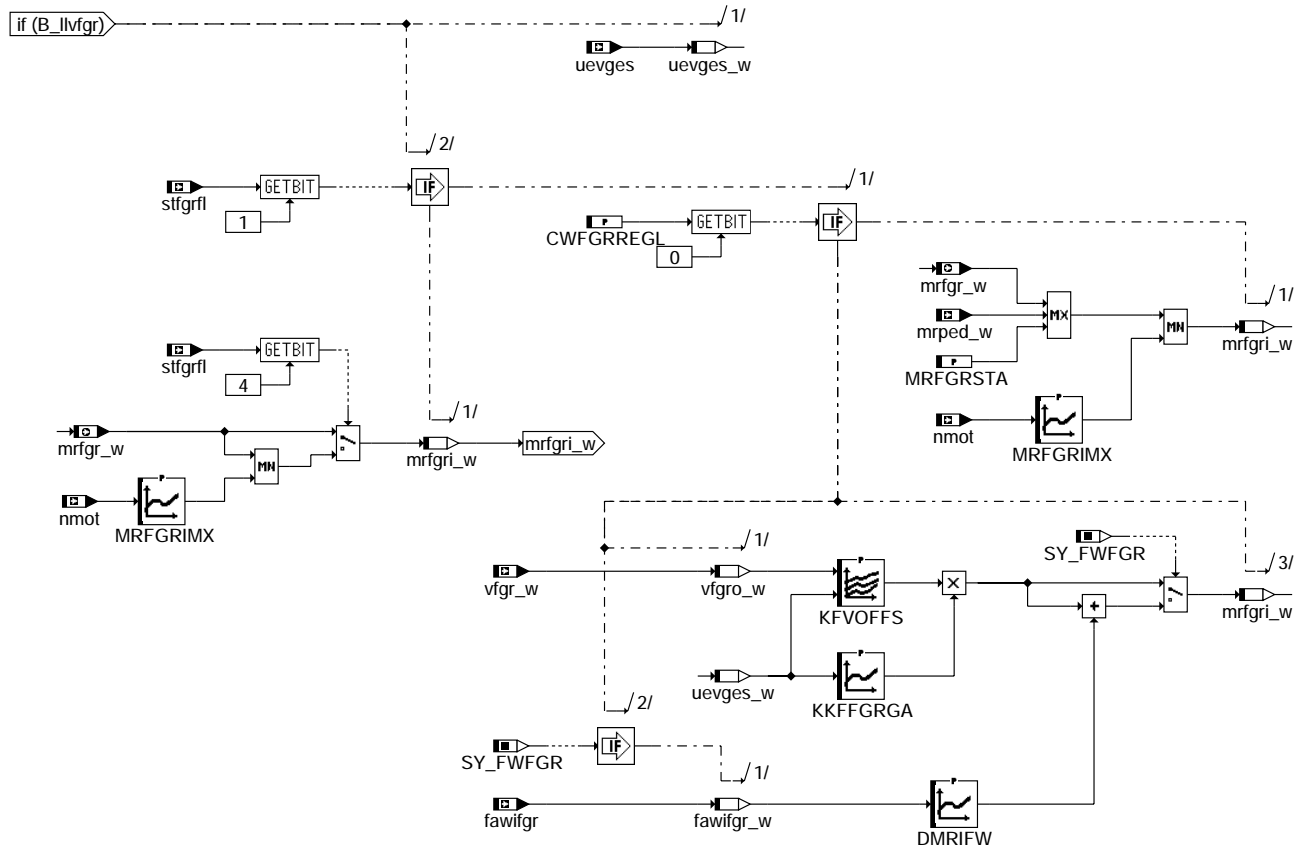
Sub-function PARAMTR: Controller parameters



### fgrregl-paramtr



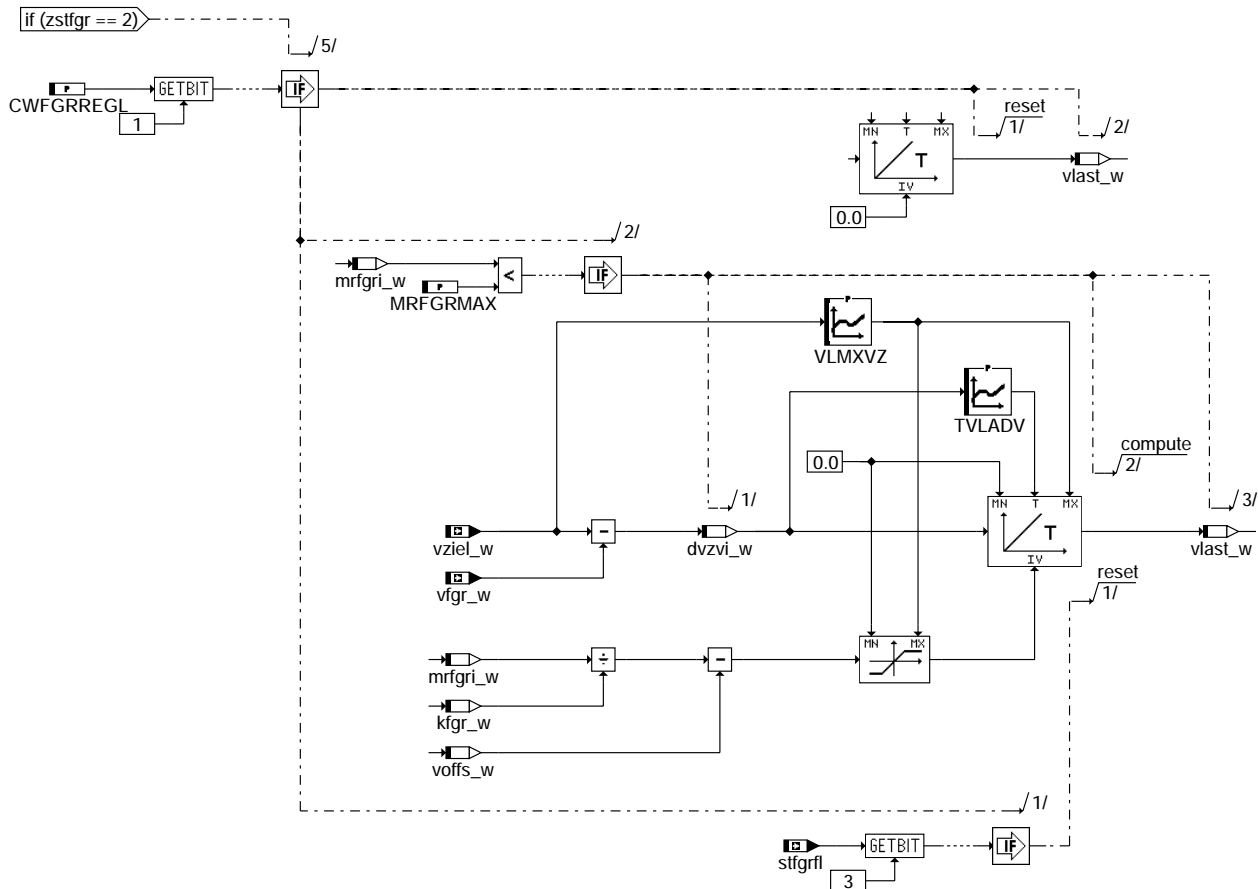
Sub-function FGRINI: Controller initialization



fgrregl-fgrini

fgrregl-fgrini

Sub-function VLAST: Load-dependent offset rate



**fgrregl-vlast**

**ABK FGRREGL 1.10 Abbreviations**

Parameter	Source-X	Source-Y	Type	Description
CWFRREGL			FW	Code word FGRREGL
DMRIFW	FAWIFGR_W		KL	Delta relative torque for FGR initialization
DVLLVO			FW	Delta speed to reset idle-speed disable from the FGR
DVLLVU			FW	Delta speed to set idle-speed disable from the FGR
DVSAVO			FW	delta velocity to set prohibited trailing throttle fuel cutoff
DVSAVU			FW	delta velocity to remove prohibited trailing throttle fuel cutoff
KFVOFFS	VFGRO_W	UEVGES_W	KF	velocity offset for cruise control
KKFFGRGA	UEVGES_W		KL	amplification rate during cruising for cruise control
KRAFGRGA	UEVGES_W		KL	amplification rate at ramp for cruise control
MRFGRIMX	NMOT		KL	Maximum FGR initialization value
MRFGRLL			FW	Relative-torque threshold from FGR for idle-speed detection
MRFGRMAX			FW	maximum value for relative torque request from cruise control
MRFGRSTA			FW	starting value for relativ torque at active cruise control
SY_2SG			SYS (REF)	system constant 2 motronic systems
SY_FWFGFR			SYS (REF)	
TFGRAR			FW	Ramp running time comfort shutdown of the FGR
TN2FGRGA	UEVGES_W		KL	double denominator time constant for cruise control
TVLADV	DVZVI_W		KL	Integrator time constant at vlast-calculation
TZ2FGRGA	UEVGES_W		KL	double numerator time constant for cruise control
VLMXVZ	VZIEL_W		KL	Max. value for vlast_w
Variable	Source	Type	Description	
B_ACC		EIN	Condition: ACC-control unit exists	
B_FGR	MDFAW	EIN	condition: driver's set engine torque determined by cruise control	
B_FGRAB	FGRREGL	AUS	CC/ACC shut-off from the function	
B_FGRDVI	FGRREGL	LOK	condition: CC initialization of the saved system deviation	
B_FGREN	FGRREGL	AUS	condition: cruise control is active (enable)	
B_LLVFGR	FGRREGL	AUS	Condition: Idling disabled by FGR	
B_LLVFGRGRC		EIN	CAN-Signal: Idling disabled by FGR	
B_MASTERHW		EIN	Condition Master-SG corresponding with code-pin (plausible)	
B_SAVACC		EIN	Condition: overrun fuel cut-off forbidden by ACC	
B_SAVFGR	FGRREGL	AUS	Condition: prohibited trailing throttle fuel cut-off by cruise control	
B_SAVFGRC		EIN	CAN-signal: prohibited trailing throttle fuel cut-off by cruise control	
CTFGRAB	FGRREGL	LOK	Time counter to transfer the FGR cut-out to function monitoring	
DMRAR_W	FGRREGL	LOK	relative delta torque at cruise control deactivation ramp	



Variable	Source	Type	Description
DVFGR_W	FGRREGL	LOK	Control deviation of the FGR
DVIVR_W	FGRREGL	LOK	Difference between actual and set speed for FGR
DVZVI_W	FGRREGL	LOK	Difference between target- and actual velocity
FAWIFGR		EIN	Driving resistance for FGR
FAWIFGR_W	FGRREGL	LOK	Driving resistance for FGR
KFGR_W	FGRREGL	LOK	Amplification factor FGR-controller
MRACC_W		EIN	Relative torque request by ACC
MRFGR_W		EIN	CAN-signal: relative torque request from cruise control
MRFGR_W	FGRREGL	LOK	Relative torque initialization value for FGR-controller
MRFGR_W	FGRREGL	AUS	relative torque demand from cruise control
MRPED_W		EIN	Relative torque request by accelerator pedal
NMOT	SWADAP	EIN	engine speed
STFGRAB_W	FGRABED	EIN	Status word, cut-out conditions, vehicle-speed controller
STFGRFL	FGRFULO	EIN	Status byte FGR function logic
TN2FGR_W	FGRREGL	LOK	double denominator time constant cruise control
TZ2FGR_W	FGRREGL	LOK	double numerator time constant cruise control
UEVGES	BBGANG	EIN	Transmission ratio total
UEVGES_W	FGRREGL	LOK	Total transmission ratio
VFGRO_W	FGRREGL	LOK	Rate for addressing KFVOFFS
VFGR_W	GGVFZG	EIN	cruise control vehicle speed
VLAST_W	FGRREGL	LOK	Additional offset of the velocity for FGR-controller at higher load
VOFFS_W	FGRREGL	LOK	offset velocity for cruise control
VREGL_W	FGRFULO	EIN	desired speed for cruise control
VZIEL_W	FGRFULO	EIN	target velocity cruise control
ZSTFGR	FGRFULO	EIN	Status of vehicle-speed controller

### FW FGRREGL 1.10 Fixed Values

Parameter	Value	Description
CWFGREGL		Code word FGRREGL
DVLLVO		Delta speed to reset idle-speed disable from the FGR
DVLLVU		Delta speed to set idle-speed disable from the FGR
DVSAVO		delta velocity to set prohibited trailing throttle fuel cutoff
DVSAVU		delta velocity to remove prohibited trailing throttle fuel cutoff
MRFGRL		Relative-torque threshold from FGR for idle-speed detection
MRFGRMX		maximum value for relative torque request from cruise control
MRFGRSTA		starting value for relative torque at active cruise control
TFGRAR		Ramp running time comfort shutdown of the FGR

### FB FGRREGL 1.10 Detailed description of function

The function calculates the relative torque demand, `mrfg_r_w`, of the vehicle-speed controller (FGR) as a function of the target speed and the actual speed. A PDT1 controller is used to do this. This controller has the following transfer function:

$$G(s) = K \frac{1 + T s}{Z} \frac{1 + T s}{N}$$

The following recursion formula is given for discrete realization:

$$y(i) = \frac{1}{2T + dT} \left[ K \left( \frac{1}{Z} (2T + dT) x(i) - \frac{1}{Z} (2T - dT) x(i-1) \right) + \frac{1}{N} (2T - dT) y(i-1) \right]$$

- x: Control deviation (delta speed)
- y: Controller output (relative torque)
- dT: Sampling time (20 ms)
- i: Computing step

Only the vehicle-speed controller in the master runs in a system where there are two ME ECU's. The relative torque demand, `mrfg_r_w`, is set in the slave to the value `mrfgrc_w` received from the master via CAN. In the case of an ACC system (externally realized vehicle-speed controller with vehicle-to-vehicle ranging), `mrfg_r_w` is set to the value `mracc_w` demanded by the ACC control unit.

The controller is not active in the FGR states "Off" and "Decelerate". As long as the controller is intervening and there is no demand for a quick shutdown, then for comfort reasons, the relative torque demand is controlled to zero over a ramp with an applicable running time.

By the conditions idle speed disabled (`B.llvfg_r`) and overrun shutdown from being triggered. Both conditions are calculated depending on the target and the actual speed and includes hysteresis. If the actual speed exceeds the target speed by a certain delta, then idling is first enabled. A larger delta then causes overrun fuel cutoff to be enabled. `mrfg_r_w` is always at zero if idling disabled is not set.

The PDT1 controller that is used is not very accurate when the vehicle is stationary. It is for this reason that in the state "Constant driving" the control deviation is increased further by an offset, `voffs_w`. This offset depends on the speed and step-up ratio. As soon as a ramp is started, `voffs_w` is initialized to a value where the controller output does not drop. `voffs_w` then remains constant throughout the subsequent course of the ramp. By using an integrator with an adjustable time constant, `vlast_w` is calculated as an additional offset for the control deviation in order to prevent control deviations that are too large when in the "Constant driving" state. During the ramps, the PDT1 controller changes to a P-controller by setting the counter constant to equal the nominal-time constant. The controller gain is calibrated separately for constant driving and the ramps.

**APP FGRREGL 1.10 Application hint**

CWFGREGL:

## Bit 0

- 0: Controller initialization depending on the pre-control map and the gain
- 1: Controller initialization depending on the accelerator pedal and a fixed starting value

## Bit 1

- 0: v<sub>last\_w</sub> calculated for constant driving from an integrator
- 1: v<sub>last\_w</sub> always equals zero



**AINTKAN** number of interval misfire frequency at which ti- cutoff

**ANALUN** number of combustions for deactivation after detected misfire

**ATMABKA** factor reduction of exhaust gas temperature = f(soak time)

**ATMABKK** factor reduction for catalyst temperature = f(soak time)

**ATMTANS** temperature correction of the exhaust model temperature

**AZKELDYN** ignition per cylinder for load dynamics => knock detection

**AZKRLDYN** number of ignition per cyl. during knock control load dynamic

**AZKRDYN** number of ignition for knock control engine speed dynamic

**BRABEVI** acceleration at accelerating ramp

**BTRKHTMS** Characteristic enabling flag B\_trkh

**CDCCAS** code word CARB: CAN interface, timeout ASC

**CDCCINS** code word CARB: CAN interface, timeout instrument

**CDCKUP** code word CARB: CAN-bus, timeout clutch

**CDCEV1** code word CARB: injector 1

**CDCEV2** code word CARB: injector 2

**CDCEV3** code word CARB: injector 3

**CDCEV4** code word CARB: injector 4

**CDCEV5** code word CARB: injector 5

**CDCEV6** code word CARB: injector 6

**CDCEV7** code word CARB: injector 7

**CDCEV8** code word CARB: injector 8

**CDCFRAO** code word CARB: mixture adaptation factor frao

**CDCFRAO2** code word CARB: mixture adaptation factor frao bank 2

**CDCFRAU** code word CARB: mixture adaptation factor frau

**CDCFRAU2** code word CARB: mixture adaptation factor frau bank 2

**CDCFRST** code word CARB: deviation of lambda closed loop control

**CDCFRST2** code word CARB : deviation of lambda closed loop control bank 2

**CDCHSH** code word CARB: lambda sensor heating downstream cat



**CDCHSH2 code word CARB: lambda sensor heating downstream cat**

**CDCHSV code word CARB: lambda sensor heating upstream cat**

**CDCHSV2 code word CARB: lambda sensor heating upstream cat; (bank2)**

**CDCHSVE code word CARB: lambda sensor heating power stage upstream cat**

**CDCHSVE2 code word CARB: lambda sensor heating2 power stage upstream cat**

**CDCKAT code word CARB: catalyst conversion**

**CDCKAT2 code word CARB: catalyst conversion, cyl.row 2**

**CDCKPE Code word CARB: fuel pump relay power stage**

**CDCKRNT code word CARB: knock control zero test pulse**

**CDCKROF code word CARB: knock control offset**

**CDCKRTP code word CARB: knock control test pulse**

**CDCKS1 code word CARB: knock sensor 1**

**CDCKS2 code word CARB: knock sensor 2**

**CDCKS3 code word CARB: knock sensor 3**

**CDCKS4 code word CARB: knock sensor 4**

**CDCLASH code word CARB: lambda sensor aging downstream cat**

**CDCLASH2 code word CARB: lambda sensor aging downstream cat, Cyl.row 2**

**CDCLATP code word CARB: lambda sensor aging tp**

**CDCLATP2 code word CARB: lambda sensor aging tp, cyl. row 2**

**CDCLATV code word CARB: lambda sensor aging tv**

**CDCLATV2 code word CARB: lambda sensor aging tv, cyl.row 2**

**CDCLSH code word CARB: lambda sensor downstream catalyst**

**CDCLSH2 code word CARB: lambda sensor downstream catalyst**

**CDCLUEA code word CARB: Power stage engine fan A**

**CDCLUEB Code word CARB: Power stage engine fan B**

**CDCMD Code word CARB: misfire, multiple**

**CDCMD00 Code word CARB: misfire cyl. 0**

**CDCMD01 Code word CARB: misfire cyl. 1**

**CDCMD02 Code word CARB: misfire cylinder 2**

**CDCMD03 Code word CARB: misfire cylinder 3**

**CDCMD04 Code word CARB: misfire cylinder 4**

**CDCMD05 Code word CARB: misfire cylinder 5**

**CDCMD06 Code word CARB: misfire cylinder 6**

**CDCMD07 Code word CARB: misfire cylinder 7**

**CDCMD08 Code word CARB: misfire cylinder 8**

**CDCMD09 Code word CARB: misfire cylinder 9**

**CDCMD10 Code word CARB: misfire cylinder 10**

**CDCMD11 Code word CARB: misfire cylinder 11**

**CDCMDB Code word CARB: Target torque limiter**

**CDCMILE Code word CARB: MIL power stage**

**CDCNWKW code word CARB: alignment between camshaft and crankshaft**

**CDCNWKW2 code word CARB: alignment between camshaft 2 and crankshaft**

**CDCNWS code word CARB: camshaft control**

**CDCNWS2 code word CARB: camshaft control bank 2**

**CDCPH code word CARB: phase sensor**

**CDCPH2 code word CARB: phase sensor 2**

**CDCRKAT code word CARB: additive adaptive mixture correction rkat**

**CDCRKAT2 code word CARB: additive adaptive mixture correction rkat bank 2**

**CDCRKAZ code word CARB: additive adaptive mixture correction rkaz**

**CDCRKAZ2 code word CARB: additive adaptive mixture correction rkaz bank 2**

**CDCTA code word CARB: intake air temperature**

**CDCTES code word CARB: canister purge system**

**CDCTEVE code word CARB: canister purge valve power stage**

**CDCTM code word CARB: engine coolant temperature TMOT**

**CDCUB code word CARB: battery voltage UB (onboard)**

**CDCUF2SG Code word CARB: monitoring of the function: data from other ECU**

**CDCUFMV Code word CARB: monitoring of the function: torque comparison**

**CDCUFSKA Code word CARB: monitoring of the function: safety fuel cut-off**

**CDCURRAM Code word CARB: monitoring of the controller: RAM**

**CDCURROM Code word CARB: monitoring of the controller: ROM**

**CDCURRST Code word CARB: monitoring of the controller: Reset**

**CDCVKUP code word CARB: electr. clutch, speed dependent**

**CDLFRAO code word lamp : LR-Adaptation multiplicative upper threshold**

**CDLFRAO2 code word lamp : LR-Adaptation multiplicative upper threshold bank 2**

**CDLFRAU code word lamp: LR-Adaptation multiplicative lower threshold**

**CDLFRAU2 code word lamp: LR-Adaptation multiplicative lower threshold bank 2**

**CDLFRST code word lamp: feul supply system short test**

**CDLFRST2 code word lamp: feul supply system short test bank 2**

**CDLRKAT code word lamp : LR-Adaptation additive per time**

**CDLRKAT2 code word lamp : LR-Adaptation additive per time bank 2**

**CDLRKAZ code word lamp : LR-Adaptation additive per ingnition**

**CDLRKAZ2 code word lamp : LR-Adaptation additive per ingnition bank 2**

**DECKSTAI decrement-step for STADAP-factor**

**DEVTMAGR offset for evtmod depending on tsges\_w at high tans caused by EGR**

**DFPSLBIT Section bits for indication of the activated error paths**

**DFSEFO2N max. plausible speed-dependent variance of FSE values**

**DFSEFON max. plausible speed-dependent variance of FSE values**

**DKNOTBEGR Limtation of set value as  $f(nmot)$  if  $B\_dknot = true$**

**DKROFN limit of integrator rise for zero test**

**DLAMOB delta lamda at overboost**

**DLBTS Delta nominal Lambda for component protection**

**DLRKIONLP0 I component as  $f(abs(dwkdldr\_w))$ , above NLP**

**DLRKIUNLP0 I component as  $f(abs(dwkdldr\_w))$ , below NLP (weak)**

**DLRKIUNLP1 I component as  $f(abs(dwkdldr\_w))$ , below NLP (medium)**



**DLRKIUNLP2 I component as  $f(\text{abs}(\text{dwkd}l_r_w))$ , below NLP (strong)**

**DLURMIN speed dependensy of engine roughness referenz minimum value 1**

**DMAUFN delta torque rise after torque intervention**

**DMDDLWS Torque for power steering function of the**

**DMDLWS Torque for power steering**

**DMDNSM Torque offset for after cranking compensation**

**DMDPUG delta torque threshold end of dashpot**

**DMLLNG LLR: D-gain depending of ngasf for air path**

**DMLLNGV LLR: D-gain depending of ngasf for air path**

**DMLLRLMNN Lower limit for dmlrl**

**DMLLRLMXN Safety concept: upper limit for dmlrl**

**DMLLRMNN Lower limit for dmlr\_w**

**DMLLRMXN Safety concept: upper limit for dmlr**

**DMLSDUG Delta torque for finishing positive slope limitation**

**DMRIFW Delta relative torque for FGR initialization**

**DMSTES characteristic line maximum increase of purge mass flow**

**DNBURN Minimum difference in engine-speed for detected combustion**

**DPUPVDK pressure difference pu-pvdk**

**DRLSOLA Misfire Detection : load-dynamic treshold for deactivation**

**DLRTML proportion factor to decrease waiting time up to tmot-threshold for closed loop**

**DTVKAML delta-tv for cat oxygen neutralization (air mass dependent)**

**DTVKAML2 delta-tv for cat oxygen neutralization (air mass dependent) bank2**

**DVNG LLR: D-gain depending of ngfil for vehicle at rest**

**DVNGV LLR: D-gain depending of ngfil for vehicle rolling**

**DVSKNBGA delta velocity for set value correction after acceleration**

**DVSKNVGA delta velocity for set value correction after deceleration**

**DWKRMSN delta ignition angle knock control distance from mean retarding**

**DZWAML Up/down regulation speed between the maps of limitation**



**DZWDYN** Spark advance for burning-limit angle at tip-in

**DZWETA** delta ignition angle from efficiency

**DZWMNSTN** nmot dependent offset on latest ign. angle during start

**DZWNWSUE** Delta ignition angle dependent on the camshaft overlap

**DZWOAGR** AGR-rate-dependent offset of optimum ignition angle

**DZWOLA** Lambda dependency of optimum ignition angle referred to Lambda 1

**DZWOM** temperature-dependent offset of optimum ignition angle

**DZWSPM** delta latest ignition angle relative to engine temperature

**DZWSTTA** Delta ignition angle during start

**DZWTIN** delta ignition angle at tip-in

**EFFDFPM** Declaration of freeze frame extension out of table DFFT

**ETADZW** ignition efficiency depending on delta ignition angle

**ETALAM** Lambda effectiveness

**EVTMODO** offset for evtmod depending on filtered engine temperature

**FABMDWA** Factor to decrease the converter torque depending of n<sub>turb</sub>

**FABSTT** Factor parking time for model temperature

**FATMRML** divide factor exhaust-/exhaust-pipe temperature

**FATMRML2** divide factor exhaust-/exhaust-pipe temperature bank2

**FA.CALID**

**FBFGRSFW** Correction factor for FGR target acceleration

**FBTEB** factor ftefvab-dependending limitation of the canister charge adaptation speed

**FBTEVA** factor ftefva-dependending canister charge adaptation speed

**FBZBTEML** Weighting factor integration speed for canister charge adaptation

**FBZFRAT** weighting factor for integration speed KFFRAT as f(abo)

**FDDN LLR**: weightning factor for D-amplification

**FDVAGR** factor temperature for flow through EGR valve

**FDVANS** Temperature factor for air at throttle valve

**FETATEBN** characteristic line: reduction of engine efficiency as f(nmot)



**FFLDZ Follow-on ignition charging time**

**FFRITMS tmst dependent factor to modify I-dynamic of lambda control**

**FFTCAS Freeze Frame table: CAN, timeout ASC**

**FFTCINS Freeze frame table: CAN-Timeout, instrument panel**

**FFTCKUP freeze frame table: CAN-timeout KUP-message**

**FFTEV1 freeze frame table: injector power stage 1**

**FFTEV2 freeze frame table: injector power stage 2**

**FFTEV3 freeze frame table: injector power stage 3**

**FFTEV4 freeze frame table: injector power stage 4**

**FFTEV5 freeze frame table: injector power stage 5**

**FFTEV6 freeze frame table: injector power stage 6**

**FFTEV7 freeze frame table: injector power stage 7**

**FFTEV8 freeze frame table: injector power stage 8**

**FFTHSH Table of ambient condition for heating O2-sensor post cat**

**FFTHSH2 Table ambient conditions heating lambda sensor downstream catalyst bank2**

**FFTHSV Table of ambient condition for heating O2-sensor pre cat**

**FFTHSV2 Table of ambient condition for heating O2-sensor post cat bank 2**

**FFTHSVE Freeze frame table: O2 Sensor Heater power stage**

**FFTHSVE2 Freeze frame table: O2 Sensor Heater power stage bank 2**

**FFTKPE Freeze frame table: fuel pump relay power stage**

**FFTKRNT freeze frame table: knock control zero test**

**FFTKROF freeze frame table: knock control offset**

**FFTKRTP freeze frame table: knock control test pulse**

**FFTKS1 freeze frame table: knock sensor 1**

**FFTKS2 freeze frame table: knock sensor 2**

**FFTKS3 freeze frame table: knock sensor 3**

**FFTKS4 freeze frame table: knock sensor 4**

**FFTLASH Table ambient conditions for Lambda sensor downstream catalyst**

**FFTLASH2 Table ambient conditions Lambda sensor downstream catalyst bank2**

**FFTLATP Table ambient conditions Lambda sensor aging Tp upstream catalyst**

**FFTLATP2 Table ambient conditions Lambda sensor aging Tp upstream catalyst bank2**

**FFTLATV Table ambient conditions Lambda sensor aging Tv upstream catalyst**

**FFTLATV2 Table ambient conditions Lambda sensor aging Tv upstream catalyst bank2**

**FFTLSH Table of ambient conditions Lambda sensor downstream catalyst**

**FFTLSH2 Table of ambient conditions Lambda sensor downstream catalyst bank 2**

**FFTMDB freeze frame table: Target torque limiter**

**FFTMILE freeze frame table: MIL power stage**

**FFTNWKW freeze frame table: alignment between camshaft and crankshaft**

**FFTNWKW2 freeze frame table: alignment between camshaft 2 and crankshaft**

**FFTNWS freeze frame table: camshaft control**

**FFTNWS2 freeze frame table: camshaft control bank 2**

**FFTPH freeze frame table: phase sensor**

**FFTPH2 freeze frame table: phase sensor**

**FFTTA freeze frame table: air intake temperature TANS**

**FFTTES freeze frame table: canister purge valve**

**FFTTEVE freeze frame table: canister purge valve (power stage)**

**FFTTM freeze frame table: engine temperature TMOT**

**FFTUB freeze frame table: battery voltage UB (onboard)**

**FFTUF2SG Freeze frame table: monitoring of the function: data from other ECU**

**FFTUFMV Freeze frame table: monitoring of the function: torque comparison**

**FFTUFKA Freeze frame table: monitoring of the function: safety fuel cut-off**

**FFTURRAM Freeze frame table: monitoring of the controller: RAM**

**FFTURROM Freeze frame table: monitoring of the controller: ROM**

**FFTURRST Freeze frame table: monitoring of the controller: Reset**

**FFTVKUP freeze frame table: "Engine OFF"-request from F1-gearbox (KUP)**

**FHSTT factor hot start**



**FIMHU** Factor pulse abrupt

**FIMWU** Factor pulse smooth

**FKATEB** Characteristic line fuel portion depending on  $t_e$  /  $TEMIN$

**FKAXAVKAT** weighting factor for oxygen capacity depending on  $avkatf$

**FKDISA** faktor difference for integrator ambient pressure during fuel cut off

**FKHLA** Weighting factor Lambda nominal for catalyzer heating

**FKHMD** Weighting factor torque reserve for catalyzer heating

**FKKVS** Factor to correct fuel delivery system

**FKSTT** factor cold start

**FLRAWG** amplification of load controller

**FLRFKATE** Rating of factor  $fkatei$  from %TEB to optimize the regulation parameter

**FLRHG** amplification of load controller

**FLRM** Engine temperature dependent factor to modify I-dynamic of lambda control

**FLUTN** filter factor running irregularity

**FMDGENTA** factor: generator torque due to temperature

**FMDKHFH** altitude correction of torque reserve for catalyst heating

**FMDKHTM**  $t_{mot}$ -correction of torque reserve for catalyst heating

**FMDWAT** Factor to calculate the converter torque depending of oil temperature

**FNSHO** weighting of afterstart enrichment

**FNSSM** after start increase

**FNSSTKM** Factor to weight the desired speed at start during catalyst heating

**FNSSTM** Faktor for target engine speed during start

**FNSTABNV** Factor for engine speed stabilisation by torque

**FPLMRM** weighting factor for P component of air-mass controller

**FPVMXN2** factor for pressure ratio maximum with secondary last sensor

**FPWDKAPP** throttle angle dependent on accelerator pedal position, only for calibration

**FQTEDL** Factor for exponential decrease of flow rate

**FQTEFR** characteristic line: purge rate reduction with big  $fr_{m}$ -deviation



**FQTEPT characteristic line: for fuel-tank underpressure limitation**

**FQTEVA progression of purge rate controller**

**FRARAWG amplification factor**

**FRARHG amplification factor**

**FRINH1 Multiplication factor for RIN nominal value downstream of the catalyzer**

**FRINH2 Multiplication factor for RIN nominal value downstream of the catalyzer**

**FRINV1 Multiplicativ factor for RIN desired value pre cat**

**FRINV2 Multiplicativ factor for RIN desired value pre cat**

**FRLFSDP injection correction for RLFS**

**FRLMNHO correction factor r<sub>lmin</sub> depending on altitude**

**FSTHO weighting of factor start**

**FSWALUV rough road detection threshold = f (vehicle speed)**

**FSWALUV1 rough road detection threshold = f (vehicle speed)**

**FSZTM Factor dwell angle correction t<sub>mot</sub> depending**

**FTAGRV Factor for temperature drop from EGR\_pipe to EGR\_valve**

**FTDAG factor for temperature drop on EGR line**

**FTEINIX characteristic line for max. purge rate = F(integral purge flow after TE-Stop)**

**FTMFFANZ Follow-on ignition weighting factor**

**FTMLAKH t<sub>mot</sub>-correction of lambda-weighting at catalyst heating**

**FUEPMLD Factor for gliding transition average pressure (reference pressure turbo)**

**FUKNSTHO altitude dependent transient control post cranking factor**

**FUKNSTM initial value of transient control post cranking factor**

**FVERMN characteristic line: filter factor for purge flow in the manifold with fresh air**

**FVERZDYN dynamic factor delay of purge flow in the manifold**

**FVRMDYN dynamic factor for purge flow in the manifold with fresh air**

**FWDMVAD factor for the weighting of d<sub>mvad\_w</sub> in %M<sub>DMIN</sub>**

**FWEMXT maximum factor for fuel cut-in temperature characteristic**

**FWFTBRTA Weighting for ft<sub>br</sub> as a function of t<sub>ans</sub>**

**FWLKFTBR** warm up correction for combustion chamber model

**FWMLHFMMN** Weighting factor for min. HFM air-mass threshold as a function of the altitude

**FWSTAA1** afterstart correction

**FWSTAB1** weighting afterstart decrease range 1

**FWSTAB2** weighting afterstart decrease range 2

**FWSTAB3** weighting afterstart decrease range 3

**FWSTAS1** correction of threshold 1 for afterstart

**FWSTAS2** correction of threshold 2 for afterstart

**FZANSSA1** factor for ign. sync. decreasing of afterstart enrichment at hot start range 1

**FZANSSA2** factor for ign. sync. decreasing of afterstart enrichment at hot start range 2

**FZANSSM1** factor for ign. sync. decreasing of afterstart enrichment above SZANSSM

**FZANSSM2** factor for ign. sync. decreasing of afterstart enrichment below SZANSSM

**FZANSSM3** factor for ign. sync. decreasing of afterstart enrichment in range 3

**FZDASHTM** factor for time constant dashpot

**FZN1** Cylinder individual factor at neutral camshaft position EV 1

**FZNWN1** Cylinder individual factor at active camshaft position EV 1

**FZPUSA** correction faktor time constant ambient pressure adaptation during fuel cut-off

**FZWSTNM** Ignition angle during start

**FZWSTTM** Ignition angle during start

**GFDLDN LLR**: weighting factor for D-amplification on the air path

**IGESGA** Total transmission ratio

**ILMLKAXTK** Threshold of richness area of O2 purging after fuel cat off, funct. of cat-temp

**ILMLKAXTK2** Thresh. of richness area of O2 purging after fuel cut off, funct. of cat-temp.

**ILMRN** integrator gain of air mass controller

**IMLKAXTK** integr. air mass threshold  $f(t_{katm})$  for cancelation of cat oxygen neutralization

**IMLKAXTK2** integr. air mass threshold  $f(t_{katm2})$  for cancelation of cat oxygen neutral.

**IMLKHTMS** implr-threshold, changing to lambda catalyst heating

**INCKSTAI** increment-step for STADAP factor

**IVDN LLR: I-gain for vehicle at rest**

**IVDNDTE LLR: I-gain at DTEV**

**IVDNV LLR: I-gain for vehicle rolling**

**KATBFML filter time constant for signal attenuation in catalyst stress**

**KATBFML2 filter-time constant for signal attenuation in catalyst stress (assymmetrical)**

**KATBFXM max. catalyst load threshold for stop condition**

**KATMEXML Temperature of the exotherme in the catalyst tkatm**

**KATMEXML2 Temperature of the exotherme in the catalyst , bank 2**

**KATMIEXML Temperature of the exotherme in the catalyst tikatm**

**KATMIEXML2 Temperature of the exotherme in the catalyst tikatm, bank 2**

**KDLASHKI evaluation factor of I-part of LRHK, f(dlashkm)**

**KDLASHKI2 evaluation factor of I-part of LRHK, f(dlashkm), bank 2**

**KDLASHKP evaluation factor of P-part of LRHK, f(dlashkm)**

**KDLASHKP2 evaluation factor of P-part of LRHK, f(dlashkm), bank 2**

**KE1N knock detection threshold at cylindertimer 1**

**KE2N knock detection threshold at cylindertimer 2**

**KE3N knock detection threshold at cylindertimer 3**

**KE4N knock detection threshold at cylindertimer 4**

**KE5N knock detection threshold at cylindertimer 5**

**KE6N knock detection threshold at cylindertimer 6**

**KE7N knock detection threshold at cylindertimer 7**

**KE8N knock detection threshold at cylindertimer 8**

**KEMLN length of the sampling window for knock control**

**KFABAK share factor wall wetting for acceleration enrichment**

**KFAFTE map flow-characteristic of PCV (incl. PCV carcoal-canister line)**

**KFAMAL map reduction factor of the engine roughness reference value at multiple misfire**

**KFAMAL1 map reduction factor of the engine roughness reference value at multiple misfire**

**KFATMLA map exhaust gas temperature correction = f(lambda)**



**KFATMLA2 map exhaust gas temperature correction = f(lambda) bank2**

**KFATMZW map exhaust gas temperature correktion = f(ignition-variation)**

**KFATMZW2 map exhaust gas temperature correktion = f(ignition) bank2**

**KFAVAK share factor wall wetting for deceleration enleanment**

**KFBAKL factor accel. enrichment (short- and long-time part)**

**KFBRAWA Target acceleration for resumption**

**KFBS bank-selective mixture factor**

**KFCFO map for definition of range characteristics (dominant..)**

**KFCFO2 map for definition of range characteristics (dominant..)**

**KFDETATE correction of ignition angle effectiveness for diagnosis of PCV**

**KFDFBTMN dynamic factor for combustion chamber temperatur model negativ gradient**

**KFDFBTMP dynamic factor for combustion chamber temperatur model positiv gradient**

**KFDLSD Damping of PT2 filter in positive torque slope limitation**

**KFDLUR map engine roughness difference dluts referenz value**

**KFDLUR1 map engine roughness difference dluts referenz value**

**KFDLUR2 map engine roughness difference dluts referenz value**

**KFDLURZ map engine roughness difference dluts referenz value at ZAS (cylinder cut-off)**

**KFDMDADP upper threshold for torque-intervention during dashpot**

**KFDMDARO Upper threshold for torque intervension**

**KFDMDKOE Starting value torque filter when air-conditioner compressor is activated**

**KFDMDPO Delta torque for starting negative slope limitation**

**KFDMLSDO Delta torque for starting positive slope limitation**

**KFDMLSDS delta torque for triggering of load-shock damping after shifting procedure**

**KFDTMRS char.line for gradient of engine coolant temp. during cutoff for reference model**

**KFDTMTE char. map for gradient of engine coolant temperature in substitute temp. model**

**KFDTMTR char. map for gradient of engine coolant temperature in reference model**

**KFDTMTU char. map for correction gradient of engine coolant temp. at low warming up**

**KFDYES Threshold for dynamic presetting values**

**KFDYESOF** Offset threshold for dynamic presetting values

**KFDZWKG** ignition angle correction due to knock limit shift

**KFETATE** characteristic map for efficiency at active purging when  $t_e$  is near **TEMIN**

**KFFDLBTS** Factor delta nominal Lambda for component protection

**KFFFANZ** Number of sequential sparks

**KFFFANZUB** Number of sequential sparks

**KFFRAT** load and speed dependent gradient of **FRAT** integrator

**KFFRMIN** lower limit of control range

**KFFTEAN** characteristic map for limitation of the purge rate with no Lambda control

**KFFTEAX** Characteristic map for limitation of the purge rate

**KFFTV** weighting map for **TVLRH**

**KFFTV2** weighting map for **TVLRH** bank 2

**KFFWL** map warm-up factor

**KFFWLRL** map warm-up factor load dependent fraction

**KFFWLW** map weighting warm-up factor

**KFFWTBR** Weighting factor for combustion chamber temperature model

**KFFWTBRA** Weighting factor for combustion chamber temperature model  $B_{agr} = \text{true}$

**KFKABMT** Map for correction of calculated amplitude, dependent on  $m_l$  and cat. temperature

**KFKHFM** HFM-correction characteristic map

**KFKSWF** map for catalyst protection, weighting factors

**KFKWTMP** Characteristic torque reserve for keeping catalyst warm, temporary

**KFLASKH** Performance characteristics lambda exhaust nominal at catalyst heating

**KFLBTS** Nominal Lambda for component protection

**KFLF** lambda characteristic map at part load

**KFLMSKH** Performance characteristics lambda engine nominal at catalyst heating

**KFLUAR** map for engine roughness distance reference value

**KFLUAR1** map for engine roughness distance reference value

**KFLUAR2** map for engine roughness distance reference value

**KFLUARZ map for engine roughness distance reference value at ZAS (cylinder cut-off)**

**KFLURB map for engine roughness - reference base value**

**KFLURB1 map for engine roughness - reference base value**

**KFLURB2 map for engine roughness - reference base value**

**KFLURBZ map for engine roughness base value, in case of ZAS**

**KFLURM reference base value map for engine roughness for misfire detection**

**KFLURM1 reference base value map for engine roughness for misfire detection**

**KFMAKR map for starting measuring window knock control**

**KFMDBGRG map with the value of the torque limitation**

**KFMDDSLA Map torque reserve at tester demand of SAI-diagnosis short test**

**KFMDCGEN Torque intake generator**

**KFMDCKH Characteristic torque reserve for catalyst heating**

**KFMDCKO map for torque needed for air condition**

**KFMDCPWM steady state load of ac-compressor for PWM-signal of its load**

**KFMDCPWME initial load of ac-compressor for PWM-signal of its load**

**KFMDCRKO look-up-table: torque loss depended of rl, nmot**

**KFMDCRKOE look-up-table: torque loss dyn. part dependend of rl, nmot**

**KFMDCS map for engine drag torque**

**KFMDCSZAS map for engine drag torque during cyclinder cut off**

**KFMDCZOF\_UM map for offset tolerance depending on permissible torque**

**KFMIFABG delta torque for gradient limitation**

**KFMIFALS Indicated driver's request torque for charge path at load-shock damping**

**KFMILSD Initial value for positive torque slope limitation**

**KFMIMN minimum drag torque**

**KFMIOPT map optimum engine torque**

**KFMIREDD Map of decreasing control torque for VMAX control**

**KFMIRL map for calculation of nominal charge**

**KFMIZUFIL Maximum permitted indicated set torque for torque limitation before Filter**

**KFMIZUNS Authorized torque for post-start torque increase**

**KFMIZUOF Maximum permitted indicated set torque for torque limitation**

**KFMI\_UM map of optimum engine torque**

**KFMLDMN air mass flow threshold for min. failure**

**KFMLDMX air mass flow threshold for max. failure**

**KFMPED\_UM map for permissible torque from the pedal position in function monitoring**

**KFMPNS\_UM map for permissible torque from pedal position for a cold engine**

**KFMRES LLR: torque reserve at idle and near-idle zone**

**KFMRESK LLR: torque reserve at idle and near-idle zone clutch disengaged**

**KFMRESKH Torque reserve during catalyst heating**

**KFMRESNL Torque reserve in non idling state**

**KFMRESTA Torque margin dependent on tans**

**KFMRESTM Map temp-dependent limiting of torque reserve**

**KFMSNWDK Map for scaled mass flow over throttle valve**

**KFNLLNST idle speed after start**

**KFNSEA after start increase**

**KFNWRL weighting of afterstart enrichment**

**KFNW characteristic map for variable camshaft spread**

**KFNWEGM Fuel cut in map depending on rpm**

**KFNWWL**

**KFPBRK factor to correct pressure at combustion chamber**

**KFPBRKNW factor to correct pressure at combustion chamber by active Camshaft control**

**KFPED accelerator pedal characteristic**

**KFPEDR Pedal characteristic for reverse gear (only automatic transmission)**

**KFPLMR P-component of air mass controller**

**KFPRG internal partial exhaust gas pressure dependent on camshaft adjustment sumode=0**

**KFPRG2SU internal partial exhaust gas pressure dependent on camshaft adjustment sumode=2**

**KFPRG3SU internal partial exhaust gas pressure dependent on camshaft adjustment sumode=3**

**KFPRGSU internal partial exhaust gas pressure dependent on camshaft adjustment sumode=1**

**KFPU pulsation characteristic map**

**KFPUNW pulsation map for camshaft control switch over**

**KFPUSU pulsation characteristic map at active variable intake system by sumode=1**

**KFPUSUNW pulsation characteristic map at active variable intake system and camshaft cont.**

**KFQTE Map for purge rate increase / decrease**

**KFRI I characteristic map**

**KFRI2 LR-I-Map for bank 2**

**KFRINH MAP for Nernst resistor post cat**

**KFRINH2 MAP for Nernst resistor post cat bank 2**

**KFRINV MAP for Nernst resistor pre cat**

**KFRINV2 MAP for Nernst resistor post cat , bank 2**

**KFRLIP\_UM characteristic map for load signal calculation on throttle angle**

**KFRLMN Minimum charge during fuel on**

**KFRLMNSA Minimum rl during fuel cut off**

**KFRLW rlw-map from throttle valve angle**

**KFRLWNW rlw-map from throttle valve angle during variable camshaft**

**KFRLWSU rlw-map from throttle valve angle during manifold switch over**

**KFRLWSUNW rlw-map from throttle valve angle during manifold switch over and aktive var. ch**

**KFRP P characteristic map**

**KFRP2 LR-P MAP for bank 2**

**KFRTV delay time characteristic map**

**KFRTV2 delay time characteristic map**

**KFSU Load/speed performance characteristics for suction tube switchover**

**KFSU2 map for intake manifold switch over, flap 2**

**KFSZT Dwell angle characteristic map**

**KFTADMS dynamic evaluation factor for close off of PCV**

**KFTAGAV EGR temperature at outlet valve**

**KFTATM map exhaust gas temperature f(nmot,rl)**

**KFTATM2 map exhaust gas temperature f(nmot,rl) bank2**

**KFTATX map for max. duty cycle**

**KFTEKA characteristic map of desired fuel portion purge control**

**KFTEVP Characteristic map for period time of the PCV**

**KFTPKOR correction map for the measured cycle duration TP (tpsvkof)**

**KFTVFRR Map: Lambda controll after this time reset at reference value**

**KFTVSA Retard time for overrun fuel cut-off**

**KFURL conversion factor from ps->rl dependent on camshaft adjustment sumode=0**

**KFURL2SU conversion factor from ps->rl dependent on camshaft adjustment sumode=2**

**KFURL3SU conversion factor from ps->rl dependent on camshaft adjustment sumode=3**

**KFURLSU conversion factor from ps->rl dependent on camshaft adjustment sumode=1**

**KFUSHK lambda sensor reference value for lambda control downstream of catalyst**

**KFUSHK2 lambda sensor reference value for lambda control downstream of catalyst bank2**

**KFVAKL factor decel. enleanment (short- and long-time part)**

**KFVERST weighting map for increasing control of friction torque**

**KFVOFFS velocity offset for cruise control**

**KFWDKMSN Map for the desired throttle blade angle**

**KFWDKPP throttle blade position dependent on air charge signal**

**KFWDKSMX max. desired throttle angle**

**KFWDKSST desired throttle position at start-up**

**KFWDKTHO desired throttle position at start-up - f (hight, engine start temperatur)**

**KFWEE characteristic map angle end of injection**

**KFWEEK map for end of injection angle (cold parameters)**

**KFWHSTT map weighting of hot start factor**

**KFWKSTAB factor cold re-start for reduction of starting fuel**

**KFWKSTN map weighting of factor cold start**

**KFWKSTT map weighting of factor cold start**

**KFWMABG map for heat-quantity threshold dew-point end upstream bank1**

**KFWMABG2 map for heat-quantity threshold dew-point end upstream bank2**

**KFWMKAT map for heat quantity threshold dew-point end downstream**

**KFWMKAT2 map for heat quantity threshold dew-point end downstream bank 2**

**KFWPFGR Inverse pedal characteristic for cruise mode**

**KFWTBR Weighting factor Tans/Tmot for combustion chamber temperature model**

**KFWTBRA Weighting factor Tans/Tmot for combustion chamber temperature model B\_agr=true**

**KFWWLML map weighting warm-up factor**

**KFWWNS repeated start time factor**

**KFZDASH Time constant for negative torque slope limitation**

**KFZDASH2 time constant PT1-filter dashpot at low clutch torque**

**KFZKPUA time constant for ambient pressure**

**KFZLSD Time constant for positive torque slope limitation**

**KFZNSM time constant for decay of reference speed**

**KFZW Ignition advance-angle charakteristik map**

**KFZW2 Ignition angle performance characteristics variant 2**

**KFZWMN Map for minimal ignition angle**

**KFZWMNKH Map for minimal ignition angle catalyst warm-up**

**KFZWMNST minimal ignition spark advance for engine start and after start**

**KFZWMS Map for ignition value as latest possible value**

**KFZWOP optimum ignition angle**

**KFZWOP2 Optimum ignition angle, variant 2**

**KFZWVLNM Delta ignition sparc advance during engine warm up phase**

**KFZWVLTM Delta ignition sparc advance during engine warm up phase**

**KFZW\_UM map of optimum ignition angle**

**KIFZGAWG amplification of vehicle model integrator at AT**

**KIFZGHG amplification of vehicle model integrator at AT**

**KINMXG gain of integral component for NMAX control**

**KINMXRLG** gain of integral component for NMAX control

**KIRMSMS** Integration speed matching of mass flow PCV with calculated mass flow

**KKFFGRGA** amplification rate during cruising for cruise control

**KLAF** characteristic of Saint-Venant

**KLAFTE** characteristic of Saint-Venant of purge control valve an line AKF-TEV

**KLATMILAE** Temperature of the exotherme decrease during enrichment tikatm

**KLATMILAE2** Temperature of the exotherme decrease during enrichment tikatm, bank2

**KLATMIZWE** Temperature of the exotherme decrease in cat during ignition retard tikatm

**KLATMIZWE2** Temperature of the exotherme decrease in cat during ignition retard tikatm, bank

**KLATMLAE** Temperature of the exotherme decrease during enrichment

**KLATMLAE2** Temperature of the exotherme decrease during enrichment, bank 2

**KLATMZWE** Temperature of the exotherme decrease in cat during ignition retard tkatm

**KLATMZWE2** Temperature of the exotherme decrease in cat during ignition retard, bank2

**KLDMDLF1** Characteristic curve reserve torque fan

**KLDMDLF2** Characteristic curve reserve torque fan 2

**KLDMMX** Maximum delta torque for air path

**KLDPDK** pressure drop at throttle blade

**KLDTPH** Fixed value characteristic for weighting the engine dynamic

**KLDTPHST** Fixed value characteristic for the engine start

**KLDYNCOR** Value for the dynamic correction after the first ignition

**KLETAZW\_UM** ignition efficiency depending on delta ignition angle

**KLFZWMNKH** Spark retard gradient of burning limit during after-start at cat.heating

**KLFZWMNST** Spark retard gradient of burning limit during after-start

**KLNLPHN** Correction of the phase frequency characteristic of the sensor

**KLNPED\_UM** Speed lim. as func. of nominal pedal value, in DK drive standby func.,func.mon.

**KLNWRLTM** Weighting of relative nominal filling over engine temp. for addressing KFNWS

**KLRSYNIN**

**KLRSYNPN**





**KLTDS** Conversion line for tank pressure sensor DS-T2

**KLTNRDE** characterisitic for tooth times at reverse rotation

**KLWDKABST** Weighting desired throttle position at start-up

**KLWDKPED** Offset desired throttle position at start-up

**KLWDKTAN** weight of throttle position at start up with intake air temperatur

**KLWNWI** Fixed value characteristic for weighting the angular displacement

**KRAFGRGA** amplification rate at ramp for cruise control

**KRAL1N** load range for adaption maps 1

**KRAL2N** load range dor adaption maps 2

**KRAL3N** load range for adaption maps 3

**KRDWSN** knock control delta angle safety

**KRFKN** retard step knock occurrence

**KRMXN** maximum retard adjustment

**KRNLZAR** cylinder individual rpm limit for lead by leading cylinder

**KRVFN** number of firings/cyl. or time for ignition advancing

**KRVFSN** number of firings/cyl. or delay-time during fast ignition advancing of the KC

**KSTAI** workingrange for STADAP factor

**LALIUSH** lambda linearization, sensor behind catalyst

**LALIUSH2** lambda linearization, sensor behind catalyst, bank 2

**LALIUSRH** lambda linearization, sensor behind catalyst

**LALIUSRH2** lambda linearization, sensor behind catalyst

**LAMFA** Lamda driver demand

**LAMKAML** lambda setpoint for catylyst deoxidation (dependent on air mass)

**LAMKAML2** lambdasetpoint for catalyst deoxidation (air mass dependent), bank 2

**LAMLGMTM** lambda limit "lean"

**LASDSLA** Lambda exhaust nominal at secondary air adaption/short test

**LASTMOT** tmot-correction of lambda exhaust nominal

**LIMXDNS** upper integrator limit for standing car

**LIMXVDNS** upper integrator limit for rolling car

**LISTM** value of idle speed control integrator during start

**LKRN** load-signal threshold knock control

**LMSTMOT** tmot-correction of lambda engine nominal

**LNXQTM** natural logarithm from temperature quotient

**LSAKTD** Impact of slow front sensor on cat. monitoring

**LURBRL8** reference value for engine roughness, vehicle speed zero

**LURKH** dmrkh-depen. engine roughness reference correction value, during cat heating

**LURKTM** Tmot-dependent engine roughness reference correcting value

**LURMIN1** speed dependensy of engine roughness referenz minimum value 1

**LURMIN2** speed dependensy of engine roughness referenz minimum value 2

**LURMIN3** speed dependensy of engine roughness referenz minimum value 3

**LZFUER** guide cylinder assignment

**MASK\_40MS** 40ms mask for function monitoring

**MASK\_FUAE** Mask for task splitting in monitoring functions (part 1: inputs)

**MDKOAB** Torque threshold to shut down the compressor during acceleration

**MDKOAN** Torque threshold to switch the AC-compressor off

**MDKOEN** Torque threshold to switch the AC-compressor on

**MDSH** Part of the resistant torque depending on altitude

**MDSM** temperatuer share of engine friction torque

**MDSMZAS** temperatuer share of engine friction torque during cylinder cut off

**MIFAMXNOT** maximum indicated engine torque at limp home

**MKFADPN** clutch torque for switch-over dashpot-filter time

**MKFADPN1** clutch torque for switch-over dashpot-fil. time when AC comp. has been enabled

**MKLLS** torque needed for air condition fan

**MLHFM** air-mass meter characteristic line

**MLSUS** reference of air mass flow integral

**MRFARUGDN** Reset threshold for linear pedal travel in the non-reduced DK range

**MRFAVLN Full load detection threshold of the relative driver request**

**MRFAVV threshold to switch end of injection angle at max. driver request**

**MRFGRIMX Maximum FGR initialization value**

**MSNTAG EGR mass flow standardised**

**MSNTATE Characteristic standardized mass flow through TEV**

**M\_SRST\_UM Mask B\_srst\_um - information SW-reset from cyclic RAM-check**

**NARLLGA speed threshold for AR at idle**

**NASNOTKL characteristic line rotational speed against engine stall**

**NDFILOG Threshold for filter output ndfil**

**NDIFFOG Threshold engine speed difference for initialization of AR during braking**

**NFS2M Target idle speed 2, B\_fs = 1**

**NFSKHM LL nominal speed with driving graduations and catalyzer heating**

**NFSM desired engine speed DRIVE-position switch on**

**NGALUN Misfire Detection : treshold for gradient of engine speed**

**NGKRWN threshold revolution gradient for dynamics detection**

**NLL2M Target engine speed 2**

**NLLCVTMXV Limitation of the target speed (CVT transmission)**

**NLLKHM Nominal idling speed during catalyzer heating**

**NLLM desired engine speed**

**NMAXDVG rpm limit in case of fault detection velocity signal**

**NMXDAEF maximum permitted engine speed for throttle actuator substitute function**

**NMXPG P component for NMAX control**

**NMXPRLG P component for NMAX control**

**NNSTA engine-speed transition normal -> start**

**NSLPP Target speed depending on the pump pressure of power steering**

**NSLPPFS Target speed depending on the pump pressure of power steering with B\_fs=1**

**NSTAMXHA engine speed limit until STADAP is active depend. on altitude**

**NSTNM transition start -> normal**



**NWDKSST** threshold for deactivation desired throttle position without torque structur

**NWEVVTM** Fuel restart-speed at CVT

**NWENG** Fuel cut-in engine speed

**NWENGFS** Delta Fuel cut-in engine speed with Drive

**NZHDTL** Speed threshold for decrementing time counter for hot idling

**NZHITL** Speed threshold for incrementing time counter for hot idling

**PAGAVML** exhaust gas pressure at outlet valve

**PLRHAV** Weighting factor of P-part LRHK depending on catalyst age

**PLRHAV2** Weighting factor of P-part LRHK depending on catalyst age range 2

**PLRHML** p-part of LRHK, f(dushk)

**PLRHML2** Partie p. dans LRHK, agit avec la difference de tension de sonde aval cata banc2

**PRG2SUNM** internal exhaust-gas part. press. dependent on the speed at active SU (2nd flap)

**PRG3SUNM** inter. exhaust-gas part. press. dependent on speed at active SU (1st + 2nd flap)

**PRGNM** internal exhaust-gas partial pressure dependent on the speed

**PRGSUNM** inter. exhaust-gas partial press. dep. on speed in case of active SU (1st flap)

**PUKANS** correction of pulsation depending on intake air temperature

**PVDN LLR**: P-gain for vehicle at rest

**PVDNKH** proportional ISC when secondary air activ

**PVDNST** proportional ISC in start

**PVDNV LLR**: P-gain for vehicle rolling

**PVLDN LLR**: P-gain for vehicle at rest (air path)

**PVLDNV LLR**: P-gain for vehicle at rest (air path)

**REDABM** fuel cut-off table for torque reduction

**REDABMB** fuel cut-off table for torque reduction slave1 or ecu B (SGB)

**REDABMC** fuel cut-off table for torque reduction slave 2 or ecu C

**REDABMZ** fuel cut-off table for torque reduction during ZAS

**REDZEM** threshold between ignition intervention and injector disabling

**RKBAUM** rk-threshold for acceleration enrichment display



**RKRMX1N** Maximum of reference level for knock detection threshold cylinder group 1

**RKRMX2N** maximum of reference level for knock detection threshold cylinder group 2

**RKVAUM** rk-threshold for deceleration enleanment display

**RLDKTSO** upper load characteristic line for DKAT-active

**RLDKTSU** lower load characteristic line for DKAT-active

**RLLRHON** char. line on nmot, upper rl control threshold for downstream lambda control

**RLLRHUN** char. line on nmot, lower control threshold rl for downstream lambda control

**RLLRUN** char.line above nmot,lower rL control limit for controller in front of catalyst

**RLNOT** limp-home relative air charge rl in case of E\_DK and E\_LM

**RLSALUN** threshold load fuel cut-off detection for deactivating misfire detection

**RLVMXN** maximum volumetric flow with open throttle valve

**RLVSMXN** maximum volumetric flow with open throttle valve and SU

**SDK10TEUB** wdkba dependet basic point (number 10)

**SDN06LLSB** 10 Sst.

**SENZZYL** knock sensor for sw-cylinder counter 0-7

**SFR05TEUB** frmit dependet basic point (number 5)

**SGA08MDUB** base point distribution of actual gear 8 b.pt.

**SGSC\_ANZ** number of module calls of %UFSGSC (refer to %URPAK) in the monitoring function

**SGSC\_K** Constant for module %UFSGSC (see %URPAK)

**SIM06ESUW** Distribution for integrated air massflow since end of start

**SKO06KOUB** Distribution PWM-signal: load of ac-compressor

**SKS06ESUB** Distribution for the start adaption factor kstaa

**SLFOO2N** speed dep. upper threshold for learning filter value at fuel-on/-off adaptation

**SLFOON** speed dep. upper threshold for learning filter value at fuel-on/-off adaptation

**SMI04LLUB** distribution: ind. torque for torque-reserve

**SMK08MDSW** Antisurge torque dependent basic point (number =8)

**SML05DKUB** base point distribution air mass

**SML06TEUB** ml dependet basic point (number 6)

**SNG06LLSB Datapoint distribution, speed gradient, 6 datapoints**

**SNM05DKUB base point distribution nmot**

**SNM06ESUB Distribution for engine speed**

**SNM06KOUB distribution for ac-compressor torque function**

**SNM06LLUB distribution of engine speed**

**SNM08DMUB Datapoint distribution in DMD, 8 speed datapoints**

**SNM08KOUB Datapoint distribution for air-conditioner compressor control 8 nmot**

**SNM08\_UB Base point distribution engine speed, 8 base points**

**SNM10TEUB nmot dependet basic point (number 10)**

**SNM12FEUB set points of WDKSMX, WDKUGDN**

**SNM16KRUB datapoint distribution engine speed, 16 datapoints**

**SNM16OPUW 16 speed set points for ?**

**SNM16ZUUW break point distribution engine speed, 16 base pts.**

**SNS06LLSB Datapoint distribution, set-speed deviation, 06 datapoints., idle-speed control.**

**SQM05TEUB air mass quotient dependet basic point (number =5)**

**SRL04DYUB basepoint distribution of rl, 4 basepoints**

**SRL04KRUB datapoint distribution relative charge, 4 datapoints**

**SRL06KOUB 6 air charge set points for A/C-compressor torque loss**

**SRL08DMUB Datapoint distribution in DMD, 8 load datapoints**

**SRL08NXUB**

**SRL11OPUW set point distribution relative charge**

**SRL12ZUUW break point distribution of relative air charge, 12 base points**

**SRP06ESUB Distribution for relative air charge**

**SRST1\_UR value for RAM data redundancy of bit B\_SRST\_UM = 1**

**STA04LLUB distribution: tans for torque resreve**

**STA06ESUB Distribution for the air temperature in the intake manifold**

**STA06LLUB temperature: ambient air, PWM -signal of AC/compressor**

**STM04SAUB Datapoint distribution, engine temperature, 4 datapoints**

**STM06LLUB Datapoint distribution, engine temperature, 6 datapoints**

**STM06\_UB Datapoint distribution, engine temperature, 6 datapoints**

**STM12ESUB Distribution for the engine coolant temperature tmot**

**STN06LLUB distribution: time after start; for determination of idle speed after start**

**STS08ESUB Distribution for engine coolant temperature at start**

**STS12ESUB Distribution for engine coolant temperature at start**

**SY\_2SG system constant 2 motronic systems**

**SY\_650ICLK system constant: external clock frequency of CC650**

**SY\_AGR System constant AGR present**

**SY\_ASG automatic standard transmission**

**SY\_ASR system constant ASR present**

**SY\_AWUE injection valve cutoff possible by function AWUE**

**SY\_BDE system constant GDI**

**SY\_BGVZS**

**SY\_BKV system constant: brake booster**

**SY\_BLOOP sys. con. resetting of irreversible EGAS fault possible during clearing of FCM**

**SY\_CANAC systemconstant: AC-compressor signal from CAN**

**SY\_CDCCSIZE System constant: Number of values CDC to each fault path**

**SY\_CDKSIZE System constant: Number of values CDK to each fault path**

**SY\_CDTSIZE System constant: Number of values CDT to each fault path**

**SY\_CLASIZE System constant: Number of values CLA to each fault path**

**SY\_CONFSL System constant: secondary air present vorhanden**

**SY\_COPOTI System constant CO-Poti present**

**SY\_CVT system constant: CVT transmission exists**

**SY\_DEGFE system constant diagnosis input values load monitoring**

**SY\_DFPMENTV system constant: environmental conditions in fault code memory**

**SY\_DGANZ system constant number rotational-speed sensor**

**SY\_DLDP SY\_DLDP = 1 there ist a DLDP in system**

**SY\_DLS system constant digital idle speed control**

**SY\_DLSHV Sys. constant condition %DLSHV (sensor exchange behind KAT) existent**

**SY\_DOPZW System constant doubled ignition output included**

**SY\_DTES system constant diagnosis evap system**

**SY\_DVEADA system constant BGVE: disabling injection and ignition during DV-E-adaptation**

**SY\_EGAS System constant E-GAS present**

**SY\_EGFE system constant input variable for charge detection**

**SY\_FANT system constant increase of the fuel cut-off speed at tester intervention**

**SY\_FFESIZE system constant: Size of Freeze Frame-extension**

**SY\_FFTSIZE System constant: Number of values FFT to each fault path**

**SY\_FFZ system constant interval ignition**

**SY\_FREQ\_CP system constant cpu frequency**

**SY\_FWFGR**

**SY\_GAP system constant: number of missing teeth in the gap**

**SY\_GGGTS system constant: sensor variable exact temperature signal**

**SY\_GRDWRT System constant basic value, space between SW reference mark to OT in ° KW**

**SY\_GRDWRTB system constant basic value 2.ECU, space between SW reference mark to OT in °KW**

**SY\_GRNDWRT system constant basis angle ref. tr-mark**

**SY\_INI\_OBD system constant to select the communication protocols for scan tool operation**

**SY\_KL50 System constant: information available in the ECU if starter is cranking**

**SY\_KLDF system constant for generator DF-signale**

**SY\_KOBIDIR AC- with bidirect. connection**

**SY\_KOEVAB coordination injection valve cutoff by function KOEVAB**

**SY\_KOPWM PWM-compressor-signal enabled**

**SY\_KR\_INT system constant: CC650 present**

**SY\_KS1 system constant: input of the CC195 onto which knock sensor 1 is connected**

**SY\_KS2 system constant: input of the CC195 onto which knock sensor 2 is connected**

**SY\_KS3 system constant: input of the CC195 onto which knock sensor 3 is connected**



**SY\_KS4 system constant: input of the CC195 onto which knock sensor 4 is connected**

**SY\_KSDIFF system constant: connection type of knock sensor(s)**

**SY\_LFS System constant Fan Control configuration**

**SY\_LWS system constant steering angle via CAN**

**SY\_ME7 system constant ECU**

**SY\_NACH System constant ignition output after KL15 off included**

**SY\_NWS system constant camshaft control: none, 2 point, continuous**

**SY\_NWSA system constant camshaft control outlet**

**SY\_NWVAR system constant for camshaft configuration**

**SY\_NZUEB system constant engine speed threshold for switching between ignition modes 1+2**

**SY\_PBRPW system constant plausibility check brake/PWG**

**SY\_PGRAD system constant: kind of the phase signal**

**SY\_PGRAD2 system constant: kind of the 2. phase signal**

**SY\_PGRAD3 system constant: kind of the 3. phase signal**

**SY\_PH2OFST system const. offset in syncros between the 2 active phase signals, 2 PGs only**

**SY\_PHTWIN system constant 1/2 phase sensing system (sensor, wheel)**

**SY\_RDE detection of reverse rotation of the engine in project included**

**SY\_REDMX system constant: max. cylinder cutoff step**

**SY\_RLAPP rlsol control during application possible**

**SY\_SGANZ system constant number engine control unit**

**SY\_SLS system constant for engines with secondary air pump**

**SY\_STADAP system constant start adaptation**

**SY\_STERHK system parameter condition stereo downstream catalyst**

**SY\_STERSY System constant Condition stereo Lambda control symmetrical**

**SY\_STERVK system constant condition: stereo exhaust system upstream of cat**

**SY\_SU system constant: version of intake runner length adjuster**

**SY\_SWE\_B system constant for rough road detection using PWM signal from ABS**

**SY\_SWE\_C system constant for rough road detection using CAN**



**SY\_SWE\_S** system constant for rough road detection using engine roughness statistics

**SY\_TEETH** system constant: number of teeth at the crankshaft wheel (gap-teeth included)

**SY\_TFA** configuration for installation position for intake-air sensor

**SY\_TFBA** system constant service device intervention accel. enrichment

**SY\_TFNS** system constant service device intervention afterstart factor

**SY\_TFST** system constant service device intervention start factor

**SY\_TFVA** system constant service device intervention decel. enrichment

**SY\_TFWL** system constant service device intervention warm-up factor

**SY\_TSFSIZE** System constant: Number of values TSF to each fault path

**SY\_TURBO** system constant for exhaust-gas turbocharger

**SY\_TWDKS** system constant: input of desired angle DVE via tester is possible

**SY\_TZW** System constant tester manipulation of zwist included

**SY\_UBR** system constant: Voltage behind main relay ubr exists

**SY\_VS** system constant valve stroke control: no, 2 position

**SY\_WMAX** System constant earliest ignition timing that can be outputted

**SY\_WMIN** System constant latest ignition timing that can be outputted

**SY\_ZAS** system constant cylinder deactivation ZAS included

**SY\_ZNDAUS** System constant ignition timing output (single or double fir.), 1: single, 2: d.

**SY\_ZYLZA** system constant number of cylinders

**SY\_ZZBANK** system constant assignment of cyl. to bank1/bank2, 0 bank1, 1 bank2, binary value

**SY\_ZZBANKB** system const. ass. of cyl. to exhaust bank1/2 for slave1/SGB; 0 b1, 1 b2 binary

**SY\_ZZBANKC** system const. ass. of cyl. to exhaust bank1/2 for slave2/SGC; 0 b1, 1 b2 binary

**SZANSSM1** switching level 1 of afterstart enrichment

**SZANSSM2** switching level 2 of afterstart enrichment

**TADTEAMX** characteristic line for max. duty cycle = F(integral purge flow after TE-Stop)

**TANDT** threshold difference intake air temperature for hot start

**TANDT1** delta threshold intake air temperature for hot start

**TANSELI** intake air temperature calculation, inverse function

**TAPVLTM** threshold soak time for EKP-lead time

**TATEMSN** characteristic line of the PCV duty-cycle depending on the desired mass-flow

**TDLAMBTSTA** delay time to enable nominal Lambda component protection

**TDMFWEMI** filter-time constant at hard fuel cut-in

**TFWDKPN** time constant for filtering DK angle before comp. with subs. value from charging

**THSHKTK** Line for switch off time of lambda sensor heating post cat dep. on temp

**THSHKTK2** ine for switch off time of lambda sensor heating 2 post cat dep. on temp

**THSVKTA** Line of switching off time for lambda sensor heating depending on exh.gas temp

**THSVKTA2** Line of switching off time for lambda sensor heating depending on exh.gas temp 2

**TKOAMNN** minimum shutdown time for air-conditioning compressor

**TKOAMXN** maximum shutdown time for air-conditioning compressor

**TKOBEMNN** Minimum switch-on time for compres. after triggering by B\_kobped or B\_kobwped

**TKODPAMNN** Minimum cut-out time of the air-conditioner compressors during acceleration (dwp

**TKODPAMXN** Maximum cut-out time for compressor cut-out by dwped

**TKOEMNN** minimal time of air-condition compressor beeing swiched on

**TKOWPAMNN** Minimum cut-out time at full load (by wped)

**TKOWPAMXN** Maximum cut-out time at full load (by wped)

**TLRBAM** blocking time for activation LC after BA

**TLRTMS** lock time for CL lambda control after start, depending on engine start temperatu

**TLRVAM** blocking time for activation LC after VA

**TLRZWTMS** Time until hard LC switch on after start (CARB)

**TMDMMAT** Default temperature dependent on parking time during TDTMMA

**TMLFAROF** Engine coolant temperature below which After run is terminated

**TMLRTMS** engine temp. threshold for lambda control depending on cranking temp. tmst

**TMOTELI** engine temperature calculation, inverse function

**TN2FGRGA** double denominator time constant for cruise control

**TNLSGM** Delay time for ECU shut-off

**TSBBVTMS** time delay control readiness after sensor readiness

**TSPERN lock time for p-offset after lambda sensor voltage jump**

**TSPERN2 lock time for p-offset after lambda sensor voltage jump, bank 2**

**TSWKNBGA time to set value correction after acceleration finished**

**TSWKNVGA time to set value correction after deceleration finished**

**TTEVUB Battery-voltage depending delay time of canister purge valve**

**TVFSAM Delay time after DRIVE-position switch off**

**TVFSEM delay time after DRIVE-position switch on**

**TVKTDTK temperature dependant delay time for catalyst monitoring**

**TVKUPHS delay time for clutch switch during shifting in higher gear**

**TVKUPRS delay time for clutch switch during shifting in lower gear**

**TVLADV Integrator time constant at v<sub>last</sub>-calculation**

**TVLLRI delay time to enable I-component after start-up**

**TVLLRPD Maximal delay time to enable PD components after start-up**

**TVNWSTTM delay time : enable of camshaft control after start, depending on engine temp**

**TVSATEM delay time for closing of the PCV after readiness for fuel cut off**

**TVSATM delay time after cranking for fuel cut off**

**TVSLR Duration of LRS downtime commanded via valve stroke control**

**TVSUM delay time for intake manifold switch over in dependence of engine temperatur**

**TVUB voltage correction**

**TWDKSNST time constant for filtering of reference throttle blade position**

**TWDKSV time constant for filtering of reference throttle blade position**

**TWLRTMS waiting time up to check engine temp. signal exceeding threshold for closed loop**

**TWSTT threshold soak time for re-start**

**TZ2FGRGA double numerator time constant for cruise control**

**UDKSNO upper reference voltage threshold for diagnosis knock sensors**

**UDKSNU lower reference voltage threshold for diagnosis knock sensors**

**UEVERG Gear ratio depending of the gear**

**URL2SUNM conversion factor from ps->rl dependent on nmot\_w for active SU (2nd flap)**

**URL3SUNM conversion factor from ps->rl dependent on nmot\_w for active SU (1st + 2nd flap)**

**URLNM conversion factor from ps->rl dependent on nmot\_w**

**URLSUNM conversion factor from ps->rl dependent on nmot\_w for active SU (1st flap)**

**VLMXVZ Max. value for vlast\_w**

**WDKARN threshold throttle angle for activation of the mixture adaptation**

**WDKHKDN High threshold throttle plate for altitude adaptation**

**WDKHKN Low threshold throttle plate for altitude adaptation**

**WDKPMXN maximum throttle angle for plausibility check with charge signal**

**WDKSNLN desired throttle angle at kl15 off**

**WDKUGDN throttle angle necessary for 95 % of the maximum possible air charge**

**WEAN angle injection break off**

**WEEM correction of prestorage angle**

**WEEMRFAN end of injection angle at max relative driver request**

**WEESTATI Offset for injection end angle towards early**

**WEESTM correction of pretiming of injection during start**

**WEESTN end of injection angle during start**

**WFRL fuel wall hang.up**

**WKRLZOF Bloc of fixed values: ignition reatard offset for guided cylinder**

**WPEDKO Accelerator position treshold for the A/C cut off**

**WPFGRBMR Back-calculated pedal value during acceleration with FGR**

**WPHN phase correction**

**WPUAVLN Throttle valve angle as of which VL ambient pressure adaptation is active**

**WPUAVLSN Throttle valve angle as of which VL ambient pressure adaptation is blocked**

**ZATMAML time constant for exhaust gas temperature model**

**ZATMAML2 time constant for exhaust gas temperature model bank2**

**ZATMIKML time constant for modelled temperature in catayst tikatm**

**ZATMIKML2 time constant for modelled temperature in catayst bank 2**

**ZATMKML time constant for catalyst temperature model tkatm**

**ZATMKML2 time constant for catalyst temperature model bank2**

**ZATMRML time constant for exhaust model temperature - pipe temperature**

**ZATMRML2 time constant for exhaust model temperature - pipe temperature bank2**

**ZBALM reduction factor L-memory (tmot) for accel. enrichment**

**ZBTEML integration speed for canister charge adaptation**

**ZDBTMN time constant combustion chamber temperatur model for negativ gradient**

**ZDBTMP time constant combustion chamber temperatur model for positiv gradient**

**ZKFRAOA time constant for frao-integrator, f(number of starts with fuel in oil)**

**ZKFRAUA time constant for frau-integrator, f(number of starts with**

**ZKMSDKT integrator speed for fast constant mass-flow adaption**

**ZKPVDKT integrator speed for slow constant mass-flow adaption**

**ZK RKATA integration speed integrator rkat, f(abo)**

**ZK RKAZA integration speed integrator rkaz, f(abo)**

**ZKTABTU time constant for engine cooling**

**ZLASOHML time constant for PT1-filter of the pseude lambda behind catalyst**

**ZLASOHML2 Time constant for PT1-filter of pseudo lambda post cat, bank 2**

**ZLRHML time constant of lambda control integrator downstream catalyst**

**ZLRHML2 time constant of lambda control integrator downstream catalyst bank 2**

**ZMDNSM time constant for decay of torque offset after cranking**

**ZPVDKR time constant for filtering of pvdkr**

**ZVALM reduction factor L-memory (tmot) for decel. enleanment**

**ZZWEETM Switchover threshold pattern angle**



## Cross reference list

Symbol	Type	Created within	Used within
A0	FW	ARMD ( 531 )	
A1	FW	ARMD ( 531 )	
A2	FW	ARMD ( 531 )	
ABAOVMX	FW	ESUKA ( 711 )	
ABGMSIGH	FW	DLSH ( 330 )	
ABGMSIGV	FW	DLSV ( 301 )	
ABOLRAR	FW	BBBO ( 853 )	
ABOMX	FW	BBBO ( 853 )	
ADCC,T_UM	FW	URADCC (1049)	
ADKATNF	FW	DKAT ( 361 )	
AFNTOL	FW	DMDMIL ( 216 )	
AGRPMN	FW	BGAGR ( 263 )	
AGRPMX	FW	BGAGR ( 263 )	
AHEAGW	FW	DMDMIL ( 216 )	
AHEAGWS	FW	DMDMIL ( 216 )	
AHEARV	FW	DMDMIL ( 216 )	
AHEKA	FW	DMDMIL ( 216 )	
AHEKS	FW	DMDMIL ( 216 )	
AHEKS1	FW	DMDMIL ( 216 )	
AHKATMN	FW	DKAT ( 361 )	
AHKATMX	FW	DKAT ( 361 )	
AHKATS	FW	DKAT ( 361 )	
AHKATSB	FW	DKAT ( 361 )	
AHKTMXT	FW	DKAT ( 361 )	
AHKTTSW	FW	DKAT ( 361 )	
AIMVM	FW	GGVFZG ( 497 )	
AINTKAN	KL	DMDMIL ( 216 )	
ALFO	FW	DMDFON ( 161 )	
AMNUUKA	FW	ESUKA ( 711 )	
ANALUN	KL	DMDLU ( 193 )	
ANRZUEMX	FW	STADAP ( 684 )	
ANWFOHE	FW	DMDFON ( 161 )	
ANWFOST	FW	DMDFON ( 161 )	
ANZDPVK	FW	DLSA ( 398 )	
ANZDYNH	FW	DLSAHK ( 339 )	
ANZEAUS	FW	NLPH ( 150 )	
ANZERDYH	FW	DLSAHK ( 339 )	
ANZERSCH	FW	DLSAHK ( 339 )	
ANZERTV	FW	DLSA ( 398 )	
ANZGEM	FW	DLSV ( 301 )	
ANZRIBEH	FW	GGLSH ( 318 )	
ANZRIBEV	FW	GGLSV ( 382 )	
ANZTP	FW	DLSA ( 398 )	
ANZTPMX	FW	FGRFULO (1160)	
APDTEFRE	FW	DTEV ( 856 )	
APDTEVX	FW	DTEV ( 856 )	
APEKTDX	FW	DKAT ( 361 )	
ASPUUKA	FW	ESUKA ( 711 )	
ATMABKA	KL	ATM ( 20 )	
ATMABKK	KL	ATM ( 20 )	
ATMTANS	KL	ATM ( 20 )	
ATVFETTO	FW	DLSSA ( 350 )	
ATVFETTU	FW	DLSSA ( 350 )	
ATVINI	FW	LRHK ( 781 )	
ATVINI2	FW	LRHK ( 781 )	
ATVMAGO	FW	DLSSA ( 350 )	
ATVMAGU	FW	DLSSA ( 350 )	
ATVMN	FW	LRHK ( 781 )	
ATVMX	FW	LRHK ( 781 )	
AUSGH,T_UM	FW	URMEM (1044)	
AUSG,T_UM	FW	URMEM (1044)	
AUSZH,T_UM	FW	URMEM (1044)	
AUSZ,T_UM	FW	URMEM (1044)	
AVAOVMX	FW	ESUKA ( 711 )	
AVDTEVX	FW	DTEV ( 856 )	
AVKATFS	FW	DKAT ( 361 )	
AVRALU	FW	DMDSTP ( 205 )	
AZKELDYN	KL		KRDY ( 659 )
AZKRLDYN	KL		KRDY ( 659 )
AZKRNDYN	KL		KRDY ( 659 )
AZYTIB	FW	DMDMIL ( 216 )	
B1	FW	ARMD ( 531 )	
B2	FW	ARMD ( 531 )	
BFGRO	FW	FGRABED ( 491 )	
BFGRU	FW	FGRABED ( 491 )	
BMFA	FW	DDG ( 141 )	
BMFMX	FW	DDG ( 141 )	
BOLATZ	FW	CAN (1124)	
BRABEVI	KL	FGRFULO (1160)	
BRATD	FW	FGRFULO (1160)	
BRATU	FW	FGRFULO (1160)	



Symbol	Type	Created within	Used within
BREMS_TJUM	FW	UFFGRE (1096)	
BTRKHTMS	KL	BBKHZ ( 890 )	
BZ_MSR_M	FW	UFMSRC (1080)	
CANINDLY	FW	CAN (1124)	
CBGRLP	FW	BGRLP ( 266 )	
CBUSOFF	FW	CAN (1124)	
CDADLCK	FW	STADAP ( 684 )	
CDAGR	FW	PROKON ( 53 )	
CDAGR1	FW	PROKON ( 53 )	
CDATR	FW	PROKON ( 53 )	
CDATS	FW	PROKON ( 53 )	
CDCCAS	KL	DCAS (1128)	
CDCCINS	KL	DCINS (1126)	
CDCCKUP	KL	DCKUP (1128)	
CDCEV1	KL	DEVE (1017)	
CDCEV2	KL	DEVE (1017)	
CDCEV3	KL	DEVE (1017)	
CDCEV4	KL	DEVE (1017)	
CDCEV5	KL	DEVE (1017)	
CDCEV6	KL	DEVE (1017)	
CDCEV7	KL	DEVE (1017)	
CDCEV8	KL	DEVE (1017)	
CDCFRAO	KL	DKVS ( 811 )	
CDCFRAO2	KL	DKVS ( 811 )	
CDCFRAU	KL	DKVS ( 811 )	
CDCFRAU2	KL	DKVS ( 811 )	
CDCFRST	KL	DKVS ( 811 )	
CDCFRST2	KL	DKVS ( 811 )	
CDCHSH	KL	DHLSHK (1154)	
CDCHSH2	KL	DHLSHK (1154)	
CDCHSV	KL	DHLSVK ( 29 )	
CDCHSV2	KL	DHLSVK ( 29 )	
CDCHSVE	KL	DHLSVKE ( 902 )	
CDCHSVE2	KL	DHLSVKE ( 902 )	
CDCKAT	KL	DKAT ( 361 )	
CDCKAT2	KL	DKAT ( 361 )	
CDCKPE	KL	DEKPE (1020)	
CDCKRNT	KL	DKRNT ( 445 )	
CDCKROF	KL	DKRNT ( 445 )	
CDCKRTP	KL	DKRTP ( 451 )	
CDCKS1	KL	DKRS ( 437 )	
CDCKS2	KL	DKRS ( 437 )	
CDCKS3	KL	DKRS ( 437 )	
CDCKS4	KL	DKRS ( 437 )	
CDCLASH	KL	DLSAHK ( 339 )	
CDCLASH2	KL	DLSAHK ( 339 )	
CDCLATP	KL	DLSA ( 398 )	
CDCLATP2	KL	DLSA ( 398 )	
CDCLATV	KL	DLSA ( 398 )	
CDCLATV2	KL	DLSA ( 398 )	
CDCLSH	KL	DLSH ( 330 )	
CDCLSH2	KL	DLSH ( 330 )	
CDCLUEA	KL	DMLSE ( 34 )	
CDCLUEB	KL	DMLSE ( 34 )	
CDCMD	KL	DMDMIL ( 216 )	
CDCMD00	KL	DMDMIL ( 216 )	
CDCMD01	KL	DMDMIL ( 216 )	
CDCMD02	KL	DMDMIL ( 216 )	
CDCMD03	KL	DMDMIL ( 216 )	
CDCMD04	KL	DMDMIL ( 216 )	
CDCMD05	KL	DMDMIL ( 216 )	
CDCMD06	KL	DMDMIL ( 216 )	
CDCMD07	KL	DMDMIL ( 216 )	
CDCMD08	KL	DMDMIL ( 216 )	
CDCMD09	KL	DMDMIL ( 216 )	
CDCMD10	KL	DMDMIL ( 216 )	
CDCMD11	KL	DMDMIL ( 216 )	
CDCMDB	KL	MDKOG ( 516 )	
CDCMILE	KL	DMILE ( 36 )	
CDCNWKW	KL	DNWKW ( 134 )	
CDCNWKW2	KL	DNWKW ( 134 )	
CDCNWS	KL	DNWS ( 622 )	
CDCNWS2	KL	DNWS ( 622 )	
CDCPH	KL	DPH ( 144 )	
CDCPH2	KL	DPH ( 144 )	
CDCRKAT	KL	DKVS ( 811 )	
CDCRKAT2	KL	DKVS ( 811 )	
CDCRKAZ	KL	DKVS ( 811 )	
CDCRKAZ2	KL	DKVS ( 811 )	
CDCTA	KL	GGTFA ( 298 )	
CDCTES	KL	DTEV ( 856 )	
CDCTEVE	KL	DTEVE (1022)	





Symbol	Type	Created within	Used within
CDCTM	KL	GGTFM ( 289 )	
CDCUB	KL	GGUB ( 487 )	
CDCUF2SG	KL	DUF (1089)	
CDCUFMV	KL	DUF (1089)	
CDCUFSKA	KL	DUF (1089)	
CDCURRAM	KL	DUR (1052)	
CDCURROM	KL	DUR (1052)	
CDCURRST	KL	DUR (1052)	
CDCKUP	KL	DVKUP (1027)	
CDDST	FW	PROKON ( 53 )	
CDFO	FW	DMDFON ( 161 )	
CDHSH	FW	PROKON ( 53 )	
CDHSHE	FW	PROKON ( 53 )	
CDHSV	FW	PROKON ( 53 )	
CDHSVE	FW	PROKON ( 53 )	
CDKAT	FW	PROKON ( 53 )	
CDKATLK	FW	DKAT ( 361 )	
CDKBREMS	FW	GGEGAS ( 474 )	
CDKKAT	FW	DKAT ( 361 )	
CDKKAT2	FW	DKAT ( 361 )	
CDKKS1	FW	DKRS ( 437 )	
CDKKS2	FW	DKRS ( 437 )	
CDKKS3	FW	DKRS ( 437 )	
CDKKS4	FW	DKRS ( 437 )	
CDKLSV2	FW	DLSV ( 301 )	
CDKMDB	FW	MDKOG ( 516 )	
CDKTES	FW	DTEV ( 856 )	
CDKUF2SG	FW	DUF (1089)	
CDKUFMV	FW	DUF (1089)	
CDKUFSKA	FW	DUF (1089)	
CDKURRAM	FW	DUR (1052)	
CDKURROM	FW	DUR (1052)	
CDKURRST	FW	DUR (1052)	
CDKVS	FW	PROKON ( 53 )	
CDLASH	FW	DLSAHK ( 339 ), PROKON ( 53 )	
CDLATP	FW	DLSA ( 398 ), PROKON ( 53 )	
CDLATV	FW	DLSA ( 398 ), PROKON ( 53 )	
CDLDP	FW	PROKON ( 53 )	
CDLFRAO	KL	DKVS ( 811 )	
CDLFRAO2	KL	DKVS ( 811 )	
CDLFRAU	KL	DKVS ( 811 )	
CDLFRAU2	KL	DKVS ( 811 )	
CDLFRST	KL	DKVS ( 811 )	
CDLFRST2	KL	DKVS ( 811 )	
CDLLR	FW	PROKON ( 53 )	
CDLRKAT	KL	DKVS ( 811 )	
CDLRKAT2	KL	DKVS ( 811 )	
CDLRKAZ	KL	DKVS ( 811 )	
CDLRKAZ2	KL	DKVS ( 811 )	
CDLSA	FW	PROKON ( 53 )	
CDLSH	FW	PROKON ( 53 )	
CDLSV	FW	PROKON ( 53 )	
CDMD	FW	DMDUE ( 158 ), PROKON ( 53 )	
CDNWS	FW	PROKON ( 53 )	
CDSL	FW	PROKON ( 53 )	
CDSLSE	FW	PROKON ( 53 )	
CDSWE	FW	PROKON ( 53 )	
CDTANKL	FW	PROKON ( 53 )	
CDTBREMS	FW	GGEGAS ( 474 )	
CDTCAS	FW	DCAS (1128)	
CDTCINS	FW	DCINS (1126)	
CDTCKUP	FW	DCKUP (1128)	
CDTES	FW	PROKON ( 53 )	
CDTEV1	FW	DEVE (1017)	
CDTEV2	FW	DEVE (1017)	
CDTEV3	FW	DEVE (1017)	
CDTEV4	FW	DEVE (1017)	
CDTEV5	FW	DEVE (1017)	
CDTEV6	FW	DEVE (1017)	
CDTEV7	FW	DEVE (1017)	
CDTEV8	FW	DEVE (1017)	
CDTHSH	FW	DHLSHK (1154)	
CDTHSH2	FW	DHLSHK (1154)	
CDTHSV	FW	DHLSVK ( 29 )	
CDTHSV2	FW	DHLSVK ( 29 )	
CDTHSVE	FW	DHLSVKE ( 902 )	
CDTHSVE2	FW	DHLSVKE ( 902 )	
CDTKAT	FW	DKAT ( 361 )	
CDTKAT2	FW	DKAT ( 361 )	
CDTKPE	FW	DEKPE (1020)	
CDTKRNT	FW	DKRNT ( 445 )	
CDTKROF	FW	DKRNT ( 445 )	



Symbol	Type	Created within	Used within
CDTKRTP	FW	DKRTP ( 451 )	
CDTKS1	FW	DKRS ( 437 )	
CDTKS2	FW	DKRS ( 437 )	
CDTKS3	FW	DKRS ( 437 )	
CDTKS4	FW	DKRS ( 437 )	
CDTLASH	FW	DLSAHK ( 339 )	
CDTLASH2	FW	DLSAHK ( 339 )	
CDTLATP	FW	DLSA ( 398 )	
CDTLATP2	FW	DLSA ( 398 )	
CDTLATV	FW	DLSA ( 398 )	
CDTLATV2	FW	DLSA ( 398 )	
CDTLSH	FW	DLSH ( 330 )	
CDTLSH2	FW	DLSH ( 330 )	
CDTLV2	FW	DLSV ( 301 )	
CDTLUEA	FW	DMLSE ( 34 )	
CDTLUEB	FW	DMLSE ( 34 )	
CDTMD	FW	DMDMIL ( 216 )	
CDTMD00	FW	DMDMIL ( 216 )	
CDTMD01	FW	DMDMIL ( 216 )	
CDTMD02	FW	DMDMIL ( 216 )	
CDTMD03	FW	DMDMIL ( 216 )	
CDTMD04	FW	DMDMIL ( 216 )	
CDTMD05	FW	DMDMIL ( 216 )	
CDTMD06	FW	DMDMIL ( 216 )	
CDTMD07	FW	DMDMIL ( 216 )	
CDTMD08	FW	DMDMIL ( 216 )	
CDTMD09	FW	DMDMIL ( 216 )	
CDTMD10	FW	DMDMIL ( 216 )	
CDTMD11	FW	DMDMIL ( 216 )	
CDTMDB	FW	MDKOG ( 516 )	
CDTMILE	FW	DMILE ( 36 )	
CDTNWKW	FW	DNWKW ( 134 )	
CDTNWKW2	FW	DNWKW ( 134 )	
CDTNWS	FW	DNWS ( 622 )	
CDTNWS2	FW	DNWS ( 622 )	
CDTPH	FW	DPH ( 144 )	
CDTPH2	FW	DPH ( 144 )	
CDTTA	FW	GGTFA ( 298 )	
CDTTES	FW	DTEV ( 856 )	
CDTTEVE	FW	DTEVE ( 1022 )	
CDTTM	FW	GGTFM ( 289 )	
CDTUB	FW	GGUB ( 487 )	
CDTUF2SG	FW	DUF ( 1089 )	
CDTUFMV	FW	DUF ( 1089 )	
CDTUFSKA	FW	DUF ( 1089 )	
CDTURRAM	FW	DUR ( 1052 )	
CDTURROM	FW	DUR ( 1052 )	
CDTURRST	FW	DUR ( 1052 )	
CDTVKUP	FW	DVKUP ( 1027 )	
CDWGANG	FW	KOS ( 896 )	
CDWGANGB	FW	KOS ( 896 )	
CDWKOB	FW	KOS ( 896 )	
CDWVERAD	FW	MDVERAD ( 549 )	
CFRA	FW	LR ( 768 )	
CIDATV	FW	DLSA ( 398 )	
CIDATV2	FW	DLSA ( 398 )	
CIDLSCHE	FW	DLSAHK ( 339 )	
CIDLSCHE2	FW	DLSAHK ( 339 )	
CIDLSDY	FW	DLSAHK ( 339 )	
CIDLSDY2	FW	DLSAHK ( 339 )	
CIDSHKF	FW	DLSAHK ( 339 )	
CIDSHKF2	FW	DLSAHK ( 339 )	
CIDSHKM	FW	DLSAHK ( 339 )	
CIDSHKM2	FW	DLSAHK ( 339 )	
CIDTP	FW	DLSA ( 398 )	
CIDTP2	FW	DLSA ( 398 )	
CLABREMS	FW	GGEGAS ( 474 )	
CLACAS	FW	DCAS ( 1128 )	
CLACINS	FW	DCINS ( 1126 )	
CLACKUP	FW	DCKUP ( 1128 )	
CLAEV1	FW	DEVE ( 1017 )	
CLAEV2	FW	DEVE ( 1017 )	
CLAEV3	FW	DEVE ( 1017 )	
CLAEV4	FW	DEVE ( 1017 )	
CLAEV5	FW	DEVE ( 1017 )	
CLAEV6	FW	DEVE ( 1017 )	
CLAEV7	FW	DEVE ( 1017 )	
CLAEV8	FW	DEVE ( 1017 )	
CLAHSH	FW	DHLSHK ( 1154 )	
CLAHSH2	FW	DHLSHK ( 1154 )	
CLAHSV	FW	DHLSVK ( 29 )	
CLAHSV2	FW	DHLSVK ( 29 )	



Symbol	Type	Created within	Used within
CLAHSV	FW	DHLSVKE ( 902 )	
CLAHSV2	FW	DHLSVKE ( 902 )	
CLAKAT	FW	DKAT ( 361 )	
CLAKAT2	FW	DKAT ( 361 )	
CLAKPE	FW	DEKPE ( 1020 )	
CLAKRNT	FW	DKRNT ( 445 )	
CLAKROF	FW	DKRNT ( 445 )	
CLAKRTP	FW	DKRTP ( 451 )	
CLAKS1	FW	DKRS ( 437 )	
CLAKS2	FW	DKRS ( 437 )	
CLAKS3	FW	DKRS ( 437 )	
CLAKS4	FW	DKRS ( 437 )	
CLALASH	FW	DLSAHK ( 339 )	
CLALASH2	FW	DLSAHK ( 339 )	
CLALATP	FW	DLSA ( 398 )	
CLALATP2	FW	DLSA ( 398 )	
CLALATV	FW	DLSA ( 398 )	
CLALATV2	FW	DLSA ( 398 )	
CLALSH	FW	DLSH ( 330 )	
CLALSH2	FW	DLSH ( 330 )	
CLALSV2	FW	DLSV ( 301 )	
CLAMDB	FW	MDKOG ( 516 )	
CLAMILE	FW	DMILE ( 36 )	
CLANWKW	FW	DNWKW ( 134 )	
CLANWKW2	FW	DNWKW ( 134 )	
CLANWS	FW	DNWS ( 622 )	
CLANWS2	FW	DNWS ( 622 )	
CLAPH	FW	DPH ( 144 )	
CLAPH2	FW	DPH ( 144 )	
CLATA	FW	GGTFA ( 298 )	
CLATES	FW	DTEV ( 856 )	
CLATEVE	FW	DTEVE ( 1022 )	
CLATM	FW	GGTFM ( 289 )	
CLAUB	FW	GGUB ( 487 )	
CLAUF2SG	FW	DUF ( 1089 )	
CLAUFMV	FW	DUF ( 1089 )	
CLAUFSKA	FW	DUF ( 1089 )	
CLAURRAM	FW	DUR ( 1052 )	
CLAURROM	FW	DUR ( 1052 )	
CLAURRST	FW	DUR ( 1052 )	
CLAVKUP	FW	DVKUP ( 1027 )	
CLRHK	FW	LRHK ( 781 )	
CLRHKA	FW	LRHK ( 781 )	
CLRKA	FW	LRKA ( 795 )	
CLRMSFS	FW	LREB ( 739 )	
CLRVS	FW	LREB ( 739 )	
CLRZWTMS	FW	LREB ( 739 )	
CMUTE	FW	CAN ( 1124 )	
CNFKUPPL	FW	LLRBB ( 575 )	
CNLLR2SG	FW	DLLR ( 578 )	
CNLLRNS	FW	LLRNS ( 562 )	
CNFMDVER	FW	MDVER ( 546 )	
CNFSL	FW	MDVERB ( 540 )	
CNMDV2SG	FW	MDVERB ( 540 )	
CPLRA	FW	DKVS ( 811 )	
CREDSTU	FW	MDRED ( 976 )	
CSCATT	FW	PROKON ( 53 )	
CSU	FW	SU ( 617 )	
CUKA	FW	ESUKA ( 711 )	
CWALE	FW	ALE ( 136 )	
CWARMD	FW	ARMD ( 531 )	
CWBGSRM	FW	BGSRM ( 245 )	
CWBGWPFGR	FW	BGWPFGR ( 548 )	
CWBWEEN	FW	GGPED ( 454 )	
CWCAN	FW	CAN ( 1124 )	
CWDEGFE	FW	DEGFE ( 592 )	
CWDHFM	FW	DHFM ( 233 )	
CWDKRNT	FW	DKRNT ( 445 )	
CWDKROF	FW	DKRNT ( 445 )	
CWDKRTP	FW	DKRTP ( 451 )	GGKS ( 412 )
CWDKS1	FW	DKRS ( 437 )	
CWDKS2	FW	DKRS ( 437 )	
CWDKS3	FW	DKRS ( 437 )	
CWDKS4	FW	DKRS ( 437 )	
CWDLSA	FW	DLSA ( 398 )	
CWDLSAHK	FW	DLSAHK ( 339 )	
CWDMDE	FW	DMDMIL ( 216 )	
CWDMFAB	FW	MDFAW ( 508 )	
CWDSS	FW	BGPU ( 276 )	
CWDTEAPP	FW	DTEV ( 856 )	
CWDVEFO	FW	BGDVE ( 934 )	
CWDVMX	FW	VMAXMD ( 588 )	



Symbol	Type	Created within	Used within
CWERFIL	FW	PROKON ( 53 ), TCSORT (1122)	
CWESWEZ	FW	ACIFI (1013)	
CWEVAB	FW	AEVAB ( 980 )	
CWFGRABED	FW	FGRABED ( 491 )	
CWFGRFULO	FW	FGRFULO (1160)	
CWFGRGA	FW	FGRABED ( 491 )	
CWFGRRGL	FW	FGRREGL (1174)	
CWFKMSDKA	FW	BGMSZS ( 239 )	
CWFUEDK	FW	FUEDK ( 597 )	
CWFUEREK	FW	FUEREK ( 595 )	
CWGGEGAS	FW	GGEGAS ( 474 )	
CWGGFST	FW	GGFST ( 502 )	
CWGGLSH	FW	GGLSH ( 318 )	
CWGGLSV	FW	GGLSV ( 382 )	
CWGGVFZG	FW	GGVFZG ( 497 )	
CWKATUM	FW	DKAT ( 361 )	
CWKHMD	FW	KHMD ( 894 )	
CWKHZ	FW	BBKHZ ( 890 )	
CWKHZW	FW	ZWMIN ( 669 )	
CWKLIMA	FW	PROKON ( 53 )	
CWKMMILSCT	FW	TC1MOD (1100)	
CWKOGANG	FW	KOS ( 896 )	
CWKONABG	FW	PROKON ( 53 )	
CWKONFZ1	FW	PROKON ( 53 )	
CWKONLS	FW	PROKON ( 53 )	
CWKR	FW	KRDY ( 659 )	
CWKRAPP	FW	GGKS ( 412 )	
CWKRNLK	FW	KRRA ( 639 )	
CWKRREF	FW	KRKE ( 427 )	
CWKUPPL	FW	LLRMR ( 572 )	
CWLFD	FW	LFS ( 69 )	
CWLLRPA	FW	LLRRM ( 566 )	
CWLRSYNC	FW	LR ( 768 )	
CWLSHA	FW	DLSAHK ( 339 )	
CWMDAPP	FW	NWS ( 618 ), PROKON ( 53 )	
CWMDKOG	FW		MDKOG ( 516 )
CWMDKOL	FW	MDKOL ( 526 )	
CWMDRLKO	FW	MDVERB ( 540 )	
CWNLPH	FW	NLPH ( 150 )	
CWNOMIL	FW	DMIL (1150)	
CWNSTAT	FW	LLRNS ( 562 )	
CWNWGE	FW	NWS ( 618 )	
CWNWLL	FW	NWS ( 618 )	
CWNWREF	FW	GGDPG ( 74 )	
CWNWS	FW	NWS ( 618 )	
CWOBD	FW	PROKON ( 53 ), TC1MOD (1100)	
CWPKAPP	FW	AES ( 973 )	
CWPUA	FW	BGPU ( 276 )	
CWREFI	FW	KRKE ( 427 )	
CWRLAPPL	FW	MDFUE ( 594 )	FUEDK ( 597 )
CWSAWE	FW	BBSAWE ( 557 )	
CWSCTMDE	FW	SCATT (1097)	
CWSTPCNF	FW	DMDSTP ( 205 )	
CWTEMPK	FW	BGTEMPK ( 252 )	
CWTEZW	FW		MDKOG ( 516 )
CWTF	FW	PROKON ( 53 )	
CWTIPIN	FW	KRDY ( 659 )	
CWTUM	FW	MDVERB ( 540 )	
CWUHR	FW	PROKON ( 53 )	
CWVSV	FW	VS_VERST ( 67 )	
CWVWKNWS	FW	ESVW (1009)	
CWWDKSPE	FW	FUEDKSA ( 610 )	
CWWL	FW		ESSTT ( 679 ), GK ( 675 )
CWZWVMX	FW		MDKOG ( 516 )
CW_AZUE	FW	AZUE ( 904 )	
CW_FUBND	FW	ZUESZ ( 632 )	
DANTGESWNV	FW	ADVE ( 918 )	
DANTGESWV	FW	ADVE ( 918 )	
DANTSCHWNV	FW	ADVE ( 918 )	
DANTSCHWV	FW	ADVE ( 918 )	
DASA	FW	DLLR ( 578 )	
DBZ_MN_UM	FW	UFMSRC (1080)	
DBZ_MX_UM	FW	UFMSRC (1080)	
DDFDTEAB	FW	DTEV ( 856 )	
DECKSTAI	KL	STADAP ( 684 )	
DEVTMAGR	KL	BGTEMPK ( 252 )	
DFAFRG	FW	FUEREK ( 595 )	
DFKMSMN	FW	BGMSZS ( 239 )	
DFKMSMX	FW	BGMSZS ( 239 )	
DFKPMN	FW	BGMSZS ( 239 )	
DFKPMX	FW	BGMSZS ( 239 )	
DFPSLBIT	KWB	D2CTR ( 496 )	



Symbol	Type	Created within	Used within
DFRBAF	FW	ESUKA ( 711 )	
DFRBAM	FW	ESUKA ( 711 )	
DFRMDTEE	FW	DTEV ( 856 )	
DFRMDTEF	FW	DTEV ( 856 )	
DFRMDTEM	FW	DTEV ( 856 )	
DFRMN	FW	LR ( 768 )	
DFRMST	FW	DKVS ( 811 )	
DFRSPS	FW	LR ( 768 )	
DFRVAF	FW	ESUKA ( 711 )	
DFRVAM	FW	ESUKA ( 711 )	
DFSEFO2N	KL	DMDFON ( 161 )	
DFSEFON	KL	DMDFON ( 161 )	
DFSERES	FW	DMDFON ( 161 )	
DFTEAHB	FW	TEB ( 826 )	
DFTEDS	FW	BBTEGA ( 750 )	
DKATCW	FW	DKAT ( 361 )	
DKLAGERT	FW	ADVE ( 918 )	
DKNOTBEGR	KL	FUEDKSA ( 610 )	
DKPSTGMIN	FW	BGDVE ( 934 )	
DKROFN	KL	DKRNT ( 445 )	
DKROKD	FW	DKRNT ( 445 ), GGKS ( 412 )	
DKROKMX	FW	GGKS ( 412 )	
DKROKO	FW	GGKS ( 412 )	
DKROKU	FW	DKRNT ( 445 )	
DLAHISATO	FW	DLSSA ( 350 )	
DLAHISATU	FW	DLSSA ( 350 )	
DLAMELSH	FW	DLSH ( 330 )	
DLAMLASHF	FW	DLSAHK ( 339 )	
DLAMLASHM	FW	DLSAHK ( 339 )	
DLAMOB	KL	LAMFAW ( 728 )	
DLBTS	KL	LAMBTS ( 732 )	
DLRDWDKSS1	FW	ADVE ( 918 )	
DLRDWDKSS2	FW	ADVE ( 918 )	
DLRIAMAXA	FW	ADVE ( 918 )	
DLRIKLPAR	FW	ADVE ( 918 )	
DLRININI	FW	ADVE ( 918 )	
DLRKDONLP0	FW	ADVE ( 918 )	
DLRKDUNLP0	FW	ADVE ( 918 )	
DLRKDUNLP1	FW	ADVE ( 918 )	
DLRKDUNLP2	FW	ADVE ( 918 )	
DLRKIONLP0	KL	ADVE ( 918 )	
DLRKIUINLP0	KL	ADVE ( 918 )	
DLRKIUINLP1	KL	ADVE ( 918 )	
DLRKIUINLP2	KL	ADVE ( 918 )	
DLRKPONLP0	FW	ADVE ( 918 )	
DLRKPUNLP0	FW	ADVE ( 918 )	
DLRKPUNLP1	FW	ADVE ( 918 )	
DLRKPUNLP2	FW	ADVE ( 918 )	
DLRKREIS	FW	ADVE ( 918 )	
DLRKREISST	FW	ADVE ( 918 )	
DLRNLPD	FW	ADVE ( 918 )	
DLRPERIMN	FW	LR ( 768 )	
DLRPERIMX	FW	LR ( 768 )	
DLRPID0T	FW	ADVE ( 918 )	
DLRPID1T	FW	ADVE ( 918 )	
DLRPID2T	FW	ADVE ( 918 )	
DLRPIDMAX	FW	ADVE ( 918 )	
DLRPIDMIN	FW	ADVE ( 918 )	
DLRPIDSTMN	FW	BGDVE ( 934 )	
DLRUBSOLL	FW	ADVE ( 918 )	
DLRUMABAND	FW	ADVE ( 918 )	
DLRUMAIINI	FW	ADVE ( 918 )	
DLURMIN	KL	DMDDLJ ( 199 )	
DMADFK	FW	MDVERAD ( 549 )	
DMADFS	FW	MDVERAD ( 549 )	
DMADKO	FW	MDVERAD ( 549 )	
DMADLL	FW	MDVERAD ( 549 )	
DMADMNFK	FW	MDVERAD ( 549 )	
DMADMNFS	FW	MDVERAD ( 549 )	
DMADMNKO	FW	MDVERAD ( 549 )	
DMADMNLL	FW	MDVERAD ( 549 )	
DMADMXFK	FW	MDVERAD ( 549 )	
DMADMXFS	FW	MDVERAD ( 549 )	
DMADMXKO	FW	MDVERAD ( 549 )	
DMADMXLL	FW	MDVERAD ( 549 )	
DMAUFN	KL	MDZW ( 636 )	
DMDDLWS	KL	MDVERB ( 540 )	
DMDGENAB	FW	MDVERB ( 540 )	
DMDLWS	KL	MDVERB ( 540 )	
DMDNSM	KL	MDVER ( 546 )	
DMDPUG	KL	MDFAW ( 508 )	
DMEBZ_MX	FW	UFMER ( 1060 )	



Symbol	Type	Created within	Used within
DMIFLSD	FW	MDFAW ( 508 )	
DMIGSL	FW	CAN ( 1124 )	
DMIVV	FW	CAN ( 1124 )	
DMLDTEFN	FW	DTEV ( 856 )	
DMLDTEFX	FW	DTEV ( 856 )	
DMLDTEMN	FW	DTEV ( 856 )	
DMLDTEMX	FW	DTEV ( 856 )	
DMLLNG	KL	LLRRM ( 566 )	
DMLLNGV	KL	LLRRM ( 566 )	
DMLLRMNN	KL	LLRRM ( 566 )	
DMLLRLMXN	KL	LLRRM ( 566 )	
DMLLRMNN	KL	LLRRM ( 566 )	
DMLLRMXN	KL	LLRRM ( 566 )	
DMLSDUG	KL	MDFAW ( 508 )	
DMRESLL	FW	LLRMR ( 572 )	
DMRESTM	FW	LLRMR ( 572 )	
DMRFAWE	FW	MDFAW ( 508 )	
DMRIFW	KL	FGRREGL ( 1174 )	
DMRKT	FW	DKAT ( 361 )	
DMRLASH	FW	DLSAHK ( 339 )	
DMRLSH	FW	DLSH ( 330 )	
DMSNTEMN	FW	DTEV ( 856 )	
DMSNTEMX	FW	DTEV ( 856 )	
DMSTES	KL	TEB ( 826 )	
DMVERLMN	FW	MDVER ( 546 )	
DMVTEVDO	FW	DTEV ( 856 )	
DMXRDL	FW	DMDLU ( 199 )	
DMXRFL	FW	DMDLUA ( 202 )	
DMXRLU	FW	DMDLU ( 193 )	
DN10BURN	FW	ESSTT ( 679 )	
DNABW	FW	RDE ( 112 )	
DNBURN	KL	STADAP ( 684 )	
DNDLLRO	FW	DLLR ( 578 )	
DNDLLRU	FW	DLLR ( 578 )	
DNDTEO	FW	DTEV ( 856 )	
DNDTEU	FW	DTEV ( 856 )	
DNFGRMX	FW	FGRABED ( 491 )	
DNFILO	FW	ARMD ( 531 )	
DNKH	FW	BBKHZ ( 890 )	
DNLLR	FW	LLRBB ( 575 )	
DNLLRES	FW	LLRMR ( 572 )	
DNLLRIST	FW	LLRRM ( 566 )	
DNLLST	FW	LLRRM ( 566 )	
DNMAX	FW	NMAXMD ( 584 )	
DNMAXDZ	FW	NMAXMD ( 584 )	
DNMAXH	FW		NMAXMD ( 584 )
DNMNI	FW	LLRRM ( 566 )	
DNSAH	FW	BBSAWE ( 557 )	
DNSAL	FW	BBSAWE ( 557 )	
DNSATIP	FW	BBSAWE ( 557 )	
DNSLL	FW	BBSAWE ( 557 )	
DNSNFST	FW	LLRNS ( 562 )	
DNSNFX	FW	LLRNS ( 562 )	
DNTIPDYN	FW	ZWMIN ( 669 )	
DNVSA	FW	BBSAWE ( 557 )	
DNWEELLS	FW	BBSAWE ( 557 )	
DNWEK	FW	BBSAWE ( 557 )	
DPDSTI	FW	DDST ( 851 )	
DPDSTO	FW	DDST ( 851 )	
DPTEMN	FW	DDST ( 851 )	
DPTEMX	FW	DDST ( 851 )	
DPUPS	FW	FUEDK ( 597 )	
DPUPVDK	KL	BGPU ( 276 )	
DRISIGH	FW	DLSH ( 330 )	
DRISIGV	FW	DLSV ( 301 )	
DRLDYNU	FW	BGRLP ( 266 )	
DRLKTD	FW	DKAT ( 361 )	
DRLKTDPT	FW	DKAT ( 361 )	
DRLMIN	FW	BGRLP ( 266 )	
DRLMINDP	FW	MDFAW ( 508 )	
DRLSOLA	KL	DMDSTP ( 205 )	
DRLSOLMF	FW	FUEDK ( 597 )	
DRLSPMN	FW	ESUKA ( 711 )	
DSTEMIN	FW	TEB ( 826 )	
DSTGRAD	FW	GGDST ( 504 )	
DSTOFFS	FW	GGDST ( 504 )	
DTABUNPL	FW	BGTABST ( 1030 )	
DTAHL	FW	LLRNS ( 562 )	
DTEPRU	FW	BGRLP ( 266 )	
DTKATMN	FW	BBKHZ ( 890 )	
DTKH	FW	BBKHZ ( 890 )	
DTLRTML	KL	GGTFM ( 289 )	



Symbol	Type	Created within	Used within
DTMDMA	FW	GGTFM ( 289 )	
DTMDNPO	FW	GGTFM ( 289 )	
DTMHLL	FW	LLRNS ( 562 )	
DTMLF	FW	LFS ( 69 )	
DTMR	FW	LREB ( 739 )	
DTMSRT	FW	GGTFM ( 289 )	
DTMTMRW	FW	LREB ( 739 )	
DTMWUC	FW	DWUC ( 1147 )	
DTUMTA	FW	BGTABST ( 1030 )	
DTUMTAT	FW	ATM ( 20 )	
DTVKAML	KL	LRKA ( 795 )	
DTVKAML2	KL	LRKA ( 795 )	
DUBLBZ	FW	BGLBZ ( 489 )	
DUDKNLPO	FW	BGDVE ( 934 )	
DUDKNLPU	FW	BGDVE ( 934 )	
DUDKP1HY	FW	BGDVE ( 934 ), GGDVE ( 477 )	
DUDKPTMP	FW	BGDVE ( 934 )	
DUF_T	FW	DUF ( 1089 )	
DUKK	FW	ESUK ( 699 )	
DUPW12	FW	GGPED ( 454 )	
DUPW12BE	FW	GGPED ( 454 )	
DUPW12TG	FW	GGPED ( 454 )	
DUPW12VG	FW	GGPED ( 454 )	
DUPWGHY	FW	GGPED ( 454 )	
DUSRIH	FW	GGLSH ( 318 )	
DUSRIV	FW	GGLSV ( 382 )	
DUSSPH	FW	GGLSH ( 318 )	
DUSSPV	FW	GGLSV ( 382 )	
DVEEST	FW	ADVE ( 918 )	
DVFZAR	FW	ARMD ( 531 )	
DVFZBEG	FW	GGVFZG ( 497 )	
DVIVZMX	FW	FGRABED ( 491 )	
DVIVZTMX	FW	FGRFULO ( 1160 )	
DVLLVO	FW	FGRREGL ( 1174 )	
DVLLVU	FW	FGRREGL ( 1174 )	
DVNG	KL	LLRRM ( 566 )	
DVNGV	KL	LLRRM ( 566 )	
DVSA	FW	BBSAWE ( 557 )	
DVSAVO	FW	FGRREGL ( 1174 )	
DVSAVU	FW	FGRREGL ( 1174 )	
DVSKNBGA	KL	FGRFULO ( 1160 )	
DVSKNVGA	KL	FGRFULO ( 1160 )	
DVTIPUD	FW	FGRFULO ( 1160 )	
DVZVIMX	FW	FGRABED ( 491 )	
DVZVITMX	FW	FGRFULO ( 1160 )	
DVZVIWA	FW	FGRFULO ( 1160 )	
DWDK12O	FW	GGDVE ( 477 )	
DWDK13O	FW	GGDVE ( 477 )	
DWDK23O	FW	GGDVE ( 477 )	
DWDKSIKLS	FW	ADVE ( 918 )	
DWEEMX	FW	ESVW ( 1009 )	
DWKRMSN	KL	KRRA ( 639 )	
DWNWEMXT	FW	NWS ( 618 )	
DWPEDKOB	FW	KOS ( 896 )	
DWPMXNB	FW	GGPED ( 454 )	
DWPMXNOT	FW	GGPED ( 454 )	
DWPR	FW	BGRLP ( 266 )	
DWPRNSP	FW	BGRLP ( 266 )	
DYADMX	FW	KRDY ( 659 )	
DYADS	FW	KRDY ( 659 )	
DYAFVS	FW	KRDY ( 659 )	
DYAMNV	FW	KRDY ( 659 )	
DYAVF	FW	KRDY ( 659 )	
DYNLSUTO	FW	DLSSA ( 350 )	
DYNLSUTU	FW	DLSSA ( 350 )	
DYNMXNL	FW	NLDG ( 157 )	
DZWAML	KL	ZWMIN ( 669 )	
DZWDYN	KL	ZWMIN ( 669 )	
DZWETA	KL	MDZW ( 636 )	
DZWMNSTN	KL	ZWMIN ( 669 )	
DZWNWSUE	KL	MDBAS ( 529 ), ZWGRU ( 634 )	
DZWOAGR	KL	MDBAS ( 529 )	
DZWOLA	KL	MDBAS ( 529 )	
DZWOM	KL	MDBAS ( 529 )	
DZWSPM	KL	ZWMIN ( 669 )	
DZWSTTA	KL	ZWSTT ( 637 )	
DZWTIN	KL		KRDY ( 659 )
DZZST	FW	GGDPG ( 74 )	
DZZST2	FW	GGDPG ( 74 )	
DZZSTNLP	FW	GGDPG ( 74 )	
EFFDFPM	KL	DFRZ ( 1144 )	
ENSAKHG	FW	BBSAWE ( 557 )	



Symbol	Type	Created within	Used within
ENTDKLL	FW	FUEDKSA ( 610 )	
ENTDKNLL	FW	FUEDKSA ( 610 )	
ESKONF	FW	DEKON ( 64 )	
ETADZW	KL	LAMBTS ( 732 ), MDIST ( 528 ), MDBAS ( 529 ) ZWMIN ( 669 )	
ETALAM	KL	MDBAS ( 529 )	
ETAZWTEEN	FW	DTEV ( 856 )	
EVTMODMNDK	FW	FUEDK ( 597 )	
EVTMODO	KL	BGTEMPK ( 252 )	
FABMDWA	KL	MDWAN ( 554 )	
FABSALU	FW	DSWEC ( 32 )	
FABSTT	KL	GGTFM ( 289 )	
FAINTEN	FW	DMDMIL ( 216 )	
FAKTABGM	FW	BGTEMPK ( 252 )	
FALRKTD	FW	DKAT ( 361 )	
FALRKTT	FW	DKAT ( 361 )	
FASKIV1	FW	DMDMIL ( 216 )	
FATMRML	KL	ATM ( 20 )	
FATMRML2	KL	ATM ( 20 )	
FA_CALID	TX	TC9MOD (1121)	
FBFGRSFW	KL	FGRFULO (1160)	
FBTEB	KL	TEB ( 826 )	
FBTEVA	KL	TEB ( 826 )	
FBZBTEML	KL	TEB ( 826 )	
FBZFRAT	KL	LRA ( 797 )	
FDDN	KL	LLRRM ( 566 )	
FDNIKOR	FW	LLRRM ( 566 )	
FDVAGR	KL	BGAGR ( 263 )	
FDVANS	KL	BGTEMPK ( 252 )	
FETATEBN	KL	TEB ( 826 )	
FFLDZ	KL	ZUESZ ( 632 )	
FFRITMS	KL	LR ( 768 )	
FFTCAS	KL	DCAS (1128)	
FFTCINS	KL	DCINS (1126)	
FFTCKUP	KL	DCKUP (1128)	
FFTEV1	KL	DEVE (1017)	
FFTEV2	KL	DEVE (1017)	
FFTEV3	KL	DEVE (1017)	
FFTEV4	KL	DEVE (1017)	
FFTEV5	KL	DEVE (1017)	
FFTEV6	KL	DEVE (1017)	
FFTEV7	KL	DEVE (1017)	
FFTEV8	KL	DEVE (1017)	
FFTHSH	KL	DHLSHK (1154)	
FFTHSH2	KL	DHLSHK (1154)	
FFTHSV	KL	DHLSVK ( 29 )	
FFTHSV2	KL	DHLSVK ( 29 )	
FFTHSVE	KL	DHLSVKE ( 902 )	
FFTHSVE2	KL	DHLSVKE ( 902 )	
FFTKPE	KL	DEKPE (1020)	
FFTKRNT	KL	DKRNT ( 445 )	
FFTKROF	KL	DKRNT ( 445 )	
FFTKRTP	KL	DKRTP ( 451 )	
FFTKS1	KL	DKRS ( 437 )	
FFTKS2	KL	DKRS ( 437 )	
FFTKS3	KL	DKRS ( 437 )	
FFTKS4	KL	DKRS ( 437 )	
FFTLASH	KL	DLSAHK ( 339 )	
FFTLASH2	KL	DLSAHK ( 339 )	
FFTLATP	KL	DLSA ( 398 )	
FFTLATP2	KL	DLSA ( 398 )	
FFTLATV	KL	DLSA ( 398 )	
FFTLATV2	KL	DLSA ( 398 )	
FFTLSH	KL	DLSH ( 330 )	
FFTLSH2	KL	DLSH ( 330 )	
FFTMDB	KL	MDKOG ( 516 )	
FFTMILE	KL	DMILE ( 36 )	
FFTNWKW	KL	DNWKW ( 134 )	
FFTNWKW2	KL	DNWKW ( 134 )	
FFTNWS	KL	DNWS ( 622 )	
FFTNWS2	KL	DNWS ( 622 )	
FFTPH	KL	DPH ( 144 )	
FFTPH2	KL	DPH ( 144 )	
FFTTA	KL	GGTFA ( 298 )	
FFTTES	KL	DTEV ( 856 )	
FFTTEVE	KL	DTEVE (1022)	
FFTTM	KL	GGTFM ( 289 )	
FFTUB	KL	GGUB ( 487 )	
FFTUF2SG	KL	DUF (1089)	
FFTUFMV	KL	DUF (1089)	
FFTUFSKA	KL	DUF (1089)	
FFTURRAM	KL	DUR (1052)	
FFTURROM	KL	DUR (1052)	





Symbol	Type	Created within	Used within
FFTURRST	KL	DUR (1052)	
FFTVKUP	KL	DVKUP (1027)	
FFWEKA	FW	LRKA (795)	
FHDLLR	FW	DLLR (578)	
FHODTEA	FW	DTEV (856)	
FHOKH	FW	BBKHZ (890)	
FHOKOB	FW	KOS (896)	
FHOMN	FW	BGPU (276)	
FHOMX	FW	BGPU (276)	
FHSTT	KL	ESSTT (679)	
FIAMALU	FW	DMDLU (193)	
FIBSALU	FW	DSWEC (32)	
FIMALU	FW	DMDLU (193)	
FIMHU	KL	ESWE (698)	
FIMWU	KL	ESWE (698)	
FIRNLIGN	FW	NLDG (157)	
FKADPMN	FW	DTEV (856)	
FKATEB	KL	TEB (826)	
FKAXAVKAT	KL	LRKA (795)	
FKDISA	KL	BGPU (276)	
FKEFMC	FW	KRKE (427)	
FKELDY	FW	KRKE (427)	
FKELDYA	FW	KRDY (659)	
FKENDY	FW	KRKE (427)	
FKHABMN	FW	BBKHZ (890)	
FKHLA	KL	BBKHZ (890)	
FKHMD	KL	BBKHZ (890)	
FKKVS	KF	RKT1 (979)	
FKMSDKMN	FW	BGMSZS (239)	
FKMSDKMX	FW	BGMSZS (239)	
FKMSHFM	FW	GGHFM (230)	
FKPVDKMN	FW	BGMSZS (239)	
FKPVDKMX	FW	BGMSZS (239)	
FKRFTPFMC	FW	KRKE (427)	
FKSTT	KL	ESSTT (679)	
FLCCAS	FW	DCAS (1128)	
FLCCINS	FW	DCINS (1126)	
FLCCKUP	FW	DCKUP (1128)	
FLCLUJA	FW	DMLSE (34)	
FLCLUJEB	FW	DMLSE (34)	
FLFO	FW	DMDFON (161)	
FLMLKAMA	FW	LRKA (795)	
FLMLKAPR	FW	LRKA (795)	
FLRAWG	KL	ARMD (531)	
FLRFKATE	KL	LR (768)	
FLRHG	KL	ARMD (531)	
FLRM	KL	LR (768)	
FLUTN	KL	DMDLUA (202)	
FLUV1	FW	DMDLU (193)	
FLUV2	FW	DMDLU (193)	
FMDGENTA	KL	MDVERB (540)	
FMDKHFH	KL	KHMD (894)	
FMDKHTM	KL	KHMD (894)	
FMDWAT	KL	MDWAN (554)	
FMFKRB0	FW	GGKS (412)	
FMFKRB1	FW	GGKS (412)	
FMFKRB2	FW	GGKS (412)	
FMFKRB3	FW	GGKS (412)	
FMIUGDS	FW	FUEDK (597)	
FMIVL	FW	MDMAX (514)	
FMLKAMA	FW	LRKA (795)	
FNLMI0	FW	NLDG (157)	
FNLMI1	FW	NLDG (157)	
FNLMI2	FW	NLDG (157)	
FNRAD	FW	MDWAN (554)	
FNSHO	KL	ESNSWL (691)	
FNSNF	FW	LLRNS (562)	
FNSSM	KL	ESNSWL (691)	
FNSSTKM	KL	LLRNS (562)	
FNSSTM	KL	LLRNS (562)	
FNSTABNV	KL	MDNSTAB (556)	
FPLMRM	KL	FUEREG (595)	
FPRAT	FW	BGDVE (934)	
FPRMT	FW	BGDVE (934)	
FPRNMAX	FW	BGDVE (934)	
FPRTIM1_T	FW	BGDVE (934)	
FPRTIM2_T	FW	BGDVE (934)	
FPRTIM3_T	FW	BGDVE (934)	
FPRTIM4_T	FW	BGDVE (934)	
FPVDKE	FW	BGPU (276)	
FPVDKMN	FW	BGPU (276)	
FPVDKMX	FW	BGPU (276)	



Symbol	Type	Created within	Used within
FPVMXN2	KL	BGSRM ( 245 )	
FPVMXP	FW	BGRLP ( 266 )	
FPWDKAPP	KL	FUEDK ( 597 )	
FQTEDL	KL	TEB ( 826 )	
FQTEFR	KL	TEB ( 826 )	
FQTEPT	KL	TEB ( 826 )	
FQTEVA	KL	TEB ( 826 )	
FRAE	FW	DKVS ( 811 )	
FRAODN	FW	DKVS ( 811 )	
FRAODX	FW	DKVS ( 811 )	
FRAOMN	FW	LRA ( 797 )	
FRAOMX	FW	LRA ( 797 )	
FRAORN	FW	LRA ( 797 )	
FRAORX	FW	LRA ( 797 )	
FRARAWG	KL	ARMD ( 531 )	
FRARHG	KL	ARMD ( 531 )	
FRATMN	FW	LRA ( 797 )	
FRATMX	FW	LRA ( 797 )	
FRAUDN	FW	DKVS ( 811 )	
FRAUDX	FW	DKVS ( 811 )	
FRAUMN	FW	LRA ( 797 )	
FRAUMX	FW	LRA ( 797 )	
FRAURN	FW	LRA ( 797 )	
FRAURX	FW	LRA ( 797 )	
FRHB	FW	TEB ( 826 )	
FRINH1	KL	DHLSHK ( 1154 )	
FRINH2	KL	DHLSHK ( 1154 )	
FRINOF	FW	GGLSH ( 318 ), GGLSV ( 382 )	
FRINV1	KL	DHLSVK ( 29 )	
FRINV2	KL	DHLSVK ( 29 )	
FRIPDSL1	FW	LR ( 768 )	
FRIPDSL4	FW	LR ( 768 )	
FRIPDTE5	FW	LR ( 768 )	
FRIPTES	FW	LR ( 768 )	
FRKAP	FW	ESGRU ( 678 )	
FRLFSDP	KL	AES ( 973 )	
FRLMNHO	KL	MDFUE ( 594 )	
FRMAX	FW	LR ( 768 )	
FRMDPMO	FW	DTEV ( 856 )	
FRMDPMU	FW	DTEV ( 856 )	
FRMDTEVO	FW	DTEV ( 856 )	
FRMDTEVU	FW	DTEV ( 856 )	
FRMINSLS	FW	LR ( 768 )	
FRMLASHO	FW	DLSAHK ( 339 )	
FRMLASHU	FW	DLSAHK ( 339 )	
FRMSTDN	FW	DKVS ( 811 )	
FRMSTDX	FW	DKVS ( 811 )	
FRTEMX	FW	LR ( 768 )	
FS1FO	FW	DMDFON ( 161 )	
FS2FO	FW	DMDFON ( 161 )	
FSRFTEF	FW	TEB ( 826 )	
FSTHO	KL	ESSTT ( 679 )	
FSTRES	FW	GGFST ( 502 )	
FSTTMX	FW	BGKV ( 71 )	
FSWALUV	KL	DSWEC ( 32 )	
FSWALUV1	KL	DSWEC ( 32 )	
FSZTM	KL	ZUESZ ( 632 )	
FTAGRV	KL	BGAGR ( 263 )	
FTDAG	KL	BGAGR ( 263 )	
FTEADAB	FW	TEB ( 826 )	
FTEADDPO	FW	DTEV ( 856 )	
FTEADDPU	FW	DTEV ( 856 )	
FTEADMX	FW	TEB ( 826 )	
FTEADSZ	FW	DTEV ( 856 )	
FTEADZU	FW	BBTEGA ( 750 )	
FTEDS	FW	BBTEGA ( 750 )	
FTEFHB	FW	TEB ( 826 )	
FTEHB	FW	TEB ( 826 )	
FTEINIX	KL	TEB ( 826 )	
FTMFFANZ	KL	ZUESZ ( 632 )	
FTMLAKH	KL	BBKHZ ( 890 )	
FUBAOF	FW	ZUESZ ( 632 )	
FUEPMLD	KL	FUEDK ( 597 )	
FUKABAKI	FW	ESUKA ( 711 )	
FUKABAKO	FW	ESUKA ( 711 )	
FUKABAKU	FW	ESUKA ( 711 )	
FUKABAWI	FW	ESUKA ( 711 )	
FUKABAWO	FW	ESUKA ( 711 )	
FUKABAWU	FW	ESUKA ( 711 )	
FUKAVAKI	FW	ESUKA ( 711 )	
FUKAVAKO	FW	ESUKA ( 711 )	
FUKAVAKU	FW	ESUKA ( 711 )	



Symbol	Type	Created within	Used within
FUKAWAWI	FW	ESUKA ( 711 )	
FUKAWAWO	FW	ESUKA ( 711 )	
FUKAWAWU	FW	ESUKA ( 711 )	
FUKE	FW	ESUK ( 699 )	
FUKNSTHO	KL	ESUK ( 699 )	
FUKNSTM	KL	ESUK ( 699 )	
FUMRBRK	FW	TEB ( 826 )	
FUMRMV	FW	BGTEV ( 257 )	
FUMSTEK	FW	BGTEV ( 257 )	
FVANST	FW	ESUK ( 699 )	
FVERMN	KL	TEB ( 826 )	
FVERZDYN	KL	TEB ( 826 )	
FVRMDYN	KL	TEB ( 826 )	
FWDMVAD	KL	MDMIN ( 538 )	
FWEAB	FW	ACIFI ( 1013 )	
FWEAUF	FW	ACIFI ( 1013 )	
FWEMXT	KL	ACIFI ( 1013 )	
FWFN	FW	ESUK ( 699 )	
FWFTBRTA	KL	BGTEMPK ( 252 )	
FWLKFTBR	KL	BGTEMPK ( 252 )	
FWMABGW	FW	ATM ( 20 )	
FWMABGW2	FW	ATM ( 20 )	
FWMKATW	FW	ATM ( 20 )	
FWMKATW2	FW	ATM ( 20 )	
FWMLHFMMN	KL	DHFM ( 233 )	
FWNMOT	FW	ZUESZ ( 632 )	
FWPEDRLS	FW	MDFUE ( 594 )	
FWSTAA1	KL	ESNSWL ( 691 )	
FWSTAB1	KL	ESNSWL ( 691 )	
FWSTAB2	KL	ESNSWL ( 691 )	
FWSTAB3	KL	ESNSWL ( 691 )	
FWSTAS1	KL	ESNSWL ( 691 )	
FWSTAS2	KL	ESNSWL ( 691 )	
FZANSSA1	KL	ESNSWL ( 691 )	
FZANSSA2	KL	ESNSWL ( 691 )	
FZANSSM1	KL	ESNSWL ( 691 )	
FZANSSM2	KL	ESNSWL ( 691 )	
FZANSSM3	KL	ESNSWL ( 691 )	
FZDASHTM	KL	MDFAW ( 508 )	
FZN1	KL	ACIFI ( 1013 )	
FZNNW1	KL	ACIFI ( 1013 )	
FZPUSA	KL	BGPU ( 276 )	
FZWKHMx	FW	ZWMIN ( 669 )	
FZWSTNM	KL	ZWSTT ( 637 )	
FZWSTTM	KL	ZWSTT ( 637 )	
GFDLDN	KL	LLRRM ( 566 )	
HLCCAS	FW	DCAS ( 1128 )	
HLCCINS	FW	DCINS ( 1126 )	
HLCKUP	FW	DCKUP ( 1128 )	
HLCLUEA	FW	DMLSE ( 34 )	
HLCLUEB	FW	DMLSE ( 34 )	
HYKATA	FW	DKAT ( 361 )	
HYKATR	FW	DKAT ( 361 )	
IGESGA	KL	BBGANG ( 501 )	
ILMLKAXTK	KL	LRKA ( 795 )	
ILMLKAXTK2	KL	LRKA ( 795 )	
ILMRMN	FW	FUEREG ( 595 )	
ILMRMX	FW	FUEREG ( 595 )	
ILMRN	KL	FUEREG ( 595 )	
IMLHS	FW	ESSTT ( 679 )	
IMLKAMN	FW	LRKA ( 795 )	
IMLKAMN2	FW	LRKA ( 795 )	
IMLKAXTK	KL	LRKA ( 795 )	
IMLKAXTK2	KL	LRKA ( 795 )	
IMLKHTMS	KL	BBKHZ ( 890 )	
IMLKS	FW	BBBO ( 853 )	
IMLKVSMX	FW	DKVS ( 811 )	
IMLSALR	FW	LREB ( 739 )	
IMSDTEVA	FW	DTEV ( 856 )	
IMTUMTA	FW	BGTABST ( 1030 )	
IMTUMTAT	FW	ATM ( 20 )	
INCKSTAI	KL	STADAP ( 684 )	
IP1A_MX_JUM	FW	UFRLC ( 1066 )	
IP2A_MN_JUM	FW	UFRLC ( 1066 )	
IPA_T_JUM	FW	UFRLC ( 1066 )	
ITNMAXP	FW	NMAXMD ( 584 )	
ITNMXH	FW	NMAXMD ( 584 )	
IVDN	KL	LLRRM ( 566 )	
IVDNDTE	KL	LLRRM ( 566 )	
IVDNV	KL	LLRRM ( 566 )	
KAMFZ	FW	DMDTSB ( 159 )	
KATBFML	KL	DKAT ( 361 )	



Symbol	Type	Created within	Used within
KATBFML2	KL	DKAT ( 361 )	
KATBFMN	FW	DKAT ( 361 )	
KATBFMNT	FW	DKAT ( 361 )	
KATBFN	FW	DKAT ( 361 )	
KATBFNM	FW	DKAT ( 361 )	
KATBFNP	FW	DKAT ( 361 )	
KATBFSX	FW	DKAT ( 361 )	
KATBFXM	KL	DKAT ( 361 )	
KATBFXT	FW	DKAT ( 361 )	
KATBSG	FW	DKAT ( 361 )	
KATBSH	FW	DKAT ( 361 )	
KATBSHF	FW	DKAT ( 361 )	
KATBSHG	FW	DKAT ( 361 )	
KATMEXML	KL	ATM ( 20 )	
KATMEXML2	KL	ATM ( 20 )	
KATMIEXML	KL	ATM ( 20 )	
KATMIEXML2	KL	ATM ( 20 )	
KDLASHKI	KL	LRHK ( 781 )	
KDLASHKI2	KL	LRHK ( 781 )	
KDLASHKP	KL	LRHK ( 781 )	
KDLASHKP2	KL	LRHK ( 781 )	
KDLRIDVVE	FW	ADVE ( 918 )	
KE1N	KL	KRKE ( 427 )	
KE2N	KL	KRKE ( 427 )	
KE3N	KL	KRKE ( 427 )	
KE4N	KL	KRKE ( 427 )	
KE5N	KL	KRKE ( 427 )	
KE6N	KL	KRKE ( 427 )	
KE7N	KL	KRKE ( 427 )	
KE8N	KL	KRKE ( 427 )	
KEMLN	KL	GGKS ( 412 )	
KFABAK	KF	ESUK ( 699 )	
KFAFTE	KF	BGTEV ( 257 )	
KFAMAL	KF	DMDLU ( 193 )	
KFAMAL1	KF	DMDLU ( 193 )	
KFATMLA	KF	ATM ( 20 )	
KFATMLA2	KF	ATM ( 20 )	
KFATMZW	KF	ATM ( 20 )	
KFATMZW2	KF	ATM ( 20 )	
KFAVAK	KF	ESUK ( 699 )	
KFBAKL	KF	ESUK ( 699 )	
KFBRAWA	KF	FGRFULO ( 1160 )	
KFBS	KF	GK ( 675 )	
KFCFO	KF	DMDFON ( 161 )	
KFCFO2	KF	DMDFON ( 161 )	
KFDEATE	KF	DTEV ( 856 )	
KFDFBTMN	KF	BGTEMPK ( 252 )	
KFDFBTMP	KF	BGTEMPK ( 252 )	
KFDLSD	KF	MDFAW ( 508 )	
KFDLUR	KF	DMDDL ( 199 )	
KFDLUR1	KF	DMDDL ( 199 )	
KFDLUR2	KF	DMDDL ( 199 )	
KFDLURZ	KF	DMDDL ( 199 )	
KFDMADAP	KF	ARMD ( 531 )	
KFDMDARO	KF	ARMD ( 531 )	
KFDMDKOE	KF	MDVERB ( 540 )	
KFDMDPO	KF	MDFAW ( 508 )	
KFDMLSDO	KF	MDFAW ( 508 )	
KFDMLSDS	KF	MDFAW ( 508 )	
KFDTMRS	KF	GGTFM ( 289 )	
KFDTMTE	KF	GGTFM ( 289 )	
KFDTMTR	KF	GGTFM ( 289 )	
KFDTMTU	KF	GGTFM ( 289 )	
KFDYES	KF	KRDY ( 659 )	
KFDYESOF	KF	KRDY ( 659 )	
KFDZWKG	KF	ZWGRU ( 634 )	
KFETATE	KF	TEB ( 826 )	
KFFDLBTS	KF	LAMBTS ( 732 )	
KFFFANZ	KF	ZUESZ ( 632 )	
KFFFANZUB	KF	ZUESZ ( 632 )	
KFFRAT	KF	LRA ( 797 )	
KFFRMIN	KF	LR ( 768 )	
KFFTEAN	KF	TEB ( 826 )	
KFFTEAX	KF	TEB ( 826 )	
KFFTV	KF	LRHK ( 781 )	
KFFTV2	KF	LRHK ( 781 )	
KFFWL	KF	ESNSWL ( 691 )	
KFFWLRL	KF	ESNSWL ( 691 )	
KFFWLW	KF	ESNSWL ( 691 )	
KFFWTBR	KF	BGTEMPK ( 252 )	
KFFWTBRA	KF	BGTEMPK ( 252 )	
KFKABMT	KF	DKAT ( 361 )	



Symbol	Type	Created within	Used within
KFKHFM	KF	GGHFM ( 230 )	
KFKSWF	KF	DMDMIL ( 216 )	
KFKWTMP	KF	KHMD ( 894 )	
KFLASKH	KF	LAKH ( 735 )	
KFLBTS	KF	LAMBTS ( 732 )	
KFLF	KF	ESGRU ( 678 )	
KFLMSKH	KF	LAKH ( 735 )	
KFLUAR	KF	DMDLUA ( 202 )	
KFLUAR1	KF	DMDLUA ( 202 )	
KFLUAR2	KF	DMDLUA ( 202 )	
KFLUARZ	KF	DMDLUA ( 202 )	
KFLURB	KF	DMDLU ( 193 )	
KFLURB1	KF	DMDLU ( 193 )	
KFLURB2	KF	DMDLU ( 193 )	
KFLURBZ	KF	DMDLU ( 193 )	
KFLURM	KF	DMDLU ( 193 )	
KFLURM1	KF	DMDLU ( 193 )	
KFMAKR	KF	GGKS ( 412 )	
KFMDBGRG	KF	MDBGRG ( 530 )	
KFMDDSLA	KF	KHMD ( 894 )	
KFMDGEN	KF	MDVERB ( 540 )	
KFMDKH	KF	KHMD ( 894 )	
KFMDKO	KF	MDVERB ( 540 )	
KFMDPWM	KF	MDVERB ( 540 )	
KFMDPWME	KF	MDVERB ( 540 )	
KFMDRKO	KF	MDVERB ( 540 )	
KFMDRKOE	KF	MDVERB ( 540 )	
KFMDS	KF	MDVER ( 546 )	
KFMDSZAS	KF	MDVER ( 546 )	
KFMDZOF_UM	KF	UFMZUL (1084)	
KFMIFABG	KF	MDFAW ( 508 )	
KFMIFALS	KF	MDFAW ( 508 )	
KFMILSD	KF	MDFAW ( 508 )	
KFMIMN	KF	MDMIN ( 538 )	
KFMiop	KF	MDBAS ( 529 ), MDMAX ( 514 )	
KFMiRED	KF	VMAXMD ( 588 )	
KFMiRL	KF	MDFUE ( 594 )	
KFMIZUFIL	KF	MDZUL ( 523 )	
KFMIZUNS	KF	MDZUL ( 523 )	
KFMIZUOF	KF	MDZUL ( 523 )	
KFMiLUM	KF	UFMIST (1086)	
KFMiLDMN	KF	DHFM ( 233 )	
KFMiLDMX	KF	DHFM ( 233 )	
KFMiPED_UM	KF	UFMZUL (1084)	
KFMiPNS_UM	KF	UFMZUL (1084)	
KFMRES	KF	LLRMR ( 572 )	
KFMRESK	KF	LLRMR ( 572 )	
KFMRESKH	KF	LLRMR ( 572 )	
KFMRESNL	KF	LLRMR ( 572 )	
KFMRESTA	KF	LLRMR ( 572 )	
KFMRESTM	KF	LLRMR ( 572 )	
KFMiSNWDK	KF	BGMSZS ( 239 ), BGRLP ( 266 )	
KFMiLLNST	KF	LLRNS ( 562 )	
KFMNSA	KF	ESNSWL ( 691 )	
KFMNSWRL	KF	ESNSWL ( 691 )	
KFMNW	KF	NWS ( 618 )	
KFMNWEGM	KF	BBSAWE ( 557 )	
KFMNWWL	KF	NWS ( 618 )	
KFMiPBRK	KF	BGSRM ( 245 )	
KFMiPBRKNW	KF	BGSRM ( 245 )	
KFMiPED	KF	MDFAW ( 508 )	
KFMiPEDR	KF	MDFAW ( 508 )	
KFMiPLMR	KF	FUEREG ( 595 )	
KFMiPRG	KF	BGSRM ( 245 )	
KFMiPRG2SU	KF	BGSRM ( 245 )	
KFMiPRG3SU	KF	BGSRM ( 245 )	
KFMiPRGSU	KF	BGSRM ( 245 )	
KFMiPU	KF	GGHFM ( 230 )	
KFMiPUNW	KF	GGHFM ( 230 )	
KFMiPUSU	KF	GGHFM ( 230 )	
KFMiPUSUNW	KF	GGHFM ( 230 )	
KFMiQTE	KF	TEB ( 826 )	
KFMiRI	KF	LR ( 768 )	
KFMiRI2	KF	LR ( 768 )	
KFMiRINH	KF	DHLSHK (1154)	
KFMiRINH2	KF	DHLSHK (1154)	
KFMiRINV	KF	DHLSVK ( 29 )	
KFMiRINV2	KF	DHLSVK ( 29 )	
KFMiRLIP_UM	KF	UFRLC (1066)	
KFMiRLMN	KF	MDFUE ( 594 )	
KFMiRLMNSA	KF	MDFUE ( 594 )	
KFMiRLW	KF	BGPU ( 276 )	



Symbol	Type	Created within	Used within
KFRLWNW	KF	BGPU ( 276 )	
KFRLWSU	KF	BGPU ( 276 )	
KFRLWSUNW	KF	BGPU ( 276 )	
KFRP	KF	LR ( 768 )	
KFRP2	KF	LR ( 768 )	
KFRTV	KF	LR ( 768 )	
KFRTV2	KF	LR ( 768 )	
KFSU	KF	SU ( 617 )	
KFSU2	KF	SU ( 617 )	
KFSZT	KF	ZUESZ ( 632 )	
KFTADMS	KF	TEB ( 826 )	
KFTAGAV	KF	BGAGR ( 263 )	
KFTATM	KF	ATM ( 20 )	
KFTATM2	KF	ATM ( 20 )	
KFTATX	KF	TEB ( 826 )	
KFTEKA	KF	TEB ( 826 )	
KFTEVP	KF	ATEV ( 969 )	
KFTPKOR	KF	DLSA ( 398 )	
KFTVFR	KF	DTEV ( 856 )	
KFTVSA	KF	BBSAWE ( 557 )	
KFURL	KF	BGSRM ( 245 )	
KFURL2SU	KF	BGSRM ( 245 )	
KFURL3SU	KF	BGSRM ( 245 )	
KFURLSU	KF	BGSRM ( 245 )	
KFUSHK	KF	LRHK ( 781 )	
KFUSHK2	KF	LRHK ( 781 )	
KFVAKL	KF	ESUK ( 699 )	
KFVERST	KF	MDMIN ( 538 )	
KFVOFFS	KF	FGRREGL ( 1174 )	
KFWDKMSN	KF	FUEDK ( 597 )	
KFWDKPP	KF	GGDVE ( 477 )	
KFWDKSMX	KF	FUEDK ( 597 )	
KFWDKSST	KF	WDKSOM ( 614 )	
KFWDKTHO	KF	WDKSOM ( 614 )	
KFWEE	KF	ESVW ( 1009 )	
KFWEEK	KF	ESVW ( 1009 )	
KFWHSTT	KF	ESSTT ( 679 )	
KFWKSTAB	KF	ESSTT ( 679 )	
KFWKSTN	KF	ESSTT ( 679 )	
KFWKSTT	KF	ESSTT ( 679 )	
KFWMABG	KF	ATM ( 20 )	
KFWMABG2	KF	ATM ( 20 )	
KFWMKAT	KF	ATM ( 20 )	
KFWMKAT2	KF	ATM ( 20 )	
KFWPFGR	KF	BGWPFGR ( 548 )	
KFWTBR	KF	BGTEMPK ( 252 )	
KFWTBRA	KF	BGTEMPK ( 252 )	
KFWWML	KF	ESNSWL ( 691 )	
KFWWNS	KF	ESNSWL ( 691 )	
KFZDASH	KF	MDFAW ( 508 )	
KFZDASH2	KF	MDFAW ( 508 )	
KFZKPUA	KF	BGPU ( 276 )	
KFZLSD	KF	MDFAW ( 508 )	
KFZNSM	KF	LLRNS ( 562 )	
KFZW	KF	ZWGRU ( 634 )	
KFZW2	KF	ZWGRU ( 634 )	
KFZWMN	KF	ZWMIN ( 669 )	
KFZWMNKH	KF	ZWMIN ( 669 )	
KFZWMNST	KF	ZWMIN ( 669 )	
KFZWMS	KF	ZWMIN ( 669 )	
KFZWOP	KF	MDBAS ( 529 )	
KFZWOP2	KF	MDBAS ( 529 )	
KFZWVWLN	KF	ZWWL ( 638 )	
KFZWVWLT	KF	ZWWL ( 638 )	
KFZWVWUM	KF	UFMIST ( 1086 )	
KHCTEAMX	FW	TEB ( 826 )	
KHCTEMN	FW	TEB ( 826 )	
KHCTEMX	FW	TEB ( 826 )	
KIDMSNTE	FW	DTEV ( 856 )	
KIELM	FW	BGPU ( 276 )	
KIFZGAWG	KL	ARMD ( 531 )	
KIFZGHG	KL	ARMD ( 531 )	
KIMSALL	FW	BGMSZS ( 239 )	
KINMXG	KL	NMAXMD ( 584 )	
KINMXNL	FW	NMAXMD ( 584 )	
KINMXRLG	KF	NMAXMD ( 584 )	
KIRMSMS	KL	DTEV ( 856 )	
KISA	FW	BGPU ( 276 )	
KISRM	FW	BGSRM ( 245 )	
KISRM2SU	FW	BGSRM ( 245 )	
KISRM3SU	FW	BGSRM ( 245 )	
KISRMSU	FW	BGSRM ( 245 )	



Symbol	Type	Created within	Used within
KKFFGRGA	KL	FGRREGL (1174)	
KLAF	KL	BGAGR ( 263 ), BGMSZS ( 239 )	FUEDK ( 597 ), BGRLP ( 266 )
KLAFTE	KL	BGTEV ( 257 )	
KLATMLAE	KL	ATM ( 20 )	
KLATMLAE2	KL	ATM ( 20 )	
KLATMIZWE	KL	ATM ( 20 )	
KLATMIZWE2	KL	ATM ( 20 )	
KLATMLAE	KL	ATM ( 20 )	
KLATMLAE2	KL	ATM ( 20 )	
KLATMZWE	KL	ATM ( 20 )	
KLATMZWE2	KL	ATM ( 20 )	
KLDFOFF	FW	LLRNS ( 562 )	
KLD FON	FW	LLRNS ( 562 )	
KLDMDLF1	KL	MDVERB ( 540 )	
KLDMDLF2	KL	MDVERB ( 540 )	
KLDMMX	KL	MDZUL ( 523 )	
KLDPDK	KL	FUEDK ( 597 )	
KLDTPH	KL	NLDG ( 157 )	
KLDTPHST	KL	NLDG ( 157 )	
KLDYNCOR	KL	NLDG ( 157 )	
KLETAZW.UM	KL	UFMIST (1086)	
KLFZWMNKH	KL	ZWMIN ( 669 )	
KLFZWMNST	KL	ZWMIN ( 669 )	
KLNLPHN	KL	NLDG ( 157 )	
KLNPED.UM	KL	UFREAC (1088)	
KLNWRLTM	KL	NWS ( 618 )	
KLRSYNIN	KL	LR ( 768 )	
KLRSYNPN	KL	LR ( 768 )	
KLTDS	KL	GGDST ( 504 )	
KLTNRDE	KL	RDE ( 112 )	
KLWDKABST	KL	WDKSOM ( 614 )	
KLWDKPED	KL	WDKSOM ( 614 )	
KLWDKTAN	KL	WDKSOM ( 614 )	
KLWNWI	KL	NLDG ( 157 )	
KMXSTG	FW	DLSAHK ( 339 )	
KNLSYN	FW	NLDG ( 157 )	
KNSNF	FW	LLRNS ( 562 )	
KRAFGRGA	KL	FGRREGL (1174)	
KRAL1N	KL	KRRA ( 639 )	
KRAL2N	KL	KRRA ( 639 )	
KRAL3N	KL	KRRA ( 639 )	
KRALH	FW	KRRA ( 639 )	
KRAN1	FW	KRRA ( 639 )	
KRAN2	FW	KRRA ( 639 )	
KRAN3	FW	KRRA ( 639 )	
KRAN4	FW	KRRA ( 639 )	
KRANH	FW	KRRA ( 639 )	GGKS ( 412 )
KRDWA	FW	KRRA ( 639 )	
KRDWKLA	FW	KRRA ( 639 )	
KRDWSA	FW	KRRA ( 639 )	
KRDWSN	KL	KRRA ( 639 )	
KRFHKS	FW	DKRS ( 437 )	
KRFHT	FW	DKRNT ( 445 ), DKRTP ( 451 ), GGKS ( 412 )	
KRFKN	KL	KRRA ( 639 )	
KRFTP1	FW	KRKE ( 427 )	
KRFTP2	FW	KRKE ( 427 )	
KRFTP3	FW	KRKE ( 427 )	
KRKFKS	FW	KRKE ( 427 )	
KRKTE	FW	AES ( 973 )	
KRLMDY	FW	KRRA ( 639 )	
KRMXN	KL	KRRA ( 639 )	
KRNZAR	KWB	KRRA ( 639 )	
KRNMDY	FW	KRRA ( 639 )	
KRVFN	KL	KRRA ( 639 )	
KRVFSN	KL	KRRA ( 639 )	
KRVST	FW	KRKE ( 427 )	
KSTAI	KL	STADAP ( 684 )	
KSTAMX0	FW	STADAP ( 684 )	
KSTAMX1	FW	STADAP ( 684 )	
KSTAMX2	FW	STADAP ( 684 )	
KSZA	FW	KRKE ( 427 ), KRRA ( 639 )	
KUMSRL	FW	BGKV ( 71 ), BGMSZS ( 239 )	TEB ( 826 ), FUEDK ( 597 )
KVLAD	FW	BGMSZS ( 239 )	
LADFIL	FW	BGMSZS ( 239 )	
LALIUSH	KL	LRHK ( 781 )	
LALIUSH2	KL	LRHK ( 781 )	
LALIUSRH	KL	LRHK ( 781 )	
LALIUSRH2	KL	LRHK ( 781 )	
LAMFA	KF	LAMFAW ( 728 )	
LAMKAML	KL	LRKA ( 795 )	
LAMKAML2	KL	LRKA ( 795 )	
LAMLGF	FW	LAMKO ( 729 )	



Symbol	Type	Created within	Used within
LAMLGMTM	KL	LAMKO ( 729 )	
LAMLRAMN	FW	LRAEB ( 759 )	
LAMLRAMX	FW	LRAEB ( 759 )	
LAMSSAMN	FW	DLSSA ( 350 )	
LAMSSAMX	FW	DLSSA ( 350 )	
LASDSLA	KL	LAKH ( 735 )	
LASHKAB	FW	LRHK ( 781 )	
LASOAB	FW	LAMKO ( 729 )	
LASTMOT	KL	LAKH ( 735 )	
LBZO1	FW	LLRNS ( 562 )	
LBZO2	FW	LLRNS ( 562 )	
LBZU	FW	LLRNS ( 562 )	
LIMN	FW	LLRRM ( 566 )	
LIMNDLLR	FW	LLRRM ( 566 )	
LIMNDTES	FW	LLRRM ( 566 )	
LIMNV	FW	LLRRM ( 566 )	
LIMXDNS	KL	LLRRM ( 566 )	
LIMXVDNS	KL	LLRRM ( 566 )	
LISTM	KL	LLRRM ( 566 )	
LKRN	KL	KRRA ( 639 )	
LLRICNF	FW	LLRRM ( 566 )	
LMSTMOT	KL	LAKH ( 735 )	
LNQXTM	KL	BGTABST (1030)	
LRNST1_T	FW	BGDVE ( 934 )	
LRNST3_T	FW	BGDVE ( 934 )	
LRNST7_T	FW	BGDVE ( 934 )	
LRNST9_T	FW	BGDVE ( 934 )	
LRNVB_T	FW	BGDVE ( 934 )	
LSAKTD	KL	DKAT ( 361 )	
LURBRL8	KL	DMDLU ( 193 )	
LURFOST	FW	DMDFON ( 161 )	
LURKH	KL	DMDLU ( 193 )	
LURKTM	KL	DMDLU ( 193 )	
LURMIN1	KL	DMDLU ( 193 )	
LURMIN2	KL	DMDLU ( 193 )	
LURMIN3	KL	DMDLU ( 193 )	
LWSER	FW	MDVERB ( 540 )	
LZFUER	KL	KRRA ( 639 )	
MASK_40MS	SYS		UFSGSC ( 1070 )
MASK_FUAE	SYS		UFSGSC ( 1070 )
MDERFOKH	FW	DMDFON ( 161 )	
MDERKFON	FW	DMDFON ( 161 )	
MDHYEZ	FW	MDRED ( 976 )	
MDIMX	FW	CAN ( 1124 ), VMAXMD ( 588 ), MDZUL ( 523 )	NMAXMD ( 584 ), MDKOL ( 526 ), MDKOG ( 516 ), MDFAW ( 508 )
MDKOAB	KL	KOS ( 896 )	
MDKOAN	KL	KOS ( 896 )	
MDKOEN	KL	KOS ( 896 )	
MDLF1	FW	MDVERB ( 540 )	
MDLF2	FW	MDVERB ( 540 )	
MDNORM	FW	MDVERB ( 540 )	
MDSH	KL	MDVER ( 546 )	
MDSL	FW	MDVERB ( 540 )	
MDSLPE	FW	MDVERB ( 540 )	
MDSLPE	FW	MDVERB ( 540 )	
MDSM	KL	MDVER ( 546 )	
MDSMZAS	KL	MDVER ( 546 )	
MEBZ_M	FW	UFMER ( 1060 )	
MER_T1_UM	FW	UFMER ( 1060 )	
MER_T2_UM	FW	UFMER ( 1060 )	
MIFABGMX	FW	MDFAW ( 508 )	
MIFAMXNOT	KL	GGPED ( 454 )	
MILANTI	FW	DMDMIL ( 216 )	
MINAKRLZ	FW	KRRA ( 639 )	
MKFADPN	KL	MDFAW ( 508 )	
MKFADPN1	KL	MDFAW ( 508 )	
MKLLS	KL	MDVERB ( 540 )	
MKMIFABG	FW	MDFAW ( 508 )	
MLDKVSF	FW	DKVS ( 811 )	
MLDKVSG	FW	DKVS ( 811 )	
MLDTEFPF	FW	DTEV ( 856 )	
MLDTEPF	FW	DTEV ( 856 )	
MLFKMSDK	FW	BGMSZS ( 239 )	
MLHFM	KL	GGHFM ( 230 )	
MLHFMMN	FW	DHFM ( 233 )	
MLKHMx	FW	BBKHZ ( 890 )	
MLLASH	FW	DLSAHK ( 339 )	
MLMAX	FW	BGRML ( 287 )	
MLMIN	FW	GGHFM ( 230 )	
MLNKAX	FW	LRHK ( 781 )	
MLO1	FW	LRA ( 797 )	
MLO1AC	FW	LRA ( 797 )	
MLO2	FW	LRA ( 797 )	





Symbol	Type	Created within	Used within
MLO3	FW	LRA ( 797 )	
MLO3AC	FW	LRA ( 797 )	
MLOFS	FW		DHFM ( 233 ), GGHF ( 230 )
MLOSTEST	FW	DLSAHK ( 339 )	
MLSUS	KL	BBKHZ ( 890 )	
MLU2	FW	LRA ( 797 )	
MLU2AC	FW	LRA ( 797 )	
MLU4	FW	LRA ( 797 )	
MLUSSTG	FW	DLSAHK ( 339 )	
MLUSTEST	FW	DLSAHK ( 339 )	
MRESLL	FW	LLRMR ( 572 )	
MRESSL	FW	LLRMR ( 572 )	
MRFABUMX	FW	FUEDK ( 597 )	
MRFALLO	FW	MDFAW ( 508 )	
MRFALLU	FW	MDFAW ( 508 )	
MRFARUGDN	KL	FUEDK ( 597 )	
MRFVAVLN	KL	MDFAW ( 508 )	
MRFVAVW	KL	ESVW ( 1009 )	
MRFGRIMX	KL	FGRREGL ( 1174 )	
MRFGRLL	FW	FGRREGL ( 1174 )	
MRFGRMAX	FW	FGRREGL ( 1174 )	FGRFULO ( 1160 )
MRFGRSTA	FW	FGRREGL ( 1174 )	
MSALLMN	FW	BGMSZS ( 239 )	
MSALLMX	FW	BGMSZS ( 239 )	
MSDKLMMN	FW	TEB ( 826 )	
MSLG	FW	BGMSZS ( 239 )	
MSNTAG	KL	BGAGR ( 263 )	
MSNTATE	KL	BGTEV ( 257 )	
MSRC.T.UJ	FW	UFMSRC ( 1080 )	
MSRMX	FW	CAN ( 1124 )	
MVER.T.UJ	FW	UFMVER ( 1087 )	
MXNLFEHL	FW	NLDG ( 157 )	
MZFFIL.UJ	FW	UFMZ ( 1083 )	
MZFTV.UJ	FW	UFMZ ( 1083 )	
M.SRST.UJ	SYS		UFSGSC ( 1070 )
NO	FW	LRA ( 797 )	
NARAO	FW	ARMD ( 531 )	
NARASTG	FW	ARMD ( 531 )	
NARLLGA	KL	ARMD ( 531 )	
NASNOTKL	KL	MDKOG ( 516 )	
NC.T.UJ	FW	UFNC ( 1063 )	
NDFILOG	KL	ARMD ( 531 )	
NDIFFOG	KL	ARMD ( 531 )	
NDIF.UJ	FW	UFNC ( 1063 )	
NDKPPU	FW	GGDVE ( 477 )	
NDKS	FW	DKRS ( 437 )	
NDKTSO	FW	DKAT ( 361 )	
NDKTSOT	FW	DKAT ( 361 )	
NDKTSU	FW	DKAT ( 361 )	
NDKTSUT	FW	DKAT ( 361 )	
NDNWMN	FW	DNWS ( 622 )	
NDNWMX	FW	DNWS ( 622 )	
NDV	FW	DVFZ ( 500 )	
NDVO	FW	DVFZ ( 500 )	
NFANWS	FW	NWS ( 618 )	
NFHZ	FW	LLRNS ( 562 )	
NFHZFS	FW	LLRNS ( 562 )	
NFLUV	FW	DMDLU ( 193 )	
NFS2M	KL	LLRNS ( 562 )	
NFSKHM	KL	BBKHZ ( 890 )	
NFSKLDL	FW	LLRNS ( 562 )	
NFSKO	FW	LLRNS ( 562 )	
NFSKS	FW	LLRNS ( 562 )	
NFSLPWG	FW	LLRNS ( 562 )	
NFSM	KL	LLRNS ( 562 )	
NFSMIN	FW	LLRNS ( 562 )	
NFSNLDG	FW	LLRNS ( 562 )	
NFSSL	FW	LLRNS ( 562 )	
NGALUN	KL	DMDSTP ( 205 )	
NGANGMIN	FW	BBGANG ( 501 ), CAN ( 1124 )	
NGDNSA	FW	BBSAWE ( 557 )	
NGFSAWE	FW	MDFAW ( 508 )	
NGKRWN	KL		KRDY ( 659 )
NGNSNF	FW	LLRNS ( 562 )	
NKLDF	FW	LLRNS ( 562 )	
NKRFM1	FW	GGKS ( 412 )	
NKRFM2	FW	GGKS ( 412 )	
NKRFM3	FW	GGKS ( 412 )	
NKRUM	FW	KRDY ( 659 )	
NKTDX	FW	DKAT ( 361 )	
NLL2M	KL	LLRNS ( 562 )	
NLLCVTMXV	KL	LLRNS ( 562 )	



Symbol	Type	Created within	Used within
NLLKHM	KL	BBKHZ ( 890 )	
NLLKHNW	FW	NWS ( 618 )	
NLLKT	FW	BBKHZ ( 890 )	
NLLM	KL	DMDMIL ( 216 ), LLRNS ( 562 )	
NLLMIN	FW	LLRNS ( 562 )	
NLPST1T	FW	BGDVE ( 934 )	
NLPST2T	FW	BGDVE ( 934 )	
NLRHO	FW	LRHK ( 781 )	
NLRHU	FW	LRHK ( 781 )	
NLRKA	FW	LRKA ( 795 )	
NLRSHB	FW	LREB ( 739 )	
NMAX	FW		NMAXMD ( 584 )
NMAXDV	FW		NMAXMD ( 584 )
NMAXDVG	KL	NMAXMD ( 584 )	
NMAXDZ	FW	NMAXMD ( 584 )	
NMAXNL	FW	NMAXMD ( 584 )	
NMAXOG	FW	NMAXMD ( 584 )	
NMAXSGS	FW	NMAXMD ( 584 )	
NMAXU	FW	BGBSZ ( 73 )	
NMIALU	FW	DMDSTP ( 205 )	
NMIDLU	FW	DMDDL ( 199 )	
NMIN	FW	GGDPG ( 74 ), LLRBB ( 575 )	
NMINVMX	FW	VMAXMD ( 588 )	
NMIN_JUM	FW	UFNC ( 1063 )	
NMIN_DUF	FW	DUF ( 1089 )	
NMOTQSYN	FW	GGDPG ( 74 )	
NMOTRDE	FW	RDE ( 112 )	
NMXALU	FW	DMDSTP ( 205 )	
NMXDAEF	KL	NMAXMD ( 584 )	
NMXDKPU	FW		NMAXMD ( 584 )
NMXPG	KL	NMAXMD ( 584 )	
NMXPNL	FW	NMAXMD ( 584 )	
NMXPRLG	KF	NMAXMD ( 584 )	
NMXSKA	FW	AEVABU ( 1002 )	
NNSTA	KL	BBSTT ( 148 )	
NO1	FW	LRA ( 797 )	
NOASR_JUM	FW	UFMSRC ( 1080 )	
NOLRA	FW	LRA ( 797 )	
NOME_T	FW	DUF ( 1089 )	
NOREA_JUM	FW	UFREAC ( 1088 )	
NOVZTE	FW	BGTEV ( 257 )	
NPHERKMN	FW	NLPH ( 150 )	
NPHERKMX	FW	NLPH ( 150 )	
NPHINVMN	FW	NLPH ( 150 )	
NPHINVMX	FW	NLPH ( 150 )	
NPMOL1	FW	GGPOEL ( 296 )	
NPUS	FW	BGPU ( 276 )	
NRKAB	FW	LRA ( 797 )	
NRLIP_JUM	FW	UFRLC ( 1066 )	
NRLMN	FW	FUEDK ( 597 )	
NRLMNLRL	FW	FUEDK ( 597 )	
NRUBMX	FW	BGLBZ ( 489 )	
NSAC	FW	LLRNS ( 562 )	
NSACFS	FW	LLRNS ( 562 )	
NSC_T_JUM	FW	UFNSC ( 1077 )	
NSHLL	FW	LLRNS ( 562 )	
NSKO	FW	LLRNS ( 562 )	
NSKS	FW	LLRNS ( 562 )	
NSL	FW	LLRNS ( 562 )	
NSLBZFS	FW	LLRNS ( 562 )	
NSLBZLL	FW	LLRNS ( 562 )	
NSLBZS	FW	LLRNS ( 562 )	
NSLFAKAT	FW	LLRNFA ( 564 )	
NSLFALSV	FW	LLRNFA ( 564 )	
NSLFASH	FW	LLRNFA ( 564 )	
NSLKVS	FW	LLRNFA ( 564 )	
NSLLSH	FW	LLRNFA ( 564 )	
NSLPP	KL	LLRNS ( 562 )	
NSLPPFS	KL	LLRNS ( 562 )	
NSLPWG	FW	LLRNS ( 562 )	
NSNLDG	FW	LLRNS ( 562 )	
NSNOT	FW	LLRNS ( 562 )	
NSOF_T_JUM	FW	UFNSC ( 1077 )	
NSTAMXHA	KL	STADAP ( 684 )	
NSTART	FW	MDZUL ( 523 )	
NSTEND	FW	MDZUL ( 523 )	
NSTNM	KL	BBSTT ( 148 )	
NSWO1	FW	PROKON ( 53 )	
NSWO2	FW	PROKON ( 53 )	
NSYN2SG	FW	GGDPG ( 74 )	
NTPKTO	FW	DLSA ( 398 )	
NTPKTU	FW	DLSA ( 398 )	



Symbol	Type	Created within	Used within
NTPVKO	FW	DLSA ( 398 )	
NTPVKU	FW	DLSA ( 398 )	
NTUMTA	FW	BGTABST (1030)	
NTUMTAT	FW	ATM ( 20 )	
NU3	FW	LRA ( 797 )	
NUKAO	FW	ESUKA ( 711 )	
NUKAU	FW	ESUKA ( 711 )	
NVERZMN	FW	TEB ( 826 )	
NVQUOT1O	FW	BBGANG ( 501 )	
NVQUOT1U	FW	BBGANG ( 501 )	
NVQUOT2O	FW	BBGANG ( 501 )	
NVQUOT2U	FW	BBGANG ( 501 )	
NVQUOT3O	FW	BBGANG ( 501 )	
NVQUOT3U	FW	BBGANG ( 501 )	
NVQUOT4O	FW	BBGANG ( 501 )	
NVQUOT4U	FW	BBGANG ( 501 )	
NVQUOT5O	FW	BBGANG ( 501 )	
NVQUOT5U	FW	BBGANG ( 501 )	
NVQUOT6O	FW	BBGANG ( 501 )	
NVQUOT6U	FW	BBGANG ( 501 )	
NWAFMN	FW	WANWKW ( 125 )	
NWAFMX	FW	WANWKW ( 125 )	
NWDK3	FW	GGDVE ( 477 )	
NWDKSST	KL	WDKSOM ( 614 )	
NWECVTM	KL	BBSAWE ( 557 )	
NWENG	KL	BBSAWE ( 557 )	
NWENGFS	KL	BBSAWE ( 557 )	
NWPMBBR	FW	GGPED ( 454 )	
NWSOS	FW	NWS ( 618 )	
NWSUS	FW	NWS ( 618 )	
NZHDTL	KL	LLRNS ( 562 )	
NZHITL	KL	LLRNS ( 562 )	
NZMUL_JUM	FW	UFNC (1063)	
N_START_JUM	FW	UFNSC (1077)	
N_STEND_JUM	FW	UFNSC (1077)	
N_ST_KRA	FW	KRDY ( 659 )	
OFQSYNADAP	FW	GGDPG ( 74 )	
PAGAVML	KL	BGAGR ( 263 )	
PGFLWA	FW	DDG ( 141 )	
PHLSNVMN	FW	DLSV ( 301 )	
PHNOKA	FW	DPH ( 144 )	
PH_MINSEG	FW	GGDPG ( 74 )	
PLRHAV	KL	LRHK ( 781 )	
PLRHAV2	KL	LRHK ( 781 )	
PLRHML	KL	LRHK ( 781 )	
PLRHML2	KL	LRHK ( 781 )	
PLSOLAP	FW	FUEDK ( 597 )	
PRG2SUNM	KL	BGSRM ( 245 )	
PRG3SUNM	KL	BGSRM ( 245 )	
PRGNM	KL	BGSRM ( 245 )	
PRGSUNM	KL	BGSRM ( 245 )	
PSAPES	FW	AES ( 973 )	
PSPVDKUG	FW	BGMSZS ( 239 ), BGRLP ( 266 )	FUEDK ( 597 )
PUE	FW	BGPU ( 276 )	
PUKANS	KL	GGHFM ( 230 )	
PUMN	FW	BGPU ( 276 )	
PUMX	FW	BGPU ( 276 )	
PVDN	KL	LLRRM ( 566 )	
PVDNKH	KL	LLRRM ( 566 )	
PVDNST	KL	LLRRM ( 566 )	
PVDNV	KL	LLRRM ( 566 )	
PVLDN	KL	LLRRM ( 566 )	
PVLDNV	KL	LLRRM ( 566 )	
PZWKRA	FW	KRDY ( 659 )	
P_ZYL	FW	DMDLU ( 193 )	
QUFRMN	FW	LR ( 768 )	
QUFRMX	FW	LR ( 768 )	
RALEZMAX	FW	ALE ( 136 )	
RAMDASR	FW	CAN (1124)	
RAMPASR	FW	CAN (1124)	
RAMPKUP	FW	CAN (1124)	
RBEL	FW	GGLSH ( 318 )	
RDUNDEF	FW	RDE ( 112 )	
REAC_T1_JUM	FW	UFREAC (1088)	
REAC_T2_JUM	FW	UFREAC (1088)	
REDABM	KF	AEVAB ( 980 )	
REDABMB	KF	AEVAB ( 980 )	
REDABMC	KF	AEVAB ( 980 )	
REDABMZ	KL	AEVAB ( 980 )	
REDHYOC	FW	MDRED ( 976 )	
REDHYUC	FW	MDRED ( 976 )	
REDMX	FW	MDIST ( 528 )	



Symbol	Type	Created within	Used within
REDMXSA	FW	MDRED ( 976 )	
REDZEM	KL	MDRED ( 976 )	
REFINI	FW	KRKE ( 427 )	
RINHMX	FW	GGLSH ( 318 )	
RINVMX	FW	GGLSV ( 382 )	
RISIGRESH	FW	DLSH ( 330 )	
RISIGRESV	FW	DLSV ( 301 )	
RKADTEVO	FW	DTEV ( 856 )	
RKADTEVU	FW	DTEV ( 856 )	
RKAE	FW	DKVS ( 811 )	
RKATDN	FW	DKVS ( 811 )	
RKATDX	FW	DKVS ( 811 )	
RKATMN	FW	LRA ( 797 )	
RKATMX	FW	LRA ( 797 )	
RKATRN	FW	LRA ( 797 )	
RKATRX	FW	LRA ( 797 )	
RKAZDN	FW	DKVS ( 811 )	
RKAZDX	FW	DKVS ( 811 )	
RKAZMN	FW	LRA ( 797 )	
RKAZMX	FW	LRA ( 797 )	
RKAZRN	FW	LRA ( 797 )	
RKAZRX	FW	LRA ( 797 )	
RKBAUM	KL	ESUK ( 699 )	
RKRMX1N	KL	KRKE ( 427 )	
RKRMX2N	KL	KRKE ( 427 )	
RKSP	FW	GGLSH ( 318 )	
RKUKKLU	FW	ESUK ( 699 )	
RKVAUM	KL	ESUK ( 699 )	
RLC.T_UM	FW	UFRLC (1066)	
RLDKTOT	FW	DKAT ( 361 )	
RLDKTSO	KL	DKAT ( 361 )	
RLDKTSU	KL	DKAT ( 361 )	
RLDKTUT	FW	DKAT ( 361 )	
RLDLLR	FW	DLLR ( 578 )	
RLIPFIL_UM	FW	UFRLC (1066)	
RLIPTV_UM	FW	UFRLC (1066)	
RLIP.T_UM	FW	UFRLC (1066)	
RLLRHON	KL	LRHK ( 781 )	
RLLRHUN	KL	LRHK ( 781 )	
RLLRSHB	FW	LREB ( 739 )	
RLLRUN	KL	LREB ( 739 )	
RLNOT	KL	BGMSZS ( 239 )	
RLO2	FW	LRA ( 797 )	
RLO3	FW	LRA ( 797 )	
RLO3AC	FW	LRA ( 797 )	
RLPHERKMN	FW	NLPH ( 150 )	
RLPHERKMX	FW	NLPH ( 150 )	
RLRVAO	FW	LREB ( 739 )	
RLSALULL	FW	DMDSTP ( 205 )	
RLSALUN	KL	DMDSTP ( 205 )	
RLSOLAP	FW	MDFUE ( 594 )	
RLTPKTO	FW	DLSA ( 398 )	
RLTPKTU	FW	DLSA ( 398 )	
RLTPVKO	FW	DLSA ( 398 )	
RLTPVKU	FW	DLSA ( 398 )	
RLU2	FW	LRA ( 797 )	
RLU2AC	FW	LRA ( 797 )	
RLU3	FW	LRA ( 797 )	
RLU4	FW	LRA ( 797 )	
RLUKAO	FW	ESUKA ( 711 )	
RLUKAU	FW	ESUKA ( 711 )	
RLVMXN	KL	MDMAX ( 514 )	
RLVSMXN	KL	MDMAX ( 514 )	
RL_BO_UM	FW	UFRLC (1066)	
RL_MO_UM	FW	UFRLC (1066)	
RMSTEVIO	FW	DTEV ( 856 )	
RMSTEVMN	FW	DTEV ( 856 )	
RMSTVEMX	FW	DTEV ( 856 )	
ROMRSTA_UM	FW	URROM (1041)	
RST_TV_UM	FW	UFREAC (1088), URMEM (1044)	
SAFK1	FW	DLSSA ( 350 )	
SAFK2	FW	DLSSA ( 350 )	
SDK10TEUB	SV		TEB ( 826 )
SDN06LLSB	SV	LLRRM ( 566 )	
SENZZYL	KWVB	GGKS ( 412 )	DKRS ( 437 ), KRRA ( 639 )
SFONTM	FW	DMDSTP ( 205 )	
SFR05TEUB	SV		TEB ( 826 )
SGA08MDUB	SV		NMAXMD ( 584 )
SGSC_ANZ	SYS		UFSGSC (1070)
SGSC_K	SYS		UFSGSC (1070)
SGSC_T_UM	FW	UFSGSC (1070)	
SIM06ESUW	SV		ESNSWL ( 691 )



Symbol	Type	Created within	Used within
SKADRHZ_JUM	FW	UFREAC (1088)	
SKO06KOUB	SV	MDVERB (540)	
SKS06ESUB	SV		ESNSWL (691)
SLFOO2N	KL	DMDFON (161)	
SLFOON	KL	DMDFON (161)	
SLFOU	FW	DMDFON (161)	
SMI04LLUB	SV	LLRMR (572)	
SMK08MDSW	SV	ARMD (531)	
SML05DKUB	SV		DKAT (361)
SML06TEUB	SV		TEB (826)
SMLDYN	FW	DLSAHK (339)	
SNG06LLSB	SV	LLRRM (566)	
SNM05DKUB	SV		DKAT (361)
SNM06ESUB	SV		ESNSWL (691)
SNM06KOUB	SV	MDVERB (540)	
SNM06LLUB	SV	LLRMR (572), LLRRM (566)	
SNM08DMUB	SV		DMDSTP (205)
SNM08KOUB	SV	KOS (896)	
SNM08_UB	SV	ZUE (627)	
SNM10TEUB	SV		TEB (826)
SNM12FEUB	SV	BGMSZS (239)	FUEDK (597)
SNM16KRUB	SV		DKRS (437), KRDY (659), GGKS (412), KRRA (639), KRKE (427)
SNM16OPUW	SV	MDVER (546)	
SNM16ZUUW	SV		ZWMIN (669)
SNS06LLSB	SV	LLRMR (572), LLRNS (562), LLRRM (566)	
SP12LL_JUM	FW	UFSPSC (1060)	
SP12VG_JUM	FW	UFSPSC (1060)	
SP1ADC_DIF	FW	URADCC (1049)	
SP1_STAT	FW	URADCC (1049)	
SP1_STAT_T	FW	URADCC (1049)	
SPSC_MINUM	FW	UFMER (1060), UFSPSC (1060)	
SPSC_T_JUM	FW	UFSPSC (1060)	
SPSVG_JUM	FW	UFSPSC (1060)	
SQM05TEUB	SV	TEB (826)	
SRKTEVS	FW	LLRRM (566)	
SRL04DYUB	SV	KRDY (659)	
SRL04KRUB	SV		GGKS (412)
SRL06KOUB	SV	MDVERB (540)	
SRL08DMUB	SV		DMDSTP (205)
SRL08NXUB	SV		NMAXMD (584)
SRL11OPUW	SV	MDVER (546)	
SRL12ZUUW	SV		ZWMIN (669)
SRP06ESUB	SV		ESNSWL (691)
SRST1_UR	SYS		UFSGSC (1070)
STA04LLUB	SV	LLRMR (572)	
STA06ESUB	SV		ESNSWL (691)
STA06LLUB	SV	MDVERB (540)	
STM04SAUB	SV	LLRMR (572)	
STM06LLUB	SV	LLRNS (562), LLRRM (566)	
STM06_UB	SV		ZWMIN (669)
STM12ESUB	SV		ESNSWL (691)
STN06LLUB	SV	LLRNS (562)	
STS08ESUB	SV		ESNSWL (691)
STS12ESUB	SV		ESNSWL (691)
SUMODE0	FW	SU (617)	
SUMODE1	FW	SU (617)	
SUMODE2	FW	SU (617)	
SUMODE3	FW	SU (617)	
SY_2SG	SYS	DUF (1089)	AEVABZK (1003), FGRREGL (1174), GGDVE (477), GGPED (454), FGRFULO (1160), DNWSE (1025), FGRABED (491), DMDSTP (205), DLLR (578), GGKS (412), BGPU (276), DMDSTP (205), BGTEMPK (252), KOEVAB (124), DMDSTP (205), KOEVAB (124), BGPU (276), FUEDK (597), KOEVAB (124), BGTEMPK (252), FGRFULO (1160)
SY_650ICLK	SYS		
SY_AGR	SYS		
SY_ASG	SYS	MDMIN (538)	
SY_ASR	SYS		
SY_AWUE	SYS		
SY_BDE	SYS	TC6MOD (1112)	
SY_BGVZS	SYS		
SY_BKV	SYS	LLRMR (572)	
SY_BLOOP	SYS		GGDVE (477), GGPED (454)
SY_CANAC	SYS	MDVERB (540)	
SY_CDCCSIZE	SYS	DCDACC (1132)	
SY_CDKSIZE	SYS	DCDACC (1132)	
SY_CDTSIZE	SYS	DCDACC (1132)	
SY_CLASIZE	SYS	DCDACC (1132)	
SY_CONFSL	SYS		DTEV (856)
SY_COPOTI	SYS		GK (675)
SY_CVT	SYS		FUEDK (597)
SY_DEGFE	SYS		BGPU (276)
SY_DFPMENV	SYS	DCDACC (1132)	
SY_DGANZ	SYS		GGKS (412)
SY_DLDP	SYS	DTEV (856), TC6MOD (1112)	TEBEB (762)



Symbol	Type	Created within	Used within
SY_DLS	SYS		AZUE ( 904 )
SY_DLSHV	SYS		DKAT ( 361 )
SY_DOPZW	SYS		AZUE ( 904 ), ZUE ( 627 )
SY_DTES	SYS	TC6MOD ( 1112 )	
SY_DVEADA	SYS		AEVABZK ( 1003 )
SY_EGAS	SYS	NWS ( 618 ), UFREAC ( 1088 )	AEVAB ( 980 ), AEVABZK ( 1003 ), BBSAWA ( 557 ), BGRLP ( 266 ), BG- PU ( 276 ), DLLR ( 578 ), DTEV ( 856 ), TEB ( 826 ), BGMSZS ( 239 )
SY_EGFE	SYS		BGPU ( 276 ), BGTEMPK ( 252 )
SY_FANT	SYS		DMDSTP ( 205 )
SY_FFESIZE	SYS	DFRZ ( 1144 )	
SY_FFFSIZE	SYS	DCDACC ( 1132 )	
SY_FFZ	SYS		AZUE ( 904 ), ZUESZ ( 632 )
SY_FREQ_CP	SYS		AZUE ( 904 )
SY_FWFGR	SYS		FGRFULO ( 1160 ), FGRREGL ( 1174 )
SY_GAP	SYS		AZUE ( 904 ), RDE ( 112 )
SY_GGGS	SYS	KOS ( 896 )	
SY_GRDWRT	SYS		GGKS ( 412 ), RDE ( 112 )
SY_GRDWRTB	SYS		GGKS ( 412 )
SY_GRNDWRT	SYS		AZUE ( 904 )
SY_JNL_OBD	SYS	TCKOMUE ( 1124 )	
SY_KL50	SYS		RDE ( 112 )
SY_KLDF	SYS	DTEV ( 856 ), MDVERB ( 540 )	
SY_KOBIDIR	SYS	KOS ( 896 )	
SY_KOEVB	SYS		AEVABZK ( 1003 )
SY_KOPWM	SYS	MDVERB ( 540 )	
SY_KR_JNT	SYS		GGKS ( 412 )
SY_KS1	SYS		GGKS ( 412 )
SY_KS2	SYS		GGKS ( 412 )
SY_KS3	SYS		GGKS ( 412 )
SY_KS4	SYS		GGKS ( 412 )
SY_KSDIFF	SYS		GGKS ( 412 )
SY_LECK	FW	BGDVE ( 934 )	
SY_LFS	SYS	MDVERB ( 540 )	
SY_LWS	SYS	MDVERB ( 540 )	
SY_ME7	SYS		ZUESZ ( 632 )
SY_NACH	SYS		AZUE ( 904 )
SY_NWS	SYS	NWS ( 618 )	BGSRM ( 245 ), DMDSTP ( 205 ), ESVW ( 1009 ), DTEV ( 856 )
SY_NWSA	SYS		BGSRM ( 245 )
SY_NWVAR	SYS		DMDSTP ( 205 )
SY_NZUEB	SYS		AZUE ( 904 )
SY_PBRPW	SYS		GGPED ( 454 )
SY_PGRAD	SYS		NLPH ( 150 )
SY_PGRAD2	SYS		DMDSTP ( 205 ), NLPH ( 150 )
SY_PGRAD3	SYS		GGVFZG ( 497 )
SY_PH2OFST	SYS		NLPH ( 150 )
SY_PHTWIN	SYS	NWS ( 618 )	
SY_RDE	SYS		KOEVB ( 124 )
SY_REDMX	SYS		AEVAB ( 980 ), ZUE ( 627 ), MDRED ( 976 )
SY_RLAPP	SYS		FUEDK ( 597 )
SY_SGANZ	SYS	DCDACC ( 1132 ), MDVERB ( 540 )	AEVAB ( 980 ), GGKS ( 412 ), BGEVAB ( 1005 )
SY_SLS	SYS	MDVERB ( 540 )	DKAT ( 361 )
SY_STADAP	SYS		ESNSWL ( 691 ), ESSTT ( 679 )
SY_STERHK	SYS		DKAT ( 361 )
SY_STERSY	SYS		DKAT ( 361 )
SY_STERVK	SYS	BGKV ( 71 )	BBTEGA ( 750 ), BGEVAB ( 1005 ), TEBEB ( 762 ), TEB ( 826 ), LRAEB ( 759 ), LRA ( 797 ), GK ( 675 ), DTEV ( 856 ), DLSV ( 301 ), DKAT ( 361 )
SY_SU	SYS		DMDSTP ( 205 )
SY_SWE_B	SYS		DMDSTP ( 205 )
SY_SWE_C	SYS		DMDSTP ( 205 )
SY_SWE_S	SYS		DMDSTP ( 205 )
SY_TEETH	SYS		AZUE ( 904 ), RDE ( 112 )
SY_TFA	SYS		BGTEMPK ( 252 )
SY_TFBA	SYS	ESUK ( 699 )	
SY_TFNS	SYS		ESNSWL ( 691 )
SY_TFST	SYS		ESSTT ( 679 )
SY_TFVA	SYS	ESUK ( 699 )	
SY_TFWL	SYS		ESNSWL ( 691 )
SY_TSFSIZE	SYS	DCDACC ( 1132 )	
SY_TURBO	SYS	BGRML ( 287 )	BGMSZS ( 239 ), GGHEM ( 230 ), FUEDK ( 597 ), DMDSTP ( 205 ), DHFM ( 233 )
SY_TWDKS	SYS		FUEDK ( 597 )
SY_TZW	SYS		ZUE ( 627 ), ZUESZ ( 632 )
SY_UBR	SYS	DUF ( 1089 )	KOEVB ( 124 )
SY_VS	SYS		ESVW ( 1009 ), FUEDK ( 597 )
SY_WMAX	SYS		ZUE ( 627 )
SY_WMIN	SYS		AZUE ( 904 ), ZUE ( 627 )
SY_ZAS	SYS	MDVER ( 546 )	AEVAB ( 980 )
SY_ZNDAUS	SYS		AZUE ( 904 )
SY_ZYLZA	SYS	BGKV ( 71 ), DKRS ( 437 )	AEVAB ( 980 ), BGEVAB ( 1005 ), BGRLP ( 266 ), DMDSTP ( 205 ), ESWE ( 698 ), KRKE ( 427 ), NLPH ( 150 ), KRRR ( 639 ), ZUE ( 627 ), RDE ( 112 ), GGKS ( 412 ), ESSTT ( 679 ), AZUE ( 904 )
SY_ZZBANK	SYS		BGEVAB ( 1005 )



Symbol	Type	Created within	Used within
SY_ZZBANKB	SYS		BGEVAB (1005)
SY_ZZBANKC	SYS		BGEVAB (1005)
SZANSSM1	KL	ESNSWL ( 691 )	
SZANSSM2	KL	ESNSWL ( 691 )	
SZOUTMIN	FW	ZUESZ ( 632 )	
TABGBTS	FW	LAMBTS ( 732 )	
TABGMCS	FW	DLSH ( 330 )	DLSV ( 301 )
TABGMEX	FW	ATM ( 20 )	
TABGMSVU	FW	DLSV ( 301 )	
TABGSTG	FW	DLSAHK ( 339 )	
TAD	FW	GGTFA ( 298 )	
TADHMN	FW	DHLSHK ( 1154 ), DHLSVK ( 29 )	
TADHMX	FW	DHLSHK ( 1154 ), DHLSVK ( 29 )	
TADLLR	FW	DLLR ( 578 )	
TADMM	FW	GGTFM ( 289 )	
TADMN	FW	GGTFA ( 298 )	
TADMX	FW	GGTFA ( 298 )	
TADTEAMX	KL	DTEV ( 856 )	
TADTEMX	FW	DTEV ( 856 )	
TAHLL	FW	LLRNS ( 562 )	
TALUST	FW	DMDSTP ( 205 )	
TAMIALU	FW	DMDSTP ( 205 )	
TANDT	KL	ESSTT ( 679 )	
TANDT1	KL	GGTFM ( 289 )	
TANH	FW	ESSTT ( 679 )	
TANH1	FW	GGTFM ( 289 )	
TANKL	FW	GGFST ( 502 )	
TANSELI	KL	GGTFA ( 298 )	
TANSKOB	FW	KOS ( 896 )	
TANSMN	FW	MDZUL ( 523 )	
TANSMN_LUM	FW	UFNSC ( 1077 )	
TANW	FW	NWS ( 618 )	
TAPVLTM	KL	AEKP ( 970 )	
TARA	FW	LRAEB ( 759 )	
TARAU	FW	LREB ( 739 )	
TAREIN	FW	ARMD ( 531 )	
TASHS	FW	LREB ( 739 )	
TASIG	FW	DLSH ( 330 )	DLSV ( 301 )
TASTBFA	FW	ATM ( 20 )	
TASUS	FW	SU ( 617 )	
TATEGMX	FW	ATEV ( 969 )	
TATELL	FW	BBTEGA ( 750 )	
TATEMSN	KL	ATEV ( 969 )	
TATMKH	FW	ATM ( 20 )	
TATMKH2	FW	ATM ( 20 )	
TATMKW	FW	ATM ( 20 )	
TATMSA	FW	ATM ( 20 )	
TATMSAE	FW	ATM ( 20 )	
TATMSAE2	FW	ATM ( 20 )	
TATMSTI	FW	ATM ( 20 )	
TATMTMOT	FW	ATM ( 20 )	
TATMTTP	FW	ATM ( 20 )	
TATMTRKH	FW	ATM ( 20 )	
TATMTRKH2	FW	ATM ( 20 )	
TATMVMK	FW	ATM ( 20 )	
TAVHKS	FW	BBSAWE ( 557 )	
TAVVKS	FW	BBSAWE ( 557 )	
TBLRH	FW	LRHK ( 781 )	
TBLRH2	FW	LRHK ( 781 )	
TC6TECI	FW	DTEV ( 856 )	
TC6TECL	FW	DTEV ( 856 )	
TC6TECNL	FW	DTEV ( 856 )	
TC6TECP	FW	DTEV ( 856 )	
TC6TECRF	FW	DTEV ( 856 )	
TC6TECRM	FW	DTEV ( 856 )	
TC6TECT	FW	DTEV ( 856 )	
TCIDIS	FW	BGDVE ( 934 )	
TDCAN	FW	CAN ( 1124 )	
TDCAS	FW	DCAS ( 1128 )	
TDCDIS	FW	SREAKT ( 963 )	
TDCINS	FW	DCINS ( 1126 ), DCKUP ( 1128 )	
TDCUP	FW	DCKUP ( 1128 )	
TDDNWS	FW	DNWS ( 622 )	
TDDST	FW	DDST ( 851 )	
TDDSTO	FW	DDST ( 851 )	
TDEGFEMN	FW	DEGFE ( 592 )	
TDEGFEMX	FW	DEGFE ( 592 )	
TDEGFENO	FW	DEGFE ( 592 )	
TDEGFEST	FW	DEGFE ( 592 )	
TDEPOEL	FW	GGPOEL ( 296 )	
TDFRKAD	FW	LRKA ( 795 )	
TDFRKAU	FW	LRKA ( 795 )	



Symbol	Type	Created within	Used within
TDHCAS	FW	DCAS (1128)	
TDHCINS	FW	DCINS (1126)	
TDHCKUP	FW	DCKUP (1128)	
TDKATAKT	FW	DKAT (361)	
TDKATATT	FW	DKAT (361)	
TDKLAGDE	FW	ADVE (918)	
TDKNACH	FW	BGDVE (934)	
TDKPAW	FW	GGDVE (477)	
TDLAMBTSTA	KL	LAMBTS (732)	
TDLLR	FW	DLLR (578)	
TDLLRMN	FW	DLLR (578)	
TDLLRMX	FW	DLLR (578)	
TDLLRNF	FW	DLLR (578)	
TDLRPIDC	FW	ADVE (918)	
TDLRPIDMX	FW	BGDVE (934)	
TDMFBSA	FW	MDFAW (508)	
TDMFBWE	FW	MDFAW (508)	
TDMFWEMI	KL	MDFAW (508)	
TDMKO	FW	MDVERB (540)	
TDMLHFM	FW	DHFM (233)	
TDMLMN	FW	DHFM (233)	
TDMLMX	FW	DHFM (233)	
TDMLNF	FW	DHFM (233)	
TDMLSDS	FW	MDFAW (508)	
TDMLST	FW	DHFM (233)	
TDMRESLL	FW	LLRMR (572)	
TDMSDKS	FW	BGMSZS (239)	
TDNSTA	FW	GGTFA (298)	
TDNSUB	FW	GGUB (487)	
TDNWSP	FW	DNWKW (134)	
TDPUA	FW	BGPU (276)	
TDRLQNWS	FW	BGPU (276)	
TDRLQSU	FW	BGPU (276)	
TDTA	FW	GGTFA (298)	
TDTAL	FW	GGTFA (298)	
TDTEFA	FW	DTEV (856)	
TDTESZO	FW	DTEV (856)	
TDTESZU	FW	DTEV (856)	
TDTEZAM	FW	DTEV (856)	
TDTM	FW	GGTFM (289)	
TDTMMA	FW	GGTFM (289)	
TDTMNP	FW	GGTFM (289)	
TDUB	FW	GGUB (487)	
TDUBHFM	FW	DHFM (233)	
TDV	FW	DVFZ (500)	
TDVIVZ	FW	FGRABED (491)	
TDVKUP	FW	DVKUP (1027)	
TDVZVI	FW	FGRABED (491)	
TDZFPUA	FW	BGPU (276)	
TEBF	FW	AEKP (970)	
TEMIN	FW	RKT1 (979), TEB (826)	
TEPBRKUP	FW	GGEGAS (474)	
TEPCL	FW	DEPCL (1151)	
TEPCLI	FW	DEPCL (1151)	
TFDLLRO	FW	DLLR (578)	
TFDLLRU	FW	DLLR (578)	
TFGRAR	FW	FGRREGL (1174)	
TFGRFDY	FW	FGRABED (491)	
TFGRHE	FW	GGFGRH (473)	
TFGRTIP	FW	GGFGRH (473)	
TFGRUEOB	FW	FGRABED (491)	
TFGRUM	FW	FGRABED (491)	
TFGRUNUB	FW	FGRABED (491)	
TFGRVRAB	FW	GGVFZG (497)	
TFMIZU	FW	MDZUL (523)	
TFPWG2	FW	GGPED (454)	
TFRA	FW	DKVS (811)	
TFRAOZ	FW	DKVS (811)	
TFRAUZ	FW	DKVS (811)	
TFRMB	FW	DLSAHK (339)	
TFRMDTEE	FW	DTEV (856)	
TFRMST	FW	DKVS (811)	
TFRMZST	FW	DKVS (811)	
TFRSGN	FW	LR (768)	
TFTEINI	FW	TEB (826)	
TFWDKPN	KL	GGDVE (477)	
TFWDKSOM	FW	WDKSOM (614)	
TFWPFGR	FW	BGWPFGR (548)	
TGGLS	FW	GGLSH (318), GGLSV (382)	
THDMB	FW		MDKOG (516)
THEH	FW	HLS (392)	
THEV	FW	HLS (392)	





Symbol	Type	Created within	Used within
THHA	FW	HLS ( 392 )	
THHA2	FW	HLS ( 392 )	
THHAWU	FW	HLS ( 392 )	
THOPP1	FW	GGPED ( 454 )	
THOPP2	FW	GGPED ( 454 )	
THSHKTK	KL	HLS ( 392 )	
THSHKTK2	KL	HLS ( 392 )	
THSRIH	FW	GGLSH ( 318 )	
THSRIV	FW	GGLSV ( 382 )	
THSVKTA	KL	HLS ( 392 )	
THSVKTA2	KL	HLS ( 392 )	
THVA	FW	HLS ( 392 )	
THVA2	FW	HLS ( 392 )	
THVAWU	FW	HLS ( 392 )	
TIKATMOE	FW	ATM ( 20 )	
TKATMLRH	FW	LRHK ( 781 )	
TKATMLRH2	FW	LRHK ( 781 )	
TKATMN	FW	BBKHZ ( 890 )	
TKATMOE	FW	ATM ( 20 )	
TKATSA	FW	BBSAWE ( 557 )	
TKATW	FW	BBKHZ ( 890 )	
TKHABB	FW	BBKHZ ( 890 )	
TKHFSAB	FW	BBKHZ ( 890 )	
TKHLL	FW	BBKHZ ( 890 )	
TKHLLAB	FW	BBKHZ ( 890 )	
TKHLLMX	FW	BBKHZ ( 890 )	
TKHMX	FW	BBKHZ ( 890 )	
TKOAMAD	FW	KOS ( 896 )	
TKOAMNN	KL	KOS ( 896 )	
TKOAMXN	KL	KOS ( 896 )	
TKOBEMNN	KL	KOS ( 896 )	
TKODPAMNN	KL	KOS ( 896 )	
TKODPAMXN	KL	KOS ( 896 )	
TKOEMNN	KL	KOS ( 896 )	
TKOMBKOA	FW	KOS ( 896 )	
TKOMBKOE	FW	KOS ( 896 )	
TKOVKO	FW	KOS ( 896 )	
TKOWPAMNN	KL	KOS ( 896 )	
TKOWPAMXN	KL	KOS ( 896 )	
TKSTBFA	FW	ATM ( 20 )	
TKTPVK	FW	DLSA ( 398 )	
TLAFA	FW	LAMFAW ( 728 )	
TLFRES	FW	LFS ( 69 )	
TLFSARMX	FW	LFS ( 69 )	
TLFSART	FW	LFS ( 69 )	
TLLASH	FW	DLSAHK ( 339 )	
TLRBAM	KL	LREB ( 739 )	
TLRHS	FW	LREB ( 739 )	
TLRTMS	KL	LREB ( 739 )	
TLRVAM	KL	LREB ( 739 )	
TLRZWTMS	KL	LREB ( 739 )	
TM1LF	FW	LFS ( 69 )	
TM6LF	FW	LFS ( 69 )	
TMADB0	FW	STADAP ( 684 )	
TMADB1	FW	STADAP ( 684 )	
TMADB2	FW	STADAP ( 684 )	
TMAR	FW	ARMD ( 531 )	
TMASKIV1	FW	DMDMIL ( 216 )	
TMASO	FW	DLSV ( 301 )	
TMAXKAT	FW	DKAT ( 361 )	
TMBVH	FW	GGPED ( 454 )	
TMCC650	FW	GGKS ( 412 )	
TMD DST	FW	DDST ( 851 )	
TMDLLR	FW	DLLR ( 578 )	
TMDMAD	FW	MDVERAD ( 549 )	
TMDMMA	FW	GGTFM ( 289 )	
TMDMMAT	KL	GGTFM ( 289 )	
TMDMMAU	FW	GGTFM ( 289 )	
TMDMMEE	FW	GGTFM ( 289 )	
TMDMMER	FW	GGTFM ( 289 )	
TMDMN	FW	GGTFM ( 289 )	
TMDMX	FW	GGTFM ( 289 )	
TMDNW	FW	DNWS ( 622 )	
TMDTEU	FW	DTEV ( 856 )	
TMDV	FW	DVFZ ( 500 )	
TMDYNA	FW	KRDY ( 659 )	
TMESP	FW	ACIFI ( 1013 )	
TMFRATMN	FW	LRA ( 797 )	
TMFRATUB	FW	LRA ( 797 )	
TMH	FW	ESSTT ( 679 )	
TMHLL	FW	LLRNS ( 562 )	
TMHSG	FW	ESSTT ( 679 )	



Symbol	Type	Created within	Used within
TMINKAT	FW	DKAT ( 361 )	
TMK	FW	ESSTT ( 679 )	
TMKOA0	FW	KOS ( 896 )	
TMKOAU	FW	KOS ( 896 )	
TMKR	FW	GGKS ( 412 ), KRRA ( 639 )	
TMKRA	FW	KRRA ( 639 )	
TMLAST	FW	ARMD ( 531 )	
TMLFAFO	FW	LFS ( 69 )	
TMLFAFU	FW	LFS ( 69 )	
TMLFAROF	KL	LFS ( 69 )	
TMLIM	FW	STADAP ( 684 )	
TMLLX	FW	LLRNS ( 562 )	
TMLRTMS	KL	GGTFM ( 289 )	
TMMIBGR	FW	MDBGRG ( 530 )	
TMMXRT	FW	GGTFM ( 289 )	
TMNEB	FW	DLSV ( 301 )	
TMNKATT	FW	DKAT ( 361 )	
TMNSMN	FW	MDZUL ( 523 )	
TMNSMN_JUM	FW	UFNSC (1077)	
TMNW	FW	NWS ( 618 )	
TMNWWLO	FW	NWS ( 618 )	
TMNWWLU	FW	NWS ( 618 )	
TMOHSMN	FW	HLS ( 392 )	
TMOTELI	KL	GGTFM ( 289 )	
TMOTNMX	FW	NMAXMD ( 584 )	
TMOTWRM	FW	BGTEMPK ( 252 )	
TMQSYN	FW	GGDPG ( 74 )	
TMRA1	FW	LREB ( 739 )	
TMRA2	FW	LREB ( 739 )	
TMRAA	FW	LRA ( 797 ), LRAEB ( 759 )	
TMRAK	FW	LREB ( 739 )	
TMRZHLL	FW	LLRNS ( 562 )	
TMSH	FW	DLSH ( 330 )	
TMSHA	FW	DLSH ( 330 )	
TMSHS	FW	LREB ( 739 )	
TMSKS	FW	BBBO ( 853 )	
TMSLOF	FW	BBKHZ ( 890 )	
TMSNOGA	FW	BBTEGA ( 750 )	
TMSTMAD	FW	KOS ( 896 )	
TMSUKTD	FW	DKAT ( 361 )	
TMSUS	FW	SU ( 617 )	
TMSUSV	FW	SU ( 617 )	
TMSUTMUMA	FW	BGDVE ( 934 )	
TMSV	FW	DLSV ( 301 )	
TMSVA	FW	DLSV ( 301 )	
TMTE	FW	TEBEB ( 762 )	
TMUKAK	FW	ESUKA ( 711 )	
TMUKAU	FW	ESUKA ( 711 )	
TMUKAW	FW	ESUKA ( 711 )	
TMVER	FW		MDKOG ( 516 )
TMWAFMN	FW	WANWKW ( 125 )	
TMWALA	FW	ATWAL ( 297 )	
TMWALE	FW	ATWAL ( 297 )	
TMWUC	FW	DMDMIL ( 216 ), DWUC (1147)	
TMWUCST	FW	DWUC (1147)	
TMZUB2MX	FW	AZUE ( 904 )	
TN2FGRA	KL	FGRREGL (1174)	
TNALU	FW	DMDLU ( 193 )	
TNLATM	FW	ATM ( 20 )	
TNLATMTM	FW	ATM ( 20 )	
TNLATMTU	FW	ATM ( 20 )	
TNLEKPVL	FW	AEKP ( 970 )	
TNLPHWAIT	FW	NLDG ( 157 )	
TNLSGM	KL	BGTABST (1030)	
TNLSGMN	FW	MOTAUS (1028)	
TNLSGMX	FW	MOTAUS (1028)	
TNLSYN	FW	NLDG ( 157 )	
TNMAXP	FW	NMAXMD ( 584 )	
TNMXH	FW	NMAXMD ( 584 )	
TNMXP	FW		NMAXMD ( 584 )
TNOME	FW	SREAKT ( 963 )	
TNSC	FW	MDZUL ( 523 )	
TNSLFA	FW	LLRNFA ( 564 )	
TNSOF	FW	MDZUL ( 523 )	
TNSRT	FW	GGTFM ( 289 )	
TNSTDN	FW	DLSV ( 301 )	
TNSTDNH	FW	DLSH ( 330 )	
TNSTFON	FW	DMDFON ( 161 )	
TNSTKO	FW	KOS ( 896 )	
TNSURLP	FW	BGRLP ( 266 )	
TNSUUK	FW	ESUK ( 699 )	
TNSUUKA	FW	ESUKA ( 711 )	



Symbol	Type	Created within	Used within
TOCKUP	FW	CAN (1124)	
TPERDTE	FW	DTEV (856)	
TPHERKMN	FW	NLPH (150)	
TPHSABSP	FW	NLPH (150)	
TPHSSP	FW	NLPH (150)	
TPNSE	FW	DDVE (950)	
TPNSE1	FW	GGPED (454)	
TPREL	FW	GGDPG (74)	
TPSVKMN	FW	DLSSA (350)	
TPSVKMX	FW	DLSSA (350)	
TPVL	FW	AEKP (970)	
TPWRSV	FW	ADVE (918)	
TQTEAB	FW	TEB (826)	
TQTEDAB	FW	TEB (826)	
TRAU	FW	LREB (739)	
TRD	FW	ALE (136)	
TREHS	FW	HLS (392)	
TRIAKTH	FW	GGLSH (318)	
TRIAKTV	FW	GGLSV (382)	
TRIIMPH	FW	GGLSH (318)	
TRIIMPV	FW	GGLSV (382)	
TRIPFASH	FW	DLSAHK (339)	
TRKA	FW	DKVS (811)	
TRKATZ	FW	DKVS (811)	
TRKAZZ	FW	DKVS (811)	
TRSA	FW	DLSV (301)	
TRSAFA	FW	DLSH (330)	
TRSAH	FW	DLSH (330)	
TRSE	FW	DLSH (330)	DLSV (301)
TSAKAMN	FW	LRKA (795)	
TSALASH	FW	DLSAHK (339)	
TSBBVTMS	KL	LREB (739)	
TSFBREMS	FW	GGEGAS (474)	
TSFEV1	FW	DEVE (1017)	
TSFEV2	FW	DEVE (1017)	
TSFEV3	FW	DEVE (1017)	
TSFEV4	FW	DEVE (1017)	
TSFEV5	FW	DEVE (1017)	
TSFEV6	FW	DEVE (1017)	
TSFEV7	FW	DEVE (1017)	
TSFEV8	FW	DEVE (1017)	
TSFHSH	FW	DHLSHK (1154)	
TSFHSH2	FW	DHLSHK (1154)	
TSFHSHV	FW	DHLSVK (29)	
TSFHSHV2	FW	DHLSVK (29)	
TSFHSHVE	FW	DHLSVKE (902)	
TSFHSHVE2	FW	DHLSVKE (902)	
TSFKAT	FW	DKAT (361)	
TSFKAT2	FW	DKAT (361)	
TSFKPE	FW	DEKPE (1020)	
TSFKRNT	FW	DKRNT (445)	
TSFKROF	FW	DKRNT (445)	
TSFKRTP	FW	DKRTP (451)	
TSFKS1	FW	DKRS (437)	
TSFKS2	FW	DKRS (437)	
TSFKS3	FW	DKRS (437)	
TSFKS4	FW	DKRS (437)	
TSFLASH	FW	DLSAHK (339)	
TSFLASH2	FW	DLSAHK (339)	
TSFLATP	FW	DLSA (398)	
TSFLATP2	FW	DLSA (398)	
TSFLATV	FW	DLSA (398)	
TSFLATV2	FW	DLSA (398)	
TSFLSH	FW	DLSH (330)	
TSFLSH2	FW	DLSH (330)	
TSFLSV2	FW	DLSV (301)	
TSFLUEA	FW	DMLSE (34)	
TSFLUEB	FW	DMLSE (34)	
TSFMDB	FW	MDKOG (516)	
TSFMILE	FW	DMILE (36)	
TSFNWKW	FW	DNWKW (134)	
TSFNWKW2	FW	DNWKW (134)	
TSFNWS	FW	DNWS (622)	
TSFNWS2	FW	DNWS (622)	
TSFPH	FW	DPH (144)	
TSFPH2	FW	DPH (144)	
TSFTA	FW	GGTFA (298)	
TSFTES	FW	DTEV (856)	
TSFTEVE	FW	DTEVE (1022)	
TSFTM	FW	GGTFM (289)	
TSFUB	FW	GGUB (487)	
TSFUF2SG	FW	DUF (1089)	



Symbol	Type	Created within	Used within
TSFUFMV	FW	DUF (1089)	
TSFUFSKA	FW	DUF (1089)	
TSFURRAM	FW	DUR (1052)	
TSFURROM	FW	DUR (1052)	
TSFURRST	FW	DUR (1052)	
TSFVKUP	FW	DVKUP (1027)	
TSGSCNU_UM	FW	UFGSGC (1070)	
TSLUES2	FW	LFS ( 69 )	
TSPERN	KL	LR ( 768 )	
TSPERN2	KL	LR ( 768 )	
TSTEAA	FW	DLSA ( 398 )	
TSVKKO	FW	DLSA ( 398 )	
TSVKKTO	FW	DLSA ( 398 )	
TSVKKTU	FW	DLSA ( 398 )	
TSVKKU	FW	DLSA ( 398 )	
TSVKO	FW	DLSA ( 398 )	
TSVKU	FW	DLSA ( 398 )	
TSWKNBGA	KL	FGRFULO (1160)	
TSWKNVGA	KL	FGRFULO (1160)	
TTBMH	FW	DLSH ( 330 ), DLSV ( 301 )	
TTDSST	FW	DDST ( 851 )	
TTDSTP	FW	DDST ( 851 )	
TTE	FW	BBTEGA ( 750 )	
TTEAE	FW	BBTEGA ( 750 )	
TTEAUS	FW	TEBEB ( 762 )	
TTEBSTP	FW	BBTEGA ( 750 )	
TTEGA	FW	BBTEGA ( 750 )	
TTEGAI	FW	BBTEGA ( 750 )	
TTEGAZO	FW	BBTEGA ( 750 )	
TTEGAZU	FW	BBTEGA ( 750 )	
TTEINI	FW	BBTEGA ( 750 )	
TTEMN	FW	BBTEGA ( 750 )	
TTEPRIO	FW	BBTEGA ( 750 )	
TTEVAZ	FW	DTEV ( 856 )	
TTEVUB	KL	ATEV ( 969 )	
TTEZAO	FW	BBTEGA ( 750 )	
TTEZAU	FW	BBTEGA ( 750 )	
TTIPINEN	FW	ZWMIN ( 669 )	
TTIPINON	FW	ZWMIN ( 669 )	
TTLASH	FW	DLSAHK ( 339 )	
TTMUMASTA	FW	BGDVE ( 934 )	
TUMDETM	FW	GGTFM ( 289 )	
TUMTAI	FW	BGTABST (1030)	
TUMTAIT	FW	ATM ( 20 )	
TUPWBWV	FW	GGPED ( 454 )	
TUPWG12	FW	GGPED ( 454 )	
TUPWG1O	FW	GGPED ( 454 )	
TUPWG1U	FW	GGPED ( 454 )	
TUPWG2O	FW	GGPED ( 454 )	
TUPWG2U	FW	GGPED ( 454 )	
TUSBELH	FW	GGLSH ( 318 )	
TUSBELV	FW	GGLSV ( 382 )	
TUSCHUB	FW	DLSAHK ( 339 )	
TUSDU	FW	DLSV ( 301 )	
TUSDUC	FW	DLSV ( 301 )	
TUSDUFA	FW	DLSH ( 330 )	
TUSDUH	FW	DLSH ( 330 )	
TUSDYN	FW	DLSAHK ( 339 )	
TUSEINH	FW	DLSH ( 330 )	
TUSEINV	FW	DLSV ( 301 )	
TUSENLASH	FW	DLSAHK ( 339 )	
TUSFETT	FW	DLSV ( 301 )	
TUSHSMIN	FW	DLSAHK ( 339 )	
TUSKS	FW	DLSH ( 330 )	DLSV ( 301 )
TUSLASH	FW	DLSAHK ( 339 )	
TUSMAX	FW	DLSH ( 330 )	DLSV ( 301 )
TUSPNMN	FW	DLSSA ( 350 )	
TUSPNMX	FW	DLSSA ( 350 )	
TUSSA	FW	DLSAHK ( 339 )	
TUSTAL	FW	DLSH ( 330 )	
TVARIS	FW	ARMD ( 531 )	
TVDK	FW	LLRBB ( 575 )	
TVDNWS	FW	DNWS ( 622 )	
TVDRREC	FW	DMS ( 37 )	
TVDTEABG	FW	DTEV ( 856 )	
TVDTEB	FW	DTEV ( 856 )	
TVDTEE	FW	DTEV ( 856 )	
TVDTELLA	FW	DTEV ( 856 )	
TVDTEVP	FW	DTEV ( 856 )	
TVDTEVPM	FW	DTEV ( 856 )	
TVDTEVZ	FW	DTEV ( 856 )	
TVERBR	FW	GGEGAS ( 474 )	



Symbol	Type	Created within	Used within
TVFHS	FW	DHLSHK (1154)	
TVFRG	FW	FUEREG (595)	
TVFSAM	KL	MDWAN (554)	
TVFSAWE	FW	MDFAW (508)	
TVFSEM	KL	MDWAN (554)	
TVFSTA	FW	GGFST (502)	
TVFUE	FW	MDWAN (554)	
TVFZNW	FW	ACIFI (1013)	
TVHSH	FW	HLS (392)	
TVHSV	FW	HLS (392)	
TVHVMX	FW	HLS (392)	
TVKOE1	FW	KOS (896)	
TVKOEV	FW	KOS (896)	
TVKOSSIM	FW	KOS (896)	
TVKTDTK	KL	DKAT (361)	
TVKUP	FW	GGEGAS (474)	
TVKUPHS	KL	ARMD (531)	
TVKUPPL	FW	LLRBB (575)	
TVKUPRS	KL	ARMD (531)	
TVKUPV	FW	GGEGAS (474)	
TVLADV	KL	FGRREGL (1174)	
TVLISTU	FW	LLRRM (566)	
TVLLR	FW	LLRBB (575)	
TVLLRI	KL	LLRBB (575)	
TVLLRPD	KL	LLRBB (575)	
TVLLRPST	FW	LLRRM (566)	
TVLLRSTE	FW	LLRBB (575)	
TVLRA	FW	LRAEB (759)	
TVLRHDK	FW	LRHK (781)	
TVLRHMN	FW	DLSA (398)	
TVLRHMN2	FW	DLSA (398)	
TVLRHMX	FW	DLSA (398)	
TVLRHMX2	FW	DLSA (398)	
TVMIBEG	FW	MDKOG (516)	
TVMXPR	FW	VMAXMD (588)	
TVNWF	FW	NWS (618)	
TVNWGE	FW	NWS (618)	
TVNWNST	FW	NWS (618)	
TVNWS	FW	NWS (618)	
TVNWSTTM	KL	NWS (618)	
TVNW_S	FW	NWS (618)	
TVPDKP1	FW	GGDVE (477)	
TVPDKP2	FW	GGDVE (477)	
TVPKH	FW	LLRRM (566)	
TVPWDK12	FW	GGDVE (477)	
TVPWDK13	FW	GGDVE (477)	
TVPWDK23	FW	GGDVE (477)	
TVRESLL	FW	LLRMR (572)	
TVRESTM	FW	LLRMR (572)	
TVRIF	FW	DHLSHK (1154), DHLSVK (29)	
TVSAGO	FW	BBSAWE (557)	
TVSATEM	KL	TEB (826)	
TVSATM	KL	BBSAWE (557)	
TVSLR	KL	LREB (739)	
TVSU	FW	SU (617)	
TVSU2	FW	SU (617)	
TVSUM	KL	SU (617)	
TVSUST	FW	SU (617)	
TVTMMWAL	FW	ATWAL (297)	
TVTUMTA	FW	BGTABST (1030)	
TVUB	KL	AES (973)	
TVWDKS	FW	FUEDKSA (610)	
TVZWMSA	FW	ZWMIN (669)	
TVZWMSE	FW	ZWMIN (669)	
TWBDCY	FW	DDCY (1146)	
TWDDTV	FW	DLSA (398)	
TWDKATST	FW	DKAT (361)	
TWDKRED	FW	WDKSOM (614)	
TWDKSNST	KL	WDKSOM (614)	
TWDKSV	KL	FUEDK (597)	
TWDLSSA	FW	DLSSA (350)	
TWDMAD	FW	MDVERAD (549)	
TWKTDLP	FW	DKAT (361)	
TWLRRTMS	KL	GGTFM (289)	
TWNSTA	FW	GGFST (502)	
TWNTAL	FW	GGFST (502)	
TWPLK	FW	GGPED (454)	
TWPMBBR	FW	GGPED (454)	
TWSTT	KL	ESSTT (679)	
TWTMNHST	FW	GGTFM (289)	
TZ2FGRGA	KL	FGRREGL (1174)	
TZMIN	FW	AEKP (970)	



Symbol	Type	Created within	Used within
TZSPINI	FW	ARMD ( 531 )	
TZTOL_UJ	FW	UFNC (1063)	
T_LAMPE	FW	ATWAL ( 297 )	
UADHFMMN	FW	DHFM ( 233 )	
UADHFMMX	FW	DHFM ( 233 )	
UANAUFRR	FW	BGDVE ( 934 )	
UANNMAX	FW	BGDVE ( 934 )	
UANPEDMAX	FW	BGDVE ( 934 )	
UANPIDMIN	FW	BGDVE ( 934 )	
UANPIDMINA	FW	BGDVE ( 934 )	
UANUATS	FW	BGDVE ( 934 )	
UANVFZG	FW	BGDVE ( 934 )	
UANZURP	FW	BGDVE ( 934 )	
UAN_OJMT	FW	BGDVE ( 934 )	
UAN_STORE	FW	BGDVE ( 934 )	
UAN_UJMT	FW	BGDVE ( 934 )	
UBDCAN	FW	CAN ( 1124), DCKUP ( 1128), DCINS ( 1126), DCAS ( 1128)	
UBDE	FW	GGUB ( 487 )	
UBDLS	FW	DHLSHK ( 1154), DHLSVK ( 29 ), DLSH ( 330 ) DLSV ( 301 )	
UBDLSMX	FW	DHLSHK ( 1154), DHLSVK ( 29 )	
UBDMN1	FW	GGUB ( 487 )	
UBDMN2	FW	GGUB ( 487 )	
UBDMN3	FW	GGUB ( 487 )	
UBDMX	FW	GGUB ( 487 )	
UBDTRDE	FW	RDE ( 112 )	
UBHFM	FW	DHFM ( 233 )	
UBHS	FW	HLS ( 392 )	
UBKST	FW	STADAP ( 684 )	
UBKSTMX	FW	STADAP ( 684 )	
UBLF	FW	LFS ( 69 )	
UBNACHL	FW	GGUB ( 487 )	
UBNLMN	FW	MOTAUS ( 1028)	
UBSOLMN	FW	BGLBZ ( 489 )	
UBSOLMX	FW	BGLBZ ( 489 )	
UBSTS	FW	AEKP ( 970 )	
UBVDKPO	FW	GGDVE ( 477 )	
UBVDKPU	FW	GGDVE ( 477 )	
UB_UANL	FW	BGDVE ( 934 )	
UDKNLP1N	FW	BGDVE ( 934 )	
UDKNLP2N	FW	BGDVE ( 934 )	
UDKNLPTOL	FW	ADVE ( 918 )	
UDKP1AMAX	FW	BGDVE ( 934 )	
UDKP1AMIN	FW	BGDVE ( 934 )	
UDKP1AURI	FW	BGDVE ( 934 )	
UDKP1DUS	FW	BGDVE ( 934 )	
UDKP1NHUB	FW	BGDVE ( 934 )	
UDKP1O	FW	GGDVE ( 477 )	
UDKP1U	FW	GGDVE ( 477 )	
UDKP1VID	FW	BGDVE ( 934 )	
UDKP1VOMA	FW	BGDVE ( 934 )	
UDKP1VOMI	FW	BGDVE ( 934 )	
UDKP1VOSC	FW	BGDVE ( 934 )	
UDKP1VUSC	FW	BGDVE ( 934 )	
UDKP1VUMA	FW	BGDVE ( 934 )	
UDKP1VVM	FW	BGDVE ( 934 )	
UDKP2AMAX	FW	BGDVE ( 934 )	
UDKP2AMIN	FW	BGDVE ( 934 )	
UDKP2AURI	FW	BGDVE ( 934 )	
UDKP2O	FW	GGDVE ( 477 )	
UDKP2U	FW	GGDVE ( 477 )	
UDKPALOS	FW	BGDVE ( 934 )	
UDKPAOFF	FW	BGDVE ( 934 )	
UDKPATMX	FW	BGDVE ( 934 )	
UDKRGOF	FW	DKRNT ( 445 )	
UDKRTP	FW	DKRTP ( 451 )	
UDKSNO	KL	DKRS ( 437 )	
UDKSNU	KL	DKRS ( 437 )	
UEVERG	KL	MDWAN ( 554 )	
UHDMN	FW	DHLSHK ( 1154 )	
UHDMX	FW	DHLSHK ( 1154 )	
UHSN	FW	HLS ( 392 )	
UNWDHFM	FW	DHFM ( 233 )	
UNWDNWS	FW	DNWS ( 622 )	
UPVGNENN	FW	BGDVE ( 934 )	
UPW1BE	FW	GGPED ( 454 )	
UPW1LLMX	FW	GGPED ( 454 )	
UPWG12U	FW	GGPED ( 454 )	
UPWG1O	FW	GGPED ( 454 )	
UPWG1U	FW	GGPED ( 454 )	
UPWG2O	FW	GGPED ( 454 )	
UPWG2U	FW	GGPED ( 454 )	



Symbol	Type	Created within	Used within
UPWGO	FW	GGPED ( 454 )	
UPWGTG	FW	GGPED ( 454 )	
UPWGTL	FW	GGPED ( 454 )	
UPWGU	FW	GGPED ( 454 )	
UPWGUBF	FW	GGPED ( 454 )	
UPWGUR	FW	GGPED ( 454 )	
UPWGVG	FW	GGPED ( 454 )	
URL2SUNM	KL	BGSRM ( 245 )	
URL3SUNM	KL	BGSRM ( 245 )	
URLNM	KL	BGSRM ( 245 )	
URLSUNM	KL	BGSRM ( 245 )	
USDBO	FW	DLSV ( 301 )	
USDBU	FW	DLSV ( 301 )	
USFHK	FW	DLSV ( 301 )	
USHKAMN	FW	LRKA ( 795 )	
USHKAMX	FW	LRKA ( 795 )	
USHLEAN	FW	DLSAHK ( 339 )	
USHOV	FW	HLS ( 392 )	
USHRICH	FW	DLSAHK ( 339 )	
USHSTGMX	FW	DLSAHK ( 339 )	
USHSTSOLL	FW	DLSAHK ( 339 )	
USHUV	FW	HLS ( 392 )	
USIVMAXH	FW	DLSSA ( 350 )	
USIVMAXV	FW	DLSSA ( 350 )	
USIVMINH	FW	DLSSA ( 350 )	
USIVMINV	FW	DLSSA ( 350 )	
USMASO	FW	DLSV ( 301 )	
USMAX	FW	DLSH ( 330 )	DLSV ( 301 )
USMHK	FW	DLSV ( 301 )	
USMIN	FW	DLSH ( 330 )	DLSV ( 301 )
USMNSAMN	FW	DLSSA ( 350 )	
USMNSAMX	FW	DLSSA ( 350 )	
USMNSHMN	FW	DLSSA ( 350 )	
USMNSHMX	FW	DLSSA ( 350 )	
USMXSAMN	FW	DLSSA ( 350 )	
USMXSAMX	FW	DLSSA ( 350 )	
USMXSHMN	FW	DLSSA ( 350 )	
USMXSHMX	FW	DLSSA ( 350 )	
USPVR	FW	DLSV ( 301 )	
USR	FW	DLSSA ( 350 ), LR ( 768 ), LREB ( 739 )	
USREF	FW	DLSV ( 301 )	
USREFH	FW	DLSH ( 330 )	
USREM	FW	DLSV ( 301 )	
USREMH	FW	DLSH ( 330 )	
USRHKSH	FW	DLSSA ( 350 )	
USRHKSHJ	FW	DLSSA ( 350 )	
USRIMINH	FW	GGLSH ( 318 )	
USRIMINV	FW	GGLSV ( 382 )	
USRIOH	FW	GGLSH ( 318 )	
USRIOV	FW	GGLSV ( 382 )	
USRIOH	FW	GGLSH ( 318 )	
USRIOV	FW	GGLSV ( 382 )	
USRIUH	FW	GGLSH ( 318 )	
USRIUV	FW	GGLSV ( 382 )	
USCHUB	FW	DLSAHK ( 339 )	
USVKAMX	FW	LRKA ( 795 )	
VABSCH	FW	VMAXMD ( 588 )	
VANF	FW	LLRMR ( 572 )	
VARAU	FW	ARMD ( 531 )	
VDASH	FW	MDFAW ( 508 )	
VDKUP	FW	DVKUP ( 1027 )	
VDMN	FW	DVFZ ( 500 )	
VDMX	FW	DVFZ ( 500 )	
VFGREMAX	FW	FGRABED ( 491 )	
VFGREMIN	FW	FGRABED ( 491 )	
VFGRMAX	FW	FGRABED ( 491 )	FGRFULO ( 1160 )
VFGRMIN	FW	FGRABED ( 491 )	FGRFULO ( 1160 )
VFZGADMD	FW	DMDSTP ( 205 )	
VFZMN	FW	GGVFZG ( 497 )	
VFZR1O	FW	GGVFZG ( 497 )	
VFZR1U	FW	GGVFZG ( 497 )	
VFZR2O	FW	GGVFZG ( 497 )	
VFZR2U	FW	GGVFZG ( 497 )	
VHA	FW	BGPU ( 276 )	
VHYST	FW	VMAXMD ( 588 )	
VKO	FW	KOS ( 896 )	
VKAOA	FW	KOS ( 896 )	
VKOB	FW	KOS ( 896 )	
VLLR	FW	LLRBB ( 575 )	
VLMXVZ	KL	FGRREGL ( 1174 )	
VLSD	FW	MDFAW ( 508 )	
VMAXO	FW	VMAXMD ( 588 )	
VMAXP	FW	VMAXMD ( 588 )	
VMDUB	FW	GGUB ( 487 )	



Symbol	Type	Created within	Used within
VMIBGR	FW	MDBGGRG ( 530 )	
VMIN_JUM	FW	UFFGRC ( 1078 )	
VNMX	FW	NMAXMD ( 584 )	
VNVKO	FW	KOS ( 896 )	
VNVKOB	FW	KOS ( 896 )	
VREGLMAX	FW	FGRFULO ( 1160 )	
VREGLMIN	FW	FGRFULO ( 1160 )	
VRFGRMN	FW	GGVFZG ( 497 )	
VSAA	FW	BBSAWE ( 557 )	
VSL	FW	LLRNS ( 562 )	
VTUMTA	FW	BGTABST ( 1030 )	
VTUMTAT	FW	ATM ( 20 )	
VVORH	FW	VMAXMD ( 588 )	
VWPMBBR	FW	GGPED ( 454 )	
WAD0T1	FW	STADAP ( 684 )	
WAD0T2	FW	STADAP ( 684 )	
WAD1T0	FW	STADAP ( 684 )	
WAD1T2	FW	STADAP ( 684 )	
WAD2T0	FW	STADAP ( 684 )	
WAD2T1	FW	STADAP ( 684 )	
WAIT_T_JUM	FW	UFREAC ( 1088 ), URMEM ( 1044 )	
WDKARN	KL	LRAEB ( 759 )	
WDKBEWS	FW	ADVE ( 918 )	
WDKETE	FW	ADVE ( 918 )	
WDKFPRO1	FW	BGDVE ( 934 )	
WDKFPRO2	FW	BGDVE ( 934 )	
WDKFPRZ1	FW	BGDVE ( 934 )	
WDKFPRZ2	FW	BGDVE ( 934 )	
WDKHKDN	KL	BGPU ( 276 )	
WDKHKN	KL	BGPU ( 276 )	
WDKNLPIA	FW	BGDVE ( 934 )	
WDKNLPMI	FW	BGDVE ( 934 )	
WDKNLPTOL	FW	ADVE ( 918 )	
WDKNSTORE	FW	BGDVE ( 934 )	
WDKPMXN	KL	GGDVE ( 477 )	
WDKREIB	FW	ADVE ( 918 )	
WDKSAPNOL	FW	ADVE ( 918 )	
WDKSAPP	FW	FUEDK ( 597 )	
WDKSFPFR	FW	BGDVE ( 934 )	
WDKSFPRO	FW	BGDVE ( 934 )	
WDKSNLN	KL	WDKSOM ( 614 )	
WDKSOFIS	FW	FUEDK ( 597 )	
WDKSTFEIN	FW	ADVE ( 918 )	
WDKSTGROB	FW	ADVE ( 918 )	
WDKSTMUMA	FW	BGDVE ( 934 )	
WDKUGDN	KL	BGMSZS ( 239 )	
WEAN	KL	ESVW ( 1009 )	
WEEM	KL	ESVW ( 1009 )	
WEEMRFAN	KL	ESVW ( 1009 )	
WEESTATI	KL	ESVW ( 1009 )	
WEESTM	KL	ESVW ( 1009 )	
WEESTN	KL	ESVW ( 1009 )	
WEESTS	FW	ACIFI ( 1013 )	
WEVS	FW	ESVW ( 1009 )	
WFRL	KL	ESUK ( 699 )	
WKRLZOF	KL	KRRA ( 639 )	
WKRLZOFKS	FW	KRRA ( 639 )	
WMABGKH	FW	ATM ( 20 )	
WMABGKH2	FW	ATM ( 20 )	
WMKATKH	FW	ATM ( 20 )	
WMKATKH2	FW	ATM ( 20 )	
WMNDOPZ	FW	ZUE ( 627 )	
WNWA	FW	DNWS ( 622 )	
WNWAFMX	FW	WANWKW ( 125 )	
WNWASA	FW	NWS ( 618 )	
WNWASMX	FW	WANWKW ( 125 )	
WNWEOA	FW	NWS ( 618 )	
WNWIMXT	FW	NWS ( 618 )	
WNWP	FW	DNWS ( 622 )	
WNWSPMN	FW	DNWKW ( 134 )	
WNWSPMX	FW	DNWKW ( 134 )	
WNWSPS2_0	FW	DNWKW ( 134 ), WANWKW ( 125 )	
WNWSPS2_1	FW	WANWKW ( 125 )	
WNWSPS2_2	FW	WANWKW ( 125 )	
WNWSPS2_3	FW	WANWKW ( 125 )	
WNWSPS_0	FW	DNWKW ( 134 ), WANWKW ( 125 )	
WNWSPS_1	FW	WANWKW ( 125 )	
WNWSPS_2	FW	WANWKW ( 125 )	
WNWSPS_3	FW	WANWKW ( 125 )	
WNWUEMNT	FW	NWS ( 618 )	
WNWUEMXT	FW	NWS ( 618 )	
WPEDKO	KL	KOS ( 896 )	





Symbol	Type	Created within	Used within
WPFGRBMR	KL	BGWPFGR ( 548 )	
WPHN	KL	ZUE ( 627 )	
WPMXBR	FW	GGPED ( 454 )	
WPMXNOT	FW	GGPED ( 454 )	
WPRMBVH	FW	GGPED ( 454 )	
WPRMX	FW	BGRLP ( 266 )	
WPUAVLN	KL	BGPU ( 276 )	
WPUAVLSN	KL	BGPU ( 276 )	
ZATMAML	KL	ATM ( 20 )	
ZATMAML2	KL	ATM ( 20 )	
ZATMIKML	KL	ATM ( 20 )	
ZATMIKML2	KL	ATM ( 20 )	
ZATMKML	KL	ATM ( 20 )	
ZATMKML2	KL	ATM ( 20 )	
ZATMRML	KL	ATM ( 20 )	
ZATMRML2	KL	ATM ( 20 )	
ZBALM	KL	ESUK ( 699 )	
ZBFIL	FW	VMAXMD ( 588 )	
ZBRT	FW	BGTEMPK ( 252 )	
ZBTEML	KL	TEB ( 826 )	
ZBURNABR	FW	STADAP ( 684 )	
ZBURNDEC	FW	STADAP ( 684 )	
ZBURNLIM	FW	ESSTT ( 679 )	
ZBURNSOL	FW	STADAP ( 684 )	
ZBWF	FW	GGPED ( 454 )	
ZDBTMN	KL	BGTEMPK ( 252 )	
ZDBTMP	KL	BGTEMPK ( 252 )	
ZDELBMSRCH	FW	GGDPG ( 74 )	
ZDFFDTE	FW	DTEV ( 856 )	
ZDFR	FW	LR ( 768 )	
ZDGZA1	FW	ESNSWL ( 691 )	
ZDGZA2	FW	ESNSWL ( 691 )	
ZDGZA3	FW	ESNSWL ( 691 )	
ZDKATAD	FW	DKAT ( 361 )	
ZDKATAF	FW	DKAT ( 361 )	
ZDKATSH	FW	DKAT ( 361 )	
ZDKTBD	FW	DKAT ( 361 )	
ZDKTBF	FW	DKAT ( 361 )	
ZDLBTS	FW	LAMBTS ( 732 )	
ZERBR	FW	GGEGAS ( 474 )	
ZETATE	FW	TEB ( 826 )	
ZFBFZGL	FW	GGVFZG ( 497 )	
ZFCNT1	FW	GGVFZG ( 497 )	
ZFCNT2	FW	GGVFZG ( 497 )	
ZFMDVERL	FW	MDVER ( 546 )	
ZFRIH	FW	GGLSH ( 318 )	
ZFRIV	FW	GGLSV ( 382 )	
ZFRMFIL	FW	DTEV ( 856 )	
ZFRMST	FW	DKVS ( 811 )	
ZFRMXAF	FW	DTEV ( 856 )	
ZFTSVK	FW	DLSA ( 398 )	
ZFUKA	FW	ESUKA ( 711 )	
ZFV	FW	GGVFZG ( 497 )	
ZHLLA	FW	LLRNS ( 562 )	
ZHLLI	FW	LLRNS ( 562 )	
ZIDFBM	FW	DDG ( 141 )	
ZIDNOBM	FW	DDG ( 141 )	
ZIVMAX	FW	VMAXMD ( 588 )	
ZKARIH	FW	DHLSHK ( 1154 )	
ZKARIV	FW	DHLSVK ( 29 )	
ZKDMADFK	FW	MDVERAD ( 549 )	
ZKDMADFS	FW	MDVERAD ( 549 )	
ZKDMADKO	FW	MDVERAD ( 549 )	
ZKDMADLL	FW	MDVERAD ( 549 )	
ZKDRLSOL	FW	MDFUE ( 594 )	
ZKFRAOA	KL	LRA ( 797 )	
ZKFRAUA	KL	LRA ( 797 )	
ZKFTEAD	FW	TEB ( 826 )	
ZKFUB	FW	BGLBZ ( 489 )	
ZKHABB	FW	BBKHZ ( 890 )	
ZKLAMKH	FW	BBKHZ ( 890 )	
ZKLBZ	FW	BGLBZ ( 489 )	
ZKLLRD	FW	LLRRM ( 566 )	
ZKMDKO	FW	MDVERB ( 540 )	
ZKMDSLP	FW	MDVERB ( 540 )	
ZKMDWA	FW	MDWAN ( 554 )	
ZKMSDKT	KL	BGMSZS ( 239 )	
ZKNS	FW	LLRNS ( 562 )	
ZKNWS	FW	NWS ( 618 )	
ZKPRIH	FW	DHLSHK ( 1154 )	
ZKPRIV	FW	DHLSVK ( 29 )	
ZKPVDKT	KL	BGMSZS ( 239 )	



Symbol	Type	Created within	Used within
ZKRKATA	KL	LRA ( 797 )	
ZKRKAZA	KL	LRA ( 797 )	
ZKRMSTEV	FW	DTEV ( 856 )	
ZKTABTU	KL	BGTABST ( 1030 )	
ZKTDRL	FW	DKAT ( 361 )	
ZKTDTKM	FW	DKAT ( 361 )	
ZKUBDLR	FW	ADVE ( 918 )	
ZKWDKSPT1	FW	ADVE ( 918 )	
ZKWNWI	FW	NWS ( 618 )	
ZLASHKAB	FW	LRHK ( 781 )	
ZLASOHTML	KL	LRHK ( 781 )	
ZLASOHTML2	KL	LRHK ( 781 )	
ZLIBG	FW	LLRRM ( 566 )	
ZLRFRI	FW	LR ( 768 )	
ZLRHML	KL	LRHK ( 781 )	
ZLRHML2	KL	LRHK ( 781 )	
ZMDNSM	KL	MDVER ( 546 )	
ZMLETAN	FW	DTEV ( 856 )	
ZMLRO	FW	DHFM ( 233 )	
ZMLTE	FW	TEB ( 826 )	
ZMSSGIN	FW	TEB ( 826 )	
ZMSTEDTE	FW	DTEV ( 856 )	
ZNFNGLL	FW	LLRRM ( 566 )	
ZNGFIL	FW	BGNG ( 121 )	
ZNOSTMX	FW	AEKP ( 970 )	
ZNSUB	FW	LLRNS ( 562 )	
ZNWSP	FW	WANWKW ( 125 )	
ZPDDST	FW	DDST ( 851 )	
ZPUN	FW	BGPU ( 276 )	
ZPUSA	FW	BGPU ( 276 )	
ZPVDKR	KL	FUEDK ( 597 )	
ZRLTEDTE	FW	DTEV ( 856 )	
ZSYNABR	FW	STADAP ( 684 )	
ZSYNAUSW	FW	STADAP ( 684 )	
ZSYNCJJUM	FW	UFNC ( 1063 )	
ZTAGR	FW	BGAGR ( 263 )	
ZTAGRV	FW	BGAGR ( 263 )	
ZTDAGR	FW	BGTEMPK ( 252 )	
ZTMMBR	FW	BGTEMPK ( 252 )	
ZTPREL	FW	GGDPG ( 74 )	
ZUKE	FW	ESUK ( 699 )	
ZUKK	FW	ESUK ( 699 )	
ZUKNST	FW	ESUK ( 699 )	
ZVALM	KL	ESUK ( 699 )	
ZVTPRGSU	FW	BGSRM ( 245 )	
ZWAPPL	FW	ZUE ( 627 )	
ZWC_TJUM	FW	UFZWC ( 1075 )	
ZWDKM1	FW	BGWDKM ( 273 )	
ZWDKM2	FW	BGWDKM ( 273 )	
ZWFUBAMN	FW	AZUE ( 904 )	
ZWSPTIP	FW	ZWMIN ( 669 )	
ZYLANZJUM	FW	UFZWC ( 1075 )	
ZYLEAUS	FW	NLPH ( 150 )	
ZYLZA	FW	DEVE ( 1017 )	
ZYRKR	FW	KRKE ( 427 )	
ZZWEETM	KL	ESVW ( 1009 )	
A	LOK	DHLSVK ( 29 )	
ABAK	LOK	ESUK ( 699 )	
ABAOV	LOK	ESUKA ( 711 )	
ABAOV2	LOK	ESUKA ( 711 )	
ABMF	AUS	AEVAB ( 980 )	BGEVAB ( 1005 )
ABMFOLD	LOK	BGEVAB ( 1005 )	
ABO	AUS	BBBO ( 853 )	LRA ( 797 ), TEB ( 826 )
ABR1_COUNT	LOK	ESNSWL ( 691 )	
ADASTEP	LOK	STADAP ( 684 )	
ADCC_CJUM	LOK	URADCC ( 1049 )	
AFNMN	LOK	DMDMIL ( 216 )	
AFNMX	LOK	DMDMIL ( 216 )	
AFRLMN	LOK	DMDMIL ( 216 )	
AFRLMX	LOK	DMDMIL ( 216 )	
AFTNMN	LOK	DMDMIL ( 216 )	
AFTNMX	LOK	DMDMIL ( 216 )	
AFRLMN	LOK	DMDMIL ( 216 )	
AFRLMX	LOK	DMDMIL ( 216 )	
AGRR	AUS	BGSRM ( 245 )	SWADAP ( 47 ), MDBAS ( 529 )
AGR_W	AUS	BGSRM ( 245 )	EGFE ( 228 ), BGTEMPK ( 252 )
AGRVP_W	AUS	EGAG ( 486 )	
AHEARV_W	LOK	DMDMIL ( 216 )	
AHKAT	LOK	DKAT ( 361 )	
AHKAT2	LOK	DKAT ( 361 )	
AHKAT1	LOK	DKAT ( 361 )	
AHKAT12	LOK	DKAT ( 361 )	



Symbol	Type	Created within	Used within
AHKATN	LOK	DKAT ( 361 )	
AHKATN2	LOK	DKAT ( 361 )	
AHKTKI2_W	LOK	DKAT ( 361 )	
AHKTKI_W	LOK	DKAT ( 361 )	
AHKTNK	LOK	DKAT ( 361 )	
AHKTNK2	LOK	DKAT ( 361 )	
AINKBA	LOK	ESUKA ( 711 )	
AINKVA	LOK	ESUKA ( 711 )	
AINTKAMIN	LOK	DMDMIL ( 216 )	
AINT_0	LOK	DMDMIL ( 216 )	
AINT_1	LOK	DMDMIL ( 216 )	
AINT_10	LOK	DMDMIL ( 216 )	
AINT_11	LOK	DMDMIL ( 216 )	
AINT_2	LOK	DMDMIL ( 216 )	
AINT_3	LOK	DMDMIL ( 216 )	
AINT_4	LOK	DMDMIL ( 216 )	
AINT_5	LOK	DMDMIL ( 216 )	
AINT_6	LOK	DMDMIL ( 216 )	
AINT_7	LOK	DMDMIL ( 216 )	
AINT_8	LOK	DMDMIL ( 216 )	
AINT_9	LOK	DMDMIL ( 216 )	
AKATBN	LOK	DKAT ( 361 )	
AKATBN2	LOK	DKAT ( 361 )	
AKATBNK	LOK	DKAT ( 361 )	
AKATBNK2	LOK	DKAT ( 361 )	
AKRLZ	LOK	KRRA ( 639 )	
ANWFOH	LOK	DMDFON ( 161 )	
ANWFOS	LOK	DMDFON ( 161 )	
ANZAIATEN	LOK	DMDMIL ( 216 )	
ANZEAB	LOK	AEVAB ( 980 )	
ANZEAUSB	AUS	NLPH ( 150 )	AEVAB ( 980 )
ANZHFMA_W	LOK	GGHFM ( 230 )	
ANZNMAX	AUS	BGBSZ ( 73 )	
ANZTI	AUS	ACIFI (1013)	BGKV ( 71 ), ESWE ( 698 ), ESUK ( 699 )
ANZTIB	AUS	ACIFI (1013)	ESSTT ( 679 ), ESWW (1009)
ANZTIB_W	AUS	ACIFI (1013)	
ANZTID	LOK	BGKV ( 71 )	
ANZTIP	LOK	FGRFULO (1160)	
ANZTI_W	AUS	ACIFI (1013)	
ANZWEFIM	LOK	ESWE ( 698 )	
APDTEV	AUS	DTEV ( 856 )	
APEDKT	LOK	DKAT ( 361 )	
APEDKT2	LOK	DKAT ( 361 )	
ASPUKA	LOK	ESUKA ( 711 )	
ASPUKA2	LOK	ESUKA ( 711 )	
ATV	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSSA ( 350 )
ATV2	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSSA ( 350 )
ATVFETT	AUS	DLSSA ( 350 )	
ATVFETT2	AUS	DLSSA ( 350 )	
ATVINII	LOK	LRHK ( 781 )	
ATVINII2	LOK	LRHK ( 781 )	
ATVMAGER	AUS	DLSSA ( 350 )	
ATVMAGER2	AUS	DLSSA ( 350 )	
AUSGH_C_UM	LOK	URMEM (1044)	
AUSG_C_UM	LOK	URMEM (1044)	
AUSZH_C_UM	LOK	URMEM (1044)	
AUSZ_C_UM	LOK	URMEM (1044)	
AVAK	LOK	ESUK ( 699 )	
AVAOV	LOK	ESUKA ( 711 )	
AVAOV2	LOK	ESUKA ( 711 )	
AVDTEV	AUS	DTEV ( 856 )	
AVKATF	AUS	DKAT ( 361 )	LRHK ( 781 ), LRKA ( 795 )
AVKATF2	AUS	DKAT ( 361 )	LRHK ( 781 )
AZKELDY	LOK	KRDY ( 659 )	
AZKRLDY	LOK	KRDY ( 659 )	
AZKRNDY	LOK	KRDY ( 659 )	
AZPDTEFRE	AUS	DTEV ( 856 )	
AZYCNT	LOK	DMDMIL ( 216 )	
AZYLWE	LOK	ESWE ( 698 )	
BBDCY	AUS	DDCY (1146)	
BBWUC	AUS	DWUC (1147)	
BBZWZYL	EIN		ZUE ( 627 ), ZUESZ ( 632 )
BFGRS_W	AUS	FGRFULO (1160)	
BFNMN	LOK	DMDMIL ( 216 )	
BFNMX	LOK	DMDMIL ( 216 )	
BFRLMN	LOK	DMDMIL ( 216 )	
BFRLMX	LOK	DMDMIL ( 216 )	
BFZGLF	LOK	VMAXMD ( 588 )	
BFZGLB	AUS	GGVFZG ( 497 )	VMAXMD ( 588 )
BFZGL_W	AUS	GGVFZG ( 497 )	FGRABED ( 491 ), FGRUE ( 490 )



Symbol	Type	Created within	Used within
BLOKNR	EIN		DDVE ( 950 ), DHFM ( 233 ), DHLSHK ( 1154 ), GGUB ( 487 ), GGTFM ( 289 ), GGTFM ( 298 ), GGPED ( 454 ), GGEGAS ( 474 ), DTEV ( 856 ), DNWS ( 622 ), DLSV ( 301 ), MDKOG ( 516 ), DKAT ( 361 ), DHLSVK ( 29 )
BMFZ_W	LOK	DDG ( 141 )	
BMLOSCTR_W	AUS	GGDPG ( 74 )	DDG ( 141 )
BMZZYL	LOK	GGDPG ( 74 )	
BRAFGR_W	LOK	FGRFULO ( 1160 )	
BSC	EIN		DSWEC ( 32 )
BSSP	LOK	DSWEC ( 32 )	
BZMSR_AJUM	LOK	UFMSRC ( 1080 )	
BZ_M	DOK	UFMSRC ( 1080 )	
BZ_MSR	EIN		UFMSRC ( 1080 )
BZ_SGSA_JUM	LOK	UFSGSC ( 1070 )	
BZ_SGSA_JUR	LOK	UFSGSC ( 1070 )	
BZ_SGS_JUM	LOK	UFSGSC ( 1070 )	
BZ_V	DOK	UFMSRC ( 1080 )	
B_2PH	LOK	NLDG ( 157 )	
B_2WART	LOK	BGDVE ( 934 )	
B_3PH	LOK	NLDG ( 157 )	
B_4WD	AUS	PROKON ( 53 )	
B_ABGL	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_ABGSTG	LOK	DLSAHK ( 339 )	
B_ABGSTG2	LOK	DLSAHK ( 339 )	
B_ABOR	AUS	BBBO ( 853 )	LRA ( 797 ), TEB ( 826 )
B_ABSFGR	EIN		FGRABED ( 491 )
B_ABSTNL	AUS	PROKON ( 53 )	BGTABST ( 1030 )
B_ABSTNLG	EIN		GGTFM ( 289 ), BGTABST ( 1030 )
B_ABSTNLGP	AUS	BGTABST ( 1030 )	
B_ABW	LOK	RDE ( 112 )	
B_AC	AUS	SWADAP ( 47 )	
B_ACC	EIN		FGRABED ( 491 ), FGRFULO ( 1160 ), FGRREGL ( 1174 )
B_ACRES	AUS	KOS ( 896 )	SWADAP ( 47 ), MDVERB ( 540 )
B_ACS DH	LOK	DLSH ( 330 )	
B_ACS DH2	LOK	DLSH ( 330 )	
B_AD	LOK	STADAP ( 684 )	
B_ADB0	LOK	STADAP ( 684 )	
B_ADB1	LOK	STADAP ( 684 )	
B_ADB2	LOK	STADAP ( 684 )	
B_ADCSD	LOK	DLSV ( 301 )	
B_ADCSD2	LOK	DLSV ( 301 )	
B_ADDE	LOK	DLSV ( 301 )	
B_ADDE2	LOK	DLSV ( 301 )	
B_ADLCK	LOK	STADAP ( 684 )	
B_ADSH	LOK	DLSH ( 330 )	
B_ADSH2	LOK	DLSH ( 330 )	
B_ADSHS	LOK	DLSH ( 330 )	
B_ADSHS2	LOK	DLSH ( 330 )	
B_ADSVB	LOK	DLSV ( 301 )	
B_ADSVB2	LOK	DLSV ( 301 )	
B_ADWFK	LOK	MDVERAD ( 549 )	
B_ADWFS	LOK	MDVERAD ( 549 )	
B_ADWKO	LOK	MDVERAD ( 549 )	
B_AFKLT	LOK	DMDMIL ( 216 )	
B_AFTKLT	LOK	DMDMIL ( 216 )	
B_AFTWRM	LOK	DMDMIL ( 216 )	
B_AFWE	LOK	ESWE ( 698 )	
B_AFWRM	LOK	DMDMIL ( 216 )	
B_AGR	EIN		BGPU ( 276 ), EGAG ( 486 ), BGTEMPK ( 252 )
B_AGRRDY	AUS	DIMC ( 1148 )	
B_AIRBAG	EIN		AEKP ( 970 ), DECJ ( 1013 )
B_ALE	AUS	ALE ( 136 )	GGDPG ( 74 )
B_AMNUKA	LOK	ESUKA ( 711 )	
B_AMNUKA2	LOK	ESUKA ( 711 )	
B_ANALU	AUS	DMDLU ( 193 )	DMDDL ( 199 )
B_ANALU_M	LOK	DMDLU ( 193 )	DMDLU ( 193 )
B_ANALU_M2	LOK	DMDLU ( 193 )	DMDLU ( 193 )
B_ANFW	LOK	GGTFM ( 289 )	
B_ANF_KUP	EIN		CAN ( 1124 ), DVKUP ( 1027 )
B_ANLAUS	LOK	RDE ( 112 )	
B_APNOLUV	LOK	ADVE ( 918 )	
B_APPNOLU	AUS	ADVE ( 918 )	SREAKT ( 963 )
B_AR	AUS	ARMD ( 531 )	
B_ASC1NEW	EIN		CAN ( 1124 ), DCAS ( 1128 )
B_ASC2NEW	EIN		DCAS ( 1128 )
B_ASC_REG	EIN		DMDSTP ( 205 )
B_ASGAB	AUS	DVKUP ( 1027 )	KOEVAB ( 124 )
B_ASR	AUS	MDKOG ( 516 )	MDFAW ( 508 ), MDRED ( 976 )
B_ASREXT	LOK	UFMSRC ( 1080 )	
B_ASRFZ	AUS	PROKON ( 53 )	CAN ( 1124 )
B_ASR_C	EIN		CAN ( 1124 )
B_ATEV	AUS	DTEVE ( 1022 )	
B_ATMST	LOK	ATM ( 20 )	



Symbol	Type	Created within	Used within
B_ATMST2	LOK	ATM ( 20 )	
B_ATMTPA	AUS	ATM ( 20 )	DHLSVK ( 29 ), DLSV ( 301 ), LR ( 768 ), TEBEB ( 762 ), HLS ( 392 )
B_ATMTPA2	AUS	ATM ( 20 )	DHLSVK ( 29 ), DLSV ( 301 ), HLS ( 392 ), LR ( 768 )
B_ATMTPF	AUS	ATM ( 20 )	
B_ATMTPF2	AUS	ATM ( 20 )	
B_ATMTPK	AUS	ATM ( 20 )	DHLSHK ( 1154 ), DLSH ( 330 ), HLS ( 392 )
B_ATMTPK2	AUS	ATM ( 20 )	DHLSHK ( 1154 ), HLS ( 392 ), DLSH ( 330 )
B_ATMTPL	AUS	ATM ( 20 )	
B_ATMTPL2	AUS	ATM ( 20 )	
B_ATVINI	LOK	LRHK ( 781 )	
B_ATVINI2	LOK	LRHK ( 781 )	
B_AUAKT	EIN		GGTFM ( 289 ), LRAEB ( 759 )
B_AUSW	LOK	STADAP ( 684 )	
B_AUTGET	AUS	PROKON ( 53 )	ARMD ( 531 ), NMAXMD ( 584 ), LLRNFA ( 564 ), KOS ( 896 ), GGEGAS ( 474 ), DMDSTP ( 205 ), DMDFON ( 161 ), CAN ( 1124 ), BBGANG ( 501 ) KOEVAB ( 124 )
B_AWUEAB	EIN		
B_BA	AUS	ESUK ( 699 )	
B_BAG	AUS	ESUK ( 699 )	LREB ( 739 )
B_BBDECJ	AUS	DECJ ( 1013 )	
B_BBUBR	AUS	DECJ ( 1013 )	
B_BEBWF	AUS	GGPED ( 454 )	
B_BEFP1P	AUS	GGPED ( 454 )	
B_BEFP2P	AUS	GGPED ( 454 )	
B_BEFP3P	AUS	GGPED ( 454 )	
B_BEKAT	AUS	DKAT ( 361 )	
B_BEKAT2	AUS	DKAT ( 361 )	
B_BELM	AUS	DHFM ( 233 )	
B_BELSV	AUS	DLSV ( 301 )	
B_BELSV2	AUS	DLSV ( 301 )	
B_BEMDB	AUS	MDKOG ( 516 )	
B_BETES	AUS	DTEV ( 856 )	
B_BEVAB	AUS	AES ( 973 )	BGEVAB ( 1005 ), LAMKO ( 729 ), LRKA ( 795 )
B_BEVAB2	AUS	AES ( 973 )	BGEVAB ( 1005 ), LAMKO ( 729 ), LRKA ( 795 )
B_BFKLT	LOK	DMDMIL ( 216 )	
B_BFWRM	LOK	DMDMIL ( 216 )	
B_BKBREMS	LOK	GGEGAS ( 474 )	
B_BKBWF	AUS	GGPED ( 454 )	
B_BKDVEN	LOK	DDVE ( 950 )	
B_BKDVEU	LOK	DDVE ( 950 )	
B_BKDVEUW	AUS	DDVE ( 950 )	
B_BKDVEV	AUS	DDVE ( 950 )	
B_BKFP1P	AUS	GGPED ( 454 )	
B_BKFP2P	AUS	GGPED ( 454 )	
B_BKFP3P	AUS	GGPED ( 454 )	
B_BKKAT	AUS	DKAT ( 361 )	
B_BKKAT2	AUS	DKAT ( 361 )	
B_BKKS1	AUS	DKRS ( 437 )	
B_BKKS2	AUS	DKRS ( 437 )	
B_BKKS3	AUS	DKRS ( 437 )	
B_BKKS4	AUS	DKRS ( 437 )	
B_BKLM	AUS	DHFM ( 233 )	
B_BKLSV	AUS	DLSV ( 301 )	
B_BKLSV2	AUS	DLSV ( 301 )	
B_BKMDB	AUS	MDKOG ( 516 )	
B_BKTA	AUS	GGTFA ( 298 )	
B_BKTES	AUS	DTEV ( 856 )	
B_BKTM	AUS	GGTFM ( 289 )	
B_BKUB	AUS	GGUB ( 487 )	
B_BKVA	EIN		GGPED ( 454 )
B_BKVLLEER	EIN		AK ( 855 ), LLRMR ( 572 )
B_BKVV	EIN		GGPED ( 454 )
B_BL	LOK	GGEGAS ( 474 )	
B_BLKEB	LOK	DMIL ( 1150 )	
B_BLKFB	EIN		DMIL ( 1150 )
B_BLKMD	AUS	DMDMIL ( 216 )	DMIL ( 1150 )
B_BLRKA	LOK	LRKA ( 795 )	
B_BLRKA2	LOK	LRKA ( 795 )	
B_BM	AUS	GGDPG ( 74 )	BGNMOT ( 111 ), WANWKW ( 125 ), NLPH ( 150 )
B_BR	LOK	GGEGAS ( 474 )	
B_BR2K	AUS	GGEGAS ( 474 )	DMDSTP ( 205 ), GGPED ( 454 )
B_BREMS	AUS	EGEG ( 453 )	GGEGAS ( 474 ), ARMD ( 531 ), FGRABED ( 491 ), FGRUE ( 490 ), LRAEB ( 759 ), LLRNFA ( 564 ), GGPED ( 454 )
B_BREMSE	AUS	SWADAP ( 47 )	
B_BREMS_JUM	AUS	UFFGRE ( 1096 )	UFFGRC ( 1078 ), UFSPSC ( 1060 )
B_BRFRGR_JUM	AUS	UFFGRE ( 1096 )	
B_BUSOFF	EIN		CAN ( 1124 )
B_BVDEL	LOK	LREB ( 739 )	
B_BWF	LOK	GGPED ( 454 )	
B_BWUNPL	LOK	GGPED ( 454 )	
B_C95BF0	LOK	GGKS ( 412 )	
B_C95BF1	LOK	GGKS ( 412 )	
B_C95BF2	LOK	GGKS ( 412 )	



Symbol	Type	Created within	Used within
B_C95BF3	LOK	GGKS ( 412 )	
B_C95DIFF	LOK	GGKS ( 412 )	
B_C95KS1	LOK	GGKS ( 412 )	
B_C95KS2	LOK	GGKS ( 412 )	
B_C95KS3	LOK	GGKS ( 412 )	
B_C95KTI	LOK	GGKS ( 412 )	
B_C95T0	LOK	GGKS ( 412 )	
B_C95T1	LOK	GGKS ( 412 )	
B_C95T2	LOK	GGKS ( 412 )	
B_C95TP0	LOK	GGKS ( 412 )	
B_C95TP1	LOK	GGKS ( 412 )	
B_C95TP2	LOK	GGKS ( 412 )	
B_C95_G0	LOK	GGKS ( 412 )	
B_C95_G1	LOK	GGKS ( 412 )	
B_C95_G2	LOK	GGKS ( 412 )	
B_CANKBI	EIN		GGVFZG ( 497 )
B_CASRLVAL	EIN		CAN ( 1124 )
B_CASRSVAL	EIN		CAN ( 1124 )
B_CDAGR	AUS	PROKON ( 53 )	DIMC ( 1148 ), TC6MOD ( 1112 )
B_CDAGR1	AUS	PROKON ( 53 )	
B_CDATR	AUS	PROKON ( 53 )	
B_CDATS	AUS	PROKON ( 53 )	
B_CDDST	AUS	PROKON ( 53 )	DDST ( 851 )
B_CDHS	AUS	PROKON ( 53 )	DHLSHK ( 1154 )
B_CDHSHE	AUS	PROKON ( 53 )	
B_CDHSV	AUS	PROKON ( 53 )	DHLSVK ( 29 ), DIMC ( 1148 )
B_CDHSVE	AUS	PROKON ( 53 )	DHLSVKE ( 902 )
B_CDKAT	AUS	PROKON ( 53 )	DKAT ( 361 ), TC6MOD ( 1112 )
B_CDKATNO	EIN		TC6MOD ( 1112 )
B_CDKVS	AUS	PROKON ( 53 )	DKVS ( 811 )
B_CDASH	AUS	PROKON ( 53 )	DLSAHK ( 339 ), TC6MOD ( 1112 )
B_CDATP	AUS	PROKON ( 53 )	DLSA ( 398 ), TC6MOD ( 1112 )
B_CDATV	AUS	PROKON ( 53 )	DLSA ( 398 ), TC6MOD ( 1112 )
B_CDLD	AUS	PROKON ( 53 )	DIMC ( 1148 ), TC6MOD ( 1112 )
B_CDLLR	AUS	PROKON ( 53 )	DLLR ( 578 )
B_CDLSA	AUS	PROKON ( 53 )	
B_CDLSH	AUS	PROKON ( 53 )	DLSH ( 330 ), DLSV ( 301 )
B_CDLSV	AUS	PROKON ( 53 )	DIMC ( 1148 ), DLSV ( 301 )
B_CDMD	AUS	PROKON ( 53 )	DMDDL ( 199 ), DMDLU ( 193 ), DMDMIL ( 216 ), DMDLUA ( 202 ), DM-DUE ( 158 ), DMDSTP ( 205 ), DMDLAD ( 215 ), DMDFON ( 161 )
B_CDNWS	AUS	PROKON ( 53 )	DNWS ( 622 )
B_CDSLS	AUS	PROKON ( 53 )	DIMC ( 1148 ), TC6MOD ( 1112 )
B_CDSLSE	AUS	PROKON ( 53 )	
B_CDSWE	AUS	PROKON ( 53 )	DSWEC ( 32 )
B_CDTANKL	AUS	PROKON ( 53 )	
B_CDTES	AUS	PROKON ( 53 )	DIMC ( 1148 ), TC6MOD ( 1112 ), DTEV ( 856 )
B_CDVKT	EIN		TC6MOD ( 1112 )
B_CFUAKABA	LOK	ESUKA ( 711 )	
B_CFUAKAVA	LOK	ESUKA ( 711 )	
B_CIDIS	LOK	BGDVE ( 934 )	
B_CKIEN	EIN		GGTFM ( 289 )
B_CLBM	EIN		DDG ( 141 ), GGDPG ( 74 )
B_CLBREMS	EIN		GGEGAS ( 474 )
B_CLBWF	EIN		GGPED ( 454 )
B_CLCAS	EIN		DCAS ( 1128 )
B_CLCINS	EIN		DCINS ( 1126 )
B_CLCKUP	EIN		DCKUP ( 1128 )
B_CLDK	EIN		GGDVE ( 477 )
B_CLDK1P	EIN		GGDVE ( 477 )
B_CLDK2P	EIN		GGDVE ( 477 )
B_CLDVEE	EIN		ADVE ( 918 )
B_CLDVEF	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLDVEFO	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLDVEL	EIN		ADVE ( 918 )
B_CLDVEN	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLDVER	EIN		ADVE ( 918 )
B_CLDVEU	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLDVEUW	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLDVEV	EIN		BGDVE ( 934 ), DDVE ( 950 )
B_CLEGFE	EIN		BGMSZS ( 239 ), DEGFE ( 592 )
B_CLEV	EIN		DEVE ( 1017 )
B_CLFP1P	EIN		GGPED ( 454 )
B_CLFP2P	EIN		GGPED ( 454 )
B_CLFPP	EIN		GGPED ( 454 )
B_CLFRAO	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLFRAO2	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLFRAU	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLFRAU2	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLFRST	EIN		DKVS ( 811 )
B_CLFRST2	EIN		DKVS ( 811 )
B_CLHSH	EIN		DHLSHK ( 1154 )
B_CLHSH2	EIN		DHLSHK ( 1154 )



Symbol	Type	Created within	Used within
B_CLHSV	EIN		DHLSVK ( 29 )
B_CLHSV2	EIN		DHLSVK ( 29 )
B_CLHSV2	EIN		DHLSVKE ( 902 )
B_CLHSV2	EIN		DHLSVKE ( 902 )
B_CLKAT	EIN		DKAT ( 361 )
B_CLKAT2	EIN		DKAT ( 361 )
B_CLKOSE	EIN		DKOSE ( 901 )
B_CLKPE	EIN		DEKPE ( 1020 )
B_CLKRNT	EIN		DKRNT ( 445 )
B_CLKROF	EIN		DKRNT ( 445 )
B_CLKRTP	EIN		DKRTP ( 451 )
B_CLKS1	EIN		DKRS ( 437 )
B_CLKS2	EIN		DKRS ( 437 )
B_CLKS3	EIN		DKRS ( 437 )
B_CLKS4	EIN		DKRS ( 437 )
B_CLLASH	EIN		DLSAHK ( 339 )
B_CLLASH2	EIN		DLSAHK ( 339 )
B_CLLATP	EIN		DLSA ( 398 )
B_CLLATP2	EIN		DLSA ( 398 )
B_CLLATV	EIN		DLSA ( 398 ), LRHK ( 781 )
B_CLLATV2	EIN		DLSA ( 398 ), LRHK ( 781 )
B_CLLLR	EIN		DLLR ( 578 )
B_CLLM	EIN		DHFM ( 233 ), EGFE ( 228 )
B_CLLSH	EIN		DLSH ( 330 )
B_CLLSH2	EIN		DLSH ( 330 )
B_CLLSV	EIN		DLSV ( 301 )
B_CLLSV2	EIN		DLSV ( 301 )
B_CLMDB	EIN		MDKOG ( 516 )
B_CLMILE	LOK	DMILE ( 36 )	
B_CLMLE	EIN		DMLSE ( 34 )
B_CLN	EIN		DDG ( 141 )
B_CLNWKW	EIN		DNWKW ( 134 )
B_CLNWKW2	EIN		DNWKW ( 134 )
B_CLNWS	EIN		DNWS ( 622 )
B_CLNWS2	EIN		DNWS ( 622 )
B_CLNWISE	EIN		DNWSE ( 1025 )
B_CLPH	EIN		DPH ( 144 ), NLPH ( 150 )
B_CLPH2	EIN		DPH ( 144 )
B_CLRKAT	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLRKAT2	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLRKAZ	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLRKAZ2	EIN		DKVS ( 811 ), LRA ( 797 )
B_CLTA	EIN		GGTFA ( 298 )
B_CLTES	EIN		DTEV ( 856 )
B_CLTEVE	EIN		DTEVE ( 1022 )
B_CLTM	EIN		GGTFM ( 289 )
B_CLUB	EIN		GGUB ( 487 )
B_CLUF2SG	EIN		DUF ( 1089 )
B_CLUFMV	EIN		DUF ( 1089 )
B_CLUFSKA	EIN		DUF ( 1089 )
B_CLURRAM	EIN		DUR ( 1052 )
B_CLURROM	EIN		DUR ( 1052 )
B_CLURRST	EIN		DUR ( 1052 )
B_CLVFZ	EIN		DVFZ ( 500 )
B_CLVKUP	LOK	CVKUP ( 1027 )	
B_CMSRVAL	EIN		CAN ( 1124 )
B_CMUTE	AUS	CAN ( 1124 )	
B_CRAUS	EIN		DCAS ( 1128 ), DCKUP ( 1128 ), DCINS ( 1126 )
B_CSCATT	AUS	PROKON ( 53 )	LREB ( 739 )
B_CVT	AUS	PROKON ( 53 )	
B_CWDK	EIN		BBGANG ( 501 ), BBSAWE ( 557 ), CAN ( 1124 )
B_CWDSL	EIN		FUEDK ( 597 )
B_CWESAKT	AUS	ACIFI ( 1013 )	TC6MOD ( 1112 )
B_CWLSHDYN	EIN		TC6MOD ( 1112 )
B_CWLSHSCH	EIN		DLSAHK ( 339 ), TC6MOD ( 1112 )
B_DAGR	EIN		DLSAHK ( 339 ), TC6MOD ( 1112 )
B_DASH	AUS	MDFAW ( 508 )	FUERE ( 595 )
B_DASHV	EIN		BBSAWE ( 557 ), LLRBB ( 575 ), MDKOG ( 516 ), MDAUTG ( 515 )
B_DCDISCAN	AUS	SREAKT ( 963 )	ARMD ( 531 ), MDKOL ( 526 ), MDFAW ( 508 )
B_DCDISFR	AUS	ADVE ( 918 )	ADVE ( 918 )
B_DCDISR	AUS	BGDVE ( 934 )	BGDVE ( 934 )
B_DCDIS_C	AUS	UFMER ( 1060 )	ADVE ( 918 )
B_DCDIS_UM	AUS	UFMER ( 1060 )	
B_DCY	AUS	DDCY ( 1146 )	UFNC ( 1063 ), UFSPSC ( 1060 ), UFZWC ( 1075 ), URADCC ( 1049 ),
B_DDYLASH	LOK	DLSAHK ( 339 )	UFRLC ( 1066 ), UFREAC ( 1088 ), UFMET ( 1060 ), UFUE ( 1056 )
B_DDYLASH2	LOK	DLSAHK ( 339 )	DFPM ( 1132 ), DMDML ( 216 ), DTRIG ( 1139 )
B_DECR	LOK	STADAP ( 684 )	
B_DELAYSYN	LOK	NLPH ( 150 )	
B_DESEE	AUS	DECJ ( 1013 )	DKOSE ( 901 ), DEKPE ( 1020 ), DHLSVKE ( 902 ), DEVE ( 1017 ), DMILE ( 36 ),
B_DFRF	AUS	LR ( 768 )	DTEVE ( 1022 ), DMLSE ( 34 )



Symbol	Type	Created within	Used within
B_DFRF2	AUS	LR ( 768 )	
B_DFRM	AUS	LR ( 768 )	
B_DFRM2	AUS	LR ( 768 )	
B_DFUKABA	LOK	ESUKA ( 711 )	
B_DFUKAVA	LOK	ESUKA ( 711 )	
B_DIDYSCH	LOK	DLSAHK ( 339 )	
B_DIDYSCH2	LOK	DLSAHK ( 339 )	
B_DISCH	LOK	DLSAHK ( 339 )	
B_DISCH2	LOK	DLSAHK ( 339 )	
B_DISTP	AUS	DLSA ( 398 )	
B_DISTP2	AUS	DLSA ( 398 )	
B_DISTV	LOK	DLSA ( 398 )	
B_DISTV2	LOK	DLSA ( 398 )	
B_DKADEN	AUS	BGDVE ( 934 )	ADVE ( 918 ), DDVE ( 950 )
B_DKBEW	LOK	ADVE ( 918 )	
B_DKINI	LOK	DKAT ( 361 )	
B_DKINI2	LOK	DKAT ( 361 )	
B_DKLP1	LOK	DKAT ( 361 )	
B_DKLP2	LOK	DKAT ( 361 )	
B_DKNACH	LOK	BGDVE ( 934 )	
B_DKNOLU	AUS	SREAKT ( 963 )	SWADAP ( 47 ), ADVE ( 918 ), FGRABED ( 491 ), FUEDKSA ( 610 ), DLLR ( 578 ), NWS ( 618 ), NMAXMD ( 584 ), MDRED ( 976 ), LLRNS ( 562 ), KOS ( 896 ), AEVABU ( 1002 ), CAN ( 1124 ), BGRLP ( 266 ), BGDVE ( 934 )
B_DKNOLU_C	EIN		FGRABED ( 491 )
B_DKNOT	AUS	SREAKT ( 963 )	BGDVE ( 934 )
B_DKP1E	AUS	GGDVE ( 477 )	ADVE ( 918 ), SREAKT ( 963 ), DDVE ( 950 ), BGDVE ( 934 )
B_DKP1EV	LOK	GGDVE ( 477 )	
B_DKP1MN	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKP1MX	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKP1NP	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKP2E	AUS	GGDVE ( 477 )	ADVE ( 918 ), DDVE ( 950 ), BGDVE ( 934 ), SREAKT ( 963 )
B_DKP2EV	LOK	GGDVE ( 477 )	
B_DKP2MN	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKP2MX	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKP2NP	AUS	GGDVE ( 477 )	DDVE ( 950 )
B_DKPAW	EIN		SREAKT ( 963 ), GGDVE ( 477 )
B_DKPIU	AUS	SREAKT ( 963 )	ADVE ( 918 ), BGDVE ( 934 ), FUEDKSA ( 610 )
B_DKPRU	AUS	SREAKT ( 963 )	
B_DKPU	AUS	SREAKT ( 963 )	SWADAP ( 47 ), AEVABU ( 1002 ), NWS ( 618 ), NMAXMD ( 584 ), MDRED ( 976 ), LLRNS ( 562 ), KOS ( 896 ), GGDVE ( 477 ), DLLR ( 578 ), DMDSTP ( 205 ), FGRABED ( 491 ), CAN ( 1124 )
B_DKPU_C	EIN		FGRABED ( 491 )
B_DKSBEG	AUS	GGDVE ( 477 )	FGRABED ( 491 ), FUEDKSA ( 610 ), GGPED ( 454 )
B_DKSBEGT	AUS	GGDVE ( 477 )	
B_DKSBEG_C	EIN		GGDVE ( 477 )
B_DKTAKT	LOK	DKAT ( 361 )	
B_DKTAKT2	LOK	DKAT ( 361 )	
B_DKTEN	LOK	DKAT ( 361 )	
B_DKTEN2	LOK	DKAT ( 361 )	
B_DKTLP	AUS	DKAT ( 361 )	ESUKA ( 711 ), LR ( 768 )
B_DKTNR	LOK	DKAT ( 361 )	
B_DKTNR2	LOK	DKAT ( 361 )	
B_DKTPB2	LOK	DKAT ( 361 )	
B_DKTSB	LOK	DKAT ( 361 )	
B_DKTSB2	LOK	DKAT ( 361 )	
B_DKTSP	LOK	DKAT ( 361 )	
B_DKTSP2	LOK	DKAT ( 361 )	
B_DKTST	LOK	DKAT ( 361 )	
B_DKTST2	LOK	DKAT ( 361 )	
B_DKTT	LOK	DKAT ( 361 )	
B_DKTT2	LOK	DKAT ( 361 )	
B_DKTTK	LOK	DKAT ( 361 )	
B_DKTTK2	LOK	DKAT ( 361 )	
B_DKUEVAB	AUS	AEVABU ( 1002 )	AEVAB ( 980 )
B_DKUNB	LOK	SREAKT ( 963 )	
B_DKVSF	AUS	DKVS ( 811 )	
B_DKVSFM	LOK	DKVS ( 811 )	
B_DKVSTR	AUS	DKVS ( 811 )	
B_DLAFF	LOK	DLSA ( 398 )	
B_DLAFF2	LOK	DLSA ( 398 )	
B_DLASH	LOK	DLSAHK ( 339 )	
B_DLASH2	LOK	DLSAHK ( 339 )	
B_DLATP	AUS	DLSA ( 398 )	DLSSA ( 350 )
B_DLATP2	AUS	DLSA ( 398 )	DLSSA ( 350 )
B_DLATV	AUS	DLSA ( 398 )	
B_DLATV2	AUS	DLSA ( 398 )	
B_DLDPTE	AUS	GKRA ( 766 )	BBTEGA ( 750 ), TEBEB ( 762 ), DTEV ( 856 )
B_DLLR	AUS	DLLR ( 578 )	SWADAP ( 47 ), LLRRM ( 566 )
B_DLLRA	AUS	DLLR ( 578 )	DTEV ( 856 ), TEBEB ( 762 )
B_DLRBE	AUS	ADVE ( 918 )	DDVE ( 950 ), SREAKT ( 963 )
B_DLRIEN	AUS	BGDVE ( 934 )	
B_DLRIKLA	LOK	ADVE ( 918 )	





Symbol	Type	Created within	Used within
B_DLRIKLST	LOK	ADVE ( 918 )	
B_DLRPARC	LOK	ADVE ( 918 )	
B_DLRPIDE	AUS	ADVE ( 918 )	DDVE ( 950 ), SREAKT ( 963 )
B_DLRSPID	AUS	ADVE ( 918 )	BGDVE ( 934 )
B_DLRUMZU	LOK	ADVE ( 918 )	
B_DLUERK	AUS	DMDDLU ( 199 )	DMDLAD ( 215 )
B_DLUERK_M	EIN		NLPH ( 150 ), DMDDLU ( 199 )
B_DLUER_M2	LOK	DMDDLU ( 199 )	
B_DMASO	LOK	DLSV ( 301 )	
B_DMASO2	LOK	DLSV ( 301 )	
B_DMBV	EIN		DMDSTP ( 205 )
B_DMTLTZ	EIN		BBTEGA ( 750 ), DTEV ( 856 )
B_DMVERLIN	LOK	MDVER ( 546 )	
B_DNSLL	LOK	BBSAWE ( 557 )	
B_DNT	LOK	GGKS ( 412 )	
B_DNTB	LOK	GGKS ( 412 )	
B_DNWS	AUS	DNWS ( 622 )	
B_DOPZUE	AUS	NLPH ( 150 )	DMDLU ( 193 ), ZUE ( 627 ), RDE ( 112 ), NMAXMD ( 584 ), KRRA ( 639 )
B_DP	LOK	MDFAW ( 508 )	
B_DRLLKRDY	LOK	KRDY ( 659 )	
B_DS	LOK	DKRS ( 437 )	
B_DSHEN	LOK	DLSH ( 330 )	
B_DSHEN2	LOK	DLSH ( 330 )	
B_DSHK	LOK	DLSAHK ( 339 )	
B_DSHK2	LOK	DLSAHK ( 339 )	
B_DSI	LOK	DKRS ( 437 )	
B_DSL1	EIN		LR ( 768 )
B_DSL4	EIN		LR ( 768 )
B_DSLA	EIN		BBKHZ ( 890 ), LAKH ( 735 ), LAMKO ( 729 )
B_DSLME	EIN		LR ( 768 )
B_DSL5	EIN		BBSAWE ( 557 ), TEBEB ( 762 ), LRHK ( 781 ), LREB ( 739 ), LRAEB ( 759 ), DLSA ( 398 ), DLSV ( 301 ), DTEV ( 856 ), DLSH ( 330 ), DLSAHK ( 339 ), DLLR ( 578 ), DKAT ( 361 )
B_DSLSK	EIN		LREB ( 739 )
B_DSLSP4	LOK	AK ( 855 )	
B_DSLVH	EIN		BGMSZS ( 239 )
B_DSSV	EIN		BGMSZS ( 239 )
B_DSUV	EIN		BGMSZS ( 239 )
B_DSVEN	AUS	DLSV ( 301 )	
B_DSVEN2	AUS	DLSV ( 301 )	
B_DTEAA	AUS	DTEV ( 856 )	BGTEV ( 257 ), TEBEB ( 762 ), LRAEB ( 759 )
B_DTEAAB	LOK	DTEV ( 856 )	
B_DTEAAM	AUS	DTEV ( 856 )	
B_DTEAAV	AUS	GKRA ( 766 )	LLRRM ( 566 )
B_DTEABU	LOK	DTEV ( 856 )	
B_DTEANFL	LOK	DTEV ( 856 )	
B_DTEEND	LOK	DTEV ( 856 )	
B_DTEENDL	LOK	DTEV ( 856 )	
B_DTEENF	LOK	DTEV ( 856 )	
B_DTEFRE	LOK	DTEV ( 856 )	
B_DTEFRR	AUS	DTEV ( 856 )	GKRA ( 766 ), LR ( 768 ), LRINI ( 749 )
B_DTELAB	LOK	DTEV ( 856 )	
B_DTELBM	LOK	DTEV ( 856 )	
B_DTELBR	LOK	DTEV ( 856 )	
B_DTELNM	LOK	DTEV ( 856 )	
B_DTELNMB	LOK	DTEV ( 856 )	
B_DTELNMV	LOK	DTEV ( 856 )	
B_DTENAM	LOK	DTEV ( 856 )	
B_DTEPHM	LOK	DTEV ( 856 )	
B_DTEPM	LOK	DTEV ( 856 )	
B_DTERAB	LOK	DTEV ( 856 )	
B_DTERAP	LOK	DTEV ( 856 )	
B_DTERES	LOK	DTEV ( 856 )	
B_DTERNM	LOK	DTEV ( 856 )	
B_DTES	AUS	DTEV ( 856 )	GKRA ( 766 ), ATEV ( 969 ), BBTEGA ( 750 ), DKAT ( 361 ), MDVERAD ( 549 ), DLSV ( 301 ), DLSH ( 330 ), DLLR ( 578 )
B_DTEST	AUS	DTEV ( 856 )	DLSA ( 398 ), LRAEB ( 759 ), LR ( 768 ), DMDSTP ( 205 ), GKEB ( 737 ), LLR- RM ( 566 ), DLSAHK ( 339 )
B_DTEZAM	LOK	DTEV ( 856 )	
B_DTP	LOK	GGKS ( 412 )	
B_DTPB	LOK	GGKS ( 412 )	
B_DUPW	LOK	GGPED ( 454 )	
B_DUPW12	LOK	GGPED ( 454 )	
B_DUSHSCH	LOK	DLSAHK ( 339 )	
B_DUSHSCH2	LOK	DLSAHK ( 339 )	
B_DVEADA	AUS	BGDVE ( 934 )	AEVABZK (1003)
B_DVEADAMC	EIN		BGDVE ( 934 )
B_DVEADASC	EIN		BGDVE ( 934 )
B_DVEADAT	AUS	BGDVE ( 934 )	
B_DVEESE	EIN		DDVE ( 950 ), ADVE ( 918 )
B_DVEESH	LOK	ADVE ( 918 )	
B_DVEESON	EIN		ADVE ( 918 )



Symbol	Type	Created within	Used within
B_DVETE	AUS	ADVE ( 918 )	BGDVE ( 934 )
B_DVETV	LOK	BGDVE ( 934 )	
B_DWDKSUS	LOK	FUEDK ( 597 )	
B_DWDKSUT	LOK	FUEDK ( 597 )	
B_DYLASH	LOK	DLSAHK ( 339 )	
B_DYLASH2	LOK	DLSAHK ( 339 )	
B_EAGRNEWS	EIN		FUEDK ( 597 )
B_ECULOCK	EIN		AEVABZK (1003)
B_EDKS	AUS	GGDVE ( 477 )	DHFM ( 233 )
B_EDKVS	AUS	DKVS ( 811 )	BBTEGA ( 750 ), LRHK ( 781 ), LRA ( 797 ), DTEV ( 856 ), DMDSTP ( 205 ), DKAT ( 361 ), DLSAHK ( 339 ), DLSA ( 398 )
B_EDKVS2	AUS	DKVS ( 811 )	BBTEGA ( 750 ), DKAT ( 361 ), DTEV ( 856 ), LRHK ( 781 ), LRA ( 797 ), DLSAHK ( 339 ), DLSA ( 398 )
B_EDP	LOK	MDFAW ( 508 )	
B_EEV	AUS	DEVE (1017)	DMDSTP ( 205 ), LREB ( 739 )
B_EFRAO	LOK	DKVS ( 811 )	
B_EFRAO2	LOK	DKVS ( 811 )	
B_EFRAU	LOK	DKVS ( 811 )	
B_EFRAU2	LOK	DKVS ( 811 )	
B_EHFM	AUS	DHFM ( 233 )	EGFE ( 228 )
B_EHFM1	LOK	DHFM ( 233 )	
B_EHFS	AUS	DHFM ( 233 )	DUF (1089), GGDVE ( 477 ), UFRCL (1066)
B_EHSV	LOK	DHLSVK ( 29 )	
B_EHSV2	LOK	DHLSVK ( 29 )	
B_EKATS	LOK	DKAT ( 361 )	
B_EKATS2	LOK	DKAT ( 361 )	
B_EKP	AUS	AEKP ( 970 )	
B_EKPD	LOK	AEKP ( 970 )	
B_EKPN	LOK	AEKP ( 970 )	
B_EKPUBN	LOK	AEKP ( 970 )	
B_EKPV	LOK	AEKP ( 970 )	
B_EKS	LOK	KRRA ( 639 )	
B_ELLS	EIN		BBSAWE ( 557 ), BGPU ( 276 ), DLLR ( 578 ), LREB ( 739 ), DTEV ( 856 ), BGMSZS ( 239 )
B_ELMI	AUS	DHFM ( 233 )	BGPU ( 276 )
B_ELS	LOK	MDFAW ( 508 )	
B_ELZMN	LOK	KRRA ( 639 )	
B_ENABALE	LOK	ALE ( 136 )	
B_ENABDDG	LOK	DDG ( 141 )	
B_ENABRDE	LOK	RDE ( 112 )	
B_ENFMST	LOK	DLSAHK ( 339 )	
B_ENLASH	LOK	DLSAHK ( 339 )	
B_ENLASH2	LOK	DLSAHK ( 339 )	
B_ENLLR1	AUS	LLRBB ( 575 )	WDKSOM ( 614 )
B_ENQSYN	LOK	GGDPG ( 74 )	
B_ENRINH	LOK	GGLSH ( 318 )	
B_ENRINH2	LOK	GGLSH ( 318 )	
B_ENRINV	LOK	GGLSV ( 382 )	
B_ENRINV2	LOK	GGLSV ( 382 )	
B_ENWS	AUS	DNWS ( 622 )	DLSA ( 398 ), DMDSTP ( 205 ), DTEV ( 856 ), LRAEB ( 759 ), ESUKA ( 711 )
B_EOBDLR	AUS	LREB ( 739 )	TEBEB ( 762 )
B_EOBDLR2	AUS	LREB ( 739 )	
B_EPCL	AUS	DEPCL (1151)	
B_ERBR	LOK	GGEGAS ( 474 )	
B_ERDKT	LOK	DKAT ( 361 )	
B_ERDKT2	LOK	DKAT ( 361 )	
B_ERINOFH	LOK	GGLSH ( 318 )	
B_ERINOFH2	LOK	GGLSH ( 318 )	
B_ERINOFV	LOK	GGLSV ( 382 )	
B_ERINOFV2	LOK	GGLSV ( 382 )	
B_ERKAT	LOK	DKVS ( 811 )	
B_ERKAT2	LOK	DKVS ( 811 )	
B_ERKAZ	LOK	DKVS ( 811 )	
B_ERKAZ2	LOK	DKVS ( 811 )	
B_ERRKUP	AUS	DVKUP (1027)	SREAKT ( 963 )
B_ESDIA	AUS	DECJ (1013)	
B_ESGCAN	EIN		AEVABZK (1003), DUF (1089), DMDSTP ( 205 ), BBTEGA ( 750 ), SREAKT ( 963 )
B_ESLS	EIN		DLSH ( 330 ), DLSV ( 301 ), LREB ( 739 )
B_EVABU	AUS	AEVABU (1002)	AEVABZK (1003)
B_EVABZ	AUS	AEVAB ( 980 )	
B_EVABZ1	LOK	AEVAB ( 980 )	
B_EVASEL	AUS	AES ( 973 )	AEVAB ( 980 ), DMDSTP ( 205 )
B_EVASGA	EIN		AEVABZK (1003)
B_EVLOC	AUS	AES ( 973 )	BGEVAB (1005), ATEV ( 969 ), DMDSTP ( 205 ), DLSAHK ( 339 ), TEB ( 826 ), LREB ( 739 )
B_F1GETR	AUS	PROKON ( 53 )	
B_FA	EIN		BBKHZ ( 890 ), DKAT ( 361 ), DLSH ( 330 ), DNWS ( 622 ), LRA ( 797 ), NWS ( 618 ), LRAEB ( 759 ), DTEV ( 856 ), DLSA ( 398 ), DKVS ( 811 )
B_FAAN	EIN		DMDSTP ( 205 )
B_FAATM	EIN		ATM ( 20 )
B_FABR	EIN		GGPED ( 454 )



Symbol	Type	Created within	Used within
B_FAEVZ	EIN		AES ( 973 ), AEVAB ( 980 )
B_FAKAT	EIN		DKAT ( 361 ), LLRNFA ( 564 )
B_FAKAT2	EIN		DKAT ( 361 )
B_FAKVS	EIN		DKVS ( 811 ), LLRNFA ( 564 ), LRA ( 797 )
B_FALRA	EIN		LRAEB ( 759 )
B_FALSH	EIN		DLSH ( 330 ), LLRNFA ( 564 ), LAMKO ( 729 ), LRHK ( 781 )
B_FALSH2	EIN		DLSH ( 330 ), LAMKO ( 729 ), LRHK ( 781 )
B_FALSV	EIN		LLRNFA ( 564 )
B_FAN	EIN		DMDSTP ( 205 )
B_FANWS	EIN		DNWS ( 622 ), NWS ( 618 )
B_FASH	EIN		DLSAHK ( 339 ), LLRNFA ( 564 )
B_FASH2	EIN		DLSAHK ( 339 )
B_FASLA	EIN		BBKHZ ( 890 ), KHMD ( 894 ), LAMKO ( 729 ), LAKH ( 735 )
B_FATES	EIN		DTEV ( 856 ), LRAEB ( 759 )
B_FATP	EIN		DLSA ( 398 )
B_FATP2	EIN		DLSA ( 398 )
B_FATV	EIN		DLSA ( 398 )
B_FATV2	EIN		DLSA ( 398 )
B_FBM	AUS	GGDPG ( 74 )	DDG ( 141 ), RDE ( 112 ), DMDSTP ( 205 )
B_FDYFGR	EIN		FGRABED ( 491 ), FGRUE ( 490 )
B_FF	AUS	ZUESZ ( 632 )	
B_FGR	AUS	MDFAW ( 508 )	ARMD ( 531 ), UFUE ( 1056 ), UFFGRC ( 1078 ), MDZUL ( 523 ), FGR- REGL ( 1174 ), FGRFULO ( 1160 ), FGRABED ( 491 ), DUF ( 1089 )
B_FGRAB	AUS	FGRREGL ( 1174 )	FGRUE ( 490 ), UFFGRE ( 1096 )
B_FGRAT	AUS	GGFGRH ( 473 )	FGRABED ( 491 ), FGRUE ( 490 )
B_FGRDVI	LOK	FGRREGL ( 1174 )	
B_FGREN	AUS	FGRREGL ( 1174 )	FGRUE ( 490 ), FGRABED ( 491 )
B_FGRENJUM	AUS	UFFGRE ( 1096 )	UFFGRC ( 1078 )
B_FGRHE	AUS	GGFGRH ( 473 )	FGRABED ( 491 ), FGRUE ( 490 )
B_FGRHEV	LOK	GGFGRH ( 473 )	
B_FGRHSA	AUS	GGFGRH ( 473 )	FGRABED ( 491 ), FGRUE ( 490 )
B_FGRTBE	LOK	FGRUE ( 490 )	
B_FGRTBH	AUS	GGFGRH ( 473 )	FGRBESI ( 1158 ), FGRUE ( 490 )
B_FGRTSB	AUS	GGFGRH ( 473 )	FGRBESI ( 1158 )
B_FGRTSE	LOK	FGRUE ( 490 )	
B_FGRTSV	AUS	GGFGRH ( 473 )	FGRBESI ( 1158 )
B_FGRTVE	LOK	FGRUE ( 490 )	
B_FGRTVH	AUS	GGFGRH ( 473 )	FGRBESI ( 1158 ), FGRUE ( 490 )
B_FGRTWA	AUS	GGFGRH ( 473 )	FGRBESI ( 1158 ), FGRUE ( 490 )
B_FGRJUM	AUS	UFFGRC ( 1078 )	UFUE ( 1056 ), DUF ( 1089 ), FGRABED ( 491 )
B_FHZ	EIN		LLRNS ( 562 )
B_FIL	AUS	MDFAW ( 508 )	LLRBB ( 575 ), MDKOG ( 516 ), MDAUTG ( 515 )
B_FKMSDKS	AUS	FUEDK ( 597 )	BGMSZS ( 239 ), FUEREG ( 595 )
B_FKMSMN	AUS	BGMSZS ( 239 )	DEGFE ( 592 )
B_FKMSMX	AUS	BGMSZS ( 239 )	DEGFE ( 592 )
B_FKPVDK	AUS	BGMSZS ( 239 )	
B_FKPVMN	AUS	BGMSZS ( 239 )	DEGFE ( 592 )
B_FKPVMX	AUS	BGMSZS ( 239 )	DEGFE ( 592 )
B_FLBC	EIN		DCINS ( 1126 ), GGPOEL ( 296 )
B_FMFKRC	AUS	GGKS ( 412 )	KRKE ( 427 )
B_FNSOFF	LOK	ESNSWL ( 691 )	
B_FODO	LOK	DMDFON ( 161 )	
B_FODON	LOK	DMDFON ( 161 )	
B_FOF	DOK	DMDFON ( 161 )	
B_FOFSTP	AUS	DMDSTP ( 205 )	DMDFON ( 161 )
B_FOFSTPC	EIN		DMDSTP ( 205 )
B_FOFSTPT	AUS	DMDSTP ( 205 )	
B_FOFJM	LOK	DMDFON ( 161 )	
B_FOHE	LOK	DMDFON ( 161 )	
B_FOHOLD	LOK	DMDFON ( 161 )	
B_FOLUNW	LOK	DMDFON ( 161 )	
B_FON	DOK	DMDFON ( 161 )	
B_FONSTP	AUS	DMDSTP ( 205 )	DMDFON ( 161 )
B_FONSTPC	EIN		DMDSTP ( 205 )
B_FONSTPT	AUS	DMDSTP ( 205 )	
B_FONTM	LOK	DMDFON ( 161 )	
B_FONJM	LOK	DMDFON ( 161 )	DMDSTP ( 205 )
B_FOPHSNL	LOK	AEVAB ( 980 )	
B_FOR	DOK	DMDFON ( 161 )	
B_FOR11	LOK	DMDFON ( 161 )	
B_FOR12	LOK	DMDFON ( 161 )	
B_FOR13	LOK	DMDFON ( 161 )	
B_FOR21	LOK	DMDFON ( 161 )	
B_FOR22	LOK	DMDFON ( 161 )	
B_FOR23	LOK	DMDFON ( 161 )	
B_FOR31	LOK	DMDFON ( 161 )	
B_FOR32	LOK	DMDFON ( 161 )	
B_FOR33	LOK	DMDFON ( 161 )	
B_FOR41	LOK	DMDFON ( 161 )	
B_FOR42	LOK	DMDFON ( 161 )	
B_FOR43	LOK	DMDFON ( 161 )	
B_FOR51	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
B_FOR52	LOK	DMDFON ( 161 )	
B_FOR53	LOK	DMDFON ( 161 )	
B_FOR61	LOK	DMDFON ( 161 )	
B_FOR62	LOK	DMDFON ( 161 )	
B_FOR63	LOK	DMDFON ( 161 )	
B_FOR71	LOK	DMDFON ( 161 )	
B_FOR72	LOK	DMDFON ( 161 )	
B_FOR73	LOK	DMDFON ( 161 )	
B_FOR81	LOK	DMDFON ( 161 )	
B_FOR82	LOK	DMDFON ( 161 )	
B_FOR83	LOK	DMDFON ( 161 )	
B_FORDO	DOK	DMDFON ( 161 )	
B_FORDOJM	LOK	DMDFON ( 161 )	
B_FORN	DOK	DMDFON ( 161 )	
B_FORN01	LOK	DMDFON ( 161 )	
B_FORN02	LOK	DMDFON ( 161 )	
B_FORN03	LOK	DMDFON ( 161 )	
B_FORN04	LOK	DMDFON ( 161 )	
B_FORN05	LOK	DMDFON ( 161 )	
B_FORN06	LOK	DMDFON ( 161 )	
B_FORN07	LOK	DMDFON ( 161 )	
B_FORN08	LOK	DMDFON ( 161 )	
B_FORN_M	LOK	DMDFON ( 161 )	
B_FORSET	LOK	DMDFON ( 161 )	
B_FORUN	LOK	DMDFON ( 161 )	
B_FOR_M	LOK	DMDFON ( 161 )	
B_FOS	LOK	DMDFON ( 161 )	
B_FOXFG	LOK	DMDFON ( 161 )	
B_FPRAKT	LOK	BGDVE ( 934 )	
B_FPROAB	AUS	BGDVE ( 934 )	DDVE ( 950 ), SREAKT ( 963 )
B_FPROE	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_FPROOK	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_FPRORDY	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_FPROVB	LOK	BGDVE ( 934 )	
B_FPRRDY	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_FPRZAB	AUS	BGDVE ( 934 )	DDVE ( 950 ), SREAKT ( 963 )
B_FPRZE	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_FPRZOK	LOK	BGDVE ( 934 )	
B_FPRZVB	LOK	BGDVE ( 934 )	
B_FPWDKAP	AUS	PROKON ( 53 )	FUEDK ( 597 )
B_FRAB	AUS	LR ( 768 )	
B_FRAB2	AUS	LR ( 768 )	
B_FRAO	AUS	LRA ( 797 )	BBTEGA ( 750 ), DKVS ( 811 )
B_FRAOAN	AUS	BBTEGA ( 750 )	TEBEB ( 762 )
B_FRAOANC	EIN		BBTEGA ( 750 )
B_FRAOR	AUS	LRA ( 797 )	
B_FRAOR2	AUS	LRA ( 797 )	
B_FRAT	LOK	LRA ( 797 )	
B_FRAU	AUS	LRA ( 797 )	DKVS ( 811 )
B_FRAUR	AUS	LRA ( 797 )	DKVS ( 811 )
B_FRAUR2	AUS	LRA ( 797 )	DKVS ( 811 )
B_FRGBS	LOK	FGRBESI ( 1158 )	
B_FRINI	AUS	LRINI ( 749 )	LR ( 768 ), GKRA ( 766 )
B_FRINI2	AUS	LRINI ( 749 )	LR ( 768 )
B_FRMAX	AUS	LR ( 768 )	DKAT ( 361 ), ESUKA ( 711 ), DLSH ( 330 ), TEB ( 826 )
B_FRMAX2	AUS	LR ( 768 )	DKAT ( 361 ), TEB ( 826 ), ESUKA ( 711 ), DLSH ( 330 )
B_FRMIN	AUS	LR ( 768 )	DKAT ( 361 ), ESUKA ( 711 ), TEB ( 826 )
B_FRMIN2	AUS	LR ( 768 )	DKAT ( 361 ), ESUKA ( 711 ), TEB ( 826 )
B_FRMINI	LOK	LR ( 768 )	
B_FRMINI2	LOK	LR ( 768 )	
B_FRMLASH	LOK	DLSAHK ( 339 )	
B_FRMLASH2	LOK	DLSAHK ( 339 )	
B_FRSP	LOK	LR ( 768 )	
B_FRSP2	LOK	LR ( 768 )	
B_FRSTE	LOK	DKVS ( 811 )	
B_FRSTE2	LOK	DKVS ( 811 )	
B_FS	AUS	BBGANG ( 501 )	BBKHZ ( 890 ), BBSAWE ( 557 ), MDWAN ( 554 ), MDVERAD ( 549 ), LL-RNS ( 562 ), LLRNFA ( 564 ), LLRBB ( 575 ), DTEV ( 856 )
B_FSLR	LOK	LREB ( 739 )	
B_FSLR2	LOK	LREB ( 739 )	
B_FSU	DOK	MDWAN ( 554 )	
B_FTBFWF	AUS	GGPED ( 454 )	
B_FTEDAB	AUS	DTEV ( 856 )	TEBEB ( 762 )
B_FTFFP1P	AUS	GGPED ( 454 )	
B_FTFFP2P	AUS	GGPED ( 454 )	
B_FTFFPP	AUS	GGPED ( 454 )	
B_FTKAT	AUS	DKAT ( 361 )	
B_FTKAT2	AUS	DKAT ( 361 )	
B_FTLM	AUS	DHFM ( 233 )	
B_FTLSV	AUS	DLSV ( 301 )	
B_FTLSV2	AUS	DLSV ( 301 )	
B_FTMDB	AUS	MDKOG ( 516 )	



Symbol	Type	Created within	Used within
B_FTTES	AUS	DTEV ( 856 )	
B_FURENA	LOK	FUEREG ( 595 )	
B_FURPEN	LOK	FUEREG ( 595 )	
B_FWE	LOK	ESWE ( 698 )	
B_GAE	AUS	DKVS ( 811 )	BBTEGA ( 750 ), DTEV ( 856 ), GKEB ( 737 )
B_GAE2	EIN		GKEB ( 737 )
B_GAEFRA	AUS	DKVS ( 811 )	BBTEGA ( 750 )
B_GAEFRA2	AUS	DKVS ( 811 )	BBTEGA ( 750 )
B_GAEING	EIN		DLSAHK ( 339 ), DKVS ( 811 )
B_GAEING2	EIN		DLSAHK ( 339 ), DKVS ( 811 )
B_GAP	AUS	BBTEGA ( 750 )	GKEB ( 737 ), DTEV ( 856 ), LRAEB ( 759 )
B_GAPNLDG	LOK	NLDG ( 157 )	
B_GASP	AUS	LRAEB ( 759 )	BBTEGA ( 750 ), DLSA ( 398 ), GKEB ( 737 )
B_GASP2	EIN		DLSA ( 398 )
B_GEKO	EIN		KOS ( 896 )
B_GLF	LOK	GGPED ( 454 )	
B_GRDST	EIN		BBTEGA ( 750 ), DTEV ( 856 ), KOS ( 896 )
B_GSCH	EIN		KOS ( 896 ), NWS ( 618 )
B_GWHS	AUS	BBGANG ( 501 )	ARMD ( 531 ), MDFAW ( 508 ), KOS ( 896 ), FGRUE ( 490 ), FGRABED ( 491 )
B_GWRTE	LOK	TEB ( 826 )	
B_HAG	AUS	BGPU ( 276 )	BBKHZ ( 890 ), DTEV ( 856 )
B_HFM	AUS	DHFM ( 233 )	BGMSZS ( 239 ), BGSRM ( 245 ), UFRLC ( 1066 ), EGFE ( 228 )
B_HLL	LOK	LLRNS ( 562 )	
B_HOLP1	LOK	GGPED ( 454 )	
B_HOLP1A	LOK	GGPED ( 454 )	
B_HOLP1L	LOK	GGPED ( 454 )	
B_HOLP2	LOK	GGPED ( 454 )	
B_HOLP2A	LOK	GGPED ( 454 )	
B_HOLP2L	LOK	GGPED ( 454 )	
B_HOP1MN	LOK	GGPED ( 454 )	
B_HOP2MN	LOK	GGPED ( 454 )	
B_HOPAKT	LOK	GGPED ( 454 )	
B_HPNMOT	AUS	ARMD ( 531 )	
B_HREVAB	EIN		KOEVAB ( 124 )
B_HSHE	AUS	HLS ( 392 )	DHLSHK ( 1154 ), DLSH ( 330 )
B_HSHE2	AUS	HLS ( 392 )	DHLSHK ( 1154 ), DLSH ( 330 )
B_HSHMX	LOK	HLS ( 392 )	
B_HSHMX2	LOK	HLS ( 392 )	
B_HSOKV	LOK	DHLSVK ( 29 )	
B_HSOKV2	LOK	DHLSVK ( 29 )	
B_HSRDY	AUS	DIMC ( 1148 )	
B_HST	AUS	ESSTT ( 679 )	ESNSWL ( 691 ), GGTFM ( 289 ), ESVST ( 677 )
B_HSVE	AUS	HLS ( 392 )	DHLSVKE ( 902 ), DLSV ( 301 )
B_HSVE2	AUS	HLS ( 392 )	DHLSVKE ( 902 ), DLSV ( 301 )
B_HSVMX	LOK	HLS ( 392 )	
B_HSVMX2	LOK	HLS ( 392 )	
B_JFLSD	LOK	MDFAW ( 508 )	
B_JFUKABA	LOK	ESUKA ( 711 )	
B_JFUKAVA	LOK	ESUKA ( 711 )	
B_JIPUMS	LOK	BGPU ( 276 )	
B_JKLREST	LOK	ADVE ( 918 )	
B_JKLSTAR	LOK	ADVE ( 918 )	
B_JLMLKAT	AUS	LRKA ( 795 )	
B_JLMLKAT2	AUS	LRKA ( 795 )	
B_JMLKVSE	LOK	DKVS ( 811 )	
B_JNCR	LOK	STADAP ( 684 )	
B_JNI	EIN		ATWAL ( 297 ), GGPOEL ( 296 ), MDWAN ( 554 )
B_JNIAR	AUS	ARMD ( 531 )	
B_JNIARV	AUS	ARMD ( 531 )	
B_JNIFRM	LOK	LR ( 768 )	
B_JNIFRM2	LOK	LR ( 768 )	
B_JNS1NEW	EIN		DCINS ( 1126 )
B_JNT	LOK	LR ( 768 )	
B_JNT2	LOK	LR ( 768 )	
B_JSOPROT	EIN		SCATT ( 1097 ), TC9MOD ( 1121 ), TC1MOD ( 1100 ), TC5MOD ( 1110 ), TC6MOD ( 1112 ), TC8MOD ( 1120 ), TC2MOD ( 1107 )
B_J_SKA	AUS	UFEING ( 1058 )	UFMVER ( 1087 ), UFRLC ( 1066 ), UFREAC ( 1088 ), UFUE ( 1056 )
B_J_SKA_FR	AUS	SREAKT ( 963 )	UFEING ( 1058 ), UFUE ( 1056 )
B_J_SKA_UM	AUS	UFMVER ( 1087 )	URADCC ( 1049 ), UFZWC ( 1075 ), UFSPSC ( 1060 ), UFNC ( 1063 ), UFUE ( 1056 ), UFRLC ( 1066 ), UFREAC ( 1088 ), ADVE ( 918 ), SREAKT ( 963 ), FUED-KSA ( 610 ), DUF ( 1089 ), BGDVE ( 934 ), AEVABU ( 1002 )
B_KATFZ	AUS	PROKON ( 53 )	BBKHZ ( 890 ), DIMC ( 1148 )
B_KATH	AUS	PROKON ( 53 )	DIMC ( 1148 )
B_KATHRDY	AUS	DIMC ( 1148 )	
B_KATRDY	AUS	DIMC ( 1148 )	
B_KAWE	LOK	LRKA ( 795 )	
B_KAWE2	LOK	LRKA ( 795 )	
B_KFVSWK	LOK	FGRFULO ( 1160 )	
B_KFWEE	LOK	ESVW ( 1009 )	
B_KH	AUS	AK ( 855 )	BBKHZ ( 890 ), ATM ( 20 ), BBSAWE ( 557 ), DMDLU ( 193 ), LAKH ( 735 ), LLRMR ( 572 ), MDAUTG ( 515 ), NWS ( 618 ), MDKOG ( 516 ), ZWMIN ( 669 ), LAMKO ( 729 ), KHMD ( 894 ), DDMDFON ( 161 )



Symbol	Type	Created within	Used within
B_KHA	AUS	BBKHZ ( 890 )	LLRRM ( 566 ), AK ( 855 )
B_KHAB	AUS	BBKHZ ( 890 )	AK ( 855 )
B_KHLL	LOK	BBKHZ ( 890 )	
B_KHLL	LOK	BBKHZ ( 890 )	
B_KHLLMX	LOK	BBKHZ ( 890 )	
B_KHNN	EIN		LLRNS ( 562 ), BBKHZ ( 890 )
B_KL	AUS	EGKE ( 409 )	KRKE ( 427 ), KRDY ( 659 ), KRRA ( 639 )
B_KL15	EIN		ADVE ( 918 ), DCKUP ( 1128 ), DCINS ( 1126 ), RDE ( 112 ), MOT AUS ( 1028 ), LFS ( 69 ), GGDPG ( 74 ), DMIL ( 1150 ), ALE ( 136 ), CAN ( 1124 ), DCAS ( 1128 )
B_KL50	EIN		RDE ( 112 )
B_KLAFBG	LOK	FUEDK ( 597 )	
B_KLDF	LOK	LLRNS ( 562 )	
B_KLDYNRM	LOK	KRDY ( 659 )	
B_KLDYSTK	LOK	KRDY ( 659 )	
B_KLIMA	AUS	PROKON ( 53 )	
B_KLLKNL	DOK	NLDG ( 157 )	
B_KMMIL	AUS	DMIL ( 1150 )	BGKMST ( 1008 )
B_KMMILSCT	EIN		TC1MOD ( 1100 )
B_KO	EIN		KOS ( 896 ), LLRNS ( 562 ), MDFAW ( 508 )
B_KOA	LOK	KOS ( 896 )	
B_KOBAUS	LOK	KOS ( 896 )	
B_KOBMNON	LOK	KOS ( 896 )	
B_KOBPED	LOK	KOS ( 896 )	
B_KOBPEDT	LOK	KOS ( 896 )	
B_KOBWPEDT	LOK	KOS ( 896 )	
B_KOE	AUS	KOS ( 896 )	BBSAWE ( 557 ), DMDSTP ( 205 ), DTEV ( 856 ), DKOSE ( 901 ), MDVER-AD ( 549 ), MDVERB ( 540 ), LRA ( 797 )
B_KOENA	LOK	KOS ( 896 )	
B_KOENAT	LOK	KOS ( 896 )	
B_KOEVAB	AUS	KOEVAB ( 124 )	AEVABZK ( 1003 )
B_KOINT	LOK	KOS ( 896 )	
B_KOMNOFF	LOK	KOS ( 896 )	
B_KOMNON	LOK	KOS ( 896 )	
B_KOMXOFF	LOK	KOS ( 896 )	
B_KOOFF	LOK	KOS ( 896 )	
B_KOOFFT	LOK	KOS ( 896 )	
B_KOTMSK	LOK	KOS ( 896 )	
B_KOTMSKO	LOK	KOS ( 896 )	
B_KOV	AUS	KOS ( 896 )	
B_KOVDOWN	LOK	KOS ( 896 )	
B_KOWPED	LOK	KOS ( 896 )	
B_KR	AUS	KRDY ( 659 )	KRRA ( 639 ), DKRS ( 437 ), KRKE ( 427 ), GGKS ( 412 ), EGKE ( 409 )
B_KRA	LOK	KRRA ( 639 )	
B_KRDWS	AUS	EGKE ( 409 )	KRRA ( 639 ), KRDY ( 659 )
B_KRFDKS	AUS	KRRA ( 639 )	DKRS ( 437 )
B_KRGZ	LOK	KRRA ( 639 )	
B_KRKEZ	AUS	KRRA ( 639 )	
B_KRLDY	AUS	KRDY ( 659 )	DKRS ( 437 ), EGKE ( 409 ), GGKS ( 412 ), KRRA ( 639 ), KRKE ( 427 )
B_KRLDYA	AUS	KRDY ( 659 )	KRRA ( 639 ), EGKE ( 409 )
B_KRLDYF	LOK	KRDY ( 659 )	
B_KRLDYV	LOK	KRDY ( 659 )	
B_KRLZ	AUS	KRRA ( 639 )	
B_KRLZN	LOK	KRRA ( 639 )	
B_KRNDY	AUS	KRDY ( 659 )	DKRS ( 437 ), KRRA ( 639 ), EGKE ( 409 ), KRKE ( 427 ), GGKS ( 412 )
B_KRNL	AUS	KRRA ( 639 )	KRKE ( 427 )
B_KRSYNE	LOK	KRRA ( 639 )	
B_KRVF	LOK	KRRA ( 639 )	
B_KSTAI	LOK	STADAP ( 684 )	
B_KSTAUE	LOK	STADAP ( 684 )	
B_KSTEBF	EIN		AEKP ( 970 )
B_KS_MINJ	LOK	DKRS ( 437 )	
B_KUP1NEW	EIN		CAN ( 1124 ), DCKUP ( 1128 ), DVKUP ( 1027 )
B_KUPGW	AUS	ARMD ( 531 )	
B_KUPPL	AUS	EGEG ( 453 )	GGEGAS ( 474 ), SWADAP ( 47 ), ARMD ( 531 ), FGRUE ( 490 ), KRDY ( 659 ), LLRMR ( 572 ), LLRBB ( 575 ), ZWMIN ( 669 ), MDFAW ( 508 ), KOS ( 896 ), FGRABED ( 491 ), BBSAWE ( 557 ), DMDSTP ( 205 )
B_KUPPLV	AUS	GGEGAS ( 474 )	MDFAW ( 508 ), MDKOG ( 516 )
B_KVSFFL	LOK	DKVS ( 811 )	
B_KVTA	AUS	BGKV ( 71 )	
B_KW	AUS	BBKHZ ( 890 )	ATM ( 20 ), MDKOG ( 516 ), ZWMIN ( 669 ), MDAUTG ( 515 ), KHMD ( 894 ), AK ( 855 )
B_LALGF	AUS	LAMKO ( 729 )	LAMSOLL ( 726 )
B_LALGF2	AUS	LAMKO ( 729 )	LAMSOLL ( 726 )
B_LAMBTS	LOK	LAMKO ( 729 )	
B_LAMBTS2	LOK	LAMKO ( 729 )	
B_LAMEND	LOK	DLSAHK ( 339 )	
B_LAMEND2	LOK	DLSAHK ( 339 )	
B_LAMKA	EIN		TEBEB ( 762 ), LAMKO ( 729 )
B_LAMKA2	EIN		TEBEB ( 762 ), LAMKO ( 729 )
B_LAMLASH	EIN		LAMKO ( 729 ), DLSAHK ( 339 )
B_LAMLASH2	EIN		LAMKO ( 729 ), DLSAHK ( 339 )



Symbol	Type	Created within	Used within
B_LAMNSE	EIN		LAMKO ( 729 )
B_LAMNSWL	LOK	LAMKO ( 729 )	
B_LAMPE	AUS	ATWAL ( 297 )	
B_LAMSDEF	AUS	LAMKO ( 729 )	TEBEB ( 762 )
B_LAMVERG	LOK	DLSAHK ( 339 )	
B_LAMVERG2	LOK	DLSAHK ( 339 )	
B_LCLMOD5	LOK	DLSSA ( 350 )	
B_LCLMOD52	LOK	DLSSA ( 350 )	
B_LDEF	LOK	LAMKO ( 729 )	
B_LDEF2	LOK	LAMKO ( 729 )	
B_LDDB	EIN		LAMFAW ( 728 )
B_LDPI	EIN		DTEV ( 856 ), TEBEB ( 762 )
B_LDRUGD	EIN		DHFM ( 233 ), FUEDK ( 597 )
B_LDSAFW	AUS	PROKON ( 53 )	
B_LDSAPP	AUS	PROKON ( 53 )	
B_LF1NBRES	AUS	LFS ( 69 )	MDVERB ( 540 )
B_LF1S	AUS	LFS ( 69 )	DMLSE ( 34 ), MDVERB ( 540 )
B_LF2NBRES	AUS	LFS ( 69 )	MDVERB ( 540 )
B_LF2S	AUS	LFS ( 69 )	DMLSE ( 34 ), MDVERB ( 540 )
B_LFB1	LOK	LFS ( 69 )	
B_LFB2	LOK	LFS ( 69 )	
B_LKKNLNL	DOK	NLDG ( 157 )	
B_LLL	AUS	MDFAW ( 508 )	MSF ( 506 ), ARMD ( 531 ), BBKHZ ( 890 ), BBSAW ( 557 ), BGRLP ( 266 ), ESWE ( 698 ), ESUK ( 699 ), DTEV ( 856 ), DMDSTP ( 205 ), DMDLU ( 193 ), DLLR ( 578 ), DDST ( 851 ), BGPU ( 276 ), LREB ( 739 ), LR ( 768 ), LLRNS ( 562 ), LLRNFA ( 564 ), LLRMR ( 572 ), LLRBB ( 575 ), KRDY ( 659 ), KOS ( 896 ), GKRA ( 766 ), GGTF ( 298 ), WANWKW ( 125 ), NWS ( 618 ), NLPH ( 150 ), MDKOG ( 516 ), MDAUTG ( 515 ), GGHF ( 230 ), FUEDKSA ( 610 ), BBTEGA ( 750 ), EGFE ( 228 )
B_LLDIA	LOK	DLLR ( 578 )	
B_LLR	AUS	LLRBB ( 575 )	DLLR ( 578 ), DTEV ( 856 ), MDVERAD ( 549 ), LLRRM ( 566 ), LLRMD ( 561 )
B_LLRREIN	AUS	LLRBB ( 575 )	LLRMD ( 561 ), FUEDK ( 597 ), MDKOG ( 516 ), MDVERAD ( 549 ), MDVER ( 546 ), ZWSTT ( 637 ), ZWMIN ( 669 ), ZUE ( 627 ), WDKSOM ( 614 ), MDVERB ( 540 ), MDKOL ( 526 ), LLRNS ( 562 ), LLRRM ( 566 )
B_LLRRI	AUS	LLRBB ( 575 )	LLRRM ( 566 ), LLRMD ( 561 )
B_LLRPD	AUS	LLRBB ( 575 )	FUEREG ( 595 ), LLRRM ( 566 ), LLRMD ( 561 )
B_LLRPKH	LOK	LLRRM ( 566 )	
B_LLRPST	LOK	LLRRM ( 566 )	
B_LLRST	AUS	LLRRM ( 566 )	LLRNS ( 562 )
B_LLVFGR	AUS	FGRREGL ( 1174 )	FGRUE ( 490 ), MDFAW ( 508 )
B_LLVFGRC	EIN		FGRREGL ( 1174 )
B_LMSSLOF	EIN		BBKHZ ( 890 )
B_LR	AUS	GKEB ( 737 )	LREB ( 739 ), BBTEGA ( 750 ), TEBEB ( 762 ), TEB ( 826 ), LRHK ( 781 ), LRAEB ( 759 ), LRA ( 797 ), ESUKA ( 711 ), DTEV ( 856 ), DLSV ( 301 ), DL-SA ( 398 ), DKVS ( 811 ), DKAT ( 361 ), GKRA ( 766 )
B_LR2	AUS	GKEB ( 737 )	LREB ( 739 ), BBTEGA ( 750 ), TEBEB ( 762 ), TEB ( 826 ), LRHK ( 781 ), LRAEB ( 759 ), LRA ( 797 ), DKVS ( 811 ), DLSA ( 398 ), DTEV ( 856 ), ESUKA ( 711 ), DLSV ( 301 ), DKAT ( 361 ), GKRA ( 766 )
B_LR2S	LOK	LREB ( 739 )	
B_LR2S2	LOK	LREB ( 739 )	
B_LR2V	LOK	LRHK ( 781 )	
B_LRA	AUS	GKEB ( 737 )	LRAEB ( 759 ), DKVS ( 811 ), LRA ( 797 ), GKRA ( 766 )
B_LRA2	AUS	GKEB ( 737 )	LRAEB ( 759 ), DKVS ( 811 ), LRA ( 797 ), GKRA ( 766 )
B_LRACT	AUS	LREB ( 739 )	
B_LRACT2	AUS	LREB ( 739 )	
B_LRAEN	LOK	LRAEB ( 759 )	
B_LRAR	AUS	TEB ( 826 )	DLLR ( 578 ), LRA ( 797 )
B_LRARE	AUS	LRA ( 797 )	DKVS ( 811 )
B_LRARE2	AUS	LRA ( 797 )	DKVS ( 811 )
B_LRAREB	AUS	LRA ( 797 )	
B_LRAT	AUS	LRAEB ( 759 )	LRA ( 797 )
B_LREB100	LOK	LREB ( 739 )	
B_LREBLE	LOK	LREB ( 739 )	
B_LREBLE2	LOK	LREB ( 739 )	
B_LREBPR	LOK	LREB ( 739 )	
B_LREBPR2	LOK	LREB ( 739 )	
B_LREBRI	LOK	LREB ( 739 )	
B_LREBRI2	LOK	LREB ( 739 )	
B_LRHK	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSH ( 330 ), DLSSA ( 350 ), DLSAHK ( 339 )
B_LRHK2	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSAHK ( 339 ), DLSH ( 330 ), DLSSA ( 350 )
B_LRHKB	LOK	LRHK ( 781 )	
B_LRHKB2	LOK	LRHK ( 781 )	
B_LRHKBV2	LOK	LRHK ( 781 )	
B_LRHKG	LOK	LRHK ( 781 )	
B_LRHKG1	LOK	LRHK ( 781 )	
B_LRHKP	LOK	LRHK ( 781 )	
B_LRHKP2	LOK	LRHK ( 781 )	
B_LRKA	AUS	LRKA ( 795 )	DKAT ( 361 ), LRHK ( 781 ), GKRA ( 766 )
B_LRKA2	AUS	LRKA ( 795 )	DKAT ( 361 ), LRHK ( 781 ), GKRA ( 766 )
B_LRKAA	LOK	LRKA ( 795 )	
B_LRKAA2	LOK	LRKA ( 795 )	
B_LRKAE	LOK	LRKA ( 795 )	



Symbol	Type	Created within	Used within
B_LRKAE2	LOK	LRKA ( 795 )	
B_LRKAEI	LOK	LRKA ( 795 )	
B_LRKAEI2	LOK	LRKA ( 795 )	
B_LRKAON	LOK	LRKA ( 795 )	
B_LRKARG	LOK	LRKA ( 795 )	
B_LRKARG2	LOK	LRKA ( 795 )	
B_LRKAST	LOK	LRKA ( 795 )	
B_LRKAST2	LOK	LRKA ( 795 )	
B_LRNAKT	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_LRND	AUS	GKEB ( 737 )	LREB ( 739 ), AK ( 855 ), LRINI ( 749 ), LR ( 768 ), GKRA ( 766 )
B_LRND2	AUS	GKEB ( 737 )	LREB ( 739 ), LR ( 768 ), LRINI ( 749 ), GKRA ( 766 )
B_LRNDA	AUS	LREB ( 739 )	
B_LRNDA2	AUS	LREB ( 739 )	
B_LRNDIA	EIN		BGDVE ( 934 )
B_LRNERF	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_LRNF	LOK	BGDVE ( 934 )	
B_LRNRDY	AUS	BGDVE ( 934 )	ADVE ( 918 ), DDVE ( 950 )
B_LRNTESA	LOK	BGDVE ( 934 )	
B_LRNVB	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_LRNWS	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_LRNWT	EIN		ADVE ( 918 ), BGDVE ( 934 )
B_LRPERF	LOK	LR ( 768 )	
B_LRPERM	LOK	LR ( 768 )	
B_LRPPA	DOK	LREB ( 739 )	
B_LRRL	LOK	LREB ( 739 )	
B_LRSP	AUS	LR ( 768 )	ESUKA ( 711 ), LRHK ( 781 )
B_LRSP2	AUS	LR ( 768 )	ESUKA ( 711 ), LRHK ( 781 )
B_LRSSA	EIN		TEBEB ( 762 )
B_LRSSA2	EIN		TEBEB ( 762 )
B_LRSTAT	AUS	LR ( 768 )	
B_LRSTAT2	AUS	LR ( 768 )	
B_LRSTTA	AUS	LR ( 768 )	
B_LRSTTA2	AUS	LR ( 768 )	
B_LRSTTAMA	LOK	LR ( 768 )	
B_LRSYINH	AUS	LR ( 768 )	DKAT ( 361 )
B_LRSYNB1	EIN		LRHK ( 781 ), LR ( 768 )
B_LRSYNC	AUS	DKAT ( 361 )	LR ( 768 ), LRHK ( 781 )
B_LRSYNI	EIN		LRHK ( 781 ), LR ( 768 )
B_LRTPP	AUS	LR ( 768 )	DLSA ( 398 ), DLSSA ( 350 )
B_LRTPP2	AUS	LR ( 768 )	DLSA ( 398 ), DLSSA ( 350 )
B_LRVK	AUS	LREB ( 739 )	
B_LRVK2	AUS	LREB ( 739 )	
B_LRWLA	DOK	LREB ( 739 )	
B_LS	LOK	MDFAW ( 508 )	
B_LS3	AUS	PROKON ( 53 )	
B_LS32	AUS	PROKON ( 53 )	
B_LS4	AUS	PROKON ( 53 )	
B_LS42	AUS	PROKON ( 53 )	
B_LSADS	LOK	DLSV ( 301 )	
B_LSADS2	LOK	DLSV ( 301 )	
B_LSAHKSP	LOK	DLSAHK ( 339 )	
B_LSAHKSP2	LOK	DLSAHK ( 339 )	
B_LSASTP	LOK	DLSA ( 398 )	
B_LSASTP2	LOK	DLSA ( 398 )	
B_LSD	AUS	MDFAW ( 508 )	ARMD ( 531 ), FUEDK ( 597 ), MDKOG ( 516 ), MDKOL ( 526 ), MDAUTG ( 515 )
B_LSFET	LOK	DLSV ( 301 )	
B_LSFET2	LOK	DLSV ( 301 )	
B_LSH	AUS	PROKON ( 53 )	GGLSH ( 318 )
B_LSH2	AUS	PROKON ( 53 )	GGLSH ( 318 )
B_LSHKLT	LOK	DLSH ( 330 )	
B_LSHUB	LOK	DLSV ( 301 )	
B_LSHUB2	LOK	DLSV ( 301 )	
B_LSRDY	AUS	DIMC ( 1148 )	
B_LSV	AUS	PROKON ( 53 )	GGLSV ( 382 )
B_LSV2	AUS	PROKON ( 53 )	GGLSV ( 382 )
B_LSVKLT	LOK	DLSV ( 301 )	
B_LSVKLT2	LOK	DLSV ( 301 )	
B_LSVN	LOK	DLSV ( 301 )	
B_LSVN2	LOK	DLSV ( 301 )	
B_LSVVSP	EIN		LRA ( 797 )
B_LUAERK	AUS	DMDLUA ( 202 )	DMDLAD ( 215 )
B_LUAERK_M	EIN		NLPH ( 150 ), DMDLUA ( 202 )
B_LUAER_M2	LOK	DMDLUA ( 202 )	
B_LUECKE	AUS	GGDPG ( 74 )	AZUE ( 904 ), WANWKW ( 125 )
B_LUECKE2	EIN		AZUE ( 904 )
B_LUENA	LOK	DMDSTP ( 205 )	
B_LUERK	AUS	DMDLU ( 193 )	DMDLAD ( 215 )
B_LUERK_M	EIN		NLPH ( 150 ), DMDLU ( 193 )
B_LUERK_M2	LOK	DMDLU ( 193 )	
B_LUSTOP	AUS	DMDSTP ( 205 )	DMDDLU ( 199 ), DMDLUA ( 202 ), DMDLU ( 193 )
B_LUSTOPC	EIN		DMDSTP ( 205 )
B_LUSTOPT	AUS	DMDSTP ( 205 )	





Symbol	Type	Created within	Used within
B_LUSTOPU	LOK	DMDSTP ( 205 )	
B_LUSTOP_M	EIN		NLPH ( 150 )
B_LWSER	EIN		MDVERB ( 540 )
B_LZUP	LOK	KRRA ( 639 )	
B_M6ATV	LOK	DLSA ( 398 )	
B_M6ATV2	LOK	DLSA ( 398 )	
B_M8TE	AUS	TC8MOD (1120)	DTEV ( 856 ), TEBEB ( 762 ), SCATT (1097)
B_MADFK	EIN		KOS ( 896 ), MDVERAD ( 549 )
B_MADFS	EIN		KOS ( 896 ), MDVERAD ( 549 )
B_MADKO	EIN		KOS ( 896 ), MDVERAD ( 549 )
B_MADLL	EIN		KOS ( 896 ), MDVERAD ( 549 )
B_MASO	LOK	DLSV ( 301 )	
B_MASO2	LOK	DLSV ( 301 )	
B_MASTER	EIN		BBTEGA ( 750 ), MDVERB ( 540 ), DMDUE ( 158 ), DMDTSB ( 159 ), DMDLUA ( 202 ), DMDLU ( 193 ), DMDLAD ( 215 ), DMDFON ( 161 ), DLLR ( 578 ), DMDDLU ( 199 )
B_MASTERHW	EIN		AEVAB ( 980 ), BGDVE ( 934 ), DDST ( 851 ), AEVABZK (1003), TEBEB ( 762 ), SREAKT ( 963 ), GGPED ( 454 ), FGRREGL (1174), FGRFULO ( 1160 ), DNWSE (1025), DMDSTP ( 205 )
B_MAXFLSH	LOK	DLSH ( 330 )	
B_MAXFLSH2	LOK	DLSH ( 330 )	
B_MAXFLSV	LOK	DLSV ( 301 )	
B_MAXFLSV2	LOK	DLSV ( 301 )	
B_MAXLASH	LOK	DLSAHK ( 339 )	
B_MAXLASH2	LOK	DLSAHK ( 339 )	
B_MAXLATV	LOK	DLSA ( 398 )	
B_MAXLATV2	LOK	DLSA ( 398 )	
B_MBVH	LOK	GGPED ( 454 )	
B_MCACTI	LOK	VS_VERST ( 67 )	
B_MJARV	AUS	DMDMIL ( 216 )	DKAT ( 361 ), DLSA ( 398 ), DTEV ( 856 ), DLSAHK ( 339 ), DMDSTP ( 205 ), ESUKA ( 711 ), LRHK ( 781 ), LRAEB ( 759 )
B_MDDRLA	LOK	DMDSTP ( 205 )	
B_MDE8E	EIN		SCATT (1097)
B_MDE9E	EIN		SCATT (1097)
B_MDEE	LOK	MDRED ( 976 )	
B_MDEIN	AUS	MDKOG ( 516 )	DMDSTP ( 205 ), LLRBB ( 575 )
B_MDERK	AUS	DMDLAD ( 215 )	DMDFON ( 161 ), DMDSTP ( 205 )
B_MDKAT	AUS	DMDMIL ( 216 )	DKAT ( 361 ), LREB ( 739 )
B_MDMAX	AUS	SWADAP ( 47 )	
B_MDMIN	AUS	MDFUE ( 594 )	SWADAP ( 47 ), LLRRM ( 566 ), MDKOG ( 516 )
B_MDMXZU	LOK	MDZUL ( 523 )	
B_MDNG	LOK	DMDSTP ( 205 )	
B_MDNMOT	LOK	DMDSTP ( 205 )	
B_MDRL	LOK	DMDSTP ( 205 )	
B_MDSTIM_M	EIN		NLPH ( 150 ), DMDUE ( 158 )
B_MDSTOP	AUS	DMDSTP ( 205 )	DMDDLU ( 199 ), DMDLU ( 193 ), DMDFON ( 161 ), DMDLUA ( 202 )
B_MDSTOPC	EIN		DMDSTP ( 205 )
B_MDSTOPT	AUS	DMDSTP ( 205 )	
B_MDSTOP_M	EIN		DMDFON ( 161 ), NLPH ( 150 )
B_MDTNST	LOK	DMDSTP ( 205 )	
B_MDZYL1	DOK	DMDFON ( 161 )	DMDLUA ( 202 )
B_MDZYL1_M	EIN		DMDFON ( 161 ), DMDUE ( 158 )
B_MFACT	LOK	FUEDK ( 597 )	
B_MGBGAKT	LOK	MDFAW ( 508 )	
B_MGBGET	EIN		FUEDK ( 597 ), MDFAW ( 508 )
B_MIBEG	AUS	MDKOG ( 516 )	DUF (1089), MDAUTG ( 515 ), MDKOL ( 526 )
B_MIBEGL	AUS	MDKOL ( 526 )	MDKOG ( 516 )
B_MIFABG	EIN		MDKOL ( 526 ), MDFAW ( 508 )
B_MIL	EIN		DMILE ( 36 )
B_MILBLK	LOK	DMIL (1150)	
B_MILEB	LOK	DMIL (1150)	
B_MILFB	EIN		DMIL (1150)
B_MILMD	AUS	DMDMIL ( 216 )	
B_MILST	LOK	DMIL (1150)	
B_MILSTAT	AUS	DMIL (1150)	TC1MOD (1100)
B_MILSTP	AUS	DMDSTP ( 205 )	DMDMIL ( 216 )
B_MINLASH	LOK	DLSAHK ( 339 )	
B_MINLASH2	LOK	DLSAHK ( 339 )	
B_MINLATV	LOK	DLSA ( 398 )	
B_MINLATV2	LOK	DLSA ( 398 )	
B_MLDYN	LOK	DLSAHK ( 339 )	
B_MLRSA	AUS	GKEB ( 737 )	LREB ( 739 ), TEBEB ( 762 )
B_MLUECKE	AUS	GGDPG ( 74 )	
B_MLUSTEST	LOK	DLSAHK ( 339 )	
B_MNBREMS	LOK	GGEGAS ( 474 )	
B_MNBWF	AUS	GGPED ( 454 )	
B_MNDK	LOK	DDVE ( 950 )	
B_MNDK1P	LOK	DDVE ( 950 )	
B_MNDK2P	LOK	DDVE ( 950 )	
B_MNDSS	LOK	EGFE ( 228 )	
B_MNDST	AUS	DDST ( 851 )	
B_MNDVEE	LOK	DDVE ( 950 )	





Symbol	Type	Created within	Used within
B_MSLOFF	EIN		BBKHZ ( 890 ), AK ( 855 )
B_MSLR	LOK	LREB ( 739 )	
B_MSLR2	LOK	LREB ( 739 )	
B_MSR	AUS	MDKOG ( 516 )	BBSAW ( 557 ), MDZUL ( 523 ), DUF ( 1089 ), MDRED ( 976 )
B_MSREXT	LOK	UFMSRC ( 1080 )	
B_MSR_C	EIN		CAN ( 1124 )
B_MSTHW_UM	EIN		UFMER ( 1060 ), UFMET ( 1060 )
B_MT	AUS	PROKON ( 53 )	
B_MUNST	AUS	WDKSOM ( 614 )	ZWMIN ( 669 )
B_MXBREMS	LOK	GGEGAS ( 474 )	
B_MXBWF	AUS	GGPED ( 454 )	
B_MXDK	LOK	DDVE ( 950 )	
B_MXDK1P	LOK	DDVE ( 950 )	
B_MXDK2P	LOK	DDVE ( 950 )	
B_MXDSS	LOK	EGFE ( 228 )	
B_MXDST	AUS	DDST ( 851 )	
B_MXDVEE	LOK	DDVE ( 950 )	
B_MXDVEF	AUS	DDVE ( 950 )	
B_MXDVEFO	AUS	DDVE ( 950 )	
B_MXDVEL	LOK	DDVE ( 950 )	
B_MXDVEN	LOK	DDVE ( 950 )	
B_MXDVER	LOK	DDVE ( 950 )	
B_MXDVEU	LOK	DDVE ( 950 )	
B_MXDVEUB	LOK	DDVE ( 950 )	
B_MXDVEV	LOK	DDVE ( 950 )	
B_MXEGFE	AUS	DEGFE ( 592 )	
B_MXE1	EIN		DEVE ( 1017 )
B_MXE2	EIN		DEVE ( 1017 )
B_MXE3	EIN		DEVE ( 1017 )
B_MXE4	EIN		DEVE ( 1017 )
B_MXE5	EIN		DEVE ( 1017 )
B_MXE6	EIN		DEVE ( 1017 )
B_MXE7	EIN		DEVE ( 1017 )
B_MXE8	EIN		DEVE ( 1017 )
B_MXFHSH	LOK	DHLSHK ( 1154 )	
B_MXFHSH2	LOK	DHLSHK ( 1154 )	
B_MXFP1P	AUS	GGPED ( 454 )	
B_MXFP2P	AUS	GGPED ( 454 )	
B_MXFPP	AUS	GGPED ( 454 )	
B_MXFRAO	LOK	DKVS ( 811 )	
B_MXFRAO2	LOK	DKVS ( 811 )	
B_MXFRAU	LOK	DKVS ( 811 )	
B_MXFRAU2	LOK	DKVS ( 811 )	
B_MXFRST	LOK	DKVS ( 811 )	
B_MXFRST2	LOK	DKVS ( 811 )	
B_MXHFM	LOK	DHFM ( 233 )	
B_MXHSH	AUS	DHLSHK ( 1154 )	
B_MXHSH2	AUS	DHLSHK ( 1154 )	
B_MXHSHVE	AUS	DHLSVKE ( 902 )	
B_MXHSHVE2	AUS	DHLSVKE ( 902 )	
B_MXKAT	AUS	DKAT ( 361 )	
B_MXKAT2	AUS	DKAT ( 361 )	
B_MXKOSE	AUS	DKOSE ( 901 )	
B_MXKPE	EIN		DEKPE ( 1020 )
B_MXKS1	AUS	DKRS ( 437 )	
B_MXKS2	AUS	DKRS ( 437 )	
B_MXKS3	AUS	DKRS ( 437 )	
B_MXKS4	AUS	DKRS ( 437 )	
B_MXLASH	AUS	DLSAHK ( 339 )	
B_MXLASH2	AUS	DLSAHK ( 339 )	
B_MXLATP	AUS	DLSA ( 398 )	
B_MXLATP2	AUS	DLSA ( 398 )	
B_MXLATV	AUS	DLSA ( 398 )	
B_MXLATV2	AUS	DLSA ( 398 )	
B_MXLLR	AUS	DLLR ( 578 )	
B_MXLM	AUS	DHFM ( 233 )	EGFE ( 228 )
B_MXLSH	AUS	DLSH ( 330 )	
B_MXLSH2	AUS	DLSH ( 330 )	
B_MXLSV	AUS	DLSV ( 301 )	
B_MXLSV2	AUS	DLSV ( 301 )	
B_MXMD	LOK	DMDMIL ( 216 )	
B_MXMDB	AUS	MDKOG ( 516 )	
B_MXMILE	AUS	DMILE ( 36 )	
B_MXNWKW	AUS	DNWKW ( 134 )	
B_MXNWKW2	AUS	DNWKW ( 134 )	
B_MXNWS	AUS	DNWS ( 622 )	
B_MXNWS2	AUS	DNWS ( 622 )	
B_MXPH	AUS	DPH ( 144 )	
B_MXPH2	AUS	DPH ( 144 )	
B_MXPUA	AUS	BGPU ( 276 )	
B_MXRKAT	LOK	DKVS ( 811 )	
B_MXRKAT2	LOK	DKVS ( 811 )	



Symbol	Type	Created within	Used within
B_MXRKAZ	LOK	DKVS ( 811 )	
B_MXRKAZ2	LOK	DKVS ( 811 )	
B_MXRLOH	EIN		BGRSM ( 245 )
B_MXTA	AUS	GGTFA ( 298 )	
B_MXTES	AUS	DTEV ( 856 )	
B_MXTEVE	AUS	DTEVE ( 1022 )	
B_MXTM	AUS	GGTFM ( 289 )	
B_MXUB	AUS	GGUB ( 487 )	
B_MZNS	LOK	MDZUL ( 523 )	
B_MZNS_C	AUS	UFMER ( 1060 )	
B_MZNS_UM	AUS	UFNSC ( 1077 )	MDZUL ( 523 ), UFMET ( 1060 ), UFMZUL ( 1084 ), UFUE ( 1056 )
B_NAC	AUS	KOS ( 896 )	LLRNS ( 562 )
B_NACHL	AUS	MOTAUS ( 1028 )	HLS ( 392 )
B_NACHLEND	AUS	MOTAUS ( 1028 )	AEKP ( 970 ), BGPU ( 276 ), ATM ( 20 )
B_NACHLRAM	AUS	MOTAUS ( 1028 )	
B_NACHLSTP	AUS	MOTAUS ( 1028 )	BGTABST ( 1030 )
B_NDYLASH	LOK	DLSAHK ( 339 )	
B_NDYLASH2	LOK	DLSAHK ( 339 )	
B_NESCH	LOK	DLSAHK ( 339 )	
B_NESCH2	LOK	DLSAHK ( 339 )	
B_NGASOK	AUS	BGNG ( 121 )	BGRLG ( 274 )
B_NKONS_UM	AUS	UFMSRC ( 1080 )	
B_NLACLS	EIN		MOTAUS ( 1028 )
B_NLAL	AUS	ALE ( 136 )	MOTAUS ( 1028 )
B_NLATM	AUS	ATM ( 20 )	MOTAUS ( 1028 )
B_NLCAN	EIN		MOTAUS ( 1028 )
B_NLDG	EIN		ALE ( 136 ), DPH ( 144 ), DLLR ( 578 ), DMDSTP ( 205 ), DTEV ( 856 ), GGDPG ( 74 ), ESUKA ( 711 ), WANWKW ( 125 ), NMAXMD ( 584 ), NLPH ( 150 ), NLDG ( 157 ), LLRNS ( 562 ), KRRA ( 639 )
B_NLDGC	EIN		GGDPG ( 74 )
B_NLDTE	EIN		MOTAUS ( 1028 )
B_NLEEPR	EIN		MOTAUS ( 1028 )
B_NLMLS	AUS	LFS ( 69 )	MOTAUS ( 1028 )
B_NLOBD	EIN		MOTAUS ( 1028 )
B_NLPE	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_NLPERF	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_NLPH	AUS	NLPH ( 150 )	GGDPG ( 74 )
B_NLPHEA	AUS	AEVAB ( 980 )	NLPH ( 150 )
B_NLPHEAI	LOK	AEVAB ( 980 )	
B_NLPNE	AUS	ADVE ( 918 )	SREAKT ( 963 )
B_NLPNEW	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_NLPREQ	AUS	BGDVE ( 934 )	
B_NLSGLS	EIN		MOTAUS ( 1028 )
B_NLSIKO	EIN		MOTAUS ( 1028 )
B_NLWFS	EIN		MOTAUS ( 1028 )
B_NLWST	AUS	BGTABST ( 1030 )	MOTAUS ( 1028 )
B_NMAX	AUS	NMAXMD ( 584 )	BGBSZ ( 73 ), GGPED ( 454 ), MDRED ( 976 )
B_NMAXD	EIN		AEVABU ( 1002 ), NMAXMD ( 584 )
B_NMIN	AUS	GGDPG ( 74 )	AEKP ( 970 ), WDKSOM ( 614 ), RDE ( 112 ), GGTFM ( 289 ), BGNMOT ( 111 ), BGTABST ( 1030 ), DECJ ( 1013 ), ESSTT ( 679 ), DDG ( 141 ), AZUE ( 904 ), ADVE ( 918 ), TEB ( 826 ), MDFAW ( 508 ), DMIL ( 1150 ), DLLR ( 578 ), DHLVK ( 29 ), DHLSHK ( 1154 ), DEPCL ( 1151 ), ALE ( 136 ), BBSTT ( 148 ), BBKHZ ( 890 ), BGKMS ( 1008 ), LLRBB ( 575 ), GGTFM ( 289 ), GGTFA ( 298 ), DLSV ( 301 ), DLSH ( 330 ), BBTEGA ( 750 )
B_NMOT	AUS	GGDPG ( 74 )	
B_NO	LOK	DTRIG ( 1139 )	
B_NOADSH	LOK	DLSH ( 330 )	
B_NOADSH2	LOK	DLSH ( 330 )	
B_NOBM	AUS	GGDPG ( 74 )	
B_NOBM1	AUS	GGDPG ( 74 )	
B_NODEC	LOK	STADAP ( 684 )	
B_NOFLR	AUS	DDST ( 851 )	
B_NOFRA	AUS	LRA ( 797 )	DKVS ( 811 )
B_NOFRAT	LOK	LRA ( 797 )	
B_NOINC	LOK	STADAP ( 684 )	
B_NOKATFZ	EIN		GGTFM ( 289 )
B_NOLASH	LOK	DLSAHK ( 339 )	
B_NOLASH2	LOK	DLSAHK ( 339 )	
B_NOLATP	LOK	DLSA ( 398 )	
B_NOLATP2	LOK	DLSA ( 398 )	
B_NOLATV	LOK	DLSA ( 398 )	
B_NOLATV2	LOK	DLSA ( 398 )	
B_NOLRB	AUS	LREB ( 739 )	
B_NOLRB2	AUS	LREB ( 739 )	
B_NOLRE	AUS	LREB ( 739 )	
B_NOLRE2	AUS	LREB ( 739 )	
B_NOLRW	AUS	LREB ( 739 )	
B_NOLRW2	AUS	LREB ( 739 )	
B_NOLSH	AUS	DLSH ( 330 )	
B_NOLSH2	AUS	DLSH ( 330 )	
B_NOLSV	LOK	DLSV ( 301 )	
B_NOLSV2	LOK	DLSV ( 301 )	
B_NOME_C	AUS	UFMER ( 1060 )	



Symbol	Type	Created within	Used within
B_NOME_JUM	AUS	UFMER (1060)	DUF (1089), SREAKT ( 963 ), UFMET (1060)
B_NOMIL	LOK	DMIL (1150)	
B_NOMSR_FR	AUS	CAN (1124)	UFMSRC (1080)
B_NOMSR_JUM	AUS	UFMSRC (1080)	UFUE (1056), CAN (1124), DUF (1089)
B_NOPH	AUS	GGDPG ( 74 )	
B_NOPH2	AUS	GGDPG ( 74 )	
B_NOPHNLDG	AUS	DPH ( 144 )	
B_NORKAM	LOK	DKVS ( 811 )	
B_NORKAT	AUS	LRA ( 797 )	DKVS ( 811 )
B_NORKAZ	AUS	LRA ( 797 )	DKVS ( 811 )
B_NOSGS_FR	EIN		UFSGSC (1070), CAN (1124)
B_NOSGS_JUM	AUS	UFSGSC (1070)	CAN (1124), DUF (1089)
B_NOSYNPH	AUS	NLPH ( 150 )	GGDPG ( 74 )
B_NOTLU	AUS	UFEING (1058)	UFMVER (1087), UFREAC (1088), UFRLC (1066), UFUE (1056)
B_NOTLU_FR	AUS	SREAKT ( 963 )	DUF (1089), UFUE (1056), UFEING (1058)
B_NOWUC	AUS	DWUC (1147)	
B_NOZWE	AUS	MDZW ( 636 )	ZUE ( 627 )
B_NPBM	AUS	DDG ( 141 )	
B_NPBREMS	LOK	GGEGAS ( 474 )	
B_NPBUOF	AUS	CAN (1124)	
B_NPBWF	AUS	GGPED ( 454 )	
B_NPDK	LOK	DDVE ( 950 )	
B_NPDK1P	LOK	DDVE ( 950 )	
B_NPDK2P	LOK	DDVE ( 950 )	
B_NPDST	AUS	DDST ( 851 )	
B_NPDVEE	LOK	DDVE ( 950 )	
B_NPDVEF	LOK	DDVE ( 950 )	
B_NPDVEL	LOK	DDVE ( 950 )	
B_NPDVEN	AUS	DDVE ( 950 )	
B_NPDVER	LOK	DDVE ( 950 )	
B_NPDVET	LOK	DDVE ( 950 )	
B_NPDVEU	AUS	DDVE ( 950 )	
B_NPDVEUW	AUS	DDVE ( 950 )	
B_NPDVEV	AUS	DDVE ( 950 )	
B_NPFHSH	LOK	DHLSHK (1154)	
B_NPFHSH2	LOK	DHLSHK (1154)	
B_NPFP1P	AUS	GGPED ( 454 )	
B_NPFP2P	AUS	GGPED ( 454 )	
B_NPFP	AUS	GGPED ( 454 )	
B_NPFRST	LOK	DKVS ( 811 )	
B_NPFRST2	LOK	DKVS ( 811 )	
B_NPHSH	AUS	DHLSHK (1154)	
B_NPHSH2	AUS	DHLSHK (1154)	
B_NPHSV	AUS	DHLSVK ( 29 )	
B_NPHSV2	AUS	DHLSVK ( 29 )	
B_NPKAT	AUS	DKAT ( 361 )	
B_NPKAT2	AUS	DKAT ( 361 )	
B_NPKRNT	AUS	DKRNT ( 445 )	
B_NPKROF	AUS	DKRNT ( 445 )	
B_NPKRTP	AUS	DKRTP ( 451 )	
B_NPKS1	AUS	DKRS ( 437 )	
B_NPKS2	AUS	DKRS ( 437 )	
B_NPKS3	AUS	DKRS ( 437 )	
B_NPKS4	AUS	DKRS ( 437 )	
B_NPLASH	AUS	DLSAHK ( 339 )	
B_NPLASH2	AUS	DLSAHK ( 339 )	
B_NPLFLSH	LOK	DLSH ( 330 )	
B_NPLFLSH2	AUS	DLSH ( 330 )	
B_NPLFLSV	LOK	DLSV ( 301 )	
B_NPLFLSV2	LOK	DLSV ( 301 )	
B_NPLM	AUS	DHFM ( 233 )	
B_NPLSV	AUS	DLSV ( 301 )	
B_NPLSV2	AUS	DLSV ( 301 )	
B_NPMD	LOK	DMDMIL ( 216 )	
B_NPMDB	AUS	MDKOG ( 516 )	
B_NPNWS	AUS	DNWS ( 622 )	
B_NPNWS2	AUS	DNWS ( 622 )	
B_NPPH	AUS	DPH ( 144 )	
B_NPPH2	AUS	DPH ( 144 )	
B_NPPOEL	AUS	GGPOEL ( 296 )	
B_NPTES	AUS	DTEV ( 856 )	
B_NPTM	AUS	GGTFM ( 289 )	
B_NPUB	AUS	GGUB ( 487 )	
B_NPUF2SG	AUS	DUF (1089)	
B_NPUFMV	AUS	DUF (1089)	
B_NPUFSKA	AUS	DUF (1089)	
B_NPURRAM	AUS	DUR (1052)	
B_NPURROM	AUS	DUR (1052)	
B_NPURRST	AUS	DUR (1052)	
B_NS2	LOK	LLRNS ( 562 )	
B_NS2A	LOK	LLRNS ( 562 )	
B_NSAKT	LOK	MDZUL ( 523 )	



Symbol	Type	Created within	Used within
B_NSAAKTJUM	LOK	UFNSC (1077)	
B_NSEND	LOK	MDZUL (523)	
B_NSENDJUM	LOK	UFNSC (1077)	
B_NSXS	LOK	LLRNS (562)	
B_NSP	AUS	BGRLP (266)	
B_NSSL	LOK	LLRNS (562)	
B_NSTU	AUS	LLRBB (575)	
B_NSWO1	AUS	PROKON (53)	BGAGR (263), FUEREG (595), FUEDK (597), TEB (826), MDVER-AD (549), LLRRM (566), LLRNS (562), LLRMR (572), DTEV (856), DLLR (578), ESUKA (711)
B_NSWO2	AUS	PROKON (53)	BGRLP (266), ESUK (699)
B_NTINI	LOK	GGKS (412)	
B_NUSGSJUM	AUS	UFGSGC (1070)	
B_NWS	AUS	FE (591)	MSF (506), NWS (618), ACIFI (1013), GGHEM (230), DNWSE (1025), DNWS (622), DMDSTP (205), BGPU (276)
B_NWS2	EIN		DMDSTP (205)
B_NWSB	LOK	NWS (618)	
B_NWSFA	AUS	DNWS (622)	
B_NWSFA2	AUS	DNWS (622)	
B_NWSFP	AUS	DNWS (622)	
B_NWSFP2	AUS	DNWS (622)	
B_NWSVF	AUS	DNWS (622)	WANWKW (125)
B_NWSVF2	AUS	DNWS (622)	WANWKW (125)
B_NWSVS	AUS	DNWS (622)	
B_NWSVS2	AUS	DNWS (622)	
B_NWVS	AUS	BGSRM (245)	
B_NW_S	AUS	NWS (618)	WANWKW (125)
B_OPTPHERK	EIN		DMDLU (193), NLPH (150)
B_PAGR	AUS	BGAGR (263)	EGFE (228)
B_PGXSQSYN	LOK	GGDPG (74)	
B_PHA2ACT	AUS	GGDPG (74)	NLPH (150)
B_PHAACT	AUS	GGDPG (74)	NLPH (150)
B_PHAD	AUS	WANWKW (125)	DNWKW (134), GGDPG (74), DPH (144), DNWS (622)
B_PHAD2	AUS	WANWKW (125)	DNWKW (134), GGDPG (74), DNWS (622), DPH (144)
B_PHAS2	AUS	GGDPG (74)	DPH (144)
B_PHASE	AUS	GGDPG (74)	DPH (144)
B_PHEXOR	LOK	DPH (144)	
B_PHEXOR2	LOK	DPH (144)	
B_PHFALSE	LOK	NLDG (157)	
B_PHNEGTV	LOK	NLDG (157)	
B_PHNLDG	AUS	NLDG (157)	GGDPG (74)
B_PHREGOK	LOK	DPH (144)	
B_PHREGOK2	LOK	DPH (144)	
B_PHSNL	AUS	NLPH (150)	AEVAB (980), DMDSTP (205), DMDUE (158)
B_PHSNLAB	AUS	NLPH (150)	
B_PHSNLINV	AUS	NLPH (150)	ALE (136)
B_PHSNLOK	AUS	NLPH (150)	
B_PHSOK	AUS	DPH (144)	GGDPG (74), NLPH (150)
B_PHSOK2	AUS	DPH (144)	GGDPG (74), NLPH (150)
B_PHW	LOK	GGDPG (74)	
B_PHW2	LOK	GGDPG (74)	
B_PHWNEG	LOK	GGDPG (74)	
B_PHWOK	LOK	GGDPG (74)	
B_PHWOK2	LOK	GGDPG (74)	
B_PHWPOS	LOK	GGDPG (74)	
B_PLOK	LOK	DMDFON (161)	
B_PLOK01	LOK	DMDFON (161)	
B_PLOK02	LOK	DMDFON (161)	
B_PLOK03	LOK	DMDFON (161)	
B_PLOK04	LOK	DMDFON (161)	
B_PLOK05	LOK	DMDFON (161)	
B_PLOK06	LOK	DMDFON (161)	
B_PLOK07	LOK	DMDFON (161)	
B_PLOK08	LOK	DMDFON (161)	
B_PLOKN	DOK	DMDFON (161)	
B_PLOKNJM	LOK	DMDFON (161)	
B_PLRA	LOK	DKVS (811)	
B_PLSOLAP	EIN		FUEDK (597)
B_PLTAB	LOK	BGTABST (1030)	
B_PN	AUS	SWADAP (47)	
B_POEL	AUS	GGPOEL (296)	
B_PRESYN	EIN		GGDPG (74)
B_PRIPH	AUS	GGLSH (318)	
B_PRIPH2	AUS	GGLSH (318)	
B_PRIPV	AUS	GGLSV (382)	
B_PRIPV2	AUS	GGLSV (382)	
B_PSPAUS	LOK	LREB (739)	
B_PSPWL	LOK	LREB (739)	
B_PUA	LOK	BGPU (276)	
B_PUAMS	AUS	BGPU (276)	EGFE (228)
B_PUAVL	LOK	BGPU (276)	
B_PUAVLE	LOK	BGPU (276)	



Symbol	Type	Created within	Used within
B_PUAVLEI	LOK	BGPU ( 276 )	
B_PVL1	LOK	AEKP ( 970 )	
B_PVL2	LOK	AEKP ( 970 )	
B_PVLNL	LOK	AEKP ( 970 )	
B_PWF	EIN		ADVE ( 918 ), BGPU ( 276 ), DDVE ( 950 ), DIMC ( 1148 ), DKRS ( 437 ), DLSV ( 301 ), DLLR ( 578 ), GGPED ( 454 ), GGFST ( 502 ), GGEGAS ( 474 ), ESSTT ( 679 ), DTEV ( 856 ), DKAT ( 361 ), DEGE ( 592 ), BGTABST ( 1030 ), NLPH ( 150 ), LRA ( 797 ), LR ( 768 ), LLRNS ( 562 ), KRRA ( 639 ), KRDY ( 659 ), BGKMST ( 1008 ), BGMSZS ( 239 ), BGDVE ( 934 )
B_PWGBWF	LOK	GGPED ( 454 )	
B_PWGLK	LOK	GGPED ( 454 )	
B_PWGNOTFR	AUS	GGPED ( 454 )	DUF ( 1089 ), UFSPSC ( 1060 ), FGRABED ( 491 )
B_PWGNOTUM	AUS	UFSPSC ( 1060 )	URADCC ( 1049 ), GGPED ( 454 )
B_PWGNOT_C	EIN		GGPED ( 454 )
B_PWRSV	LOK	ADVE ( 918 )	
B_QSYN	AUS	GGDPG ( 74 )	
B_QTEDAB	AUS	TEBEB ( 762 )	TEB ( 826 )
B_RALECTR	LOK	ALE ( 136 )	
B_RALEOK	LOK	ALE ( 136 )	
B_RDEPLAUS	AUS	RDE ( 112 )	
B_RDEUNDEF	AUS	RDE ( 112 )	
B_REDKL	LOK	ESUK ( 699 )	
B_REFMAX	LOK	DLSV ( 301 )	
B_REFMAX2	LOK	DLSV ( 301 )	
B_REHS	LOK	HLS ( 392 )	
B_RESETSUN	LOK	NLDG ( 157 )	
B_RIAKV	LOK	GGLSV ( 382 )	
B_RIAKV2	LOK	GGLSV ( 382 )	
B_RIBEH	LOK	GGLSH ( 318 )	
B_RIBEH2	LOK	GGLSH ( 318 )	
B_RIBEV	LOK	GGLSV ( 382 )	
B_RIBEV2	LOK	GGLSV ( 382 )	
B_RIIBV	LOK	GGLSV ( 382 )	
B_RIIBV2	LOK	GGLSV ( 382 )	
B_RIIMPH	LOK	GGLSH ( 318 )	
B_RIIMPV	LOK	GGLSV ( 382 )	
B_RIMH	LOK	GGLSH ( 318 )	
B_RIMH2	LOK	GGLSH ( 318 )	
B_RIMV	LOK	GGLSV ( 382 )	
B_RIMV2	LOK	GGLSV ( 382 )	
B_RINH	AUS	GGLSH ( 318 )	DHLSHK ( 1154 )
B_RINH2	AUS	GGLSH ( 318 )	DHLSHK ( 1154 )
B_RINV	AUS	GGLSV ( 382 )	DHLSVK ( 29 )
B_RINV2	AUS	GGLSV ( 382 )	DHLSVK ( 29 )
B_RIPUH	LOK	GGLSH ( 318 )	
B_RIPUH2	LOK	GGLSH ( 318 )	
B_RIPUV	LOK	GGLSV ( 382 )	
B_RIPUV2	LOK	GGLSV ( 382 )	
B_RIREH	LOK	GGLSH ( 318 )	
B_RIREH2	LOK	GGLSH ( 318 )	
B_RIREV	LOK	GGLSV ( 382 )	
B_RIREV2	LOK	GGLSV ( 382 )	
B_RISIGH	LOK	DLSH ( 330 )	
B_RISIGH2	LOK	DLSH ( 330 )	
B_RISIGV	LOK	DLSV ( 301 )	
B_RISIGV2	LOK	DLSV ( 301 )	
B_RKAM	LOK	DKVS ( 811 )	
B_RKAMR	LOK	DKVS ( 811 )	
B_RKAMR2	LOK	DKVS ( 811 )	
B_RKAT	AUS	LRA ( 797 )	DKVS ( 811 )
B_RKATR	AUS	LRA ( 797 )	DKVS ( 811 )
B_RKATR2	AUS	LRA ( 797 )	DKVS ( 811 )
B_RKAZ	AUS	LRA ( 797 )	DKVS ( 811 )
B_RKAZR	AUS	LRA ( 797 )	DKVS ( 811 )
B_RKAZR2	AUS	LRA ( 797 )	DKVS ( 811 )
B_RLP	LOK	BGRLP ( 266 )	
B_RLPNS	LOK	BGRLP ( 266 )	
B_RLRAB	AUS	GKEB ( 737 )	
B_RMSVAL	AUS	DTEV ( 856 )	
B_RPHSP	LOK	NLDG ( 157 )	
B_SA	AUS	AES ( 973 )	MDRED ( 976 ), ACIFI ( 1013 ), BGPU ( 276 ), ARMD ( 531 ), DLLR ( 578 ), DVFZ ( 500 ), ESUK ( 699 ), EGAG ( 486 ), ZWMIN ( 669 ), ZUE ( 627 ), MDVER ( 546 ), LREB ( 739 ), LLRBB ( 575 ), KOS ( 896 ), GGTFM ( 289 ), GGTFA ( 298 ), GGLSV ( 382 ), GGLSH ( 318 ), ESWE ( 698 ), MDKOG ( 516 ), MDFUE ( 594 ), MDFAW ( 508 ), LRKA ( 795 ), DMDSTP ( 205 ), DLSV ( 301 ), DKVS ( 811 ), DEVE ( 1017 ), ATM ( 20 )
B_SAB	AUS	BBSAWE ( 557 )	MSF ( 506 ), LLRBB ( 575 ), TEB ( 826 ), MDRED ( 976 ), MDMIN ( 538 ), MDAUTG ( 515 ), MDFAW ( 508 )
B_SABFG	AUS	BBSAWE ( 557 )	MDFAW ( 508 )
B_SABGT	LOK	BBSAWE ( 557 )	
B_SABT	LOK	BBSAWE ( 557 )	
B_SACVT	EIN		BBSAWE ( 557 )



Symbol	Type	Created within	Used within
B_SAVACC	EIN		FGRREGL (1174)
B_SAVFGR	AUS	FGRREGL (1174)	FGRUE (490), BBSAWE (557)
B_SAVFGRC	EIN		FGRREGL (1174)
B_SAVMD	AUS	MDKOG (516)	
B_SAVMSR	EIN		BBSAWE (557)
B_SBBHK	AUS	DLSH (330)	DKAT (361), DLSAHK (339), LRKA (795), LRHK (781), HLS (392), DLSV (301)
B_SBBHK2	AUS	DLSH (330)	DKAT (361), DLSAHK (339), HLS (392), LRKA (795), LRHK (781), DLSV (301)
B_SBBVK	AUS	DLSV (301)	HLS (392), LR (768), TEBEB (762), LREB (739)
B_SBBVK2	AUS	DLSV (301)	DKAT (361), HLS (392), LR (768), TEBEB (762), LREB (739)
B_SBBVKSL	LOK	LR (768)	
B_SELESPED	EIN		BBGANG (501), SREAKT (963), NMAXMD (584), CAN (1124), DVKUP (1027)
B_SELESPEE	EIN		DCKUP (1128)
B_SGNALT	LOK	LR (768)	
B_SGNALT2	LOK	LR (768)	
B_SGNDFET	LOK	LR (768)	
B_SGNDFET2	LOK	LR (768)	
B_SGNDMAG	LOK	LR (768)	
B_SGNDMAG2	LOK	LR (768)	
B_SGNLR	AUS	LR (768)	
B_SGNLR2	AUS	LR (768)	
B_SGNRA	LOK	LR (768)	
B_SGNRA2	LOK	LR (768)	
B_SGS	AUS	MDKOG (516)	DUF (1089), MDZUL (523), MDRED (976)
B_SGSAC_UM	LOK	UFGSGC (1070)	
B_SGSRH_C	EIN		CAN (1124)
B_SGSKON_C	EIN		CAN (1124)
B_SGSNL	EIN		NMAXMD (584)
B_SGSRED	AUS	CAN (1124)	DVKUP (1027), MDRED (976)
B_SGSRED_C	EIN		CAN (1124)
B_SHUERF	EIN		GGLSV (382), GGLSH (318)
B_SHUERF2	EIN		GGLSV (382), GGLSH (318)
B_SIBREMS	LOK	GGEGAS (474)	
B_SIBWF	AUS	GGPED (454)	
B_SICAS	AUS	DCAS (1128)	
B_SICINS	AUS	DCINS (1126)	
B_SICKUP	LOK	DCKUP (1128)	
B_SIDK1P	LOK	DDVE (950)	
B_SIDVEE	LOK	DDVE (950)	
B_SIDVEF	LOK	DDVE (950)	
B_SIDVEL	LOK	DDVE (950)	
B_SIDVEN	LOK	DDVE (950)	
B_SIDVER	LOK	DDVE (950)	
B_SIDVEU	LOK	DDVE (950)	
B_SIDVEV	LOK	DDVE (950)	
B_SIEV1	EIN		DEVE (1017)
B_SIEV2	EIN		DEVE (1017)
B_SIEV3	EIN		DEVE (1017)
B_SIEV4	EIN		DEVE (1017)
B_SIEV5	EIN		DEVE (1017)
B_SIEV6	EIN		DEVE (1017)
B_SIEV7	EIN		DEVE (1017)
B_SIEV8	EIN		DEVE (1017)
B_SIFHSH	LOK	DHLSHK (1154)	
B_SIFHSH2	LOK	DHLSHK (1154)	
B_SIFP1P	AUS	GGPED (454)	
B_SIFP2P	AUS	GGPED (454)	
B_SIFPP	AUS	GGPED (454)	
B_SIGFLSH	LOK	DLSH (330)	
B_SIGFLSH2	LOK	DLSH (330)	
B_SIGFLSV	LOK	DLSV (301)	
B_SIGFLSV2	LOK	DLSV (301)	
B_SIHSH	AUS	DHLSHK (1154)	
B_SIHSH2	AUS	DHLSHK (1154)	
B_SIHVE	AUS	DHLSVKE (902)	
B_SIHVE2	AUS	DHLSVKE (902)	
B_SIKAT	AUS	DKAT (361)	
B_SIKAT2	AUS	DKAT (361)	
B_SIKOSE	AUS	DKOSE (901)	
B_SIKPE	EIN		DEKPE (1020)
B_SIKS1	AUS	DKRS (437)	
B_SIKS2	AUS	DKRS (437)	
B_SIKS3	AUS	DKRS (437)	
B_SIKS4	AUS	DKRS (437)	
B_SILM	AUS	DHFM (233)	
B_SILSH	AUS	DLSH (330)	
B_SILSH2	AUS	DLSH (330)	
B_SILSV	AUS	DLSV (301)	
B_SILSV2	AUS	DLSV (301)	
B_SIMDB	AUS	MDKOG (516)	





Symbol	Type	Created within	Used within
B_SIMILE	AUS	DMILE ( 36 )	
B_SIMUTE	AUS	CAN (1124)	
B_SIN	AUS	DDG ( 141 )	
B_SIPH	AUS	DPH ( 144 )	
B_SIPH2	AUS	DPH ( 144 )	
B_SITES	AUS	DTEV ( 856 )	
B_SITEVE	AUS	DTEVE (1022)	
B_SITM	AUS	GGTFM ( 289 )	
B_SIVFZ	AUS	DVFZ ( 500 )	
B_SIVKUP	LOK	DVKUP (1027)	
B_SKAEVAB	LOK	AEVABU (1002)	
B_SL	EIN		LLRMR ( 572 ), MDVERB ( 540 ), LLRNS ( 562 )
B_SLKHOF	LOK	AK ( 855 )	
B_SLP	AUS	AK ( 855 )	MDVERB ( 540 )
B_SLPC	EIN		MDVERB ( 540 )
B_SLPOFF	EIN		BBKHZ ( 890 )
B_SLS	AUS	AK ( 855 )	DKAT ( 361 ), DTEV ( 856 ), LRAEB ( 759 ), TEBEB ( 762 ), TC1MOD (1100), LRKA ( 795 ), LREB ( 739 ), DLSH ( 330 ), DLSV ( 301 )
B_SLSFZ	AUS	PROKON ( 53 )	BBKHZ ( 890 ), LAMKO ( 729 ), TC1MOD (1100), LAKH ( 735 )
B_SLSN2	AUS	AZUE ( 904 )	
B_SLSOFF	AUS	AK ( 855 )	LREB ( 739 )
B_SLSRDY	AUS	DIMC (1148)	
B_SLV	AUS	AK ( 855 )	
B_SP1	AUS	DMDMIL ( 216 )	DTRIG (1139)
B_SP1S	AUS	GGPED ( 454 )	DUF (1089), UFSPSC (1060)
B_SP2	AUS	DMDMIL ( 216 )	DTRIG (1139)
B_SP2S	AUS	GGPED ( 454 )	DUF (1089), UFSPSC (1060)
B_SP3	EIN		DTRIG (1139)
B_SPSA	AUS	WANWKW ( 125 )	DNWKW ( 134 )
B_SPSA2	AUS	WANWKW ( 125 )	DNWKW ( 134 )
B_SPSMIN	AUS	GGPED ( 454 )	DUF (1089), LLRNS ( 562 ), UFSPSC (1060)
B_SRSTZ_UM	LOK	URMEM (1044)	
B_SRST_UM	LOK	URMEM (1044)	
B_ST	AUS	BBSTT ( 148 )	SWADAP ( 47 ), ADVE ( 918 ), AEKP ( 970 ), ATM ( 20 ), BGRLP ( 266 ), DLLR ( 578 ), DDST ( 851 ), DLSV ( 301 ), DPH ( 144 ), DMDSTP ( 205 ), ZWMIN ( 669 ), WANWKW ( 125 ), LFS ( 69 ), KOS ( 896 ), GGTFM ( 289 ), GGDVE ( 477 ), GGDPG ( 74 ), ESUK ( 699 ), DLSH ( 330 ), BGLBZ ( 489 ), NLDG ( 157 ), LRHK ( 781 ), LREB ( 739 ), LLRRM ( 566 ), LLRNS ( 562 ), LLRMR ( 572 )
B_STAA	AUS	STADAP ( 684 )	ESNSWL ( 691 ), ESVST ( 677 )
B_STARTINI	AUS	GGDPG ( 74 )	ALE ( 136 )
B_STDPERR	LOK	STADAP ( 684 )	
B_STEIGM	LOK	DLSAHK ( 339 )	
B_STEIGM2	LOK	DLSAHK ( 339 )	
B_STEND	AUS	BBSTT ( 148 )	AEKP ( 970 ), RKTl ( 979 ), MOTAUS (1028), MDKOG ( 516 ), MDFAW ( 508 ), LREB ( 739 ), LRA ( 797 ), LLRRM ( 566 ), LLRNS ( 562 ), LLRMR ( 572 ), LLRBB ( 575 ), LFS ( 69 ), KRRA ( 639 ), KRKE ( 427 ), KOS ( 896 ), HLS ( 392 ), GGUB ( 487 ), GGTFM ( 289 ), GGKS ( 412 ), GGFTS ( 502 ), FUEREG ( 595 ), ESUV ( 1009 ), BGTABST ( 1030 ), BGRLP ( 266 ), BBSAW ( 557 ), BBKHZ ( 890 ), BBBO ( 853 ), AZUE ( 904 ), ATWAL ( 297 ), ATM ( 20 ), ARMD ( 531 ), ALE ( 136 ), SU ( 617 ), GGTFM ( 298 ), GGPED ( 454 ), ESUK ( 699 ), ESSTT ( 679 ), DWUC ( 1147 ), DHLVSK ( 29 ), DHFM ( 233 ), DEVE ( 1017 ), DEGFE ( 592 ), DDVE ( 950 ), DDCY ( 1146 ), BGDVE ( 934 ), EGFE ( 228 )
B_STENDES	AUS	ESSTT ( 679 )	ESNSWL ( 691 ), GK ( 675 )
B_STERHK	EIN		DLSH ( 330 )
B_STERVK	EIN		LRINI ( 749 )
B_STIMNLP	AUS	NLPH ( 150 )	
B_STNDFR	LOK	FUEREG ( 595 )	
B_STNDNL	LOK	ATM ( 20 )	
B_SU	AUS	FE ( 591 )	MSF ( 506 ), SU ( 617 ), BGPU ( 276 ), DMDSTP ( 205 ), GGHFM ( 230 ), MDMAX ( 514 )
B_SU2	AUS	FE ( 591 )	SU ( 617 ), DMDSTP ( 205 )
B_SUKP	LOK	SU ( 617 )	
B_SUKP2	LOK	SU ( 617 )	
B_SUMOD1	LOK	BGSRM ( 245 )	
B_SUMOD2	LOK	BGSRM ( 245 )	
B_SUMOD3	LOK	BGSRM ( 245 )	
B_SVUERF	EIN		GGLSH ( 318 ), GGLSV ( 382 )
B_SVUERF2	EIN		GGLSH ( 318 ), GGLSV ( 382 )
B_SW0	AUS	AZUE ( 904 )	
B_SW1	AUS	AZUE ( 904 )	
B_SWEV	LOK	DSWEC ( 32 )	
B_SWE_B	EIN		DMDSTP ( 205 )
B_SWE_C	AUS	DSWEC ( 32 )	DMDSTP ( 205 )
B_SWE_P	EIN		DMDSTP ( 205 )
B_SWE_S	EIN		DMDSTP ( 205 )
B_SWITCHPG	AUS	DPH ( 144 )	NLDG ( 157 )
B_SYN	AUS	GGDPG ( 74 )	
B_SYNMALE	LOK	GGDPG ( 74 )	
B_SYNCM	AUS	LR ( 768 )	LREB ( 739 )
B_SYNCM2	AUS	LR ( 768 )	LREB ( 739 )



Symbol	Type	Created within	Used within
B._SYNNLDG	AUS	NLDG ( 157 )	GGDPG ( 74 ), WANWKW ( 125 )
B._SYNNOT	EIN		KOEVAB ( 124 )
B._SYNOKNL	LOK	NLDG ( 157 )	
B._SYNPH	AUS	GGDPG ( 74 )	DMDMIL ( 216 ), EGKE ( 409 ), NLPH ( 150 ), DMDSTP ( 205 ), KRRA ( 639 )
B._SYSERR	AUS	D2CTR ( 496 )	
B._SZ	LOK	BGPU ( 276 )	
B._SZKAT	LOK	DKAT ( 361 )	
B._SZKAT2	LOK	DKAT ( 361 )	
B._TABUNPL	LOK	BGTABST ( 1030 )	
B._TAL	AUS	GGFST ( 502 )	DKVS ( 811 ), DLSH ( 330 )
B._TALVAL	AUS	GGFST ( 502 )	DKVS ( 811 ), DLSH ( 330 )
B._TARAU	LOK	LREB ( 739 )	
B._TATMSA	LOK	BBSAWE ( 557 )	
B._TDCAN	AUS	CAN ( 1124 )	DCAS ( 1128 ), DCINS ( 1126 )
B._TE	AUS	GKEB ( 737 )	TEBEB ( 762 ), BBTEGA ( 750 ), LRAEB ( 759 ), TEB ( 826 ), LR ( 768 ), DKVS ( 811 ), ESUKA ( 711 ), DLSA ( 398 ), GKRA ( 766 )
B._TEABB	AUS	TEB ( 826 )	BBTEGA ( 750 ), GKEB ( 737 )
B._TEAKT	LOK	TEB ( 826 )	
B._TEBTES	LOK	LR ( 768 )	
B._TEF	AUS	GKEB ( 737 )	TEBEB ( 762 ), TEB ( 826 )
B._TEHB	AUS	TEB ( 826 )	DKAT ( 361 ), DLSA ( 398 ), DLSAHK ( 339 ), LRHK ( 781 ), ESUKA ( 711 ), DMDSTP ( 205 ), DLLR ( 578 )
B._TEHBX	AUS	TEB ( 826 )	BBTEGA ( 750 ), LR ( 768 )
B._TEHBXF	LOK	BBTEGA ( 750 )	
B._TEI	AUS	GKEB ( 737 )	TEBEB ( 762 ), TEB ( 826 )
B._TEIC	EIN		TEBEB ( 762 )
B._TEMIN	AUS	RKTI ( 979 )	LREB ( 739 )
B._TEMIN2	AUS	RKTI ( 979 )	LREB ( 739 )
B._TEN	AUS	TEBEB ( 762 )	BBTEGA ( 750 ), TEB ( 826 )
B._TENC	EIN		BBTEGA ( 750 ), TEBEB ( 762 )
B._TEP	AUS	BBTEGA ( 750 )	GKEB ( 737 ), TEB ( 826 ), TEBEB ( 762 )
B._TEPC	EIN		BBTEGA ( 750 )
B._TEPI	LOK	BBTEGA ( 750 )	
B._TEPZUS	LOK	BBTEGA ( 750 )	
B._TESLASH	LOK	DLSAHK ( 339 )	
B._TESLASH2	LOK	DLSAHK ( 339 )	
B._TESRDY	AUS	DIMC ( 1148 )	
B._TESSTP	LOK	BBTEGA ( 750 )	
B._TEVIOI	EIN		DTEV ( 856 )
B._TEVIOL	LOK	DTEV ( 856 )	
B._TEVIOLM	LOK	DTEV ( 856 )	
B._TEVIOP	LOK	DTEV ( 856 )	
B._TEVIOR	LOK	DTEV ( 856 )	
B._TEVIOT	EIN		DTEV ( 856 )
B._TEVNIO	LOK	DTEV ( 856 )	
B._TEVNIOM	LOK	DTEV ( 856 )	
B._TEZA	EIN		BBTEGA ( 750 )
B._TEZSTP	LOK	BBTEGA ( 750 )	
B._TFU	AUS	PROKON ( 53 )	ATM ( 20 ), BGTABST ( 1030 )
B._TFWDKSOM	AUS	WDKSOM ( 614 )	FUEDK ( 597 )
B._TIAB0	AUS	DMDMIL ( 216 )	
B._TIAB1	AUS	DMDMIL ( 216 )	
B._TIAB10	AUS	DMDMIL ( 216 )	
B._TIAB11	AUS	DMDMIL ( 216 )	
B._TIAB2	AUS	DMDMIL ( 216 )	
B._TIAB3	AUS	DMDMIL ( 216 )	
B._TIAB4	AUS	DMDMIL ( 216 )	
B._TIAB5	AUS	DMDMIL ( 216 )	
B._TIAB6	AUS	DMDMIL ( 216 )	
B._TIAB7	AUS	DMDMIL ( 216 )	
B._TIAB8	AUS	DMDMIL ( 216 )	
B._TIAB9	AUS	DMDMIL ( 216 )	
B._TIM	LOK	DTRIG ( 1139 )	
B._TIPIN	LOK	KRDY ( 659 )	
B._TIPPG	EIN		BBGANG ( 501 ), BBSAWE ( 557 )
B._TIRED	AUS	BGRPL ( 266 )	
B._TLFSARMX	LOK	LFS ( 69 )	
B._TLFSART	LOK	LFS ( 69 )	
B._TMKICB	EIN		GGTFM ( 289 )
B._TMKR	AUS	KRRA ( 639 )	EGKE ( 409 ), KRDY ( 659 ), GGKS ( 412 )
B._TMLR	AUS	LREB ( 739 )	
B._TMMN	LOK	GGTFM ( 289 )	
B._TMSRT	AUS	GGTFM ( 289 )	
B._TNALU	AUS	DMDLU ( 193 )	
B._TNALU.M	LOK	DMDLU ( 193 )	
B._TNALU.M2	LOK	DMDLU ( 193 )	
B._TNMAX	LOK	NMAXMD ( 584 )	
B._TOCASR1	LOK	CAN ( 1124 )	
B._TOCKUP	LOK	CAN ( 1124 )	
B._TPNMOT	AUS	ARMD ( 531 )	
B._TPNT.AW	LOK	GGKS ( 412 )	
B._TPNT.E	LOK	GGKS ( 412 )	



Symbol	Type	Created within	Used within
B_TPVL	LOK	AEKP ( 970 )	
B_TRFASH	LOK	DLSAHK ( 339 )	
B_TRFASH2	LOK	DLSAHK ( 339 )	
B_TRIP	AUS	D2CTR ( 496 )	
B_TRKH	AUS	AK ( 855 )	BBKHZ ( 890 ), ATM ( 20 ), LLRRM ( 566 )
B_TRSA	LOK	DLSV ( 301 )	
B_TRSA2	LOK	DLSV ( 301 )	
B_TRSAH	LOK	DLSH ( 330 )	
B_TRSAH2	LOK	DLSH ( 330 )	
B_TSPER	LOK	LR ( 768 )	
B_TSPER2	LOK	LR ( 768 )	
B_TSPON	LOK	LR ( 768 )	
B_TSPON2	LOK	LR ( 768 )	
B_TSROOV	AUS	DMDTSB ( 159 )	DMDFON ( 161 ), DMDSTP ( 205 )
B_TSROOV_M	LOK	DMDFON ( 161 )	
B_TTBMH	EIN		GGLSV ( 382 ), DLSV ( 301 )
B_TTBMH2	EIN		GGLSV ( 382 ), DLSV ( 301 )
B_TTBMHH	AUS	DLSH ( 330 )	GGLSH ( 318 )
B_TTBMHH2	AUS	DLSH ( 330 )	GGLSH ( 318 )
B_TTEAE	LOK	BBTEGA ( 750 )	
B_TUMCB	EIN		MDVERB ( 540 )
B_TUSPN	LOK	DLSSA ( 350 )	
B_TUSPN2	LOK	DLSSA ( 350 )	
B_TUSRE	LOK	DLSSA ( 350 )	
B_TUSRE2	LOK	DLSSA ( 350 )	
B_TVARS	LOK	ARM ( 531 )	
B_UBDVE	AUS	ADVE ( 918 )	BGDVE ( 934 ), SREAKT ( 963 )
B_UBDVEC	EIN		ADVE ( 918 )
B_UBDVET	AUS	ADVE ( 918 )	
B_UBPVG	AUS	ADVE ( 918 )	GGDVE ( 477 ), GGPED ( 454 )
B_UBRK	EIN		DECJ ( 1013 ), GGUB ( 487 )
B_UBRMAX	EIN		DECJ ( 1013 )
B_UBVDKP	LOK	GGDVE ( 477 )	
B_UB_OK	AUS	ADVE ( 918 )	DUF ( 1089 ), SREAKT ( 963 ), UFEING ( 1058 ), UFUE ( 1056 )
B_UB_SKA	AUS	UFEING ( 1058 )	UFMET ( 1060 ), UFSPSC ( 1060 ), UFRLC ( 1066 ), UFMVER ( 1087 ), UFRAC ( 1088 ), UFUE ( 1056 )
B_UB_SKA_C	AUS	UFMER ( 1060 )	
B_JDK1NV	LOK	GGDVE ( 477 )	
B_JEINH	LOK	DLSH ( 330 )	
B_JEINH2	LOK	DLSH ( 330 )	
B_JEINV	LOK	DLSV ( 301 )	
B_JEINV2	LOK	DLSV ( 301 )	
B_JFGRHE	AUS	UFFGRE ( 1096 )	
B_JFGRHS	AUS	UFFGRE ( 1096 )	GGFGRH ( 473 )
B_JFGRSB	AUS	UFFGRE ( 1096 )	GGFGRH ( 473 )
B_JFGRSV	AUS	UFFGRE ( 1096 )	GGFGRH ( 473 )
B_JFGRWA	AUS	UFFGRE ( 1096 )	GGFGRH ( 473 )
B_JGD	AUS	BGMSZS ( 239 )	BGPU ( 276 )
B_JGDS	LOK	FUEDK ( 597 )	
B_JGDSP	LOK	BGRLP ( 266 )	
B_UHRRMIN	AUS	PROKON ( 53 )	ATM ( 20 ), BGTABST ( 1030 )
B_UHRRSEC	AUS	PROKON ( 53 )	AEKP ( 970 ), ATM ( 20 ), BGTABST ( 1030 )
B_UHSIG	LOK	DLSH ( 330 )	
B_UHSIG2	LOK	DLSH ( 330 )	
B_UK1	LOK	ESUK ( 699 )	
B_UKA	LOK	ESUKA ( 711 )	
B_UKA2	LOK	ESUKA ( 711 )	
B_UKAB	LOK	ESUKA ( 711 )	
B_UKABA	LOK	ESUKA ( 711 )	
B_UKABA2	LOK	ESUKA ( 711 )	
B_UKABAF	LOK	ESUKA ( 711 )	
B_UKABAF2	LOK	ESUKA ( 711 )	
B_UKABAH	LOK	ESUKA ( 711 )	
B_UKABAL	LOK	ESUKA ( 711 )	
B_UKABAM	LOK	ESUKA ( 711 )	
B_UKABAM2	LOK	ESUKA ( 711 )	
B_UKADBA	LOK	ESUKA ( 711 )	
B_UKADBA2	LOK	ESUKA ( 711 )	
B_UKADVA	LOK	ESUKA ( 711 )	
B_UKADVA2	LOK	ESUKA ( 711 )	
B_UKAIBA	LOK	ESUKA ( 711 )	
B_UKAIBA2	LOK	ESUKA ( 711 )	
B_UKAIVA	LOK	ESUKA ( 711 )	
B_UKAIVA2	LOK	ESUKA ( 711 )	
B_UKAT	LOK	ESUKA ( 711 )	
B_UKAVA	LOK	ESUKA ( 711 )	
B_UKAVA2	LOK	ESUKA ( 711 )	
B_UKAVAF	LOK	ESUKA ( 711 )	
B_UKAVAF2	LOK	ESUKA ( 711 )	
B_UKAVAH	LOK	ESUKA ( 711 )	
B_UKAVAH2	LOK	ESUKA ( 711 )	
B_UKAVAM	LOK	ESUKA ( 711 )	



Symbol	Type	Created within	Used within
B_JKAVAM2	LOK	ESUKA ( 711 )	
B_JKE	LOK	ESUK ( 699 )	
B_JKG	AUS	ESUK ( 699 )	DKAT ( 361 ), LRAEB ( 759 ), ESVST ( 677 )
B_JKNS	LOK	ESUK ( 699 )	
B_UMAE	AUS	BGDVE ( 934 )	DDVE ( 950 )
B_UMAUAB	AUS	BGDVE ( 934 )	DDVE ( 950 ), SREAKT ( 963 )
B_UPW12E	LOK	GGPED ( 454 )	
B_UPW1MN	LOK	GGPED ( 454 )	
B_UPW1MX	LOK	GGPED ( 454 )	
B_UPW2MN	LOK	GGPED ( 454 )	
B_UPW2MX	LOK	GGPED ( 454 )	
B_UPWG1O	LOK	GGPED ( 454 )	
B_UPWG1U	LOK	GGPED ( 454 )	
B_UPWG2O	LOK	GGPED ( 454 )	
B_UPWG2U	LOK	GGPED ( 454 )	
B_USBEV	LOK	GGLSV ( 382 )	
B_USBEV2	LOK	GGLSV ( 382 )	
B_USHKF	LOK	DLSAHK ( 339 )	
B_USHKF2	LOK	DLSAHK ( 339 )	
B_USHKM	LOK	DLSAHK ( 339 )	
B_USHKM2	LOK	DLSAHK ( 339 )	
B_USHSCH	LOK	DLSAHK ( 339 )	
B_USHSCH2	LOK	DLSAHK ( 339 )	
B_UVSIG	LOK	DLSV ( 301 )	
B_UVSIG2	LOK	DLSV ( 301 )	
B_VA	AUS	ESUK ( 699 )	
B_VAAU	LOK	ESUK ( 699 )	
B_VADGE	LOK	DLSV ( 301 )	
B_VADGE2	LOK	DLSV ( 301 )	
B_VAG	AUS	ESUK ( 699 )	LREB ( 739 )
B_VAKL	LOK	ESUK ( 699 )	
B_VBEMG	AUS	ESSTT ( 679 )	BGTABST ( 1030 ), STADAP ( 684 )
B_VBMG	LOK	ESSTT ( 679 )	
B_VEKAT	AUS	DKAT ( 361 )	
B_VEKAT2	AUS	DKAT ( 361 )	
B_VERRUECK	LOK	RDE ( 112 )	
B_VGEFLR	LOK	DLSV ( 301 )	
B_VGEFLR2	LOK	DLSV ( 301 )	
B_VIRT_TR	EIN		AZUE ( 904 )
B_VL	AUS	MDFAW ( 508 )	MSF ( 506 ), LRAEB ( 759 ), NWS ( 618 )
B_VLLR	AUS	LLRBB ( 575 )	BBSAWE ( 557 ), LLRRM ( 566 ), MDVERAD ( 549 ), LLRMD ( 561 )
B_VMAX	AUS	VMAXMD ( 588 )	
B_VNULL	AUS	GGVFZG ( 497 )	BBGANG ( 501 ), MDFAW ( 508 ), KRDY ( 659 )
B_VPWGERR	LOK	GGPED ( 454 )	
B_VS	EIN		ESVW ( 1009 ), LREB ( 739 )
B_VZIELS	EIN		FGRFULO ( 1160 )
B_WAITGAP	LOK	RDE ( 112 )	
B_WAL	AUS	ATWAL ( 297 )	
B_WALALT	LOK	ATWAL ( 297 )	
B_WDK12EV	LOK	GGDVE ( 477 )	
B_WDK13EV	LOK	GGDVE ( 477 )	
B_WDK1V	EIN		ADVE ( 918 ), FUEDKSA ( 610 ), GGDVE ( 477 )
B_WDK23EV	LOK	GGDVE ( 477 )	
B_WDK2SEL	AUS	GGDVE ( 477 )	ADVE ( 918 ), UFRLC ( 1066 ), BGDVE ( 934 ), DUF ( 1089 )
B_WDK2ST	LOK	GGDVE ( 477 )	
B_WDKAP	LOK	FUEDK ( 597 )	
B_WDKSAP	AUS	PROKON ( 53 )	FUEDK ( 597 )
B_WDKSIVE	AUS	ADVE ( 918 )	DDVE ( 950 ), SREAKT ( 963 )
B_WDKSOM	AUS	WDKSOM ( 614 )	FUEDK ( 597 )
B_WF	LOK	ESUK ( 699 )	
B_WK	EIN		ARMD ( 531 ), DMDLU ( 193 ), DMDLUA ( 202 ), DMDSTP ( 205 ), DSWEC ( 32 ), DMDDL ( 199 )
B_WKAUF	EIN		LLRNS ( 562 )
B_WKR	EIN		DMDDL ( 199 ), DMDLU ( 193 ), DMDSTP ( 205 ), DMDLUA ( 202 )
B_WKRAL	LOK	KRRA ( 639 )	
B_WKS	AUS	ESSTT ( 679 )	ESNSWL ( 691 ), STADAP ( 684 ), ESVST ( 677 )
B_WNWI2OUT	AUS	WANWKW ( 125 )	NLDG ( 157 )
B_WNWIOU	AUS	WANWKW ( 125 )	NLDG ( 157 )
B_WNWIOUTX	LOK	NLDG ( 157 )	
B_WPABNB	LOK	GGPED ( 454 )	
B_WPMBBR	LOK	GGPED ( 454 )	
B_WST	AUS	ESSTT ( 679 )	AK ( 855 ), BBKHZ ( 890 )
B_WST0	LOK	ESSTT ( 679 )	
B_WST1	LOK	ESSTT ( 679 )	
B_WST2	LOK	ESSTT ( 679 )	
B_WUC	AUS	DWUC ( 1147 )	DFPM ( 1132 ), DTRIG ( 1139 ), DMDMIL ( 216 )
B_YDKT	LOK	DKAT ( 361 )	
B_Z1	AUS	AZUE ( 904 )	
B_ZAS	EIN		AEVAB ( 980 )
B_ZASA	EIN		DMDDL ( 199 ), DMDLU ( 193 ), DMDLUA ( 202 )
B_ZASAKT	EIN		MDVER ( 546 )
B_ZASAM	LOK	DMDUE ( 158 )	



Symbol	Type	Created within	Used within
B_ZESYNC	AUS	AZUE ( 904 )	ESSTT ( 679 )
B_ZKATB	LOK	DKAT ( 361 )	
B_ZKATB2	LOK	DKAT ( 361 )	
B_ZKATS	LOK	DKAT ( 361 )	
B_ZKATS2	LOK	DKAT ( 361 )	
B_ZKATZ	LOK	DKAT ( 361 )	
B_ZKATZ2	LOK	DKAT ( 361 )	
B_ZPREL	AUS	GGDPG ( 74 )	ALE ( 136 )
B_ZTEV	AUS	DTEVE ( 1022 )	
B_ZWAFH	AUS	LLRMR ( 572 )	
B_ZWAPPL	AUS	PROKON ( 53 )	ZUE ( 627 )
B_ZWGET	LOK	MDKOG ( 516 )	
B_ZWKRA	LOK	ZUE ( 627 )	
B_ZWKRAA	AUS	KRRA ( 639 )	KRDY ( 659 ), EGKE ( 409 )
B_ZWKRAM	LOK	KRRA ( 639 )	
B_ZWMNPST	LOK	ZWMIN ( 669 )	
B_ZWNGET	LOK	MDKOG ( 516 )	
B_ZWS0	AUS	AZUE ( 904 )	
B_ZWVS	AUS	MDKOG ( 516 )	MDZW ( 636 )
B_ZWVZ	AUS	MDKOG ( 516 )	MDAUTG ( 515 ), MDZW ( 636 )
B_ZWVZVB	LOK	MDKOG ( 516 )	
B_ZZTAB	AUS	GGDPG ( 74 )	DPH ( 144 ), WANWKW ( 125 )
CFOX	LOK	DMDFON ( 161 )	
CIDISTIM	LOK	BGDVE ( 934 )	
CPAW1	LOK	GGDVE ( 477 )	
CPAW2	LOK	GGDVE ( 477 )	
CRYAGR	EIN		DIMC ( 1148 )
CRYHS	EIN		DIMC ( 1148 )
CRYKAT	EIN		DIMC ( 1148 )
CRYLS	EIN		DIMC ( 1148 )
CRYSLS	EIN		DIMC ( 1148 )
CRYTES	EIN		DIMC ( 1148 )
CTBETIP	LOK	GGFGRH ( 473 )	
CTDVIV_ZW	LOK	FGRABED ( 491 )	
CTDVZV_W	LOK	FGRABED ( 491 )	
CTFGRAB	LOK	FGRREGL ( 1174 )	
CTFGRFDY	LOK	FGRABED ( 491 )	
CTFGRHE	LOK	GGFGRH ( 473 )	
CTFGRUEOB	LOK	FGRABED ( 491 )	
CTFGRUM	LOK	FGRABED ( 491 )	
CTFGRUNUB	LOK	FGRABED ( 491 )	
CTRBWF	LOK	GGPED ( 454 )	
CTRERBR	LOK	GGEGAS ( 474 )	
CTRERF1	AUS	D2CTR ( 496 )	
CTRRDY1	AUS	D2CTR ( 496 )	
CTRSFP	AUS	D2CTR ( 496 )	
CTRZYF0	AUS	D2CTR ( 496 )	
CTRZYF1	AUS	D2CTR ( 496 )	
CTSWK	LOK	FGRFULO ( 1160 )	
CTVETIP	LOK	GGFGRH ( 473 )	
CVFUBAANZ	EIN		ZUESZ ( 632 )
CVOFFZ_W	EIN		ZUESZ ( 632 )
CVSZFUBA_W	EIN		ZUESZ ( 632 )
CVWDK	EIN		FUEDK ( 597 )
CVZWZYL	EIN		ZUE ( 627 )
CW_DKNOLU	EIN		ADVE ( 918 )
CWDLRIKL	EIN		ADVE ( 918 )
CW_ERFIL	AUS	PROKON ( 53 )	TCSORT ( 1122 )
CW_OBD	AUS	PROKON ( 53 )	
CW_TABST	EIN		GGTFM ( 289 )
C_BMSUCH	EIN		BGNMOT ( 111 ), GGDPG ( 74 )
C_FCMCLR	EIN		BGDVE ( 934 ), DCAS ( 1128 ), CAN ( 1124 ), DCINS ( 1126 ), DDCY ( 1146 ), DEKPE ( 1020 ), DHLSHK ( 1154 ), DEVE ( 1017 ), DLSAHK ( 339 ), DLSA ( 398 ), DKVS ( 811 ), DKRTP ( 451 ), DKRNT ( 445 ), DKOSE ( 901 ), DIMC ( 1148 ), DHLVKE ( 902 ), GGDPG ( 74 ), DWUC ( 1147 ), DVFZ ( 500 ), DTEVE ( 1022 ), DPH ( 144 ), DNWSE ( 1025 ), DNWS ( 622 ), DNWKW ( 134 ), DMILE ( 36 ), DMIL ( 1150 ), DLSH ( 330 ), WANWKW ( 125 ), LRHK ( 781 ), GGUB ( 487 ), GGTFM ( 289 ), GGTFM ( 298 ), DHLSVK ( 29 ), DDG ( 141 ), BGKMST ( 1008 ), DCKUP ( 1128 ), EGFE ( 228 ), DVKUP ( 1027 )



Symbol	Type	Created within	Used within
C_JNI	AUS	SWADAP ( 47 )	AEKP ( 970 ), BBBO ( 853 ), BGDVE ( 934 ), BBKHZ ( 890 ), GGLSV ( 382 ), GGLSH ( 318 ), GGDGP ( 74 ), FUEREG ( 595 ), ESUKA ( 711 ), DWUC ( 1147 ), DVFZ ( 500 ), DTEVE ( 1022 ), MOTAUS ( 1028 ), MDZUL ( 523 ), MDWAN ( 554 ), MDVERAD ( 549 ), MDNSTAB ( 556 ), MDFUE ( 594 ), LRKA ( 795 ), LRHK ( 781 ), UFUE ( 1056 ), UFRLC ( 1066 ), UFREAC ( 1088 ), UFNSC ( 1077 ), UFMsrc ( 1080 ), STADAP ( 684 ), RRTI ( 979 ), LREB ( 739 ), LR ( 768 ), LAMKO ( 729 ), LAMBTS ( 732 ), HLS ( 392 ), GGUB ( 487 ), GGTFM ( 289 ), GGTFM ( 289 ), DMLSE ( 34 ), DLSH ( 330 ), DLSAHK ( 339 ), DLSA ( 398 ), DKVS ( 811 ), DKRTP ( 451 ), DKRNT ( 445 ), DKOSE ( 901 ), DPH ( 144 ), DNWSE ( 1025 ), DNWS ( 622 ), DNWKW ( 134 ), BGTEV ( 257 ), BGNMOT ( 111 ), BGLBZ ( 489 ), BGKMS ( 1008 ), BGAGR ( 263 ), ALE ( 136 ), ATM ( 20 ), AES ( 973 ), DMILE ( 36 ), DIMC ( 1148 ), DHLVKE ( 902 ), DHLVK ( 29 ), DHLSHK ( 1154 ), DEVE ( 1017 ), DEKPE ( 1020 ), DDST ( 851 ), DDG ( 141 ), DDCY ( 1146 ), DCKUP ( 1128 ), DCINS ( 1126 ), DCAS ( 1128 ), CAN ( 1124 ), BGWDM ( 273 ), DVKUP ( 1027 )
C_JNI2	EIN		BGTABST ( 1030 )
C_JNISYN	EIN		ALE ( 136 ), BGNMOT ( 111 ), BGRGL ( 274 ), DDG ( 141 ), DMIL ( 1150 ), DPH ( 144 ), NLDG ( 157 ), WANWKW ( 125 ), GGDGP ( 74 ), DNWS ( 622 ), DEPCL ( 1151 ), BGTABST ( 1030 ), BNG ( 121 ), BBSTT ( 148 )
C_JNACHL	EIN		AEKP ( 970 ), GGUB ( 487 ), GGTFM ( 289 ), GGTFM ( 298 ), DMIL ( 1150 ), BGTABST ( 1030 ), BGDVE ( 934 ), BBKHZ ( 890 ), ATM ( 20 ), WANWKW ( 125 ), MOTAUS ( 1028 ), ALE ( 136 )
C_NMAX	AUS	BGBSZ ( 73 )	
C_NORM	EIN		MOTAUS ( 1028 ), WANWKW ( 125 )
C_NOSERE	EIN		CAN ( 1124 )
C_NSUCH	EIN		GGDPG ( 74 )
C_PWF	AUS	SWADAP ( 47 )	ALE ( 136 ), ATM ( 20 ), BGDVE ( 934 ), BBBO ( 853 ), DWUC ( 1147 ), DVFZ ( 500 ), DTOP ( 1145 ), DTEVE ( 1022 ), DPH ( 144 ), DNWSE ( 1025 ), DNWKW ( 134 ), DMILE ( 36 ), DKOSE ( 901 ), DHLVKE ( 902 ), DHLVK ( 29 ), DHLSHK ( 1154 ), DEVE ( 1017 ), DEKPE ( 1020 ), DDG ( 141 ), DDCY ( 1146 ), GGUB ( 487 ), ESUKA ( 711 ), DLSSA ( 350 ), DLSAHK ( 339 ), DKVS ( 811 ), DKRTP ( 451 ), DKRNT ( 445 ), DCKUP ( 1128 ), DCINS ( 1126 ), WANWKW ( 125 ), STADAP ( 684 ), MOTAUS ( 1028 ), MDVERAD ( 549 ), LRHK ( 781 ), GGTFM ( 289 ), GGTFM ( 298 ), GGDGP ( 74 ), DCAS ( 1128 ), CAN ( 1124 ), BGTABST ( 1030 ), DVKUP ( 1027 )
C_SYN	EIN		BNG ( 121 ), WANWKW ( 125 ), DNWS ( 622 ), GGDGP ( 74 )
DCYCNT	AUS	DDCY ( 1146 )	
DEKPUB	LOK	AEKP ( 970 )	
DETAZWBS	LOK	LAMBTS ( 732 )	
DETAZWTE	LOK	DTEV ( 856 )	
DEVOFF	EIN		AES ( 973 ), AEVAB ( 980 )
DFP_AAVE	DOK	DTEV ( 856 )	TEBEB ( 762 )
DFP_AGRE	DOK	DKAT ( 361 )	DTEV ( 856 ), LRAEB ( 759 ), DMDSTP ( 205 )
DFP_AGRF	DOK	DKAT ( 361 )	DTEV ( 856 ), LRAEB ( 759 ), DMDSTP ( 205 )
DFP_BM	DOK	LRAEB ( 759 )	RDE ( 112 ), DMDSTP ( 205 )
DFP_BREMS	DOK	GGEGAS ( 474 )	
DFP_BWF	DOK	GGPED ( 454 )	
DFP_DK	DOK	BGMSZS ( 239 )	
DFP_DK1P	DOK	GGDVE ( 477 )	DTEV ( 856 ), DKAT ( 361 ), GGDVE ( 477 ), TEBEB ( 762 ), LRAEB ( 759 )
DFP_DK2P	DOK	GGDVE ( 477 )	
DFP_DPL	DOK	LRA ( 797 )	
DFP_DVEE	DOK	DDVE ( 950 )	
DFP_DVEF	DOK	DDVE ( 950 )	
DFP_DVEFO	DOK	DDVE ( 950 )	
DFP_DVEL	DOK	DDVE ( 950 )	
DFP_DVEN	DOK	DDVE ( 950 )	
DFP_DVER	DOK	DDVE ( 950 )	
DFP_DVET	DOK	DDVE ( 950 )	
DFP_DVEU	DOK	DDVE ( 950 )	LRAEB ( 759 ), DTEV ( 856 )
DFP_DVEUB	DOK	DDVE ( 950 )	
DFP_DVEUW	DOK	DDVE ( 950 )	
DFP_DVEV	DOK	DDVE ( 950 )	GGDVE ( 477 )
DFP_EV1	DOK	AEVAB ( 980 )	
DFP_EV2	DOK	AEVAB ( 980 )	
DFP_EV3	DOK	AEVAB ( 980 )	
DFP_EV4	DOK	AEVAB ( 980 )	
DFP_EV5	DOK	AEVAB ( 980 )	
DFP_EV6	DOK	AEVAB ( 980 )	
DFP_EV7	DOK	AEVAB ( 980 )	
DFP_EV8	DOK	AEVAB ( 980 )	
DFP_FP1P	DOK	GGPED ( 454 )	
DFP_FP2P	DOK	GGPED ( 454 )	
DFP_FPP	DOK	GGPED ( 454 )	
DFP_FRAO	DOK	LRA ( 797 )	
DFP_FRAO2	DOK	LRA ( 797 )	
DFP_FRAU	DOK	LRA ( 797 )	
DFP_FRAU2	DOK	LRA ( 797 )	
DFP_HSH	DOK	DKAT ( 361 )	
DFP_HSH2	DOK	DKAT ( 361 )	
DFP_HSV	DOK	DKAT ( 361 )	
DFP_HSV2	DOK	DKAT ( 361 )	
DFP_KAT	DOK	DKAT ( 361 )	



Symbol	Type	Created within	Used within
DFP_KAT2	DOK	DKAT ( 361 )	
DFP_KRNT	DOK	KRRA ( 639 )	
DFP_KROF	DOK	KRRA ( 639 )	
DFP_KRTP	DOK	KRRA ( 639 )	
DFP_KS1	DOK	KRRA ( 639 )	
DFP_KS2	DOK	KRRA ( 639 )	
DFP_KS3	DOK	KRRA ( 639 )	
DFP_KS4	DOK	KRRA ( 639 )	
DFP_LASH	DOK	DKAT ( 361 )	
DFP_LASH2	DOK	DKAT ( 361 )	
DFP_LATP	DOK	DKAT ( 361 )	
DFP_LATP2	DOK	DKAT ( 361 )	
DFP_LATV	DOK	DKAT ( 361 )	
DFP_LATV2	DOK	DKAT ( 361 )	
DFP_LDE	EIN		DMDSTP ( 205 )
DFP_LDPE	DOK	DTEV ( 856 )	TEBEB ( 762 )
DFP_LLR	DOK	DTEV ( 856 )	
DFP_LM	DOK	BGMSZS ( 239 )	DTEV ( 856 ), DLLR ( 578 ), DKAT ( 361 ), DHFM ( 233 )
DFP_LSH	DOK	DKAT ( 361 )	
DFP_LSH2	DOK	DKAT ( 361 )	
DFP_LSHV	DOK	DKAT ( 361 )	
DFP_LSV	DOK	DKAT ( 361 )	DLSV ( 301 ), TEB ( 826 )
DFP_LSV2	DOK	DKAT ( 361 )	DLSV ( 301 ), TEB ( 826 )
DFP_MD	DOK	DKAT ( 361 )	DMDSTP ( 205 )
DFP_MDB	DOK	MDKOG ( 516 )	
DFP_N	DOK	RDE ( 112 )	DMDSTP ( 205 )
DFP_NWKW	EIN		DMDSTP ( 205 )
DFP_NWKW2	EIN		DMDSTP ( 205 )
DFP_NWS	EIN		DMDSTP ( 205 )
DFP_NWS2	EIN		DMDSTP ( 205 )
DFP_NWSE	EIN		DMDSTP ( 205 )
DFP_PH	DOK	NLPH ( 150 )	
DFP_RKAT	DOK	LRA ( 797 )	
DFP_RKAT2	DOK	LRA ( 797 )	
DFP_RKAZ	DOK	LRA ( 797 )	
DFP_RKAZ2	DOK	LRA ( 797 )	
DFP_SLPE	DOK	DKAT ( 361 )	
DFP_SLS	DOK	DTEV ( 856 )	
DFP_SLVE	DOK	DKAT ( 361 )	
DFP_SUE	EIN		DMDSTP ( 205 )
DFP_SUE2	EIN		DMDSTP ( 205 )
DFP_TA	DOK	DLLR ( 578 )	LRAEB ( 759 )
DFP_TES	DOK	DKAT ( 361 )	LRAEB ( 759 ), DTEV ( 856 ), DLSV ( 301 ), DLLR ( 578 ), DMDSTP ( 205 )
DFP_TEVE	DOK	DKAT ( 361 )	DLLR ( 578 ), DTEV ( 856 ), TEBEB ( 762 ), LRAEB ( 759 ), DLSV ( 301 ), DMDSTP ( 205 )
DFP_TM	DOK	DLLR ( 578 )	LRAEB ( 759 ), DTEV ( 856 ), DLSV ( 301 )
DFP_UB	DOK	DTEV ( 856 )	LRAEB ( 759 )
DFP_UVSE	EIN		DMDSTP ( 205 )
DFP_VFZ	DOK	BBGANG ( 501 )	RDE ( 112 ), GGVFZG ( 497 ), GGPED ( 454 ), DTEV ( 856 ), DLLR ( 578 ), DMDSTP ( 205 )
DFRKA2_W	LOK	GKRA ( 766 )	
DFRKA_W	LOK	GKRA ( 766 )	
DFRM2_W	LOK	LRA ( 797 )	
DFRMT2_W	LOK	LRA ( 797 )	
DFRMT_W	LOK	LRA ( 797 )	
DFRM_W	LOK	LRA ( 797 )	
DFRSP2_W	AUS	LR ( 768 )	ESUKA ( 711 )
DFRSP_W	AUS	LR ( 768 )	ESUKA ( 711 )
DFRST2_W	AUS	LR ( 768 )	ESUKA ( 711 )
DFRSTGA2_W	DOK	LR ( 768 )	
DFRSTGA_W	DOK	LR ( 768 )	
DFRSTTE2_W	DOK	LR ( 768 )	
DFRSTTE_W	DOK	LR ( 768 )	
DFRST_W	AUS	LR ( 768 )	ESUKA ( 711 )
DFSE01	LOK	DMDFON ( 161 )	
DFSE02	LOK	DMDFON ( 161 )	
DFSE03	LOK	DMDFON ( 161 )	
DFSE04	LOK	DMDFON ( 161 )	
DFSE05	LOK	DMDFON ( 161 )	
DFSE06	LOK	DMDFON ( 161 )	
DFSE07	LOK	DMDFON ( 161 )	
DFSE08	LOK	DMDFON ( 161 )	
DFSEN	LOK	DMDFON ( 161 )	
DFSERESZ	LOK	DMDFON ( 161 )	
DFTEF_W	LOK	TEB ( 826 )	
DFUELSAN_W	AUS	BGMSZS ( 239 )	DTEV ( 856 )
DKATAKT2_W	LOK	DKAT ( 361 )	
DKATAKT_W	LOK	DKAT ( 361 )	
DKATEFRG	LOK	TEB ( 826 )	
DKHC_W	LOK	TEB ( 826 )	
DKLAGERC	LOK	ADVE ( 918 )	
DKLDFPWWL_W	LOK	DTEV ( 856 )	



Symbol	Type	Created within	Used within
DKPSTG_W	AUS	BGDVE ( 934 )	GGDVE ( 477 )
DLAHI2_W	EIN		DLSSA ( 350 )
DLAHISA	AUS	DLSSA ( 350 )	
DLAHISA2	AUS	DLSSA ( 350 )	
DLAHL_W	EIN		DLSSA ( 350 )
DLAHKAB2_W	LOK	LRHK ( 781 )	
DLAHKAB_W	LOK	LRHK ( 781 )	
DLAMATR2_W	EIN		LAMKO ( 729 ), LAMSOLL ( 726 )
DLAMATR_W	EIN		LAMKO ( 729 ), LAMSOLL ( 726 )
DLAMBTS_W	AUS	LAMBTS ( 732 )	LAMKO ( 729 ), LAMSOLL ( 726 )
DLASHK12_W	LOK	LRHK ( 781 )	
DLASHK1_W	LOK	LRHK ( 781 )	
DLASHKM2_W	LOK	LRHK ( 781 )	
DLASHKM_W	LOK	LRHK ( 781 )	
DLASHKP2_W	LOK	LRHK ( 781 )	
DLASHKP_W	LOK	LRHK ( 781 )	
DLRBATKP_W	LOK	ADVE ( 918 )	
DLRD	LOK	ADVE ( 918 )	
DLRDANT_W	LOK	ADVE ( 918 )	
DLRDSV_W	LOK	ADVE ( 918 )	
DLRDSW_W	LOK	ADVE ( 918 )	
DLRI	LOK	ADVE ( 918 )	
DLRIAMAX	LOK	ADVE ( 918 )	
DLRIANTMAN	LOK	ADVE ( 918 )	
DLRIANT_L	LOK	ADVE ( 918 )	
DLRIANT_W	LOK	ADVE ( 918 )	
DLRIKLMAN	LOK	ADVE ( 918 )	
DLRIK1ST_W	LOK	ADVE ( 918 )	
DLRIK1_W	LOK	ADVE ( 918 )	
DLRKOMP	LOK	ADVE ( 918 )	
DLRMXT	LOK	BGDVE ( 934 )	
DLRP	LOK	ADVE ( 918 )	
DLRPANT_L	LOK	ADVE ( 918 )	
DLRPER1_W	LOK	LR ( 768 )	
DLRPERP_W	LOK	LR ( 768 )	
DLRPER_W	LOK	LR ( 768 )	
DLRPIDC	LOK	ADVE ( 918 )	
DLRRAST	LOK	ADVE ( 918 )	
DLRSPID_W	AUS	ADVE ( 918 )	BGDVE ( 934 )
DLSD_W	LOK	MDFAW ( 508 )	
DLURS	LOK	DMDDL ( 199 )	
DLURS_M	LOK	DMDDL ( 199 )	
DLURS_M2	LOK	DMDDL ( 199 )	
DLUTS	LOK	DMDDL ( 199 )	
DLUTS1	AUS	DMDDL ( 199 )	
DLUTS10	AUS	DMDDL ( 199 )	
DLUTS11	AUS	DMDDL ( 199 )	
DLUTS12	AUS	DMDDL ( 199 )	
DLUTS2	AUS	DMDDL ( 199 )	
DLUTS3	AUS	DMDDL ( 199 )	
DLUTS4	AUS	DMDDL ( 199 )	
DLUTS5	AUS	DMDDL ( 199 )	
DLUTS6	AUS	DMDDL ( 199 )	
DLUTS7	AUS	DMDDL ( 199 )	
DLUTS8	AUS	DMDDL ( 199 )	
DLUTS9	AUS	DMDDL ( 199 )	
DLUTS_M	LOK	DMDDL ( 199 )	
DLUTS_M2	LOK	DMDDL ( 199 )	
DLWSL_W	LOK	MDVERB ( 540 )	
DLWS_W	EIN		MDVERB ( 540 )
DMAR_W	AUS	ARMD ( 531 )	MSF ( 506 ), MDKOG ( 516 )
DMAUFR_W	EIN		MDAUTG ( 515 ), MDZW ( 636 )
DMBEBL_W	LOK	MDFAW ( 508 )	
DMDEVAB	LOK	AEVAB ( 980 )	
DMDPO_W	LOK	MDFAW ( 508 )	
DMDPU_W	LOK	MDFAW ( 508 )	
DMGBEG_W	LOK	MDFAW ( 508 )	
DMLETANF_W	LOK	DTEV ( 856 )	
DMLETANU	LOK	DTEV ( 856 )	
DMLETAN_W	LOK	DTEV ( 856 )	
DMLFTEF	LOK	TEB ( 826 )	
DMLLRD_W	AUS	LLRRM ( 566 )	
DMLLRI_W	AUS	LLRMD ( 561 )	LLRRM ( 566 ), DLLR ( 578 ), MDVERAD ( 549 ), MDFAW ( 508 ), KHMD ( 894 )
DMLLRL_W	AUS	LLRRM ( 566 )	MDKOL ( 526 )
DMLLRP_W	AUS	LLRRM ( 566 )	
DMLLR_W	AUS	LLRMD ( 561 )	LLRRM ( 566 ), MDAUTG ( 515 ), MSF ( 506 ), MDKOG ( 516 )
DMLMS_W	LOK	MDKOL ( 526 )	
DMLSDO_W	LOK	MDFAW ( 508 )	
DMLSDU_W	LOK	MDFAW ( 508 )	
DMNMXP_W	LOK	NMAXMD ( 584 )	
DMRAC	AUS	MDVERB ( 540 )	LLRMR ( 572 )
DMRAR_W	LOK	FGRREGL ( 1174 )	





Symbol	Type	Created within	Used within
DMRDAGR_W	EIN		MDTRIP ( 538 )
DMRDKT_W	AUS	DKAT ( 361 )	MDTRIP ( 538 )
DMRDSL_W	AUS	KHMD ( 894 )	MDTRIP ( 538 )
DMRESLL_W	LOK	LLRMR ( 572 )	
DMRKH	AUS	AK ( 855 )	MSF ( 506 ), KHMD ( 894 ), DMDLU ( 193 ), MDKOL ( 526 ), MDKOG ( 516 )
DMRKHZ_W	LOK	KHMD ( 894 )	
DMRKH_W	AUS	KHMD ( 894 )	
DMRKT_W	AUS	MDTRIP ( 538 )	MDKOG ( 516 ), MDKOL ( 526 )
DMRLASH_W	AUS	DLSAHK ( 339 )	MDTRIP ( 538 )
DMRLF	AUS	MDVERB ( 540 )	LLRMR ( 572 )
DMRLF1	LOK	MDVERB ( 540 )	
DMRLF2	LOK	MDVERB ( 540 )	
DMRLLR_W	AUS	LLRMD ( 561 )	LLRMR ( 572 ), MDKOG ( 516 ), MSF ( 506 ), MDKOL ( 526 )
DMRLSH_W	AUS	DLSH ( 330 )	MDTRIP ( 538 )
DMRLSV_W	EIN		MDTRIP ( 538 )
DMRMX_W	AUS	MDKOL ( 526 )	MDZUL ( 523 )
DMRWAN	EIN		LLRMR ( 572 )
DMSNTE_W	AUS	DTEV ( 856 )	
DMSSGINR	LOK	TEB ( 826 )	
DMVADFK_W	LOK	MDVERAD ( 549 )	
DMVADFS_W	LOK	MDVERAD ( 549 )	
DMVADKO_W	LOK	MDVERAD ( 549 )	
DMVADLL_W	LOK	MDVERAD ( 549 )	
DMVAD_W	AUS	MDVERAD ( 549 )	DTEV ( 856 ), MDMIN ( 538 ), MDVER ( 546 )
DMVAMNFK_W	DOK	MDVERAD ( 549 )	
DMVAMNFS_W	DOK	MDVERAD ( 549 )	
DMVAMNKO_W	DOK	MDVERAD ( 549 )	
DMVAMNLL_W	DOK	MDVERAD ( 549 )	
DMVAMXFK_W	DOK	MDVERAD ( 549 )	
DMVAMXFS_W	DOK	MDVERAD ( 549 )	
DMVAMXKO_W	DOK	MDVERAD ( 549 )	
DMVAMXLL_W	DOK	MDVERAD ( 549 )	
DMVERL_W	AUS	MDVER ( 546 )	MDFAW ( 508 )
DMVLLRSU_W	LOK	LLRMR ( 572 )	
DMVMXI_W	LOK	VMAXMD ( 588 )	
DMVMXP_W	LOK	VMAXMD ( 588 )	
DMZMS_W	AUS	MDKOG ( 516 )	
DN	AUS	LLRRM ( 566 )	LLRBB ( 575 ), LLRMR ( 572 ), LLRMD ( 561 )
DNIKORR_W	LOK	LLRRM ( 566 )	
DNMOTAS_W	AUS	BGNG ( 121 )	
DNMOT_W	AUS	BGNG ( 121 )	ESSTT ( 679 ), STADAP ( 684 ), RDE ( 112 )
DNS	AUS	LLRNS ( 562 )	DLLR ( 578 ), LLRRM ( 566 ), LLRMR ( 572 ), LLRMD ( 561 )
DNSA	LOK	BBSAWE ( 557 )	
DNSL_W	LOK	NMAXMD ( 584 )	
DNTURB	LOK	MDWAN ( 554 )	
DN_W	AUS	LLRRM ( 566 )	LLRMD ( 561 )
DPDK_W	LOK	FUEDK ( 597 )	
DPERMF_W	LOK	LR ( 768 )	
DPSDVS_W	LOK	BGRLP ( 266 )	BGRLP ( 266 ), EGFE ( 228 )
DPSFG_W	AUS	BGSRM ( 245 )	
DPSMP_W	LOK	BGRLP ( 266 )	
DPUS_W	AUS	AES ( 973 )	
DPWRSVC	LOK	ADVE ( 918 )	
DRKUKEL	LOK	ESUK ( 699 )	
DRKUKEL_W	LOK	ESUK ( 699 )	
DRKWTMP_W	LOK	KHMD ( 894 )	
DRLAS_W	AUS	BGRLG ( 274 )	
DRLFUE_W	AUS	FUEREG ( 595 )	FUEDK ( 597 ), FE ( 591 )
DRLKRDY	LOK	KRDY ( 659 )	
DRLLAD_W	LOK	BGMSZS ( 239 )	
DRLM_W	LOK	FUEREG ( 595 )	
DRLP	AUS	BGRLP ( 266 )	
DRLP_W	AUS	BGRLP ( 266 )	ESUK ( 699 ), KRDY ( 659 )
DRLSOLF_W	AUS	MDFUE ( 594 )	
DRLSOLMF_W	LOK	FUEDK ( 597 )	
DRLSOL_W	AUS	MDFUE ( 594 )	
DRLSP	LOK	ESUKA ( 711 )	
DRLSP2	LOK	ESUKA ( 711 )	
DRL_W	AUS	BGSRM ( 245 )	SWADAP ( 47 ), BGRLP ( 266 ), KRDY ( 659 ), EGFE ( 228 )
DRUCK	LOK	EGAG ( 486 )	
DSTERT20_W	LOK	TEB ( 826 )	
DTBRT_W	LOK	BGTEMPK ( 252 )	
DTSEGP_W	LOK	NLDG ( 157 )	
DTVKA	AUS	LRKA ( 795 )	LR ( 768 ), GKRA ( 766 )
DTVKA2	AUS	LRKA ( 795 )	LR ( 768 ), GKRA ( 766 )
DTVKAI	LOK	LRKA ( 795 )	
DTVKAI2	LOK	LRKA ( 795 )	
DUB	LOK	BGLBZ ( 489 )	
DUF_C	AUS	DUF ( 1089 )	
DUMMY	LOK	AEVAB ( 980 )	
DVEADCHST	AUS	BGDVE ( 934 )	DDVE ( 950 )
DVFG_R	LOK	FGREGL ( 1174 )	



Symbol	Type	Created within	Used within
DVIVR_W	LOK	FGRREGL (1174)	
DVPRAE_W	LOK	VMAXMD (588)	
DVSI_W	LOK	VMAXMD (588)	
DVZL_W	LOK	FGRFULO (1160)	
DVZVL_W	LOK	FGRREGL (1174)	
DWDKBA_W	AUS	GGDVE (477)	
DWDKDLR_W	LOK	ADVE (918)	
DWDKSUMX_W	LOK	FUEDK (597)	
DWDKSUS_W	LOK	FUEDK (597)	
DWDKSUT_W	LOK	FUEDK (597)	
DWDKS_KGE	LOK	ADVE (918)	
DWDKS_W	AUS	FE (591)	FUEDKSA (610), ADVE (918)
DWFK_W	LOK	ESUK (699)	
DWFL_W	LOK	ESUK (699)	
DWF_W	AUS	ESUK (699)	
DWKR	AUS	EGKE (409)	KRRA (639)
DWKRMSW	LOK	KRRA (639)	
DWKRZ	AUS	KRRA (639)	ZUE (627)
DWNWSP2_W	AUS	DNWKW (134)	
DWNWSP_W	AUS	DNWKW (134)	
DWPED	AUS	GGPED (454)	KOS (896)
DWPED_W	AUS	EGEG (453)	GGPED (454)
DYESOFV	LOK	KRDY (659)	
DYESV	LOK	KRDY (659)	
DYNLSU2_W	EIN		DLSSA (350)
DYNLSUSA	AUS	DLSSA (350)	
DYNLSUSA2	AUS	DLSSA (350)	
DYNLSU_W	EIN		DLSSA (350)
DZWDYNT	LOK	ZWMIN (669)	
DZWG	LOK	LAMBTS (732)	
DZWI	LOK	MDIST (528)	
DZWKG	LOK	ZWGRU (634)	
DZWMNA	LOK	ZWMIN (669)	
DZWOAG	AUS	MDBAS (529)	ZWGRU (634), ZWMIN (669)
DZWOL	AUS	MDBAS (529)	ZWGRU (634)
DZWOTM	LOK	MDBAS (529)	
DZWS	LOK	MDZW (636)	
DZWSPA	LOK	ZWMIN (669)	
DZWWL	AUS	ZWWL (638)	ZUE (627)
DZW_UM	LOK	UFMIST (1086)	
EDGE_CTR	LOK	GGDPG (74)	
EEVMNC	EIN		DMDMIL (216)
EEVX	AUS	AEVAB (980)	
EGASPFAD	AUS	DUF (1089)	DFFT (1140)
EIADCC_UM	AUS	URADCC (1049)	DUF (1089)
EIIPA_UM	AUS	UFRLC (1066)	DUF (1089)
EIMSRC_UM	AUS	UFMSRC (1080)	
EIMVER_UM	AUS	UFMVER (1087)	DUF (1089)
EI_NC_UM	AUS	UFNC (1063)	DUF (1089)
EI_REAC_UM	AUS	UFREAC (1088)	DUF (1089)
EI_RLC_UM	AUS	UFRLC (1066)	DUF (1089)
EI_RLIP_UM	AUS	UFRLC (1066)	DUF (1089)
EISGSC_UM	AUS	UFSGSC (1070)	
EIS_PSC_UM	AUS	UFSPSC (1060)	DUF (1089)
EIUBR_UM	EIN		DUF (1089)
EIZWC_UM	AUS	UFZWC (1075)	DUF (1089)
EKPFZ	LOK	DEKPE (1020)	
EKPPZ	LOK	DEKPE (1020)	
ETALAB	AUS	MDBAS (529)	FE (591), MDFUE (594)
ETATE	AUS	TEB (826)	
ETATEINT	LOK	TEB (826)	
ETATESOL	LOK	TEB (826)	
ETATRMN	AUS	MDBAS (529)	
ETAZAIST	AUS	MDIST (528)	MSF (506), MDZW (636)
ETAZWB	AUS	MDBAS (529)	MDKOG (516)
ETAZWBM	AUS	MDBAS (529)	FE (591), MDFUE (594), MDKOL (526), MSF (506), MDZUL (523)
ETAZWG	LOK	LAMBTS (732)	
ETAZWIF	LOK	DTEV (856)	
ETAZWIM	LOK	LAMBTS (732)	
ETAZWIMT	LOK	ATM (20)	
ETAZWIST	AUS	MDIST (528)	ATM (20), DTEV (856), LAMBTS (732)
ETAZWKTE	LOK	DTEV (856)	
ETAZWMN	AUS	ZWMIN (669)	AES (973), MDKOL (526), MDZUL (523), MDRED (976)
ETAZWMN_W	LOK	AES (973)	
ETAZWS	LOK	MDZW (636)	
ETAZW_UM	LOK	UFMIST (1086)	
EVRBGN_ONE	LOK	AEVAB (980)	
EVSUP1	AUS	DIMC (1148)	
EVTMOD	AUS	BGTEMPK (252)	FUEDK (597), EGFE (228)
EVZ_AGS	LOK	AES (973)	
EVZ_AUS	AUS	AEVAB (980)	AEVABZK (1003), KRRA (639), UFUE (1056), AES (973)
EVZ_AUSOLD	LOK	BGEVAB (1005)	



Symbol	Type	Created within	Used within
EVZ_AUSTOT	AUS	AEVABZK (1003)	ACIFI (1013), UFEING (1058), DEVE (1017), BGEVAB (1005), AES ( 973 )
EVZ_AUS_JUM	AUS	UFEING (1058)	UFREAC (1088), UFUE (1056)
E_AAIVE	EIN		DTEV ( 856 ), TEBEB ( 762 )
E_AGRE	EIN		DKAT ( 361 ), LRAEB ( 759 ), DLSA ( 398 ), DMDSTP ( 205 ), DTEV ( 856 ), DLSAHK ( 339 )
E_AGRF	EIN		DIMC (1148), LRAEB ( 759 ), DTEV ( 856 ), DMDSTP ( 205 ), DLSAHK ( 339 ), DLSA ( 398 ), DKAT ( 361 )
E_BM	AUS	DDG ( 141 )	DMDSTP ( 205 ), WANWKW ( 125 ), RDE ( 112 ), LRAEB ( 759 ), DNWS ( 622 ), GGDPG ( 74 )
E_BREMS	AUS	EGEG ( 453 )	GGEGAS ( 474 )
E_BUOF	AUS	CAN (1124)	NMAXMD ( 584 )
E_BUSOFF	AUS	CAN (1124)	DCAS (1128), DCKUP (1128), DCINS (1126)
E_BWF	AUS	GGPED ( 454 )	
E_CAS	AUS	DCAS (1128)	CAN (1124), DVFZ ( 500 )
E_CINS	AUS	DCINS (1126)	
E_CKUP	EIN		CAN (1124), DCKUP (1128), NMAXMD ( 584 )
E_DK	AUS	DDVE ( 950 )	BGMSZS ( 239 ), TEBEB ( 762 ), SU ( 617 ), LRAEB ( 759 ), EGFE ( 228 ), DTEV ( 856 ), DKAT ( 361 ), BGPU ( 276 ), BGRLP ( 266 )
E_DK1P	AUS	DDVE ( 950 )	
E_DK2P	AUS	DDVE ( 950 )	
E_DPL	EIN		LRA ( 797 )
E_DSL	EIN		BGMSZS ( 239 )
E_DSLI	LOK	BGMSZS ( 239 )	
E_DSS	EIN		BGPU ( 276 ), EGFE ( 228 )
E_DST	AUS	EGAG ( 486 )	
E_DVEE	AUS	DDVE ( 950 )	
E_DVEF	AUS	DDVE ( 950 )	BGDVE ( 934 )
E_DVEFO	AUS	DDVE ( 950 )	BGDVE ( 934 )
E_DVEL	AUS	DDVE ( 950 )	
E_DVEN	AUS	DDVE ( 950 )	BGDVE ( 934 )
E_DVER	AUS	DDVE ( 950 )	
E_DVET	AUS	DDVE ( 950 )	ADVE ( 918 )
E_DVEU	AUS	DDVE ( 950 )	DTEV ( 856 ), LRAEB ( 759 )
E_DVEUB	AUS	DDVE ( 950 )	
E_DVEUW	AUS	DDVE ( 950 )	
E_DVEV	AUS	DDVE ( 950 )	BGDVE ( 934 ), GGDVE ( 477 )
E_EGFE	AUS	DEGFE ( 592 )	BGPU ( 276 )
E_EV	EIN		DMDMIL ( 216 )
E_EV1	AUS	DEVE (1017)	AEVAB ( 980 ), DMDMIL ( 216 ), STADAP ( 684 )
E_EV2	AUS	DEVE (1017)	AEVAB ( 980 ), STADAP ( 684 ), DMDMIL ( 216 )
E_EV3	AUS	DEVE (1017)	AEVAB ( 980 ), DMDMIL ( 216 ), STADAP ( 684 )
E_EV4	AUS	DEVE (1017)	AEVAB ( 980 ), DMDMIL ( 216 ), STADAP ( 684 )
E_EV5	AUS	DEVE (1017)	AEVAB ( 980 ), DMDMIL ( 216 ), STADAP ( 684 )
E_EV6	AUS	DEVE (1017)	AEVAB ( 980 ), STADAP ( 684 ), DMDMIL ( 216 )
E_EV7	AUS	DEVE (1017)	AEVAB ( 980 ), STADAP ( 684 ), DMDMIL ( 216 )
E_EV8	AUS	DEVE (1017)	AEVAB ( 980 ), STADAP ( 684 ), DMDMIL ( 216 )
E_FP1P	AUS	GGPED ( 454 )	
E_FP2P	AUS	GGPED ( 454 )	
E_FPP	AUS	EGEG ( 453 )	GGPED ( 454 )
E_FRA	AUS	GKRA ( 766 )	
E_FRA2	AUS	GKRA ( 766 )	
E_FRAO	AUS	DKVS ( 811 )	STADAP ( 684 )
E_FRAO2	AUS	DKVS ( 811 )	STADAP ( 684 )
E_FRAU	AUS	DKVS ( 811 )	STADAP ( 684 )
E_FRAU2	AUS	DKVS ( 811 )	STADAP ( 684 )
E_FRST	AUS	DKVS ( 811 )	
E_FRST2	AUS	DKVS ( 811 )	
E_HKSJ	LOK	DKRS ( 437 )	
E_HLPKS_J	LOK	DKRS ( 437 )	
E_HSH	AUS	DHLSHK (1154)	DIMC (1148), DKAT ( 361 ), DLSA ( 398 ), LRHK ( 781 ), DLSAHK ( 339 )
E_HSH2	AUS	DHLSHK (1154)	DIMC (1148), LRHK ( 781 ), DLSAHK ( 339 ), DLSA ( 398 ), DKAT ( 361 )
E_HSV	AUS	DHLSVK ( 29 )	DIMC (1148), LRHK ( 781 ), DLSA ( 398 ), DKAT ( 361 )
E_HSV2	AUS	DHLSVK ( 29 )	DIMC (1148), LRHK ( 781 ), DLSA ( 398 ), DKAT ( 361 )
E_HSVE	AUS	DHLSVKE ( 902 )	DHLSVK ( 29 )
E_HSVE2	AUS	DHLSVKE ( 902 )	DHLSVK ( 29 )
E_KAT	AUS	DKAT ( 361 )	DIMC (1148), LRHK ( 781 ), DLSA ( 398 )
E_KAT2	AUS	DKAT ( 361 )	DIMC (1148), LRHK ( 781 ), DLSA ( 398 )
E_KOSE	AUS	DKOSE ( 901 )	
E_KPPE	AUS	DEKPE (1020)	
E_KRNT	AUS	DKRNT ( 445 )	KRRA ( 639 ), EGKE ( 409 )
E_KROF	AUS	DKRNT ( 445 )	KRRA ( 639 ), EGKE ( 409 )
E_KRTP	AUS	DKRTP ( 451 )	KRRA ( 639 ), EGKE ( 409 )
E_KS1	AUS	DKRS ( 437 )	KRRA ( 639 ), EGKE ( 409 )
E_KS1H	LOK	KRRA ( 639 )	
E_KS2	AUS	DKRS ( 437 )	KRRA ( 639 ), EGKE ( 409 )
E_KS2H	LOK	KRRA ( 639 )	
E_KS3	AUS	DKRS ( 437 )	KRRA ( 639 ), EGKE ( 409 )
E_KS3H	LOK	KRRA ( 639 )	
E_KS4	AUS	DKRS ( 437 )	KRRA ( 639 ), EGKE ( 409 )
E_KS4H	LOK	KRRA ( 639 )	
E_LASH	AUS	DLSAHK ( 339 )	DKAT ( 361 ), LRHK ( 781 )
E_LASH2	AUS	DLSAHK ( 339 )	DKAT ( 361 ), LRHK ( 781 )



Symbol	Type	Created within	Used within
E_LATP	AUS	DLSA ( 398 )	DIMC ( 1148 ), DKAT ( 361 )
E_LATP2	AUS	DLSA ( 398 )	DIMC ( 1148 ), DKAT ( 361 )
E_LATV	AUS	DLSA ( 398 )	DKAT ( 361 )
E_LATV2	AUS	DLSA ( 398 )	DKAT ( 361 )
E_LDE	EIN		DMDSTP ( 205 )
E_LDPE	EIN		DTEV ( 856 ), TEBEB ( 762 )
E_LLR	AUS	DLLR ( 578 )	DTEV ( 856 )
E_LLM	AUS	DHFM ( 233 )	SWADAP ( 47 ), EGFE ( 228 ), BBKHZ ( 890 ), BGTEV ( 257 ), BGM-SZS ( 239 ), LRHK ( 781 ), FUEREG ( 595 ), DTEV ( 856 ), DLSA ( 398 ), DLLR ( 578 ), DKAT ( 361 ), BGPU ( 276 )
E_LSH	AUS	DLSH ( 330 )	DIMC ( 1148 ), DKAT ( 361 ), DLSAHK ( 339 )
E_LSH2	AUS	DLSH ( 330 )	DIMC ( 1148 ), DLSAHK ( 339 ), DKAT ( 361 )
E_LSHV	EIN		DKAT ( 361 )
E_LSV	AUS	DLSV ( 301 )	DIMC ( 1148 ), LREB ( 739 ), TEB ( 826 ), DKAT ( 361 )
E_LSV2	AUS	DLSV ( 301 )	DIMC ( 1148 ), DKAT ( 361 ), TEB ( 826 ), LREB ( 739 )
E_LUEA	AUS	DMLSE ( 34 )	
E_LUEB	AUS	DMLSE ( 34 )	
E_MD	AUS	DMDMIL ( 216 )	DKAT ( 361 ), DMDSTP ( 205 )
E_MD00	AUS	DMDMIL ( 216 )	
E_MD01	AUS	DMDMIL ( 216 )	
E_MD02	AUS	DMDMIL ( 216 )	
E_MD03	AUS	DMDMIL ( 216 )	
E_MD04	AUS	DMDMIL ( 216 )	
E_MD05	AUS	DMDMIL ( 216 )	
E_MD06	AUS	DMDMIL ( 216 )	
E_MD07	AUS	DMDMIL ( 216 )	
E_MD08	AUS	DMDMIL ( 216 )	
E_MD09	AUS	DMDMIL ( 216 )	
E_MD10	AUS	DMDMIL ( 216 )	
E_MD11	AUS	DMDMIL ( 216 )	
E_MDB	AUS	MDKOG ( 516 )	
E_MILE	AUS	DMILE ( 36 )	
E_MUTE	AUS	CAN ( 1124 )	NMAXMD ( 584 )
E_N	AUS	DDG ( 141 )	DMDSTP ( 205 ), RDE ( 112 ), STADAP ( 684 ), GGDPG ( 74 )
E_NWKW	AUS	DNWKW ( 134 )	DMDSTP ( 205 )
E_NWKW2	AUS	DNWKW ( 134 )	DMDSTP ( 205 )
E_NWS	AUS	DNWS ( 622 )	DMDSTP ( 205 )
E_NWS2	AUS	DNWS ( 622 )	DMDSTP ( 205 )
E_NWSE	AUS	DNWSE ( 1025 )	DMDSTP ( 205 ), WANWKW ( 125 ), DNWS ( 622 )
E_NWSE2	EIN		DMDSTP ( 205 )
E_NWSE_C	EIN		DNWSE ( 1025 )
E_PH	AUS	DPH ( 144 )	DLSA ( 398 ), NWS ( 618 ), WANWKW ( 125 ), STADAP ( 684 ), DLSAHK ( 339 ), NLPH ( 150 )
E_PH2	AUS	DPH ( 144 )	NWS ( 618 ), WANWKW ( 125 )
E_POEL	AUS	GGPOEL ( 296 )	
E_PUA	AUS	BGPU ( 276 )	
E_RKAT	AUS	DKVS ( 811 )	STADAP ( 684 )
E_RKAT2	AUS	DKVS ( 811 )	STADAP ( 684 )
E_RKAZ	AUS	DKVS ( 811 )	
E_RKAZ2	AUS	DKVS ( 811 )	
E_SGCAN	EIN		GGDPG ( 74 )
E_SLPE	EIN		DKAT ( 361 )
E_SLS	EIN		DIMC ( 1148 ), LRHK ( 781 ), DTEV ( 856 )
E_SLS2	EIN		LRHK ( 781 )
E_SLVE	EIN		DKAT ( 361 )
E_SUE	EIN		DMDSTP ( 205 )
E_SUE2	EIN		DMDSTP ( 205 )
E_SWE	EIN		DSWEC ( 32 )
E_TA	AUS	GGTFA ( 298 )	ATM ( 20 ), BBKHZ ( 890 ), SU ( 617 ), NWS ( 618 ), LRAEB ( 759 ), LL-RNS ( 562 ), GGTFM ( 289 ), DLSA ( 398 ), DLLR ( 578 ), BGTABST ( 1030 )
E_TANKL	EIN		STADAP ( 684 )
E_TES	AUS	DTEV ( 856 )	DIMC ( 1148 ), DLSH ( 330 ), DMDSTP ( 205 ), LRHK ( 781 ), LRAEB ( 759 ), LR ( 768 ), ESUKA ( 711 ), DLSV ( 301 ), DLSAHK ( 339 ), DKAT ( 361 ), DLLR ( 578 ), DLSA ( 398 )
E_TEVE	AUS	DTEVE ( 1022 )	DKAT ( 361 ), TEBEB ( 762 ), LRHK ( 781 ), LRAEB ( 759 ), ESUKA ( 711 ), DTEV ( 856 ), DMDSTP ( 205 ), DLSV ( 301 ), DLSH ( 330 ), DLSAHK ( 339 ), DLLR ( 578 ), DLSA ( 398 )
E_TEVE2	EIN		LRHK ( 781 )
E_TM	AUS	GGTFM ( 289 )	ATWAL ( 297 ), WANWKW ( 125 ), SU ( 617 ), STADAP ( 684 ), LRAEB ( 759 ), LLRNS ( 562 ), LFS ( 69 ), DTEV ( 856 ), DNWS ( 622 ), DLSV ( 301 ), DLSH ( 330 ), DLSA ( 398 ), DLLR ( 578 ), BBKHZ ( 890 ), BGTABST ( 1030 )
E_TOL	EIN		GGTFM ( 289 )
E_TUM	EIN		ATM ( 20 ), BGTABST ( 1030 )
E_UB	AUS	EGAG ( 486 )	GGUB ( 487 ), DLSA ( 398 ), STADAP ( 684 ), LRAEB ( 759 ), DLSAHK ( 339 ), DTEV ( 856 )
E_JF2SG	AUS	DUF ( 1089 )	
E_JFMV	AUS	DUF ( 1089 )	
E_JFSKA	AUS	DUF ( 1089 )	
E_JRRAM	AUS	DUR ( 1052 )	
E_JRRROM	AUS	DUR ( 1052 )	
E_JRRST	AUS	DUR ( 1052 )	
E_UVSE	EIN		DMDSTP ( 205 )



Symbol	Type	Created within	Used within
E_VFZ	AUS	DVFZ ( 500 )	EGAG ( 486 ), BBGANG ( 501 ), RDE ( 112 ), NMAXMD ( 584 ), GGVFZG ( 497 ), GGUB ( 487 ), GGPED ( 454 ), DVKUP ( 1027 ), DTEV ( 856 ), DMDSTP ( 205 ), DMDLU ( 193 ), DDG ( 141 ), DLLR ( 578 ), BGPU ( 276 )
E_VKUP	LOK	DVKUP ( 1027 )	
FAFTEKF	LOK	BGTEV ( 257 )	
FAFTE_W	LOK	BGTEV ( 257 )	
FALRDKT	AUS	DKAT ( 361 )	LR ( 768 )
FAMAL	LOK	DMDLU ( 193 )	
FAVKATMX	LOK	LRKA ( 795 )	
FAWIFGR	EIN		FGRFULO ( 1160 ), FGRREGL ( 1174 )
FAWIFGR_W	LOK	FGRREGL ( 1174 )	
FBAKL_W	AUS	ESUK ( 699 )	
FBANS	LOK	ESUK ( 699 )	
FBANS_W	LOK	ESUK ( 699 )	
FBAVST_W	LOK	ESUK ( 699 )	
FBETATE	LOK	TEB ( 826 )	
FBKATE	LOK	TEB ( 826 )	
FDAR	AUS	ARMD ( 531 )	
FDMD_M	LOK	DMDFON ( 161 )	DMDUE ( 158 )
FFLUTN	LOK	DMDLUA ( 202 )	
FFONN1	LOK	DMDFON ( 161 )	
FFONN2	LOK	DMDFON ( 161 )	
FFONN3	LOK	DMDFON ( 161 )	
FFORN1	LOK	DMDFON ( 161 )	
FFPL1	LOK	DMDFON ( 161 )	
FFRI	LOK	LR ( 768 )	
FFRI2	LOK	LR ( 768 )	
FFRIP_W	LOK	LR ( 768 )	
FFZDFP	EIN		TC2MOD ( 1107 )
FGRU	AUS	ESGRU ( 678 )	ESVST ( 677 ), GK ( 675 )
FGWRTE	LOK	TEB ( 826 )	
FHO	AUS	BGPU ( 276 )	DLLR ( 578 ), WDKSOM ( 614 ), STADAP ( 684 ), MDVER ( 546 ), MD-FUE ( 594 ), KOS ( 896 ), ESUK ( 699 ), ESSTT ( 679 ), ESNSWL ( 691 )
FHODSS_W	LOK	BGPU ( 276 )	
FHOMS_W	LOK	BGPU ( 276 )	
FHO_W	AUS	BGPU ( 276 )	BBKHZ ( 890 ), MDMAX ( 514 ), KHMD ( 894 ), FUEDK ( 597 ), FE ( 591 ), DTEV ( 856 ), DHFM ( 233 ), BGTEV ( 257 ), BGSRM ( 245 ), EGFE ( 228 )
FIVZABG	LOK	DMDMIL ( 216 )	
FKATEAPP	LOK	TEB ( 826 )	
FKATEFRG	LOK	TEB ( 826 )	
FKATEI	AUS	TEB ( 826 )	DTEV ( 856 ), LR ( 768 )
FKATES	AUS	TEB ( 826 )	
FKHAB	AUS	BBKHZ ( 890 )	
FKHFM	LOK	GGHFM ( 230 )	
FKLAFS_W	LOK	FUEDK ( 597 )	
FKLAF_W	AUS	BGMSZS ( 239 )	DTEV ( 856 )
FKMSDKK_W	LOK	BGPU ( 276 )	
FKMSDKS_W	AUS	BGMSZS ( 239 )	
FKMSDK_W	AUS	BGMSZS ( 239 )	BGPU ( 276 ), FUEDK ( 597 )
FKPVDK_W	AUS	BGMSZS ( 239 )	
FKTNS_W	LOK	ESNSWL ( 691 )	
FLAKH	AUS	BBKHZ ( 890 )	LAKH ( 735 ), AK ( 855 )
FLAMKH	AUS	BBKHZ ( 890 )	LAMKO ( 729 ), AK ( 855 ), LAMSOLL ( 726 )
FLAMSL	LOK	AK ( 855 )	
FLAMSL2_W	EIN		LAKH ( 735 ), LAMKO ( 729 )
FLAMSL_W	EIN		LAKH ( 735 ), LAMKO ( 729 )
FLGKAT_W	LOK	DMDMIL ( 216 )	
FLGLRS	AUS	LREB ( 739 )	DFFT ( 1140 ), TC1MOD ( 1100 )
FLGLRS2	AUS	LREB ( 739 )	DFFT ( 1140 ), TC1MOD ( 1100 )
FLGTIAB	AUS	DMDMIL ( 216 )	AES ( 973 ), AEVAB ( 980 )
FLGTIABC	EIN		AEVAB ( 980 )
FLGTIABT	AUS	DMDMIL ( 216 )	
FLG_M	LOK	DMDFON ( 161 )	DMDUE ( 158 )
FLMSSL	EIN		LAKH ( 735 ), AK ( 855 )
FLMX	LOK	DMDFON ( 161 )	
FLMXRESZ	LOK	DMDFON ( 161 )	
FLN11_02	LOK	DMDFON ( 161 )	
FLN11_03	LOK	DMDFON ( 161 )	
FLN11_04	LOK	DMDFON ( 161 )	
FLN11_05	LOK	DMDFON ( 161 )	
FLN11_06	LOK	DMDFON ( 161 )	
FLN11_07	LOK	DMDFON ( 161 )	
FLN11_08	LOK	DMDFON ( 161 )	
FLN11_09	LOK	DMDFON ( 161 )	
FLN11_10	LOK	DMDFON ( 161 )	
FLN11_11	LOK	DMDFON ( 161 )	
FLN11_12	LOK	DMDFON ( 161 )	
FLN12_02	LOK	DMDFON ( 161 )	
FLN12_03	LOK	DMDFON ( 161 )	
FLN12_04	LOK	DMDFON ( 161 )	
FLN12_05	LOK	DMDFON ( 161 )	
FLN12_06	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLN12_07	LOK	DMDFON ( 161 )	
FLN12_08	LOK	DMDFON ( 161 )	
FLN12_09	LOK	DMDFON ( 161 )	
FLN12_10	LOK	DMDFON ( 161 )	
FLN12_11	LOK	DMDFON ( 161 )	
FLN12_12	LOK	DMDFON ( 161 )	
FLN13_02	LOK	DMDFON ( 161 )	
FLN13_03	LOK	DMDFON ( 161 )	
FLN13_04	LOK	DMDFON ( 161 )	
FLN13_05	LOK	DMDFON ( 161 )	
FLN13_06	LOK	DMDFON ( 161 )	
FLN13_07	LOK	DMDFON ( 161 )	
FLN13_08	LOK	DMDFON ( 161 )	
FLN13_09	LOK	DMDFON ( 161 )	
FLN13_10	LOK	DMDFON ( 161 )	
FLN13_11	LOK	DMDFON ( 161 )	
FLN13_12	LOK	DMDFON ( 161 )	
FLN21_02	LOK	DMDFON ( 161 )	
FLN21_03	LOK	DMDFON ( 161 )	
FLN21_04	LOK	DMDFON ( 161 )	
FLN21_05	LOK	DMDFON ( 161 )	
FLN21_06	LOK	DMDFON ( 161 )	
FLN21_07	LOK	DMDFON ( 161 )	
FLN21_08	LOK	DMDFON ( 161 )	
FLN21_09	LOK	DMDFON ( 161 )	
FLN21_10	LOK	DMDFON ( 161 )	
FLN21_11	LOK	DMDFON ( 161 )	
FLN21_12	LOK	DMDFON ( 161 )	
FLN22_02	LOK	DMDFON ( 161 )	
FLN22_03	LOK	DMDFON ( 161 )	
FLN22_04	LOK	DMDFON ( 161 )	
FLN22_05	LOK	DMDFON ( 161 )	
FLN22_06	LOK	DMDFON ( 161 )	
FLN22_07	LOK	DMDFON ( 161 )	
FLN22_08	LOK	DMDFON ( 161 )	
FLN22_09	LOK	DMDFON ( 161 )	
FLN22_10	LOK	DMDFON ( 161 )	
FLN22_11	LOK	DMDFON ( 161 )	
FLN22_12	LOK	DMDFON ( 161 )	
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FLN23_03	LOK	DMDFON ( 161 )	
FLN23_04	LOK	DMDFON ( 161 )	
FLN23_05	LOK	DMDFON ( 161 )	
FLN23_06	LOK	DMDFON ( 161 )	
FLN23_07	LOK	DMDFON ( 161 )	
FLN23_08	LOK	DMDFON ( 161 )	
FLN23_09	LOK	DMDFON ( 161 )	
FLN23_10	LOK	DMDFON ( 161 )	
FLN23_11	LOK	DMDFON ( 161 )	
FLN23_12	LOK	DMDFON ( 161 )	
FLN31_02	LOK	DMDFON ( 161 )	
FLN31_03	LOK	DMDFON ( 161 )	
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FLN31_05	LOK	DMDFON ( 161 )	
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FLN31_08	LOK	DMDFON ( 161 )	
FLN31_09	LOK	DMDFON ( 161 )	
FLN31_10	LOK	DMDFON ( 161 )	
FLN31_11	LOK	DMDFON ( 161 )	
FLN31_12	LOK	DMDFON ( 161 )	
FLN32_02	LOK	DMDFON ( 161 )	
FLN32_03	LOK	DMDFON ( 161 )	
FLN32_04	LOK	DMDFON ( 161 )	
FLN32_05	LOK	DMDFON ( 161 )	
FLN32_06	LOK	DMDFON ( 161 )	
FLN32_07	LOK	DMDFON ( 161 )	
FLN32_08	LOK	DMDFON ( 161 )	
FLN32_09	LOK	DMDFON ( 161 )	
FLN32_10	LOK	DMDFON ( 161 )	
FLN32_11	LOK	DMDFON ( 161 )	
FLN32_12	LOK	DMDFON ( 161 )	
FLN33_02	LOK	DMDFON ( 161 )	
FLN33_03	LOK	DMDFON ( 161 )	
FLN33_04	LOK	DMDFON ( 161 )	
FLN33_05	LOK	DMDFON ( 161 )	
FLN33_06	LOK	DMDFON ( 161 )	
FLN33_07	LOK	DMDFON ( 161 )	
FLN33_08	LOK	DMDFON ( 161 )	
FLN33_09	LOK	DMDFON ( 161 )	
FLN33_10	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLN33_11	LOK	DMDFON ( 161 )	
FLN33_12	LOK	DMDFON ( 161 )	
FLN41_02	LOK	DMDFON ( 161 )	
FLN41_03	LOK	DMDFON ( 161 )	
FLN41_04	LOK	DMDFON ( 161 )	
FLN41_05	LOK	DMDFON ( 161 )	
FLN41_06	LOK	DMDFON ( 161 )	
FLN41_07	LOK	DMDFON ( 161 )	
FLN41_08	LOK	DMDFON ( 161 )	
FLN41_09	LOK	DMDFON ( 161 )	
FLN41_10	LOK	DMDFON ( 161 )	
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FLN41_12	LOK	DMDFON ( 161 )	
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FLN42_03	LOK	DMDFON ( 161 )	
FLN42_04	LOK	DMDFON ( 161 )	
FLN42_05	LOK	DMDFON ( 161 )	
FLN42_06	LOK	DMDFON ( 161 )	
FLN42_07	LOK	DMDFON ( 161 )	
FLN42_08	LOK	DMDFON ( 161 )	
FLN42_09	LOK	DMDFON ( 161 )	
FLN42_10	LOK	DMDFON ( 161 )	
FLN42_11	LOK	DMDFON ( 161 )	
FLN42_12	LOK	DMDFON ( 161 )	
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FLN43_03	LOK	DMDFON ( 161 )	
FLN43_04	LOK	DMDFON ( 161 )	
FLN43_05	LOK	DMDFON ( 161 )	
FLN43_06	LOK	DMDFON ( 161 )	
FLN43_07	LOK	DMDFON ( 161 )	
FLN43_08	LOK	DMDFON ( 161 )	
FLN43_09	LOK	DMDFON ( 161 )	
FLN43_10	LOK	DMDFON ( 161 )	
FLN43_11	LOK	DMDFON ( 161 )	
FLN43_12	LOK	DMDFON ( 161 )	
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FLN51_03	LOK	DMDFON ( 161 )	
FLN51_04	LOK	DMDFON ( 161 )	
FLN51_05	LOK	DMDFON ( 161 )	
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FLN51_07	LOK	DMDFON ( 161 )	
FLN51_08	LOK	DMDFON ( 161 )	
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FLN51_12	LOK	DMDFON ( 161 )	
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FLN52_03	LOK	DMDFON ( 161 )	
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FLN52_12	LOK	DMDFON ( 161 )	
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FLN53_09	LOK	DMDFON ( 161 )	
FLN53_10	LOK	DMDFON ( 161 )	
FLN53_11	LOK	DMDFON ( 161 )	
FLN53_12	LOK	DMDFON ( 161 )	
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FLN61_03	LOK	DMDFON ( 161 )	
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FLN61_06	LOK	DMDFON ( 161 )	
FLN61_07	LOK	DMDFON ( 161 )	
FLN61_08	LOK	DMDFON ( 161 )	
FLN61_09	LOK	DMDFON ( 161 )	
FLN61_10	LOK	DMDFON ( 161 )	
FLN61_11	LOK	DMDFON ( 161 )	
FLN61_12	LOK	DMDFON ( 161 )	
FLN62_02	LOK	DMDFON ( 161 )	
FLN62_03	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLN62_04	LOK	DMDFON ( 161 )	
FLN62_05	LOK	DMDFON ( 161 )	
FLN62_06	LOK	DMDFON ( 161 )	
FLN62_07	LOK	DMDFON ( 161 )	
FLN62_08	LOK	DMDFON ( 161 )	
FLN62_09	LOK	DMDFON ( 161 )	
FLN62_10	LOK	DMDFON ( 161 )	
FLN62_11	LOK	DMDFON ( 161 )	
FLN62_12	LOK	DMDFON ( 161 )	
FLN63_02	LOK	DMDFON ( 161 )	
FLN63_03	LOK	DMDFON ( 161 )	
FLN63_04	LOK	DMDFON ( 161 )	
FLN63_05	LOK	DMDFON ( 161 )	
FLN63_06	LOK	DMDFON ( 161 )	
FLN63_07	LOK	DMDFON ( 161 )	
FLN63_08	LOK	DMDFON ( 161 )	
FLN63_09	LOK	DMDFON ( 161 )	
FLN63_10	LOK	DMDFON ( 161 )	
FLN63_11	LOK	DMDFON ( 161 )	
FLN63_12	LOK	DMDFON ( 161 )	
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FLN71_03	LOK	DMDFON ( 161 )	
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FLN71_06	LOK	DMDFON ( 161 )	
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FLN82_07	LOK	DMDFON ( 161 )	
FLN82_08	LOK	DMDFON ( 161 )	
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FLN82_11	LOK	DMDFON ( 161 )	
FLN82_12	LOK	DMDFON ( 161 )	
FLN83_02	LOK	DMDFON ( 161 )	
FLN83_03	LOK	DMDFON ( 161 )	
FLN83_04	LOK	DMDFON ( 161 )	
FLN83_05	LOK	DMDFON ( 161 )	
FLN83_06	LOK	DMDFON ( 161 )	
FLN83_07	LOK	DMDFON ( 161 )	





Symbol	Type	Created within	Used within
FLN83_08	LOK	DMDFON ( 161 )	
FLN83_09	LOK	DMDFON ( 161 )	
FLN83_10	LOK	DMDFON ( 161 )	
FLN83_11	LOK	DMDFON ( 161 )	
FLN83_12	LOK	DMDFON ( 161 )	
FLP11_02	LOK	DMDFON ( 161 )	
FLP11_03	LOK	DMDFON ( 161 )	
FLP11_04	LOK	DMDFON ( 161 )	
FLP11_05	LOK	DMDFON ( 161 )	
FLP11_06	LOK	DMDFON ( 161 )	
FLP11_07	LOK	DMDFON ( 161 )	
FLP11_08	LOK	DMDFON ( 161 )	
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FLP11_12	LOK	DMDFON ( 161 )	
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FLP12_06	LOK	DMDFON ( 161 )	
FLP12_07	LOK	DMDFON ( 161 )	
FLP12_08	LOK	DMDFON ( 161 )	
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FLP12_12	LOK	DMDFON ( 161 )	
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FLP13_04	LOK	DMDFON ( 161 )	
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FLP13_07	LOK	DMDFON ( 161 )	
FLP13_08	LOK	DMDFON ( 161 )	
FLP13_09	LOK	DMDFON ( 161 )	
FLP13_10	LOK	DMDFON ( 161 )	
FLP13_11	LOK	DMDFON ( 161 )	
FLP13_12	LOK	DMDFON ( 161 )	
FLP21_02	LOK	DMDFON ( 161 )	
FLP21_03	LOK	DMDFON ( 161 )	
FLP21_04	LOK	DMDFON ( 161 )	
FLP21_05	LOK	DMDFON ( 161 )	
FLP21_06	LOK	DMDFON ( 161 )	
FLP21_07	LOK	DMDFON ( 161 )	
FLP21_08	LOK	DMDFON ( 161 )	
FLP21_09	LOK	DMDFON ( 161 )	
FLP21_10	LOK	DMDFON ( 161 )	
FLP21_11	LOK	DMDFON ( 161 )	
FLP21_12	LOK	DMDFON ( 161 )	
FLP22_02	LOK	DMDFON ( 161 )	
FLP22_03	LOK	DMDFON ( 161 )	
FLP22_04	LOK	DMDFON ( 161 )	
FLP22_05	LOK	DMDFON ( 161 )	
FLP22_06	LOK	DMDFON ( 161 )	
FLP22_07	LOK	DMDFON ( 161 )	
FLP22_08	LOK	DMDFON ( 161 )	
FLP22_09	LOK	DMDFON ( 161 )	
FLP22_10	LOK	DMDFON ( 161 )	
FLP22_11	LOK	DMDFON ( 161 )	
FLP22_12	LOK	DMDFON ( 161 )	
FLP23_02	LOK	DMDFON ( 161 )	
FLP23_03	LOK	DMDFON ( 161 )	
FLP23_04	LOK	DMDFON ( 161 )	
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FLP23_06	LOK	DMDFON ( 161 )	
FLP23_07	LOK	DMDFON ( 161 )	
FLP23_08	LOK	DMDFON ( 161 )	
FLP23_09	LOK	DMDFON ( 161 )	
FLP23_10	LOK	DMDFON ( 161 )	
FLP23_11	LOK	DMDFON ( 161 )	
FLP23_12	LOK	DMDFON ( 161 )	
FLP31_02	LOK	DMDFON ( 161 )	
FLP31_03	LOK	DMDFON ( 161 )	
FLP31_04	LOK	DMDFON ( 161 )	
FLP31_05	LOK	DMDFON ( 161 )	
FLP31_06	LOK	DMDFON ( 161 )	
FLP31_07	LOK	DMDFON ( 161 )	
FLP31_08	LOK	DMDFON ( 161 )	
FLP31_09	LOK	DMDFON ( 161 )	
FLP31_10	LOK	DMDFON ( 161 )	
FLP31_11	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLP31_12	LOK	DMDFON ( 161 )	
FLP32_02	LOK	DMDFON ( 161 )	
FLP32_03	LOK	DMDFON ( 161 )	
FLP32_04	LOK	DMDFON ( 161 )	
FLP32_05	LOK	DMDFON ( 161 )	
FLP32_06	LOK	DMDFON ( 161 )	
FLP32_07	LOK	DMDFON ( 161 )	
FLP32_08	LOK	DMDFON ( 161 )	
FLP32_09	LOK	DMDFON ( 161 )	
FLP32_10	LOK	DMDFON ( 161 )	
FLP32_11	LOK	DMDFON ( 161 )	
FLP32_12	LOK	DMDFON ( 161 )	
FLP33_02	LOK	DMDFON ( 161 )	
FLP33_03	LOK	DMDFON ( 161 )	
FLP33_04	LOK	DMDFON ( 161 )	
FLP33_05	LOK	DMDFON ( 161 )	
FLP33_06	LOK	DMDFON ( 161 )	
FLP33_07	LOK	DMDFON ( 161 )	
FLP33_08	LOK	DMDFON ( 161 )	
FLP33_09	LOK	DMDFON ( 161 )	
FLP33_10	LOK	DMDFON ( 161 )	
FLP33_11	LOK	DMDFON ( 161 )	
FLP33_12	LOK	DMDFON ( 161 )	
FLP41_02	LOK	DMDFON ( 161 )	
FLP41_03	LOK	DMDFON ( 161 )	
FLP41_04	LOK	DMDFON ( 161 )	
FLP41_05	LOK	DMDFON ( 161 )	
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FLP41_07	LOK	DMDFON ( 161 )	
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FLP41_11	LOK	DMDFON ( 161 )	
FLP41_12	LOK	DMDFON ( 161 )	
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FLP42_05	LOK	DMDFON ( 161 )	
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FLP42_07	LOK	DMDFON ( 161 )	
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FLP42_11	LOK	DMDFON ( 161 )	
FLP42_12	LOK	DMDFON ( 161 )	
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FLP43_12	LOK	DMDFON ( 161 )	
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FLP51_11	LOK	DMDFON ( 161 )	
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FLP52_08	LOK	DMDFON ( 161 )	
FLP52_09	LOK	DMDFON ( 161 )	
FLP52_10	LOK	DMDFON ( 161 )	
FLP52_11	LOK	DMDFON ( 161 )	
FLP52_12	LOK	DMDFON ( 161 )	
FLP53_02	LOK	DMDFON ( 161 )	
FLP53_03	LOK	DMDFON ( 161 )	
FLP53_04	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLP53_05	LOK	DMDFON ( 161 )	
FLP53_06	LOK	DMDFON ( 161 )	
FLP53_07	LOK	DMDFON ( 161 )	
FLP53_08	LOK	DMDFON ( 161 )	
FLP53_09	LOK	DMDFON ( 161 )	
FLP53_10	LOK	DMDFON ( 161 )	
FLP53_11	LOK	DMDFON ( 161 )	
FLP53_12	LOK	DMDFON ( 161 )	
FLP61_02	LOK	DMDFON ( 161 )	
FLP61_03	LOK	DMDFON ( 161 )	
FLP61_04	LOK	DMDFON ( 161 )	
FLP61_05	LOK	DMDFON ( 161 )	
FLP61_06	LOK	DMDFON ( 161 )	
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FLP61_08	LOK	DMDFON ( 161 )	
FLP61_09	LOK	DMDFON ( 161 )	
FLP61_10	LOK	DMDFON ( 161 )	
FLP61_11	LOK	DMDFON ( 161 )	
FLP61_12	LOK	DMDFON ( 161 )	
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FLP62_03	LOK	DMDFON ( 161 )	
FLP62_04	LOK	DMDFON ( 161 )	
FLP62_05	LOK	DMDFON ( 161 )	
FLP62_06	LOK	DMDFON ( 161 )	
FLP62_07	LOK	DMDFON ( 161 )	
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FLP62_11	LOK	DMDFON ( 161 )	
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FLP63_03	LOK	DMDFON ( 161 )	
FLP63_04	LOK	DMDFON ( 161 )	
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FLP63_08	LOK	DMDFON ( 161 )	
FLP63_09	LOK	DMDFON ( 161 )	
FLP63_10	LOK	DMDFON ( 161 )	
FLP63_11	LOK	DMDFON ( 161 )	
FLP63_12	LOK	DMDFON ( 161 )	
FLP71_02	LOK	DMDFON ( 161 )	
FLP71_03	LOK	DMDFON ( 161 )	
FLP71_04	LOK	DMDFON ( 161 )	
FLP71_05	LOK	DMDFON ( 161 )	
FLP71_06	LOK	DMDFON ( 161 )	
FLP71_07	LOK	DMDFON ( 161 )	
FLP71_08	LOK	DMDFON ( 161 )	
FLP71_09	LOK	DMDFON ( 161 )	
FLP71_10	LOK	DMDFON ( 161 )	
FLP71_11	LOK	DMDFON ( 161 )	
FLP71_12	LOK	DMDFON ( 161 )	
FLP72_02	LOK	DMDFON ( 161 )	
FLP72_03	LOK	DMDFON ( 161 )	
FLP72_04	LOK	DMDFON ( 161 )	
FLP72_05	LOK	DMDFON ( 161 )	
FLP72_06	LOK	DMDFON ( 161 )	
FLP72_07	LOK	DMDFON ( 161 )	
FLP72_08	LOK	DMDFON ( 161 )	
FLP72_09	LOK	DMDFON ( 161 )	
FLP72_10	LOK	DMDFON ( 161 )	
FLP72_11	LOK	DMDFON ( 161 )	
FLP72_12	LOK	DMDFON ( 161 )	
FLP73_02	LOK	DMDFON ( 161 )	
FLP73_03	LOK	DMDFON ( 161 )	
FLP73_04	LOK	DMDFON ( 161 )	
FLP73_05	LOK	DMDFON ( 161 )	
FLP73_06	LOK	DMDFON ( 161 )	
FLP73_07	LOK	DMDFON ( 161 )	
FLP73_08	LOK	DMDFON ( 161 )	
FLP73_09	LOK	DMDFON ( 161 )	
FLP73_10	LOK	DMDFON ( 161 )	
FLP73_11	LOK	DMDFON ( 161 )	
FLP73_12	LOK	DMDFON ( 161 )	
FLP81_02	LOK	DMDFON ( 161 )	
FLP81_03	LOK	DMDFON ( 161 )	
FLP81_04	LOK	DMDFON ( 161 )	
FLP81_05	LOK	DMDFON ( 161 )	
FLP81_06	LOK	DMDFON ( 161 )	
FLP81_07	LOK	DMDFON ( 161 )	
FLP81_08	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FLP81_09	LOK	DMDFON ( 161 )	
FLP81_10	LOK	DMDFON ( 161 )	
FLP81_11	LOK	DMDFON ( 161 )	
FLP81_12	LOK	DMDFON ( 161 )	
FLP82_02	LOK	DMDFON ( 161 )	
FLP82_03	LOK	DMDFON ( 161 )	
FLP82_04	LOK	DMDFON ( 161 )	
FLP82_05	LOK	DMDFON ( 161 )	
FLP82_06	LOK	DMDFON ( 161 )	
FLP82_07	LOK	DMDFON ( 161 )	
FLP82_08	LOK	DMDFON ( 161 )	
FLP82_09	LOK	DMDFON ( 161 )	
FLP82_10	LOK	DMDFON ( 161 )	
FLP82_11	LOK	DMDFON ( 161 )	
FLP82_12	LOK	DMDFON ( 161 )	
FLP83_02	LOK	DMDFON ( 161 )	
FLP83_03	LOK	DMDFON ( 161 )	
FLP83_04	LOK	DMDFON ( 161 )	
FLP83_05	LOK	DMDFON ( 161 )	
FLP83_06	LOK	DMDFON ( 161 )	
FLP83_07	LOK	DMDFON ( 161 )	
FLP83_08	LOK	DMDFON ( 161 )	
FLP83_09	LOK	DMDFON ( 161 )	
FLP83_10	LOK	DMDFON ( 161 )	
FLP83_11	LOK	DMDFON ( 161 )	
FLP83_12	LOK	DMDFON ( 161 )	
FLRAR	AUS	ARMD ( 531 )	
FLURKH	LOK	DMDLU ( 193 )	
FLUTS1	LOK	DMDLUA ( 202 )	
FLUTS10	LOK	DMDLUA ( 202 )	
FLUTS11	LOK	DMDLUA ( 202 )	
FLUTS12	LOK	DMDLUA ( 202 )	
FLUTS2	LOK	DMDLUA ( 202 )	
FLUTS3	LOK	DMDLUA ( 202 )	
FLUTS4	LOK	DMDLUA ( 202 )	
FLUTS5	LOK	DMDLUA ( 202 )	
FLUTS6	LOK	DMDLUA ( 202 )	
FLUTS7	LOK	DMDLUA ( 202 )	
FLUTS8	LOK	DMDLUA ( 202 )	
FLUTS9	LOK	DMDLUA ( 202 )	
FLUTS_M	LOK	DMDLUA ( 202 )	
FLUTS_M2	LOK	DMDLUA ( 202 )	
FMDKH	AUS	BBKHZ ( 890 )	KHMD ( 894 ), ZWMIN ( 669 ), AK ( 855 )
FMFKRAKT	LOK	GGKS ( 412 )	
FMFKRAKTOL	LOK	GGKS ( 412 )	
FMFW	LOK	GGKS ( 412 )	
FMKHFHO_W	LOK	KHMD ( 894 )	
FMKHTM	LOK	KHMD ( 894 )	
FNGWRTE	LOK	TEB ( 826 )	
FNS	AUS	ESVST ( 677 )	
FNSTAB_W	AUS	MDNSTAB ( 556 )	MADMIN ( 538 )
FNSWLST_W	AUS	ESNSWL ( 691 )	
FNSWL_W	AUS	ESNSWL ( 691 )	GK ( 675 )
FNS_W	AUS	ESNSWL ( 691 )	
FNWUE	AUS	NWS ( 618 )	BGSRM ( 245 ), ZWGRU ( 634 ), MDBAS ( 529 )
FOSTAT	AUS	DMDFON ( 161 )	DMDDLU ( 199 ), DMDLU ( 193 )
FPAG	DOK	BGAGR ( 263 )	
FPBRKDS_W	AUS	BGSRM ( 245 )	BGRLP ( 266 ), FUEDK ( 597 )
FPRSTEP_C	AUS	BGDVE ( 934 )	DDVE ( 950 )
FPRTIM_C	LOK	BGDVE ( 934 )	
FPUK	LOK	GGHFM ( 230 )	
FPVDK	AUS	BGMSZS ( 239 )	SWADAP ( 47 ), EGFE ( 228 )
FPVDKDS	AUS	BGPU ( 276 )	GGDVE ( 477 )
FPVDKDSS_W	LOK	BGPU ( 276 )	
FPVDKDS_W	AUS	BGPU ( 276 )	BGMSZS ( 239 ), EGFE ( 228 )
FPVDKMS_W	LOK	BGPU ( 276 )	
FPVDK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 ), BGRML ( 287 )
FR	LOK	GKRA ( 766 )	
FR2_U	AUS	DFFTCNV ( 1143 )	DFFT ( 1140 )
FR2_W	AUS	GKRA ( 766 )	LR ( 768 ), DFFTCNV ( 1143 ), TC1MOD ( 1100 ), TC2MOD ( 1107 ), LREB ( 739 ), GK ( 675 ), DKAT ( 361 )
FRA	LOK	GKRA ( 766 )	
FRA2_U	AUS	DFFTCNV ( 1143 )	DFFT ( 1140 )
FRA2_W	AUS	GKRA ( 766 )	LRA ( 797 ), DFFTCNV ( 1143 ), GK ( 675 ), TC2MOD ( 1107 ), TC1MOD ( 1100 )
FRAO2_W	AUS	LRA ( 797 )	DKVS ( 811 ), GKRA ( 766 )
FRAO_W	AUS	LRA ( 797 )	DKVS ( 811 ), GKRA ( 766 )
FRAT2_W	LOK	LRA ( 797 )	
FRAT12_W	LOK	LRA ( 797 )	
FRAT1_W	LOK	LRA ( 797 )	
FRAT_W	LOK	LRA ( 797 )	
FRAU2_W	AUS	LRA ( 797 )	DKVS ( 811 ), GKRA ( 766 )
FRAUZS2_W	LOK	DKVS ( 811 )	



Symbol	Type	Created within	Used within
FRAU_ZS_W	LOK	DKVS ( 811 )	
FRAU_W	AUS	LRA ( 797 )	DKVS ( 811 ), GKRA ( 766 )
FRA_U	AUS	DFFTCNV (1143)	DFFT (1140)
FRA_W	AUS	GKRA ( 766 )	LRA ( 797 ), DFFTCNV (1143), GK ( 675 ), TC1MOD (1100), TC2MOD (1107)
FRBAND2_W	LOK	LR ( 768 )	
FRBAND_W	LOK	LR ( 768 )	
FRDTER_W	AUS	DTEV ( 856 )	LRINI ( 749 ), GKRA ( 766 )
FREGFTE	LOK	TEB ( 826 )	
FRHODKR_W	LOK	FUEDK ( 597 )	
FRHODK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 ), BGRLP ( 266 ), FUEDK ( 597 )
FRHOL_W	AUS	BGPU ( 276 )	EGFE ( 228 )
FRI	LOK	LR ( 768 )	
FRI2	LOK	LR ( 768 )	
FRIBAND2_W	LOK	LR ( 768 )	
FRIBAND_W	LOK	LR ( 768 )	
FRIINT	LOK	LR ( 768 )	
FRIINT2	LOK	LR ( 768 )	
FRINI2_W	AUS	LRINI ( 749 )	LR ( 768 )
FRINI_W	AUS	LRINI ( 749 )	LR ( 768 ), GKRA ( 766 )
FRINT2_W	LOK	LR ( 768 )	
FRINT_W	LOK	LR ( 768 )	
FRKTE	EIN		RKTI ( 979 ), AES ( 973 )
FRM	EIN		AK ( 855 )
FRM2_W	AUS	LR ( 768 )	DKVS ( 811 ), DLSAHK ( 339 ), TEB ( 826 ), LRA ( 797 ), GKRA ( 766 )
FRMA_W	LOK	LR ( 768 )	
FRMFDIF_W	LOK	DTEV ( 856 )	
FRMFREF_W	LOK	DTEV ( 856 )	
FRMI2_W	LOK	LR ( 768 )	
FRMIT	AUS	TEB ( 826 )	
FRMITF_W	LOK	DTEV ( 856 )	
FRMIT_W	AUS	TEB ( 826 )	DTEV ( 856 )
FRMI_W	LOK	LR ( 768 )	
FRMMA_W	LOK	LR ( 768 )	
FRMN2_W	AUS	LR ( 768 )	
FRMN_W	AUS	LR ( 768 )	DTEV ( 856 )
FRMSL_W	LOK	LR ( 768 )	
FRMTRIP2_W	LOK	DLSAHK ( 339 )	
FRMTRIP_W	LOK	DLSAHK ( 339 )	
FRMX2_W	AUS	LR ( 768 )	
FRMXA	LOK	TEB ( 826 )	
FRMXAF_W	LOK	DTEV ( 856 )	
FRMXA_W	AUS	TEB ( 826 )	DTEV ( 856 )
FRMX_W	AUS	LR ( 768 )	DTEV ( 856 )
FRM_W	AUS	LR ( 768 )	DKVS ( 811 ), TEB ( 826 ), LRA ( 797 ), DLSAHK ( 339 ), GKRA ( 766 )
FRP	LOK	LR ( 768 )	
FRP2	LOK	LR ( 768 )	
FRPINT	LOK	LR ( 768 )	
FRPINT2	LOK	LR ( 768 )	
FRSL_W	LOK	LR ( 768 )	
FRSP2_W	LOK	LR ( 768 )	
FRSP_W	LOK	LR ( 768 )	
FRTV	LOK	LR ( 768 )	
FRTV2	LOK	LR ( 768 )	
FR_U	AUS	DFFTCNV (1143)	DFFT (1140)
FR_W	AUS	GKRA ( 766 )	LR ( 768 ), DFFTCNV (1143), GK ( 675 ), LREB ( 739 ), TC2MOD (1107), TC1MOD (1100), DKAT ( 361 )
FS11_02	LOK	DMDFON ( 161 )	
FS11_03	LOK	DMDFON ( 161 )	
FS11_04	LOK	DMDFON ( 161 )	
FS11_05	LOK	DMDFON ( 161 )	
FS11_06	LOK	DMDFON ( 161 )	
FS11_07	LOK	DMDFON ( 161 )	
FS11_08	LOK	DMDFON ( 161 )	
FS11_09	LOK	DMDFON ( 161 )	
FS11_10	LOK	DMDFON ( 161 )	
FS11_11	LOK	DMDFON ( 161 )	
FS11_12	LOK	DMDFON ( 161 )	
FS12_02	LOK	DMDFON ( 161 )	
FS12_03	LOK	DMDFON ( 161 )	
FS12_04	LOK	DMDFON ( 161 )	
FS12_05	LOK	DMDFON ( 161 )	
FS12_06	LOK	DMDFON ( 161 )	
FS12_07	LOK	DMDFON ( 161 )	
FS12_08	LOK	DMDFON ( 161 )	
FS12_09	LOK	DMDFON ( 161 )	
FS12_10	LOK	DMDFON ( 161 )	
FS12_11	LOK	DMDFON ( 161 )	
FS12_12	LOK	DMDFON ( 161 )	
FS13_02	LOK	DMDFON ( 161 )	
FS13_03	LOK	DMDFON ( 161 )	
FS13_04	LOK	DMDFON ( 161 )	
FS13_05	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FS13_06	LOK	DMDFON ( 161 )	
FS13_07	LOK	DMDFON ( 161 )	
FS13_08	LOK	DMDFON ( 161 )	
FS13_09	LOK	DMDFON ( 161 )	
FS13_10	LOK	DMDFON ( 161 )	
FS13_11	LOK	DMDFON ( 161 )	
FS13_12	LOK	DMDFON ( 161 )	
FS21_02	LOK	DMDFON ( 161 )	
FS21_03	LOK	DMDFON ( 161 )	
FS21_04	LOK	DMDFON ( 161 )	
FS21_05	LOK	DMDFON ( 161 )	
FS21_06	LOK	DMDFON ( 161 )	
FS21_07	LOK	DMDFON ( 161 )	
FS21_08	LOK	DMDFON ( 161 )	
FS21_09	LOK	DMDFON ( 161 )	
FS21_10	LOK	DMDFON ( 161 )	
FS21_11	LOK	DMDFON ( 161 )	
FS21_12	LOK	DMDFON ( 161 )	
FS22_02	LOK	DMDFON ( 161 )	
FS22_03	LOK	DMDFON ( 161 )	
FS22_04	LOK	DMDFON ( 161 )	
FS22_05	LOK	DMDFON ( 161 )	
FS22_06	LOK	DMDFON ( 161 )	
FS22_07	LOK	DMDFON ( 161 )	
FS22_08	LOK	DMDFON ( 161 )	
FS22_09	LOK	DMDFON ( 161 )	
FS22_10	LOK	DMDFON ( 161 )	
FS22_11	LOK	DMDFON ( 161 )	
FS22_12	LOK	DMDFON ( 161 )	
FS23_02	LOK	DMDFON ( 161 )	
FS23_03	LOK	DMDFON ( 161 )	
FS23_04	LOK	DMDFON ( 161 )	
FS23_05	LOK	DMDFON ( 161 )	
FS23_06	LOK	DMDFON ( 161 )	
FS23_07	LOK	DMDFON ( 161 )	
FS23_08	LOK	DMDFON ( 161 )	
FS23_09	LOK	DMDFON ( 161 )	
FS23_10	LOK	DMDFON ( 161 )	
FS23_11	LOK	DMDFON ( 161 )	
FS23_12	LOK	DMDFON ( 161 )	
FS31_02	LOK	DMDFON ( 161 )	
FS31_03	LOK	DMDFON ( 161 )	
FS31_04	LOK	DMDFON ( 161 )	
FS31_05	LOK	DMDFON ( 161 )	
FS31_06	LOK	DMDFON ( 161 )	
FS31_07	LOK	DMDFON ( 161 )	
FS31_08	LOK	DMDFON ( 161 )	
FS31_09	LOK	DMDFON ( 161 )	
FS31_10	LOK	DMDFON ( 161 )	
FS31_11	LOK	DMDFON ( 161 )	
FS31_12	LOK	DMDFON ( 161 )	
FS32_02	LOK	DMDFON ( 161 )	
FS32_03	LOK	DMDFON ( 161 )	
FS32_04	LOK	DMDFON ( 161 )	
FS32_05	LOK	DMDFON ( 161 )	
FS32_06	LOK	DMDFON ( 161 )	
FS32_07	LOK	DMDFON ( 161 )	
FS32_08	LOK	DMDFON ( 161 )	
FS32_09	LOK	DMDFON ( 161 )	
FS32_10	LOK	DMDFON ( 161 )	
FS32_11	LOK	DMDFON ( 161 )	
FS32_12	LOK	DMDFON ( 161 )	
FS33_02	LOK	DMDFON ( 161 )	
FS33_03	LOK	DMDFON ( 161 )	
FS33_04	LOK	DMDFON ( 161 )	
FS33_05	LOK	DMDFON ( 161 )	
FS33_06	LOK	DMDFON ( 161 )	
FS33_07	LOK	DMDFON ( 161 )	
FS33_08	LOK	DMDFON ( 161 )	
FS33_09	LOK	DMDFON ( 161 )	
FS33_10	LOK	DMDFON ( 161 )	
FS33_11	LOK	DMDFON ( 161 )	
FS33_12	LOK	DMDFON ( 161 )	
FS41_02	LOK	DMDFON ( 161 )	
FS41_03	LOK	DMDFON ( 161 )	
FS41_04	LOK	DMDFON ( 161 )	
FS41_05	LOK	DMDFON ( 161 )	
FS41_06	LOK	DMDFON ( 161 )	
FS41_07	LOK	DMDFON ( 161 )	
FS41_08	LOK	DMDFON ( 161 )	
FS41_09	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FS41_10	LOK	DMDFON (161)	
FS41_11	LOK	DMDFON (161)	
FS41_12	LOK	DMDFON (161)	
FS42_02	LOK	DMDFON (161)	
FS42_03	LOK	DMDFON (161)	
FS42_04	LOK	DMDFON (161)	
FS42_05	LOK	DMDFON (161)	
FS42_06	LOK	DMDFON (161)	
FS42_07	LOK	DMDFON (161)	
FS42_08	LOK	DMDFON (161)	
FS42_09	LOK	DMDFON (161)	
FS42_10	LOK	DMDFON (161)	
FS42_11	LOK	DMDFON (161)	
FS42_12	LOK	DMDFON (161)	
FS43_02	LOK	DMDFON (161)	
FS43_03	LOK	DMDFON (161)	
FS43_04	LOK	DMDFON (161)	
FS43_05	LOK	DMDFON (161)	
FS43_06	LOK	DMDFON (161)	
FS43_07	LOK	DMDFON (161)	
FS43_08	LOK	DMDFON (161)	
FS43_09	LOK	DMDFON (161)	
FS43_10	LOK	DMDFON (161)	
FS43_11	LOK	DMDFON (161)	
FS43_12	LOK	DMDFON (161)	
FS51_02	LOK	DMDFON (161)	
FS51_03	LOK	DMDFON (161)	
FS51_04	LOK	DMDFON (161)	
FS51_05	LOK	DMDFON (161)	
FS51_06	LOK	DMDFON (161)	
FS51_07	LOK	DMDFON (161)	
FS51_08	LOK	DMDFON (161)	
FS51_09	LOK	DMDFON (161)	
FS51_10	LOK	DMDFON (161)	
FS51_11	LOK	DMDFON (161)	
FS51_12	LOK	DMDFON (161)	
FS52_02	LOK	DMDFON (161)	
FS52_03	LOK	DMDFON (161)	
FS52_04	LOK	DMDFON (161)	
FS52_05	LOK	DMDFON (161)	
FS52_06	LOK	DMDFON (161)	
FS52_07	LOK	DMDFON (161)	
FS52_08	LOK	DMDFON (161)	
FS52_09	LOK	DMDFON (161)	
FS52_10	LOK	DMDFON (161)	
FS52_11	LOK	DMDFON (161)	
FS52_12	LOK	DMDFON (161)	
FS53_02	LOK	DMDFON (161)	
FS53_03	LOK	DMDFON (161)	
FS53_04	LOK	DMDFON (161)	
FS53_05	LOK	DMDFON (161)	
FS53_06	LOK	DMDFON (161)	
FS53_07	LOK	DMDFON (161)	
FS53_08	LOK	DMDFON (161)	
FS53_09	LOK	DMDFON (161)	
FS53_10	LOK	DMDFON (161)	
FS53_11	LOK	DMDFON (161)	
FS53_12	LOK	DMDFON (161)	
FS61_02	LOK	DMDFON (161)	
FS61_03	LOK	DMDFON (161)	
FS61_04	LOK	DMDFON (161)	
FS61_05	LOK	DMDFON (161)	
FS61_06	LOK	DMDFON (161)	
FS61_07	LOK	DMDFON (161)	
FS61_08	LOK	DMDFON (161)	
FS61_09	LOK	DMDFON (161)	
FS61_10	LOK	DMDFON (161)	
FS61_11	LOK	DMDFON (161)	
FS61_12	LOK	DMDFON (161)	
FS62_02	LOK	DMDFON (161)	
FS62_03	LOK	DMDFON (161)	
FS62_04	LOK	DMDFON (161)	
FS62_05	LOK	DMDFON (161)	
FS62_06	LOK	DMDFON (161)	
FS62_07	LOK	DMDFON (161)	
FS62_08	LOK	DMDFON (161)	
FS62_09	LOK	DMDFON (161)	
FS62_10	LOK	DMDFON (161)	
FS62_11	LOK	DMDFON (161)	
FS62_12	LOK	DMDFON (161)	
FS63_02	LOK	DMDFON (161)	



Symbol	Type	Created within	Used within
FS63_03	LOK	DMDFON ( 161 )	
FS63_04	LOK	DMDFON ( 161 )	
FS63_05	LOK	DMDFON ( 161 )	
FS63_06	LOK	DMDFON ( 161 )	
FS63_07	LOK	DMDFON ( 161 )	
FS63_08	LOK	DMDFON ( 161 )	
FS63_09	LOK	DMDFON ( 161 )	
FS63_10	LOK	DMDFON ( 161 )	
FS63_11	LOK	DMDFON ( 161 )	
FS63_12	LOK	DMDFON ( 161 )	
FS71_02	LOK	DMDFON ( 161 )	
FS71_03	LOK	DMDFON ( 161 )	
FS71_04	LOK	DMDFON ( 161 )	
FS71_05	LOK	DMDFON ( 161 )	
FS71_06	LOK	DMDFON ( 161 )	
FS71_07	LOK	DMDFON ( 161 )	
FS71_08	LOK	DMDFON ( 161 )	
FS71_09	LOK	DMDFON ( 161 )	
FS71_10	LOK	DMDFON ( 161 )	
FS71_11	LOK	DMDFON ( 161 )	
FS71_12	LOK	DMDFON ( 161 )	
FS72_02	LOK	DMDFON ( 161 )	
FS72_03	LOK	DMDFON ( 161 )	
FS72_04	LOK	DMDFON ( 161 )	
FS72_05	LOK	DMDFON ( 161 )	
FS72_06	LOK	DMDFON ( 161 )	
FS72_07	LOK	DMDFON ( 161 )	
FS72_08	LOK	DMDFON ( 161 )	
FS72_09	LOK	DMDFON ( 161 )	
FS72_10	LOK	DMDFON ( 161 )	
FS72_11	LOK	DMDFON ( 161 )	
FS72_12	LOK	DMDFON ( 161 )	
FS73_02	LOK	DMDFON ( 161 )	
FS73_03	LOK	DMDFON ( 161 )	
FS73_04	LOK	DMDFON ( 161 )	
FS73_05	LOK	DMDFON ( 161 )	
FS73_06	LOK	DMDFON ( 161 )	
FS73_07	LOK	DMDFON ( 161 )	
FS73_08	LOK	DMDFON ( 161 )	
FS73_09	LOK	DMDFON ( 161 )	
FS73_10	LOK	DMDFON ( 161 )	
FS73_11	LOK	DMDFON ( 161 )	
FS73_12	LOK	DMDFON ( 161 )	
FS81_02	LOK	DMDFON ( 161 )	
FS81_03	LOK	DMDFON ( 161 )	
FS81_04	LOK	DMDFON ( 161 )	
FS81_05	LOK	DMDFON ( 161 )	
FS81_06	LOK	DMDFON ( 161 )	
FS81_07	LOK	DMDFON ( 161 )	
FS81_08	LOK	DMDFON ( 161 )	
FS81_09	LOK	DMDFON ( 161 )	
FS81_10	LOK	DMDFON ( 161 )	
FS81_11	LOK	DMDFON ( 161 )	
FS81_12	LOK	DMDFON ( 161 )	
FS82_02	LOK	DMDFON ( 161 )	
FS82_03	LOK	DMDFON ( 161 )	
FS82_04	LOK	DMDFON ( 161 )	
FS82_05	LOK	DMDFON ( 161 )	
FS82_06	LOK	DMDFON ( 161 )	
FS82_07	LOK	DMDFON ( 161 )	
FS82_08	LOK	DMDFON ( 161 )	
FS82_09	LOK	DMDFON ( 161 )	
FS82_10	LOK	DMDFON ( 161 )	
FS82_11	LOK	DMDFON ( 161 )	
FS82_12	LOK	DMDFON ( 161 )	
FS83_02	LOK	DMDFON ( 161 )	
FS83_03	LOK	DMDFON ( 161 )	
FS83_04	LOK	DMDFON ( 161 )	
FS83_05	LOK	DMDFON ( 161 )	
FS83_06	LOK	DMDFON ( 161 )	
FS83_07	LOK	DMDFON ( 161 )	
FS83_08	LOK	DMDFON ( 161 )	
FS83_09	LOK	DMDFON ( 161 )	
FS83_10	LOK	DMDFON ( 161 )	
FS83_11	LOK	DMDFON ( 161 )	
FS83_12	LOK	DMDFON ( 161 )	
FSE	LOK	DMDFON ( 161 )	
FSE11_02	LOK	DMDFON ( 161 )	
FSE11_03	LOK	DMDFON ( 161 )	
FSE11_04	LOK	DMDFON ( 161 )	
FSE11_05	LOK	DMDFON ( 161 )	





Symbol	Type	Created within	Used within
FSE11_06	LOK	DMDFON (161)	
FSE11_07	LOK	DMDFON (161)	
FSE11_08	LOK	DMDFON (161)	
FSE11_09	LOK	DMDFON (161)	
FSE11_10	LOK	DMDFON (161)	
FSE11_11	LOK	DMDFON (161)	
FSE11_12	LOK	DMDFON (161)	
FSE12_02	LOK	DMDFON (161)	
FSE12_03	LOK	DMDFON (161)	
FSE12_04	LOK	DMDFON (161)	
FSE12_05	LOK	DMDFON (161)	
FSE12_06	LOK	DMDFON (161)	
FSE12_07	LOK	DMDFON (161)	
FSE12_08	LOK	DMDFON (161)	
FSE12_09	LOK	DMDFON (161)	
FSE12_10	LOK	DMDFON (161)	
FSE12_11	LOK	DMDFON (161)	
FSE12_12	LOK	DMDFON (161)	
FSE13_02	LOK	DMDFON (161)	
FSE13_03	LOK	DMDFON (161)	
FSE13_04	LOK	DMDFON (161)	
FSE13_05	LOK	DMDFON (161)	
FSE13_06	LOK	DMDFON (161)	
FSE13_07	LOK	DMDFON (161)	
FSE13_08	LOK	DMDFON (161)	
FSE13_09	LOK	DMDFON (161)	
FSE13_10	LOK	DMDFON (161)	
FSE13_11	LOK	DMDFON (161)	
FSE13_12	LOK	DMDFON (161)	
FSE21_02	LOK	DMDFON (161)	
FSE21_03	LOK	DMDFON (161)	
FSE21_04	LOK	DMDFON (161)	
FSE21_05	LOK	DMDFON (161)	
FSE21_06	LOK	DMDFON (161)	
FSE21_07	LOK	DMDFON (161)	
FSE21_08	LOK	DMDFON (161)	
FSE21_09	LOK	DMDFON (161)	
FSE21_10	LOK	DMDFON (161)	
FSE21_11	LOK	DMDFON (161)	
FSE21_12	LOK	DMDFON (161)	
FSE22_02	LOK	DMDFON (161)	
FSE22_03	LOK	DMDFON (161)	
FSE22_04	LOK	DMDFON (161)	
FSE22_05	LOK	DMDFON (161)	
FSE22_06	LOK	DMDFON (161)	
FSE22_07	LOK	DMDFON (161)	
FSE22_08	LOK	DMDFON (161)	
FSE22_09	LOK	DMDFON (161)	
FSE22_10	LOK	DMDFON (161)	
FSE22_11	LOK	DMDFON (161)	
FSE22_12	LOK	DMDFON (161)	
FSE23_02	LOK	DMDFON (161)	
FSE23_03	LOK	DMDFON (161)	
FSE23_04	LOK	DMDFON (161)	
FSE23_05	LOK	DMDFON (161)	
FSE23_06	LOK	DMDFON (161)	
FSE23_07	LOK	DMDFON (161)	
FSE23_08	LOK	DMDFON (161)	
FSE23_09	LOK	DMDFON (161)	
FSE23_10	LOK	DMDFON (161)	
FSE23_11	LOK	DMDFON (161)	
FSE23_12	LOK	DMDFON (161)	
FSE31_02	LOK	DMDFON (161)	
FSE31_03	LOK	DMDFON (161)	
FSE31_04	LOK	DMDFON (161)	
FSE31_05	LOK	DMDFON (161)	
FSE31_06	LOK	DMDFON (161)	
FSE31_07	LOK	DMDFON (161)	
FSE31_08	LOK	DMDFON (161)	
FSE31_09	LOK	DMDFON (161)	
FSE31_10	LOK	DMDFON (161)	
FSE31_11	LOK	DMDFON (161)	
FSE31_12	LOK	DMDFON (161)	
FSE32_02	LOK	DMDFON (161)	
FSE32_03	LOK	DMDFON (161)	
FSE32_04	LOK	DMDFON (161)	
FSE32_05	LOK	DMDFON (161)	
FSE32_06	LOK	DMDFON (161)	
FSE32_07	LOK	DMDFON (161)	
FSE32_08	LOK	DMDFON (161)	
FSE32_09	LOK	DMDFON (161)	



Symbol	Type	Created within	Used within
FSE32_10	LOK	DMDFON (161)	
FSE32_11	LOK	DMDFON (161)	
FSE32_12	LOK	DMDFON (161)	
FSE33_02	LOK	DMDFON (161)	
FSE33_03	LOK	DMDFON (161)	
FSE33_04	LOK	DMDFON (161)	
FSE33_05	LOK	DMDFON (161)	
FSE33_06	LOK	DMDFON (161)	
FSE33_07	LOK	DMDFON (161)	
FSE33_08	LOK	DMDFON (161)	
FSE33_09	LOK	DMDFON (161)	
FSE33_10	LOK	DMDFON (161)	
FSE33_11	LOK	DMDFON (161)	
FSE33_12	LOK	DMDFON (161)	
FSE41_02	LOK	DMDFON (161)	
FSE41_03	LOK	DMDFON (161)	
FSE41_04	LOK	DMDFON (161)	
FSE41_05	LOK	DMDFON (161)	
FSE41_06	LOK	DMDFON (161)	
FSE41_07	LOK	DMDFON (161)	
FSE41_08	LOK	DMDFON (161)	
FSE41_09	LOK	DMDFON (161)	
FSE41_10	LOK	DMDFON (161)	
FSE41_11	LOK	DMDFON (161)	
FSE41_12	LOK	DMDFON (161)	
FSE42_02	LOK	DMDFON (161)	
FSE42_03	LOK	DMDFON (161)	
FSE42_04	LOK	DMDFON (161)	
FSE42_05	LOK	DMDFON (161)	
FSE42_06	LOK	DMDFON (161)	
FSE42_07	LOK	DMDFON (161)	
FSE42_08	LOK	DMDFON (161)	
FSE42_09	LOK	DMDFON (161)	
FSE42_10	LOK	DMDFON (161)	
FSE42_11	LOK	DMDFON (161)	
FSE42_12	LOK	DMDFON (161)	
FSE43_02	LOK	DMDFON (161)	
FSE43_03	LOK	DMDFON (161)	
FSE43_04	LOK	DMDFON (161)	
FSE43_05	LOK	DMDFON (161)	
FSE43_06	LOK	DMDFON (161)	
FSE43_07	LOK	DMDFON (161)	
FSE43_08	LOK	DMDFON (161)	
FSE43_09	LOK	DMDFON (161)	
FSE43_10	LOK	DMDFON (161)	
FSE43_11	LOK	DMDFON (161)	
FSE43_12	LOK	DMDFON (161)	
FSE51_02	LOK	DMDFON (161)	
FSE51_03	LOK	DMDFON (161)	
FSE51_04	LOK	DMDFON (161)	
FSE51_05	LOK	DMDFON (161)	
FSE51_06	LOK	DMDFON (161)	
FSE51_07	LOK	DMDFON (161)	
FSE51_08	LOK	DMDFON (161)	
FSE51_09	LOK	DMDFON (161)	
FSE51_10	LOK	DMDFON (161)	
FSE51_11	LOK	DMDFON (161)	
FSE51_12	LOK	DMDFON (161)	
FSE52_02	LOK	DMDFON (161)	
FSE52_03	LOK	DMDFON (161)	
FSE52_04	LOK	DMDFON (161)	
FSE52_05	LOK	DMDFON (161)	
FSE52_06	LOK	DMDFON (161)	
FSE52_07	LOK	DMDFON (161)	
FSE52_08	LOK	DMDFON (161)	
FSE52_09	LOK	DMDFON (161)	
FSE52_10	LOK	DMDFON (161)	
FSE52_11	LOK	DMDFON (161)	
FSE52_12	LOK	DMDFON (161)	
FSE53_02	LOK	DMDFON (161)	
FSE53_03	LOK	DMDFON (161)	
FSE53_04	LOK	DMDFON (161)	
FSE53_05	LOK	DMDFON (161)	
FSE53_06	LOK	DMDFON (161)	
FSE53_07	LOK	DMDFON (161)	
FSE53_08	LOK	DMDFON (161)	
FSE53_09	LOK	DMDFON (161)	
FSE53_10	LOK	DMDFON (161)	
FSE53_11	LOK	DMDFON (161)	
FSE53_12	LOK	DMDFON (161)	
FSE61_02	LOK	DMDFON (161)	



Symbol	Type	Created within	Used within
FSE61_03	LOK	DMDFON ( 161 )	
FSE61_04	LOK	DMDFON ( 161 )	
FSE61_05	LOK	DMDFON ( 161 )	
FSE61_06	LOK	DMDFON ( 161 )	
FSE61_07	LOK	DMDFON ( 161 )	
FSE61_08	LOK	DMDFON ( 161 )	
FSE61_09	LOK	DMDFON ( 161 )	
FSE61_10	LOK	DMDFON ( 161 )	
FSE61_11	LOK	DMDFON ( 161 )	
FSE61_12	LOK	DMDFON ( 161 )	
FSE62_02	LOK	DMDFON ( 161 )	
FSE62_03	LOK	DMDFON ( 161 )	
FSE62_04	LOK	DMDFON ( 161 )	
FSE62_05	LOK	DMDFON ( 161 )	
FSE62_06	LOK	DMDFON ( 161 )	
FSE62_07	LOK	DMDFON ( 161 )	
FSE62_08	LOK	DMDFON ( 161 )	
FSE62_09	LOK	DMDFON ( 161 )	
FSE62_10	LOK	DMDFON ( 161 )	
FSE62_11	LOK	DMDFON ( 161 )	
FSE62_12	LOK	DMDFON ( 161 )	
FSE63_02	LOK	DMDFON ( 161 )	
FSE63_03	LOK	DMDFON ( 161 )	
FSE63_04	LOK	DMDFON ( 161 )	
FSE63_05	LOK	DMDFON ( 161 )	
FSE63_06	LOK	DMDFON ( 161 )	
FSE63_07	LOK	DMDFON ( 161 )	
FSE63_08	LOK	DMDFON ( 161 )	
FSE63_09	LOK	DMDFON ( 161 )	
FSE63_10	LOK	DMDFON ( 161 )	
FSE63_11	LOK	DMDFON ( 161 )	
FSE63_12	LOK	DMDFON ( 161 )	
FSE71_02	LOK	DMDFON ( 161 )	
FSE71_03	LOK	DMDFON ( 161 )	
FSE71_04	LOK	DMDFON ( 161 )	
FSE71_05	LOK	DMDFON ( 161 )	
FSE71_06	LOK	DMDFON ( 161 )	
FSE71_07	LOK	DMDFON ( 161 )	
FSE71_08	LOK	DMDFON ( 161 )	
FSE71_09	LOK	DMDFON ( 161 )	
FSE71_10	LOK	DMDFON ( 161 )	
FSE71_11	LOK	DMDFON ( 161 )	
FSE71_12	LOK	DMDFON ( 161 )	
FSE72_02	LOK	DMDFON ( 161 )	
FSE72_03	LOK	DMDFON ( 161 )	
FSE72_04	LOK	DMDFON ( 161 )	
FSE72_05	LOK	DMDFON ( 161 )	
FSE72_06	LOK	DMDFON ( 161 )	
FSE72_07	LOK	DMDFON ( 161 )	
FSE72_08	LOK	DMDFON ( 161 )	
FSE72_09	LOK	DMDFON ( 161 )	
FSE72_10	LOK	DMDFON ( 161 )	
FSE72_11	LOK	DMDFON ( 161 )	
FSE72_12	LOK	DMDFON ( 161 )	
FSE73_02	LOK	DMDFON ( 161 )	
FSE73_03	LOK	DMDFON ( 161 )	
FSE73_04	LOK	DMDFON ( 161 )	
FSE73_05	LOK	DMDFON ( 161 )	
FSE73_06	LOK	DMDFON ( 161 )	
FSE73_07	LOK	DMDFON ( 161 )	
FSE73_08	LOK	DMDFON ( 161 )	
FSE73_09	LOK	DMDFON ( 161 )	
FSE73_10	LOK	DMDFON ( 161 )	
FSE73_11	LOK	DMDFON ( 161 )	
FSE73_12	LOK	DMDFON ( 161 )	
FSE81_02	LOK	DMDFON ( 161 )	
FSE81_03	LOK	DMDFON ( 161 )	
FSE81_04	LOK	DMDFON ( 161 )	
FSE81_05	LOK	DMDFON ( 161 )	
FSE81_06	LOK	DMDFON ( 161 )	
FSE81_07	LOK	DMDFON ( 161 )	
FSE81_08	LOK	DMDFON ( 161 )	
FSE81_09	LOK	DMDFON ( 161 )	
FSE81_10	LOK	DMDFON ( 161 )	
FSE81_11	LOK	DMDFON ( 161 )	
FSE81_12	LOK	DMDFON ( 161 )	
FSE82_02	LOK	DMDFON ( 161 )	
FSE82_03	LOK	DMDFON ( 161 )	
FSE82_04	LOK	DMDFON ( 161 )	
FSE82_05	LOK	DMDFON ( 161 )	
FSE82_06	LOK	DMDFON ( 161 )	



Symbol	Type	Created within	Used within
FSE82_07	LOK	DMDFON ( 161 )	
FSE82_08	LOK	DMDFON ( 161 )	
FSE82_09	LOK	DMDFON ( 161 )	
FSE82_10	LOK	DMDFON ( 161 )	
FSE82_11	LOK	DMDFON ( 161 )	
FSE82_12	LOK	DMDFON ( 161 )	
FSE83_02	LOK	DMDFON ( 161 )	
FSE83_03	LOK	DMDFON ( 161 )	
FSE83_04	LOK	DMDFON ( 161 )	
FSE83_05	LOK	DMDFON ( 161 )	
FSE83_06	LOK	DMDFON ( 161 )	
FSE83_07	LOK	DMDFON ( 161 )	
FSE83_08	LOK	DMDFON ( 161 )	
FSE83_09	LOK	DMDFON ( 161 )	
FSE83_10	LOK	DMDFON ( 161 )	
FSE83_11	LOK	DMDFON ( 161 )	
FSE83_12	LOK	DMDFON ( 161 )	
FSLPDYN	EIN		LAKH ( 735 )
FSP_CL	EIN		DCINS ( 1126 )
FSTQ_W	LOK	ESSTT ( 679 )	
FST_W	AUS	ESSTT ( 679 )	ESVST ( 677 ), GK ( 675 )
FSWARES	LOK	DSWEC ( 32 )	
FTADMSTE	LOK	TEB ( 826 )	
FTBR	AUS	BGTEMPK ( 252 )	EGFE ( 228 )
FTBR_W	AUS	BGTEMPK ( 252 )	BGSRM ( 245 ), EGFE ( 228 )
FTEADF	AUS	TEB ( 826 )	
FTEADF_W	LOK	TEB ( 826 )	
FTEAD_W	AUS	TEB ( 826 )	BBTEGA ( 750 ), DTEV ( 856 )
FTEFSOLD_W	LOK	TEB ( 826 )	
FTEFSOLL_W	EIN		DTEV ( 856 ), TEB ( 826 )
FTEFVA	LOK	TEB ( 826 )	
FTEFVAB	LOK	TEB ( 826 )	
FTEFVAMX_W	LOK	TEB ( 826 )	
FTEFVA_W	AUS	TEB ( 826 )	
FTEML	AUS	TEB ( 826 )	
FTHOZS_W	LOK	DTEV ( 856 )	
FTHO_W	LOK	BGTEV ( 257 )	
FTKLRA_W	LOK	LRA ( 797 )	
FTSR	AUS	BGTEMPK ( 252 )	BGSRM ( 245 ), EGFE ( 228 )
FTU	AUS	BGTEMPK ( 252 )	BGPU ( 276 ), EGFE ( 228 )
FTV	LOK	LRHK ( 781 )	
FTV2	LOK	LRHK ( 781 )	
FTVDK	AUS	BGTEMPK ( 252 )	SWADAP ( 47 ), BGMSZS ( 239 ), BGTEV ( 257 ), BGPU ( 276 ), MD-MAX ( 514 ), GGDVE ( 477 ), FUEDK ( 597 ), DTEV ( 856 ), EGFE ( 228 )
FTW	LOK	BGTEMPK ( 252 )	
FUBAANZ	AUS	ZUESZ ( 632 )	
FUEPMLD_W	LOK	FUEDK ( 597 )	
FUKABAK_W	LOK	ESUKA ( 711 )	
FUKABAW_W	LOK	ESUKA ( 711 )	
FUKABA_W	AUS	ESUKA ( 711 )	ESUK ( 699 )
FUKAVA	EIN		ESUK ( 699 )
FUKAVAK_W	LOK	ESUKA ( 711 )	
FUKAVAW_W	LOK	ESUKA ( 711 )	
FUKAVA_W	AUS	ESUKA ( 711 )	
FUPSRLL_W	AUS	BGSRM ( 245 )	EGFE ( 228 ), BGRLP ( 266 ), FUEDK ( 597 )
FVAKL_W	AUS	ESUK ( 699 )	
FVANS	LOK	ESUK ( 699 )	
FVAVST_W	LOK	ESUK ( 699 )	
FVERMTE_W	LOK	TEB ( 826 )	
FVISRM_W	AUS	BGSRM ( 245 )	BGAGR ( 263 ), BGRLP ( 266 ), EGFE ( 228 )
FVST_W	LOK	GK ( 675 )	
FWE	AUS	ESVST ( 677 )	ESWE ( 698 ), GK ( 675 ), LRKA ( 795 )
FWEG	AUS	ACIFI ( 1013 )	
FWEZ0	AUS	ACIFI ( 1013 )	
FWL	AUS	ESNSWL ( 691 )	ESVST ( 677 )
FWLRL	LOK	ESNSWL ( 691 )	
FWMLHFM	AUS	DHFM ( 233 )	
FWPRS_W	LOK	BGRLP ( 266 )	
FZABGS	EIN		DMDFON ( 161 )
FZABGS_W	LOK	DMDMIL ( 216 )	
FZABG_W_0	LOK	DMDMIL ( 216 )	
FZABG_W_1	LOK	DMDMIL ( 216 )	
FZABG_W_10	LOK	DMDMIL ( 216 )	
FZABG_W_11	LOK	DMDMIL ( 216 )	
FZABG_W_2	LOK	DMDMIL ( 216 )	
FZABG_W_3	LOK	DMDMIL ( 216 )	
FZABG_W_4	LOK	DMDMIL ( 216 )	
FZABG_W_5	LOK	DMDMIL ( 216 )	
FZABG_W_6	LOK	DMDMIL ( 216 )	
FZABG_W_7	LOK	DMDMIL ( 216 )	
FZABG_W_8	LOK	DMDMIL ( 216 )	
FZABG_W_9	LOK	DMDMIL ( 216 )	



Symbol	Type	Created within	Used within
FZANS1	LOK	ESNSWL ( 691 )	
FZARV_W	LOK	DMDMIL ( 216 )	
FZDASH	LOK	MDFAW ( 508 )	
FZKATS1_W	LOK	DMDMIL ( 216 )	
FZKATS2_W	LOK	DMDMIL ( 216 )	
FZKATS_W	LOK	DMDMIL ( 216 )	
FZKAT_W_0	LOK	DMDMIL ( 216 )	
FZKAT_W_1	LOK	DMDMIL ( 216 )	
FZKAT_W_10	LOK	DMDMIL ( 216 )	
FZKAT_W_11	LOK	DMDMIL ( 216 )	
FZKAT_W_2	LOK	DMDMIL ( 216 )	
FZKAT_W_3	LOK	DMDMIL ( 216 )	
FZKAT_W_4	LOK	DMDMIL ( 216 )	
FZKAT_W_5	LOK	DMDMIL ( 216 )	
FZKAT_W_6	LOK	DMDMIL ( 216 )	
FZKAT_W_7	LOK	DMDMIL ( 216 )	
FZKAT_W_8	LOK	DMDMIL ( 216 )	
FZKAT_W_9	LOK	DMDMIL ( 216 )	
FZWMN_W	LOK	ZWMIN ( 669 )	
GANGAUTI	EIN		BBGANG ( 501 )
GANGI	AUS	BBGANG ( 501 )	SWADAP ( 47 ), ARMD ( 531 ), BBSAWE ( 557 ), FGRUE ( 490 ), KOS ( 896 ), LLRBB ( 575 ), KRDY ( 659 ), ZWMIN ( 669 ), MDWAN ( 554 ), MDMIN ( 538 ), MDFAW ( 508 ), MDBGRG ( 530 ), FGRABED ( 491 ), EGAG ( 486 )
GANGJ	AUS	EGAG ( 486 )	
GANG_KUP	AUS	CAN ( 1124 )	BBGANG ( 501 )
GAPTOOTH	AUS	GGDPG ( 74 )	ALE ( 136 ), WANWKW ( 125 ), RDE ( 112 )
GKLFNSSM	LOK	ESNSWL ( 691 )	
GRUNDWERT	EIN		BGRLP ( 266 ), GGKS ( 412 )
HAGR	AUS	EGAG ( 486 )	BGAGR ( 263 ), EGFE ( 228 )
I	LOK	KRDY ( 659 )	
IASP1PLAUS	EIN		URADCC ( 1049 )
IAVKATF	DOK	LRHK ( 781 )	
IDLASHKM_W	DOK	LRHK ( 781 )	
IDXFOB	LOK	DMDFON ( 161 )	
IDXFON	LOK	DMDFON ( 161 )	
IDXFORL	LOK	DMDFON ( 161 )	
IGOD_W	AUS	GGKS ( 412 )	DKRNT ( 445 )
IGOKR_W	AUS	GGKS ( 412 )	EGKE ( 409 )
IKR	AUS	GGKS ( 412 )	KRKE ( 427 ), EGKE ( 409 )
IKRMA	EIN		DKRNT ( 445 ), DKRTP ( 451 ), KRKE ( 427 ), EGKE ( 409 ), GGKS ( 412 )
IKRME	EIN		KRKE ( 427 ), EGKE ( 409 ), GGKS ( 412 )
IKRMEN	AUS	GGKS ( 412 )	
IKRMET	EIN		DKRTP ( 451 ), EGKE ( 409 ), GGKS ( 412 )
IKR_TST	LOK	GGKS ( 412 )	
ILMLKA2_W	LOK	LRKA ( 795 )	
ILMLKAH2_W	LOK	LRKA ( 795 )	
ILMLKAH_W	LOK	LRKA ( 795 )	
ILMLKAM_W	LOK	LRKA ( 795 )	
ILMLKAT2_W	AUS	LRKA ( 795 )	
ILMLKAT_W	AUS	LRKA ( 795 )	
ILMLKAV2_W	LOK	LRKA ( 795 )	
ILMLKAV_W	LOK	LRKA ( 795 )	
ILMLKAX2_W	LOK	LRKA ( 795 )	
ILMLKAX_W	LOK	LRKA ( 795 )	
ILMLKA_W	LOK	LRKA ( 795 )	
IMLATM	AUS	ATM ( 20 )	AK ( 855 ), ESSTT ( 679 ), BGTABST ( 1030 )
IMLATM_W	AUS	ATM ( 20 )	BBKHZ ( 890 )
IMLBBO	AUS	BBBO ( 853 )	
IMLKA2_W	LOK	LRKA ( 795 )	
IMLKAV2_W	LOK	LRKA ( 795 )	
IMLKAV_W	LOK	LRKA ( 795 )	
IMLKAX2_W	LOK	LRKA ( 795 )	
IMLKAX_W	LOK	LRKA ( 795 )	
IMLKA_W	LOK	LRKA ( 795 )	
IMLKVSZS_W	LOK	DKVS ( 811 )	
IMLKVS_W	LOK	DKVS ( 811 )	
IMLPR	AUS	BBKHZ ( 890 )	AK ( 855 )
IMLPR_W	AUS	BBKHZ ( 890 )	
IMLRSW	LOK	LREB ( 739 )	
IMSTEINI	EIN		DTEV ( 856 ), TEB ( 826 )
INGAS	LOK	BGNG ( 121 )	
IOKKR	AUS	GGKS ( 412 )	
IPA_C_JJM	LOK	UFRLC ( 1066 )	
IPLSUVJ2_W	EIN		TC1MOD ( 1100 )
IPLSUVJ_W	EIN		TC1MOD ( 1100 )
IPSN_JJM	LOK	UFRLC ( 1066 )	
IRSPSYN	AUS	BGNG ( 121 )	
IUIPOT1	EIN		BGRLG ( 274 )
IUIPOT2	EIN		UFRLC ( 1066 ), UFUE ( 1056 )
IUSPOT1	EIN		UFRLC ( 1066 ), UFUE ( 1056 )
IUSPOT2	EIN		UFSPSC ( 1060 ), UFUE ( 1056 ), URADCC ( 1049 )
IVER	LOK	LLRRM ( 566 )	UFSPSC ( 1060 ), UFUE ( 1056 )



Symbol	Type	Created within	Used within
IVMAX	LOK	VMAXMD ( 588 )	
IVZABG_W	LOK	DMDMIL ( 216 )	
IVZAIN_T_W	LOK	DMDMIL ( 216 )	
IVZARV_W	LOK	DMDMIL ( 216 )	
IVZKAT_W	LOK	DMDMIL ( 216 )	
IWFLSD_W	LOK	MDFAW ( 508 )	
IWMATM2_W	AUS	ATM ( 20 )	
IWMATM_W	AUS	ATM ( 20 )	
KAKBMT	LOK	DKAT ( 361 )	
KAKBMT2	LOK	DKAT ( 361 )	
KATBF	LOK	DKAT ( 361 )	
KATBF2	LOK	DKAT ( 361 )	
KATBF12_W	LOK	DKAT ( 361 )	
KATBF1_W	LOK	DKAT ( 361 )	
KATBFS	LOK	DKAT ( 361 )	
KATBFS2	LOK	DKAT ( 361 )	
KATBFTP	LOK	DKAT ( 361 )	
KATBFTP2	LOK	DKAT ( 361 )	
KATBSHD2_W	LOK	DKAT ( 361 )	
KATBSHD_W	LOK	DKAT ( 361 )	
KBDKT2_W	LOK	DKAT ( 361 )	
KBDKT_W	LOK	DKAT ( 361 )	
KE0W	LOK	KRKE ( 427 )	
KE1W	LOK	KRKE ( 427 )	
KE2W	LOK	KRKE ( 427 )	
KE3W	LOK	KRKE ( 427 )	
KE4W	LOK	KRKE ( 427 )	
KE5W	LOK	KRKE ( 427 )	
KE6W	LOK	KRKE ( 427 )	
KE7W	LOK	KRKE ( 427 )	
KEK	AUS	EGKE ( 409 )	KRKE ( 427 ), KRKY ( 659 )
KEK_TST	AUS	KRKE ( 427 )	
KFBS2_W	LOK	GK ( 675 )	
KFBS_W	LOK	GK ( 675 )	
KFGR_W	LOK	FGRREGL ( 1174 )	
KFKFWWNS	LOK	ESNSWL ( 691 )	
KFMDSZAS_W	LOK	MDVER ( 546 )	
KFMDS_W	LOK	MDVER ( 546 )	
KHC_W	LOK	TEB ( 826 )	
KIFZ_W	AUS	ARMD ( 531 )	
KINMX	LOK	NMAXMD ( 584 )	
KLDFPWM	EIN		DTEV ( 856 ), LLRNS ( 562 ), MDVERB ( 540 )
KL_TWSTT_W	LOK	ESSTT ( 679 )	
KMST100M_W	AUS	BGBSZ ( 73 )	
KMST6553_W	AUS	BGBSZ ( 73 )	
KMSTMIL_W	AUS	BGKMST ( 1008 )	TC1MOD ( 1100 )
KMST_L	AUS	BGBSZ ( 73 )	
KMST_W	AUS	BGKMST ( 1008 )	
KRAL1W	LOK	KRRA ( 639 )	
KRAL2W	LOK	KRRA ( 639 )	
KRAL3W	LOK	KRRA ( 639 )	
KRDWSW	LOK	KRRA ( 639 )	
KRFKW	LOK	KRRA ( 639 )	
KRFTPAKT	AUS	KRKE ( 427 )	GGKS ( 412 )
KRLZN	LOK	KRRA ( 639 )	
KRMXW	LOK	KRRA ( 639 )	
KRVFSW	LOK	KRRA ( 639 )	
KRVFW	LOK	KRRA ( 639 )	
KSTA0	LOK	STADAP ( 684 )	
KSTA0W	LOK	STADAP ( 684 )	
KSTA1	LOK	STADAP ( 684 )	
KSTA1W	LOK	STADAP ( 684 )	
KSTA2	LOK	STADAP ( 684 )	
KSTA2W	LOK	STADAP ( 684 )	
KSTAA	AUS	STADAP ( 684 )	ESSTT ( 679 ), ESVST ( 677 )
KSWF	LOK	DMDMIL ( 216 )	
KS_SYM	AUS	GGKS ( 412 )	
KTEEV_W	LOK	TEB ( 826 )	
KTETEVVZ_W	LOK	TEB ( 826 )	
KTETEV_W	LOK	TEB ( 826 )	
KVB_W	AUS	BGKV ( 71 )	
LAHKMZ	LOK	LRHK ( 781 )	
LAHKMZ2	LOK	LRHK ( 781 )	
LALSUVJ2_W	EIN		TC1MOD ( 1100 )
LALSUVJ_W	EIN		TC1MOD ( 1100 )
LAMBAS	AUS	LAMKO ( 729 )	MSF ( 506 ), SWADAP ( 47 ), MDBAS ( 529 ), ZWGRU ( 634 )
LAMBAS_W	AUS	SWADAP ( 47 )	
LAMBTS_W	AUS	LAMBTS ( 732 )	
LAMELSH2_W	AUS	DLSH ( 330 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMELSH_W	AUS	DLSH ( 330 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMFA_W	AUS	LAMFAW ( 728 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMFRM2_W	LOK	DLSAHK ( 339 )	LAMKO ( 729 ), LAMSOLL ( 726 )



Symbol	Type	Created within	Used within
LAMFRM_W	LOK	DLSAHK ( 339 )	
LAMHF2_W	LOK	LRHK ( 781 )	
LAMHF_W	LOK	LRHK ( 781 )	
LAMHM2_W	LOK	LRHK ( 781 )	
LAMHM_W	LOK	LRHK ( 781 )	
LAMKA2_W	AUS	LRKA ( 795 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMKAI2_W	LOK	LRKA ( 795 )	
LAMKAII2_W	LOK	LRKA ( 795 )	
LAMKAIL_W	LOK	LRKA ( 795 )	
LAMKAI_W	LOK	LRKA ( 795 )	
LAMKA_W	AUS	LRKA ( 795 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMKH	LOK	AK ( 855 )	
LAMKH2_W	AUS	LAKH ( 735 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMKHE2_W	LOK	LAMKO ( 729 )	
LAMKHE_W	LOK	LAMKO ( 729 )	
LAMKHR2_W	LOK	LAKH ( 735 )	
LAMKHR_W	LOK	LAKH ( 735 )	
LAMKH_W	AUS	LAKH ( 735 )	MSF ( 506 ), LAMKO ( 729 ), LAMSOLL ( 726 )
LAMLASH2_W	AUS	DLSAHK ( 339 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMLASH_W	AUS	DLSAHK ( 339 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMLGM	LOK	LAMKO ( 729 )	
LAMNSWL_W	AUS	ESVST ( 677 )	LAMKO ( 729 ), LAMSOLL ( 726 )
LAMNS_W	AUS	ESVST ( 677 )	GK ( 675 )
LAMS2_W	LOK	LAMKO ( 729 )	
LAMSBG	AUS	AK ( 855 )	
LAMSBG2_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 ), ATM ( 20 ), GK ( 675 )
LAMSBG_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 ), ATM ( 20 ), GK ( 675 )
LAMSISA	AUS	DLSSA ( 350 )	
LAMSISA2	AUS	DLSSA ( 350 )	
LAMSNKA2_W	LOK	LRKA ( 795 )	
LAMSNKA_W	LOK	LRKA ( 795 )	
LAMSOLH2_W	AUS	LRHK ( 781 )	
LAMSOLH_W	AUS	LRHK ( 781 )	
LAMSONH2_W	AUS	LRHK ( 781 )	
LAMSONH_W	AUS	LRHK ( 781 )	
LAMSONI2_W	EIN		DLSSA ( 350 )
LAMSONI_W	EIN		DLSSA ( 350 )
LAMSONS	AUS	AK ( 855 )	
LAMSONS2_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 ), DLSH ( 330 ), LRKA ( 795 ), LREB ( 739 ), GKRA ( 766 ), GKEB ( 737 ), DLSV ( 301 ), DLSSA ( 350 )
LAMSONS_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 ), DLSH ( 330 ), GKRA ( 766 ), GKEB ( 737 ), TEBEB ( 762 ), LRKA ( 795 ), LREB ( 739 ), LRAEB ( 759 ), DLSV ( 301 ), DLSSA ( 350 )
LAMSOS2_W	LOK	LAMKO ( 729 )	
LAMSOSA	AUS	DLSSA ( 350 )	
LAMSOSA2	AUS	DLSSA ( 350 )	
LAMSOS_W	LOK	LAMKO ( 729 )	
LAMSUBG2_W	LOK	LAMKO ( 729 )	
LAMSUBG_W	LOK	LAMKO ( 729 )	
LAMS_W	LOK	LAMKO ( 729 )	
LAMVOA2_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 )
LAMVOA_W	AUS	LAMKO ( 729 )	LAMSOLL ( 726 )
LASDSL_W	LOK	LAKH ( 735 )	
LASKH_W	LOK	LAKH ( 735 )	
LBZ	AUS	BGLBZ ( 489 )	SWADAP ( 47 ), EGAG ( 486 ), LLRNS ( 562 )
LDTV_W	EIN		FUEDK ( 597 )
LDTV_M	AUS	FE ( 591 )	
LEN_HISEG	LOK	GGDPG ( 74 )	
LEN_LOSEG	LOK	GGDPG ( 74 )	
LIMAX_W	EIN		DLLR ( 578 ), LLRRM ( 566 )
LIMIN_W	EIN		DLLR ( 578 ), LLRRM ( 566 )
LIMNST	LOK	LLRRM ( 566 )	
LKRNEW	LOK	KRDY ( 659 )	
LKROLD	LOK	KRDY ( 659 )	
LKRW	LOK	KRRA ( 639 )	
LMSKH_W	LOK	LAKH ( 735 )	
LMSL2_W	LOK	LAKH ( 735 )	
LMSL_W	LOK	LAKH ( 735 )	
LRFRMZ	LOK	LR ( 768 )	
LRFRMZ2	LOK	LR ( 768 )	
LRFRZ	LOK	LR ( 768 )	
LRFRZ2	LOK	LR ( 768 )	
LRKAZ	LOK	LRKA ( 795 )	
LRKAZ2	LOK	LRKA ( 795 )	
LRNSTAT	AUS	BGDVE ( 934 )	
LRNSTEP_C	AUS	BGDVE ( 934 )	DDVE ( 950 )
LRNTIM_C	LOK	BGDVE ( 934 )	
LRNVB_C	LOK	BGDVE ( 934 )	
LSADKT	LOK	DKAT ( 361 )	
LUAR	DOK	DMDLUA ( 202 )	
LUARMN	LOK	DMDLUA ( 202 )	
LUAROFF	LOK	DMDLUA ( 202 )	
LUAR_M	LOK	DMDLUA ( 202 )	



Symbol	Type	Created within	Used within
LUAR_M2	LOK	DMDLUA ( 202 )	
LUMS	DOK	DMDLU ( 193 )	
LUMS_M	LOK	DMDLU ( 193 )	
LUMS_M2	LOK	DMDLU ( 193 )	
LUNW	LOK	DMDFON ( 161 )	
LURMS	DOK	DMDLU ( 193 )	
LURMS_M	LOK	DMDLU ( 193 )	
LURMS_M2	LOK	DMDLU ( 193 )	
LURS	DOK	DMDLU ( 193 )	
LURSKTM	AUS	DMDLU ( 193 )	DMDDL ( 199 )
LURS_M	LOK	DMDLU ( 193 )	
LURS_M2	LOK	DMDLU ( 193 )	
LURS_MIN	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS	AUS	DMDLU ( 193 )	DMDDL ( 199 )
LUTS1	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS10	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS11	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS12	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS2	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS3	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS4	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS5	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS6	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS7	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS8	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS9	AUS	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS_M	LOK	DMDLU ( 193 )	DMDLUA ( 202 )
LUTS_M2	LOK	DMDLU ( 193 )	
LWS_W	EIN		MDVERB ( 540 )
LZIST	LOK	KRRA ( 639 )	
M6CATV	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6CATV2	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6CKTH	EIN		TC6MOD ( 1112 )
M6CKTH2	EIN		TC6MOD ( 1112 )
M6CLSCH	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CLSCH2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CLSDY	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CLSDY2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CMSL	EIN		TC6MOD ( 1112 )
M6CMSL2	EIN		TC6MOD ( 1112 )
M6CMSLV	EIN		TC6MOD ( 1112 )
M6CMSLV2	EIN		TC6MOD ( 1112 )
M6CSHKF	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CSHKF2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CSHKM	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CSHKM2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6CTP	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6CTP2	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6KATNC	EIN		TC6MOD ( 1112 )
M6KATNS_W	EIN		TC6MOD ( 1112 )
M6SATV	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6SATV2	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6SKTH2_W	EIN		TC6MOD ( 1112 )
M6SKTH_W	EIN		TC6MOD ( 1112 )
M6SLSCH	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SLSCH2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SLSDY	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SLSDY2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SMSL2_W	EIN		TC6MOD ( 1112 )
M6SMSLV2_W	EIN		TC6MOD ( 1112 )
M6SMSLV_W	EIN		TC6MOD ( 1112 )
M6SMSL_W	EIN		TC6MOD ( 1112 )
M6SSHKF	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SSHKF2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SSHKM	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6SSHKM2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6STP2_W	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6STP_W	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6VKANW_W	EIN		TC6MOD ( 1112 )
M6WATV	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6WATV2	AUS	DLSA ( 398 )	TC6MOD ( 1112 )
M6WKTH2_W	EIN		TC6MOD ( 1112 )
M6WKTH_W	EIN		TC6MOD ( 1112 )
M6WLSCH	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6WLSCH2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6WLSDY	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6WLSDY2	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )
M6WMSL2_W	EIN		TC6MOD ( 1112 )
M6WMSLV2_W	EIN		TC6MOD ( 1112 )
M6WMSLV_W	EIN		TC6MOD ( 1112 )
M6WMSL_W	EIN		TC6MOD ( 1112 )
M6WWSHKF	AUS	DLSAHK ( 339 )	TC6MOD ( 1112 )





Symbol	Type	Created within	Used within
M6WSHKF2	AUS	DLSAHK ( 339 )	TC6MOD (1112)
M6WSHKM	AUS	DLSAHK ( 339 )	TC6MOD (1112)
M6WSHKM2	AUS	DLSAHK ( 339 )	TC6MOD (1112)
M6WTP2_W	AUS	DLSA ( 398 )	TC6MOD (1112)
M6WTP_W	AUS	DLSA ( 398 )	TC6MOD (1112)
MBEG_C	AUS	UFSGSC (1070)	
MDBES_W	AUS	ARMD ( 531 )	
MDDLWS_W	LOK	MDVERB ( 540 )	
MDGEN	AUS	MDVERB ( 540 )	
MDGRAD_W	EIN		MDFAW ( 508 )
MDIF_W_UM	AUS	UFMVER (1087)	
MDINDG_W	LOK	MDIST ( 528 )	
MDIND_ASRL	LOK	UFMSRC (1080)	
MDIND_ASRS	LOK	UFMSRC (1080)	
MDIND_MSR	LOK	UFMSRC (1080)	
MDKO	AUS	MDVERB ( 540 )	KOS ( 896 )
MDKOINI	LOK	MDVERB ( 540 )	
MDLFS	AUS	MDVERB ( 540 )	
MDLWS_W	LOK	MDVERB ( 540 )	
MDNS_W	AUS	MDVER ( 546 )	
MDSLFP	AUS	MDVERB ( 540 )	
MDSMZAS_W	LOK	MDVER ( 546 )	
MDSM_W	LOK	MDVER ( 546 )	
MDSWL	AUS	MDVERB ( 540 )	
MDS_W	LOK	MDVER ( 546 )	
MDVERB	AUS	MDVERB ( 540 )	MDVER ( 546 )
MDVERBC	EIN		MDVERB ( 540 )
MDVERF_W	AUS	MDVER ( 546 )	MDMIN ( 538 )
MDVERL_W	AUS	MDVER ( 546 )	ARMD ( 531 ), CAN (1124), MDFAW ( 508 )
MDVERVF_W	LOK	MDVER ( 546 )	
MDWAN_W	AUS	MDWAN ( 554 )	MDVER ( 546 )
MEBZA_UM_C	LOK	UFMER (1060)	
MEBZ_UM	AUS	UFMET (1060)	
MEBZ_UM_C	LOK	UFMER (1060)	
MECS_UM	AUS	UFMET (1060)	
MECS_UM_C	LOK	UFMER (1060)	
MEND_C	AUS	UFSGSC (1070)	
MER_C1_UM	EIN		DUF (1089)
MER_C2_UM	EIN		DUF (1089)
MEST_UM	AUS	UFMET (1060)	
MEST_UM_C	LOK	UFMER (1060)	
MFGR_UM	AUS	UFFGRC (1078)	UFMET (1060), UFMZUL (1084), UFUE (1056)
MFGR_UM_C	AUS	UFMER (1060)	
MIASRL_C	EIN		CAN (1124)
MIASRL_W	AUS	CAN (1124)	SWADAP ( 47 ), MDKOG ( 516 ), MSF ( 506 ), MDKOL ( 526 )
MIASRS_C	EIN		CAN (1124)
MIASRS_W	AUS	CAN (1124)	SWADAP ( 47 ), MDAUTG ( 515 ), MDKOG ( 516 ), MSF ( 506 )
MIAUTGET_W	AUS	MDAUTG ( 515 )	
MIAUTGS_W	AUS	MDAUTG ( 515 )	
MIBAS_W	AUS	MDBAS ( 529 )	AES ( 973 ), MDAUTG ( 515 ), MDRED ( 976 ), MSF ( 506 ), MDZW ( 636 ), MDKOG ( 516 )
MIBDP_W	LOK	MDFAW ( 508 )	
MIBEG_W	LOK	MDKOG ( 516 )	
MIBGR_W	AUS	MDBGRG ( 530 )	MDAUTG ( 515 ), MDKOG ( 516 ), MDKOL ( 526 )
MIBLSD_W	LOK	MDFAW ( 508 )	
MIFA	AUS	MDFAW ( 508 )	AK ( 855 )
MIFABG_W	LOK	MDFAW ( 508 )	
MIFABH_W	LOK	NMAXMD ( 584 )	
MIFAB_W	AUS	MDKOG ( 516 )	NMAXMD ( 584 ), VMAXMD ( 588 )
MIFAFU_W	AUS	MDKOL ( 526 )	FUEDK ( 597 )
MIFAKH_W	LOK	KHMD ( 894 )	
MIFAL_W	AUS	MDFAW ( 508 )	MSF ( 506 ), KOS ( 896 ), MDKOL ( 526 )
MIFAMX_W	AUS	GGPED ( 454 )	
MIFA_UM	EIN		UFFGRC (1078), UFUE (1056)
MIFA_W	AUS	MDFAW ( 508 )	MSF ( 506 ), ARMD ( 531 ), MDKOL ( 526 ), TEB ( 826 ), MDKOG ( 516 ), MDAUTG ( 515 ), GKRA ( 766 ), LLRMR ( 572 ), KHMD ( 894 )
MIGEF_W	LOK	MDFAW ( 508 )	
MIGES_W	AUS	SWADAP ( 47 )	MDKOL ( 526 ), MSF ( 506 )
MIGSL_W	AUS	CAN (1124)	MDKOL ( 526 )
MIGS_W	AUS	CAN (1124)	SWADAP ( 47 ), MDKOG ( 516 ), MSF ( 506 ), ZWMIN ( 669 )
MIISTOAR_W	AUS	MDAUTG ( 515 )	MDFAW ( 508 )
MIIST_W	AUS	MDIST ( 528 )	MSF ( 506 ), VMAXMD ( 588 ), WDKSOM ( 614 )
MILL_W	AUS	MDMIN ( 538 )	LLRMD ( 561 )
MILRES_W	AUS	MDKOL ( 526 )	MDKOG ( 516 )
MILSOL_UM	AUS	UFEING (1058)	UFUE (1056)
MILSOL_W	AUS	MDKOL ( 526 )	FE ( 591 ), FUEDK ( 597 ), UFUE (1056), UFEING (1058), MSF ( 506 ), MD-FUE ( 594 )
MIMAX_W	AUS	MDMAX ( 514 )	MDFAW ( 508 ), MSF ( 506 ), MDKOG ( 516 )
MIMINDS_W	AUS	MDMIN ( 538 )	
MIMINI_W	AUS	MDMIN ( 538 )	
MIMINS_W	LOK	MDMIN ( 538 )	
MIMIN_W	AUS	MDMIN ( 538 )	MDFAW ( 508 ), MSF ( 506 )



Symbol	Type	Created within	Used within
MIMSR_C	EIN		CAN (1124)
MIMSR_W	AUS	CAN (1124)	SWADAP ( 47 ), MDAUTG ( 515 ), MDKOL ( 526 ), MSF ( 506 ), MDKOG ( 516 )
MIMXL1_W	LOK	MDMAX ( 514 )	
MINBEG_W	LOK	MDFAW ( 508 )	
MINMX_W	AUS	NMAXMD ( 584 )	MDAUTG ( 515 ), MDKOG ( 516 ), MSF ( 506 ), MDKOL ( 526 )
MINZAHN	AUS	AZUE ( 904 )	
MIOPTL1_W	LOK	MDBAS ( 529 )	
MIOPT_UM	LOK	UFMIST (1086)	
MIOPT_W	AUS	MDBAS ( 529 )	AES ( 973 ), MSF ( 506 ), MDZW ( 636 ), MDRED ( 976 ), MDKOG ( 516 ), MDIST ( 528 )
MIRE	LOK	VMAXMD ( 588 )	
MIRRORCSP	LOK	RSTMON (1152)	
MIRRORIP	LOK	RSTMON (1152)	
MIRRORTFR	LOK	RSTMON (1152)	
MISGSL_W	AUS	CAN (1124)	MDKOL ( 526 )
MISGS_C	EIN		CAN (1124), DVKUP (1027)
MISGS_UM	LOK	UFSGSC (1070)	
MISGS_W	AUS	CAN (1124)	MDKOG ( 516 )
MISOLP_W	LOK	MDKOG ( 516 )	
MISOLV_W	AUS	MDKOG ( 516 )	ARMD ( 531 ), ZWMIN ( 669 )
MISOL_W	AUS	MDKOG ( 516 )	MSF ( 506 ), AES ( 973 ), MDRED ( 976 ), ZWMIN ( 669 ), MDZW ( 636 )
MISOPL1_W	LOK	MDFUE ( 594 )	
MISTT	EIN		LLRMD ( 561 )
MISZULLB_W	DOK	MDZUL ( 523 )	
MISZULL_W	AUS	MDZUL ( 523 )	MDKOL ( 526 )
MISZUL_W	AUS	MDZUL ( 523 )	MDAUTG ( 515 ), WDKSOM ( 614 ), MSF ( 506 ), MDKOG ( 516 )
MITEBG_W	AUS	GKRA ( 766 )	TEB ( 826 ), MDKOG ( 516 ), MDKOL ( 526 )
MIVBEB_W	EIN		MDAUTG ( 515 ), MDFAW ( 508 )
MIVBEG_W	LOK	MDFAW ( 508 )	
MIVMXS	LOK	VMAXMD ( 588 )	
MIVMX_W	AUS	VMAXMD ( 588 )	MDAUTG ( 515 ), MSF ( 506 ), MDKOG ( 516 ), MDKOL ( 526 )
MIZSOLV_W	AUS	MDKOG ( 516 )	
MIZSOL_W	AUS	MDKOG ( 516 )	MSF ( 506 ), MDZW ( 636 )
MIZUFIL_W	LOK	MDZUL ( 523 )	
MIZUOFIL	LOK	MDZUL ( 523 )	
MIZUVFIL	LOK	MDZUL ( 523 )	
MIZWMN_W	AUS	MDRED ( 976 )	MDAUTG ( 515 ), MDZW ( 636 ), MDFAW ( 508 )
ML_DUF	AUS	DUF (1089)	DFFT (1140)
ML_UM	AUS	UFMIST (1086)	DUF (1089), UFMVER (1087), UFUE (1056)
MKAR_W	AUS	ARMD ( 531 )	
MKFANB_W	AUS	MDFAW ( 508 )	
MKFA_W	LOK	MDFAW ( 508 )	
MKLLSC	EIN		MDVERB ( 540 )
MKOLSC	EIN		MDVERB ( 540 )
ML	AUS	BGSRM ( 245 )	SWADAP ( 47 ), AK ( 855 ), BBKHZ ( 890 ), DFFT ( 1140 ), DKVS ( 811 ), GGTFM ( 289 ), LRHK ( 781 ), ZWMIN ( 669 ), TEB ( 826 ), LRKA ( 795 ), LAKH ( 735 ), DTEV ( 856 ), DKAT ( 361 ), BGMSABG ( 328 ), BGAGR ( 263 )
MLAST_W	AUS	ARMD ( 531 )	
MLBB	AUS	BGMSABG ( 328 )	
MLBB2	AUS	BGMSABG ( 328 )	
MLBB2_W	AUS	BGMSABG ( 328 )	
MLBB_W	AUS	BGMSABG ( 328 )	
MLDMN_W	AUS	DHFM ( 233 )	
MLDMX_W	AUS	DHFM ( 233 )	GGHFM ( 230 )
MLDYN_W	LOK	DLSAHK ( 339 )	
MLETANZS_W	LOK	DTEV ( 856 )	
MLETAN_W	LOK	DTEV ( 856 )	
MLHFMA_S_W	LOK	GGHFM ( 230 )	
MLHFMA_W	LOK	GGHFM ( 230 )	
MLHFMF_W	LOK	DHFM ( 233 )	
MLHFMM_W	AUS	GGHFM ( 230 )	DHFM ( 233 )
MLKGE_W	LOK	FUEDK ( 597 )	
MLNKA2_W	LOK	LRHK ( 781 )	
MLNKA_W	LOK	LRHK ( 781 )	
MLSOL_W	AUS	FUEDK ( 597 )	TEB ( 826 )
MLSU	LOK	BBKHZ ( 890 )	
MLWDKNF_W	LOK	FUEDK ( 597 )	
ML_W	AUS	BGSRM ( 245 )	SWADAP ( 47 ), EGFE ( 228 ), ATM ( 20 ), BGMSABG ( 328 ), BB-BO ( 853 ), TEB ( 826 ), LRKA ( 795 ), LRHK ( 781 ), LREB ( 739 ), LRA ( 797 ), FUEDK ( 597 ), DTEV ( 856 ), DLSAHK ( 339 ), BGRML ( 287 ), BGPU ( 276 ), BGMSZS ( 239 ), BGAGR ( 263 ), AK ( 855 )
MMSR_UM	AUS	UFMSRC (1080)	UFMZUL (1084), UFUE (1056)
MPED_UM	LOK	UFMZUL (1084)	
MPFAD	AUS	DUF (1089)	DFFT (1140)
MRACC_W	EIN		FGRREGL (1174)
MRFABUGD_W	LOK	FUEDK ( 597 )	
MRFAMX_W	AUS	MDFAW ( 508 )	FUEDK ( 597 )
MRF AUGD_W	LOK	FUEDK ( 597 )	
MRF_AW	AUS	MDFAW ( 508 )	ESVW (1009), FUEDK ( 597 ), LAMFAW ( 728 )
MRFGR_C_W	EIN		FGRREGL (1174)
MRFGR_L_W	LOK	FGRREGL (1174)	



Symbol	Type	Created within	Used within
MRFGR_W	AUS	FGRREGL (1174)	SWADAP ( 47 ), FGRUE ( 490 ), MSF ( 506 ), BGWPFGR ( 548 ), FGR-FULO (1160), MDFAW ( 508 ) FGRREGL (1174), MDFAW ( 508 )
MRPED_W	EIN		
MSABG	AUS	BGMSABG ( 328 )	
MSABG2	AUS	BGMSABG ( 328 )	
MSABG2_W	AUS	BGMSABG ( 328 )	DKAT ( 361 )
MSABG_W	AUS	BGMSABG ( 328 )	DKAT ( 361 )
MSAGR	AUS	BGAGR ( 263 )	EGFE ( 228 )
MSDIF_W	AUS	EGFE ( 228 )	
MSDKALM_W	AUS	BGMSZS ( 239 )	TEB ( 826 ), EGFE ( 228 )
MSDKOO_W	LOK	DTEV ( 856 )	
MSDKS_W	LOK	FUEDK ( 597 )	
MSDKUE_W	AUS	BGMSZS ( 239 )	
MSDK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 )
MSGSCPLLUM	LOK	UFSGSC (1070)	
MSGSLUM	AUS	UFSGSC (1070)	
MSGSLJR	AUS	UFSGSC (1070)	
MSG_DATA_R	EIN		UFSGSC (1070)
MSHFMS_W	AUS	GGHFM ( 230 )	
MSHF_W	AUS	GGHFM ( 230 )	BGMSZS ( 239 ), TC1MOD (1100), EGFE ( 228 )
MSL	EIN		BGMSABG ( 328 ), AK ( 855 )
MSL2	EIN		BGMSABG ( 328 )
MSLSTAT	LOK	AK ( 855 )	
MSNDKOOS_W	LOK	FUEDK ( 597 )	
MSNDKOO_W	AUS	BGMSZS ( 239 )	DTEV ( 856 )
MSNDKO_W	AUS	BGMSZS ( 239 )	EGFE ( 228 ), BGRLP ( 266 ), FUEDK ( 597 )
MSNDKPK_W	LOK	BGRLP ( 266 )	
MSNDKS_W	LOK	FUEDK ( 597 )	
MSNDK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 )
MSNLLS_W	EIN		BGMSZS ( 239 ), BGRLP ( 266 )
MSNSAUG_W	AUS	BGMSZS ( 239 )	
MSNTAGR	DOK	BGAGR ( 263 )	
MSNTETEVE_W	LOK	BGTEV ( 257 )	
MSNTEVO_W	AUS	BGTEV ( 257 )	ATEV ( 969 )
MSRC_C_UM	LOK	UFMSRC (1080)	
MSSAUG_W	AUS	BGMSZS ( 239 )	
MSSGINMN_W	LOK	TEB ( 826 )	
MSSGIN_W	LOK	TEB ( 826 )	
MSTE	AUS	BGTEV ( 257 )	BGMSZS ( 239 ), BGRLP ( 266 ), TEB ( 826 ), EGFE ( 228 ), BGPU ( 276 )
MSTEDTE	AUS	BGTEV ( 257 )	DTEV ( 856 )
MSTEDTEFE_W	LOK	DTEV ( 856 )	
MSTEDTE_W	AUS	BGTEV ( 257 )	TEB ( 826 )
MSTEEV_W	LOK	TEB ( 826 )	
MSTEO_W	AUS	BGTEV ( 257 )	ATEV ( 969 ), TEB ( 826 )
MSTESMX_W	LOK	TEB ( 826 )	
MSTESOLL_W	AUS	MSF ( 506 )	TEB ( 826 ), ATEV ( 969 )
MSTETEVE_W	LOK	BGTEV ( 257 )	
MSTE_W	AUS	BGTEV ( 257 )	FUEDK ( 597 ), TEB ( 826 ), GKRA ( 766 )
MTSEGPH_W	LOK	NLDG ( 157 )	
MVER_C_UM	LOK	UFMVER (1087)	
MZFO_UM	LOK	UFMVER (1087)	
MZF_LOW_UM	LOK	UFMZ (1083)	
MZF_UM	AUS	UFMZ (1083)	UFMVER (1087), UFUE (1056)
MZMAX_UM	LOK	UFMZUL (1084)	
MZO_UM	AUS	UFMZUL (1084)	UFMVER (1087), UFUE (1056)
MZ_UM	AUS	UFMZUL (1084)	UFMZ (1083), UFUE (1056)
NASNOTTOM	AUS	MDKOG ( 516 )	MDKOL ( 526 )
NBM	EIN		GGDPG ( 74 )
NC_C_UM	LOK	UFNC (1063)	
NDAR_W	AUS	ARMD ( 531 )	
NDFIL_W	AUS	ARMD ( 531 )	
NDIFFOG_W	AUS	ARMD ( 531 )	
NDIFF_W	AUS	ARMD ( 531 )	
NFSKH	AUS	BBKHZ ( 890 )	SWADAP ( 47 ), LLRNS ( 562 )
NGASF_W	LOK	LLRRM ( 566 )	
NGAS_W	AUS	BGNG ( 121 )	KRDY ( 659 ), LLRRM ( 566 )
NGFIL	AUS	BGNG ( 121 )	SWADAP ( 47 ), BBSAWE ( 557 ), LLRRM ( 566 ), ZWMIN ( 669 ), LLRNS ( 562 )
NGFIL_W	AUS	BGNG ( 121 )	SWADAP ( 47 ), DMDSTP ( 205 ), NMAXMD ( 584 ), MDFAW ( 508 )
NGKRV_W	LOK	KRDY ( 659 )	
NLLCVT1	EIN		LLRNS ( 562 )
NLLCVT2	LOK	LLRNS ( 562 )	
NLLDAGKT	EIN		LLRNFA ( 564 )
NLLKH	AUS	AK ( 855 )	SWADAP ( 47 ), BBKHZ ( 890 ), LLRNS ( 562 ), NWS ( 618 )
NLP1TIM	LOK	BGDVE ( 934 )	
NMAXDVG_W	LOK	NMAXMD ( 584 )	
NMOD_W	AUS	ARMD ( 531 )	



Symbol	Type	Created within	Used within
NMOT	AUS	BGNMOT ( 111 )	SWADAP ( 47 ), ACIFI ( 1013 ), ZWWL ( 638 ), ZWSTT ( 637 ), ZWMIN ( 669 ), ZWGRU ( 634 ), ZUESZ ( 632 ), ZUE ( 627 ), WDKSOM ( 614 ), WANWKKW ( 125 ), VMAXMD ( 588 ), UFUE ( 1056 ), UFNC ( 1063 ), TEB ( 826 ), SU ( 617 ), STADAP ( 684 ), RKT1 ( 979 ), PROKON ( 53 ), NWS ( 618 ), NLPH ( 150 ), NLDG ( 157 ), MSF ( 506 ), MDZUL ( 523 ), MDVERB ( 540 ), MDMIN ( 538 ), MDMAX ( 514 ), MDKOL ( 526 ), MDKOG ( 516 ), MDFUE ( 594 ), MDBGRG ( 530 ), LRKA ( 795 ), LRHK ( 781 ), LREB ( 739 ), LRAEB ( 759 ), LRA ( 797 ), LR ( 768 ), LLRNS ( 562 ), LLRBB ( 575 ), LAMFAW ( 728 ), LAMBTS ( 732 ), LAKH ( 735 ), KRRA ( 639 ), KRKE ( 427 ), KRDY ( 659 ), KOS ( 896 ), GK ( 675 ), GGPED ( 454 ), GGKS ( 412 ), GGHEM ( 230 ), GGDVE ( 477 ), GGDPG ( 74 ), FUEREG ( 595 ), FUEDKSA ( 610 ), FUEDK ( 597 ), FGRREGL ( 1174 ), ESWV ( 1009 ), ESUKA ( 711 ), ESUK ( 699 ), ESSTT ( 679 ), ESGRU ( 678 ), DVFZ ( 500 ), DNWS ( 622 ), DMDSTP ( 205 ), DMDMIL ( 216 ), DMDLUA ( 202 ), DMDLU ( 193 ), DMDFON ( 161 ), DMDDL ( 199 ), DLSA ( 398 ), DKRS ( 437 ), DKRNT ( 445 ), DKAT ( 361 ), DFFTK ( 1142 ), DFFT ( 1140 ), DECJ ( 1013 ), BGMSZS ( 239 ), BGBSZ ( 73 ), BGAGR ( 263 ), BBSTT ( 148 ), BBSAWE ( 557 ), AZUE ( 904 ), ATM ( 20 ), ATEV ( 969 ), BGTEV ( 257 ), BGTEMPK ( 252 ), BGTABST ( 1030 ), BGPU ( 276 ), AK ( 855 ), AEVABU ( 1002 ), ADVE ( 918 ), EGAG ( 486 ), EGFE ( 228 )
NMOTKOR	LOK	GGHEM ( 230 )	
NMOTLL	AUS	BGNMOT ( 111 )	BGDVE ( 934 ), DTEV ( 856 ), LLRBB ( 575 ), FUEREG ( 595 ), BGLBZ ( 489 ), LLRMD ( 561 ), MDVER ( 546 ), RDE ( 112 ), LLRNS ( 562 )
NMOTLLFIL	AUS	BGNMOT ( 111 )	DDG ( 141 )
NMOTPR_W	LOK	NMAXMD ( 584 )	
NMOTRSP_W	AUS	BGNG ( 121 )	
NMOT_UM	AUS	UFNC ( 1063 )	DUF ( 1089 ), UFRLC ( 1066 ), UFMIST ( 1086 ), UFNCS ( 1077 ), UFREAC ( 1088 ), UFUE ( 1056 )
NMOT_W	AUS	BGNMOT ( 111 )	SWADAP ( 47 ), ARMD ( 531 ), ZWMIN ( 669 ), ZUESZ ( 632 ), TEB ( 826 ), TC1MOD ( 1100 ), NMAXMD ( 584 ), MDZW ( 636 ), MDVER ( 546 ), MDNSTAB ( 556 ), MDMIN ( 538 ), MDMAX ( 514 ), MDFUE ( 594 ), MDFAW ( 508 ), MDBAS ( 529 ), LLRRM ( 566 ), LLRMR ( 572 ), LLRMD ( 561 ), KHMD ( 894 ), GGPOEL ( 296 ), GGDPG ( 74 ), FUEDK ( 597 ), FGRUE ( 490 ), FGRABED ( 491 ), ESUK ( 699 ), EGFE ( 228 ), EGAG ( 486 ), CAN ( 1124 ), BGWPFGR ( 548 ), BGSRM ( 245 ), BGRPL ( 266 ), BGPU ( 276 ), BGNG ( 121 ), BGMSZS ( 239 ), BBGANG ( 501 ), DHFM ( 233 )
NMXPR	LOK	NMAXMD ( 584 )	
NOME_C	AUS	DUF ( 1089 )	
NSA	LOK	BBSAWE ( 557 )	
NSACTR	LOK	ESNSWL ( 691 )	ESVST ( 677 )
NSACTR_W	LOK	ESVST ( 677 )	
NSBER_W	EIN		FGRABED ( 491 ), NMAXMD ( 584 )
NSFSMN	LOK	LLRNS ( 562 )	
NSKA_UM	LOK	UFREAC ( 1088 )	
NSLBZ	LOK	LLRNS ( 562 )	
NSLFA	AUS	LLRNFA ( 564 )	LLRNS ( 562 )
NSLLMN	LOK	LLRNS ( 562 )	
NSNF	LOK	LLRNS ( 562 )	
NSOL	AUS	LLRMD ( 561 )	LLRNS ( 562 ), DTEV ( 856 ), MDWAN ( 554 ), MDVER ( 546 ), LLRBB ( 575 )
NSOL_W	EIN		LLRRM ( 566 )
NSST	AUS	LLRNS ( 562 )	
NSTAT	AUS	LLRMD ( 561 )	LLRNS ( 562 ), DDG ( 141 ), MDNSTAB ( 556 ), LLRBB ( 575 ), LLRRM ( 566 )
NSTAT2	AUS	LLRNS ( 562 )	
NSTAT3	LOK	LLRNS ( 562 )	
NSTATFIL	AUS	LLRNS ( 562 )	
NSWRL	LOK	ESNSWL ( 691 )	
NSYNNLPH	LOK	NLPH ( 150 )	
NTURB	LOK	MDWAN ( 554 )	
NTURBV	LOK	MDWAN ( 554 )	
NVER_W	EIN		MDMIN ( 538 )
NVQUOT_W	AUS	BBGANG ( 501 )	
NWE	LOK	BBSAWE ( 557 )	
NWECVT	LOK	BBSAWE ( 557 )	
NWEMA	LOK	BBSAWE ( 557 )	
NWENGA	LOK	BBSAWE ( 557 )	
NZ_UM	LOK	UFNC ( 1063 )	
OFFZ_W	AUS	ZUESZ ( 632 )	
OFFPRINT_W	EIN		FUEDK ( 597 )
OVLCTR	AUS	AZUE ( 904 )	
PA_W	LOK	BGAGR ( 263 )	
PBRINT_W	EIN		BGTEMPK ( 252 )
PBRMP_W	LOK	BGRPL ( 266 )	
PBRP_W	LOK	BGRPL ( 266 )	
PBR_W	AUS	BGSRM ( 245 )	
PDPLD	EIN		FUEDK ( 597 )
PERCNT2_W	LOK	LRHK ( 781 )	
PERCNT_W	LOK	LRHK ( 781 )	
PERMFMA_W	LOK	LR ( 768 )	
PERMFSL_W	LOK	LR ( 768 )	
PH	EIN		GGDPG ( 74 ), WANWKKW ( 125 ), NLDG ( 157 )
PH2	EIN		GGDPG ( 74 ), NLDG ( 157 ), WANWKKW ( 125 )
PHLOSCTR_W	AUS	NLPH ( 150 )	



Symbol	Type	Created within	Used within
PHLSNH	AUS	HLS ( 392 )	DHLSHK ( 1154 )
PHLSNH2	AUS	HLS ( 392 )	DHLSHK ( 1154 )
PHLSNHF	DOK	DHLSVK ( 29 )	DHLSHK ( 1154 )
PHLSNHF2	LOK	DHLSHK ( 1154 )	
PHLSNV	AUS	HLS ( 392 )	DHLSVK ( 29 ), DLSV ( 301 )
PHLSNV2	AUS	HLS ( 392 )	DHLSVK ( 29 ), DLSV ( 301 )
PHLSNVF2	DOK	DHLSVK ( 29 )	
PHPW	LOK	DPH ( 144 )	
PHPW2	LOK	DPH ( 144 )	
PIRGFUE_W	EIN		FUEDK ( 597 )
PIRGRO_W	LOK	BGSRM ( 245 )	
PIRG_W	AUS	BGSRM ( 245 )	EGFE ( 228 ), BGRLP ( 266 ), FUEDK ( 597 ), BGTEMPK ( 252 )
PLSOL	AUS	FUEDK ( 597 )	
PLSOL_W	AUS	FUEDK ( 597 )	
PRG2SU_W	AUS	BGSRM ( 245 )	
PRG3SU_W	AUS	BGSRM ( 245 )	
PRGSU_W	AUS	BGSRM ( 245 )	
PRG_W	AUS	BGSRM ( 245 )	
PS	EIN		BGTEMPK ( 252 )
PSAGR_W	AUS	BGAGR ( 263 )	BGSRM ( 245 ), EGFE ( 228 )
PSDSS_U	AUS	DFFTCNV ( 1143 )	TC1MOD ( 1100 )
PSDSS_W	EIN		BGPU ( 276 ), DFFTCNV ( 1143 ), EGFE ( 228 )
PSES_W	LOK	AES ( 973 )	
PSFG_W	AUS	BGSRM ( 245 )	EGFE ( 228 )
PSL	EIN		LLRNS ( 562 )
PSMPPVDK_W	LOK	BGRLP ( 266 )	
PSMP_W	LOK	BGRLP ( 266 )	
PSMX_W	AUS	BGSRM ( 245 )	EGFE ( 228 )
PSPMX_W	LOK	BGRLP ( 266 )	
PSPU	LOK	TEB ( 826 )	
PSPVDB_W	AUS	BGMSZS ( 239 )	EGFE ( 228 )
PSPVDK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 ), BGPU ( 276 ), FUEDK ( 597 ), BGTEV ( 257 )
PSPVDS_W	AUS	BGMSZS ( 239 )	BGRLP ( 266 )
PSPVMIN_W	LOK	FUEDK ( 597 )	
PSP_W	LOK	BGRLP ( 266 )	
PSRLFUE_W	EIN		FUEDK ( 597 )
PSRLRO_W	LOK	BGSRM ( 245 )	
PSSOL_W	AUS	FUEDK ( 597 )	FE ( 591 )
PSSPVDKB_W	LOK	FUEDK ( 597 )	
PSSPVDK_W	LOK	FUEDK ( 597 )	
PS_W	AUS	BGSRM ( 245 )	EGFE ( 228 ), AES ( 973 ), BGAGR ( 263 ), TEB ( 826 ), BGTEMPK ( 252 ), BGRLP ( 266 ), BGMSZS ( 239 )
PTE	AUS	EGAG ( 486 )	GGDST ( 504 ), GKRA ( 766 ), TEB ( 826 )
PTERW	AUS	GGDST ( 504 )	DDST ( 851 )
PTERW_W	AUS	EGAG ( 486 )	GGDST ( 504 )
PTE_W	AUS	GGDST ( 504 )	
PTV	LOK	LRHK ( 781 )	
PTV2	LOK	LRHK ( 781 )	
PU	AUS	BGPU ( 276 )	AES ( 973 ), DFFT ( 1140 ), TEB ( 826 )
PUANS	LOK	GGHFM ( 230 )	
PU_W	AUS	BGPU ( 276 )	BGAGR ( 263 ), FUEDK ( 597 ), BGSRM ( 245 ), EGFE ( 228 )
PVDK	AUS	BGMSZS ( 239 )	EGFE ( 228 )
PVDKDS	AUS	BGPU ( 276 )	
PVDKDS_W	AUS	BGPU ( 276 )	BGMSZS ( 239 ), BGSRM ( 245 ), EGFE ( 228 )
PVDKR_W	LOK	FUEDK ( 597 )	
PVDK_W	AUS	BGMSZS ( 239 )	EGFE ( 228 ), BGRLP ( 266 ), FUEDK ( 597 )
QMSDYN	LOK	TEB ( 826 )	
QNTNS	LOK	MDWAN ( 554 )	
QTETEMIN	LOK	TEB ( 826 )	
QZZYL	LOK	GGDPG ( 74 )	
R	DOK	GGDPG ( 74 )	
R10MSCTR	EIN		UFSGSC ( 1070 )
RAM_C_JM	LOK	URMEM ( 1044 )	
REAC_C1_JM	LOK	UFREAC ( 1088 )	
REAC_C2_JM	LOK	UFREAC ( 1088 )	
REAC_C_JM	LOK	UFREAC ( 1088 )	
READY	AUS	DIMC ( 1148 )	
REDBAS	AUS	AES ( 973 )	SWADAP ( 47 ), BGEVAB ( 1005 )
REDHYST	LOK	MDRED ( 976 )	
REDIST	AUS	AES ( 973 )	SWADAP ( 47 ), BGEVAB ( 1005 ), MDIST ( 528 ), MDRED ( 976 ), MSF ( 506 ), ZUE ( 627 ), MDZW ( 636 )
REDNEU	LOK	MDRED ( 976 )	
REDSOL	AUS	MDRED ( 976 )	SWADAP ( 47 ), AEVAB ( 980 ), AES ( 973 )
REDSOLR	AUS	AEVAB ( 980 )	
REDSOL_ONE	LOK	AEVAB ( 980 )	
REDZE	LOK	MDRED ( 976 )	
REDZST_W	LOK	MDRED ( 976 )	
RFAGRROH_W	DOK	BGAGR ( 263 )	
RFAGR_W	AUS	BGSRM ( 245 )	BGAGR ( 263 ), FUEDK ( 597 ), BGRLP ( 266 ), BGPU ( 276 ), EGFE ( 228 )
RFGES_W	LOK	BGSRM ( 245 )	
RFRS_W	EIN		FUEDK ( 597 )
RFR_W	EIN		FUEDK ( 597 )



Symbol	Type	Created within	Used within
RINH2_U	AUS	DFFTCNV (1143)	DFFT (1140)
RINH2_W	AUS	GGLSH (318)	DFFTCNV (1143), DHLSHK (1154), DLSH (330)
RINH_U	AUS	DFFTCNV (1143)	DFFT (1140)
RINH_W	AUS	GGLSH (318)	DFFTCNV (1143), DHLSHK (1154), DLSH (330)
RINKFH	LOK	DHLSHK (1154)	
RINKFH2	LOK	DHLSHK (1154)	
RINKFV	DOK	DHLSVK (29)	
RINKFV2	DOK	DHLSVK (29)	
RINOFH2_W	LOK	GGLSH (318)	
RINOFH_W	LOK	GGLSH (318)	
RINOFV2_W	AUS	GGLSV (382)	
RINOFVA2_W	LOK	GGLSV (382)	
RINOFVA_W	LOK	GGLSV (382)	
RINOFV_W	AUS	GGLSV (382)	
RINSH2_W	LOK	DHLSHK (1154)	
RINSH_W	LOK	DHLSHK (1154)	
RINSV2_W	DOK	DHLSVK (29)	
RINSV_W	DOK	DHLSVK (29)	
RINV2_U	AUS	DFFTCNV (1143)	DFFT (1140)
RINV2_W	AUS	GGLSV (382)	DFFTCNV (1143), DLSV (301), DHLSVK (29)
RINV_U	AUS	DFFTCNV (1143)	DFFT (1140)
RINV_W	AUS	GGLSV (382)	DFFTCNV (1143), DHLSVK (29), DLSV (301)
RK2_W	AUS	GK (675)	MSF (506), AES (973), Rkti (979), BGKV (71)
RKA2_W	AUS	GKRA (766)	LRA (797), GK (675)
RKACO_W	EIN		GK (675)
RKAM2_W	LOK	DKVS (811)	
RKAMZS2_W	LOK	DKVS (811)	
RKAMZS_W	LOK	DKVS (811)	
RKAM_W	LOK	DKVS (811)	
RKAT2_W	AUS	LRA (797)	DKVS (811), GKRA (766)
RKAT_W	AUS	LRA (797)	DKVS (811), DTEV (856), GKRA (766)
RKAZ2_W	AUS	LRA (797)	DKVS (811), GKRA (766)
RKAZ_W	AUS	LRA (797)	DKVS (811), DTEV (856), GKRA (766)
RKA_W	AUS	GKRA (766)	LRA (797), GK (675)
RKR	AUS	KRKE (427)	DKRS (437), EGKE (409)
RKRMX	LOK	KRKE (427)	
RKRMX1W	LOK	KRKE (427)	
RKRMX2W	LOK	KRKE (427)	
RKRN_W	LOK	DKRS (437)	
RKRTP	LOK	KRKE (427)	
RKR_TST	AUS	KRKE (427)	
RKTE_W	AUS	GKRA (766)	TEB (826), BGKV (71), GK (675)
RKUKE_W	LOK	ESUK (699)	
RKUKG_W	AUS	ESUK (699)	ESVST (677), GK (675)
RKUKKL_W	LOK	ESUK (699)	
RKUKK_W	AUS	ESUK (699)	
RKUKL_W	LOK	ESUK (699)	
RKUK_W	LOK	ESUK (699)	
RK_W	AUS	GK (675)	MSF (506), AES (973), Rkti (979), BGKV (71)
RL	AUS	BGSRM (245)	SWADAP (47), AK (855), DFFT (1140), DKAT (361), GGKS (412), GGHFM (230), GGDVE (477), ESUKA (711), ESGRU (678), DMDMIL (216), DMDLUA (202), DMDLU (193), DMDFON (161), DMDDLU (199), DLSA (398), DLLR (578), BGTEMPK (252), LRA (797), LR (768), LLRNS (562), LAMBTS (732), LAKH (735), KRRA (639), KRDY (659), GK (675), UFRLC (1066), TEB (826), NWS (618), NLPH (150), MSF (506), MDVERB (540), LRHK (781), LREB (739), ZWMIN (669), ZWGRU (634), UFUE (1056), ESVW (1009), DMDSTP (205), ATM (20), EGFE (228)
RLC_C_UM	LOK	UFRLC (1066)	
RLDKTHP	LOK	DKAT (361)	
RLDKTHP2	LOK	DKAT (361)	
RLDVS_W	AUS	BGMSZS (239)	EGFE (228), BGRLP (266)
RLFGKS_W	LOK	FUEDK (597)	
RLFGS_W	LOK	FUEDK (597)	
RLGAS_W	AUS	BGRLG (274)	DMDSTP (205)
RLIPF_UM	LOK	UFRLC (1066)	
RLIP_UM	LOK	UFRLC (1066)	
RLMAX_W	EIN		MDFUE (594), MDMAX (514), FE (591)
RLMINDP_W	LOK	MDFAW (508)	
RLMIN_W	AUS	MDFUE (594)	MDFAW (508), MDKOG (516)
RLMP_W	LOK	BGRLP (266)	
RLNOTN	LOK	BGMSZS (239)	
RLP	AUS	BGRLP (266)	ESUK (699)
RLP_W	AUS	BGRLP (266)	GK (675), KRDY (659), ESUK (699), ESVST (677)
RLQK_W	LOK	BGPU (276)	
RLQ_W	LOK	BGPU (276)	
RLROHMP_W	LOK	BGRLP (266)	
RLROH_W	AUS	BGMSZS (239)	BGSRM (245), EGFE (228)
RLRSP_W	LOK	BGRLG (274)	
RLRS_W	EIN		FUEDK (597)
RLR_W	EIN		BGPU (276), FUEDK (597)
RLSHK	EIN		NWS (618), SU (617), FE (591)



Symbol	Type	Created within	Used within
RLSNW	LOK	NWS ( 618 )	
RLSNWTM	LOK	NWS ( 618 )	
RLSOL_W	AUS	MDFUE ( 594 )	FUEDK ( 597 ), MDKOG ( 516 ), NWS ( 618 ), FUEREG ( 595 ), FE ( 591 )
RLSP	LOK	ESUKA ( 711 )	
RLSP2	LOK	ESUKA ( 711 )	
RLTEDTE_W	AUS	DTEV ( 856 )	MDFUE ( 594 )
RLTEEV_W	LOK	TEB ( 826 )	
RLUGD_W	LOK	MDMAX ( 514 )	
RLVPPL	LOK	GGDVE ( 477 )	
RLVUGD	LOK	MDMAX ( 514 )	
RLWKS_W	AUS	BGPU ( 276 )	
RLWK_W	LOK	BGPU ( 276 )	
RLW_W	LOK	BGPU ( 276 )	
RLZO_UM	LOK	UFRLC (1066)	
RL_U	AUS	DFFTCNV (1143)	
RL_UM	EIN		UFMIST (1086), UFRLC (1066), UFUE (1056)
RL_W	AUS	BGSRM ( 245 )	SWADAP ( 47 ), EGFE ( 228 ), BGPU ( 276 ), DFFTCNV ( 1143 ), VMAXMD ( 588 ), UFUE ( 1056 ), UFRLC ( 1066 ), MSF ( 506 ), MDVER ( 546 ), MDFAW ( 508 ), MDBAS ( 529 ), KRDY ( 659 ), ZWMIN ( 669 ), FUEREG ( 595 ), FE ( 591 ), BGRLG ( 274 ), BGRLP ( 266 )
RL_W_UM	LOK	UFRLC (1066)	
RML	AUS	BGRML ( 287 )	DFFT ( 1140 )
RMSTEVF_W	LOK	DTEV ( 856 )	
RMSTEVUF_W	LOK	DTEV ( 856 )	
RMSTEV_W	AUS	DTEV ( 856 )	
ROMRSTC_UM	LOK	URROM (1041)	
ROMZ_C_UM	LOK	URMEM (1044)	
RREXT_W	EIN		BGTEMPK ( 252 )
RSTMON_0	LOK	RSTMON (1152)	
RSTMON_1	LOK	RSTMON (1152)	
RSTMON_10	LOK	RSTMON (1152)	
RSTMON_11	LOK	RSTMON (1152)	
RSTMON_2	LOK	RSTMON (1152)	
RSTMON_3	LOK	RSTMON (1152)	
RSTMON_4	LOK	RSTMON (1152)	
RSTMON_5	LOK	RSTMON (1152)	
RSTMON_6	LOK	RSTMON (1152)	
RSTMON_7	LOK	RSTMON (1152)	
RSTMON_8	LOK	RSTMON (1152)	
RSTMON_9	LOK	RSTMON (1152)	
RSTPFAD	AUS	DUR (1052)	DFFT ( 1140 )
RST_TV	AUS	UFREAC (1088)	URMEM (1044), URRAM (1043)
R_BM	DOK	GGDPG ( 74 )	
R_BURN	DOK	STADAP ( 684 )	
R_FLAGS_UM	AUS	UFSGSC (1070)	
R_NBM	AUS	GGDPG ( 74 )	AEKP ( 970 ), BGNMOT ( 111 )
R_NBMNLDG	AUS	NLDG ( 157 )	GGDPG ( 74 )
R_NNLDG	LOK	NLDG ( 157 )	
R_PH	LOK	WANWKW ( 125 )	
R_PH2	LOK	WANWKW ( 125 )	
R_PHNLDG	LOK	NLDG ( 157 )	
R_SYN	AUS	GGDPG ( 74 )	BGAGR ( 263 ), BGRLG ( 274 ), WANWKW ( 125 ), STADAP ( 684 ), RK-TI ( 979 ), MDBAS ( 529 ), MDZW ( 636 ), DMDFON ( 161 ), BGNMOT ( 111 ), BGNG ( 121 ), DMDSB ( 159 )
R_SYNPH	AUS	GGDPG ( 74 )	DDG ( 141 ), DPH ( 144 )
R_SYNPH2	AUS	GGDPG ( 74 )	DPH ( 144 )
R_T1	EIN		ALE ( 136 ), GGLSH ( 318 ), GGLSV ( 382 )
R_T10	EIN		AEKP ( 970 ), AEVABU (1002), ALE ( 136 ), BBKHZ ( 890 ), BBSTT ( 148 ), HLS ( 392 ), GGUB ( 487 ), GGLSV ( 382 ), GGLSH ( 318 ), GGDST ( 504 ), GGDPG ( 74 ), ESUKA ( 711 ), DECJ (1013), MOTAUS (1028), MDFUE ( 594 ), LRHK ( 781 ), LREB ( 739 ), LAMKO ( 729 ), LAMBTS ( 732 ), BGWDKM ( 273 ), BGRLG ( 274 ), BGNMOT ( 111 ), BGNG ( 121 ), ATM ( 20 )
R_T100	EIN		BBKHZ ( 890 ), BBSTT ( 148 ), BGAGR ( 263 ), LAMBTS ( 732 ), HLS ( 392 ), GGUB ( 487 ), GGTFM ( 289 ), GGTFM ( 298 ), GGLSV ( 382 ), GGLSH ( 318 ), ESUKA ( 711 ), RKT ( 979 ), MOTAUS (1028), LRHK ( 781 ), LAMKO ( 729 ), DPH ( 144 ), DHLVK ( 29 ), DHLSHK (1154), DECJ (1013), DDG ( 141 )
R_T1000	EIN		BGKMST (1008)
R_T1S	EIN		AEKP ( 970 ), BGTABST (1030), MOTAUS (1028), GGTFM ( 289 )
R_T20	EIN		BGTEV ( 257 ), STADAP ( 684 )
R_T200	EIN		ATM ( 20 ), DNWKW ( 134 ), DNWS ( 622 ), WANWKW ( 125 )
R_T50	EIN		BGTABST (1030), DHLSHK (1154)
SDWFK_W	LOK	ESUK ( 699 )	
SDWFL_W	LOK	ESUK ( 699 )	
SEN_C95	AUS	GGKS ( 412 )	
SFPBREMS	AUS	GGEGAS ( 474 )	
SFPBWF	AUS	GGPED ( 454 )	
SFPCAS	AUS	DCAS (1128)	
SFPCINS	AUS	DCINS (1126)	
SFPCKUP	LOK	DCKUP (1128)	
SFPDK	EIN		DDVE ( 950 )
SFPDK1P	EIN		DDVE ( 950 )
SFPDK2P	EIN		DDVE ( 950 )



Symbol	Type	Created within	Used within
SFPDVEE	EIN		DDVE ( 950 )
SFPDVEF	EIN		DDVE ( 950 )
SFPDVEFO	EIN		DDVE ( 950 )
SFPDVEL	EIN		DDVE ( 950 )
SFPDVEN	EIN		DDVE ( 950 )
SFPDVER	EIN		DDVE ( 950 )
SFPDVET	EIN		DDVE ( 950 )
SFPDVEU	EIN		DDVE ( 950 )
SFPDVEUB	EIN		DDVE ( 950 )
SFPDVEUW	EIN		DDVE ( 950 )
SFPDVEV	EIN		DDVE ( 950 )
SFPFP1P	AUS	GGPED ( 454 )	
SFPFP2P	AUS	GGPED ( 454 )	
SFPFPP	AUS	GGPED ( 454 )	
SFPHSH	AUS	DHLSHK ( 1154 )	
SFPHSH2	AUS	DHLSHK ( 1154 )	
SFPHSV	AUS	DHLSVK ( 29 )	
SFPHSV2	AUS	DHLSVK ( 29 )	
SFPKAT	AUS	DKAT ( 361 )	
SFPKAT2	AUS	DKAT ( 361 )	
SFPKRNT	AUS	DKRNT ( 445 )	
SFPKROF	AUS	DKRNT ( 445 )	
SFPKRTP	AUS	DKRTP ( 451 )	
SFPKS1	AUS	DKRS ( 437 )	
SFPKS2	AUS	DKRS ( 437 )	
SFPKS3	AUS	DKRS ( 437 )	
SFPKS4	AUS	DKRS ( 437 )	
SFPLASH	AUS	DLSAHK ( 339 )	
SFPLASH2	AUS	DLSAHK ( 339 )	
SFPLATP	AUS	DLSA ( 398 )	
SFPLATP2	AUS	DLSA ( 398 )	
SFPLATV	AUS	DLSA ( 398 )	
SFPLATV2	AUS	DLSA ( 398 )	
SFPLM	AUS	DHFM ( 233 )	
SFPLSH	AUS	DLSH ( 330 )	
SFPLSH2	AUS	DLSH ( 330 )	
SFPLSV	AUS	DLSV ( 301 )	
SFPLSV2	AUS	DLSV ( 301 )	
SFPMDB	AUS	MDKOG ( 516 )	
SFPMILE	AUS	DMILE ( 36 )	
SFPNWKW	AUS	DNWKW ( 134 )	
SFPNWKW2	AUS	DNWKW ( 134 )	
SFPNWS	AUS	DNWS ( 622 )	
SFPNWS2	AUS	DNWS ( 622 )	
SFPPH	AUS	DPH ( 144 )	
SFPPH2	AUS	DPH ( 144 )	
SFPTA	AUS	GGTFA ( 298 )	
SFPTES	AUS	DTEV ( 856 )	
SFPTM	AUS	GGTFM ( 289 )	
SFPUB	AUS	GGUB ( 487 )	
SFPUFMV	AUS	DUF ( 1089 )	
SFPUFKA	AUS	DUF ( 1089 )	
SFPURRAM	AUS	DUR ( 1052 )	
SFPURROM	AUS	DUR ( 1052 )	
SFPURRST	AUS	DUR ( 1052 )	
SFPVKUP	LOK	DVKUP ( 1027 )	
SGID	EIN		AEVAB ( 980 ), BGEVAB ( 1005 )
SGSC.C_UM	LOK	UFSGSC ( 1070 )	
SGSC.C_UR	LOK	UFSGSC ( 1070 )	
SGSNU.C_UM	LOK	UFSGSC ( 1070 )	
SGSNU.C_UR	LOK	UFSGSC ( 1070 )	
SKAPFAD	AUS	DUF ( 1089 )	DFFT ( 1140 )
SLSNINKR	AUS	AZUE ( 904 )	
SLSNINKR2	AUS	AZUE ( 904 )	
SLSNZAHN	AUS	AZUE ( 904 )	
SLSNZAHN2	AUS	AZUE ( 904 )	
SN2ZKVEK	AUS	AZUE ( 904 )	
SNZKVEK	AUS	AZUE ( 904 )	
SP1P_A_UM	LOK	URADCC ( 1049 )	
SP1P_ST_UM	LOK	URADCC ( 1049 )	
SP1SN_UM	LOK	UFSPSC ( 1060 )	
SP1S_A_UM	LOK	URADCC ( 1049 )	
SP1S_ST_UM	LOK	URADCC ( 1049 )	
SP1S_UM	LOK	UFSPSC ( 1060 )	
SP2SN_UM	LOK	UFSPSC ( 1060 )	
SP2S_UM	LOK	UFSPSC ( 1060 )	
SPSC.C_UM	LOK	UFSPSC ( 1060 )	
SPSN_UM	AUS	UFSPSC ( 1060 )	UFMET ( 1060 ), UFREAC ( 1088 ), UFUE ( 1056 )
SPSN_UM.C	AUS	UFMER ( 1060 )	
SRST.C_UM	LOK	URMEM ( 1044 )	
SRST_UR	AUS	UFSGSC ( 1070 )	
STACTR	LOK	STADAP ( 684 )	





Symbol	Type	Created within	Used within
STATEAEVAB	AUS	AEVAB ( 980 )	BGEVAB (1005)
STATEQSYN	LOK	GGDPG ( 74 )	
STAT_MD_E	AUS	CAN (1124)	
STFGRAB_W	AUS	FGRABED ( 491 )	FGRFULO (1160), FGRREGL (1174), FGRUE ( 490 )
STFGRBS_W	AUS	FGRBESI (1158)	FGRFULO (1160), FGRUE ( 490 )
STFGRFL	AUS	FGRFULO (1160)	FGRREGL (1174), FGRUE ( 490 )
STKRAX	LOK	KRRA ( 639 )	
STKRLX	LOK	KRRA ( 639 )	
STKRNX	AUS	KRRA ( 639 )	KRDY ( 659 ), EGKE ( 409 )
SUMODE	AUS	SU ( 617 )	BGRSM ( 245 ), EGFE ( 228 )
SWOUT	AUS	AZUE ( 904 )	
SYNSTATE	EIN		GGDPG ( 74 ), NLPH ( 150 ), RDE ( 112 )
SY_2SG	AUS	PROKON ( 53 )	ADVE ( 918 ), SREAKT ( 963 ), DMDUE ( 158 ), DMDTSB ( 159 ), DMD-LUA ( 202 ), DMDLU ( 193 ), DMDLAD ( 215 ), DMDDL ( 199 ), BGDVE ( 934 )
SY_2SLS	EIN		LRHK ( 781 )
SY_2TEV	EIN		LRHK ( 781 )
SY_AAU	AUS	PROKON ( 53 )	
SY_AAV	AUS	PROKON ( 53 )	DTEV ( 856 ), TEBEB ( 762 )
SY_AGR	AUS	PROKON ( 53 )	
SY_AIRBAG	AUS	PROKON ( 53 )	AEKP ( 970 )
SY_ATR	AUS	PROKON ( 53 )	LAMKO ( 729 )
SY_BLOOP	EIN		BGDVE ( 934 )
SY_CAN	AUS	PROKON ( 53 )	
SY_CDCCSIZE	AUS	PROKON ( 53 )	
SY_CDKSIZE	AUS	PROKON ( 53 )	
SY_CDTSIZE	AUS	PROKON ( 53 )	
SY_CLASIZE	AUS	PROKON ( 53 )	
SY_CONFSL	AUS	PROKON ( 53 )	
SY_DELFCMS	AUS	PROKON ( 53 )	SCATT (1097)
SY_DFPMENTV	EIN		DFPM (1132)
SY_DFPMTIM	AUS	PROKON ( 53 )	DFPM (1132)
SY_DFPMPVAR	AUS	PROKON ( 53 )	DFPM (1132)
SY_DGANZ	AUS	PROKON ( 53 )	
SY_DLS	AUS	PROKON ( 53 )	
SY_DOPZW	AUS	PROKON ( 53 )	
SY_DTANKL	AUS	PROKON ( 53 )	
SY_DVEADA	AUS	PROKON ( 53 )	
SY_EGAS	AUS	PROKON ( 53 )	LREB ( 739 )
SY_EGFE	AUS	PROKON ( 53 )	
SY_ENVBLOK	EIN		DFPM (1132)
SY_FCMSIZE	AUS	PROKON ( 53 )	DFPM (1132)
SY_FFCSIZE	AUS	PROKON ( 53 )	
SY_FFESIZE	AUS	PROKON ( 53 )	DFPM (1132)
SY_FFTSIZE	AUS	PROKON ( 53 )	
SY_FLUQ	AUS	PROKON ( 53 )	
SY_FREQCPU	AUS	PROKON ( 53 )	DMDTSB ( 159 )
SY_GAP	AUS	PROKON ( 53 )	ALE ( 136 ), GGDPG ( 74 ), WANWKW ( 125 ), NLDG ( 157 )
SY_GDWRT	EIN		ALE ( 136 )
SY_GGGTS	AUS	PROKON ( 53 )	
SY_GRDWRT	AUS	PROKON ( 53 )	DMDTSB ( 159 )
SY_HYBRID	AUS	PROKON ( 53 )	
SY_JNGASOS	LOK	BGN ( 121 )	
SY_JSOPROT	AUS	PROKON ( 53 )	
SY_KMTR	AUS	PROKON ( 53 )	
SY_KOAC	EIN		KOS ( 896 )
SY_KS1	AUS	PROKON ( 53 )	
SY_KS2	AUS	PROKON ( 53 )	
SY_KS3	AUS	PROKON ( 53 )	
SY_KS4	AUS	PROKON ( 53 )	
SY_KWP71	AUS	PROKON ( 53 )	
SY_LAMBTS	AUS	PROKON ( 53 )	LAMBTS ( 732 )
SY_LLR	AUS	PROKON ( 53 )	
SY_M1I00A	AUS	PROKON ( 53 )	TC1MOD (1100)
SY_M1I00B	AUS	PROKON ( 53 )	TC1MOD (1100)
SY_M1I00C	AUS	PROKON ( 53 )	TC1MOD (1100)
SY_M1I00D	AUS	PROKON ( 53 )	TC1MOD (1100)
SY_M1I20A	EIN		TC1MOD (1100)
SY_M1I20B	EIN		TC1MOD (1100)
SY_M1I20C	EIN		TC1MOD (1100)
SY_M1I20D	EIN		TC1MOD (1100)
SY_M2I00A	AUS	PROKON ( 53 )	TC2MOD (1107)
SY_M2I00B	AUS	PROKON ( 53 )	TC2MOD (1107)
SY_M2I00C	AUS	PROKON ( 53 )	TC2MOD (1107)
SY_M2I00D	AUS	PROKON ( 53 )	TC2MOD (1107)
SY_M5IH00A	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH00B	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH00C	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH00D	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH20A	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH20B	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH20C	AUS	PROKON ( 53 )	TC5MOD (1110)
SY_M5IH20D	AUS	PROKON ( 53 )	TC5MOD (1110)



Symbol	Type	Created within	Used within
SY_M5IH40A	AUS	PROKON ( 53 )	
SY_M5IH40B	AUS	PROKON ( 53 )	
SY_M5IH40C	AUS	PROKON ( 53 )	
SY_M5IH40D	AUS	PROKON ( 53 )	
SY_M5IH60A	AUS	PROKON ( 53 )	
SY_M5IH60B	AUS	PROKON ( 53 )	
SY_M5IH60C	AUS	PROKON ( 53 )	
SY_M5IH60D	AUS	PROKON ( 53 )	
SY_M5IH80A	AUS	PROKON ( 53 )	
SY_M5IH80B	AUS	PROKON ( 53 )	
SY_M5IH80C	AUS	PROKON ( 53 )	
SY_M5IH80D	AUS	PROKON ( 53 )	
SY_M5IV00A	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV00B	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV00C	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV00D	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV20A	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV20B	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV20C	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV20D	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV40A	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV40B	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV40C	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV40D	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV60A	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV60B	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV60C	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV60D	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV80A	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV80B	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV80C	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M5IV80D	AUS	PROKON ( 53 )	TC5MOD ( 1110 )
SY_M6I00A	AUS	PROKON ( 53 )	TC6MOD ( 1112 )
SY_M6I00B	AUS	PROKON ( 53 )	TC6MOD ( 1112 )
SY_M6I00C	AUS	PROKON ( 53 )	TC6MOD ( 1112 )
SY_M6I00D	AUS	PROKON ( 53 )	TC6MOD ( 1112 )
SY_M7VAR	EIN		SCATT ( 1097 )
SY_M8I00A	AUS	PROKON ( 53 )	
SY_M8I00B	AUS	PROKON ( 53 )	SCATT ( 1097 ), TC8MOD ( 1120 )
SY_M8I00C	AUS	PROKON ( 53 )	SCATT ( 1097 ), TC8MOD ( 1120 )
SY_M8I00D	AUS	PROKON ( 53 )	SCATT ( 1097 ), TC8MOD ( 1120 )
SY_M8I00E	AUS	PROKON ( 53 )	SCATT ( 1097 ), TC8MOD ( 1120 )
SY_M9I00A	EIN		SCATT ( 1097 ), TC9MOD ( 1121 )
SY_M9I00B	EIN		SCATT ( 1097 ), TC9MOD ( 1121 )
SY_M9I00C	EIN		SCATT ( 1097 ), TC9MOD ( 1121 )
SY_M9I00D	EIN		SCATT ( 1097 ), TC9MOD ( 1121 )
SY_MAX_EV	AUS	PROKON ( 53 )	
SY_NLDG	AUS	PROKON ( 53 )	GGDPG ( 74 )
SY_NWS	AUS	PROKON ( 53 )	DNWS ( 622 ), MDBAS ( 529 ), ZWGRU ( 634 ), WANWKW ( 125 ), VS_VERST ( 67 )
SY_NZUEB	AUS	PROKON ( 53 )	
SY_PBRPW	AUS	PROKON ( 53 )	
SY_PGRAD	AUS	PROKON ( 53 )	
SY_PGRAD2	AUS	PROKON ( 53 )	DPH ( 144 ), GGDPG ( 74 ), WANWKW ( 125 )
SY_PGTP	EIN		DDG ( 141 ), DPH ( 144 ), GGDPG ( 74 ), WANWKW ( 125 ), DNWKW ( 134 )
SY_PH2OFST	AUS	PROKON ( 53 )	GGDPG ( 74 )
SY_PHTWIN	AUS	PROKON ( 53 )	DPH ( 144 ), GGDPG ( 74 )
SY_REDMX	AUS	PROKON ( 53 )	DNWS ( 622 )
SY_SGANZ	AUS	PROKON ( 53 )	
SY_STEREO	AUS	PROKON ( 53 )	GGDPG ( 74 )
SY_STERHK	AUS	PROKON ( 53 )	DHLSHK ( 1154 ), DLSA ( 398 ), HLS ( 392 ), LR ( 768 ), LRHK ( 781 ), LREB ( 739 ), TC6MOD ( 1112 ), TC1MOD ( 1100 ), LRKA ( 795 ), GGLSH ( 318 ), DLSAHK ( 339 )
SY_STERSY	AUS	PROKON ( 53 )	DLSA ( 398 ), LRKA ( 795 ), LRHK ( 781 ), LR ( 768 )
SY_STERVK	AUS	PROKON ( 53 )	DHLSVK ( 29 ), DHLVKE ( 902 ), DKVS ( 811 ), TC6MOD ( 1112 ), TC2MOD ( 1107 ), TC1MOD ( 1100 ), RKTl ( 979 ), LRKA ( 795 ), LRHK ( 781 ), LREB ( 739 ), LR ( 768 ), LAMKO ( 729 ), LAKH ( 735 ), HLS ( 392 ), GGLSV ( 382 ), ESUKA ( 711 ), DLSA ( 398 )
SY_STETLR	AUS	PROKON ( 53 )	DLSSA ( 350 ), TC6MOD ( 1112 ), GGLSV ( 382 ), LAKH ( 735 )
SY_SU	AUS	PROKON ( 53 )	
SY_SWE_S	AUS	PROKON ( 53 )	
SY_TAGR	AUS	PROKON ( 53 )	
SY_TCNS	AUS	PROKON ( 53 )	
SY_TDZW	AUS	PROKON ( 53 )	
SY_TEBF	AUS	PROKON ( 53 )	
SY_TEETH	AUS	PROKON ( 53 )	AEKP ( 970 )
SY_TFA	AUS	PROKON ( 53 )	ALE ( 136 ), GGDPG ( 74 ), NLDG ( 157 ), BGNMOT ( 111 )
SY_TFBA	AUS	PROKON ( 53 )	
SY_TFMA	AUS	PROKON ( 53 )	GGTFM ( 289 )
SY_TFMAP	AUS	PROKON ( 53 )	GGTFA ( 298 )
SY_TFMHST	EIN		GGTFM ( 289 )
SY_TFMO	AUS	PROKON ( 53 )	GGTFM ( 289 )



Symbol	Type	Created within	Used within
SY_TFNS	AUS	PROKON ( 53 )	
SY_TFRK	AUS	PROKON ( 53 )	ESGRU ( 678 )
SY_TFST	AUS	PROKON ( 53 )	
SY_TFUMG	AUS	PROKON ( 53 )	GGTFM ( 289 )
SY_TFVA	AUS	PROKON ( 53 )	
SY_TFWL	AUS	PROKON ( 53 )	
SY_TLR	AUS	PROKON ( 53 )	LR ( 768 )
SY_TMDR	AUS	PROKON ( 53 )	
SY_TN	AUS	PROKON ( 53 )	
SY_TNLS	AUS	PROKON ( 53 )	
SY_TRLX	AUS	PROKON ( 53 )	
SY_TSFSIZE	AUS	PROKON ( 53 )	
SY_TURBO	AUS	PROKON ( 53 )	LAMFAW ( 728 ), VS_VERST ( 67 ), MDMAX ( 514 ), MDFUE ( 594 )
SY_TVVR	AUS	PROKON ( 53 )	VMAXMD ( 588 )
SY_TWDKS	EIN		ADVE ( 918 ), BGDVE ( 934 )
SY_UB13V	AUS	PROKON ( 53 )	
SY_UBDEDIS	AUS	PROKON ( 53 )	ADVE ( 918 )
SY_UBDEEN	AUS	PROKON ( 53 )	ADVE ( 918 )
SY_UBKL15	EIN		GGUB ( 487 )
SY_UBOKDIS	AUS	PROKON ( 53 )	
SY_UBOKEN	AUS	PROKON ( 53 )	
SY_UBR	AUS	PROKON ( 53 )	BGDVE ( 934 ), GGUB ( 487 ), SREAKT ( 963 )
SY_UBSQ_W	EIN		BGDVE ( 934 ), GGUB ( 487 )
SY_UMALS	AUS	PROKON ( 53 )	
SY_USOFF	AUS	PROKON ( 53 )	
SY_VS	EIN		LREB ( 739 )
SY_WMAX	AUS	PROKON ( 53 )	
SY_WMIN	AUS	PROKON ( 53 )	
SY_WNBM	AUS	PROKON ( 53 )	ALE ( 136 ), NLDG ( 157 ), WANWKW ( 125 )
SY_ZAS	AUS	PROKON ( 53 )	
SY_ZNDAUS	AUS	PROKON ( 53 )	
SY_ZSGMT	EIN		KRRA ( 639 )
SY_ZYLZA	AUS	PROKON ( 53 )	WANWKW ( 125 )
SY_ZZBANK	AUS	PROKON ( 53 )	ALE ( 136 ), GGDPG ( 74 ), BGNMOT ( 111 ), BGR LG ( 274 ), BNGG ( 121 )
SZFUBA_W	AUS	ZUESZ ( 632 )	
SZOUT_W	AUS	MSF ( 506 )	ZUESZ ( 632 ), AZUE ( 904 )
SZTCALC_W	AUS	ZUESZ ( 632 )	
S_AC	EIN		KOS ( 896 ), LLRNS ( 562 )
S_ASR	AUS	CAN ( 1124 )	
S_BLS	EIN		EGEG ( 453 ), GGEGAS ( 474 ), UFFGRE ( 1096 )
S_BRS	EIN		EGEG ( 453 ), UFFGRE ( 1096 ), GGEGAS ( 474 )
S_FGRHS	EIN		UFFGRE ( 1096 )
S_FGRSB	EIN		UFFGRE ( 1096 )
S_FGRSV	EIN		UFFGRE ( 1096 )
S_FGRWA	EIN		UFFGRE ( 1096 )
S_FS	AUS	SWADAP ( 47 )	BBGANG ( 501 ), MDWAN ( 554 )
S_KO	AUS	SWADAP ( 47 )	LLRNS ( 562 )
S_KUPP	EIN		EGEG ( 453 ), GGEGAS ( 474 )
S_ML1	EIN		LFS ( 69 )
S_ML2	EIN		LFS ( 69 )
S_MSR	AUS	CAN ( 1124 )	
S_POEL	EIN		GGPOEL ( 296 )
T	EIN		BGNMOT ( 111 ), NLDG ( 157 ), WANWKW ( 125 ), GGDPG ( 74 )
TABGM	AUS	ATM ( 20 )	DFFT ( 1140 ), DHLSVK ( 29 ), DLSA ( 398 ), DLSV ( 301 ), HLS ( 392 ), DL-SAHK ( 339 )
TABGM2	AUS	ATM ( 20 )	DFFT ( 1140 ), DLSV ( 301 ), DLSAHK ( 339 ), HLS ( 392 ), DLSA ( 398 ), DHLSVK ( 29 )
TABGM2_W	AUS	ATM ( 20 )	
TABGMAB	LOK	ATM ( 20 )	
TABGMAB2	LOK	ATM ( 20 )	
TABGMF	DOK	DHLSVK ( 29 )	
TABGMST	LOK	ATM ( 20 )	
TABGMST2	LOK	ATM ( 20 )	
TABGM_W	AUS	ATM ( 20 )	BGTEMPK ( 252 ), LAMBTS ( 732 )
TABGSANT_W	LOK	BGTEMPK ( 252 )	
TABSMN_W	LOK	BGTABST ( 1030 )	
TABSNL_W	LOK	BGTABST ( 1030 )	
TABSSC_W	LOK	BGTABST ( 1030 )	
TABST	EIN		AK ( 855 )
TABSTATM	LOK	ATM ( 20 )	
TABSTMX_W	LOK	ATM ( 20 )	
TABSTM_W	LOK	BGTABST ( 1030 )	
TABST_W	AUS	BGTABST ( 1030 )	AEKP ( 970 ), ATM ( 20 ), ESSTT ( 679 ), GGTFM ( 289 ), WDKSOM ( 614 ), ESNSWL ( 691 )
TADTEA	AUS	DTEV ( 856 )	ATEV ( 969 ), GKRA ( 766 )
TADTEAZS	LOK	DTEV ( 856 )	
TAGAV	DOK	BGAGR ( 263 )	
TAGRV	LOK	BGAGR ( 263 )	
TAGRV_W	DOK	BGAGR ( 263 )	
TAGS_W	AUS	BGAGR ( 263 )	EGFE ( 228 ), BGTEMPK ( 252 )
TAKOLS	EIN		MDVERB ( 540 )
TALT_UJM	LOK	UFNC ( 1063 )	



Symbol	Type	Created within	Used within
TANKFST	EIN		GGFST ( 502 )
TANS	AUS	GGTFA ( 298 )	SWADAP ( 47 ), AK ( 855 ), BBKHZ ( 890 ), BGAGR ( 263 ), BGDVE ( 934 ), BGTEMPK ( 252 ), DLLR ( 578 ), DFFT ( 1140 ), ZWWL ( 638 ), ZWSTT ( 637 ), WDKSOM ( 614 ), UFUE ( 1056 ), UFEING ( 1058 ), TEB ( 826 ), SU ( 617 ), NWS ( 618 ), MDZUL ( 523 ), MDVERB ( 540 ), LREB ( 739 ), LRAEB ( 759 ), LLRNS ( 562 ), LLRMR ( 572 ), KOS ( 896 ), GGTFM ( 289 ), GGHEM ( 230 ), ESSTT ( 679 ), ESNWL ( 691 ), EGFE ( 228 ), DMDSTP ( 205 ), BGTABST ( 1030 ), BBSTT ( 148 ), BBTEGA ( 750 ), ATM ( 20 )
TANSAB	AUS	GGTFA ( 298 )	ESSTT ( 679 ), GGTFM ( 289 )
TANSABK_W	AUS	GGTFA ( 298 )	
TANSK_W	AUS	GGTFA ( 298 )	
TANSLIN	AUS	GGTFA ( 298 )	TC1MOD ( 1100 )
TANSST	LOK	LREB ( 739 )	
TANSJUM	AUS	UFEING ( 1058 )	UFNSC ( 1077 ), UFUE ( 1056 )
TAS_W	LOK	BGRLG ( 274 )	
TATEIST	LOK	BGTEV ( 257 )	
TATEOUT	AUS	ATEV ( 969 )	DTEV ( 856 ), DTEVE ( 1022 )
TATESLO1	LOK	BGTEV ( 257 )	
TATESLO2	LOK	BGTEV ( 257 )	
TATESLO3	LOK	BGTEV ( 257 )	
TATESOLL	AUS	ATEV ( 969 )	GKRA ( 766 ), BGTEV ( 257 ), GKEB ( 737 ), TEBEB ( 762 )
TATMKF	LOK	ATM ( 20 )	
TATMKF2	LOK	ATM ( 20 )	
TATMSTA	LOK	ATM ( 20 )	
TATMSTA2	LOK	ATM ( 20 )	
TATU	LOK	ATM ( 20 )	
TAVHKM_W	EIN		BBSAWE ( 557 )
TAVVKM_W	EIN		BBSAWE ( 557 )
TBRRAJUM_W	LOK	BGTEMPK ( 252 )	
TC6KATA	AUS	DKAT ( 361 )	
TC6KATC	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6KATC2	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6KATS	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6KATS2	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6KATW	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6KATW2	AUS	DKAT ( 361 )	TC6MOD ( 1112 )
TC6LDPC	EIN		TC6MOD ( 1112 )
TC6LDPS	EIN		TC6MOD ( 1112 )
TC6LDPW	EIN		TC6MOD ( 1112 )
TC6TESC	AUS	DTEV ( 856 )	TC6MOD ( 1112 )
TC6TESS	AUS	DTEV ( 856 )	TC6MOD ( 1112 )
TC6TESW	AUS	DTEV ( 856 )	TC6MOD ( 1112 )
TCAPJUM	LOK	UFNC ( 1063 )	
TDDSTST	DOK	DDST ( 851 )	
TDIFJUM	LOK	UFNC ( 1063 )	
TDKNACH_W	LOK	BGDVE ( 934 )	
TDLRTM	AUS	GGTFM ( 289 )	
TDTESTA	LOK	DTEV ( 856 )	
TDTEVEVO	LOK	DTEV ( 856 )	
TE2_W	EIN		TEB ( 826 )
TEMPIN	LOK	BGTEMPK ( 252 )	
TEPHC	LOK	BBTEGA ( 750 )	
TEVPER	AUS	ATEV ( 969 )	BGTEV ( 257 )
TEVPERO1	LOK	BGTEV ( 257 )	
TEVPERO2	LOK	BGTEV ( 257 )	
TEVPERO3	LOK	BGTEV ( 257 )	
TEVPERVZ	LOK	BGTEV ( 257 )	
TEXOIKM2_W	LOK	ATM ( 20 )	
TEXOIKM_W	LOK	ATM ( 20 )	
TEXOM2_W	LOK	ATM ( 20 )	
TEXOM_W	LOK	ATM ( 20 )	
TE_W	EIN		BGRLP ( 266 ), TEB ( 826 )
TFETTIF_W	LOK	LR ( 768 )	
TFETTIMA_W	LOK	LR ( 768 )	
TFETTIM_W	LOK	LR ( 768 )	
TFETTMA_W	LOK	LR ( 768 )	
TFETTSL_W	LOK	LR ( 768 )	
TFRGSANT_W	LOK	BGTEMPK ( 252 )	
TFRN2_W	AUS	LR ( 768 )	DLSA ( 398 ), DLSSA ( 350 )
TFRNINT2_W	LOK	LR ( 768 )	
TFRNINT_W	LOK	LR ( 768 )	
TFRN_W	AUS	LR ( 768 )	DLSA ( 398 ), DLSSA ( 350 )
TFRP2_W	EIN		DLSA ( 398 ), LR ( 768 )
TFRPINT2_W	LOK	LR ( 768 )	
TFRPINT_W	LOK	LR ( 768 )	
TFRP_W	EIN		DLSA ( 398 ), LR ( 768 )
TFST	AUS	GGFST ( 502 )	DFFT ( 1140 ), DMDMIL ( 216 )
TFWDKSOM_W	AUS	WDKSOM ( 614 )	FUEDK ( 597 )
TFWDKS_W	LOK	FUEDK ( 597 )	
THHAIST	LOK	HLS ( 392 )	
THHAIST2	LOK	HLS ( 392 )	
THHAT	LOK	HLS ( 392 )	



Symbol	Type	Created within	Used within
THHAT2	LOK	HLS ( 392 )	
THVAIST	LOK	HLS ( 392 )	
THVAIST2	LOK	HLS ( 392 )	
THVAT	LOK	HLS ( 392 )	
THVAT2	LOK	HLS ( 392 )	
TI2.W	AUS	RKTI ( 979 )	
TIKATM	AUS	ATM ( 20 )	DKAT ( 361 ), LRHK ( 781 )
TIKATM2	AUS	ATM ( 20 )	DKAT ( 361 ), LRHK ( 781 )
TIKATM2.W	AUS	ATM ( 20 )	
TIKATM.W	AUS	ATM ( 20 )	
TIMMOT	EIN		DCKUP ( 1128 )
TIMMOT.W	EIN		DCAS ( 1128 ), DCINS ( 1126 ), DVKUP ( 1027 )
TINKR	AUS	AZUE ( 904 )	
TISPLDPX.W	EIN		DTEV ( 856 )
TISPLDP.W	EIN		DTEV ( 856 )
TI.B1	AUS	RKTI ( 979 )	ACIFI ( 1013 ), AES ( 973 )
TI.B2	AUS	RKTI ( 979 )	ACIFI ( 1013 ), AES ( 973 )
TI.EV0	AUS	ACIFI ( 1013 )	AES ( 973 )
TI.EV1	LOK	AES ( 973 )	
TI.EV7	AUS	AES ( 973 )	
TI.EV8	LOK	AES ( 973 )	
TI.TVU.W	AUS	RKTI ( 979 )	ACIFI ( 1013 ), AES ( 973 )
TI.W	AUS	RKTI ( 979 )	
TKATM	AUS	ATM ( 20 )	AK ( 855 ), DFFT ( 1140 ), DHLSHK ( 1154 ), DKAT ( 361 ), DLSH ( 330 ), HLS ( 392 ), BBSAWE ( 557 ), LRHK ( 781 ), BBKHZ ( 890 )
TKATM2	AUS	ATM ( 20 )	DFFT ( 1140 ), LRHK ( 781 ), HLS ( 392 ), DLSH ( 330 ), DHLSHK ( 1154 ), DKAT ( 361 )
TKATM2.W	AUS	ATM ( 20 )	LRKA ( 795 )
TKATMAB	LOK	ATM ( 20 )	
TKATMAB2	LOK	ATM ( 20 )	
TKATMF	LOK	DHLSHK ( 1154 )	
TKATMF2	LOK	DHLSHK ( 1154 )	
TKATMST	LOK	ATM ( 20 )	
TKATMST2	LOK	ATM ( 20 )	
TKATM.W	AUS	ATM ( 20 )	LRKA ( 795 )
TKDKTE	LOK	DKAT ( 361 )	
TKDKTE2	LOK	DKAT ( 361 )	
TKDKTH	LOK	DKAT ( 361 )	
TKDKTH2	LOK	DKAT ( 361 )	
TKDKTHP	LOK	DKAT ( 361 )	
TKDKTHP2	LOK	DKAT ( 361 )	
TLFSAR.W	LOK	LFS ( 69 )	
TLOK	LOK	MDVERB ( 540 )	
TLOOP	LOK	BGDVE ( 934 )	
TMADB	LOK	STADAP ( 684 )	
TMAGERMA.W	LOK	LR ( 768 )	
TMAGERSL.W	LOK	LR ( 768 )	
TMAGRIF.W	LOK	LR ( 768 )	
TMAGRIMA.W	LOK	LR ( 768 )	
TMAGRIM.W	LOK	LR ( 768 )	
TMCORCTR.W	AUS	GGDPG ( 74 )	
TMEW	AUS	GGTFM ( 289 )	DFFT ( 1140 )
TMEWAB	AUS	GGTFM ( 289 )	
TMFA.W	AUS	GGKS ( 412 )	
TMFLN.W	EIN		DKRNT ( 445 ), GGKS ( 412 )
TMFL.W	AUS	GGKS ( 412 )	
TMISCHBR.W	LOK	BGTEMPK ( 252 )	
TMKI	EIN		KOS ( 896 )
TMKIC	EIN		GGTFM ( 289 )
TMOT	AUS	GGTFM ( 289 )	SWADAP ( 47 ), ACIFI ( 1013 ), GGKS ( 412 ), GGDPG ( 74 ), FUEREG ( 595 ), ESVW ( 1009 ), EGFE ( 228 ), DWUC ( 1147 ), DVFZ ( 500 ), DTEV ( 856 ), DNWS ( 622 ), DLSH ( 330 ), DLLR ( 578 ), DFFTK ( 1142 ), DFFT ( 1140 ), BGTEMPK ( 252 ), BGDVE ( 934 ), BBSTT ( 148 ), BBKHZ ( 890 ), ATWAL ( 297 ), ATM ( 20 ), ARMD ( 531 ), KRDY ( 659 ), KOS ( 896 ), KHMD ( 894 ), HLS ( 392 ), ESUKA ( 711 ), ESUK ( 699 ), ESNSWL ( 691 ), DMDSTP ( 205 ), ZWWL ( 638 ), ZWMIN ( 669 ), ZUESZ ( 632 ), WANWKW ( 125 ), UFUE ( 1056 ), UFEING ( 1058 ), TEBEB ( 762 ), TEB ( 826 ), SU ( 617 ), RDE ( 112 ), NWS ( 618 ), NMAXMD ( 584 ), NLPH ( 150 ), NLDG ( 157 ), MDZUL ( 523 ), MDVERAD ( 549 ), MDVER ( 546 ), MDRED ( 976 ), MDKOG ( 516 ), MD-FUE ( 594 ), MDFAW ( 508 ), MDBGRG ( 530 ), MDBAS ( 529 ), LREB ( 739 ), LRAEB ( 759 ), LRA ( 797 ), LR ( 768 ), LLRRM ( 566 ), LLRNS ( 562 ), LL-RMR ( 572 ), LLRBB ( 575 ), LFS ( 69 ), LAMKO ( 729 ), LAKH ( 735 ), KR-RA ( 639 ), DMDML ( 216 ), DMDLU ( 193 ), DLSV ( 301 ), AK ( 855 )
TMOTAB	AUS	GGTFM ( 289 )	AEKP ( 970 ), DLSV ( 301 ), DLSH ( 330 ), ESSTT ( 679 ), BGTABST ( 1030 )
TMOTDIF	LOK	BGTEMPK ( 252 )	
TMOTFIL	LOK	BGTEMPK ( 252 )	
TMOTLIN	AUS	GGTFM ( 289 )	DFFTCNV ( 1143 ), TC1MOD ( 1100 ), LREB ( 739 )
TMOTLIN.W	AUS	GGTFM ( 289 )	
TMOTST	AUS	SWADAP ( 47 )	
TMOTVT	LOK	GGTFM ( 289 )	
TMOTJ	AUS	DFFTCNV ( 1143 )	DFFT ( 1140 )
TMOTJUM	AUS	UFEING ( 1058 )	UFNSC ( 1077 ), UFUE ( 1056 )



Symbol	Type	Created within	Used within
TMPUMAST	LOK	BGDVE ( 934 )	
TMRW	AUS	GGTFM ( 289 )	LREB ( 739 )
TMRWEND	LOK	GGTFM ( 289 )	
TMST	AUS	GGTFM ( 289 )	AK ( 855 ), ZWWL ( 638 ), ZWSTT ( 637 ), WDKSOM ( 614 ), STADAP ( 684 ), LLRNS ( 562 ), KOS ( 896 ), DKAT ( 361 ), DDST ( 851 ), BGTABST ( 1030 ), ATM ( 20 ), BBKHZ ( 890 ), BBSAWE ( 557 ), BBTEGA ( 750 ), BBBO ( 853 ), LREB ( 739 ), LR ( 768 ), ESVW ( 1009 ), ESUK ( 699 ), ESSSTT ( 679 ), ESNSWL ( 691 ), EGAG ( 486 )
TMSTEM	LOK	DWUC ( 1147 )	
TN2	EIN		GGKS ( 412 )
TN2FGR_W	LOK	FGRREGL ( 1174 )	
TNACHL_W	AUS	MOTAUS ( 1028 )	AEKP ( 970 ), BGDVE ( 934 )
TNBM1_W	AUS	GGDPG ( 74 )	BGNMOT ( 111 )
TNBM2_W	AUS	GGDPG ( 74 )	
TNBMPHS0_W	LOK	NLDG ( 157 )	
TNBMRDE	LOK	RDE ( 112 )	
TNBMRDE1	LOK	RDE ( 112 )	
TNBMRDE2	LOK	RDE ( 112 )	
TNBM_W	AUS	GGDPG ( 74 )	WANWKW ( 125 ), BGNMOT ( 111 )
TNSE_W	AUS	BBSTT ( 148 )	BBTEGA ( 750 ), DTEV ( 856 ), DLLR ( 578 )
TNST	EIN		AK ( 855 ), LR ( 768 ), LLRNS ( 562 )
TNST_W	AUS	BBSTT ( 148 )	BBKHZ ( 890 ), DMDSTP ( 205 ), ZWMIN ( 669 ), NWS ( 618 ), ESUKA ( 711 ), DMDFON ( 161 ), DNWS ( 622 )
TNTEVZU	LOK	DTEV ( 856 )	
TNTIMER	EIN		BGPU ( 276 )
TOEL	EIN		GGTFM ( 289 )
TOOTH_RALE	LOK	ALE ( 136 )	
TOP_W	AUS	DTOP ( 1145 )	
TPCORCTR_W	AUS	GGDPG ( 74 )	
TPH1_W	DOK	NLDG ( 157 )	
TPLDPCTX_W	EIN		DTEV ( 856 )
TPLDPTC_W	EIN		DTEV ( 856 )
TPLRVK2_W	AUS	LR ( 768 )	DLSA ( 398 )
TPLRVK_W	AUS	LR ( 768 )	DLSA ( 398 )
TPNT_AKTIV	AUS	EGKE ( 409 )	DKRNT ( 445 ), KRRA ( 639 ), KRKE ( 427 ), DKRTP ( 451 ), GGKS ( 412 )
TPOTV2_W	LOK	DLSA ( 398 )	
TPOTV_W	LOK	DLSA ( 398 )	
TPSVKMF2_U	AUS	DFFTCNV ( 1143 )	DFFT ( 1140 )
TPSVKMF2_W	AUS	DLSA ( 398 )	DFFTCNV ( 1143 ), DKAT ( 361 ), DLSSA ( 350 )
TPSVKMF_U	AUS	DFFTCNV ( 1143 )	DFFT ( 1140 )
TPSVKMF_W	AUS	DLSA ( 398 )	DFFTCNV ( 1143 ), DKAT ( 361 ), DLSSA ( 350 )
TPSVKOF2_W	LOK	DLSA ( 398 )	
TPSVKOF_W	LOK	DLSA ( 398 )	
TPSVLSA2	AUS	DLSSA ( 350 )	
TPSVLSSA	AUS	DLSSA ( 350 )	
TPSVLSSA2	AUS	DLSSA ( 350 )	
TR_ZAHN	EIN		AZUE ( 904 )
TR_ZEIT	EIN		AZUE ( 904 )
TS01	LOK	DMDFON ( 161 )	
TS02	LOK	DMDFON ( 161 )	
TS03	LOK	DMDFON ( 161 )	
TS04	LOK	DMDFON ( 161 )	
TS05	LOK	DMDFON ( 161 )	
TS06	LOK	DMDFON ( 161 )	
TS07	LOK	DMDFON ( 161 )	
TS08	LOK	DMDFON ( 161 )	
TSAKA	LOK	LRKA ( 795 )	
TSAKA2	LOK	LRKA ( 795 )	
TSAS_W	LOK	BGNG ( 121 )	
TSEGHI	AUS	BGNMOT ( 111 )	
TSEGPH_W	LOK	NLDG ( 157 )	
TSEGRSP_W	AUS	BGNG ( 121 )	BGRLG ( 274 )
TSEG_W	AUS	BGNMOT ( 111 )	AZUE ( 904 ), BGNG ( 121 )
TSGES_W	LOK	BGTEMPK ( 252 )	
TSK	AUS	DMDFON ( 161 )	DMDLU ( 193 )
TSK01	LOK	DMDFON ( 161 )	
TSK02	LOK	DMDFON ( 161 )	
TSK03	LOK	DMDFON ( 161 )	
TSK04	LOK	DMDFON ( 161 )	
TSK05	LOK	DMDFON ( 161 )	
TSK06	LOK	DMDFON ( 161 )	
TSK07	LOK	DMDFON ( 161 )	
TSK08	LOK	DMDFON ( 161 )	
TSK_M	LOK	DMDFON ( 161 )	
TSPERR	LOK	LR ( 768 )	
TSPERR2	LOK	LR ( 768 )	
TSROH2_W	AUS	DMDTSB ( 159 )	DMDFON ( 161 )
TSROH_W	AUS	DMDTSB ( 159 )	DMDFON ( 161 )
TSWK	LOK	FGRFULO ( 1160 )	
TS_M	LOK	DMDFON ( 161 )	
TTMUMAD	LOK	BGDVE ( 934 )	
TTOOTH10MS	AUS	GGDPG ( 74 )	ALE ( 136 )



Symbol	Type	Created within	Used within
TUM	LOK	GGTFM ( 289 )	
TUMC	EIN		MDVERB ( 540 )
TUMG	EIN		ATM ( 20 ), DFFT ( 1140 ), BGTABST ( 1030 )
TUMTA	LOK	BGTABST ( 1030 )	
TUM_EIN	EIN		MDVERB ( 540 ), BGTABST ( 1030 )
TUSPNF	AUS	DLSSA ( 350 )	
TUSPNF2	AUS	DLSSA ( 350 )	
TV	LOK	LR ( 768 )	
TV2	LOK	LR ( 768 )	
TVDKTTK	LOK	DKAT ( 361 )	
TVDKTTK2	LOK	DKAT ( 361 )	
TVFRRDTE	LOK	DTEV ( 856 )	
TVLR	LOK	LR ( 768 )	
TVLR2	LOK	LR ( 768 )	
TVLRH	AUS	LRHK ( 781 )	LR ( 768 ), GKRA ( 766 )
TVLRH2	AUS	LRHK ( 781 )	LR ( 768 ), GKRA ( 766 )
TVLRHI	AUS	LRHK ( 781 )	LR ( 768 )
TVLRHI2	AUS	LRHK ( 781 )	LR ( 768 )
TVLRHP	LOK	LRHK ( 781 )	
TVLRHP2	LOK	LRHK ( 781 )	
TVRNR	LOK	AEVAB ( 980 )	
TVSAA	LOK	BBSAWE ( 557 )	
TVSANS	LOK	BBSAWE ( 557 )	
TVU	EIN		BGRLP ( 266 )
TVU_W	EIN		RKTI ( 979 ), AES ( 973 )
TWAN	AUS	SWADAP ( 47 )	MDWAN ( 554 )
TWDLSSA2_W	LOK	DLSSA ( 350 )	
TWDLSSA_W	LOK	DLSSA ( 350 )	
TWDLSSH2_W	LOK	DLSSA ( 350 )	
TWDLSSH_W	LOK	DLSSA ( 350 )	
TYP_LASH	AUS	DLSAHK ( 339 )	
TYP_LASH2	AUS	DLSAHK ( 339 )	
TYP_LATP	LOK	DLSA ( 398 )	
TYP_LATP2	LOK	DLSA ( 398 )	
TYP_LATV	LOK	DLSA ( 398 )	
TYP_LATV2	LOK	DLSA ( 398 )	
TYP_LSH	AUS	DLSH ( 330 )	
TYP_LSH2	AUS	DLSH ( 330 )	
TZ2FGR_W	LOK	FGRREGL ( 1174 )	
TZLSATV	LOK	DLSA ( 398 )	
TZLSATV2	LOK	DLSA ( 398 )	
TZND	AUS	AZUE ( 904 )	
TZWMNNST_W	LOK	ZWMIN ( 669 )	
UADKI	EIN		EGKE ( 409 ), GGKS ( 412 )
UADMFA	LOK	GGKS ( 412 )	
UB	AUS	GGUB ( 487 )	SWADAP ( 47 ), ADVE ( 918 ), AEKP ( 970 ), AES ( 973 ), ZUESZ ( 632 ), STADAP ( 684 ), RDE ( 112 ), MOT AUS ( 1028 ), HLS ( 392 ), GGDVE ( 477 ), EGFE ( 228 ), DLSV ( 301 ), DLSH ( 330 ), DHL SVK ( 29 ), DHL SHK ( 1154 ), DHFM ( 233 ), DFFT ( 1140 ), DECJ ( 1013 ), DCKUP ( 1128 ), DCINS ( 1126 ), DCAS ( 1128 ), CAN ( 1124 ), BGLBZ ( 489 ), BGDVE ( 934 ), ATEV ( 969 ), EGAG ( 486 )
UBF	LOK	BGLBZ ( 489 )	
UBRDE	LOK	RDE ( 112 )	
UBRSQ	EIN		BGDVE ( 934 )
UBRSQ_W	EIN		GGUB ( 487 )
UBSOL	LOK	BGLBZ ( 489 )	
UBSQ	AUS	GGUB ( 487 )	LFS ( 69 )
UBSQF	AUS	GGUB ( 487 )	
UBSQF_W	AUS	GGUB ( 487 )	
UBSQ_W	AUS	GGUB ( 487 )	
UBUANLR	LOK	BGDVE ( 934 )	
UDKNLP1	EIN		ADVE ( 918 ), BGDVE ( 934 )
UDKNLP1R	LOK	BGDVE ( 934 )	
UDKNLP2	EIN		ADVE ( 918 ), BGDVE ( 934 )
UDKNLP2R	LOK	BGDVE ( 934 )	
UDKP1A	AUS	BGDVE ( 934 )	
UDKP1AALT	LOK	BGDVE ( 934 )	
UDKP1ASR_W	LOK	BGDVE ( 934 )	
UDKP1AS_W	AUS	BGDVE ( 934 )	
UDKP1A_W	AUS	BGDVE ( 934 )	GGDVE ( 477 )
UDKP1ROB	LOK	BGDVE ( 934 )	
UDKP1RUN	LOK	BGDVE ( 934 )	
UDKP1SV	AUS	BGDVE ( 934 )	GGDVE ( 477 )
UDKP1VOR	LOK	BGDVE ( 934 )	
UDKP1VOU	AUS	BGDVE ( 934 )	
UDKP1VO_W	AUS	BGDVE ( 934 )	GGDVE ( 477 )
UDKP1VROB	LOK	BGDVE ( 934 )	
UDKP1VRUN	LOK	BGDVE ( 934 )	
UDKP1VV	AUS	BGDVE ( 934 )	
UDKP1VVR	LOK	BGDVE ( 934 )	
UDKP1VV_W	AUS	BGDVE ( 934 )	GGDVE ( 477 )
UDKP1V_W	EIN		BGDVE ( 934 ), GGDVE ( 477 )



Symbol	Type	Created within	Used within
UDKP1_U	AUS	DFFTCNV (1143)	DFFT (1140)
UDKP1_W	EIN		ADVE ( 918 ), BGDVE ( 934 ), DFFTCNV (1143), GGDVE ( 477 )
UDKP2A	AUS	BGDVE ( 934 )	UFRLC (1066), UFUE (1056)
UDKP2AALT	LOK	BGDVE ( 934 )	
UDKP2ASR_W	LOK	BGDVE ( 934 )	
UDKP2AS_W	AUS	BGDVE ( 934 )	
UDKP2A_W	AUS	BGDVE ( 934 )	GGDVE ( 477 )
UDKP2_U	AUS	DFFTCNV (1143)	DFFT (1140)
UDKP2_W	EIN		ADVE ( 918 ), DFFTCNV (1143), BGDVE ( 934 ), GGDVE ( 477 )
UDKPATR_W	LOK	BGDVE ( 934 )	
UDKPAT_W	LOK	BGDVE ( 934 )	
UDKSNOA_W	LOK	DKRS ( 437 )	
UDKSNUA_W	LOK	DKRS ( 437 )	
UDSM_W	LOK	EGFE ( 228 )	
UDSS_W	EIN		EGFE ( 228 )
UEFKTGET	EIN		BBGANG ( 501 )
UEVGES	AUS	BBGANG ( 501 )	FGRFULO (1160), FGRREGL (1174)
UEVGES_W	LOK	FGRREGL (1174)	
UFST_W	EIN		GGFST ( 502 )
UHAGR	LOK	EGAG ( 486 )	
UHFM_W	EIN		DHFM ( 233 ), EGFE ( 228 ), GGHEM ( 230 )
UHSH	EIN		DFFT (1140), DHLSHK (1154)
UHSH2	EIN		DFFT (1140), DHLSHK (1154)
UHSV	EIN		DFFT (1140)
UHSV2	EIN		DFFT (1140)
UMSRLN_W	AUS	BGMSZS ( 239 )	BGAGR ( 263 ), BGSRM ( 245 ), BGPU ( 276 ), FUEDK ( 597 ), DTEV ( 856 ), BGRLP ( 266 ), EGFE ( 228 )
UPW2LL_W	LOK	GGPED ( 454 )	
UPWG1_U	AUS	DFFTCNV (1143)	DFFT (1140)
UPWG1_W	EIN		DFFTCNV (1143), GGPED ( 454 ), EGEG ( 453 )
UPWG2D_U	AUS	DFFTCNV (1143)	DFFT (1140)
UPWG2D_W	EIN		DFFTCNV (1143), GGPED ( 454 )
UPWG2FIL_W	LOK	GGPED ( 454 )	
UPWG2_U	AUS	DFFTCNV (1143)	DFFT (1140)
UPWG2_W	EIN		DFFTCNV (1143), EGEG ( 453 ), GGPED ( 454 )
UPWGEJ_W	LOK	GGPED ( 454 )	
UPWG_W	LOK	GGPED ( 454 )	
URDDKTP	LOK	DKAT ( 361 )	
URDDKTP2	LOK	DKAT ( 361 )	
URL2SU_W	AUS	BGSRM ( 245 )	
URL3SU_W	AUS	BGSRM ( 245 )	
URLSU_W	AUS	BGSRM ( 245 )	
URL_W	AUS	BGSRM ( 245 )	
URMCKSCO	LOK	URMEM (1044)	
URMCKSDA	LOK	URMEM (1044)	
URMPATCO	LOK	URMEM (1044)	
USBEH2_W	LOK	GGLSH ( 318 )	
USBEH_W	LOK	GGLSH ( 318 )	
USBEV2_W	LOK	GGLSV ( 382 )	
USBEV_W	LOK	GGLSV ( 382 )	
USHDKTP	LOK	DKAT ( 361 )	
USHDKTP2	LOK	DKAT ( 361 )	
USHFMXSTG	LOK	DLSAHK ( 339 )	
USHFMXSTG2	LOK	DLSAHK ( 339 )	
USHK	AUS	GGLSH ( 318 )	DFFT (1140), DLSA ( 398 ), DKAT ( 361 ), TC1MOD (1100), LRKA ( 795 ), GKRA ( 766 ), DLSSA ( 350 ), DLSH ( 330 ), DLSAHK ( 339 )
USHK2	AUS	GGLSH ( 318 )	DFFT (1140), DLSAHK ( 339 ), DLSSA ( 350 ), DLSH ( 330 ), DLSA ( 398 ), TC1MOD (1100), LRKA ( 795 ), GKRA ( 766 ), DKAT ( 361 )
USHK2_W	AUS	GGLSH ( 318 )	SWADAP ( 47 ), DLSV ( 301 ), LRHK ( 781 )
USHKJ	LOK	DLSSA ( 350 )	
USHKJ2	LOK	DLSSA ( 350 )	
USHKJF2_W	LOK	DLSSA ( 350 )	
USHKJF_W	LOK	DLSSA ( 350 )	
USHKMXSTG	LOK	DLSAHK ( 339 )	
USHKMXSTG2	LOK	DLSAHK ( 339 )	
USHKR2_W	LOK	GGLSH ( 318 )	
USHKR_W	LOK	GGLSH ( 318 )	
USHKSTEIG	LOK	DLSAHK ( 339 )	
USHKSTEIG2	LOK	DLSAHK ( 339 )	
USHK_W	AUS	GGLSH ( 318 )	SWADAP ( 47 ), DLSV ( 301 ), LRHK ( 781 )
USMNSAA	LOK	DLSSA ( 350 )	
USMNSAA2	LOK	DLSSA ( 350 )	
USMNSAN	AUS	DLSSA ( 350 )	
USMNSAN2	AUS	DLSSA ( 350 )	
USMNSHA	LOK	DLSSA ( 350 )	
USMNSHA2	LOK	DLSSA ( 350 )	
USMNSHN	AUS	DLSSA ( 350 )	
USMNSHN2	AUS	DLSSA ( 350 )	
USMXSAA	LOK	DLSSA ( 350 )	
USMXSAA2	LOK	DLSSA ( 350 )	
USMXSAN	AUS	DLSSA ( 350 )	
USMXSAN2	AUS	DLSSA ( 350 )	





Symbol	Type	Created within	Used within
USMXSHA	LOK	DLSSA ( 350 )	
USMXSHA2	LOK	DLSSA ( 350 )	
USMXSHN	AUS	DLSSA ( 350 )	
USMXSHN2	AUS	DLSSA ( 350 )	
USOBH2_W	LOK	GGLSH ( 318 )	
USOBH_W	LOK	GGLSH ( 318 )	
USOBV2_W	LOK	GGLSV ( 382 )	
USOBV_W	LOK	GGLSV ( 382 )	
USRHK	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSAHK ( 339 )
USRHK2	AUS	LRHK ( 781 )	DLSA ( 398 ), DLSAHK ( 339 )
USRJ	AUS	DLSSA ( 350 )	
USVK	AUS	GGLSV ( 382 )	DFFT ( 1140 ), TC1MOD ( 1100 ), DLSSA ( 350 ), LR ( 768 ), LREB ( 739 ), LRKA ( 795 )
USVK2	AUS	GGLSV ( 382 )	DFFT ( 1140 ), DLSSA ( 350 ), TC1MOD ( 1100 ), LRKA ( 795 ), LREB ( 739 ), LR ( 768 )
USVK2_W	AUS	GGLSV ( 382 )	SWADAP ( 47 ), DLSV ( 301 ), LR ( 768 ), HLS ( 392 ), GKRA ( 766 )
USVKJ	AUS	DLSSA ( 350 )	
USVKJ2	AUS	DLSSA ( 350 )	
USVKJF2_W	LOK	DLSSA ( 350 )	
USVKJF_W	LOK	DLSSA ( 350 )	
USVKMA_W	LOK	LR ( 768 )	
USVKR2_W	LOK	GGLSV ( 382 )	
USVKR_W	LOK	GGLSV ( 382 )	
USVKSL_W	LOK	LR ( 768 )	
USVK_W	AUS	GGLSV ( 382 )	SWADAP ( 47 ), DLSV ( 301 ), LR ( 768 ), HLS ( 392 ), GKRA ( 766 )
USVMB2_W	LOK	GGLSV ( 382 )	
USVMB_W	LOK	GGLSV ( 382 )	
USVOB2_W	LOK	GGLSV ( 382 )	
USVOB_W	LOK	GGLSV ( 382 )	
UUSHK2_W	LOK	GGLSH ( 318 )	
UUSHK_W	LOK	GGLSH ( 318 )	
UUSHMB2_W	LOK	GGLSH ( 318 )	
UUSHMB_W	LOK	GGLSH ( 318 )	
UUSHOB2_W	LOK	GGLSH ( 318 )	
UUSHOB_W	LOK	GGLSH ( 318 )	
UUSVK2_W	LOK	GGLSV ( 382 )	
UUSVK_W	LOK	GGLSV ( 382 )	
UUSVMB2_W	LOK	GGLSV ( 382 )	
UUSVMB_W	LOK	GGLSV ( 382 )	
UUSVOB2_W	LOK	GGLSV ( 382 )	
UUSVOB_W	LOK	GGLSV ( 382 )	
UZKW_W	AUS	GGDPG ( 74 )	DHFM ( 233 ), ESVW ( 1009 ), DNWS ( 622 )
VAMSR_W	EIN		GGVFZG ( 497 )
VFGRO_W	LOK	FGRREGL ( 1174 )	
VFGR_W	AUS	GGVFZG ( 497 )	FGRABED ( 491 ), FGRUE ( 490 ), FGRFULO ( 1160 ), FGRREGL ( 1174 )
VFIL_W	LOK	GGVFZG ( 497 )	
VFZG	AUS	GGVFZG ( 497 )	SWADAP ( 47 ), ARMD ( 531 ), TC1MOD ( 1100 ), NMAXMD ( 584 ), MDWAN ( 554 ), MDFAW ( 508 ), MDBGRG ( 530 ), LLRNS ( 562 ), LLRNFA ( 564 ), LLRMR ( 572 ), LLRBB ( 575 ), KOS ( 896 ), GGUB ( 487 ), GGPED ( 454 ), FUEDK ( 597 ), DTEV ( 856 ), DSWEC ( 32 ), DMDSTP ( 205 ), DMDLU ( 193 ), DLLR ( 578 ), DFFTCNV ( 1143 ), BGTABST ( 1030 ), BGPU ( 276 ), BGDVE ( 934 ), ATM ( 20 ), BBSAWE ( 557 )
VFZGKB_W	EIN		GGVFZG ( 497 )
VFZGPR_W	LOK	VMAXMD ( 588 )	
VFZG_U	AUS	DFFTCNV ( 1143 )	BGBSZ ( 73 ), BGKMST ( 1008 ), DFFT ( 1140 )
VFZG_UM	EIN		UFFGRC ( 1078 ), UFUE ( 1056 )
VFZG_W	AUS	EGAG ( 486 )	GGVFZG ( 497 ), BBGANG ( 501 ), DVKUP ( 1027 ), DDG ( 141 ), RDE ( 112 ), VMAXMD ( 588 ), UFUE ( 1056 ), MSF ( 506 )
VFZROH_W	AUS	GGVFZG ( 497 )	DVFZ ( 500 ), EGAG ( 486 )
VIRKR	AUS	EGKE ( 409 )	KRKE ( 427 ), KRDY ( 659 )
VKR	AUS	KRKE ( 427 )	DKRS ( 437 ), EGKE ( 409 )
VKR_C95	AUS	KRKE ( 427 )	GGKS ( 412 ), EGKE ( 409 )
VKR_TST	AUS	KRKE ( 427 )	
VLAST_W	LOK	FGRREGL ( 1174 )	
VOFFS_W	LOK	FGRREGL ( 1174 )	
VPSSPLS_W	EIN		FUEDK ( 597 )
VPSSPU_W	EIN		FUEDK ( 597 )
VREGDIA_W	AUS	BGTEV ( 257 )	
VREGL_W	AUS	FGRFULO ( 1160 )	FGRREGL ( 1174 ), FGRUE ( 490 )
VROH_W	LOK	GGVFZG ( 497 )	
VSDMR	AUS	VS_VERST ( 67 )	MDKOL ( 526 )
VSFPSES	AUS	VS_VERST ( 67 )	AES ( 973 )
VSFRK	AUS	VS_VERST ( 67 )	ESGRU ( 678 )
VSKE	AUS	VS_VERST ( 67 )	KRKE ( 427 )
VSKSML_W	AUS	BGKV ( 71 )	
VSKS_W	AUS	BGKV ( 71 )	
VSLDTV	AUS	VS_VERST ( 67 )	
VSNS	AUS	VS_VERST ( 67 )	LLRNS ( 562 )
VSRLMX	AUS	VS_VERST ( 67 )	
VSTCNS	EIN		LLRNS ( 562 )
VSTFBA	EIN		ESUK ( 699 )
VSTFNS	EIN		ESNSWL ( 691 )



Symbol	Type	Created within	Used within
VSTFRK	EIN		ESGRU ( 678 )
VSTFST	EIN		ESSTT ( 679 )
VSTFVA	EIN		ESUK ( 699 )
VSTFWL	EIN		ESNSWL ( 691 )
VSTLR	EIN		LR ( 768 )
VSTMDR	EIN		LLRMR ( 572 )
VSTNLS	EIN		LLRNS ( 562 )
VSTVVR	EIN		VMAXMD ( 588 )
VS VW	AUS	VS_VERST ( 67 )	ESVW (1009)
VSWNWS	AUS	VS_VERST ( 67 )	
VSZ W	AUS	VS_VERST ( 67 )	ZUE ( 627 )
VSZWK R	AUS	VS_VERST ( 67 )	KRRA ( 639 )
VSZWM	AUS	KRRA ( 639 )	
VWK W	LOK	BGRLP ( 266 )	
VZIEL S_W	EIN		FGRFULO (1160)
VZIEL_W	AUS	FGRFULO (1160)	FGRABED ( 491 ), FGRREGL (1174), FGRUE ( 490 )
WDK1	LOK	GGDVE ( 477 )	
WDK1G	LOK	GGDVE ( 477 )	
WDK2	LOK	GGDVE ( 477 )	
WDK2G	LOK	GGDVE ( 477 )	
WDK3	LOK	GGDVE ( 477 )	
WDKADA_W	AUS	BGDVE ( 934 )	ADVE ( 918 )
WDKBA	AUS	GGDVE ( 477 )	BGPU ( 276 ), BGTEV ( 257 ), DFFT (1140), TC1MOD (1100), LRAEB ( 759 ), GGHEM ( 230 ), EGFE ( 228 )
WDKBAALT_W	LOK	ADVE ( 918 )	
WDKBAB_W	LOK	BGMSZS ( 239 )	
WDKBADMN_W	LOK	DHFM ( 233 )	
WDKBADMX_W	LOK	DHFM ( 233 )	
WDKBAPB_W	LOK	BGRLP ( 266 )	
WDKBAP_L	LOK	BGWDKM ( 273 )	
WDKBAP_W	AUS	BGWDKM ( 273 )	BGRLP ( 266 )
WDKBAS_W	LOK	ADVE ( 918 )	
WDKBA_W	AUS	GGDVE ( 477 )	ADVE ( 918 ), BGDVE ( 934 ), DHFM ( 233 ), BGPU ( 276 ), BGMSZS ( 239 ), EGFE ( 228 )
WDKDLR_W	LOK	ADVE ( 918 )	
WDKINK_W	LOK	FUEDKSA ( 610 )	
WDKNLP	AUS	BGDVE ( 934 )	
WDKNLPR	AUS	BGDVE ( 934 )	
WDKNLPR_W	AUS	BGDVE ( 934 )	
WDKNLP_W	AUS	BGDVE ( 934 )	ADVE ( 918 ), FUEDKSA ( 610 )
WDKPMX	LOK	GGDVE ( 477 )	
WDKS	AUS	FUEDKSA ( 610 )	DFFT (1140)
WDKSAP_W	AUS	FUEDK ( 597 )	FUEDKSA ( 610 )
WDKSBA2_W	LOK	FUEDKSA ( 610 )	
WDKSBA_W	LOK	FUEDKSA ( 610 )	
WDKSB_W	LOK	FUEDKSA ( 610 )	
WDKSFL_W	LOK	ADVE ( 918 )	
WDKSFL	LOK	FUEDKSA ( 610 )	
WDKSGV_W	LOK	FUEDK ( 597 )	
WDKSMX_W	LOK	FUEDK ( 597 )	
WDKSOM_W	AUS	WDKSOM ( 614 )	FUEDK ( 597 )
WDKSPA_W	LOK	FUEDKSA ( 610 )	
WDKSP_W	AUS	FUEDKSA ( 610 )	BGWDKM ( 273 )
WDKSSTSW_W	LOK	ADVE ( 918 )	
WDKSVFL	LOK	FUEDKSA ( 610 )	
WDKSV_W	LOK	FUEDK ( 597 )	
WDKSWE_W	LOK	FUEDKSA ( 610 )	
WDKS_W	AUS	FE ( 591 )	FUEDKSA ( 610 ), MSF ( 506 ), ADVE ( 918 ), BGDVE ( 934 )
WDKUGD_W	AUS	BGMSZS ( 239 )	BGRLP ( 266 ), EGFE ( 228 ), FUEDK ( 597 )
WDKVABOB	LOK	BGDVE ( 934 )	
WDKVABUB	LOK	BGDVE ( 934 )	
WMDMKOE	LOK	MDVERB ( 540 )	
WEA	AUS	AES ( 973 )	ESVW (1009), BGRLP ( 266 )
WEE	AUS	AES ( 973 )	ESVW (1009), BGRLP ( 266 )
WEEMRFA	LOK	ESVW (1009)	
WEENST	LOK	ESVW (1009)	
WEER	AUS	ESVW (1009)	AES ( 973 )
WEEST	LOK	ESVW (1009)	
WEESTZ	LOK	AES ( 973 )	
WESSBM	EIN		BGRLP ( 266 )
WF_W	LOK	ESUK ( 699 )	
WKFMDKO	LOK	MDVERB ( 540 )	
WKR	LOK	KRRA ( 639 )	
WKRA	LOK	KRRA ( 639 )	
WKRAST	AUS	KRRA ( 639 )	
WKRDY	AUS	KRDY ( 659 )	ZUE ( 627 ), EGKE ( 409 )
WKRDYA	LOK	KRDY ( 659 )	
WKRDYAA	LOK	KRDY ( 659 )	
WKRDYTI	LOK	KRDY ( 659 )	
WKR M	LOK	KRRA ( 639 )	
WKRMA	AUS	EGKE ( 409 )	KRRA ( 639 )
WKR_TST	AUS	KRRA ( 639 )	



Symbol	Type	Created within	Used within
WKWAS	LOK	ALE ( 136 )	
WKWAS_KOR	LOK	ALE ( 136 )	
WKWAS_RDE	LOK	RDE ( 112 )	
WKWBZM0_W	AUS	GGDPG ( 74 )	ALE ( 136 ), RDE ( 112 )
WKWNEG_W	LOK	GGDPG ( 74 )	
WKWPOS_W	LOK	GGDPG ( 74 )	
WKWSTART_W	LOK	GGDPG ( 74 )	
WKWSTOP	AUS	ALE ( 136 )	GGDPG ( 74 )
WKWSYN_W	AUS	GGDPG ( 74 )	WANWKW ( 125 )
WKW_W	AUS	GGDPG ( 74 )	ALE ( 136 ), RDE ( 112 ), WANWKW ( 125 )
WMFA	LOK	GGKS ( 412 )	
WMFL	LOK	GGKS ( 412 )	
WNWEM	EIN		ESVW (1009)
WNWI2_AD_W	AUS	WANWKW ( 125 )	NLDG ( 157 ), NWS ( 618 )
WNWIAW2_W	AUS	NWS ( 618 )	DNWS ( 622 )
WNWIAW_W	AUS	NWS ( 618 )	DNWS ( 622 )
WNWIA_W	AUS	NWS ( 618 )	
WNWIM2_W	LOK	WANWKW ( 125 )	
WNWIM_W	LOK	WANWKW ( 125 )	
WNWISA_W	EIN		BGSRM ( 245 )
WNWIX_W	LOK	NLDG ( 157 )	
WNWI_AD_W	AUS	WANWKW ( 125 )	NLDG ( 157 ), NWS ( 618 )
WNWI_W	EIN		ESVW (1009)
WNWKWAS2_W	AUS	WANWKW ( 125 )	NLDG ( 157 )
WNWKWASX_W	LOK	NLDG ( 157 )	
WNWKWAS_W	AUS	WANWKW ( 125 )	NLDG ( 157 )
WNWSE	AUS	NWS ( 618 )	
WNWSP2_W	AUS	WANWKW ( 125 )	DNWKW ( 134 ), GGDPG ( 74 )
WNWSPAS2_W	AUS	WANWKW ( 125 )	NLDG ( 157 )
WNWSPASX_W	LOK	NLDG ( 157 )	
WNWSPAS_W	AUS	WANWKW ( 125 )	NLDG ( 157 )
WNWSP_W	AUS	WANWKW ( 125 )	DNWKW ( 134 ), GGDPG ( 74 )
WNWSRM_W	AUS	BGSRM ( 245 )	
WNWUE	AUS	NWS ( 618 )	MDBAS ( 529 ), ZWGRU ( 634 )
WNWUE_W	AUS	NWS ( 618 )	BGSRM ( 245 )
WOUTA0	AUS	AZUE ( 904 )	
WOUTA1	AUS	AZUE ( 904 )	
WOUTA2	AUS	AZUE ( 904 )	
WOUTA3	AUS	AZUE ( 904 )	
WOUTST0	AUS	AZUE ( 904 )	
WOUTST1	AUS	AZUE ( 904 )	
WOUTST2	AUS	AZUE ( 904 )	
WOUTST3	AUS	AZUE ( 904 )	
WPED	AUS	GGPED ( 454 )	ADVE ( 918 ), WDKSOM ( 614 ), NMAXMD ( 584 ), MDZUL ( 523 ), MD-MIN ( 538 ), KOS ( 896 ), DFFT ( 1140 ), BGDVE ( 934 )
WPEDC_W	EIN		GGPED ( 454 )
WPEDT_W	LOK	GGPED ( 454 )	
WPEDV_W	LOK	GGPED ( 454 )	
WPED_W	AUS	EGEG ( 453 )	GGPED ( 454 ), SWADAP ( 47 ), FUEDK ( 597 ), MSF ( 506 ), MDFUE ( 594 ), MDAFW ( 508 )
WPFGR_W	AUS	BGWPFGR ( 548 )	
WPHG	LOK	ZUE ( 627 )	
WPR	LOK	BGRLP ( 266 )	
WPRNSP	LOK	BGRLP ( 266 )	
WRI_C_UJ	LOK	URMEM ( 1044 )	
WTANS	EIN		GGTFA ( 298 )
WTMOT_W	EIN		GGTFM ( 289 )
WUB	EIN		RDE ( 112 ), EGAG ( 486 ), GGUB ( 487 )
WUB_W	EIN		GGUB ( 487 )
WUCCNT	AUS	DWUC ( 1147 )	
XQTM_W	LOK	BGTABST ( 1030 )	
XS02	LOK	DMDFON ( 161 )	
XS03	LOK	DMDFON ( 161 )	
XS04	LOK	DMDFON ( 161 )	
XS05	LOK	DMDFON ( 161 )	
XS06	LOK	DMDFON ( 161 )	
XS07	LOK	DMDFON ( 161 )	
XS08	LOK	DMDFON ( 161 )	
XZKRZNT	LOK	DKRNT ( 445 )	
XZKRZOF	LOK	DKRNT ( 445 )	
XZKRZS(I)	LOK	DKRS ( 437 )	
XZKRZTP	LOK	DKRTP ( 451 )	
XZSEN(I)	LOK	DKRS ( 437 )	
XZSKRNT	AUS	DKRNT ( 445 )	GGKS ( 412 ), EGKE ( 409 )
XZSKROF	AUS	DKRNT ( 445 )	GGKS ( 412 ), EGKE ( 409 )
XZSKRTP	AUS	DKRTP ( 451 )	GGKS ( 412 ), EGKE ( 409 )
ZALDY	LOK	KRDY ( 659 )	
ZALT_UJ	LOK	UFNC ( 1063 )	
ZATV	LOK	LRHK ( 781 )	
ZATV2	LOK	LRHK ( 781 )	
ZBALE	LOK	ESUK ( 699 )	
ZBURN	LOK	STADAP ( 684 )	



Symbol	Type	Created within	Used within
ZBURNSU	LOK	STADAP ( 684 )	
ZBURNSUM	LOK	ESSTT ( 679 )	
ZCAP_JUM	LOK	UFNC (1063)	
ZDASH_W	LOK	MDFAW ( 508 )	
ZDELAY	LOK	GGDPG ( 74 )	
ZDIF_JUM	LOK	UFNC (1063)	
ZERDYSH	LOK	DLSAHK ( 339 )	
ZERDYSH2	LOK	DLSAHK ( 339 )	
ZERLATV	LOK	DLSA ( 398 )	
ZERLATV2	LOK	DLSA ( 398 )	
ZERSCH	LOK	DLSAHK ( 339 )	
ZERSCH2	LOK	DLSAHK ( 339 )	
ZFCNT	LOK	GGVFZG ( 497 )	
ZHLL	LOK	LLRNS ( 562 )	
ZKRFMU	LOK	GGKS ( 412 )	
ZKRVF	LOK	KRRA ( 639 )	
ZKVEK	AUS	AZUE ( 904 )	
ZLASH2_W	LOK	DLSAHK ( 339 )	
ZLASH_W	LOK	DLSAHK ( 339 )	
ZLDY	LOK	KRDY ( 659 )	
ZLDYKE	LOK	KRDY ( 659 )	
ZLSATP	LOK	DLSA ( 398 )	
ZLSATP2	LOK	DLSA ( 398 )	
ZLSD_W	LOK	MDFAW ( 508 )	
ZNACHANZ	AUS	ZUE ( 627 )	
ZNBM_W	AUS	GGDPG ( 74 )	
ZNDY	LOK	KRDY ( 659 )	
ZNLPHAUFS	LOK	NLPH ( 150 )	
ZNLPHAUSTR	LOK	NLPH ( 150 )	
ZNLPHSTIM	LOK	NLPH ( 150 )	
ZNOSTEND	LOK	AEKP ( 970 )	
ZNZKVEK	AUS	AZUE ( 904 )	
ZOUTTMX	AUS	AZUE ( 904 )	
ZPHFL	AUS	WANWKW ( 125 )	NLDG ( 157 )
ZPHFL2	AUS	WANWKW ( 125 )	NLDG ( 157 )
ZPHFLSYN	AUS	NLDG ( 157 )	WANWKW ( 125 )
ZPHFLX	LOK	NLDG ( 157 )	
ZPHNOK	LOK	DPH ( 144 )	
ZPHNOK2	LOK	DPH ( 144 )	
ZRIBERV	LOK	GGLSV ( 382 )	
ZRIBERV2	LOK	GGLSV ( 382 )	
ZRINV2_W	LOK	GGLSV ( 382 )	
ZRINV_W	LOK	GGLSV ( 382 )	
ZRPH	AUS	GGDPG ( 74 )	DDG ( 141 ), DPH ( 144 )
ZRPH2	AUS	GGDPG ( 74 )	DDG ( 141 ), DPH ( 144 )
ZSTFGR	AUS	FGRFULO (1160)	BGWPFGR ( 548 ), FGRREGL (1174), FGRBESI (1158), FGRABED ( 491 ), FGRUE ( 490 )
ZSYNCHRO	LOK	STADAP ( 684 )	
ZSYNC_JUM	LOK	UFNC (1063)	
ZSYNC_JUR	LOK	UFNC (1063)	
ZSYNSU	LOK	STADAP ( 684 )	
ZTPNT_A	LOK	GGKS ( 412 )	
ZUBKST	LOK	STADAP ( 684 )	
ZUENBEG	EIN		AZUE ( 904 )
ZUENINKR	AUS	AZUE ( 904 )	
ZUENTMX	AUS	AZUE ( 904 )	
ZUENZAHN	AUS	AZUE ( 904 )	
ZVALE	LOK	ESUK ( 699 )	
ZWBAS	AUS	ZUE ( 627 )	MDBAS ( 529 ), MSF ( 506 )
ZWBASAR	AUS	ZUE ( 627 )	
ZWC_C_JUM	LOK	UFZWC (1075)	
ZWDYNOSH	LOK	DLSAHK ( 339 )	
ZWDYNOSH2	LOK	DLSAHK ( 339 )	
ZWGEFLR	AUS	DLSV ( 301 )	
ZWGEFLR2	AUS	DLSV ( 301 )	
ZWGRU	AUS	ZWGRU ( 634 )	LAMBTS ( 732 ), ZUE ( 627 )
ZWIST	AUS	ZUE ( 627 )	MDIST ( 528 ), MSF ( 506 ), ZWMIN ( 669 )
ZWKRAFLD	AUS	ZUE ( 627 )	KRRA ( 639 )
ZWLATE	LOK	ZWMIN ( 669 )	
ZWMATM	AUS	ATM ( 20 )	
ZWMATM2	AUS	ATM ( 20 )	
ZWMATMF	AUS	ATM ( 20 )	
ZWMATMF2	AUS	ATM ( 20 )	
ZWMN	LOK	ZWMIN ( 669 )	
ZWMND	LOK	ZWMIN ( 669 )	
ZWMNMS	LOK	ZWMIN ( 669 )	
ZWMNT	LOK	ZWMIN ( 669 )	
ZWNWS	LOK	ZWGRU ( 634 )	
ZWOPT	AUS	MDBAS ( 529 )	MSF ( 506 ), LAMBTS ( 732 ), MDIST ( 528 ), MDZW ( 636 ), ZWMIN ( 669 )
ZWOPTL1	LOK	MDBAS ( 529 )	
ZWOPT_JUM	LOK	UFMIST (1086)	
ZWOUT	AUS	MSF ( 506 )	ZUE ( 627 ), AZUE ( 904 ), UFZWC (1075), UFUE (1056), CAN (1124)



Symbol	Type	Created within	Used within
ZWOUTAR	AUS	ZUE ( 627 )	
ZWOUTAR0	EIN		AZUE ( 904 )
ZWOUTAR1	EIN		AZUE ( 904 )
ZWOUTAR2	EIN		AZUE ( 904 )
ZWOUTAR3	EIN		AZUE ( 904 )
ZWOUTCPL	AUS	ZUE ( 627 )	UFUE (1056), UFZWC (1075)
ZWOUT_JM	AUS	UFZWC (1075)	UFMIST (1086), UFUE (1056)
ZWPVK	LOK	DLSA ( 398 )	
ZWSOL	AUS	MDZW ( 636 )	ZUE ( 627 )
ZWSPA	AUS	ZWMIN ( 669 )	CAN (1124), ZUE ( 627 )
ZWSTNM	LOK	ZWSTT ( 637 )	
ZWSTT	AUS	ZWSTT ( 637 )	ZUE ( 627 ), ZWMIN ( 669 )
ZWSTTA	LOK	ZWSTT ( 637 )	
ZWSTTM	LOK	ZWSTT ( 637 )	
ZWZYL1	AUS	ZUE ( 627 )	TC1MOD (1100)
ZYLEAUSB	AUS	NLPH ( 150 )	AEVAB ( 980 )
ZYLINDEX	LOK	GGKS ( 412 )	
ZYLVEK	EIN		AZUE ( 904 )
ZYLVIRT	AUS	GGDPG ( 74 )	
ZZALE_JNI	LOK	GGDPG ( 74 )	
ZZBANK	EIN		ACIFI (1013)
ZZPRZ	LOK	KRDY ( 659 )	
ZZSEG	AUS	GGDPG ( 74 )	ALE ( 136 ), RDE ( 112 ), WANWKW ( 125 )
ZZTAB	AUS	GGDPG ( 74 )	WANWKW ( 125 )
ZZVIRT	AUS	GGDPG ( 74 )	
ZZWDYKR	LOK	KRDY ( 659 )	
ZZWDYMD	LOK	KRDY ( 659 )	
ZZYL	AUS	GGDPG ( 74 )	AEVAB ( 980 ), WANWKW ( 125 ), NLPH ( 150 ), GGKS ( 412 ), EGKE ( 409 ), DMDLU ( 193 ), DMDFON ( 161 )
ZZYLKR	AUS	EGKE ( 409 )	GGKS ( 412 ), KRDY ( 659 ), KRKE ( 427 ), KRRA ( 639 )
ZZYLZUE	EIN		ZUE ( 627 )
ZZYL_VIRT	LOK	GGDPG ( 74 )	
Z_AGRF	EIN		DIMC (1148)
Z_BM	AUS	DDG ( 141 )	
Z_BREMS	AUS	EGEG ( 453 )	GGEGAS ( 474 )
Z_BUOF	AUS	CAN (1124)	
Z_BWF	AUS	GGPED ( 454 )	
Z_CAS	AUS	DCAS (1128)	
Z_CINS	AUS	DCINS (1126)	
Z_CKUP	EIN		DCKUP (1128)
Z_DK	AUS	DDVE ( 950 )	
Z_DK1P	AUS	DDVE ( 950 )	
Z_DK2P	AUS	DDVE ( 950 )	
Z_DSS	LOK	EGFE ( 228 )	
Z_DST	AUS	EGAG ( 486 )	
Z_DVEE	AUS	DDVE ( 950 )	
Z_DVEF	AUS	DDVE ( 950 )	
Z_DVEFO	AUS	DDVE ( 950 )	
Z_DVEL	AUS	DDVE ( 950 )	
Z_DVEN	AUS	DDVE ( 950 )	
Z_DVER	AUS	DDVE ( 950 )	
Z_DVET	AUS	DDVE ( 950 )	
Z_DVEU	AUS	DDVE ( 950 )	
Z_DVEUB	AUS	DDVE ( 950 )	
Z_DVEUW	AUS	DDVE ( 950 )	
Z_DVEV	AUS	DDVE ( 950 )	
Z_EGFE	AUS	DEGFE ( 592 )	
Z_EV1	AUS	DEVE (1017)	
Z_EV2	AUS	DEVE (1017)	
Z_EV3	AUS	DEVE (1017)	
Z_EV4	AUS	DEVE (1017)	
Z_EV5	AUS	DEVE (1017)	
Z_EV6	AUS	DEVE (1017)	
Z_EV7	AUS	DEVE (1017)	
Z_EV8	AUS	DEVE (1017)	
Z_FP1P	AUS	GGPED ( 454 )	
Z_FP2P	AUS	GGPED ( 454 )	
Z_FPP	AUS	EGEG ( 453 )	GGPED ( 454 )
Z_FRA	AUS	GKRA ( 766 )	
Z_FRA2	AUS	GKRA ( 766 )	
Z_FRAO	AUS	DKVS ( 811 )	BBTEGA ( 750 )
Z_FRAO2	AUS	DKVS ( 811 )	BBTEGA ( 750 )
Z_FRAU	AUS	DKVS ( 811 )	
Z_FRAU2	AUS	DKVS ( 811 )	
Z_FRST	AUS	DKVS ( 811 )	
Z_FRST2	AUS	DKVS ( 811 )	
Z_HLPKS_J	LOK	DKRS ( 437 )	
Z_HSH	AUS	DHLSHK (1154)	DIMC (1148), DLSAHK ( 339 ), DLSA ( 398 )
Z_HSH2	AUS	DHLSHK (1154)	DIMC (1148), DLSA ( 398 ), DLSAHK ( 339 )
Z_HSV	AUS	DHLSVK ( 29 )	DIMC (1148), DLSA ( 398 )
Z_HSV2	AUS	DHLSVK ( 29 )	DIMC (1148), DLSA ( 398 )
Z_HSVE	AUS	DHLSVKE ( 902 )	DHLSVK ( 29 )



Symbol	Type	Created within	Used within
Z_HSVE2	AUS	DHLSVKE ( 902 )	DHLSVK ( 29 )
Z_KAT	AUS	DKAT ( 361 )	DIMC ( 1148 )
Z_KAT2	AUS	DKAT ( 361 )	DIMC ( 1148 )
Z_KOSE	AUS	DKOSE ( 901 )	
Z_KPE	AUS	DEKPE ( 1020 )	
Z_KRNT	AUS	DKRNT ( 445 )	EGKE ( 409 )
Z_KROF	AUS	DKRNT ( 445 )	EGKE ( 409 )
Z_KRTP	AUS	DKRTP ( 451 )	EGKE ( 409 )
Z_KS1	AUS	DKRS ( 437 )	EGKE ( 409 )
Z_KS2	AUS	DKRS ( 437 )	EGKE ( 409 )
Z_KS3	AUS	DKRS ( 437 )	EGKE ( 409 )
Z_KS4	AUS	DKRS ( 437 )	EGKE ( 409 )
Z_LASH	AUS	DLSAHK ( 339 )	LRHK ( 781 )
Z_LASH2	AUS	DLSAHK ( 339 )	LRHK ( 781 )
Z_LATP	AUS	DLSA ( 398 )	DIMC ( 1148 ), DKAT ( 361 )
Z_LATP2	AUS	DLSA ( 398 )	DIMC ( 1148 ), DKAT ( 361 )
Z_LATV	AUS	DLSA ( 398 )	
Z_LATV2	AUS	DLSA ( 398 )	
Z_LLR	AUS	DLLR ( 578 )	
Z_LM	AUS	DHFM ( 233 )	EGFE ( 228 )
Z_LSH	AUS	DLSH ( 330 )	DIMC ( 1148 ), DLSAHK ( 339 )
Z_LSH2	AUS	DLSH ( 330 )	DIMC ( 1148 ), DLSAHK ( 339 )
Z_LSHV	EIN		DKAT ( 361 )
Z_LSV	AUS	DLSV ( 301 )	DIMC ( 1148 )
Z_LSV2	AUS	DLSV ( 301 )	DIMC ( 1148 )
Z_LUEA	AUS	DMLSE ( 34 )	
Z_LUEB	AUS	DMLSE ( 34 )	
Z_MD	AUS	DMDMIL ( 216 )	
Z_MD00	AUS	DMDMIL ( 216 )	
Z_MD01	AUS	DMDMIL ( 216 )	
Z_MD02	AUS	DMDMIL ( 216 )	
Z_MD03	AUS	DMDMIL ( 216 )	
Z_MD04	AUS	DMDMIL ( 216 )	
Z_MD05	AUS	DMDMIL ( 216 )	
Z_MD06	AUS	DMDMIL ( 216 )	
Z_MD07	AUS	DMDMIL ( 216 )	
Z_MD08	AUS	DMDMIL ( 216 )	
Z_MD09	AUS	DMDMIL ( 216 )	
Z_MD10	AUS	DMDMIL ( 216 )	
Z_MD11	AUS	DMDMIL ( 216 )	
Z_MDB	AUS	MDKOG ( 516 )	
Z_MILE	AUS	DMILE ( 36 )	
Z_MUTE	AUS	CAN ( 1124 )	
Z_N	AUS	DDG ( 141 )	
Z_NWKW	AUS	DNWKW ( 134 )	
Z_NWKW2	AUS	DNWKW ( 134 )	
Z_NWS	AUS	DNWS ( 622 )	
Z_NWS2	AUS	DNWS ( 622 )	
Z_NWSE	AUS	DNWSE ( 1025 )	
Z_PH	AUS	DPH ( 144 )	
Z_PH2	AUS	DPH ( 144 )	
Z_POEL	AUS	GGPOEL ( 296 )	
Z_PUA	AUS	BGPU ( 276 )	
Z_RKAT	AUS	DKVS ( 811 )	
Z_RKAT2	AUS	DKVS ( 811 )	
Z_RKAZ	AUS	DKVS ( 811 )	
Z_RKAZ2	AUS	DKVS ( 811 )	
Z_SLS	EIN		DIMC ( 1148 )
Z_TA	AUS	GGTFA ( 298 )	
Z_TES	AUS	DTEV ( 856 )	DIMC ( 1148 ), DLLR ( 578 )
Z_TEVE	AUS	DTEVE ( 1022 )	
Z_TM	AUS	GGTFM ( 289 )	
Z_JB	AUS	EGAG ( 486 )	GGUB ( 487 )
Z_UF2SG	AUS	DUF ( 1089 )	
Z_UFMV	AUS	DUF ( 1089 )	
Z_UFSKA	AUS	DUF ( 1089 )	
Z_JRRAM	AUS	DUR ( 1052 )	
Z_JRRAM	AUS	DUR ( 1052 )	
Z_JRRST	AUS	DUR ( 1052 )	
Z_VFZ	AUS	DVFZ ( 500 )	EGAG ( 486 ), DLLR ( 578 )
Z_VKUP	LOK	DVKUP ( 1027 )	



## Production Note

This document is concatenated from different SGML fragments. The SGML tree transformations needed have been done by the tool MetaMorphosis from Ovidius. The typesetting has been done by the typesetting system TeX using the macro package MMTeX.

Chosen (resp. default) options

Option	Value
colophon	yes
damosfile	i:\programme\mm3\..\mmapps\fdr3\lib\damos_dummy.sgm
efatable	yes
efatree	no
graphicborder	no
graphicinfo	no
inputfile	FRE07E0.SGM
lineart	fast
minlines	2
newpage	owners
pavastfile	i:\programme\mm3\..\mmapps\fdr3\lib\pavast_dummy.sgm
pavastnew	yes
pavastorig	retain